

USM3D-ME Solutions for RANS Test Suite of High-Fidelity CFD Verification Workshop 2024

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Outline

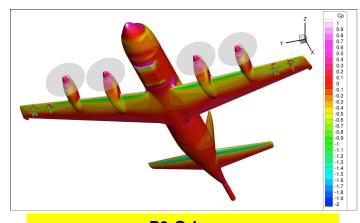


- USM3D-ME Overview
- Results for the RANS Test Suite
 - Joukowski Airfoil
 - NACA 0012 Wing in Tunnel
 - **O CRM High-Lift Wing-Body Configuration**
- Summary

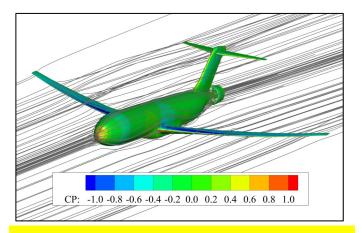
USM3D-ME Features for Workshop Solutions



- Cell-centered, finite-volume, mixed-element, unstructured-grid discretization for Reynolds-averaged Navier-Stokes (RANS) equations
- Second-order spatial accuracy
- Upwind spatial discretization for meanflow inviscid flux
 - Cell gradients using Green-Gauss method and nodal solution
 - No gradient limiter
 - o Roe's flux-difference splitting scheme
- Second-order diffusion terms; face-gradients using Mitchell's method
- Nonlinear Spalart-Allmaras turbulence model, SA-neg-QCR2000-R (Crot=1)
 - Discretization of convective term is first order, upwind
 - Modified discretization of diffusion term for improved robustness
- Hierarchical Adaptive Nonlinear iteration Method (HANIM)
 - Decoupled meanflow and turbulence-model preconditioners with approximate Jacobian
 - Jacobian-free Newton-Krylov solver for second-order linearization
 - Nonlinear control for solution updates
 - Adaptive CFL
- Solutions initialized using freestream conditions
- Several iterations performed with first-order meanflow discretization before switching to second order



P3-Orion
Courtesy: Craig Hunter (NASA LaRC)



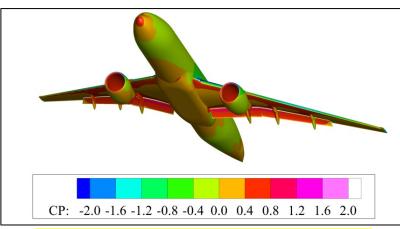
CRM-TCT Configuration
Courtesy: Michael Bozeman (NASA LaRC)

USM3D-ME Other Key Features Building on Legacy USM3D Flow Solver

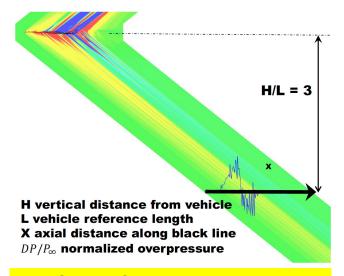


- Standard and specialized boundary conditions
- Force-term approach for propellers and other applications
- Time integration
 - Second-order BDF2 for temporal accuracy
- Rigid-body 6-DoF motion support
- Parallelized using MPI paradigm; excellent scalability
- Internal extraction of solution functions (e.g., pressure signatures)
- Extensive verification through benchmark flow solutions and participation in community workshops
- 20–30x increase in solution throughput relative to legacy USM3D on complex configuration
- Leveraged capabilities
 - Integration with NASA CDISC for knowledge-based design
 - Integration with NASA grid adaptation tool REFINE

AIAA 2013-2541, *AIAA Journal*, 54(9) 2016, *AIAA Journal*, 55(10) 2017, AIAA 2019-2333, *AIAA Journal*, 59(8) 2021, *AIAA Journal*, 59(11) 2021



CRM-HL Configuration (HLPW4)
Courtesy: Michael Bozeman(NASA LaRC)

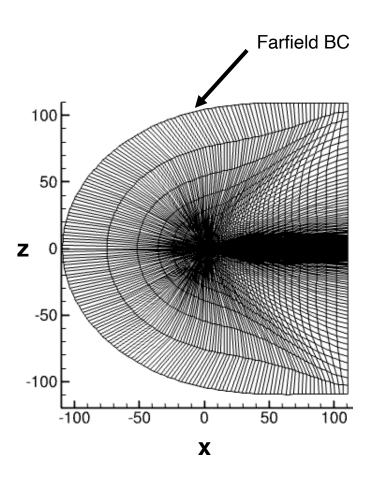


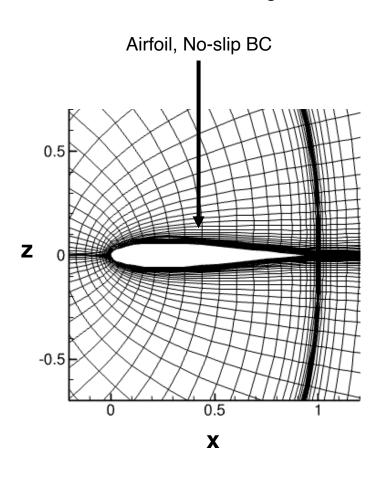
Generic Supersonic Transport
Courtesy: Alaa Elmiligui (NASA LaRC)

Joukowski Airfoil







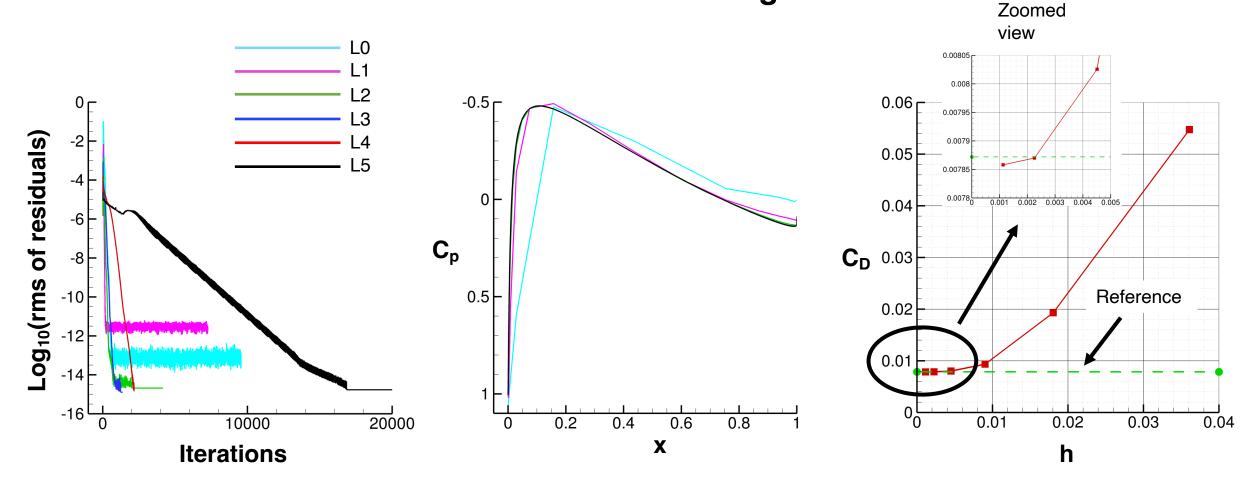


MIT Grid Family

| Grid Identifier | Nodes | Cells |
|--------------------|--------|--------|
| L0 | 1.6K | 0.8K |
| L1 | 6.3K | 3.1K |
| L2 | 25.0K | 12.3K |
| L3 | 99.1K | 49.2K |
| L4 | 394.8K | 196.6K |
| L5 | 1.6M | 786.4K |

Joukowski Airfoil Iterative and Grid Convergence



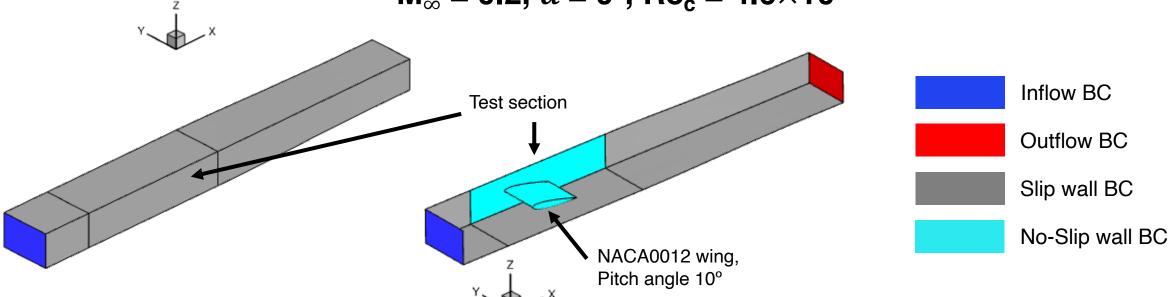


- Meanflow and SA model residuals are combined
- First-order iterations are not shown in the plots
- Reference is fourth-order MIT FEM solution on finest adaptive grid

NACA 0012 Wing in Tunnel

 $M_{\infty} = 0.2$, $\alpha = 0^{\circ}$, $Re_{c} = 4.6 \times 10^{6}$





HeldenMesh Family

| Grid Identifier | Nodes | Cells |
|--------------------|--------|--------|
| A1 | 40.6K | 162.1K |
| B1 | 166.6K | 520.8K |
| C1 | 990.9K | 2.5M |
| D1 | 6.8M | 15.7M |
| E1 | 51.1M | 111.2M |

Pointwise Family, Version 4

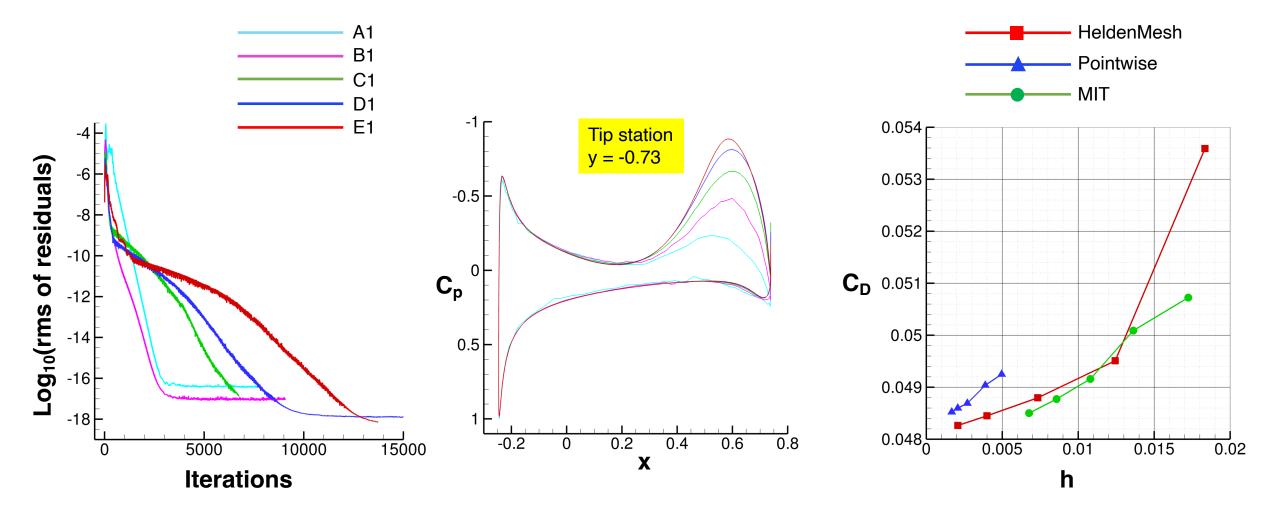
| Grid Identifier | Nodes | Cells |
|--------------------|-------|--------|
| 1.5 | 3.3M | 8.2M |
| 2.0 | 6.8M | 17.1M |
| 3.0 | 19.5M | 50.7M |
| 4.0 | 42.3M | 112.9M |
| 5.0 | 78.0M | 212.1M |

MIT Solution-Adapted Grids

| Grid Identifier | Nodes | Cells |
|--------------------|--------|--------|
| 40K | 36.7K | 195.2K |
| 80K | 72.4K | 395.7K |
| 160K | 142.5K | 794.5K |
| 320K | 280.6K | 1.6M |
| 640K | 566.5K | 3.2M |

NACA 0012 Wing in Tunnel Iterative and Grid Convergence



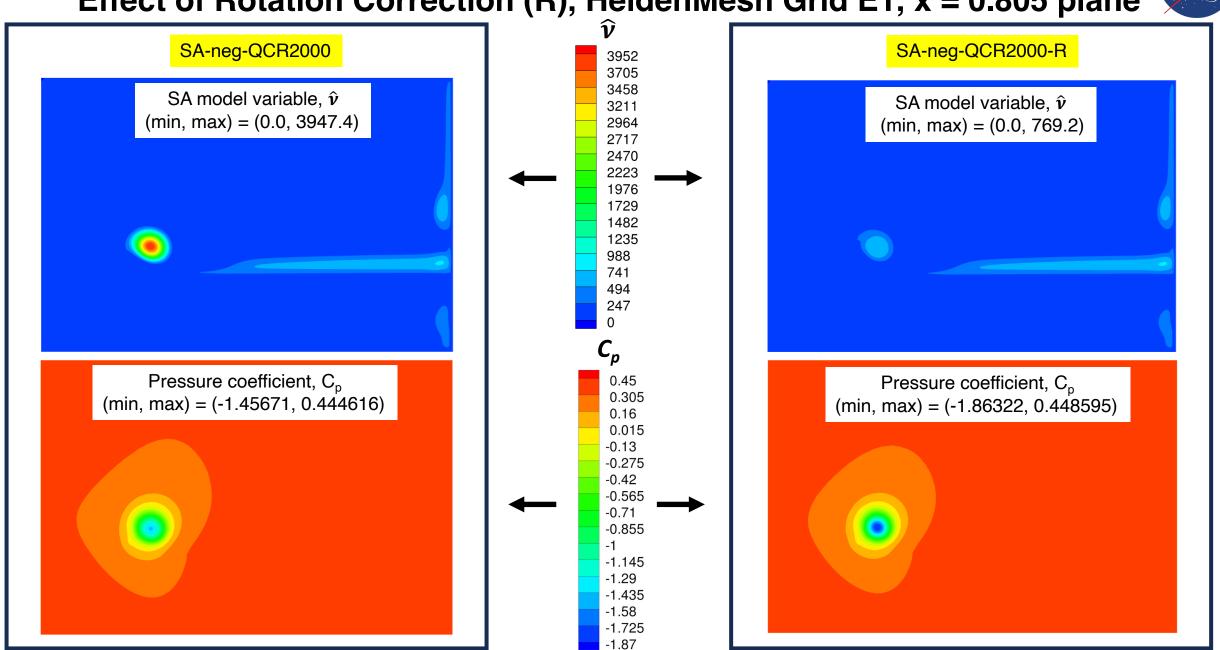


- Residual and Cp plots for HeldenMesh grid family
- Meanflow and SA model residuals are combined
- First-order iterations are not shown in the plots

NACA 0012 Wing in Tunnel

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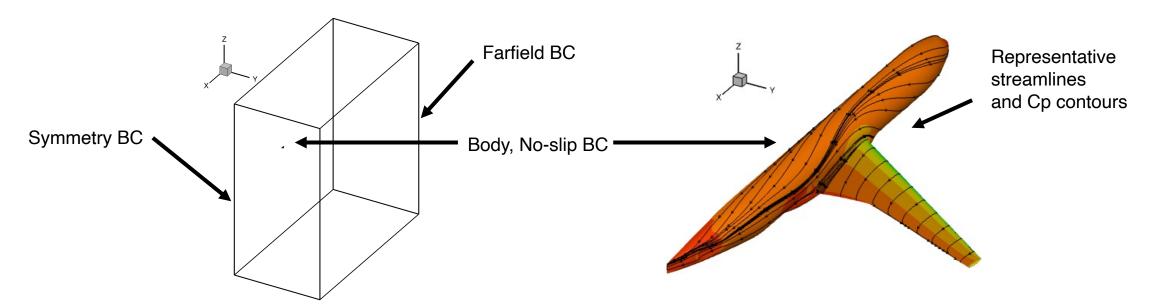
Effect of Rotation Correction (R), HeldenMesh Grid E1, x = 0.805 plane



CRM High-Lift Wing-Body Configuration



 $M_{\infty} = 0.2$, $\alpha = 11^{\circ}$, $Re_{c} = 5.6 \times 10^{6}$



HeldenMesh R.05 Family

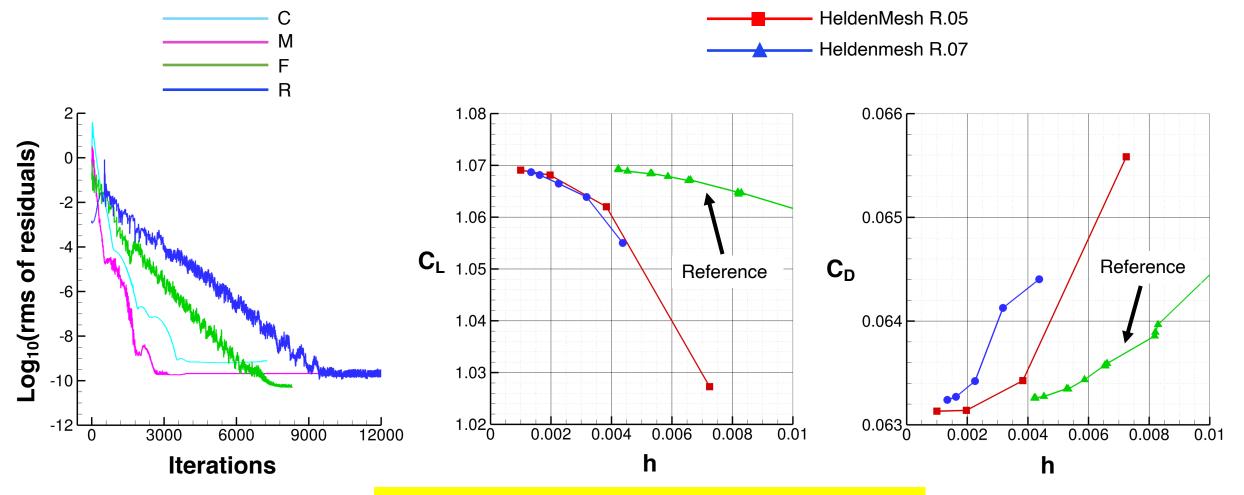
| Grid Identifier | Nodes | Cells |
|--------------------|--------|--------|
| С | 864.0K | 2.6M |
| M | 5.8M | 17.8M |
| F | 42.9M | 131.0M |
| R | 331.2M | 1.01B |

HeldenMesh R.07 Family

| Grid Identifier | Nodes | Cells |
|--------------------|--------|--------|
| Coarse | 5.0M | 12.0M |
| Medium | 13.4M | 31.2M |
| Fine | 38.9M | 87.1M |
| XFine | 105.6M | 232.4M |
| UFine | 191.0M | 415.1M |

CRM High-Lift Wing-Body Configuration Iterative and Grid Convergence





- Residual plot for HeldenMesh R.05 grid family
- Meanflow and SA model residuals are combined
- First-order iterations are not shown in the plots
- Reference is Boeing FEM solution on adaptive grids

Summary



- USM3D-ME solutions computed using SA-neg-QCR2000-R (C_{rot} = 1) turbulence model
 - Joukowski airfoil
 - NACA 0012 wing in tunnel
 - CRM High-Lift Wing-Body Configuration
- Solutions on different grid families
 - Structured, unstructured mixed-element, and adaptive tetrahedral grids
- Machine-zero residuals achieved on all cases and grids
- Satisfactory grid convergence observed for all cases
- Joukowski airfoil
 - Difference in C_D on two finest grids is 0.12 count
- NACA 0012 wing in tunnel
 - Difference in C_D between finest grids within two families is 2.57 count
 - Effect of rotation correction (R) illustrated
- CRM High-Lift Wing-Body Configuration
 - Difference in C_D between finest grids within two families is 1.09 count
 - Difference in C_L between finest grids within two families is 0.04%

Acknowledgments



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