



# Certification by Analysis of Woven TPS: Fiber- and Weave-Scale Modeling

## EDL Summer Seminar

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July 6, 2023



# Acknowledgements



## Entry Systems Modeling (ESM) Project TPS Certification by Analysis

### Core Team Members

#### ARC

Justin Haskins  
Lauren Abbott  
Sergio Fraile Izquierdo  
Sander Visser  
Andrew Santos  
Federico Semeraro  
William Tucker  
Kevin Wheeler  
Vasyl Hafiychuk  
Michael von Pohle  
Karan Doss

#### GRC

Trenton Ricks  
Brett Bednarczyk  
Subodh Mital  
Pappu Murthy  
Evan Pineda

### NASA ARC

Kyle Hendrickson  
Magnus Haw  
Tane Boghozian  
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Don Ellerby  
Keith Peterson  
Todd White  
Jeremy Vander Kam

### NASA GRC

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Sadeq Malakooti  
Richard Martin

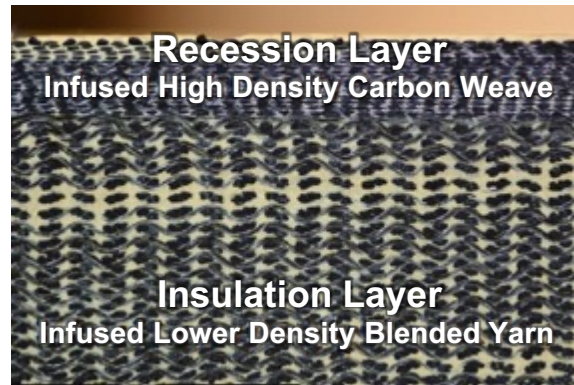
### Interns / NSTF / NSTGRO

Will Schill, Caltech  
Aaron Allred, CU Boulder  
Chloe Zeller, UMN  
Michael Olaya, U Mass Lowell  
Victoria Arias, UIUC  
Joseph Ferguson, Stanford

# Woven Thermal Protection Systems (TPS)



## Heat Shield for Extreme Entry Environment Technology (HEEET)



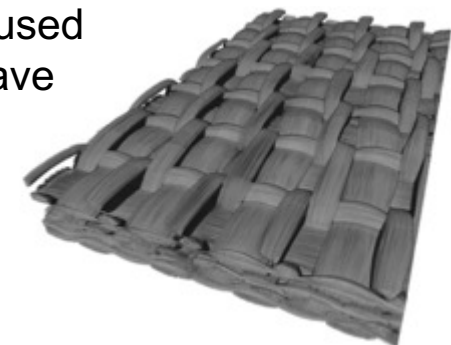
## Adaptable Deployable Entry and Placement Technology (ADEPT)



### 3D Woven Mid-Density Carbon Phenolic (3MDCP)

- Derived from HEEET insulation layer
- Mars Sample Return Earth Entry System (MSR-EES)

Uninfused Weave



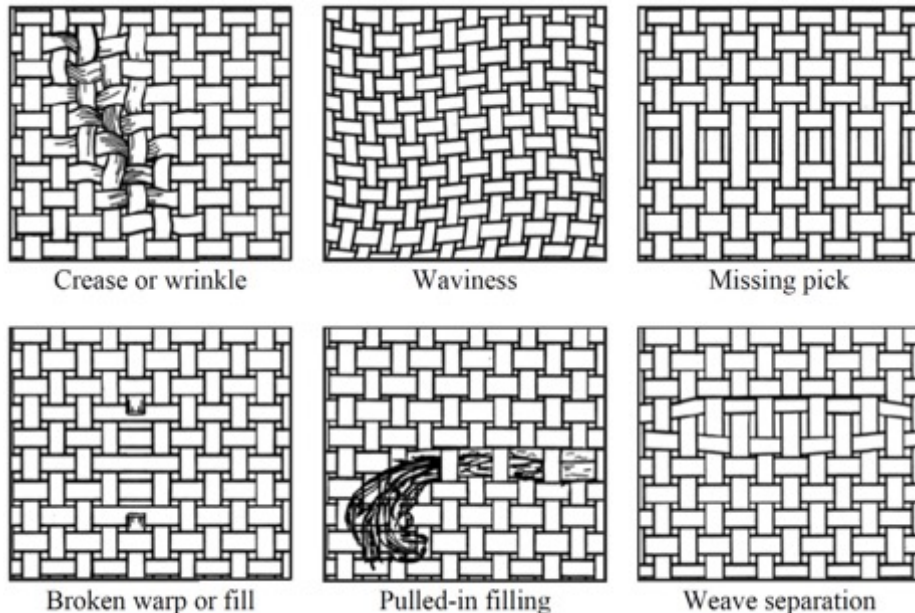
# Certification by Analysis of Woven TPS



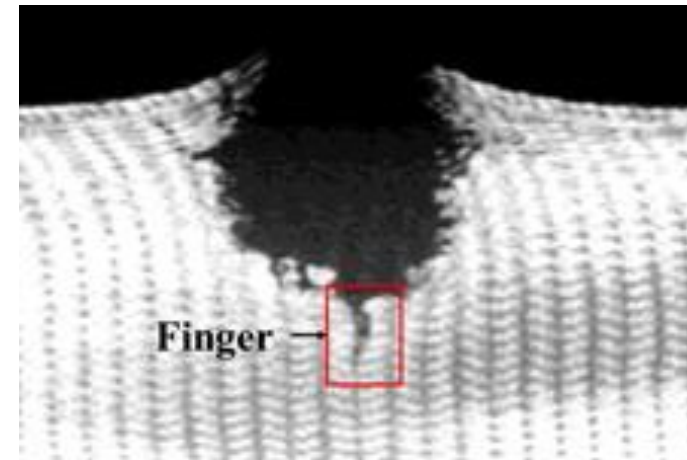
**Goal:** Develop computational tools and techniques to support certification of woven TPS materials

- Identify and characterize material features, defects, and damage
- Determine how these features/defects/damage affect properties, performance, and failure

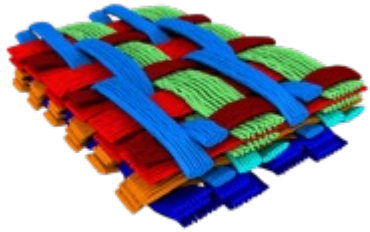
## Weave features or defects



## Impact from micrometeoroids and orbital debris (MMOD)



# TPS Certification by Analysis Thrusts

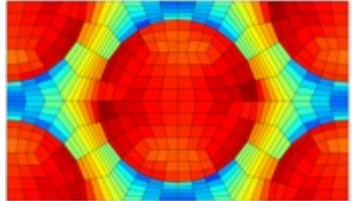


## Multiscale Materials Modeling

Ames Research Center  
Thermal Protection Materials Branch

Justin Haskins  
Lauren Abbott  
Andrew Santos  
Sergio Fraile Izquierdo

William Tucker  
Federico Semeraro  
Sander Visser

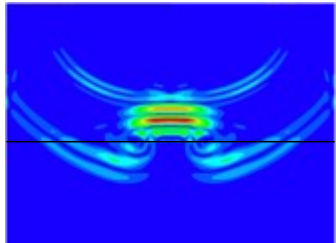


## Multiscale Materials Modeling

Glenn Research Center  
Multiscale & Multiphysics Modeling Branch

Trenton Ricks  
Brett Bednarcyk  
Subodh Mital

Pappu Murthy  
Evan Pineda



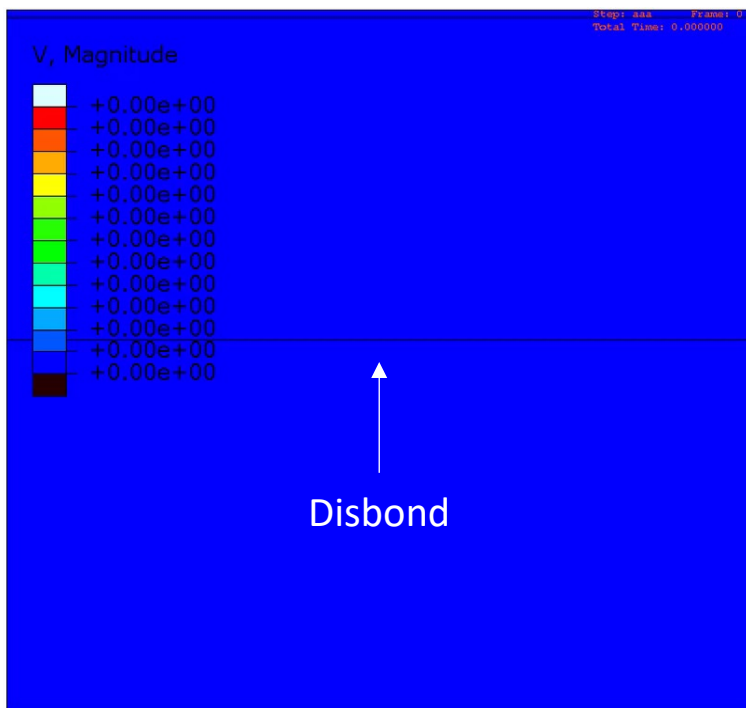
## Machine Learning and Nondestructive Evaluation

Ames Research Center  
Intelligent Systems Division

Kevin Wheeler  
Vasyl Hafiychuk

Michael von Pohle  
Karan Doss

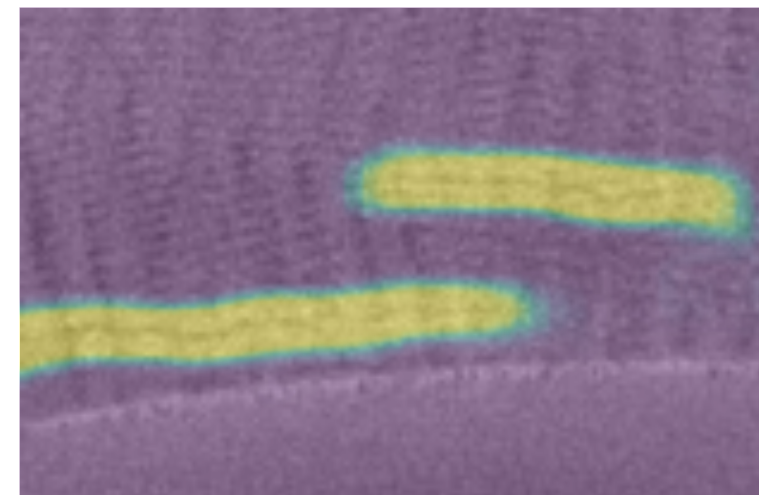
## Computational Nondestructive Evaluation (CNDE)



Detection of disbonds by ultrasonic interrogation

POC: Vasyl Hafiychuk (ARC/TI)

## Machine Learning

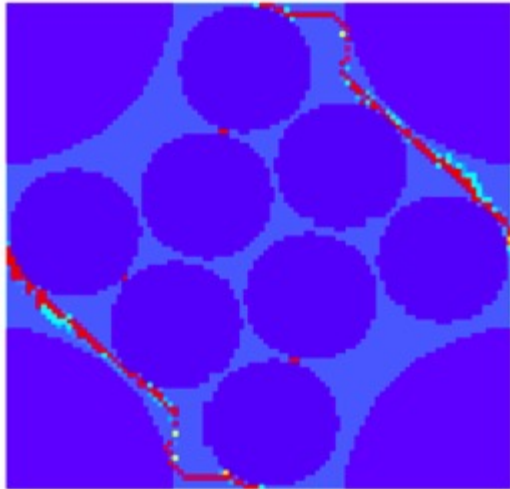


Automated detection of faults in CT scans using deep learning

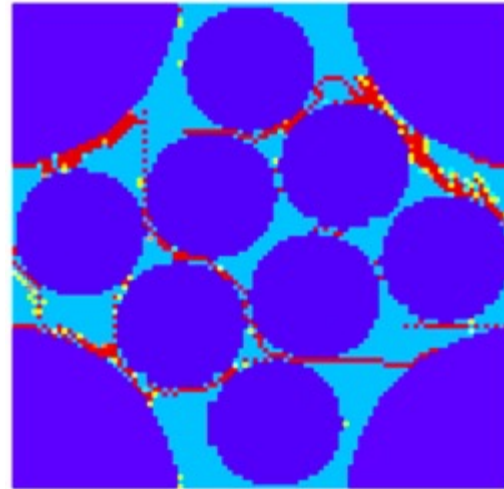
POC: Michael von Pohle (ARC/TI)

## Progressive Damage Simulations

Tensile



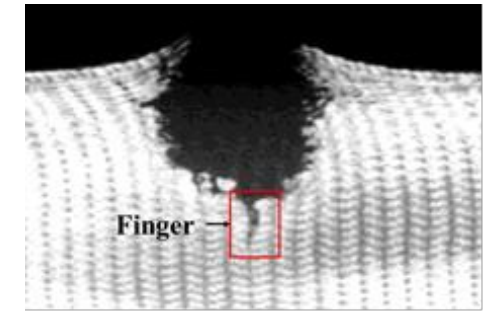
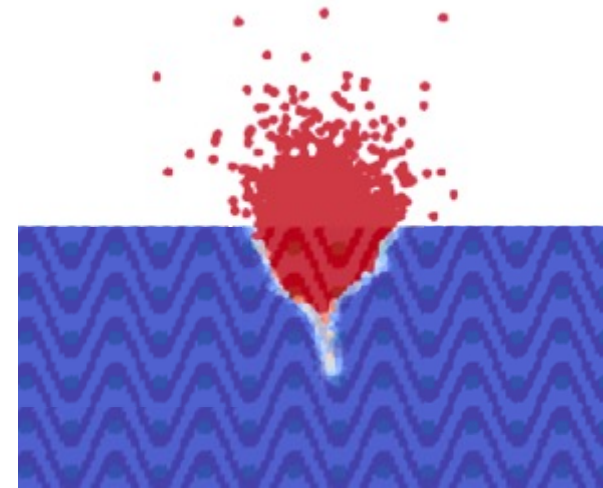
Shear



Stress damage in blended yarns using multiscale recursive micromechanics models

POC: Brett Bednarczyk (GRC)

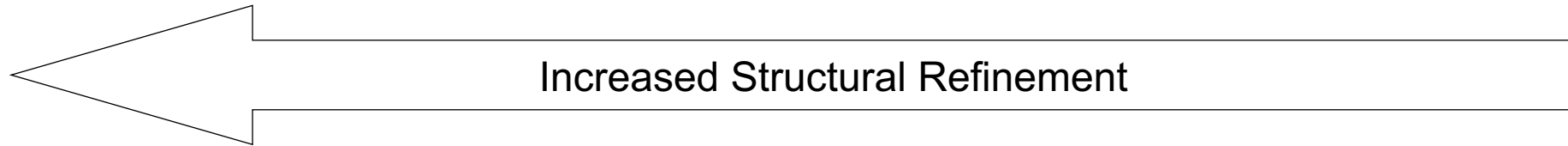
## Impact Simulations



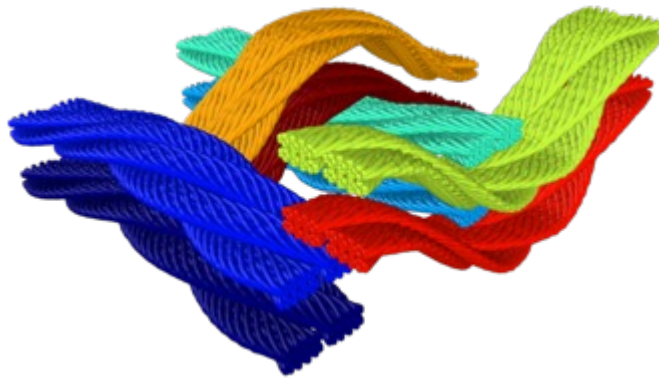
Impact damage using peridynamics simulations with microstructure representation

POC: Justin Haskins (ARC/TSM)

# Computational Materials Modeling

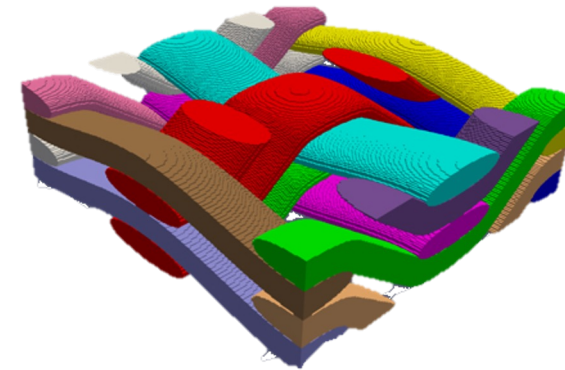


**Particle-based, discrete-element  
methods (LAMMPS, HYDRA)**

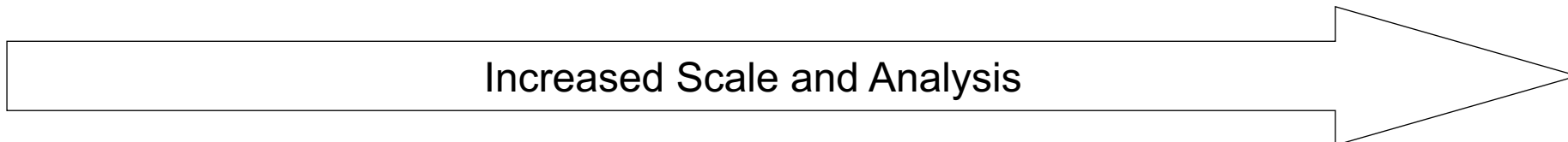


Fiber-level resolution  
Andrew P. Santos

**Porous Microstructure Analysis  
(PuMA)**



Yarn-level resolution  
Sergio Friale Izquierdo

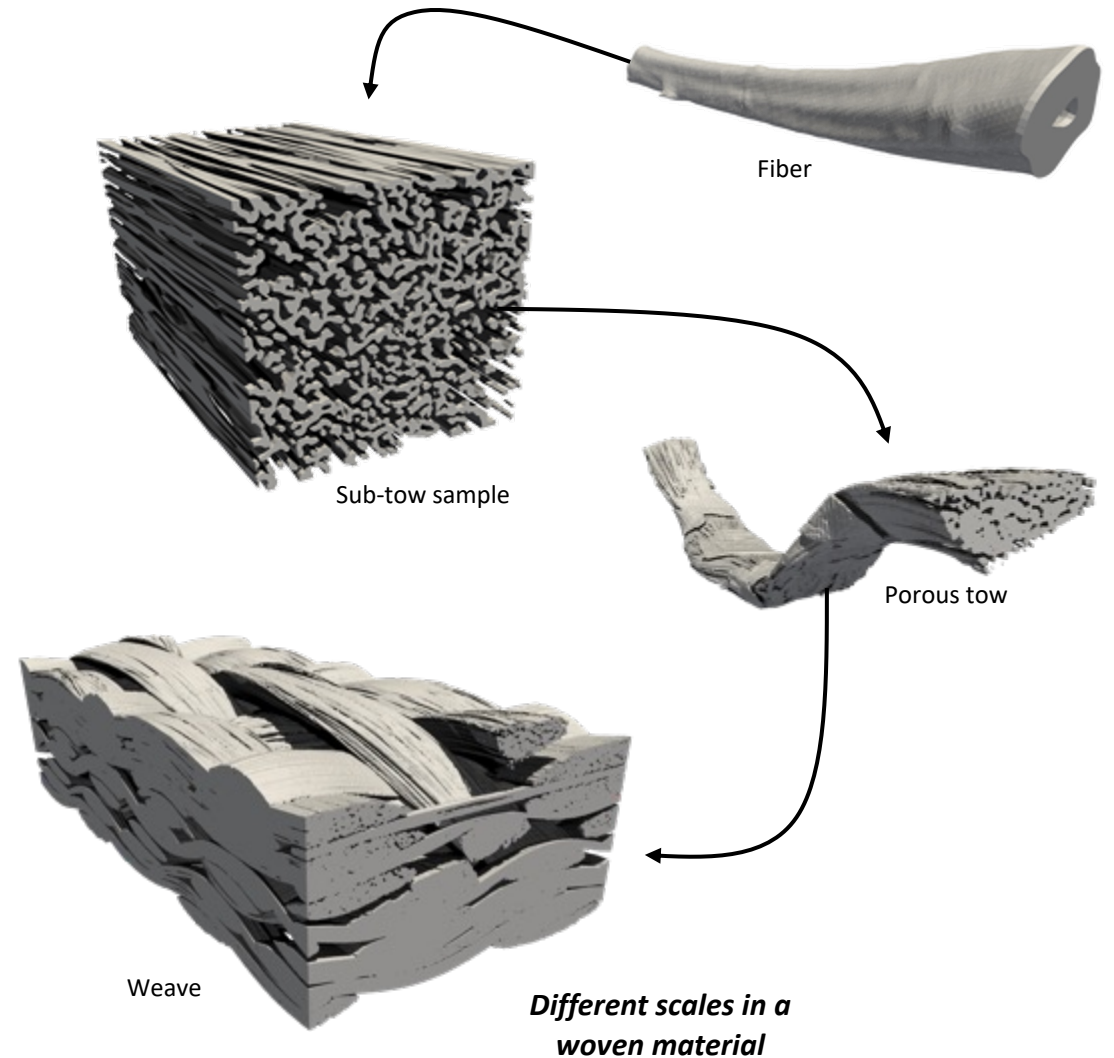




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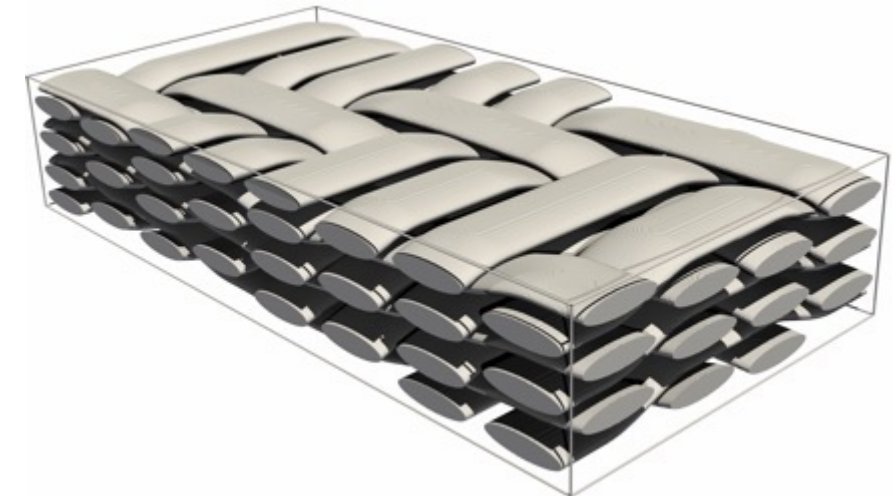
- Woven TPS Multi-scale Modeling
- Tools Overview
- Constituents Conductivity / Elasticity
  - Porous Matrix
  - Tow Modeling
- Unit Cell Conductivity / Elasticity
  - Micro-CT Data
  - Segmentation
  - Tows' Orientation
- Conclusions & Future Work



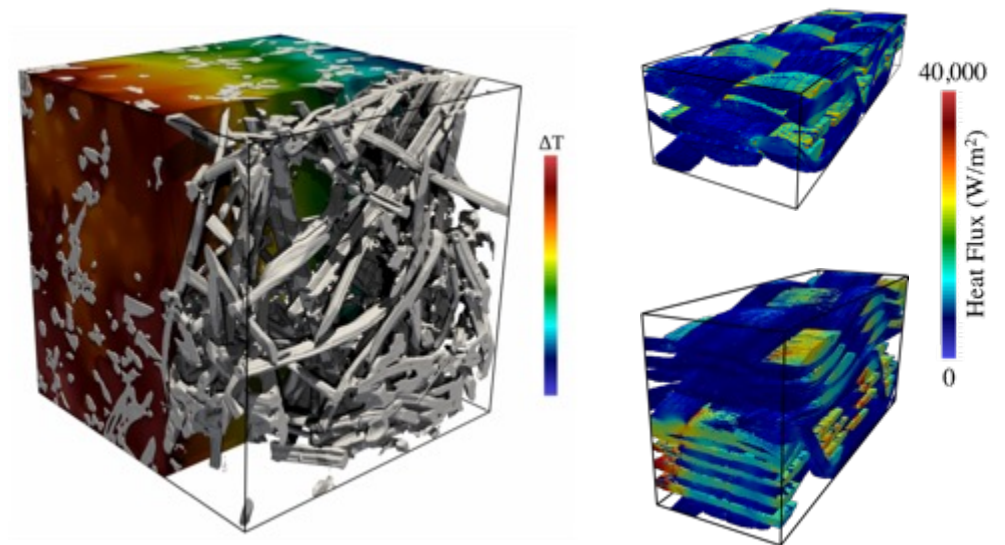
# Woven TPS Multi-scale Modeling



- In 3D woven composites, some yarns are also weaved through the thickness direction.
- Designing this type of composite for specific applications is not trivial due to the high number of design options.
- This study focuses on multi-scale modeling to obtain the mechanical properties of different 3D woven composites.
  - Modeling steps: Matrix  $\rightarrow$  Yarn  $\rightarrow$  Unit Cell
- Use of PuMA's voxel-based thermal conductivity and stress analysis solver for anisotropic materials.
  - Finite volume
  - Cell-centered discretization



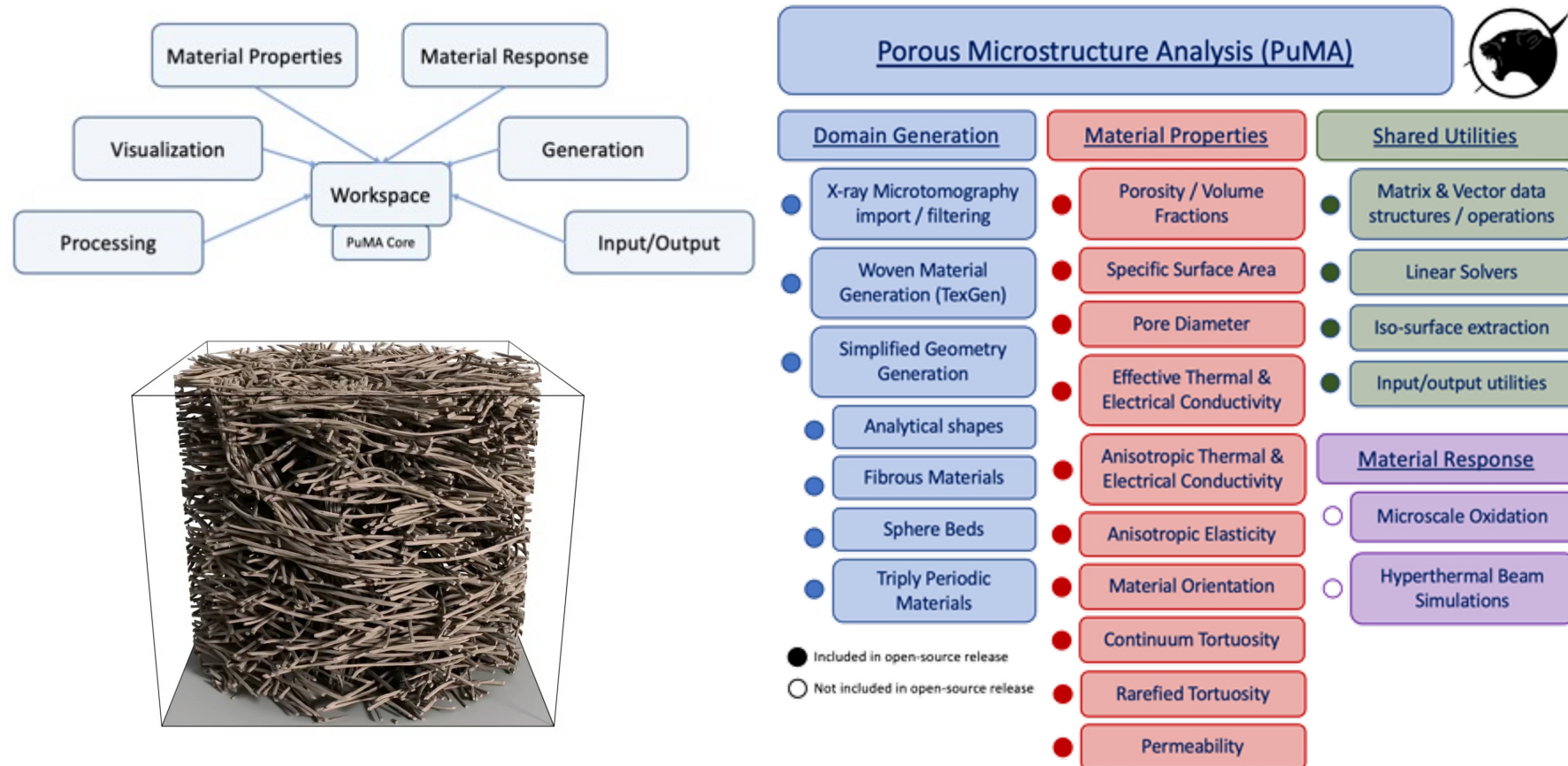
3D weave structure



Heat transfer in fibrous material

# Tools Overview: PuMA

- The PuMA software is able to either generate domains artificially or import them from micro-CT scans and compute material properties such as: porosity, specific surface area, effective thermal conductivity, pore diameter, tortuosity, permeability. It also enables the computation of mechanical properties through its anisotropic elasticity solver.



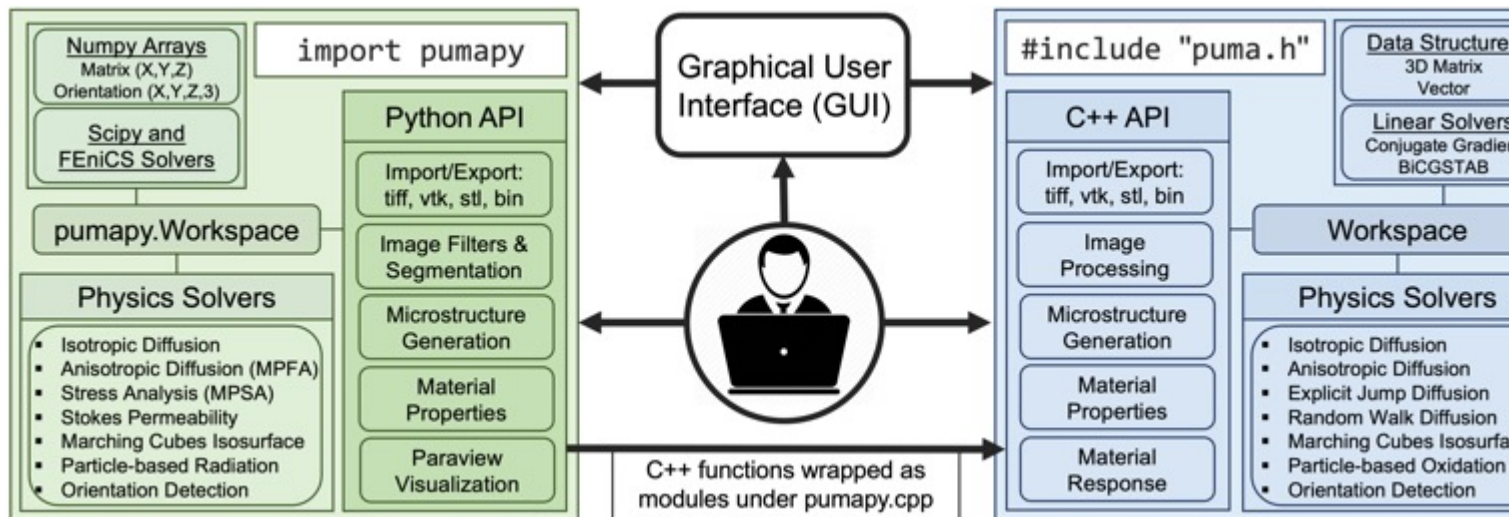
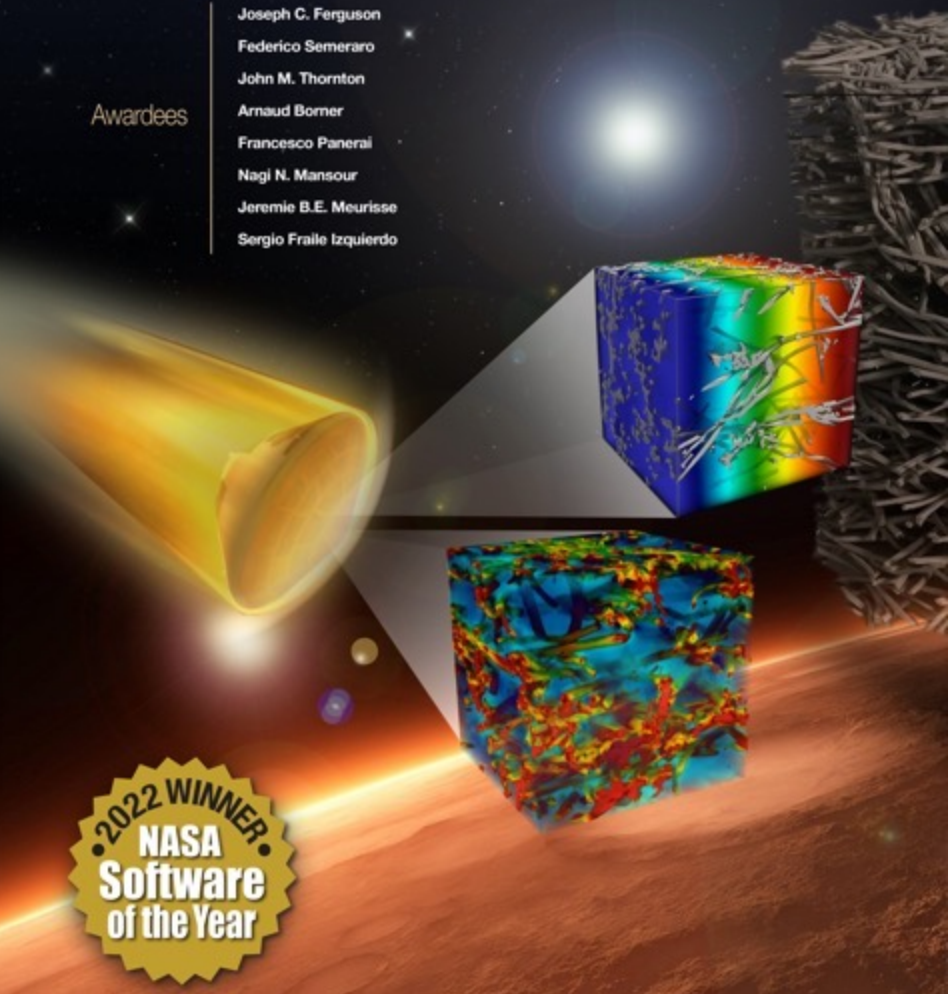
# Tools Overview: PuMA

- **Lead developers:** J.C. Ferguson and F. Semeraro
- **Installation:** `conda install -c conda-forge puma`
- **Open-source repository:** <https://github.com/nasa/puma>
- **Documentation:** <https://puma-nasa.readthedocs.io>
- **Community chat:** <https://gitter.im/puma-nasa/community>
- **Tutorials:** [YouTube](#) channel and [Colab notebook](#)

# PuMA

**Porous Microstructure Analysis**

- Awardees
- Joseph C. Ferguson
  - Federico Semeraro
  - John M. Thornton
  - Arnaud Borner
  - Francesco Panerai
  - Nagi N. Mansour
  - Jeremie B.E. Meurisse
  - Sergio Fraile Izquierdo

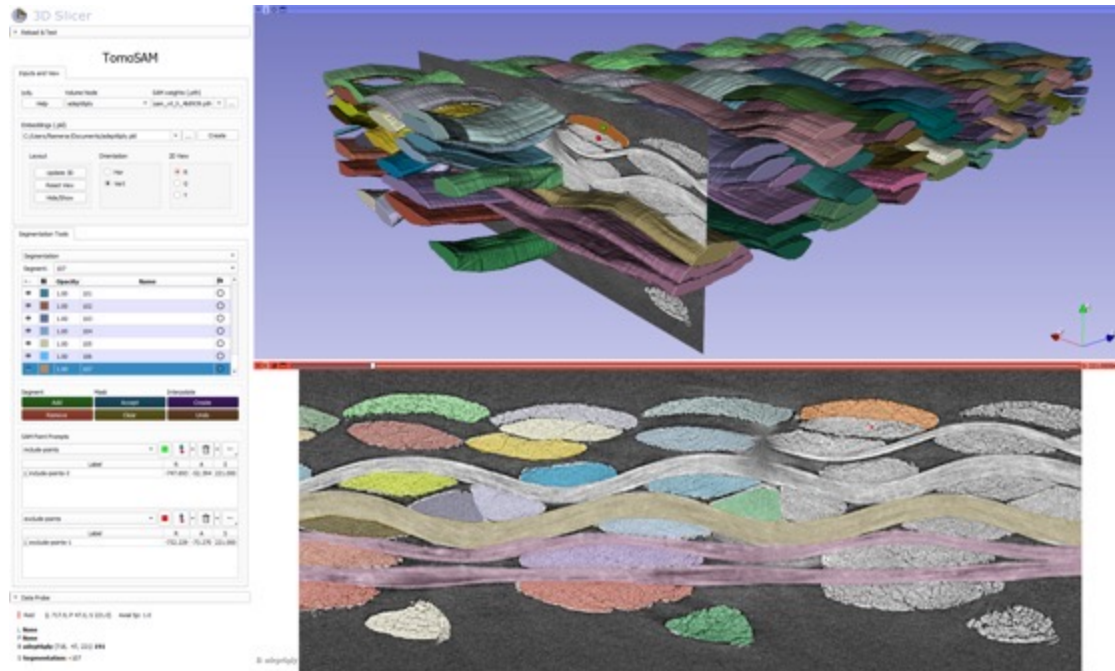


*PuMA architecture diagram*

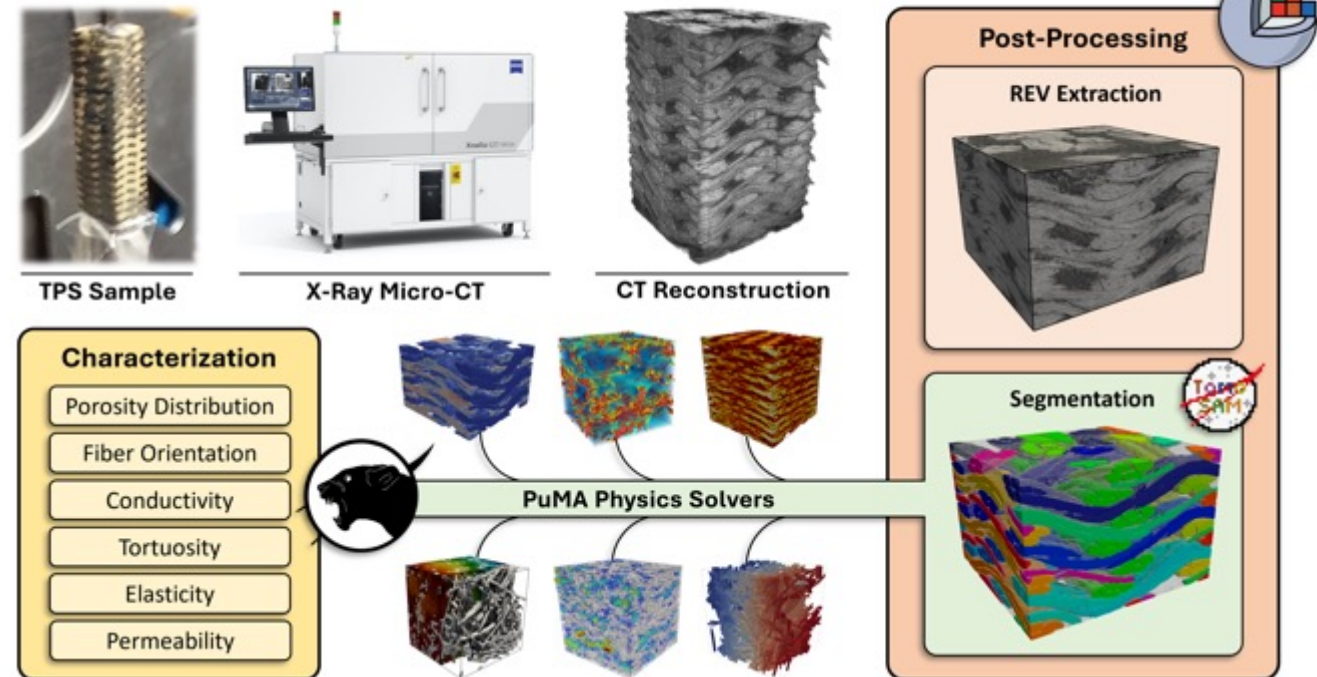
# Tools Overview: TomoSAM



- An extension of 3D Slicer using the Segment Anything Model (SAM) from Meta to aid the segmentation of 3D data from tomography or other imaging techniques.
- **Lead developers:** F. Semeraro
- **Open-source repository:** <https://github.com/fsemerar/SlicerTomoSAM>



TomoSAM graphical user interface



Micro-CT workflow diagram

# Porous Matrix Modeling: Elasticity



Fully dense isotropic phenolic resin:  $E = 4.5 \text{ GPa}$ ,  $\nu = 0.30$

Random intersecting spherical pores:  $\Phi = 0.0 / 0.2 / 0.4 / 0.6$

Pore diameter sensitivity study: 4 – 20 voxels

Domain: 100 x 100 x 100 voxels

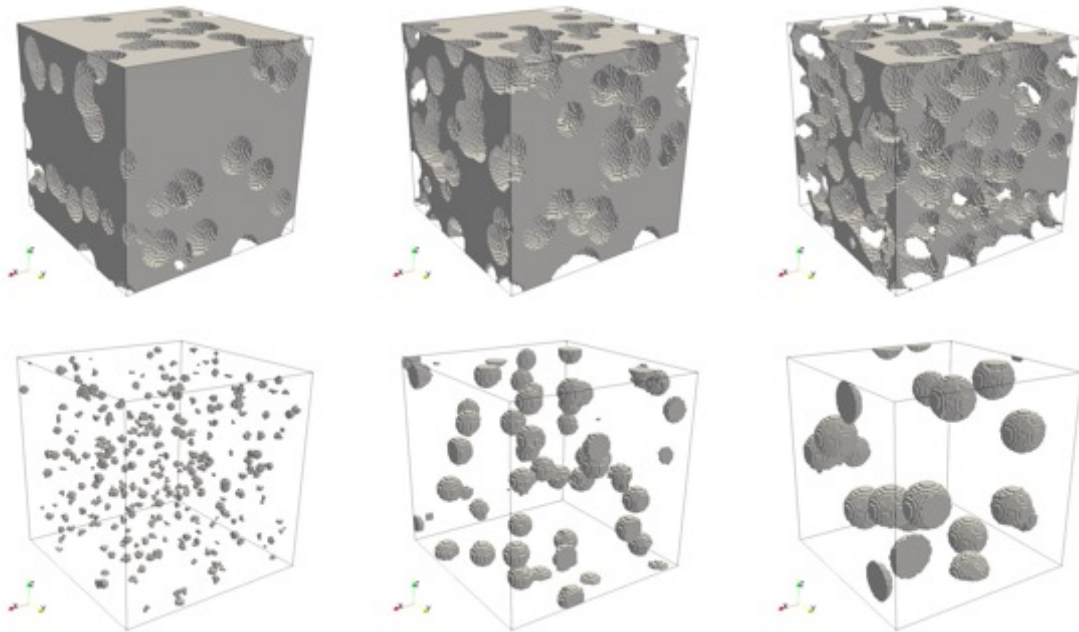


Fig.5 - Voxelized models of porous resin matrix (top) and different pore sizes (bottom)

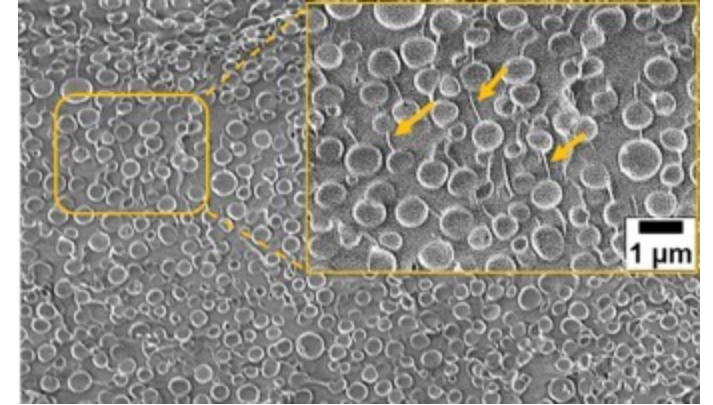


Fig.6 - Micrograph of cured porous phenolic resin [3]

Results compared with semi-empirical equations found in the literature:

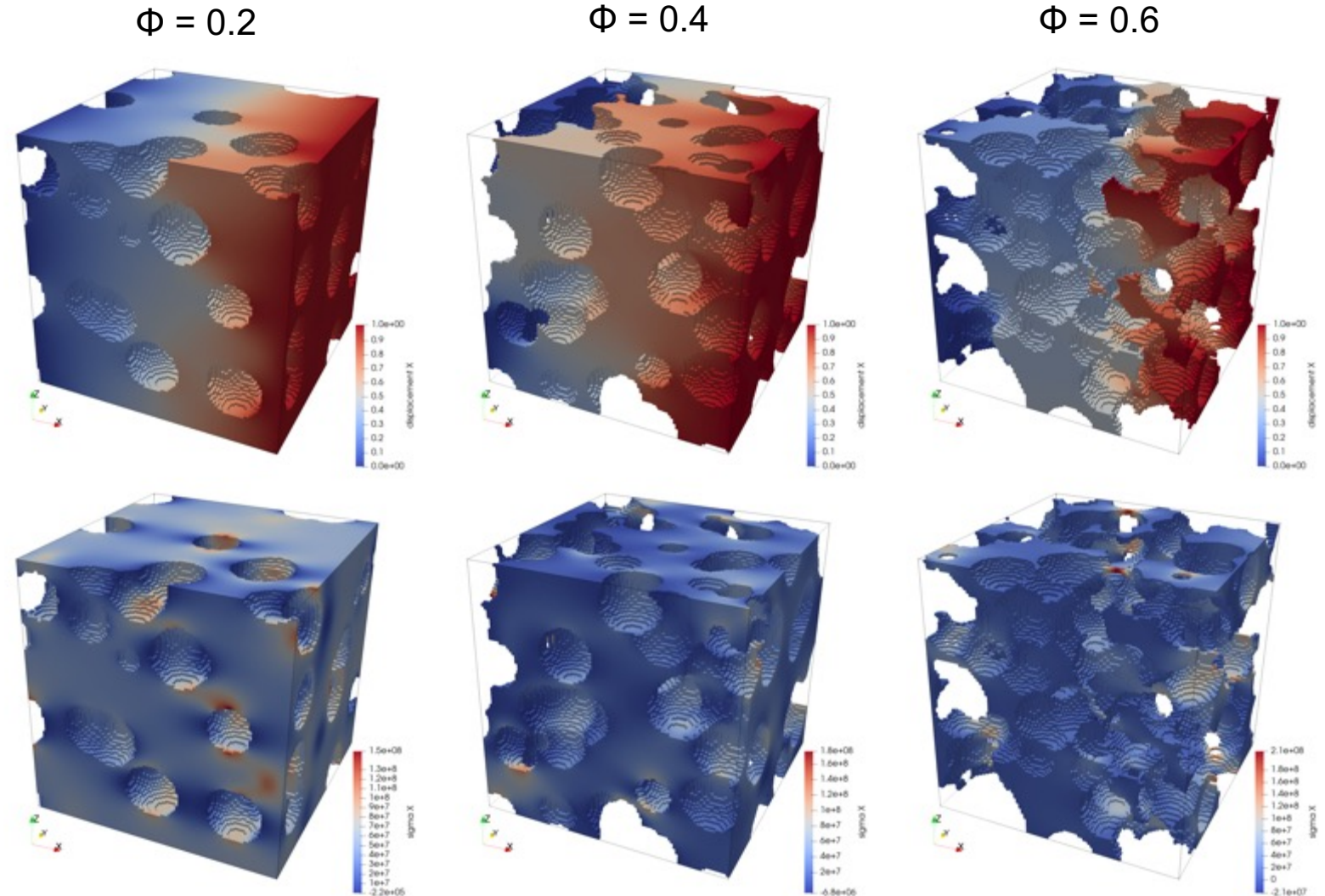
- Bert: solid with spherical pores following a hexagonal distribution,  $\phi_{max} = 0.7405$  and  $c = 2 \phi_{max}$  [4]
- Roberts: solid with random overlapping spherical pores,  $\phi_{max} = 0.818$  and  $c = 1.65$  [5]

$$E_{\phi} = E_0 \left( 1 - \frac{\phi}{\phi_{max}} \right)^c$$

# Porous Matrix Modeling: Elasticity



- Pore diameter of the simulations shown:  $D = 16$  voxels
- Assumed isotropic material
- RVE homogenization method:
  - Model's face in XY plane fixed
  - Displacement of 1 voxel in +X
  - Symmetry BC in the other 4 faces
- Top: Displacement field (X)
- Bottom: Direct stress field (X)

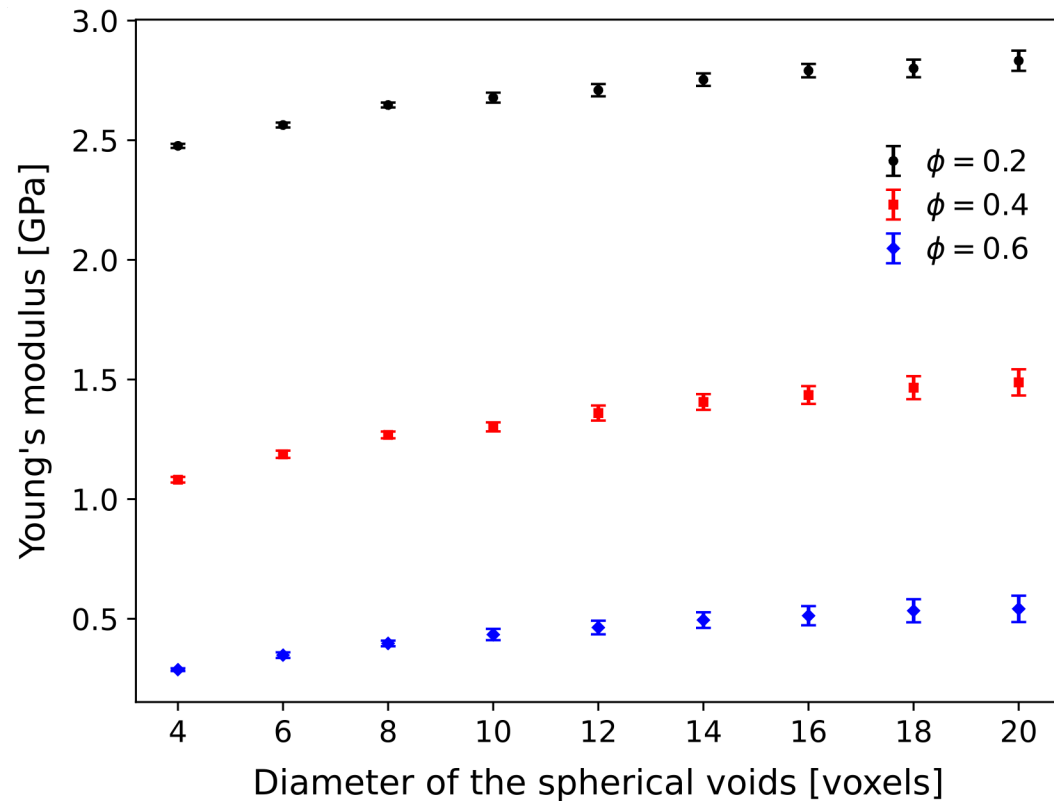


Displacement field (top) and direct stress field (bottom) in the X direction

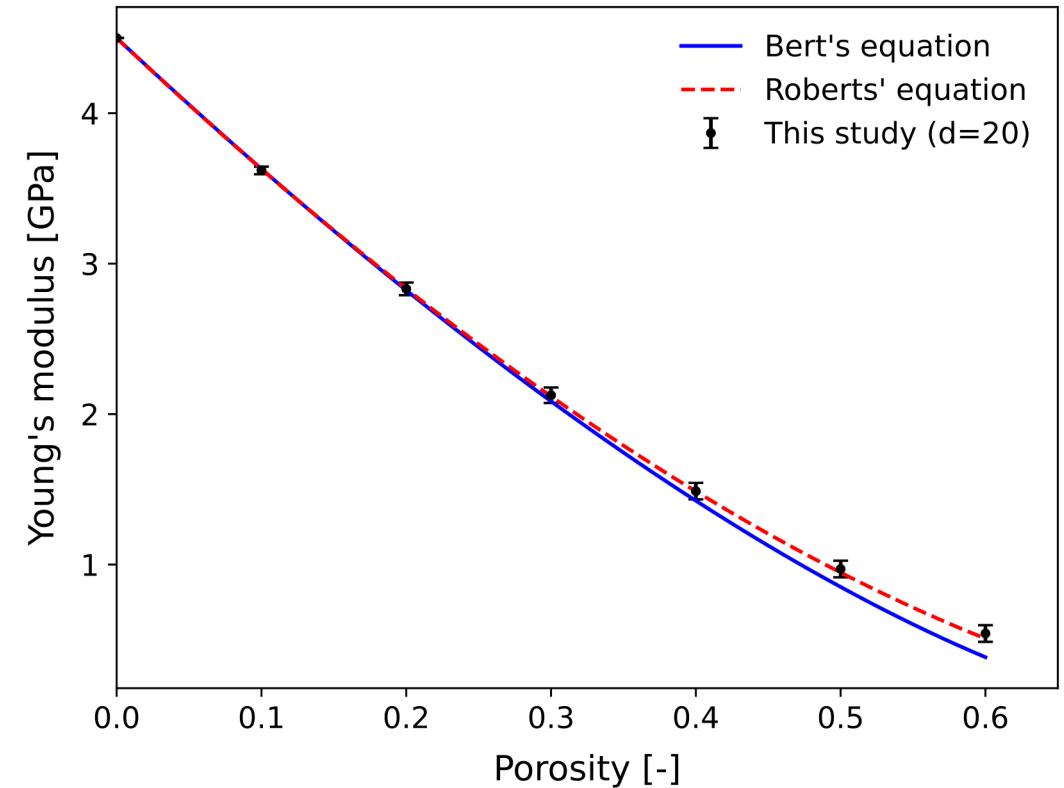
# Porous Matrix Modeling: Elasticity



- 9 pore diameters analyzed, up to 30 simulations each to minimize the random generation uncertainty.
- Pore diameter selected for this study:  $d = 20$  voxels.
- Great agreement with Robert's equation.



Young's moduli for different pore diameters and porosities



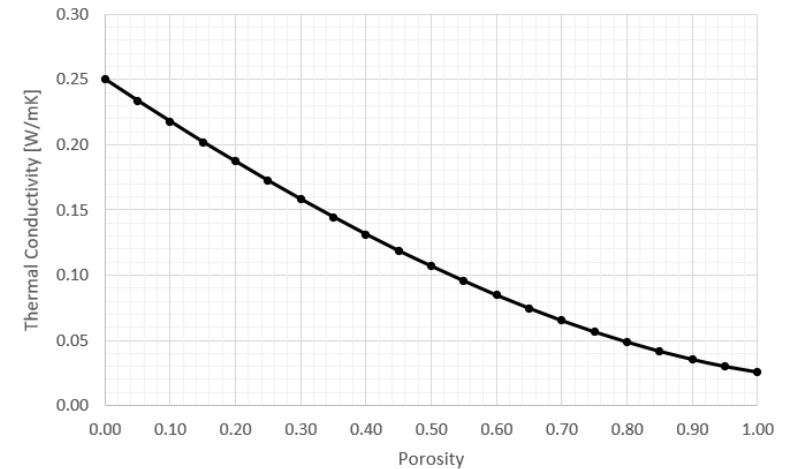
Young's moduli comparison for different porosities



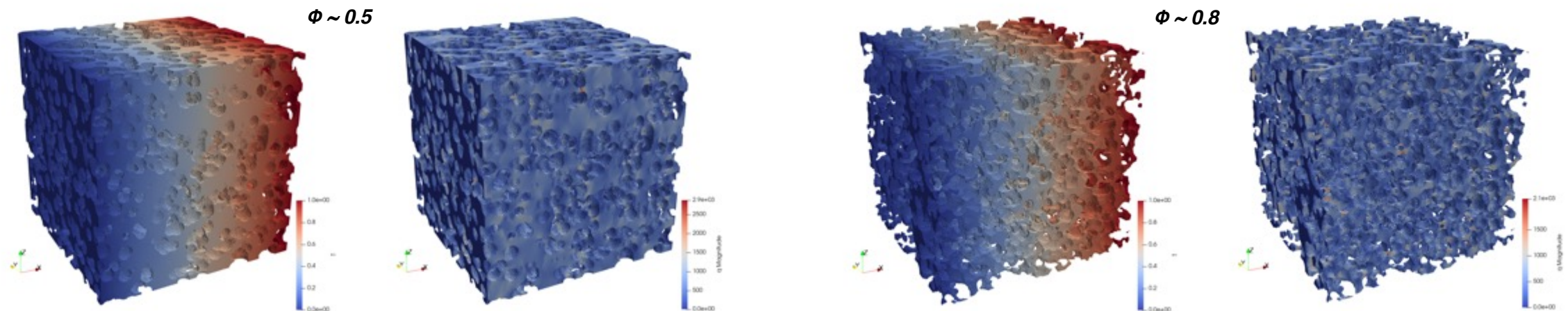
# Porous Matrix Modeling: Thermal Conductivity



- Porous phenolic model generated via random intersecting spherical voids.
- Fully dense isotropic phenolic resin (SC-1008):  $k = 0.25 \text{ W/mK}$
- Pores filled with air:  $k = 0.0257 \text{ W/mK}$
- Pore diameter = 20 voxels
- Domain =  $300 \times 300 \times 300$  voxels
- Multiple simulations  $\Phi = [0 - 1]$



*Phenolic resin thermal conductivity as function of porosity (PuMA)*



*Temperature and heat flux fields for different porosity values*

# Tow Modeling: Artificially Generated – Elasticity



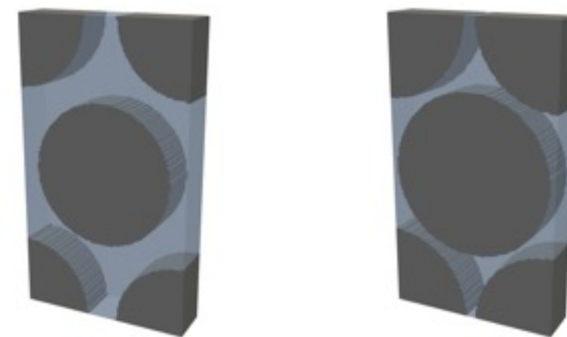
**Yarns made of carbon and porous phenolic resin (hex distribution).**

**Porous phenolic:** mechanical properties from this study,  $\Phi = 0.0 - 0.6$

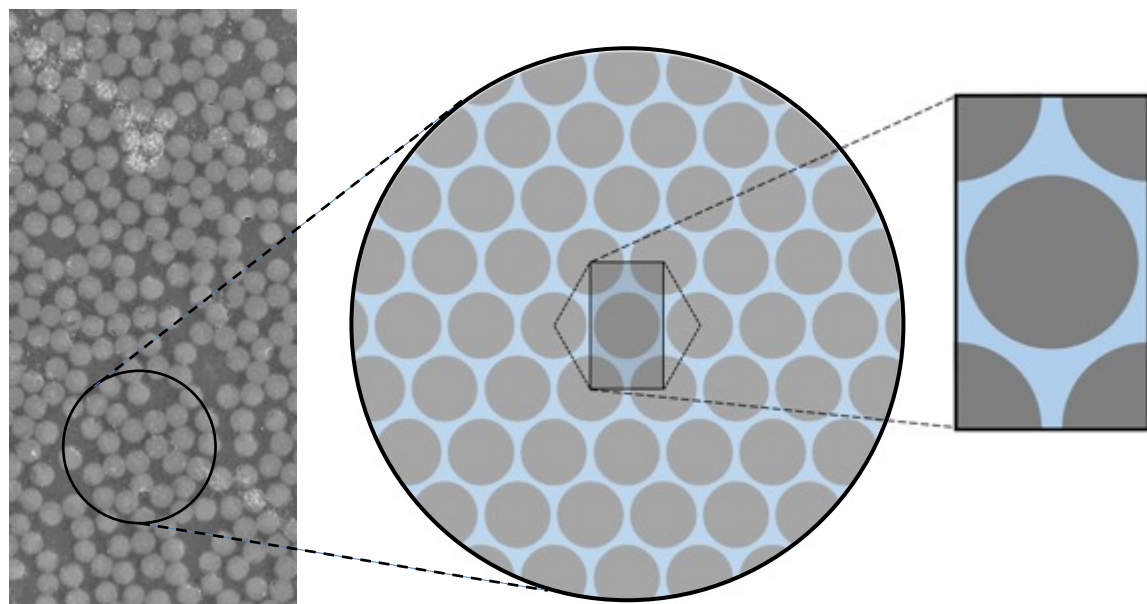
**Carbon fibers:**  $E_L = 230$  GPa,  $E_T = 15$  GPa,  $\nu_{LT} = 0.20$ ,  $\nu_{TT} = 0.20$

**Fiber volume fraction in tow:**  $V_f = 0.5 / 0.6 / 0.7 / 0.8$

**Domain:**  $25 \times 100 \times 173$  voxels



Voxelized tow models,  $V_f = 0.6, 0.8$



Micrograph of carbon fibers [6]

**Results compared with theoretical and semi-empirical equations found in the literature:**

- Rule of Mixtures (ROM): good approximation for  $E_L$  and  $\nu_{LT}$
- Halpin-Tsai: better approximation of  $E_T$  than ROM with empirical parameter for hex distribution  $\xi = 1$  ( $\eta = 1$ ) [7]
- Nielsen: modified Halpin-Tsai equation with maximum fiber packing parameter  $\eta = 0.907$  [8]
- Chamis: widely used due its simplicity and greater accuracy compared to ROM [9]

# Tow Modeling: Artificially Generated – Elasticity



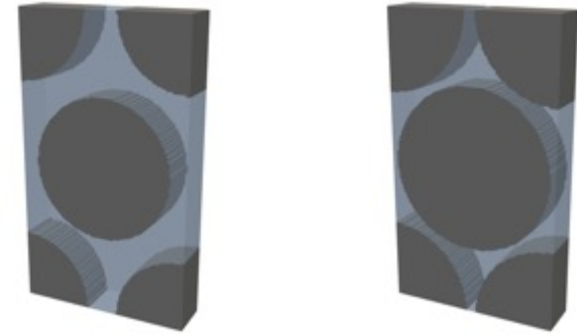
**Yarns made of carbon and porous phenolic resin (hex distribution).**

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**Domain:**  $25 \times 100 \times 173$  voxels



Voxelized tow models,  $V_f = 0.6, 0.8$

ROM  $E_L = E_{fL}V_f + E_mV_m$   $\nu_{LT} = \nu_{fLT}V_f + \nu_mV_m$

Halpin-Tsai  
Nielsen  $E_T = E_m \frac{1 + \xi\eta V_f}{1 - \psi\eta V_f}$  where,  $\eta = \frac{r-1}{r+\xi}$   $r = \frac{E_{fT}}{E_m}$

Chamis  $E_T = \frac{E_m}{1 - \sqrt{V_f} \left(1 - \frac{E_m}{E_{fT}}\right)}$

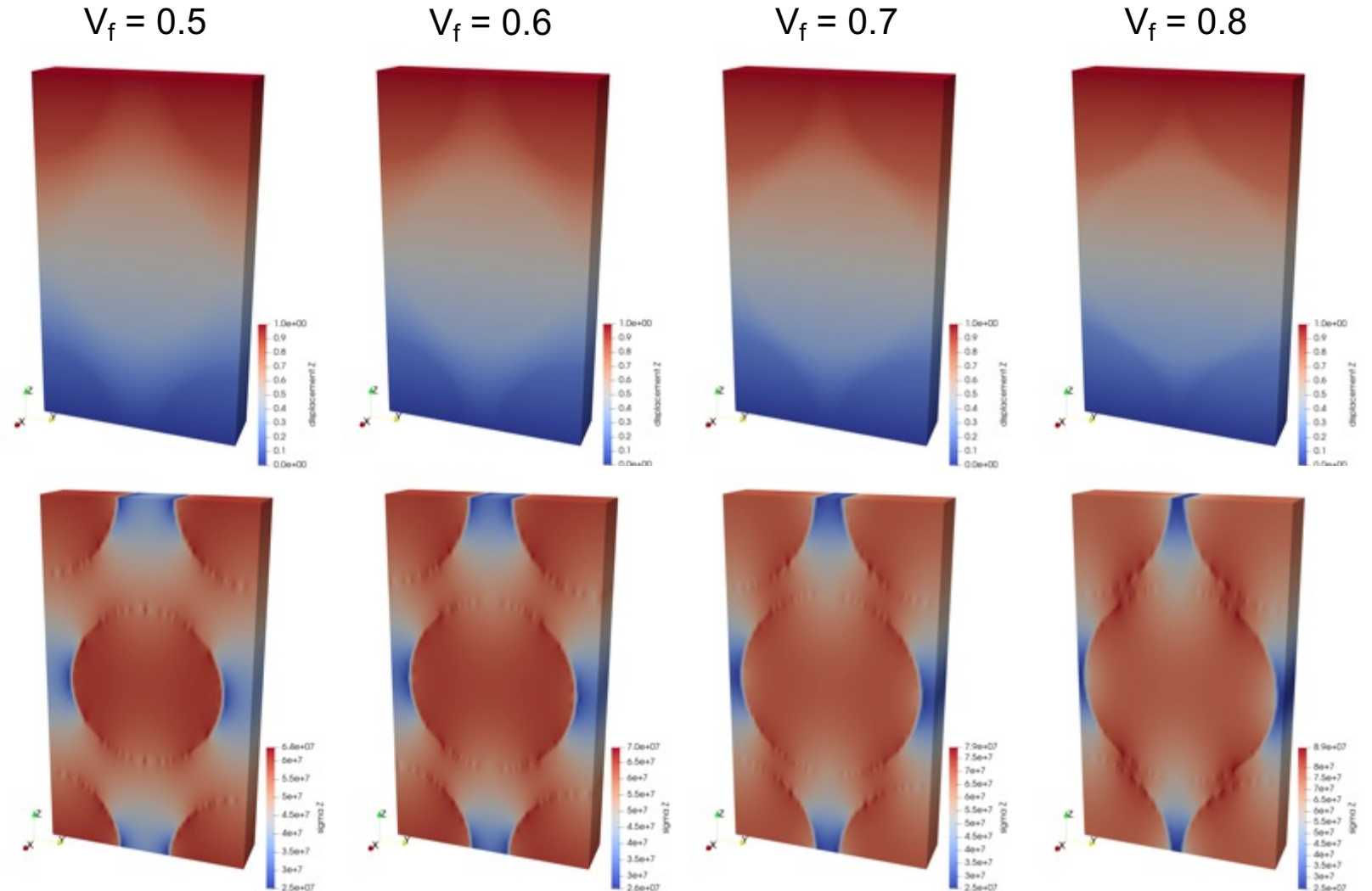
## Results compared with theoretical and semi-empirical equations found in the literature:

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- Halpin-Tsai: better approximation of  $E_T$  than ROM with empirical parameter for hex distribution  $\xi = 1$  ( $\eta = 1$ ) [7]
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# Tow Modeling: Artificially Generated – Elasticity



- Fully dense phenolic matrix for the simulations shown.
- RVE homogenization method:
  - Model's face in XY plane fixed
  - Displacement of 1 voxel in +Z
  - Periodic BC in the other 4 faces
- Top: Displacement field (Z)
- Bottom: Direct stress field (Z)



Displacement field (top) and direct stress field (bottom) in the Z direction

# Tow Modeling: Artificially Generated – Elasticity



- Halpin-Tsai shows the best agreement with the results from PuMA for  $E_T$

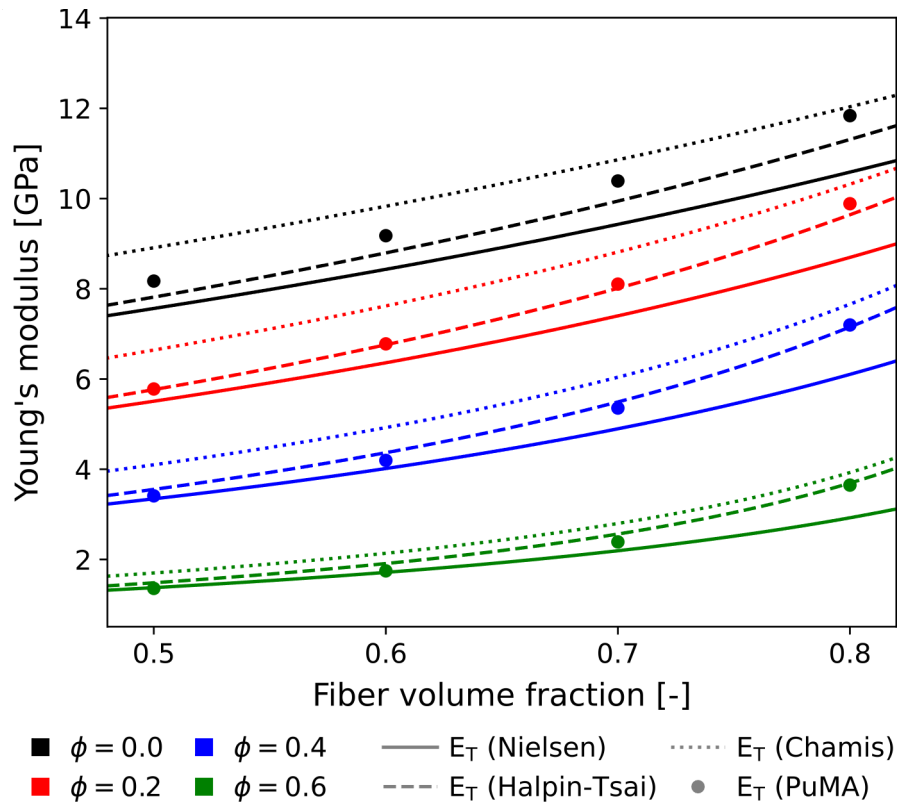


Fig.16 - Yarns Transverse Young's modulus

- ROM shows great agreement with results from PuMA for  $E_L$  and  $\nu_{LT}$

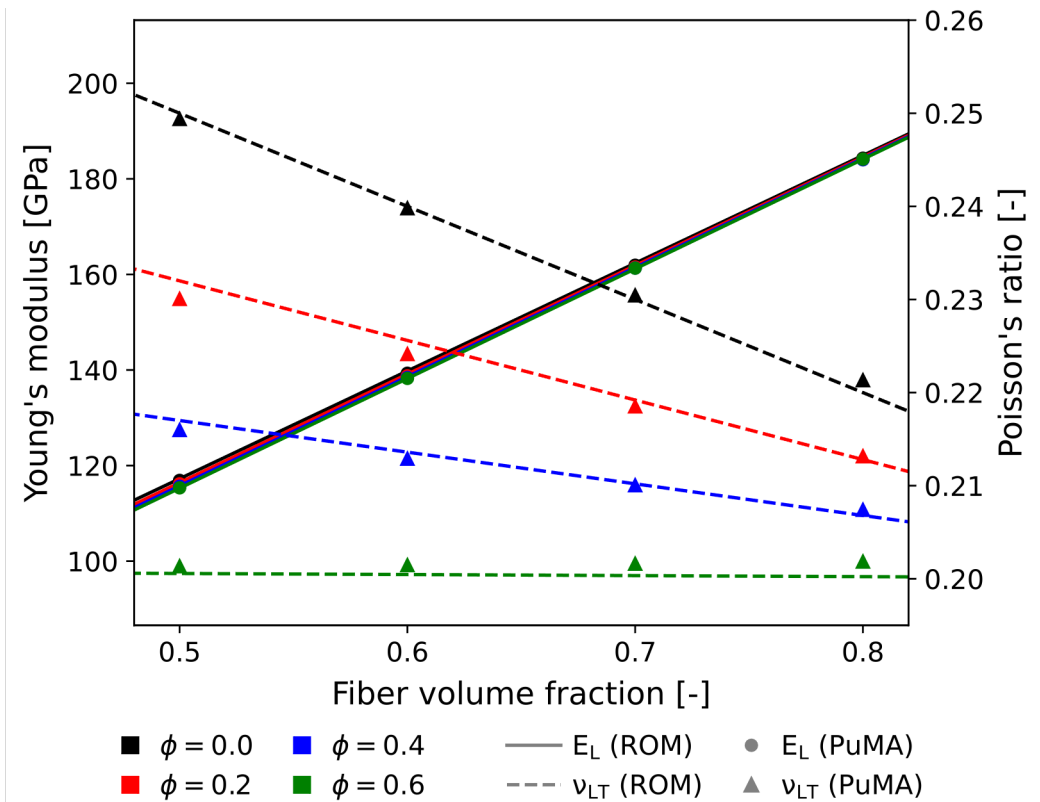
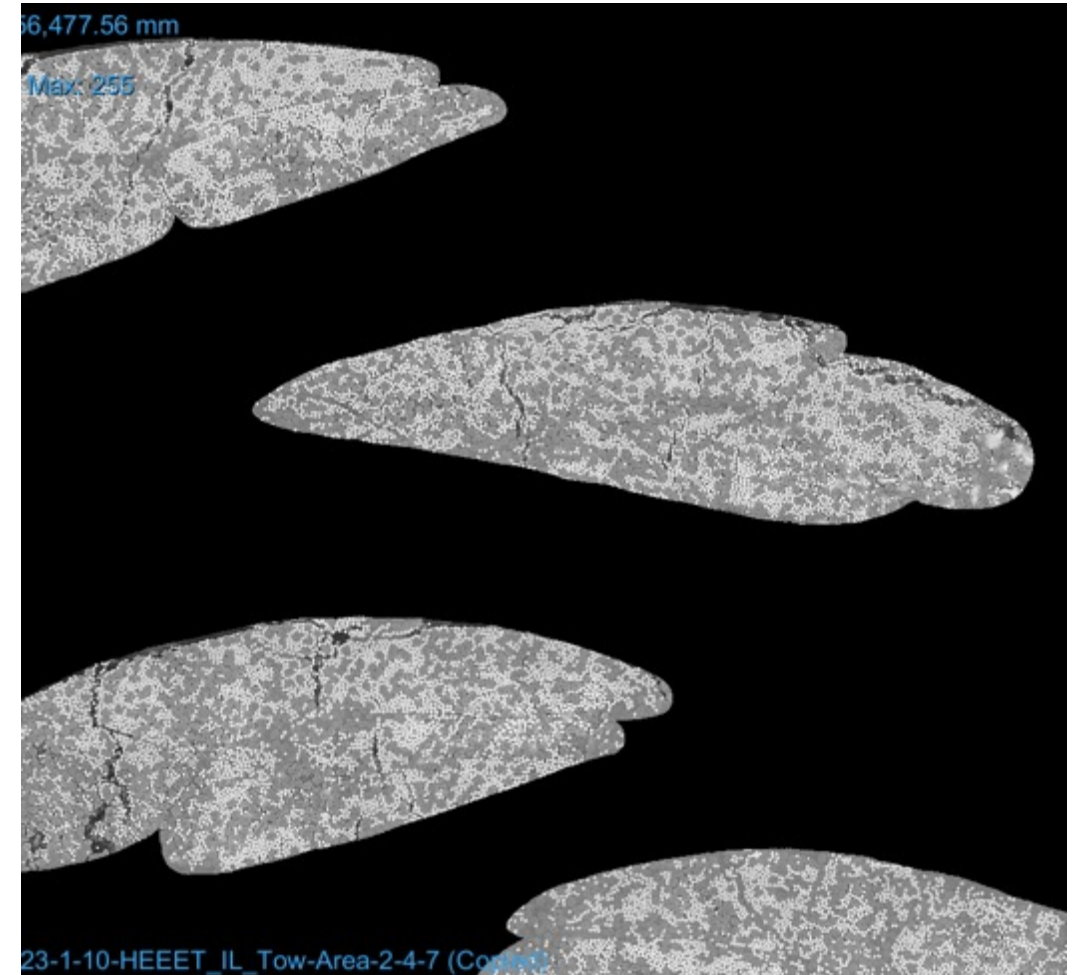


Fig.17 - Longitudinal Young's modulus and Poisson's ratio

# Tow Modeling: Microscopy – Thermal Conductivity

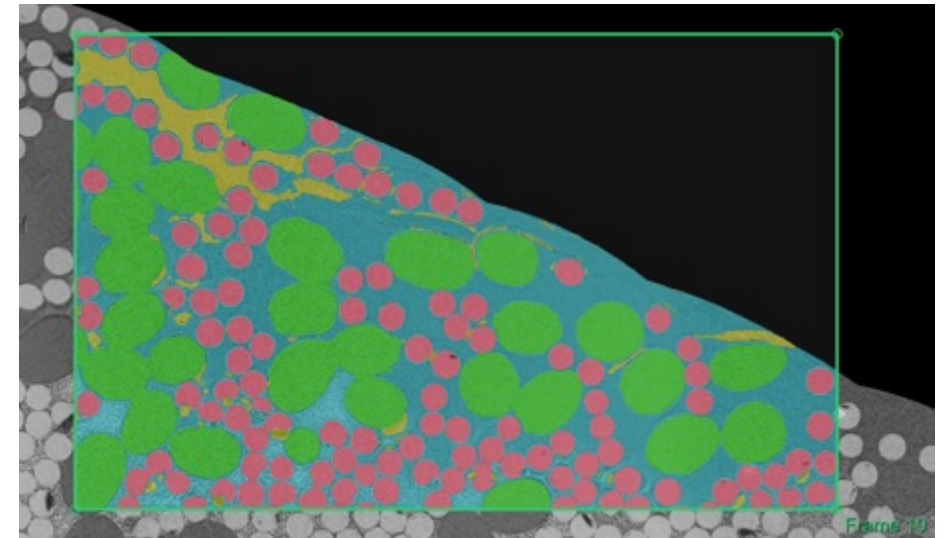
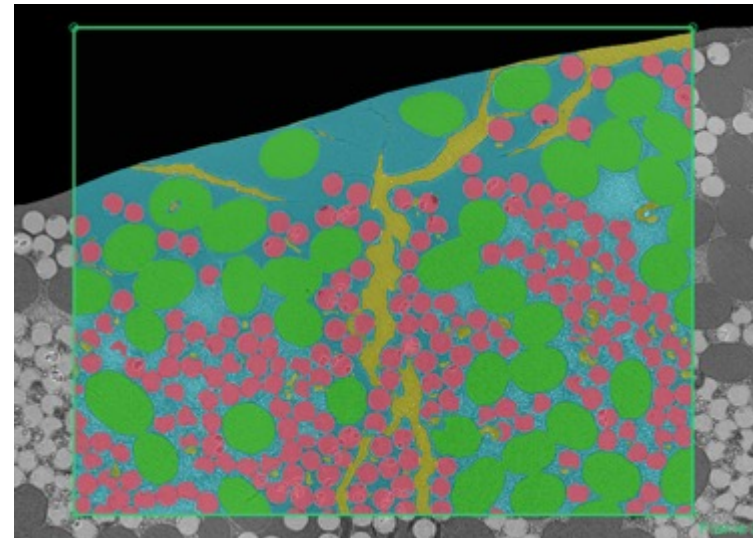
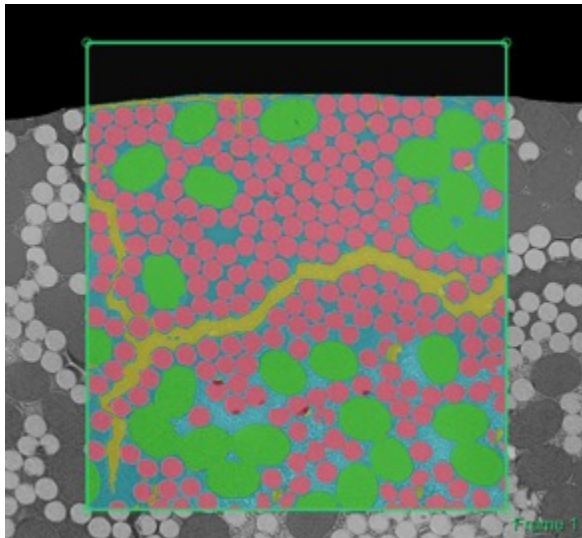
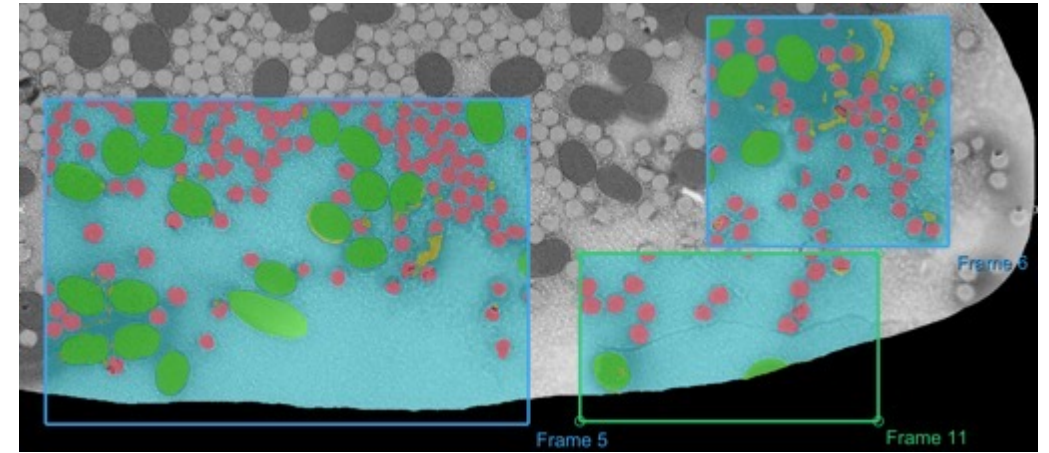
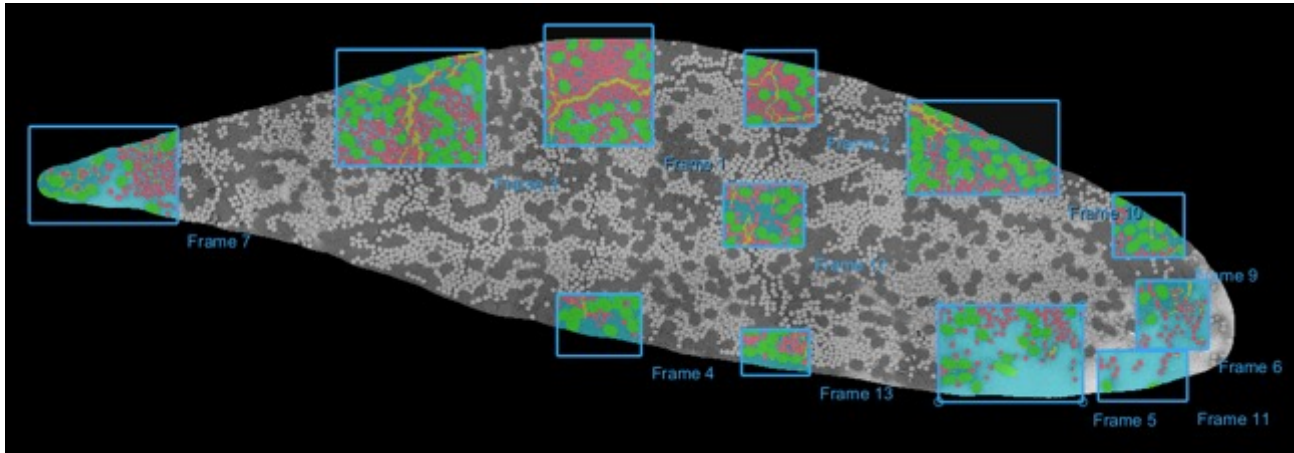


- Segmentation of HEEET-IL microscopy images is important to obtain more accurate material properties and composition data of the TPS constituents.
- A UNet CNN was trained to automate the segmentation process leveraging Dragonfly's Deep Learning capabilities.
- Approach followed for the segmentation:
  - Mask out the in-plane tows to clean up the images and train the UNet CNN only with the through-thickness tows.
  - Segment manually a few regions to start training the UNet CNN and use the initial model's predictions to help with the segmentation of additional regions.
  - Correct the segmentation of the predicted labels and continue training the UNet model with the new data.
  - Continue the process with different microscopy images to generate additional training data.



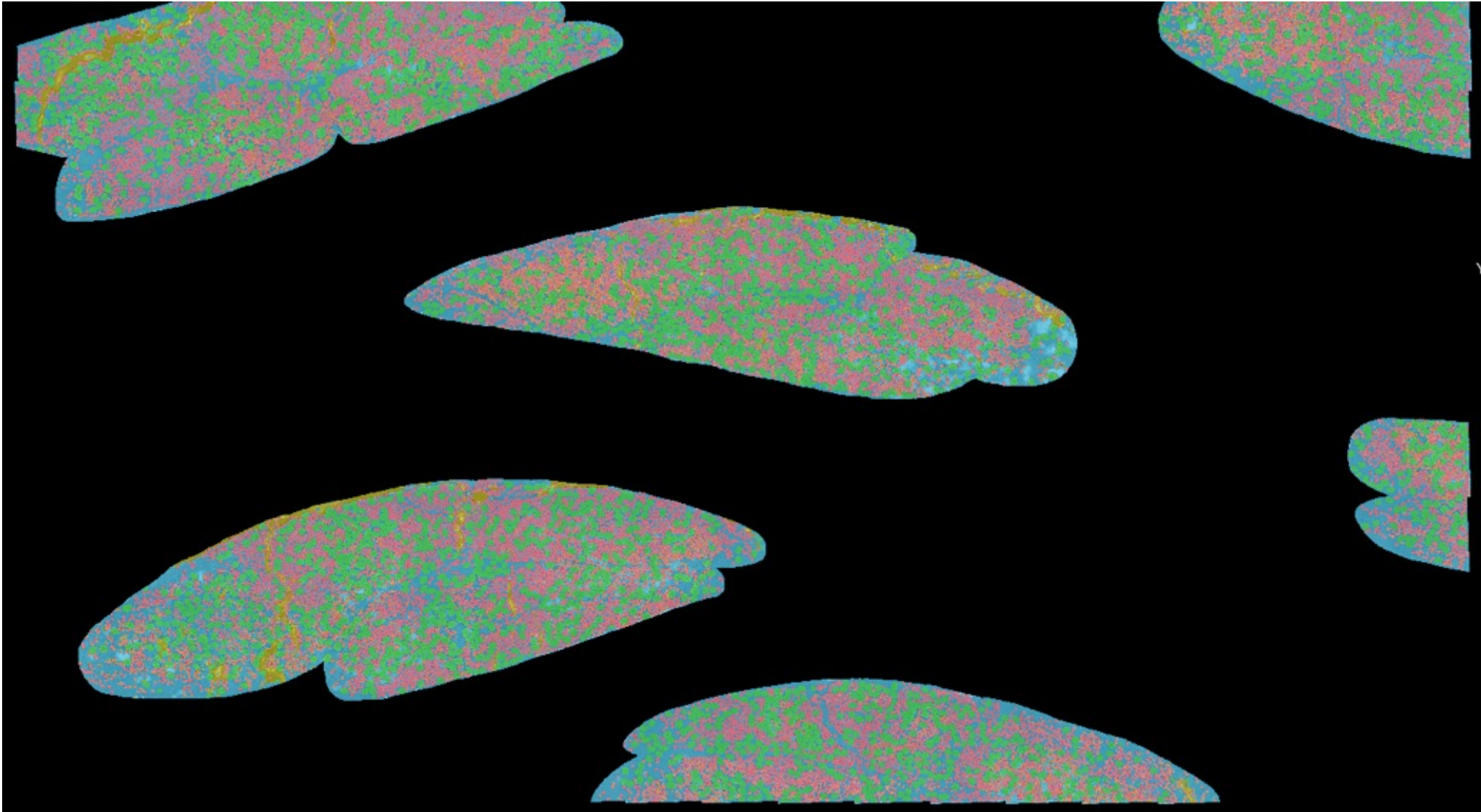
HEEET-IL microscopy image (NASA-GRC) through the steps of masking out the in-plane tows

# Tow Modeling: Microscopy – Thermal Conductivity



Selection of regions segmented of the HEET-IL microscopy image (NASA-GRC) to train the UNet CNN

# Tow Modeling: Microscopy – Thermal Conductivity



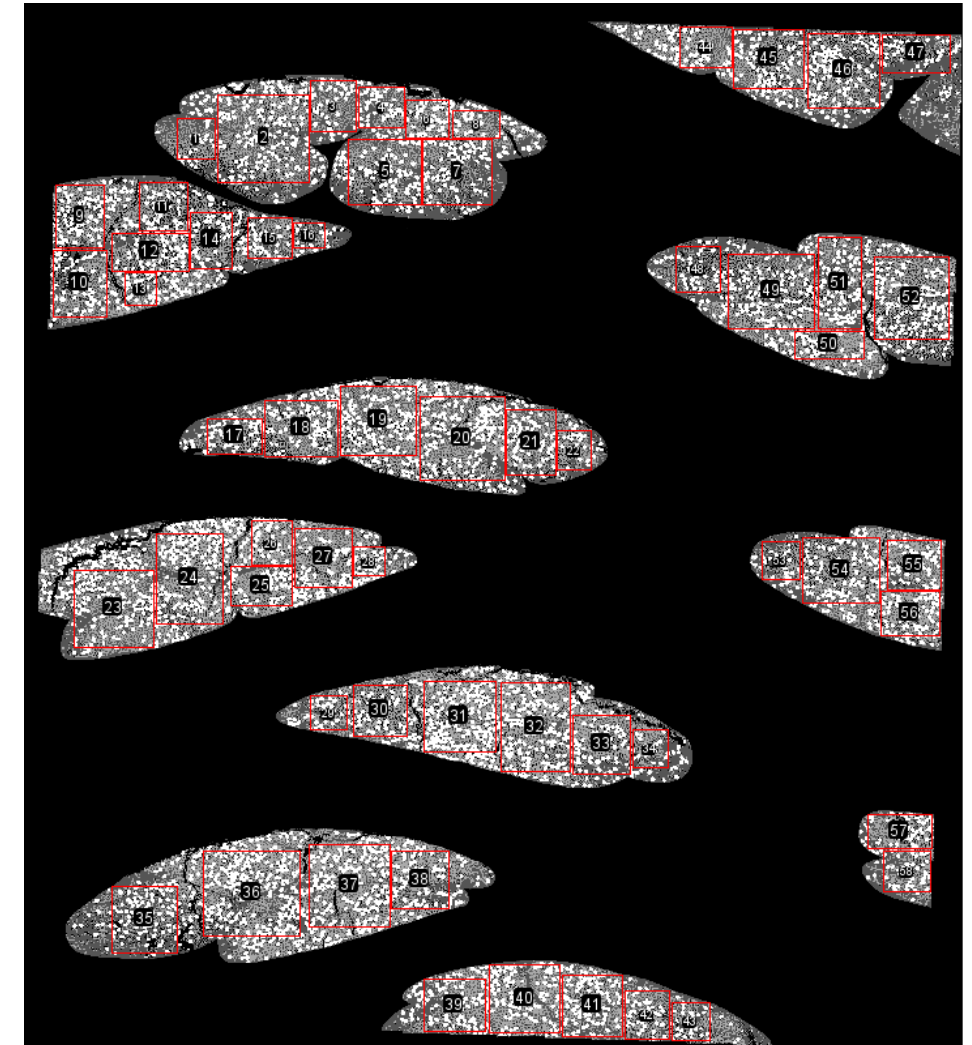
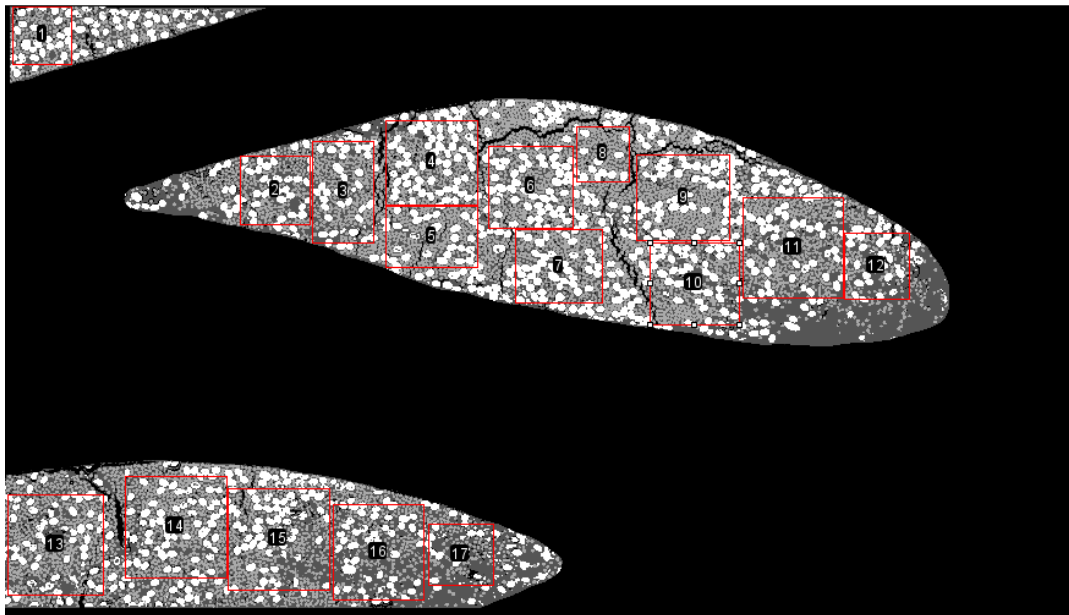
Segmented microscopy image using the trained UNet model



# Tow Modeling: Microscopy – Thermal Conductivity



- Once the microscopy data is fully segmented, PuMA can calculate the average thermal conductivity of a tow.
- Selected 75 regions or “frames” of sizes between  $500^2$  and  $1600^2$  pixels for thermal conductivity evaluation.

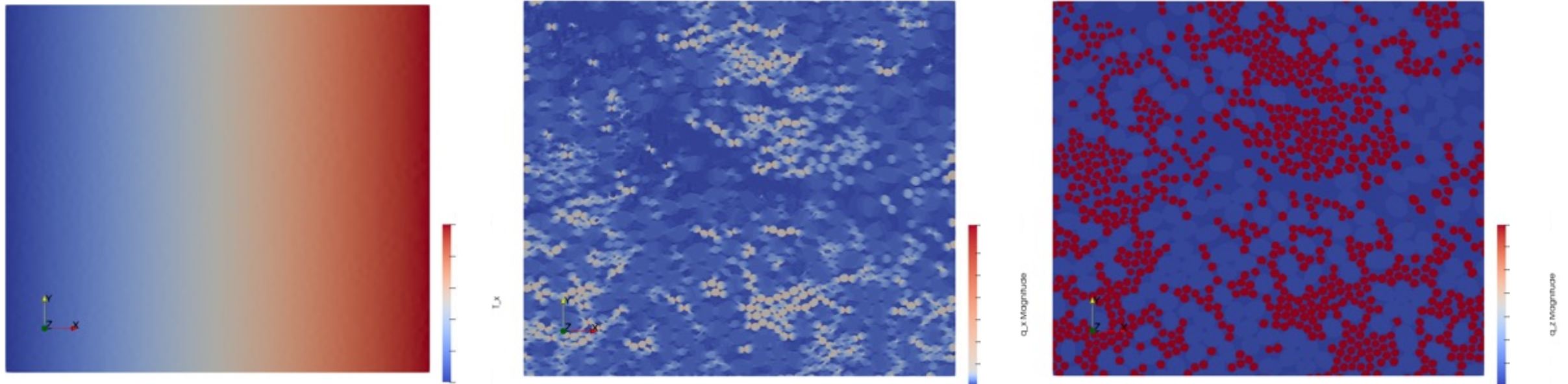


*Frames selected for thermal conductivity calculation, 2023-1-10-HEEET\_IL\_Warp\_L2 (left) and 2023-1-10-HEEET\_IL\_Tow-Area-2-4-7 (right)*

# Tow Modeling: Microscopy – Thermal Conductivity

- AS4 carbon fiber:  $k_{axial} = 6.9 \text{ W/mK}$ ,  $k_{transverse} = 2.52 \text{ W/mK}$
- Phenolic fiber assumed fully dense phenolic resin:  $k = 0.25 \text{ W/mK}$
- Porosity of infiltrated phenolic resin considered.
- Final conductivity value computed by volume averaging the results for all frames.

Tow Properties	Value
VF Cracks	
VF Phenolic Resin	
VF Carbon Fibers	
VF Phenolic Fibers	
$k_{transverse}$	
$k_{axial}$	

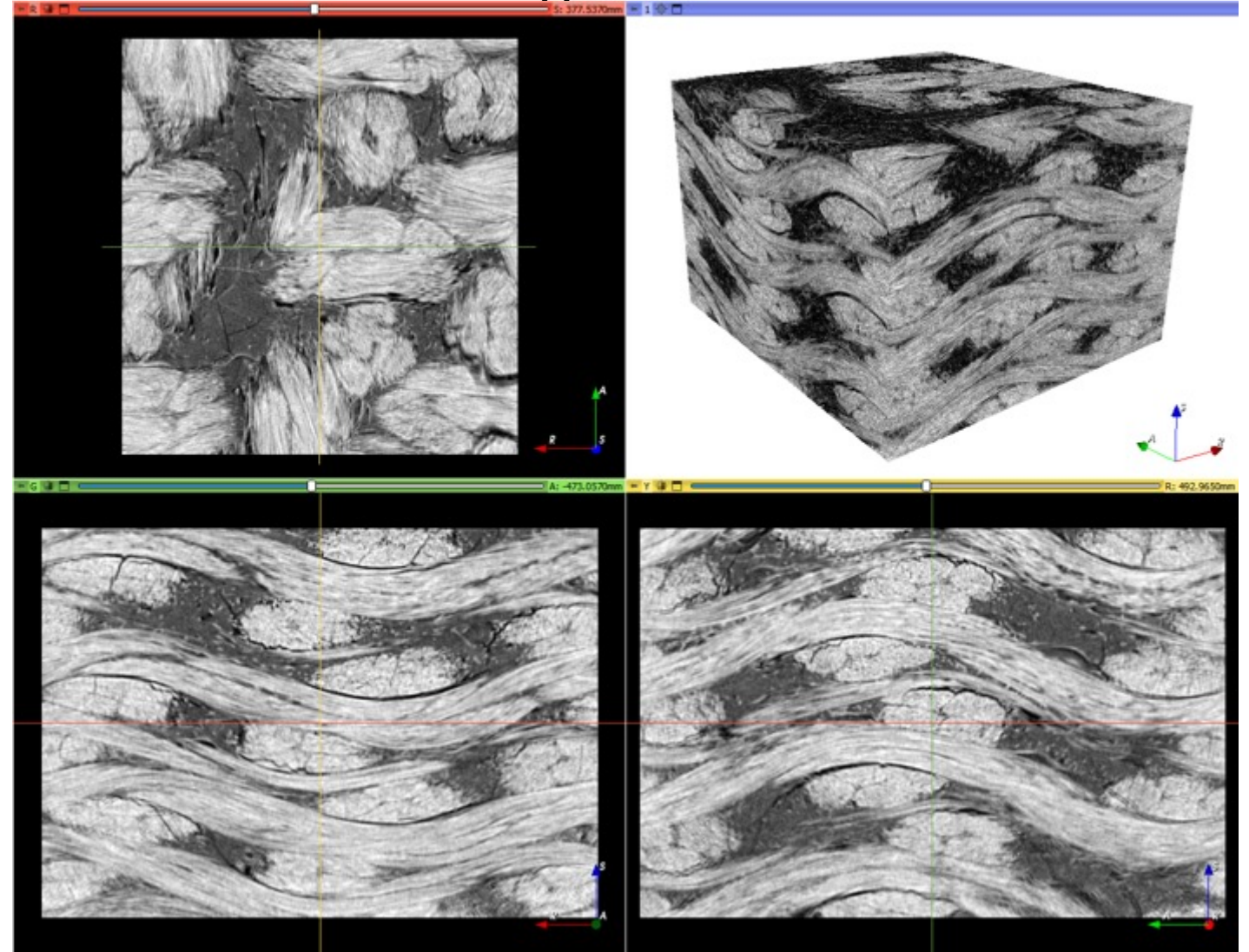


HEET\_IL\_Tow-Area-2-4-7 frame #36, temperature\_x (left), heat flux\_x (center) and heat flux\_z (right) fields.

# Unit Cell: Micro-CT Data

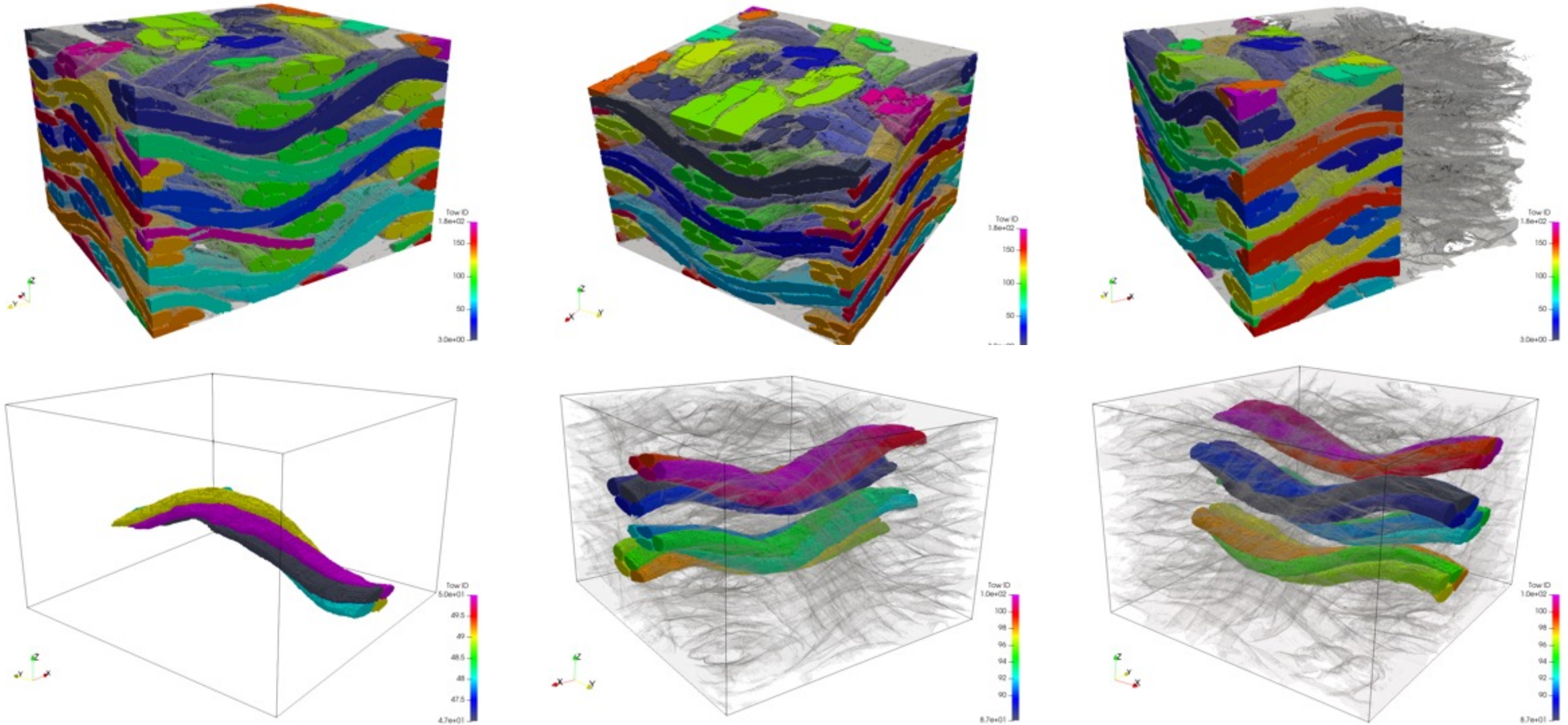
- Micro-CT data provided by Kyle Hendrickson, infused sample “HEEET-24-016-001-12”
- Sample object of this study taken from the middle section of the reconstructed image.
- Tows made of four twisted sub-tows, and visible matrix cracks.
- Sample resolution:
  - X (R) - 472px (Fill)
  - Y (A) - 497px (Warp)
  - Z (S) - 330px (Thickness)

*Raw and cropped micro-CT data*



*HEEET-24-016-001-12 sample (credits: Kyle Hendrickson)*

# Unit Cell: Micro-CT Segmentation



*Segmented 3MDCP visualizations*

# Unit Cell: Micro-CT Orientation



- Orientation of the tows computed for the full resolution micro-CT data.
- Orientation fields are important to apply different mechanical properties or thermal conductivity values along and across the sub-tows.
- Tow's orientation computed using PuMA's Structure Tensor method for each tow individually.
- Final orientation values obtained by averaging the results for each cross-section of each tow to reduce errors.



*Sub-tows number 48, 59, 110 and 125*

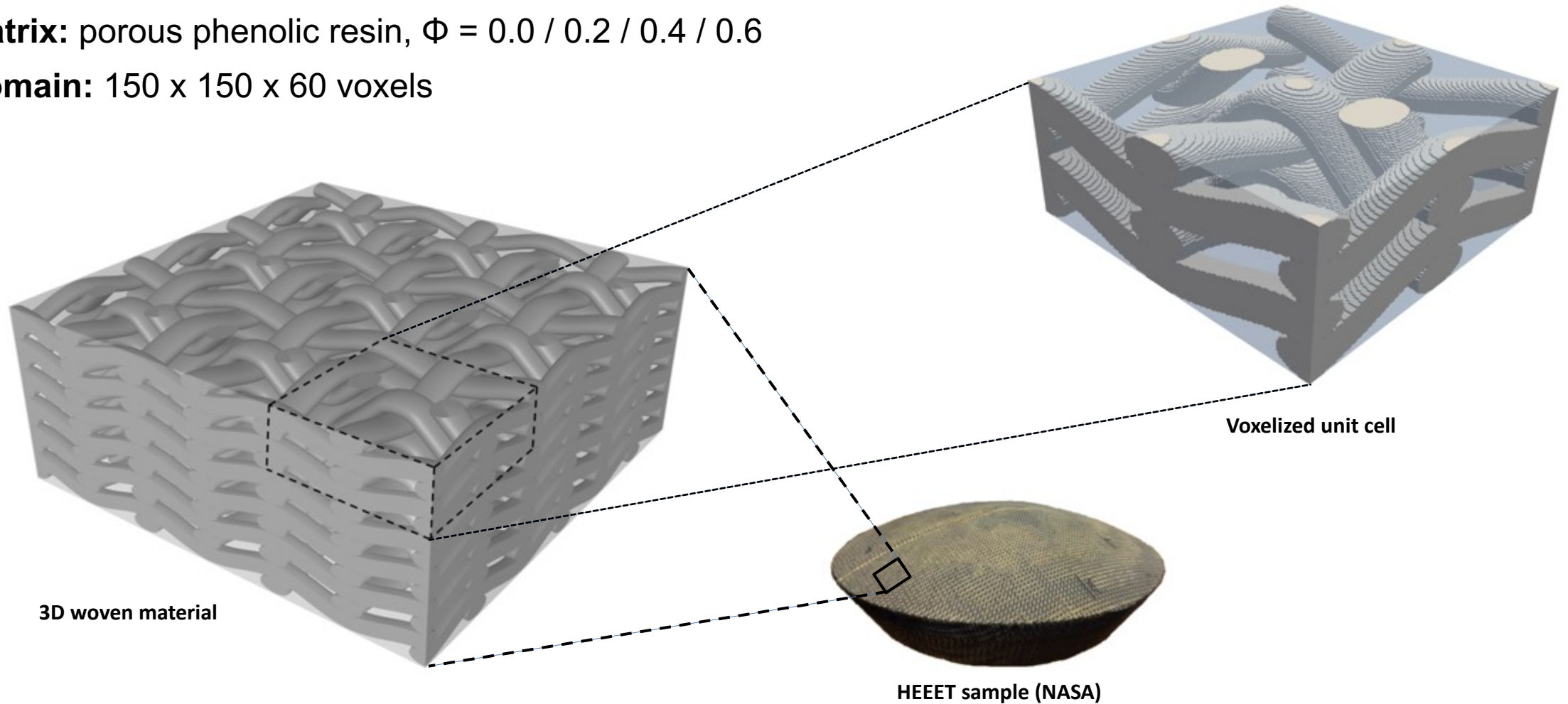
# Unit Cell: Artificially Generated – Elasticity



**Yarns:** phenolic resin impregnated carbon fibers,  $V_f = 0.5 / 0.6 / 0.7 / 0.8$

**Matrix:** porous phenolic resin,  $\Phi = 0.0 / 0.2 / 0.4 / 0.6$

**Domain:** 150 x 150 x 60 voxels



# Unit Cell: Artificially Generated – Elasticity



- RVE homogenization method: displacement of 1 voxel in +X, +Y and +Z respectively with periodic BCs.

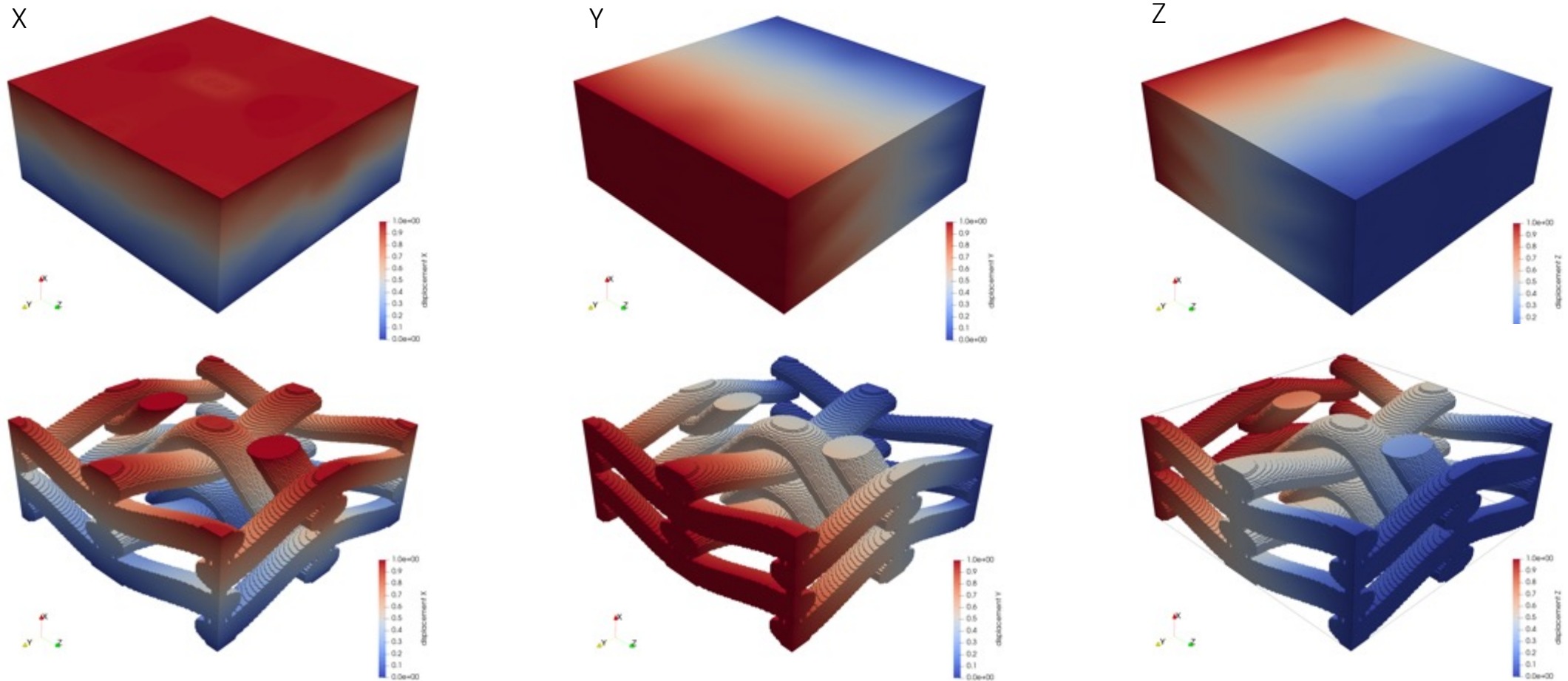


Fig.18 - Displacement field with matrix visible (top) and matrix hidden (bottom) in the X, Y and Z directions

# Unit Cell: Artificially Generated – Elasticity



- RVE homogenization method: displacement of 1 voxel in +X, +Y and +Z respectively with periodic BCs.

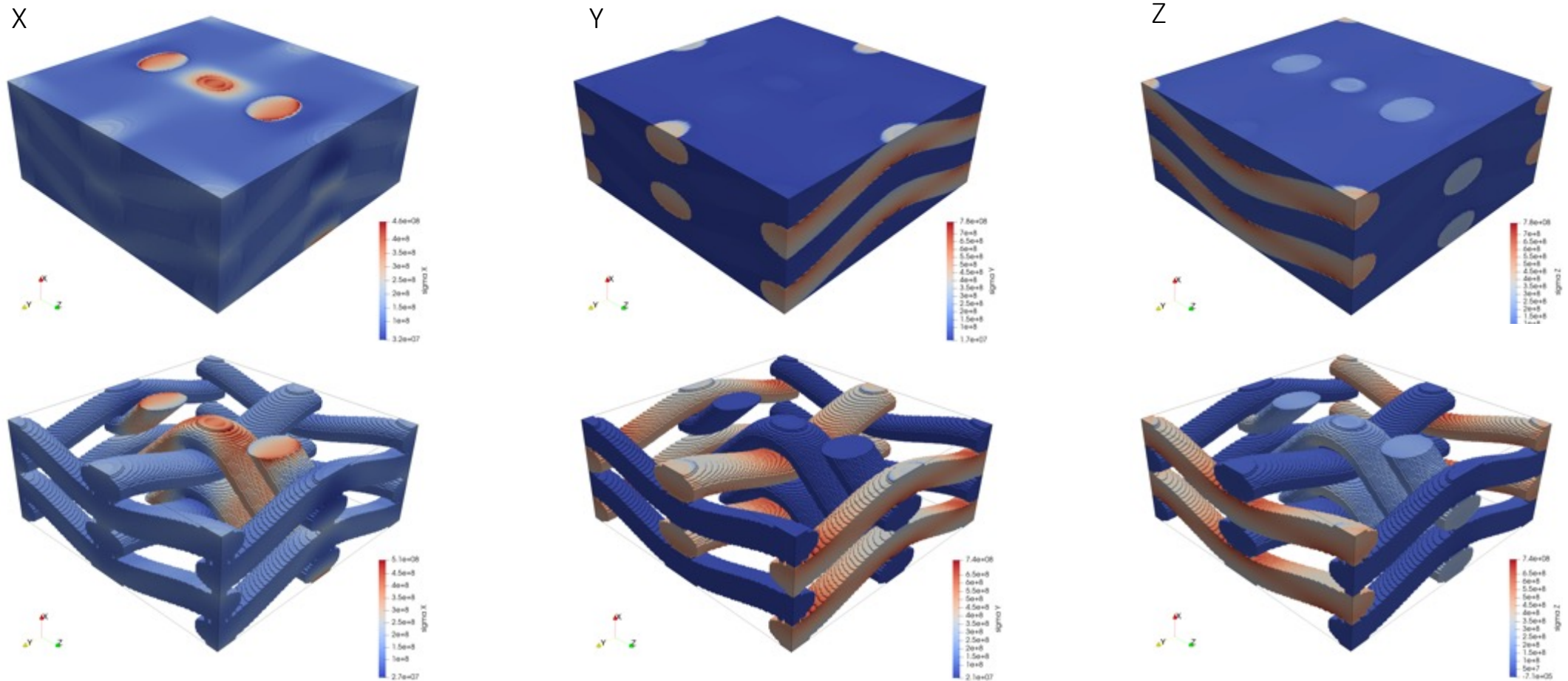


Fig.19 – Direct stress field with matrix visible (top) and matrix hidden (bottom) in the X, Y and Z directions



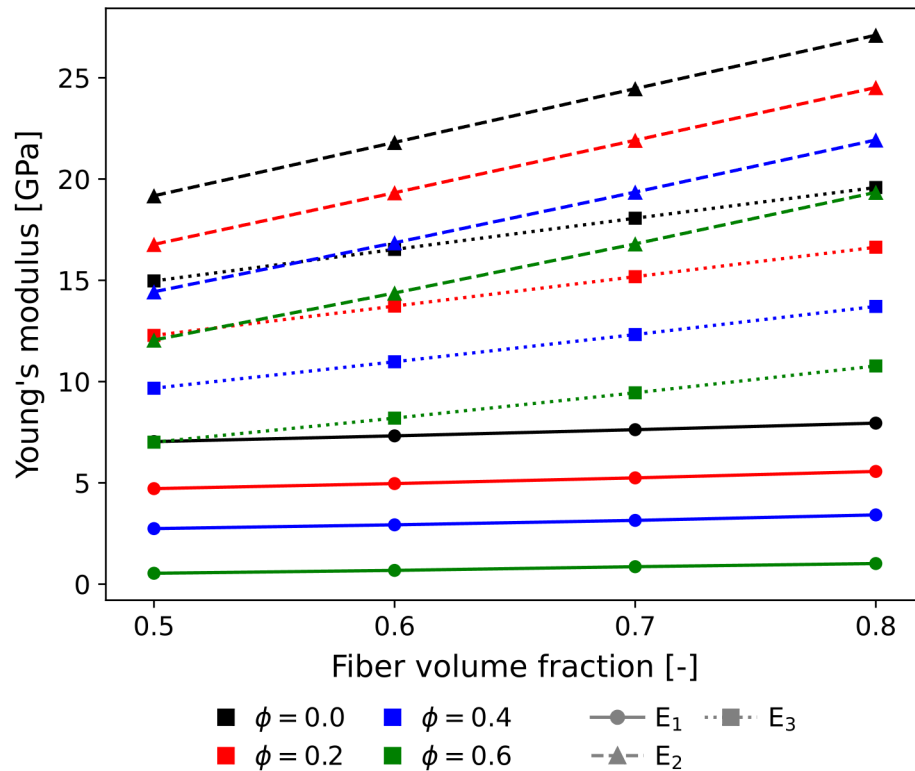
# Unit Cell: Artificially Generated – Elasticity



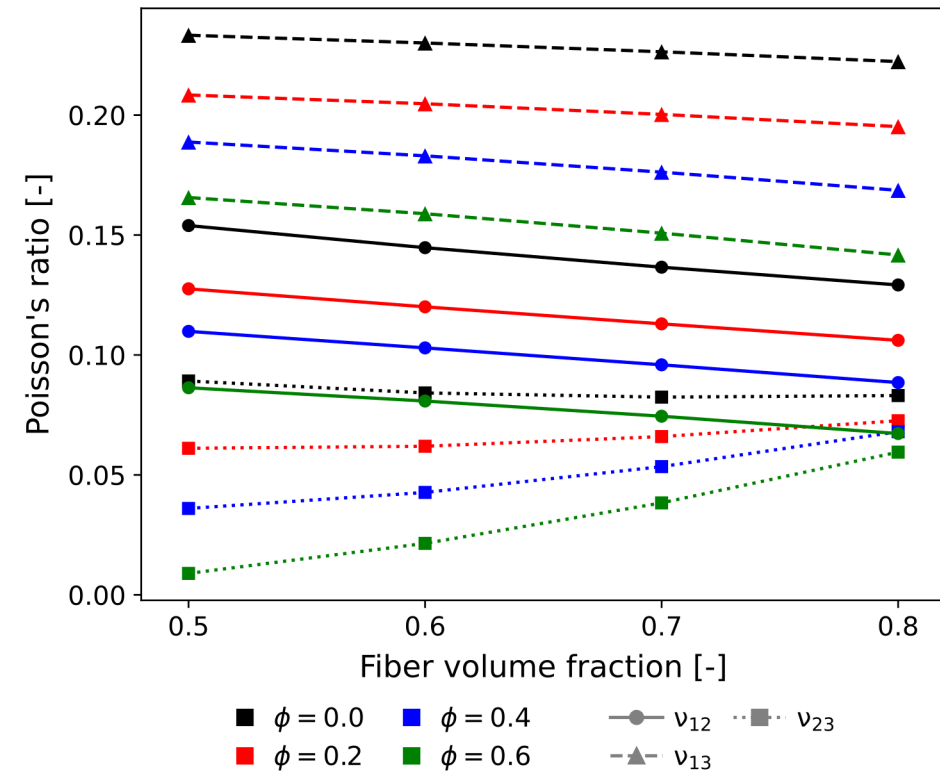
- The same methodology used at the micro-scale for the constituents was applied to obtain the effective mechanical properties of the unit cell.

Directions:

- X = 1
- Y = 2
- Z = 3



Young's moduli of the unit cell



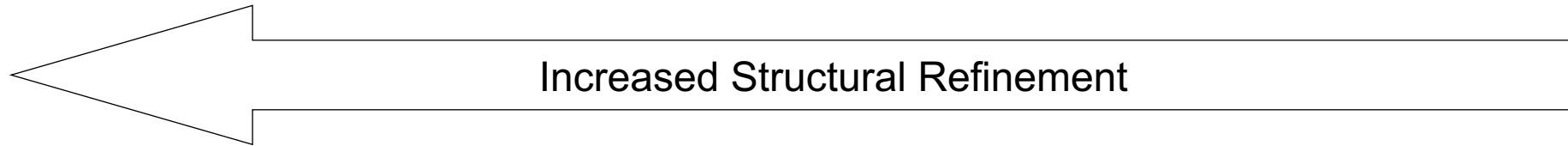
Poisson's ratios of the unit cell

# Conclusions

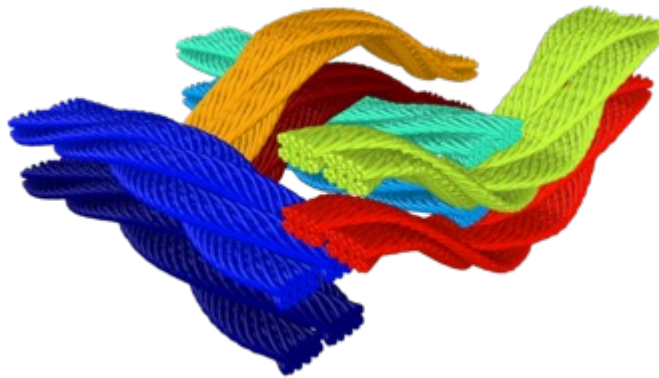


- This work described a methodology to carry out multi-scale analyses of porous 3D woven materials using artificially generated models, and models segmented from microscopy / micro-CT data.
- This methodology can be applied to any type of composite material to obtain its homogenized orthotropic mechanical properties, and anisotropic thermal conductivity.
- The PuMA software allowed us to analyze the constituents at the micro-scale and then use those results to accurately model the unit cell at the macro-scale.
- Results were validated for the elasticity results of the porous matrix and the yarns by comparing them to analytical expressions listed in the literature.
- Future work investigate as-manufactured weaves.

# Computational Materials Modeling

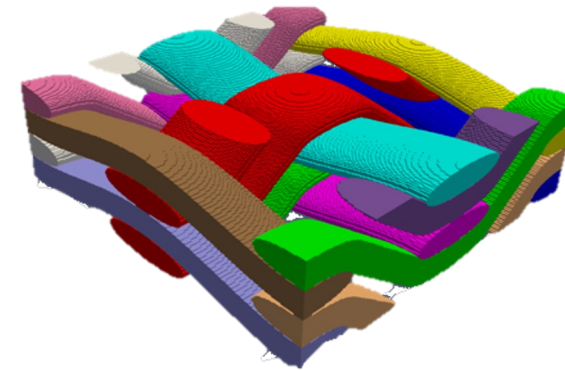


**Particle-based, discrete-element  
methods (LAMMPS, HYDRA)**

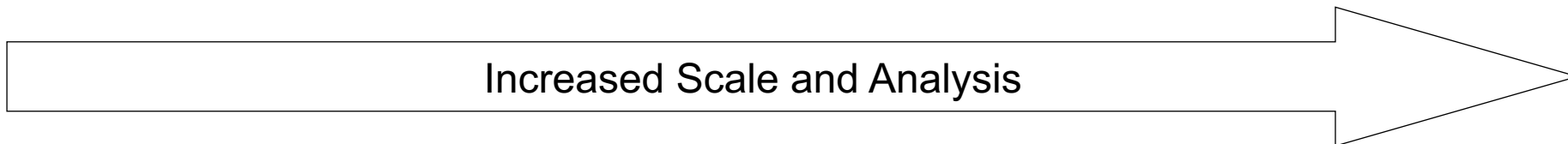


Fiber-level resolution  
Andrew P. Santos

**Porous Microstructure Analysis  
(PuMA)**



Yarn-level resolution  
Sergio Friale Izquierdo

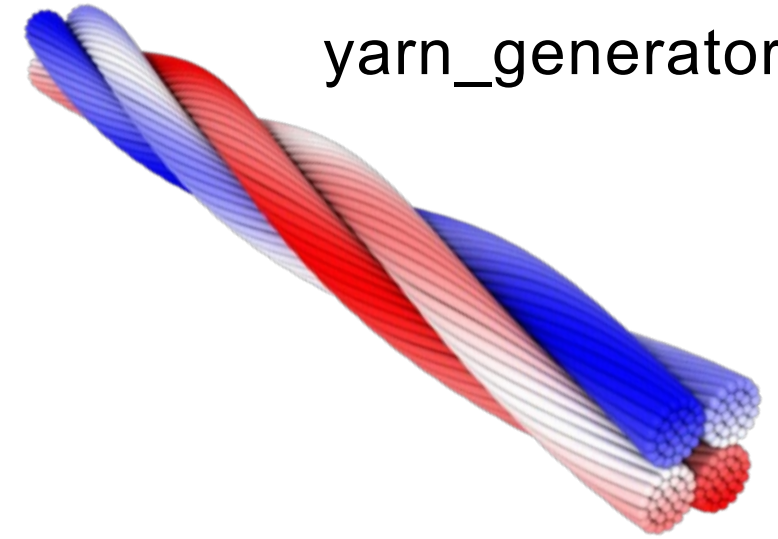


# Particle-based/Meshless/Lagrangian Woven TPS Modeling



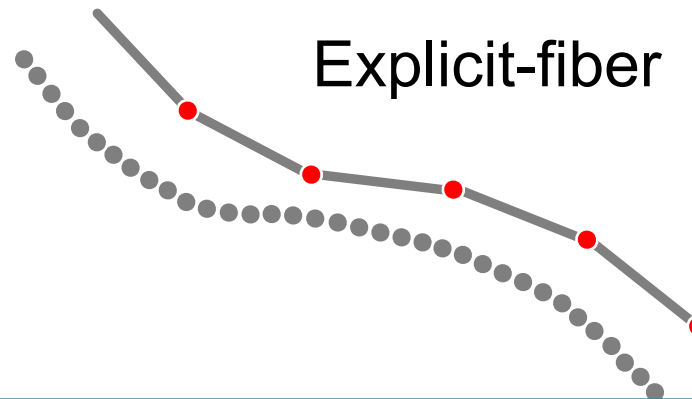
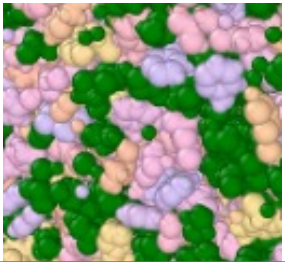
## Goal of the bottom-up approach

- if the fiber model is correct, the weave will be correct
- extract fiber-level behavior and contribution in weaves and yarns during damage, impact or ablation



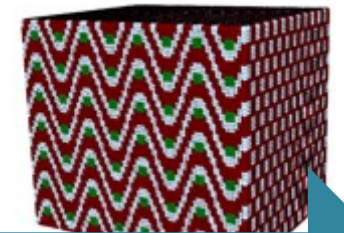
yarn\_generator

Molecular dynamics



Explicit-fiber

peridynamics



microscale

mesoscale

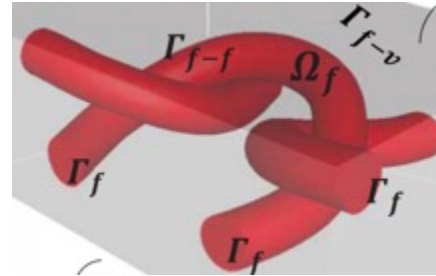
# Phenomena Captured by Explicit-Fiber Modeling



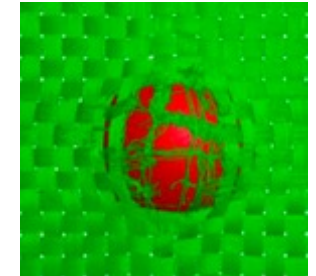
Explicit-fiber modeling captures certain experimental observations where continuum is unable

## Physics incorporated with explicit-fiber models

- Role of geometry and directionality
- Fiber-fiber friction
- Rupture
- Dynamic collective motion



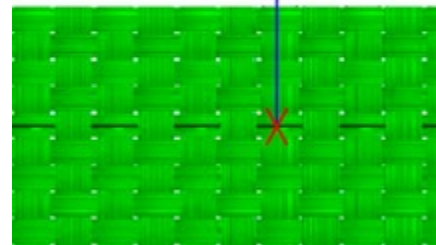
Strength of knit vs purl\*



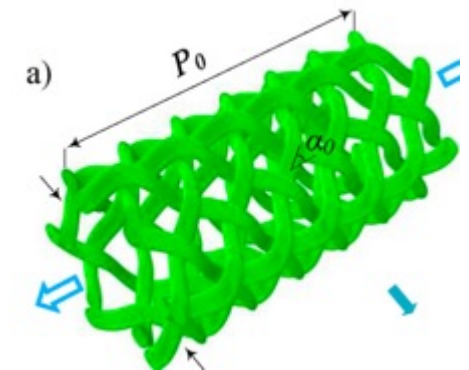
Impact with friction<sup>^</sup>

## Explicit-fiber applications

Center failed element



Friction controlled deformation with localized failure<sup>+</sup>



Yarn evolution during Braiding<sup>#</sup>

\*Liu, D. *et al. J. App. Mech.* **2019**, 86 (11). [doi.org/10.1115/1.4044014](https://doi.org/10.1115/1.4044014)

#Ghaedsharaf, M. *et al. Composites Part B* **2021**, 218, 108938. [doi.org/10.1016/j.compositesb.2021.108938](https://doi.org/10.1016/j.compositesb.2021.108938)

<sup>+</sup>Wang, Y. *et al. Int. J. Impact Eng.* **2016**, 97, 66–78. [doi.org/10.1016/j.ijimpeng.2016.06.007](https://doi.org/10.1016/j.ijimpeng.2016.06.007)

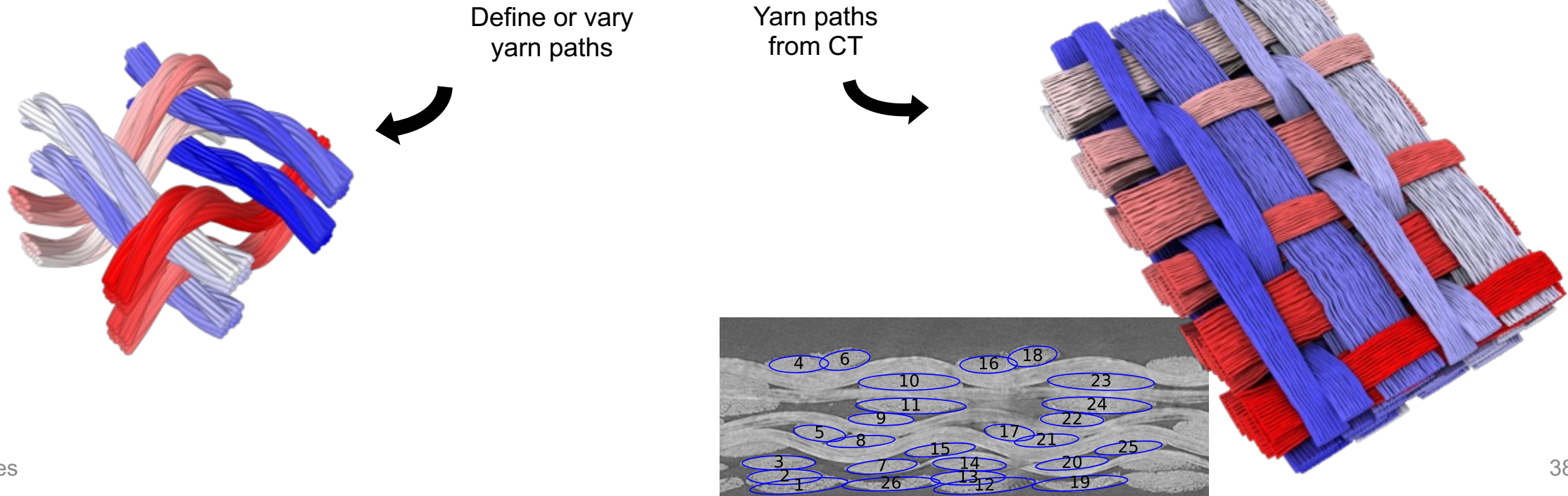
<sup>^</sup>Wang, Y.; *et al. Int. J. Impact Eng* **2016**, 97, 66–78. [doi.org/10.1016/j.ijimpeng.2016.06.007](https://doi.org/10.1016/j.ijimpeng.2016.06.007)

# Configuration Generation with Relevant Features



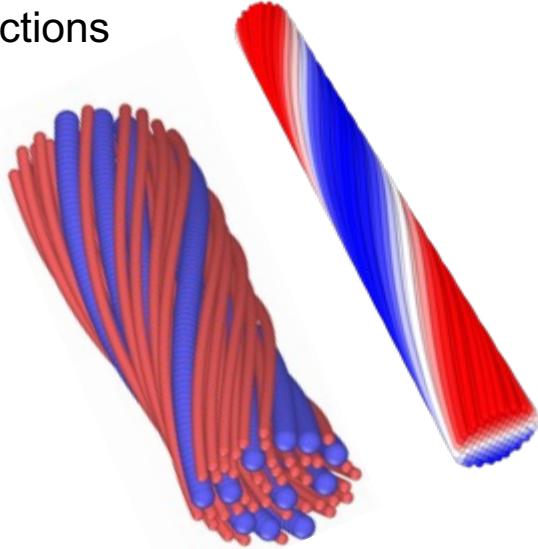
- Idealized and realistic yarn and weave configurations are required to calibrate and verify fiber models and test hypotheses on weaves
- Python package, `yarn_generator`, developed to generate fiber-level models of yarns and weaves

## Two ways to generate a weave



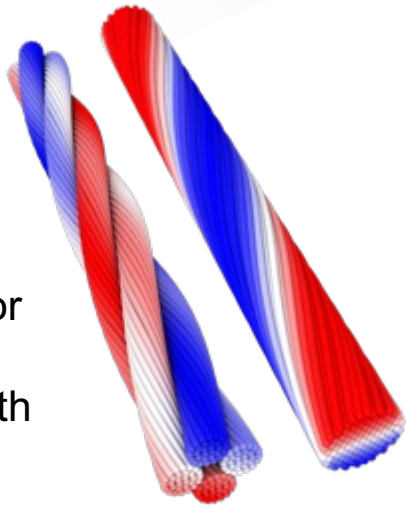
# Yarn Features

Circular or ellipsoidal cross sections

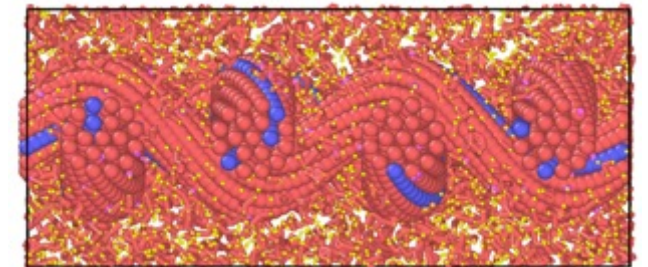
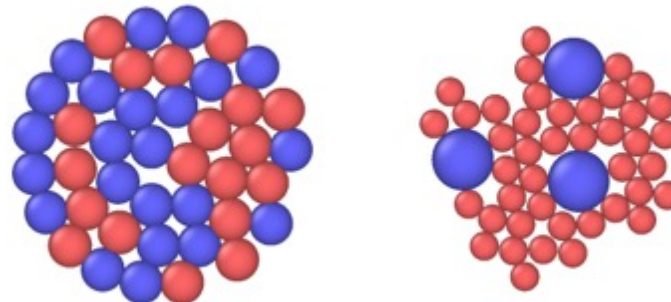


- Woven heat shields use yarns composed of different fibers and processing conditions
- Explicit-fiber simulations model the yarn microstructure
- The yarn\_generator builds configurations with the relevant features

Single- or multi-ply yarns with twisting



optimal circle-in-circle or random 2d blended packing



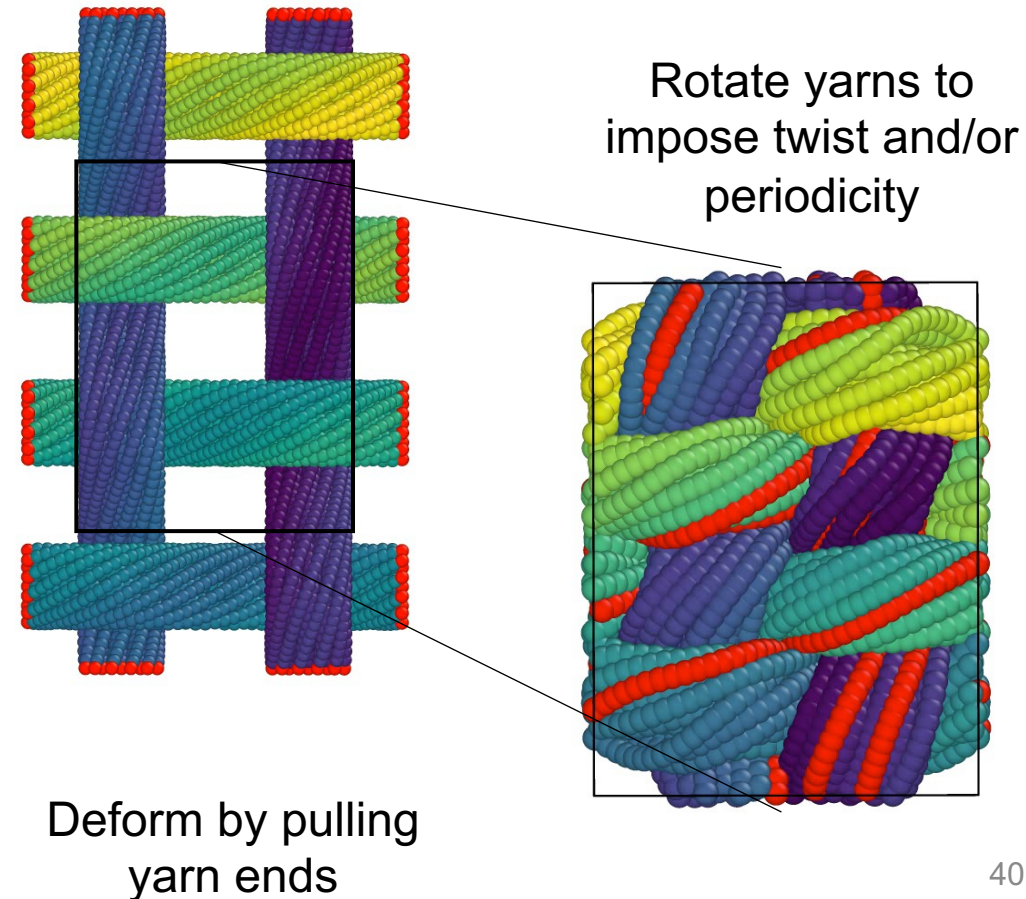
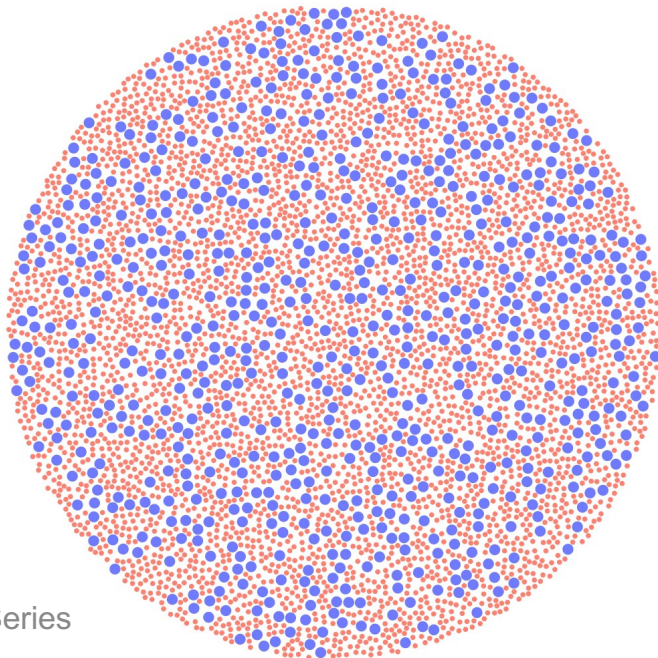
infusion

# Yarn-Weave Manipulation



- Yarn manipulation can control the weave density or yarn packing
- Enables wrinkle and other behaviors
- Satisfies contact mechanics

circular packing protocol

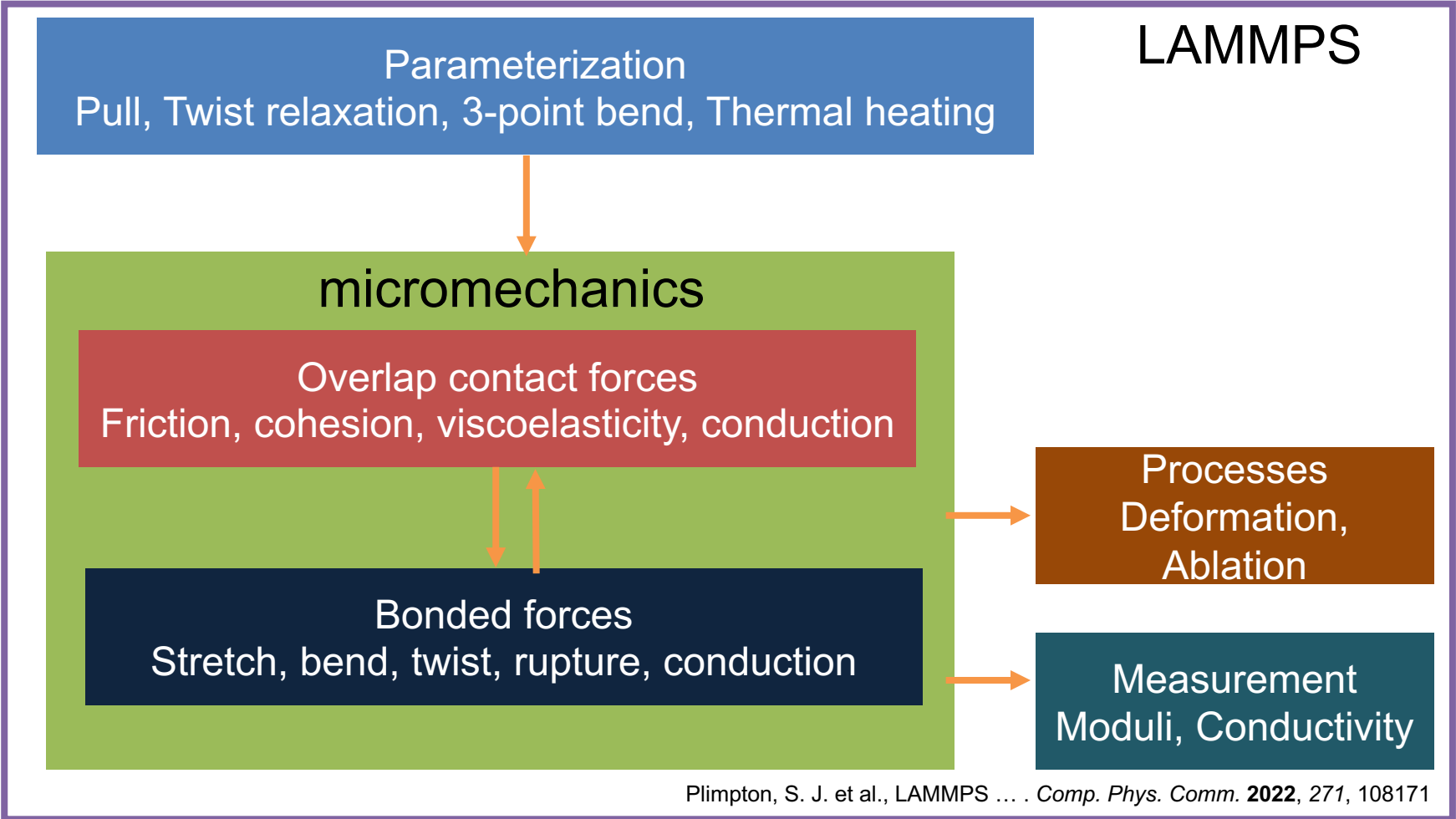
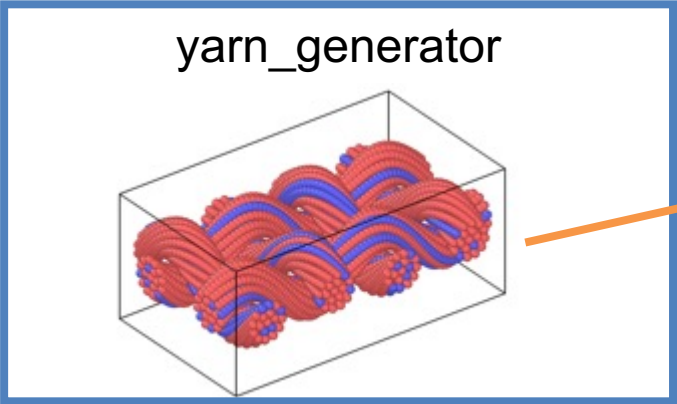




# Explicit-Fiber Simulation Methodology



Explicit-fiber simulations allow for the fibers to evolve independently during yarn-weave manipulation, parameterization and entry phenomena



Plimpton, S. J. et al., LAMMPS ... *Comp. Phys. Comm.* **2022**, 271, 108171

# Fiber Model Details

- Explicit-fiber simulation forces model each contact and internal mode independently
- Analysis of trajectories and forces can highlight the magnitude and directionality of each mode's contribution

## Micromechanics-informed model:

- **Intra**<sup>1,2</sup>-fiber, bonded forces
  - Stretch
  - Bend
  - Shear
  - Twist
  - Rupture
- **Inter**<sup>3</sup>-fiber, contact forces
  - Friction
  - Viscoelastic repulsion
  - Cohesion

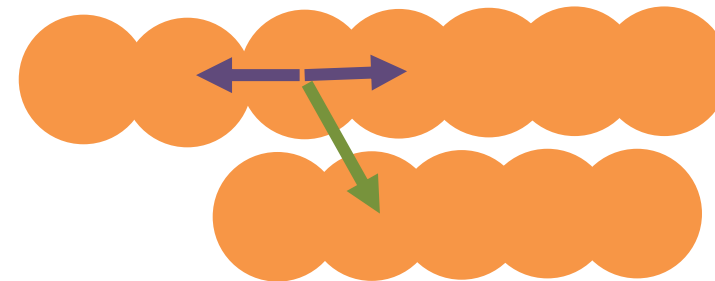
## Method

- Meshless
- dynamic
- apply heat and deformation
- microstructure can change during simulation
- implemented in an open-source parallelized code<sup>4</sup>

Most model forces are modeled as a Hookean spring + damping



$$f_r = k_r(r - r_0)$$



<sup>1</sup>Chen, X. et al. Comparative Assessment and Unification of Bond Models in DEM Simulations. *Granular Matter* **2021**, 24 (1), 29.

<sup>2</sup>Wang, Y. and Sun, X. Digital-Element Simulation of Textile Processes. *Composites Sci. Tech.* **2001**, 61 (2), 311–319.

<sup>3</sup>Silbert, L. E. et al., Granular Flow down an Inclined Plane: Bagnold Scaling and Rheology. *Phys. Rev. E* **2001**, 64 (5), 051302.

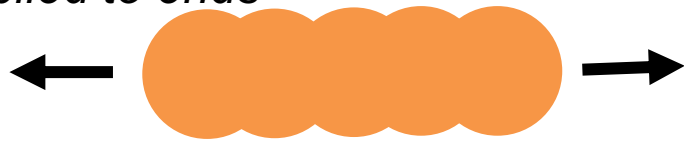
<sup>4</sup>Plimpton, S. J. et al., LAMMPS ... . *Comp. Phys. Comm.* **2022**, 271, 108171

# Tensile, Bending and Shear Moduli



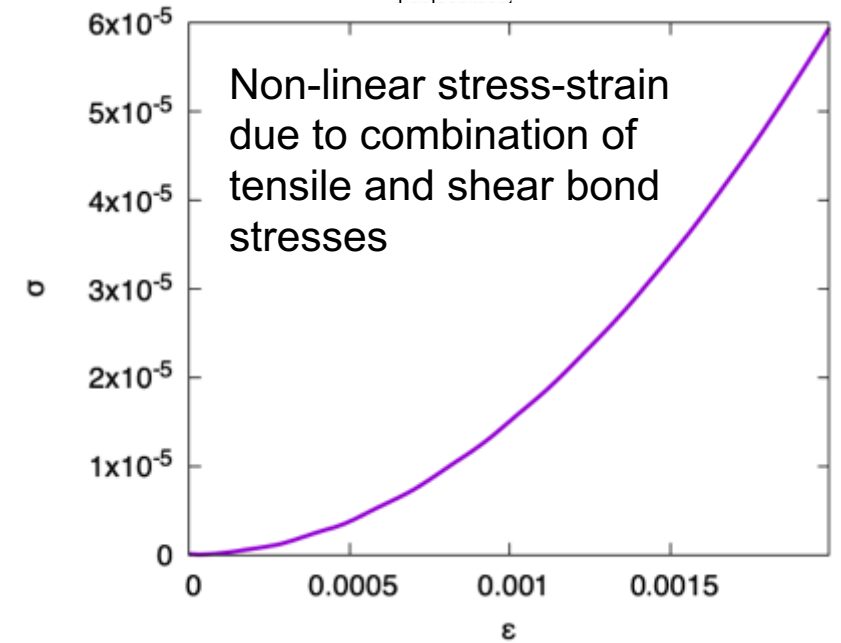
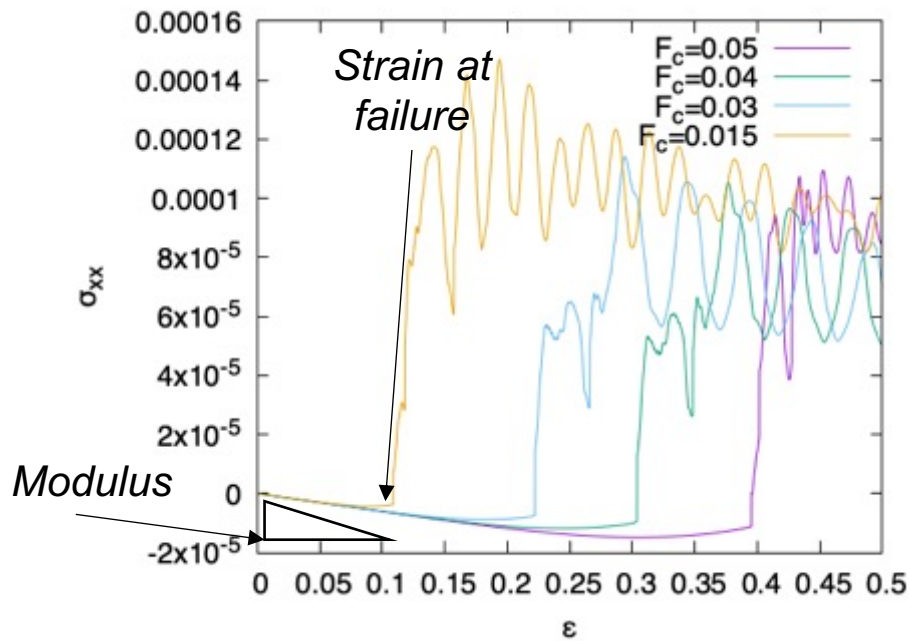
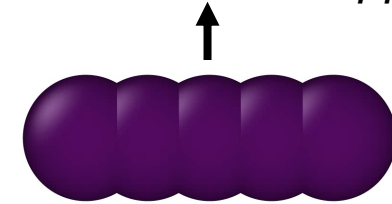
Tuning model spring parameters can capture the rupture behavior due to different modes for carbon fibers, e.g., enabling experimental comparison

*strain applied to ends*



single, short fiber simulations

*strain applied to center*

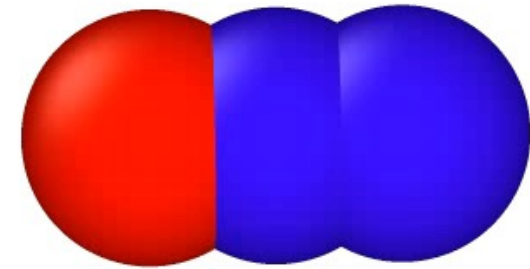


# Rod Thermal Conduction Model

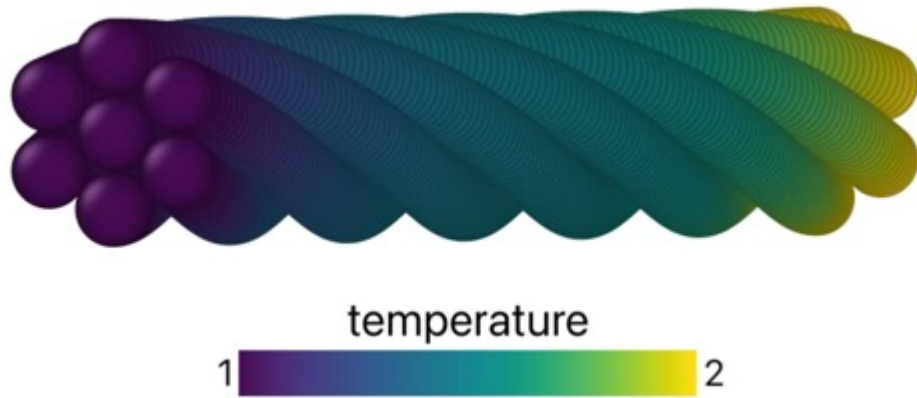


- Explicit-fiber models can characterize conduction along and across fibers
- New model enables thermo-mechanical processes
- Yarn feature-property relationships can be tested

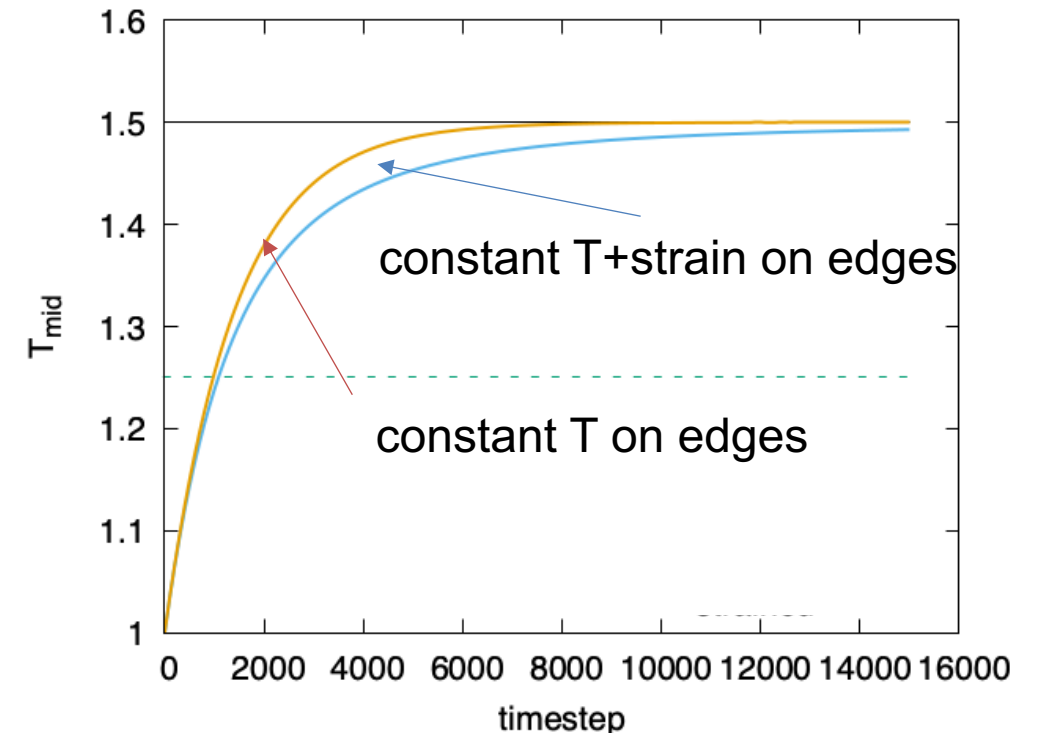
- Strain slows approach to steady-state



7 twisted Kynol phenolic fibers



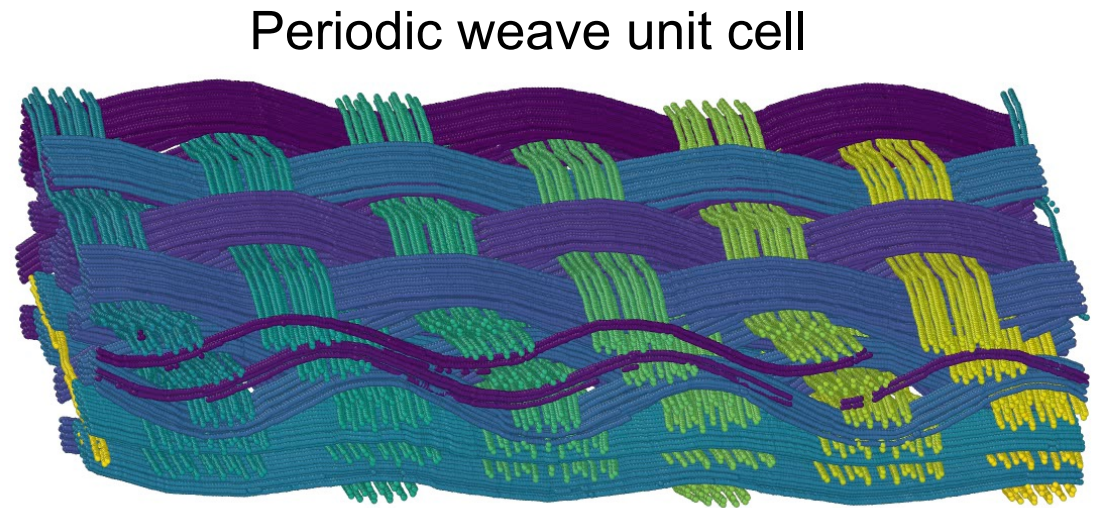
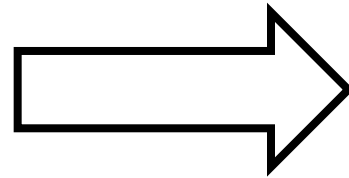
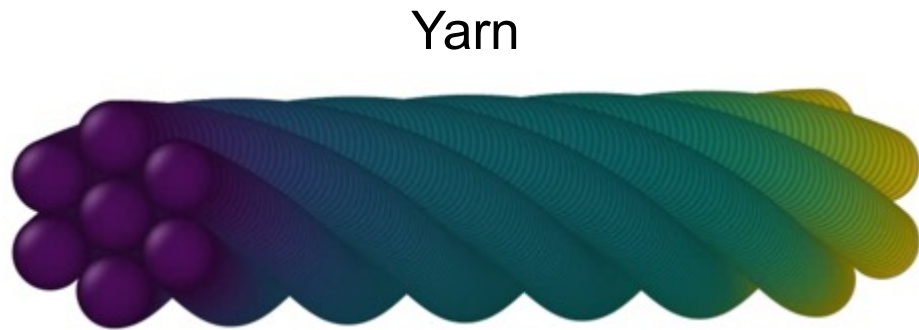
- Yarn coarse-graining changes the conduction timescale to steady-state due to
  - Number of fibers changes the contact area
  - Exterior fibers are longer than interior fibers in twisted yarns



# Weave Simulations of Heat Shield Ablation



The multi-fiber yarn representation can be incorporated into a full weave



We can apply weave simulations to test hypotheses, such as heat shield ablation

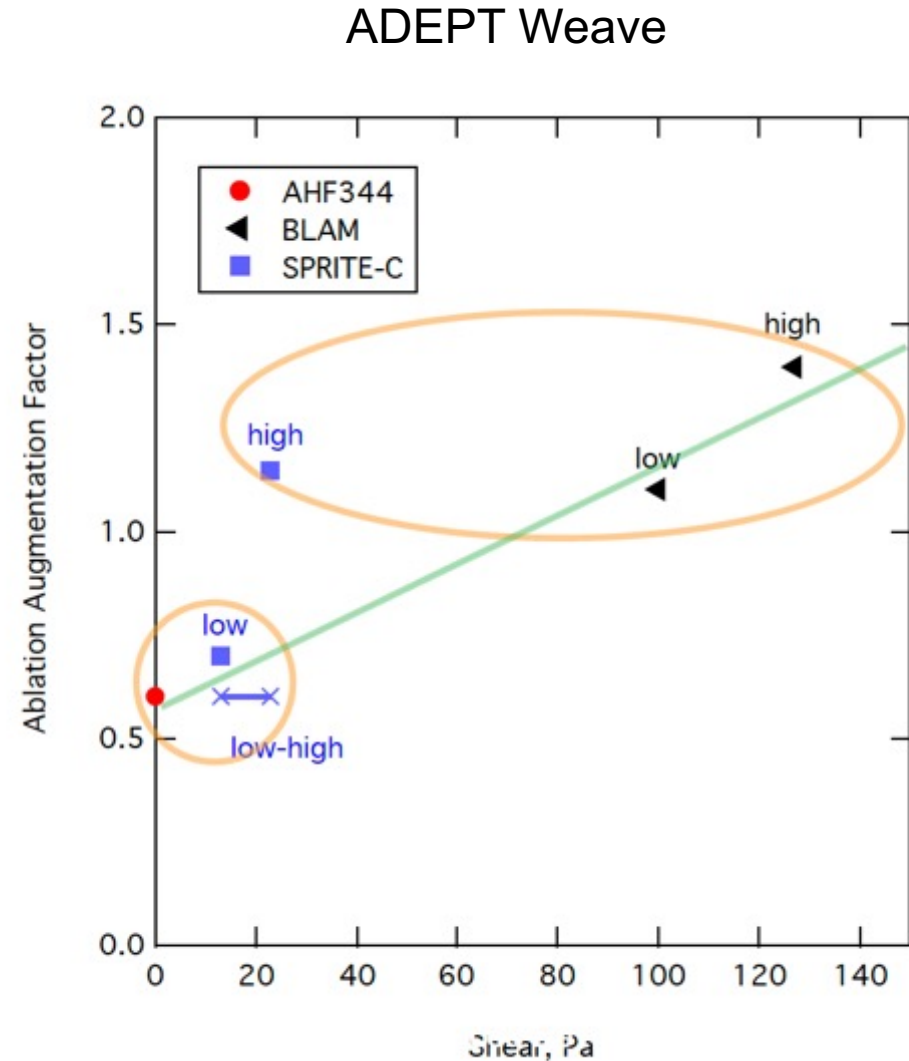
# State of Ablation Modeling



- Available ablation model (FIAT) shows that the standard approach to ablation (chemical only) underpredicts experimental recession values
- Ablation augmentation factor (AF) was proposed to scale chemical ablation rate to fit experiments:

$$\frac{\partial m}{\partial t} = (1 + AF) \frac{\partial m_c}{\partial t}$$

- The AF is not well posed but does appear to correlate to available surface shear stresses in some cases
- What are the contributing factors to non-chemical ablation augmentation?

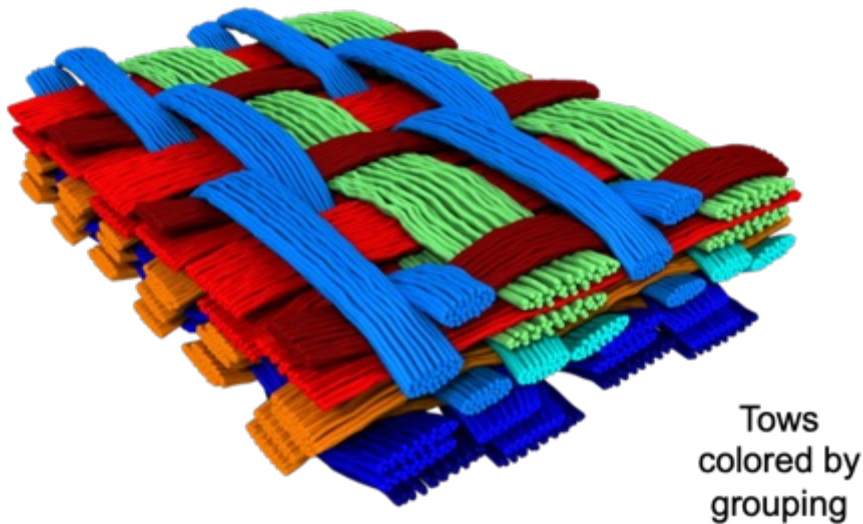


Courtesy F. Milos

# Ablative Disconnection of Yarns

- Erosion of the weave such that regions of tows become disconnected and “fall off” from having no structural connection to the remaining weave

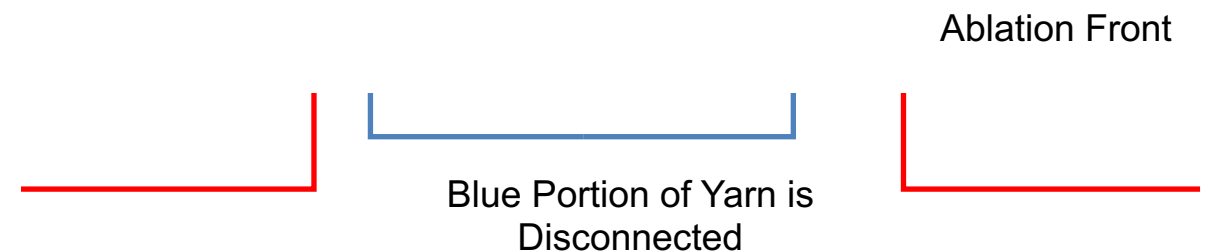
ADEPT Weave



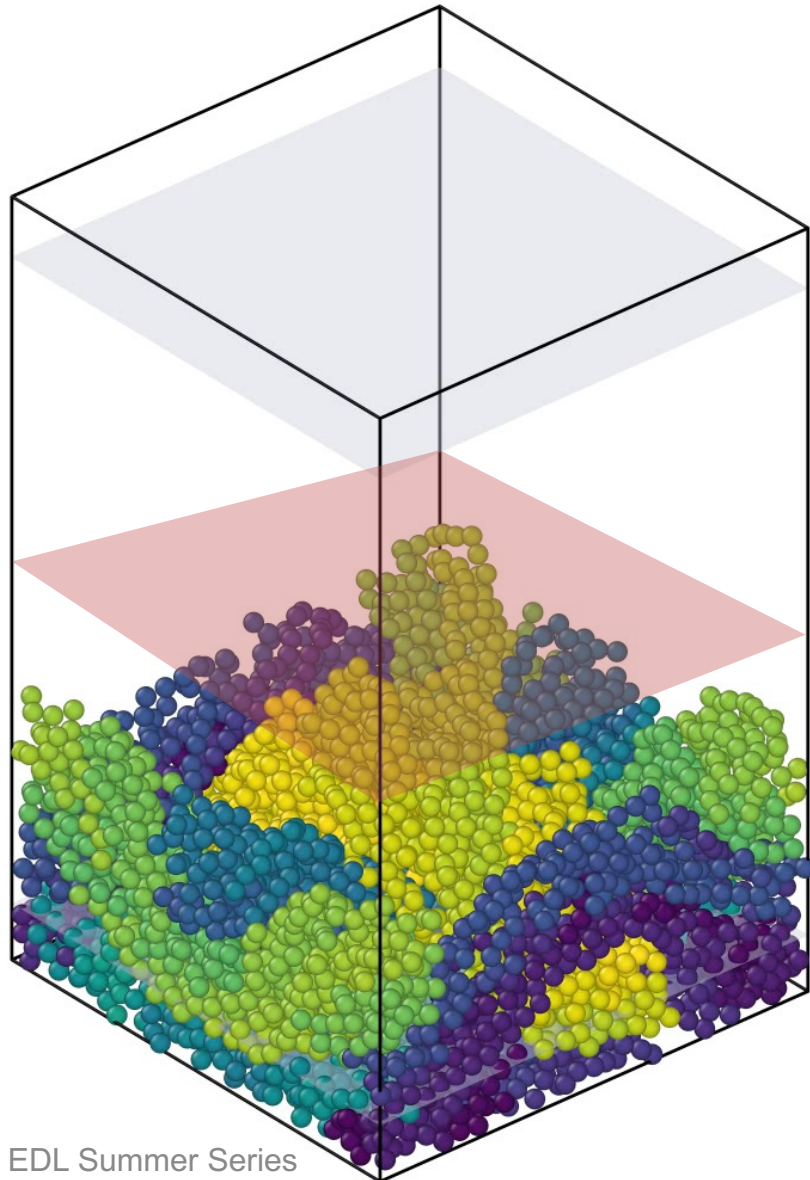
Weave before ablation



Weave at some point during ablation



# Model of Weave Ablation and Connectivity



- Ablation front moves into the material and removes particles
- Forces applied such that disconnected portions of fibers are ejected from the surface into the ablation zone

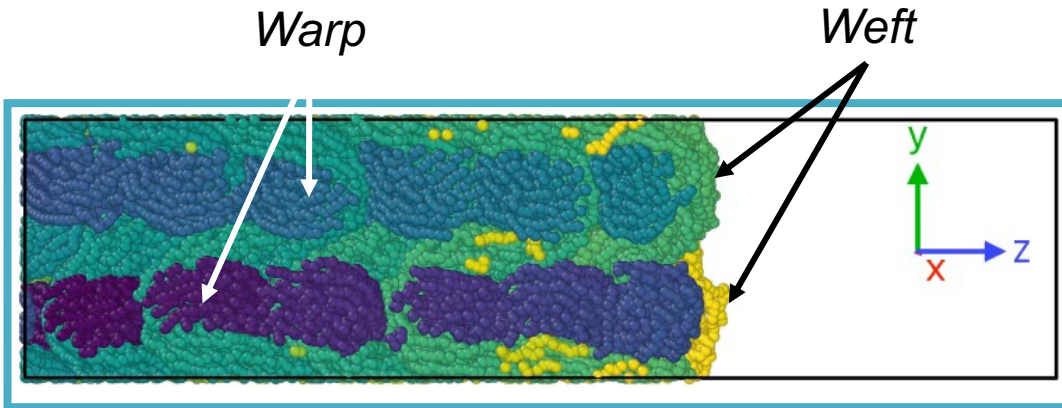
ablation zone

*Fiber tension: harmonic bonds*

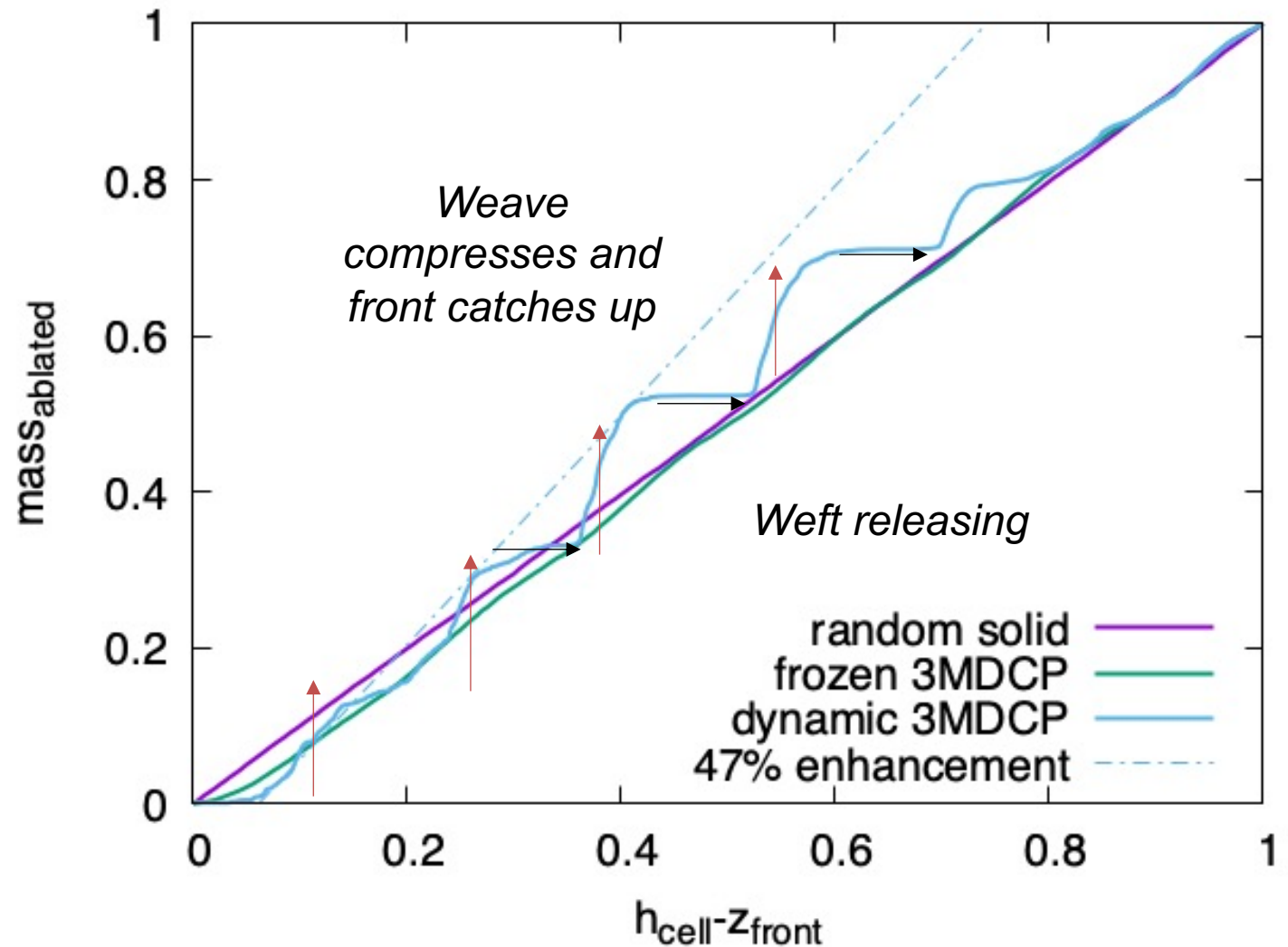
*Fiber-fiber repulsion: viscoelasticity*



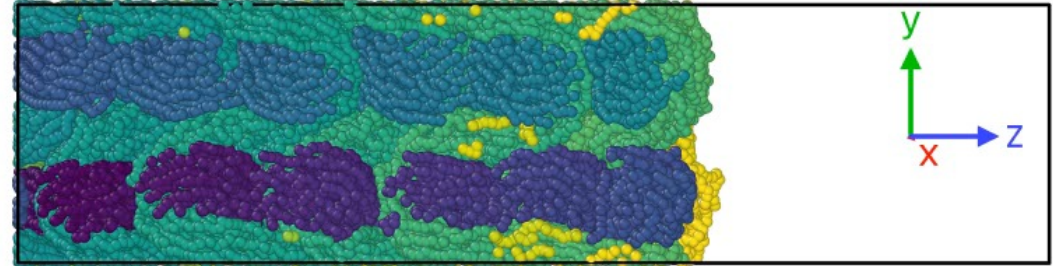
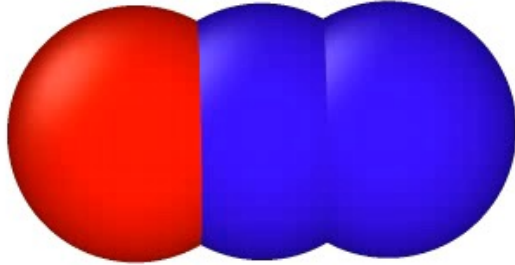
# Augmentation from Loss of Weave Connectivity



- Large portions of weft yarns ablate faster due to the 3D geometry
- Weave disconnection enhances erosion by ~47%
- Other phenomena, such as pitting, are likely present
- With more development, the method could predict this behavior



# Explicit-Fiber Simulation Conclusions



- Yarn processing, like twist, changes material properties, requiring explicit-fiber simulations
- Enabled modeling of thermo-mechanical behavior
- 3D woven heat shields have enhanced ablation, ~47%, due to the weave geometry

## Future work

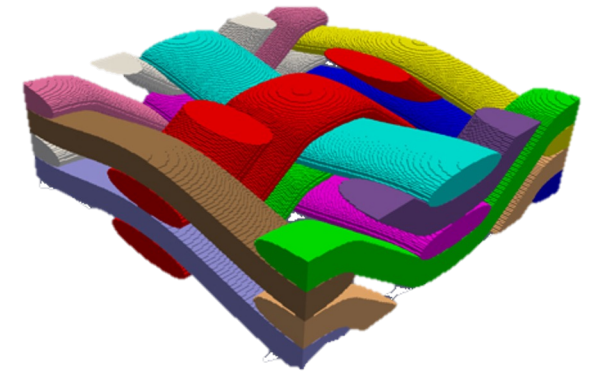
- Incorporate material-specific, coarse-grained yarn-models into full weaves
- Identify defect deformation mechanisms

# Fiber and Weave Modeling Conclusions



- Entry System Modeling - Certification by Analysis task is
  - **Multi-center** (ARC-TSM, ARC-TI and GRC) and
  - **Multi-method** (non-destructive evaluation, machine learning, material characterization, finite element, peridynamics, explicit-fiber)
- The PuMA software
  - Measured the orthotropic mechanical properties, and anisotropic thermal conductivity
  - Modeled a composite woven system, and it's constituents, including the porous matrix and yarns
- Explicit-fiber simulations
  - Demonstrated a ~47% ablation enhancement due to the weave geometry

Porous Microstructure Analysis  
(PuMA)



Particle-based, discrete-element  
methods (LAMMPS, HYDRA)

