



NASA Hypersonic Technology Project (HTP) SiC/SiC Research for Hypersonic Airframe Hot Structures

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- **Introduction**
 - Thermal protection systems (TPS) and hot structures
 - Hot structures weight savings
- **Ceramic matrix composite (CMC) hot structures**
 - Carbon/carbon (C/C)
 - Carbon/silicon-carbide (C/SiC)
 - Silicon-carbide/silicon-carbide (SiC/SiC)
- **Technical challenges**
- **Concluding remarks**

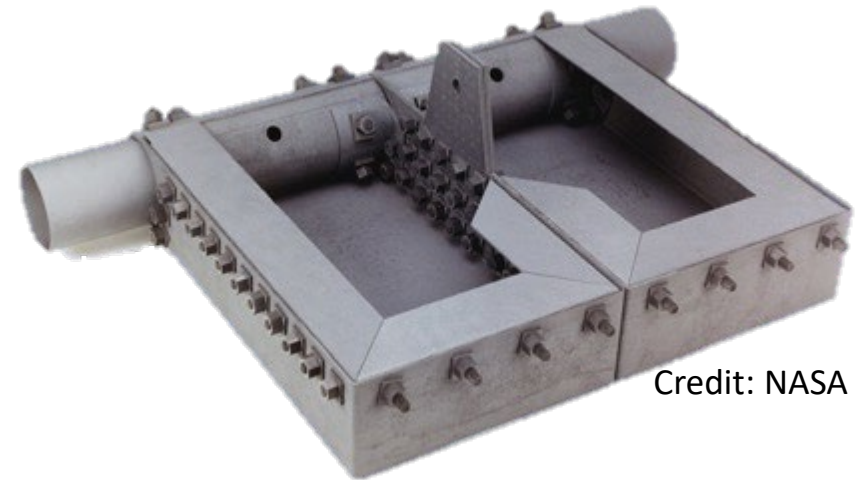
- In the US, the term “TPS” is usually used to include:
 - Acreage TPS such as tiles, blankets, and ablators
 - Insulation
 - Hot structures such as leading edges, nose caps, control surfaces, and aeroshells
 - Multi-functional structure that carries load at operating temperatures
- Europe (and the rest of the world) uses the terms TPS and hot structures

The US will only realize the benefits of hot structures by first understanding the differences from TPS



Credit: NASA

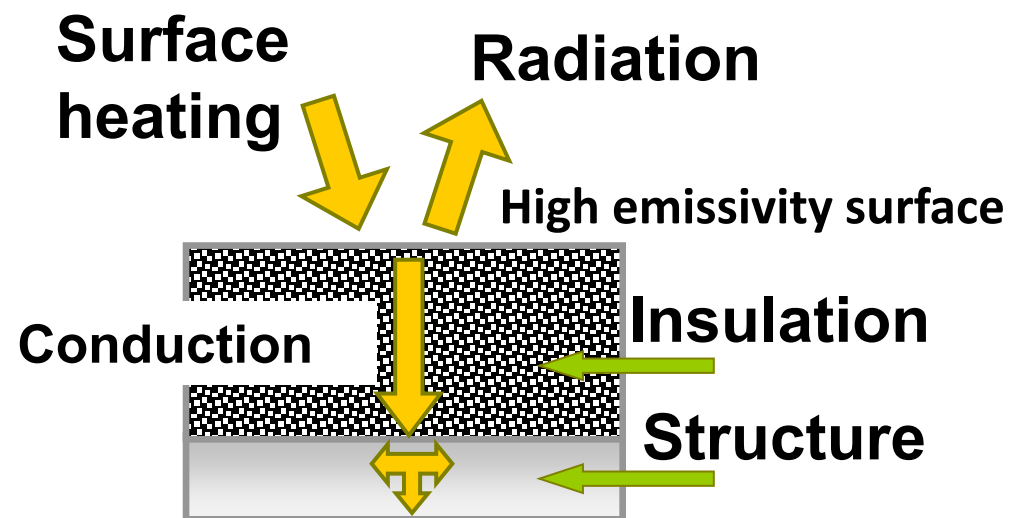
Tile TPS



Credit: NASA

Hot structure control surface

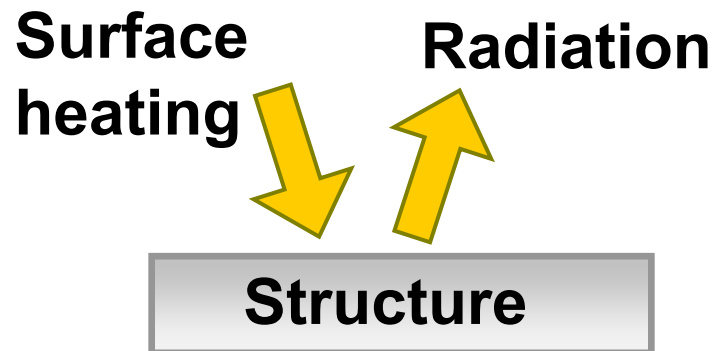
**Use: Moderate heat flux,
short times**



Tile TPS

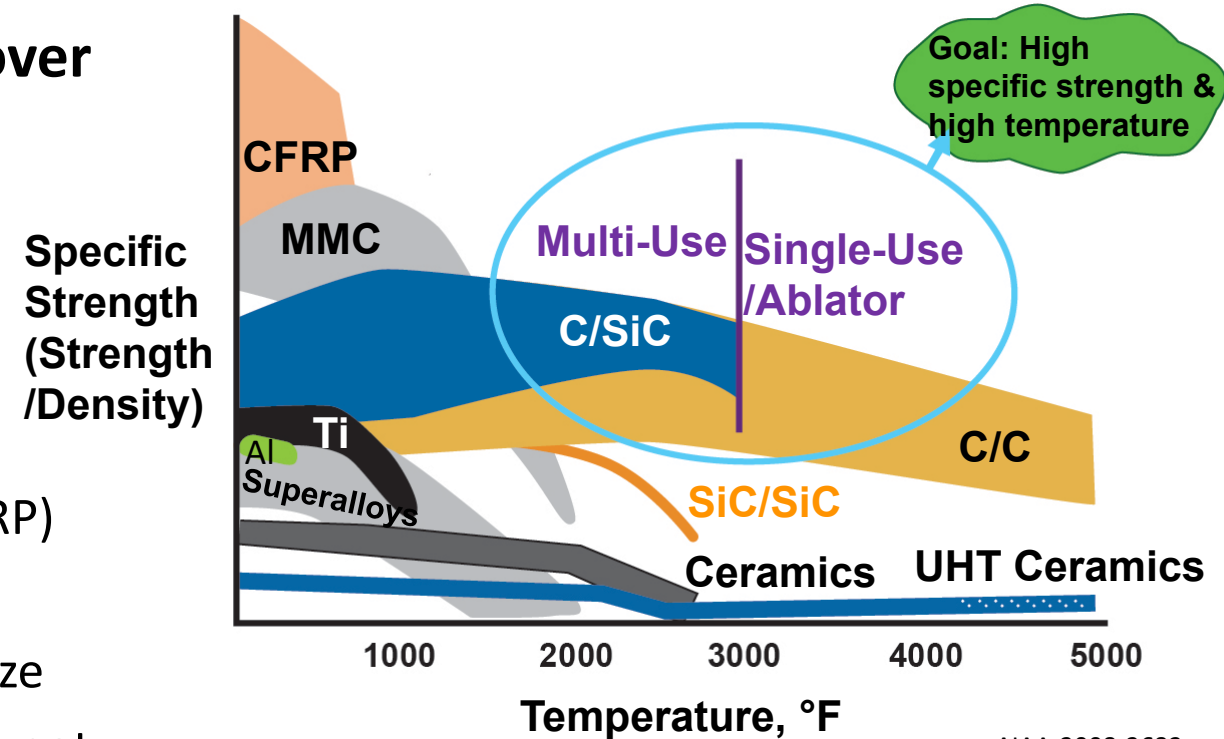
- **Heat radiated away**
 - Maximize surface emissivity
- **Minimal heat conducted inward**
- **Structure remains cool**

**Use: Moderate heat flux,
long times (steady state
conduction)**



- **Heat radiated away**
- **Heat conducted inward**
- **Structure carries load while operating hot**

- Hot structures provide ~ 25% weight savings over insulated cold structure
- High-performance vehicles utilize high specific strength/stiffness materials
 - Aluminum (Al)
 - Composites: carbon fiber reinforced polymers (CFRP)
 - Titanium (Ti)
 - Beyond Ti use temperatures (~ Mach 5), often utilize superalloys, refractory metals, and active cooling – not high specific strength
 - Refractory composite hot structures extend high specific strength structures to 3000°F and above



AIAA-2008-2682

ACC: Advanced carbon/carbon
 MMC: Metal matrix composite
 HfC: Hafnium carbide
 C/SiC: Carbon/silicon carbide
 UHT: Ultra high temperature



Hot-Structure Weight Savings Over Insulated Cold Structure



- **HSR (NASA High Speed Research program) SiC/SiC combustor liner**
 - Projected 30% weight savings
 - Reduced NOx and CO emissions due to higher temp
- **X-38 C/SiC hot structures**
 - Bearings 50% lighter weight than traditional bearings
 - Body flap 50% less than insulated cold structure (5.25 ft x 4.6 ft, 150 lb)
 - Rudder (different design temperature)
 - PM-1000 with Ti inner structure and insulation: 133 lb with growth factor of ~ 5%
 - CMC: 97 lb with higher growth factor (27% weight savings)
- **Space shuttle orbiter body flap (AIAA-1983-913)**
 - Baseline 1460 lb, insulated cold structure
 - ACC body flap 1207 lb (253 lb, 17% weight savings)
- **X-37 hot structures**
 - 50% weight savings potential over metallic structure with TPS
- **JSF (Joint Strike Fighter) 3rd stage, low pressure, CMC turbine vanes**
 - ~200 lb weight savings per mid-size turbine engine
- **Aircraft brakes**
 - 500-1000 lbs per plane weight savings
- **Actively cooled CMC combustor (French study, AIAA-2011-2208)**
 - 30% weight savings over metallic

Rule of thumb, ~ 25% weight savings with CMCs

- **Advanced carbon/carbon-6 (ACC-6)**

- Oxidizes in air if uncoated $> \sim 800^{\circ}\text{F}$
- When coated, oxidation resistance to $\sim 3000^{\circ}\text{F}$
- Limited reusability
- Low interlaminar properties
- Used on Parker Solar Probe, rocket nozzle extensions, and aeroshells

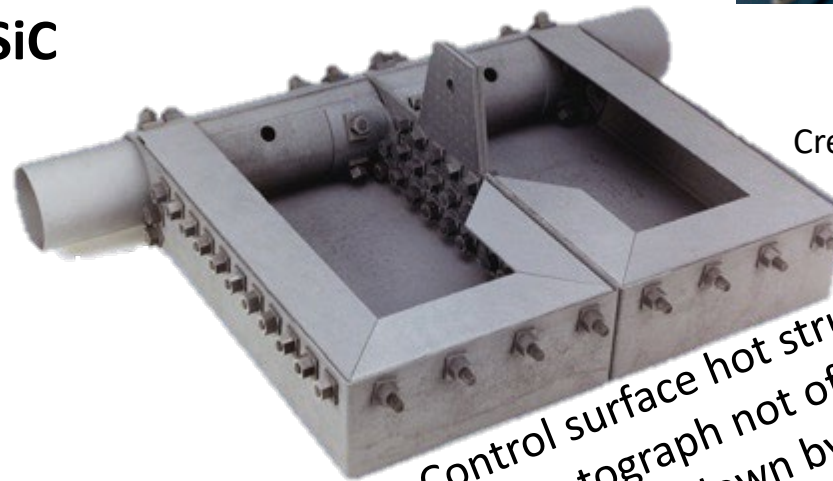
Parker Solar Probe
heat shield (ACC-6)



Credit: NASA

- **Chemical vapor infiltration (CVI) C/SiC**

- Good oxidation resistance to $\sim 3000^{\circ}\text{F}$
- Reasonable reusability
- Good interlaminar properties
- Flown by European Space Agency (ESA)

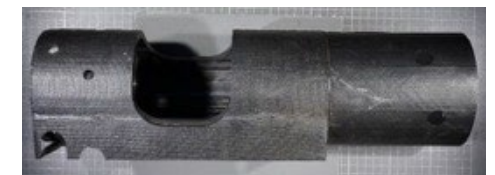


Credit: NASA

Control surface hot structure
(photograph not of hot
structure flown by ESA)

- **SiC/SiC**

- Expect excellent oxidation resistance in air
- Expect excellent reusability
- High interlaminar properties
- Challenges scaling up with tolerances required for airframe hot structures
- Primary design challenge is high coefficient of thermal expansion (CTE) coupled with high modulus



SiC/SiC torque tube

Objectives

- Provide design data for ACC-6
- Increase understanding of ACC-6
- Workforce development

Special topics

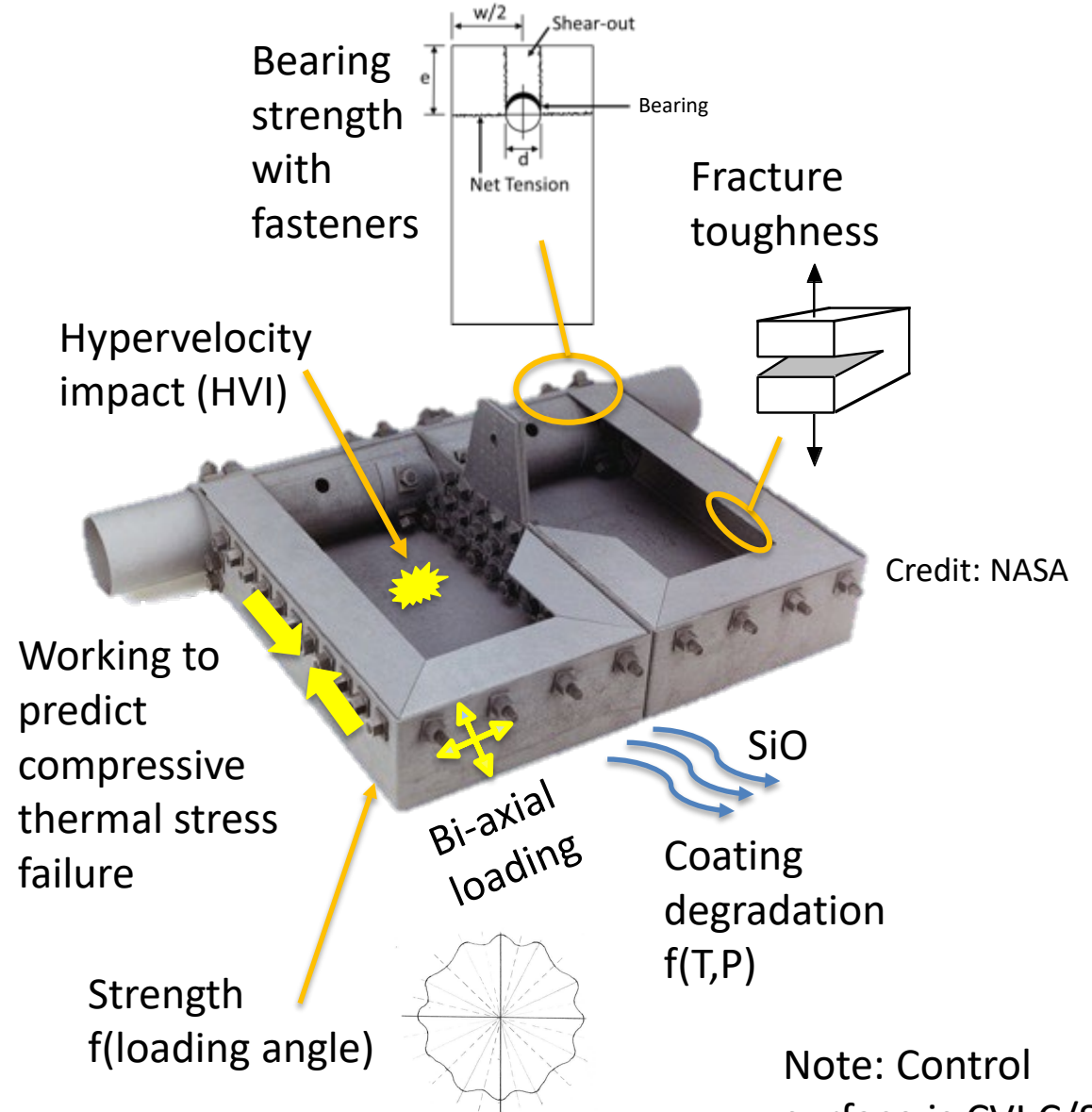
- Flat panels vs. flight structures
- Strength $f(\text{specimen width})$
- DoE for testing
- Manufacturing features
 - Butt splices
 - Assembly bonds



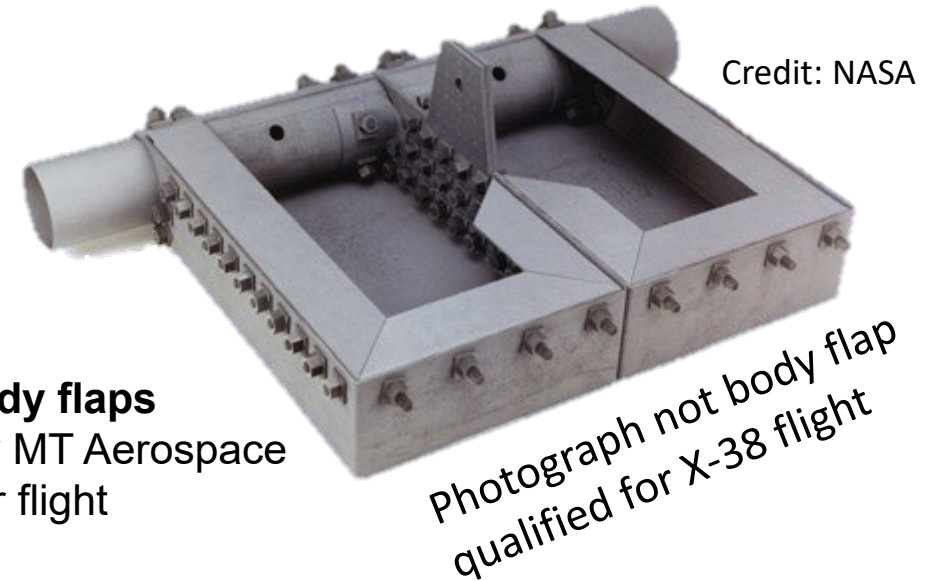
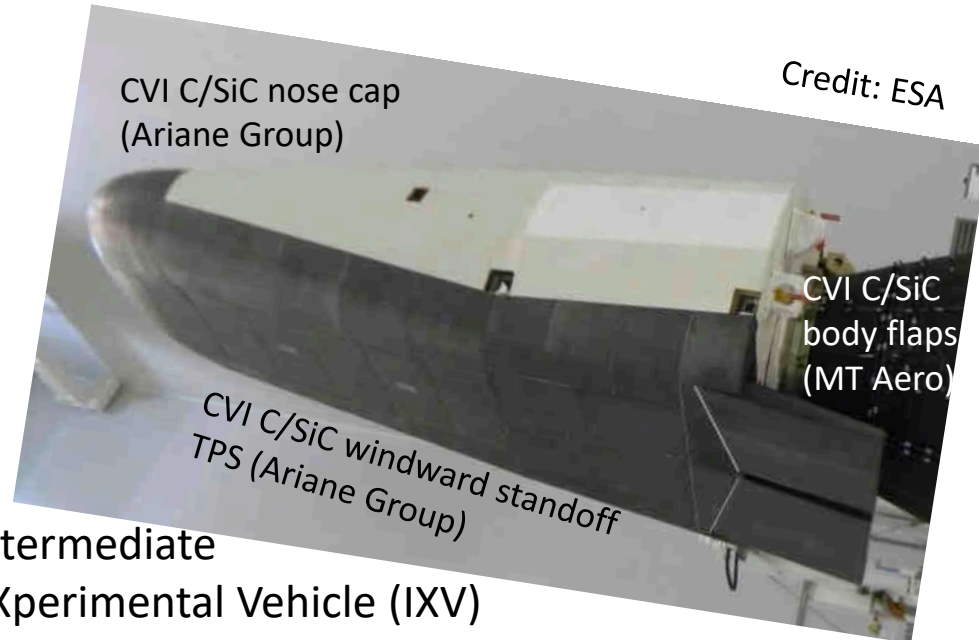
Credit: NASA

Challenges

- Difficult to measure our “weakest” property (ILT) at elevated temp
- Uncertainty in thermal conductivity data



High technology readiness level (TRL) material for single use and reusable hypersonic vehicles



♦ X-38 C/SiC body flaps

- Provided by MT Aerospace
- Qualified for flight



Space Shuttle nose cap shown

♦ X-38 C/SiC nosecap, skirts & chin panel

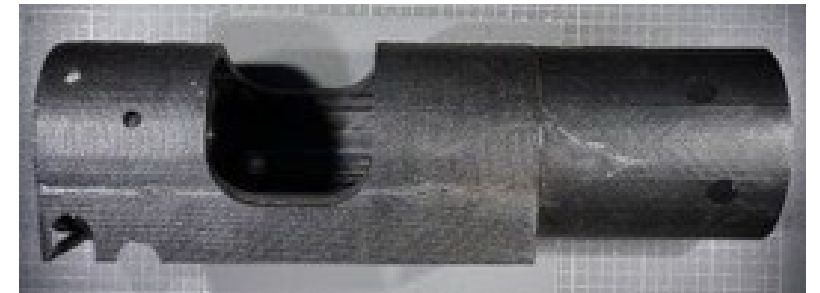
- Nosecap provided by DLR (Germany)
- Nose skirts (2) provided by Astrium (Germany)
- Chin panel provided by MT Aerospace
- Nose assembly has undergone full qualification (qual units)
 - Vibration
 - Thermal (radiant)
 - Mechanical

- **SiC/SiC benefits**

- Demonstrated by GE Aerospace as a highly reusable, high-temperature material system
- High interlaminar properties compared to 2-dimensional ACC-6 and C/SiC
- Strong GE industrial base with market pull
 - Fiber (joint venture) and unidirectional tape pre-preg plants in Huntsville, AL
 - Fabrication facility in Asheville, NC
 - Prototyping facility in Evendale, OH

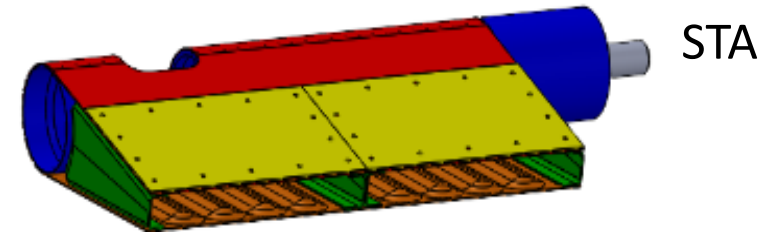
- **SiC/SiC challenges**

- Manufacturing scale-up to the complexity of high tolerance and highly-loaded structures
- High CTE coupled with high modulus
(design issue not a material limitation)

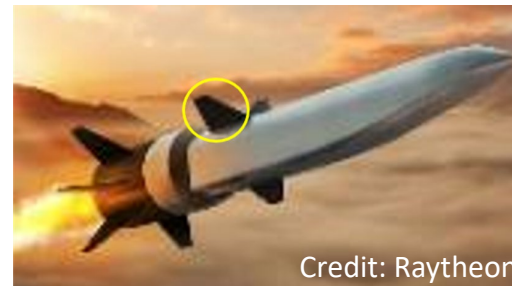


SiC/SiC torque tube

- **Design of X-37-based flaperon component**
 - Detailed design and analyses of X-37-based structural test article (STA)
 - Support building block testing and modeling efforts
 - Gain understanding of SiC/SiC for hot-structure applications
 - MDA completed
- **Ceramic Matrix Composite Control Surface (CMCS)**
 - Different thermal management than STA
 - Thick monolithic versus stiffened-skin structure
- **Hypersonic vehicle wing supporting studies**
 - Static, fatigue, and creep properties for variety of layups
 - Rib, spar, and stiffened-skin trade studies
- **Automated fiber placement (AFP)**
 - High speed, low cost, repeatable structures



STA

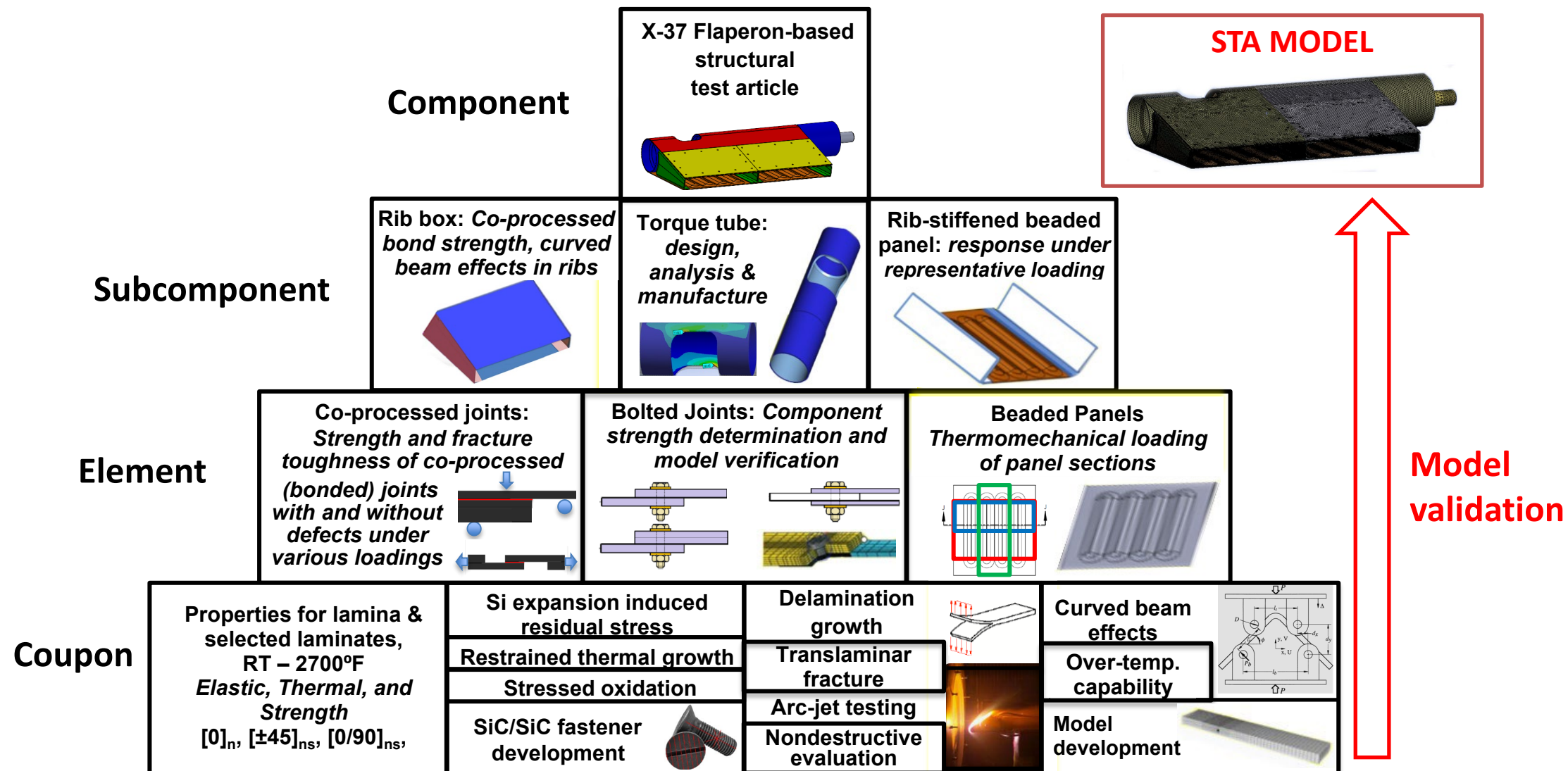


Credit: Raytheon

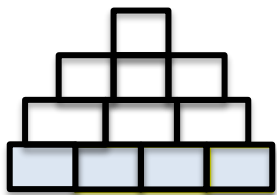
NASA ISAAC



NASA LaRC has extensive on-going efforts toward enabling reusable hypersonic vehicles with SiC/SiC hot structures



- For any material system to be utilized on a flight vehicle, properties must be available for detailed finite element analysis
- Panels are being procured from GE for testing at NIAR (mechanical) and Kratos (thermal)
- **Mechanical Properties (RT – 2700°F)**
 - Static mechanical properties
 - Proportional limit, moduli, and Poisson's ratio
 - Bearing strength
 - Fatigue up to 100k cycles (or failure) and 2 stress levels (above and below the proportional limit)
 - Creep



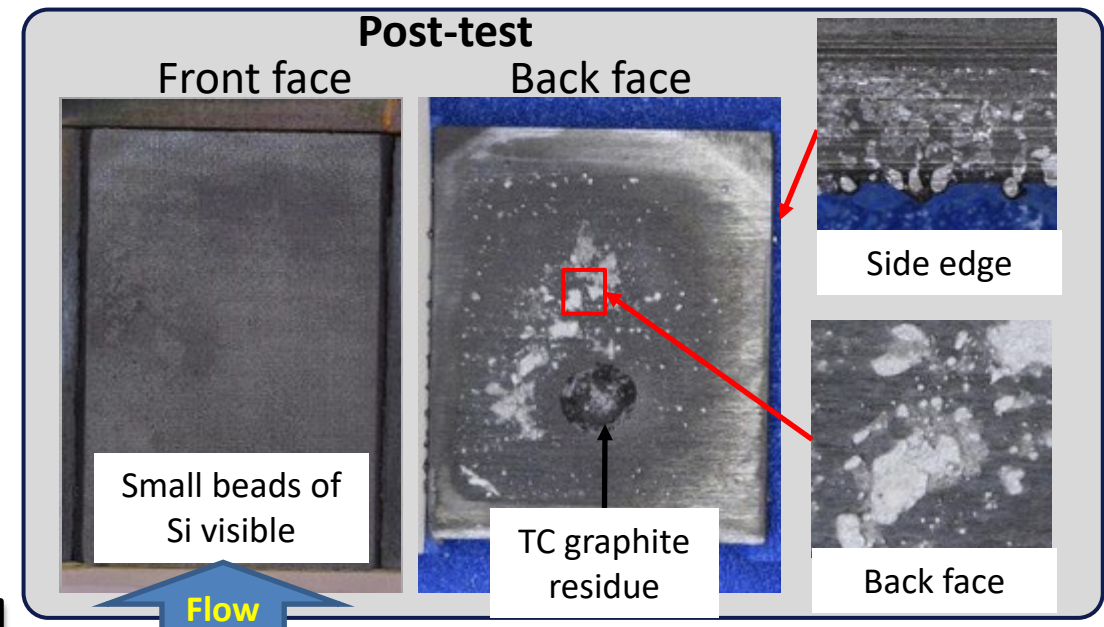
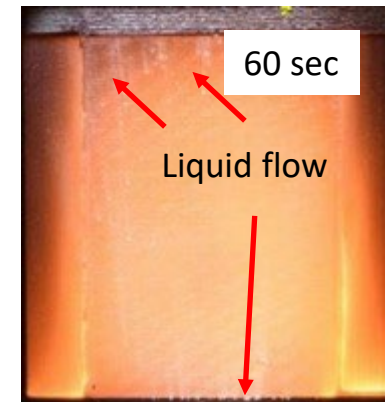
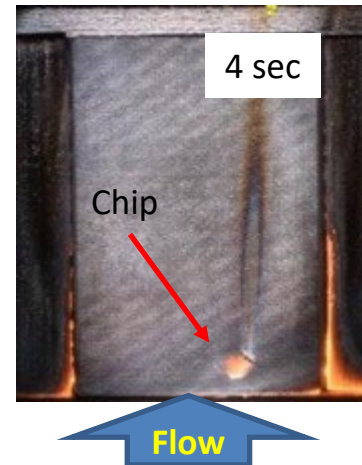
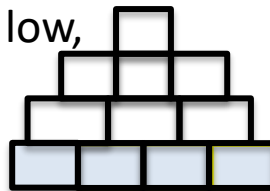
Number Plies	Layup	Number Panels	Comments
16	$[(45/0/-45/90)_{2D}]_s$	7	L & T properties the same, testing only required in 1 dir
12	$[(0/\pm 60)_{2D}]_s$	14	Testing in L&T dirs, fatigue and creep
12	$[(0/90)_{3D}]_s$	7	L & T properties the same, testing only required in 1 dir
12	$[(45/-45)_{3D}]_s$	6	L & T properties same, testing in 1 dir, no fatigue or creep
12	$[(0/90/0)_{2D}]_s$	12	Testing in L&T dirs, no fatigue or creep
12	$[(0/\pm 30)_{2D}]_s$	14	Testing in L&T dirs, fatigue and creep
12	$[(0/\pm 45)_{2D}]_s$	12	Testing in L&T dirs, no fatigue or creep
8	$[0_{4D}]_s$	6	Testing in L&T dirs, no bearing, fatigue or creep
TOTAL		78	

(Fatigue and creep testing at 2200°F)

- Testing performed at Large Core Arc Tunnel (LCAT)
- Use of novel reusable Type-C thermocouples
- Diagnostics
 - Three pyrometers with spot size ~ 0.4 -in. diameter
 - Pre/post-test photography and blue-light scanning
 - Post-test X-ray computed tomography (CT)
- Results
 - All specimens survived full durations

Spec. No.	Run No.	Cold-Wall Heat Flux, Center Slug (BTU/ft ² -s)	Pressure (atm)	Run Time (s)	Max Surface Temp (°F)
ARC-07	1	127	0.199	180	2673
ARC-08	1	140	0.208	64	2640
ARC-09	1	145	0.207	180	2750
ARC-10	1	178	0.271	180	2975
ARC-11	1	177	0.211	300	2725
ARC-11	2	169	0.195	600	2743

- Material contains ~ 20 vol % free Si
Above 2550°F, liquid Si preferentially flowed to cooler back face and side edges where pressure was low, then resolidified



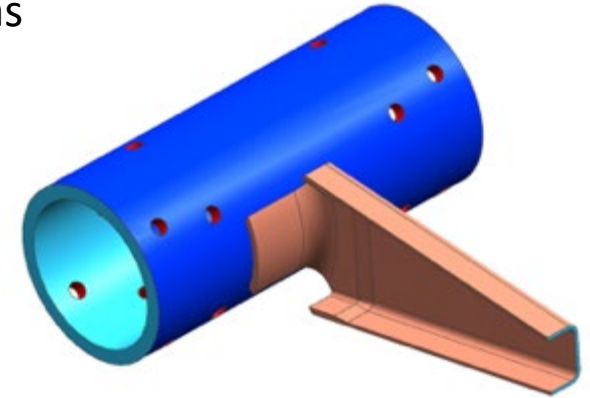
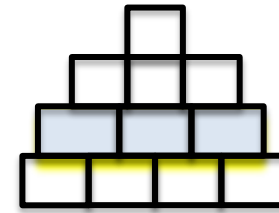
- Detailed post-test analyses in progress

- **Objective**

- Evaluate the manufactured bond line between the torque tube and a single rib, as well as back-to-back ribs bonded to a torque tube

- **Approach**

- Fabricate two of each type of torque tube with ribs
- Apply mechanical load to the ribs to evaluate integrated manufacturing
- Perform parallel experimental studies to determine bond strength and toughness under various modes of loading

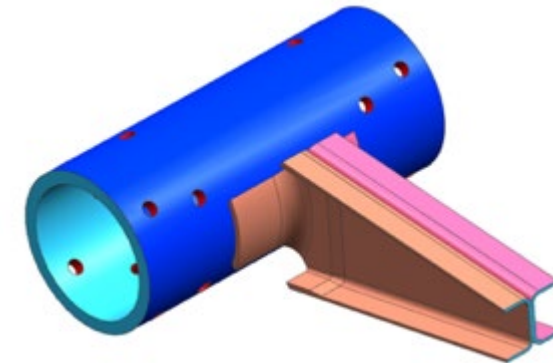


- **Accomplishments / status**

- Modifying Task Order to address torque tube / rib manufacturing

- **Plans**

- Evaluate bond line via nondestructive evaluation (NDE)
- Perform finite element analysis (FEA) to predict load at which the bond will fail and the load and failure mode for structural failure.
- Perform room temperature tests applying load to the ribs to evaluate failure mode and load
- Perform post-test NDE
- Perform post-test FEA to correlate test and analysis



• Objective

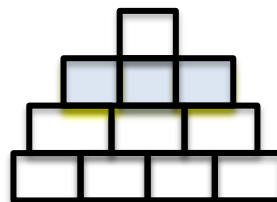
- Verify impact of ply-breaks and other manufacturing defects on the load-carrying capability of a SiC/SiC torque tube for an X-37-based flaperon
- Develop and validate SiC/SiC modeling approaches for complex airframe hot structures
- Identify damage mechanisms leading to torque tube failure

• Approach

- Test MDA torque tube in torsion and offset tension-bending load cases, which are the driving load cases as predicted by STA model
- FEA-informed fixture design and predicted failure loads
- Pre- and post-test NDE (CT scanning) for defect quantification and VCCT modeling
- In-situ monitoring with strain gauges and digital image correlation (DIC)

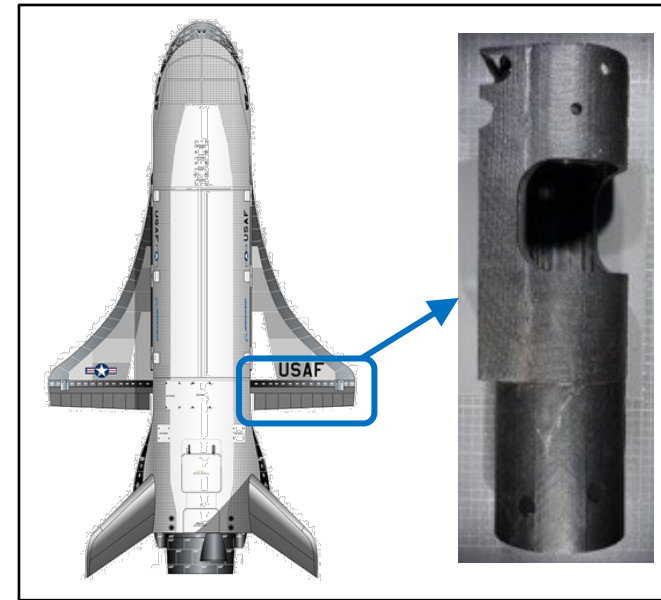
• Accomplishments / Status

- FEA predictions complete, test plan drafted, parts fabricated, NDE of tube in progress



• Plans

- Instrumentation, testing, data analysis



X-37 flaperon and extracted MDA torque tube (test article)

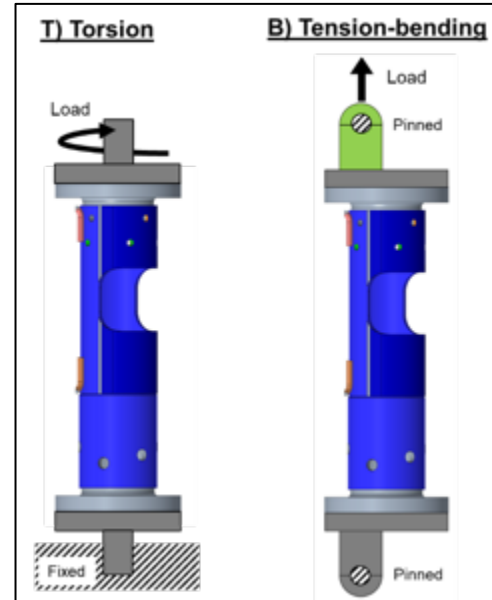
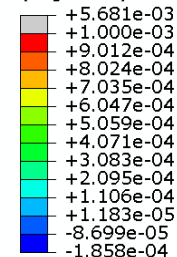
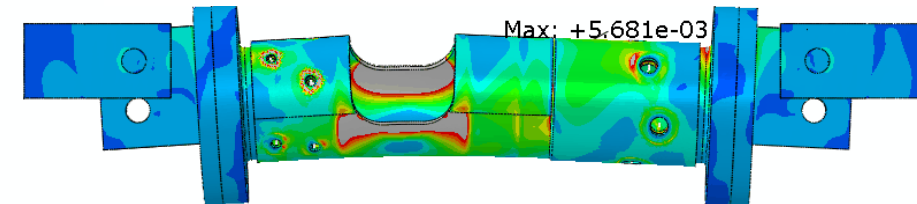


Diagram of loading configurations and fixturing

E, Max. Principal
Rel. radius = 1.0000, Angle = -90.0000
(Avg: 75%)



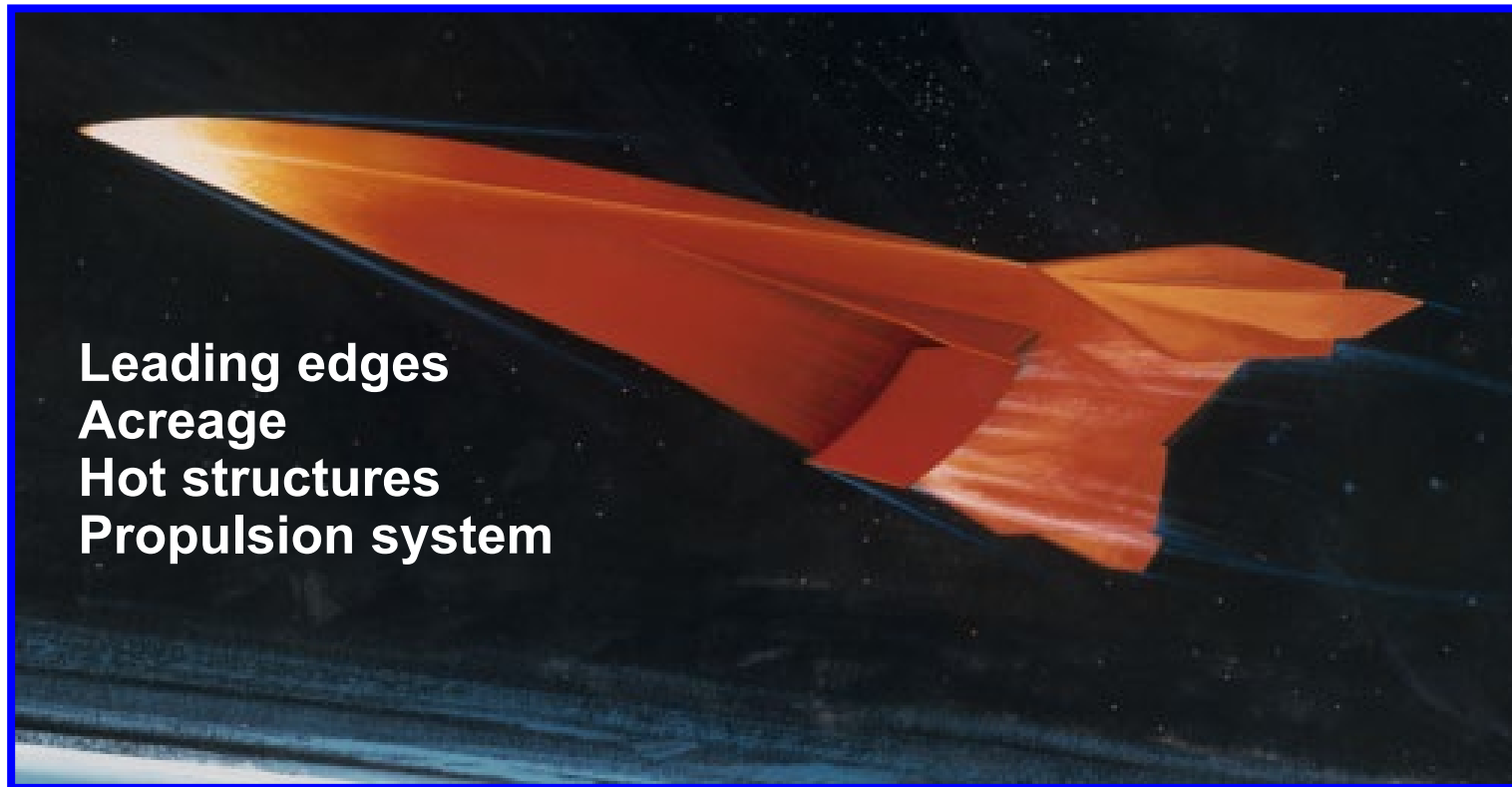
Max: +5.681e-03
Elem: PART-1-1.8061
Node: 40886



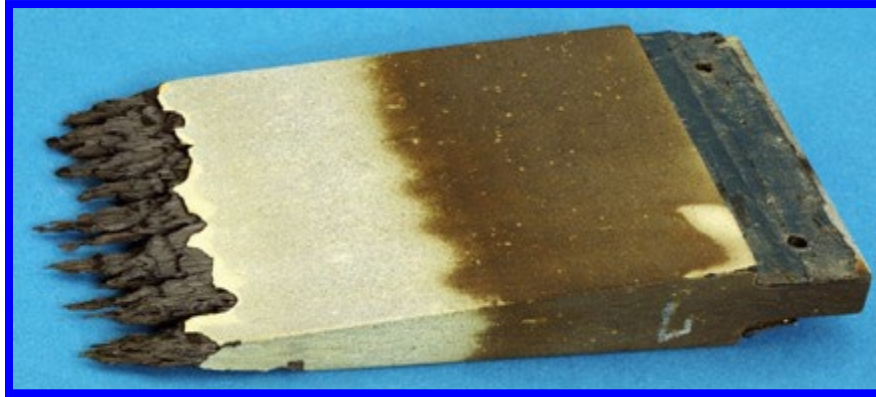
Step: Step-2, IMPOSE OFFSET AXIAL LOADING
Increment 23: Step Time = 1.000
Primary Var: E, Max. Principal

FEA strain predictions for tension-bending test

- CMCs are the family of materials that will enable hypersonic vehicles



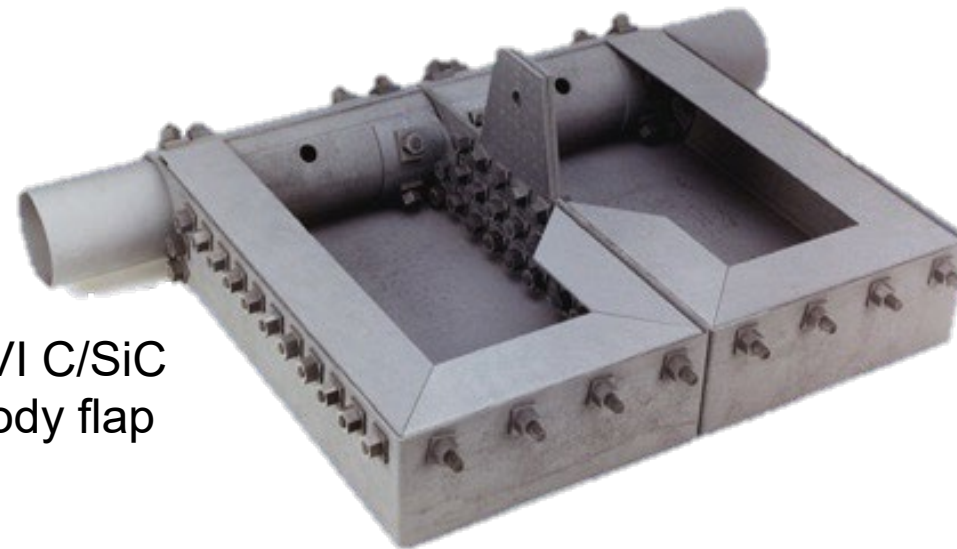
- For most hypersonic vehicles, there are two key materials and structures technical challenges



- **Oxidation resistance**
- **Mission life**
 - Cycles under combined loads
 - Inspection
 - Repair
 - Life prediction



A state-of-the-art material is not the same thing as a state-of-the-art structure



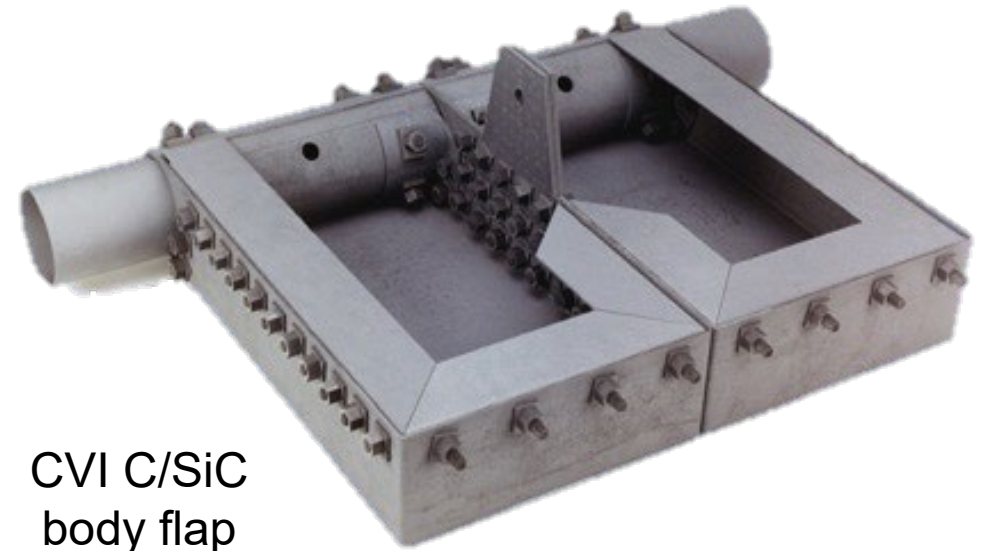
CVI C/SiC
body flap

Big difference!

Experience is gained through building flight hardware and integrating it into flight vehicles

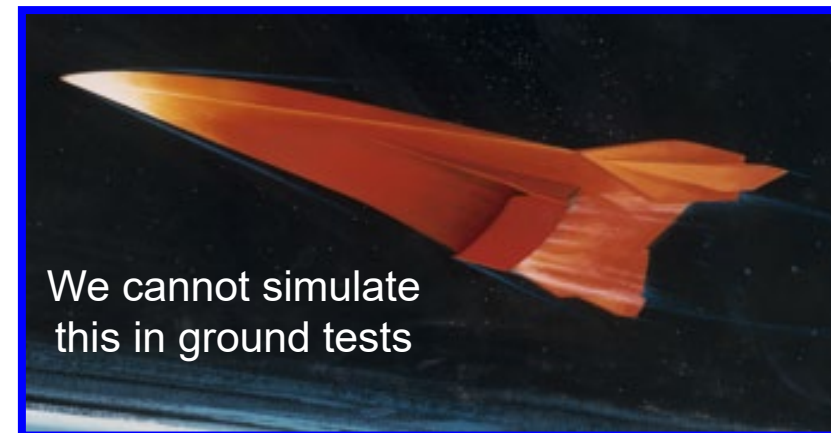
- Thick
- Complex curvature
- Large scale
- Low interlaminar properties
- Delamination
- Critical flaw size
- Non-destructive inspection
- Tooling
- Assembly methods and tolerances
- Reproducibility
- Fabrication modeling
- Design of manufacturable structures (cannot throw the design “over the wall”)
- Affordable (cost and schedule) fabrication techniques

**Fabrication challenges
are process dependent**

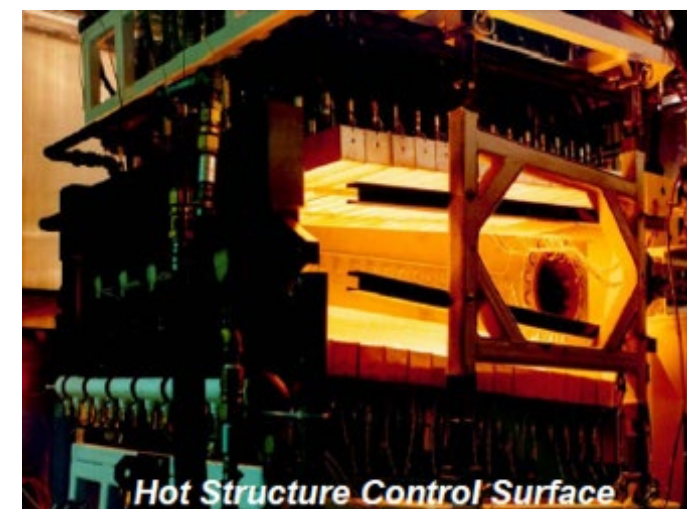


CVI C/SiC
body flap

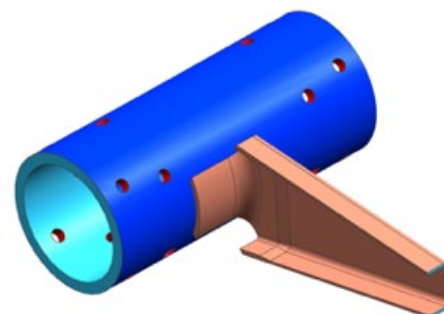
- How do we qualify the vehicle for flight?
- We are unable to test many components in relevant, combined loads, environments (even small scale)
 - Thermal, mechanical, plasma, shear, oxygen partial pressure, vibration and acoustic, etc.
 - Apply appropriate boundary conditions over entire structure
 - Thermal gradients (spatial and temporal) from boundary layer transition
- **Extensive testing is required**
 - Performance testing and benchmarking for analyses
- **Building block approach**



Component test



Sub-element test



Material / coupon test

Test as much as you can, and still include adequate margins for uncertainties



Workforce Development

Langley Hot Structures Team



- **Interns (undergraduate, masters, and PhD)**
 - 58 students (107 sessions) since 2013
 - 23 with aerospace-related jobs (> 10 still in school)
 - Psionic Technologies, JPL, Lockheed Martin
 - Peraton, Boeing, Blue Origin, C-CAT, Actalent
 - Northrop Grumman, Lockheed Martin, HRL
 - Motiv Space Robotics, NASA Langley (3 former interns)
 - NASA Marshall, Relativity Space, SpaceX
 - Cocoa Beach / CMS, AIAA, AFOSR, and JANNAF attendance and papers

Interns on education /
team-building trip (all
4 planning to present
at CMS in January)



- **Early-career mentorship**

- Conference attendance: CMS, NSMMS, JANNAF, HTSC
- International conference: FAR, HiSST, HT-CMC
- Partner visits:
 - NASA Glenn, GE, APL
 - CA: HRL, Allcomp, Ultramet, NASA Armstrong
 - AL/MS: AvMC, PPI, MSFC, Kratos, GE, ReLogic, Mississippi State Univ.
 - Northeast: GE GRC, TEAM (Spirit), Draper Labs, Textron, Bond Enterprise, FMI (Spirit), Exothermics, PSI

Early-career employees
on NE partner visit



- Hypersonic vehicles will require us to move beyond an insulated aluminum or titanium “airplane” to a vehicle with multiple TPS and hot-structure approaches
- Results to-date support that SiC/SiC may be a key enabler of reusable hot structures for hypersonic vehicles
- Our ability to build and fly these vehicles successfully will depend on our ability to utilize multiple types of CMC structures, first having solved the environmental durability and fabrication challenges