

Analysis of Mars 2020 Entry with Coupled Material Response and CFD

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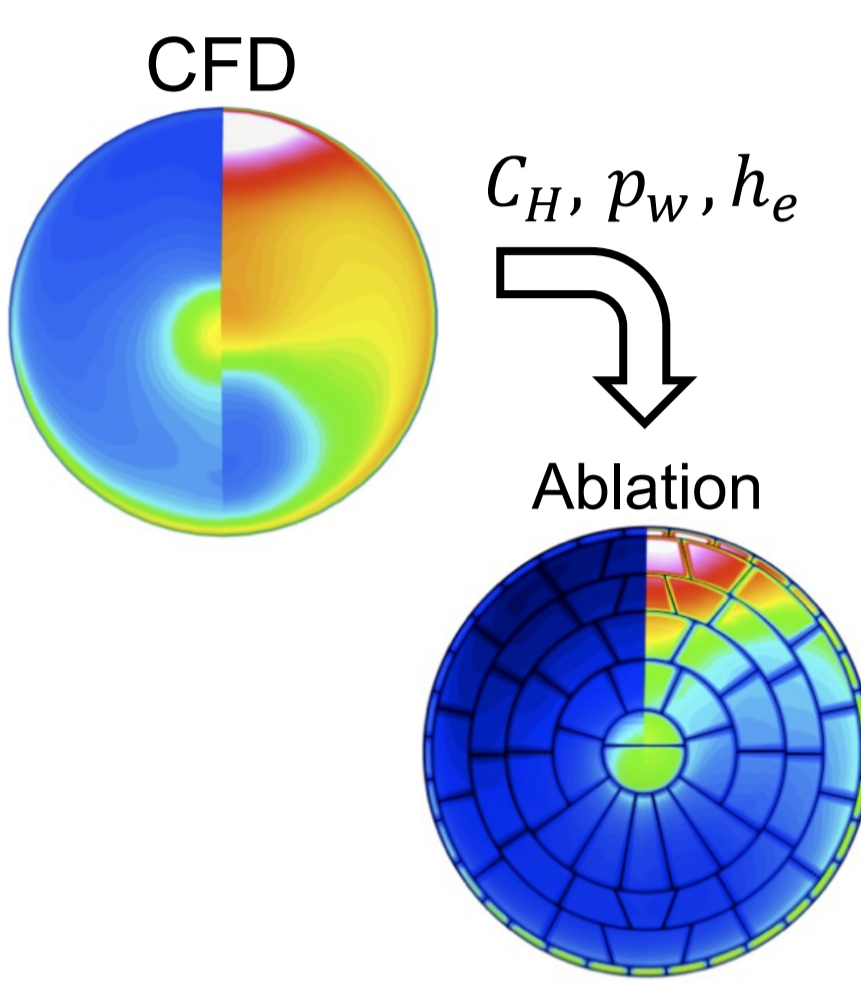
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Objective

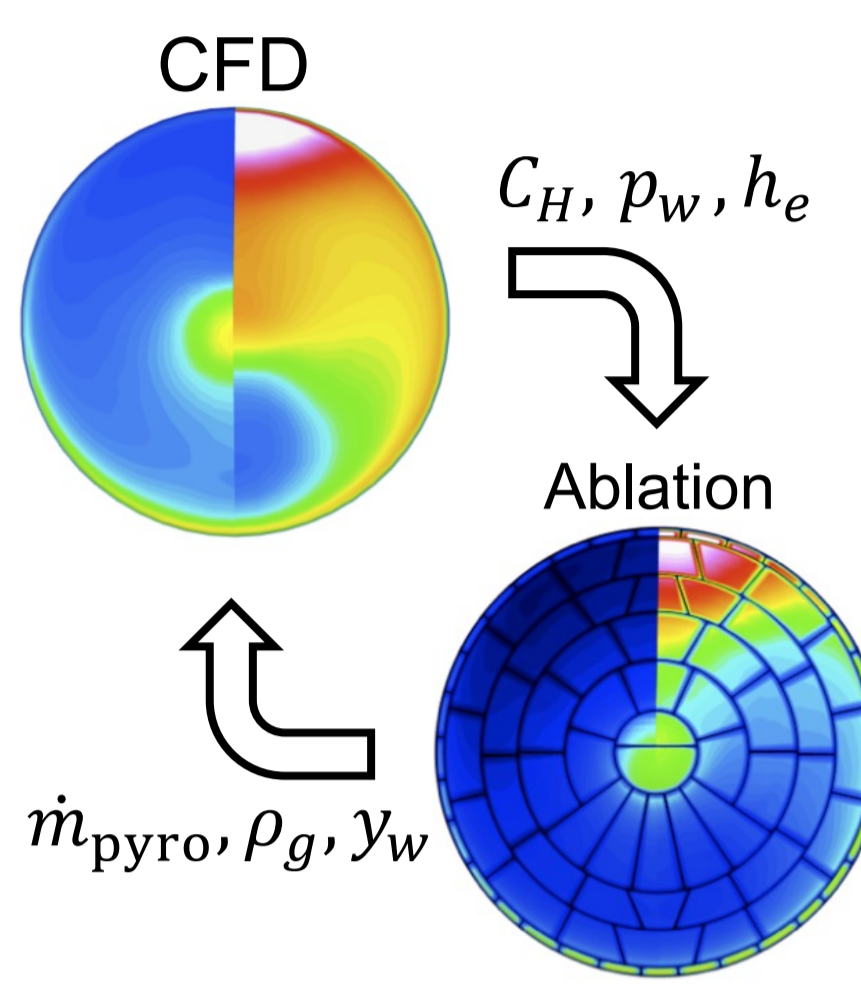
The objective of this work is to showcase and analyze the coupling between the material response and the aerothermal environment in simulating the Mars atmospheric entry of the Mars 2020 in 3D. This work represents an important milestone toward the development of validated predictive capabilities for designing thermal protection systems for planetary probes.

Uncoupled approach



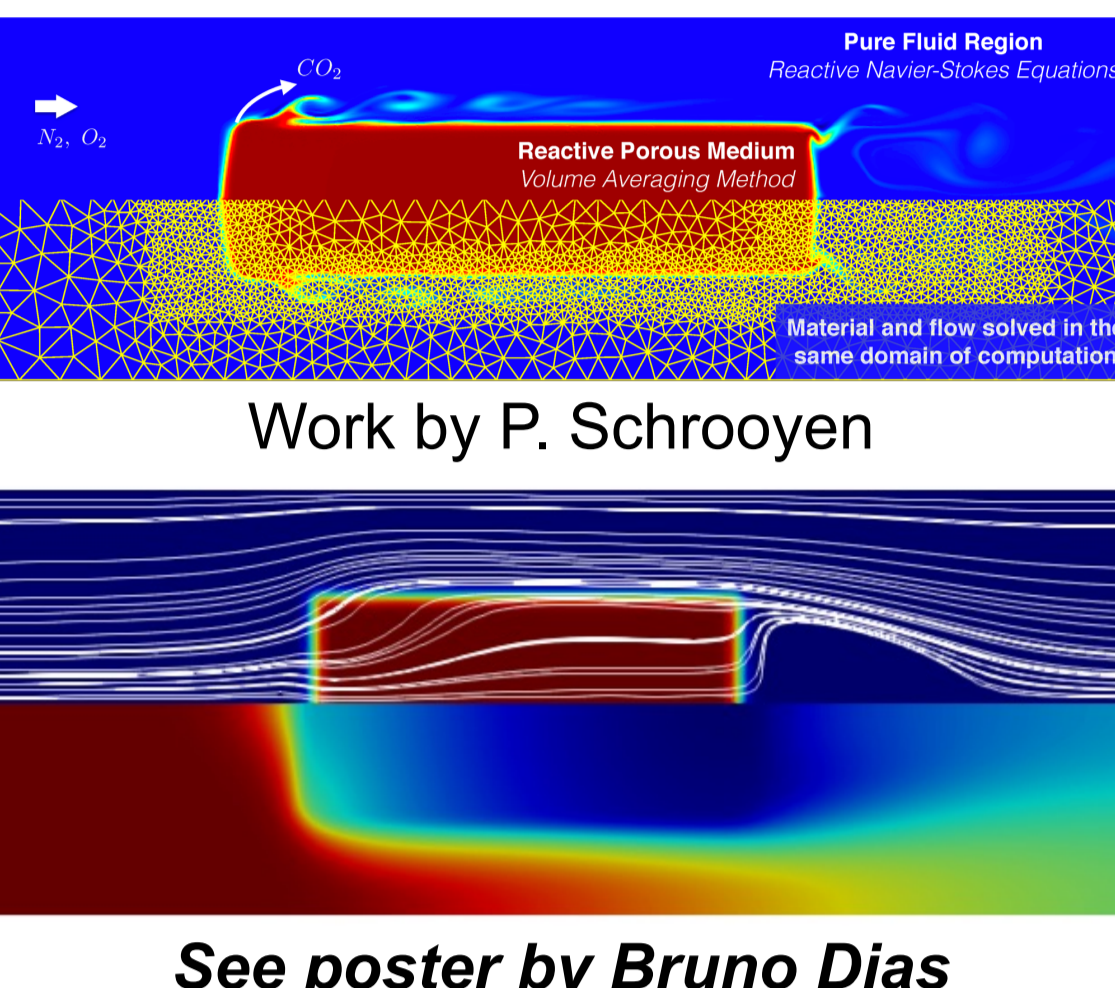
- Uncoupled CFD and MR simulations.
- Approximate methodologies for mass and energy transfer.

Coupled approach



- Simultaneous CFD and MR simulations.
- Direct exchange of information through BCs.

Unified approach



Work by P. Schrooyen

See poster by Bruno Dias

- Unified CFD and MR simulations.
- No need for exchange of information.

We are comparing the uncoupled and coupled approaches for Mars entry conditions

Mars 2020 Supercomputer Runtime and Usage

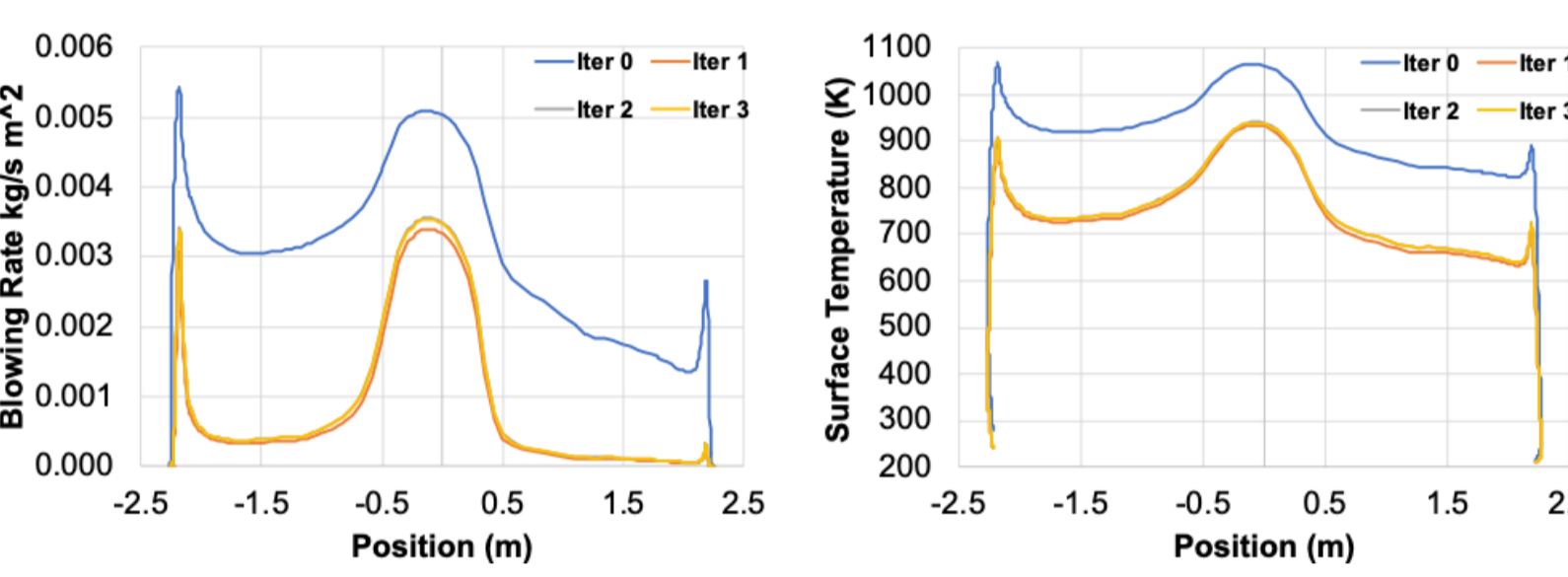
Restart Capability implemented in PATO

- Do not compute entire trajectory for each iteration.
- Cut down on simulation time by over half.

Massive Mars 2020 Coupled Simulations

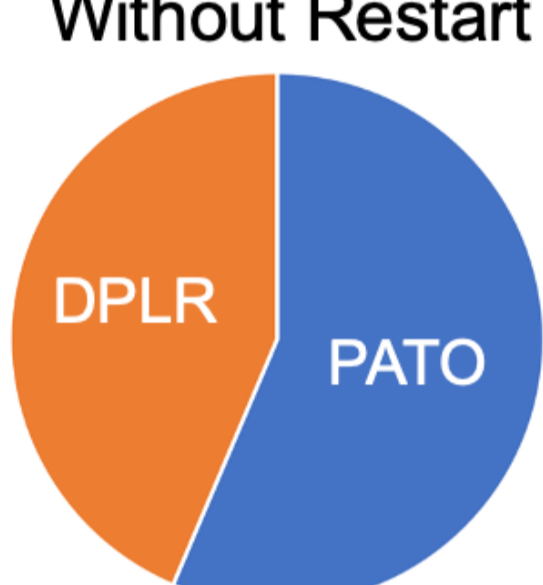
Resources:	600 processors (Haswell)
Without Restart:	30 days
With Restart:	14 days
3D Refined Grid:	9M (DPLR) & 1M (PATO)

Simulations require 1 to 3 iterations to converge




Computing time for each code

Without Restart



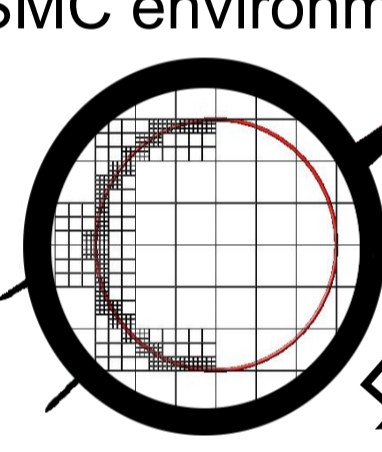
With Restart



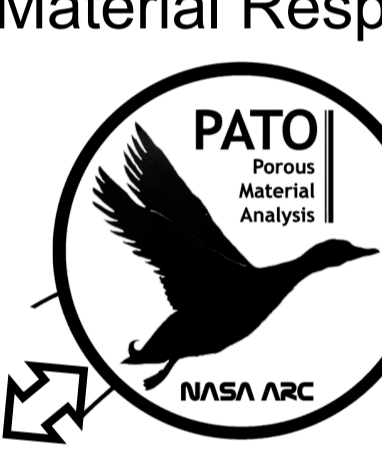
Coupling Tool

Interfaces and automates the interaction between NASA tools


SPARTA^[1]
DSMC environments



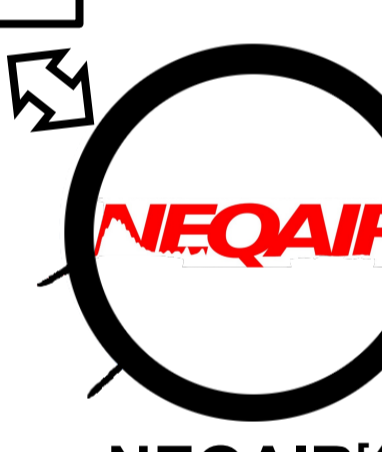
PATO^[2]
Material Response

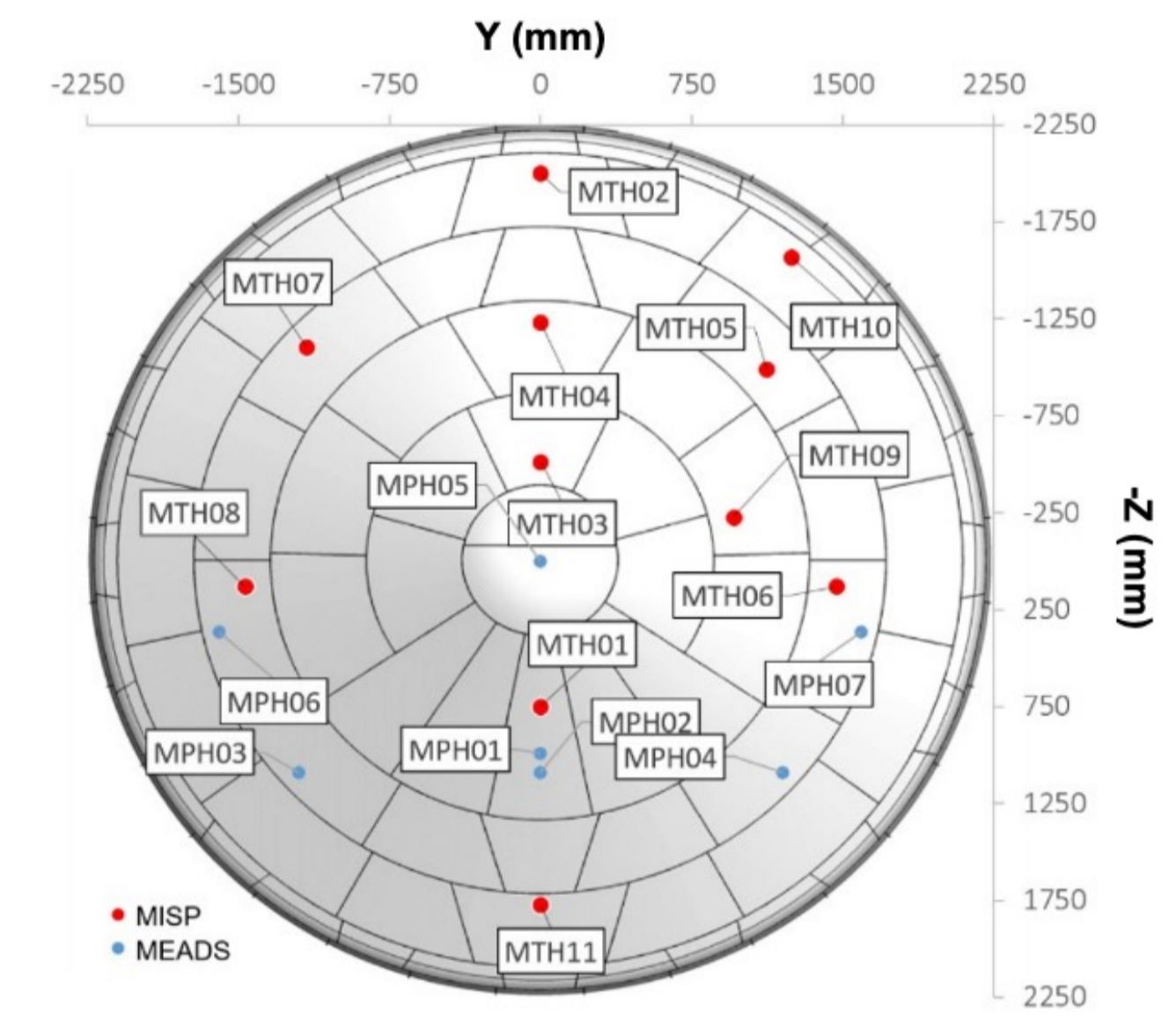


DPLR^[3]
Aerothermal Environment



NEQAIR^[4]
Radiation

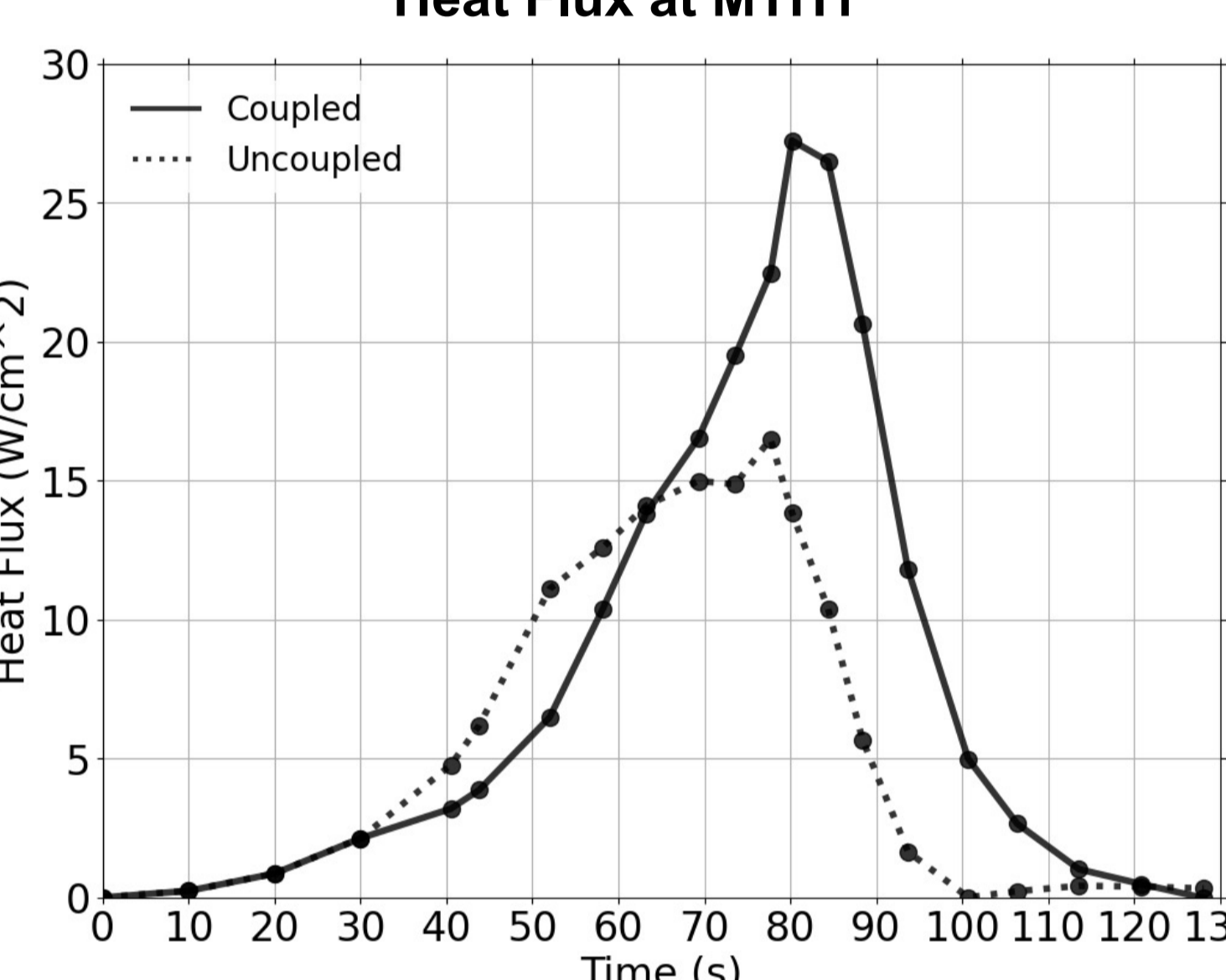




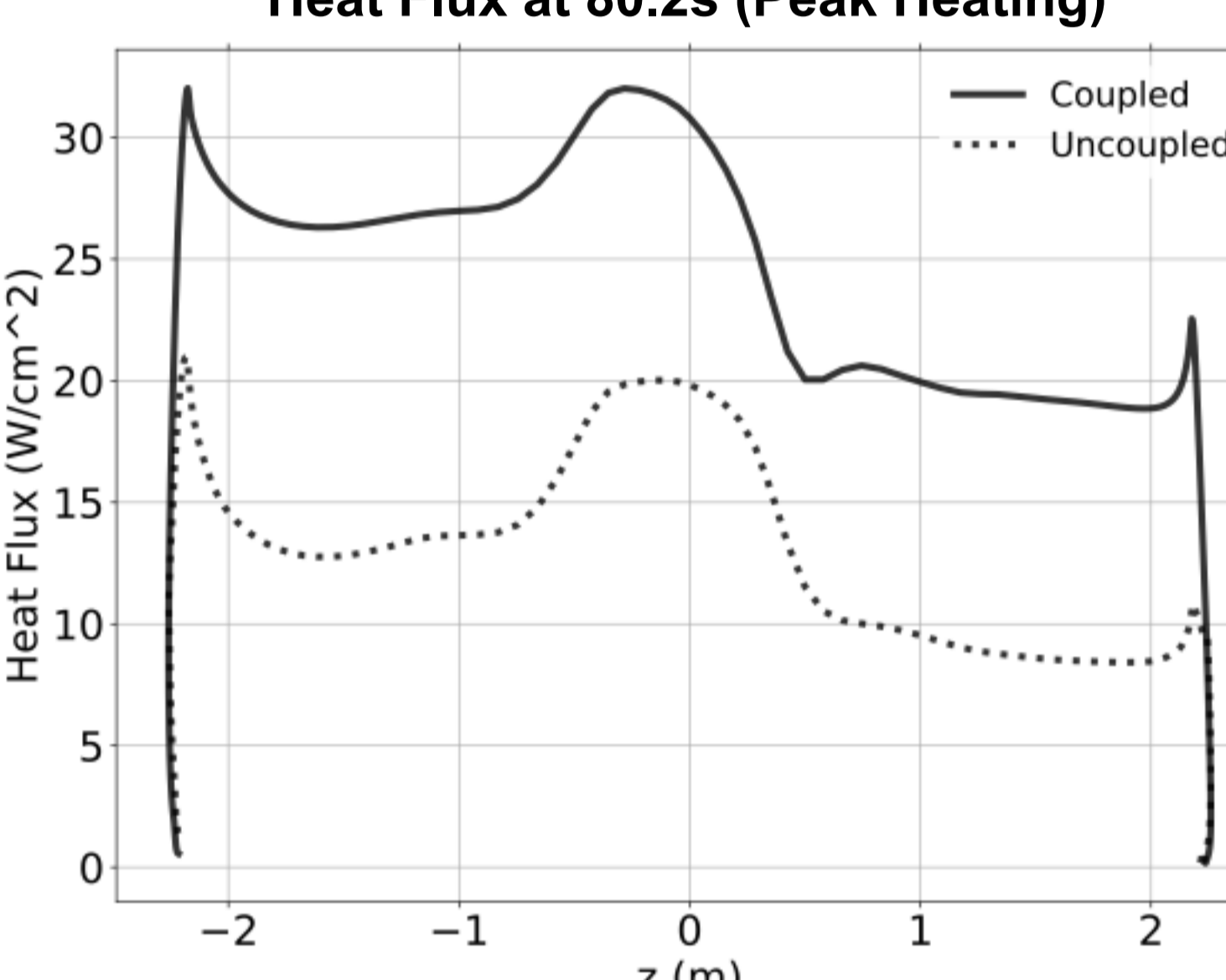
MEDLI2 Plug Layout on Mars 2020 Heatshield

Mars 2020 Coupled and Uncoupled Cases

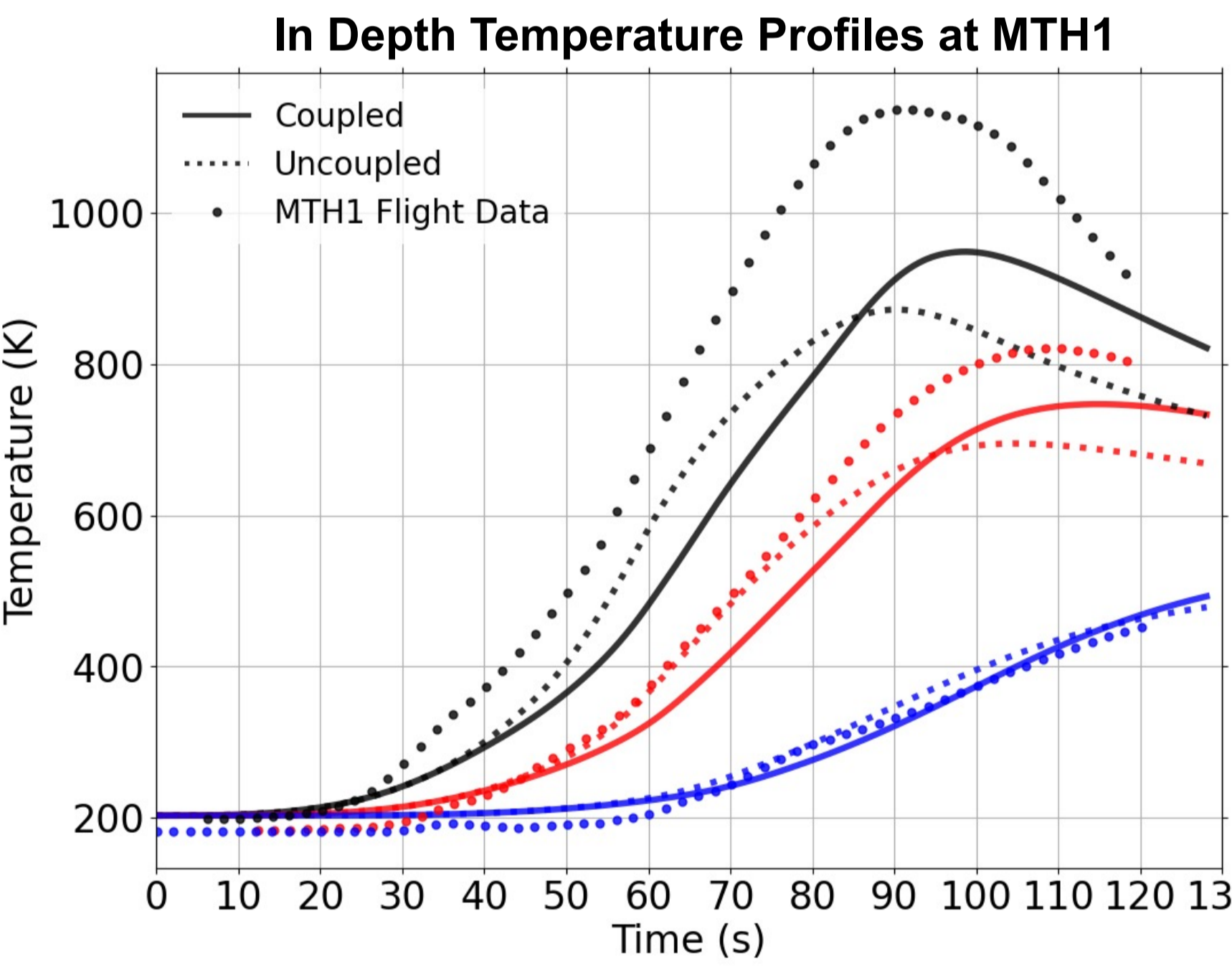
Heat Flux at MTH1



Heat Flux at 80.2s (Peak Heating)



In Depth Temperature Profiles at MTH1



- Flow assumed to be laminar and did not include radiation or recession.
- Underpredicting flight data. Radiation accounts for some of the underprediction, but not all.
- Similar trends as with previous study on MSL.
- Higher heating at peak with coupled cases.
- Lower heating initially.

Coupling Methodology

Blowing correction

$$C_H = C_H \frac{\ln\{1 + 2\lambda(B'_{pyro} + B'_{char})\}}{2\lambda(B'_{pyro} + B'_{char})}$$

B' Boundary

1. DPLR No blowing
2. NEQAIR Radiation
3. PATO Fixed blowing correction

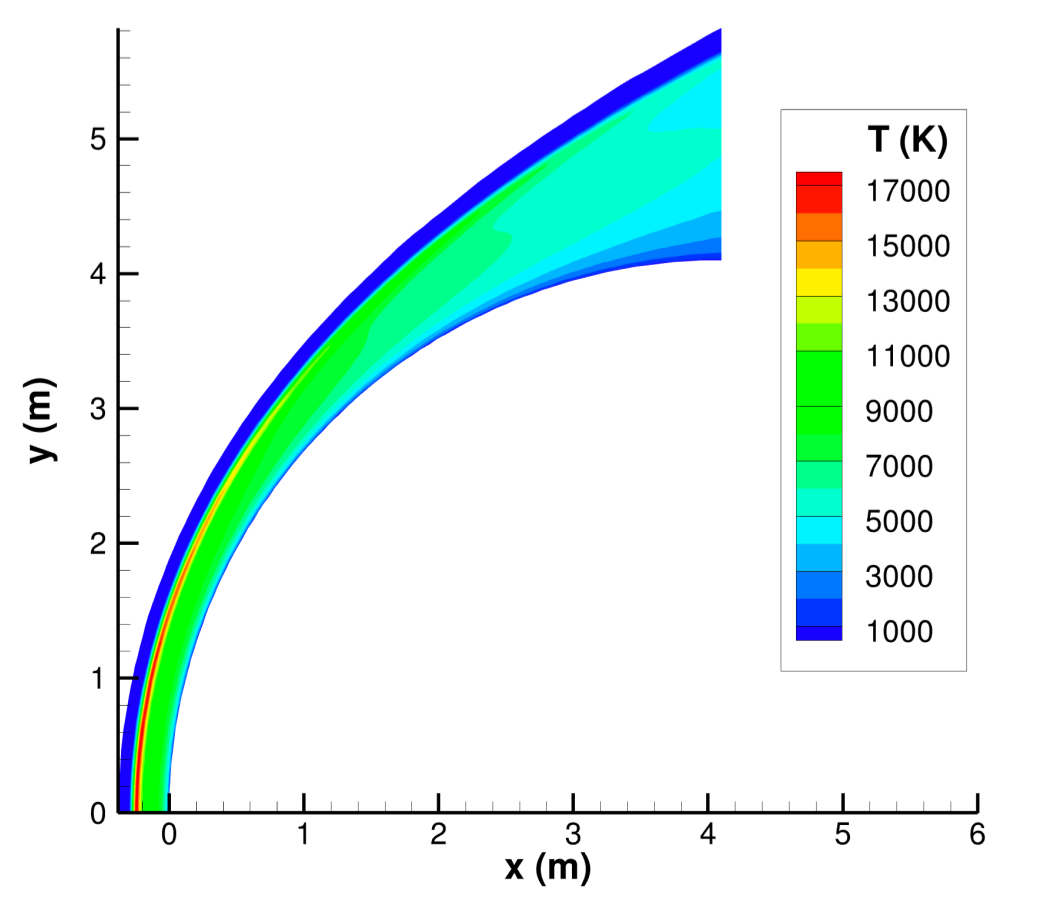
Heat Flux Boundary

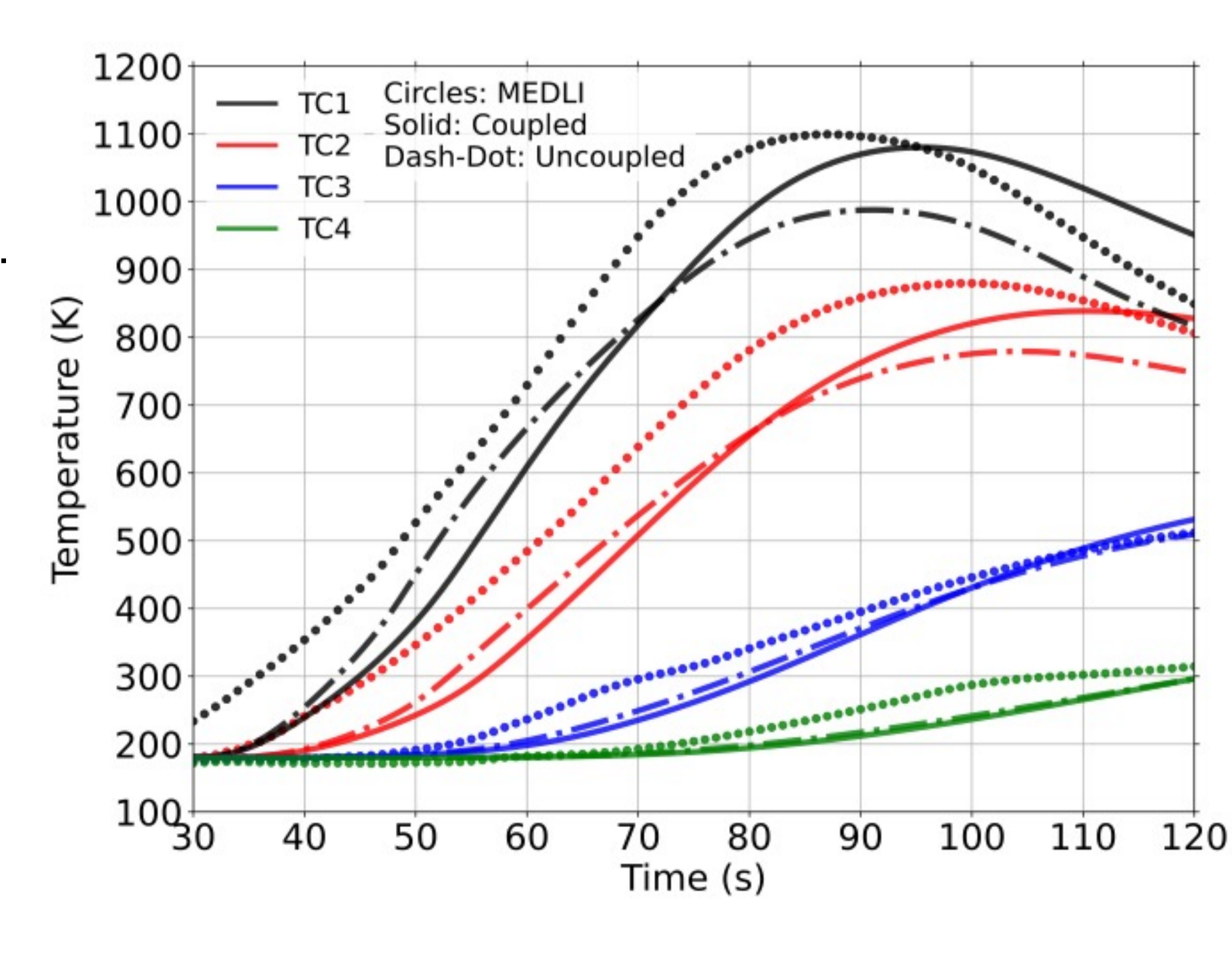
4. DPLR Blowing from PATO
5. NEQAIR Radiation
6. PATO No blowing correction

Convergence of surface temperature → END

Sphere Case for MSL

- 2D axisymmetric sphere case with environments from MSL MISP1 [5].
- Includes radiative heating.
- No DSMC or char blowing/recession.
- Good agreement with flight data.



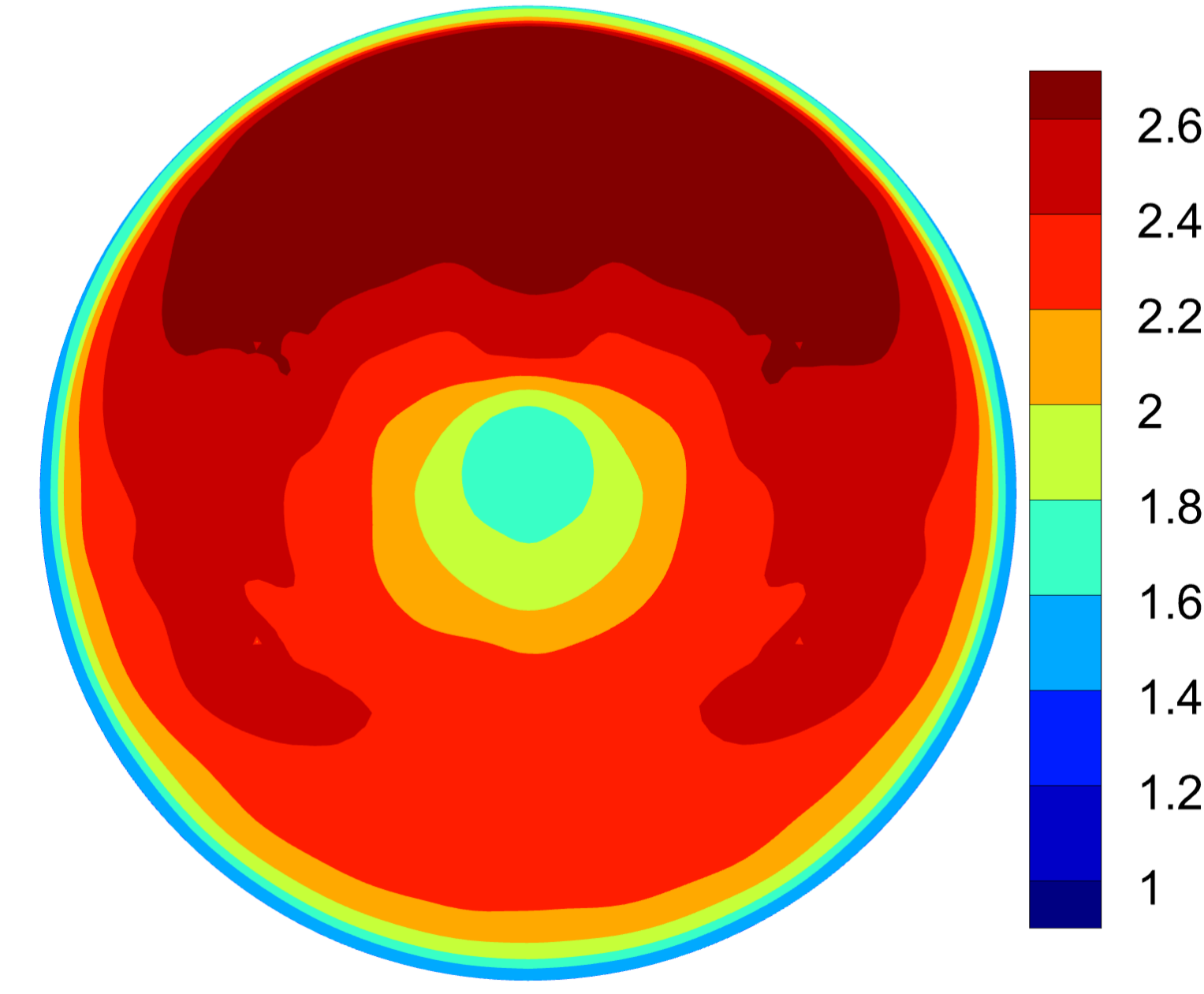


Conclusions

- Significant differences in heating between coupled and uncoupled cases
- Underpredicting flight data. Adding radiation and char blowing could possibly alleviate discrepancies.

Future Work:

- Efforts have been made to create a coupling process which includes char blowing/recession [6].
 - See poster by Georgios Bellas Chatzigeorgis and talk by Brett Cruden
- A Mars 2020 coupled case which includes radiation is currently being run.
- Using comparison between coupled and uncoupled cases to create new blowing correction models.



References

- [1] S.J. Plimpton *et al.* (2019), Phys. Fluids, 31(8), 086101.
- [2] J. Lachaud *et al.* (2017), Int J Heat Mass Tran, 108, 1406–1417.
- [3] M.J. Wright *et al.* (2009), DPLR Code User Manual: Acadia-Version 4.01.1.
- [4] A.M. Brandis and B.A. Cruden (2014), NEQAIRv14.0 Release Notes: Nonequilibrium and Equilibrium Radiative Transport.
- [5] J.M. Thornton *et al.* (2023), AIAA SCITECH 2023 Forum.
- [6] B.A. Cruden *et al.* (2023), AIAA AVIATION 2023 Forum.