

# NASA LANGLEY RESEARCH FACILITY LANDING AND IMPACT RESEARCH FACILITY



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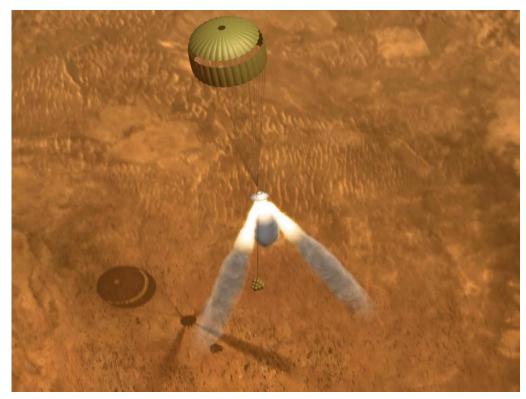
https://newatlas.com/nasa-tests-helicopter-airbag/13571/



https://www.nasa.gov/centers-and-facilities/langley/nasa-crash-tests-evtol-concept/

#### **BACKGROUND**

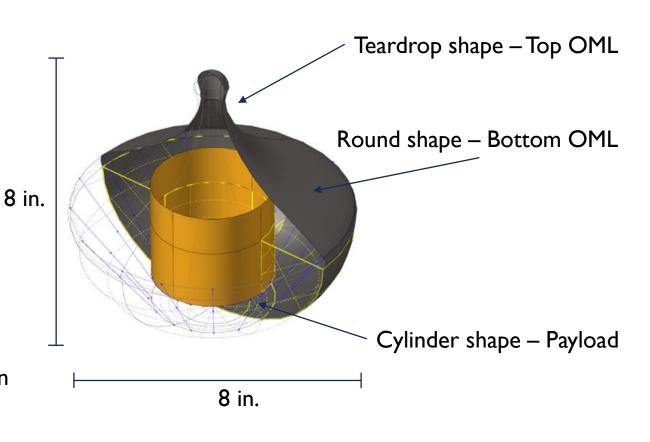
- Delivery of equipment and payload requires a transportation mechanism that can ensure safe arrival of these items to the planetary surface.
- Landing system designs must consider the variability in payload size and landing conditions.
- Many designs consider the use of active energy attenuation system such as retrorockets and deployable parachutes, but these systems are prone to failure.
- A different design approach was considered using passive energy attenuation mechanisms. Energy absorption materials were identified and designed to withstand acceleration at various landing conditions.
- This approach has also been used by various NASA projects as alternative means of designing landing system.



https://en.wikipedia.org/wiki/Retrorocket#/media/File:Rocket\_assisted\_descent.jpg

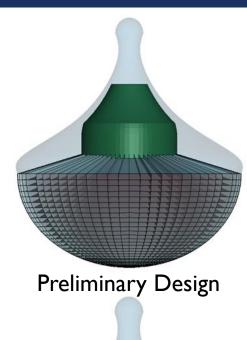
# OBJECTIVE

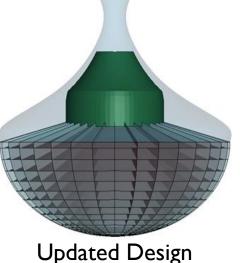
- The goal is to design a payload delivery system using passive energy attenuation mechanisms i.e., energy absorption materials previously studied at NASA.
- The design of the outer mold line (OML) of the capsule needs to contain the payload as well as provide passive up-righting capability.
- Design needs to be robust enough to ensure the internal payload doesn't exceed the specified acceleration limits.
- Honeycomb design was used as energy absorption material inside the payload capsule.
- Different density of honeycomb structure was modeled to observe the changes in the peak loads in the capsule during impact.

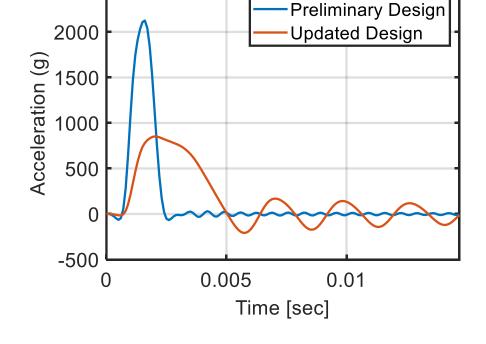


#### HONEYCOMB CELL SIZING

- Model for the honeycomb lander was accomplished in LS-DYNA.
- Quadrilateral shell elements of approximately 0.2 in was used for outer capsule, payload shell, and honeycomb structure.
- Previously modeled concrete was used as landing surface. Simulation was vertical drop at 50 ft/s.
- Two honeycomb designs are presented here.
  - Preliminary design: 0.2 in x 0.4 in.
  - Updated design: 0.4 in x 0.8 in.
- 62% reduction in peak acceleration with updated design.



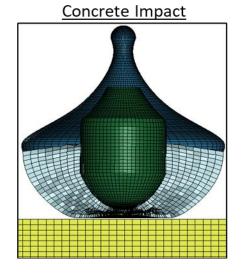


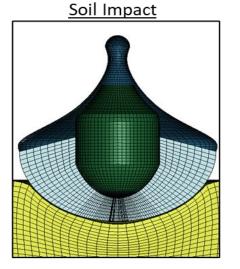


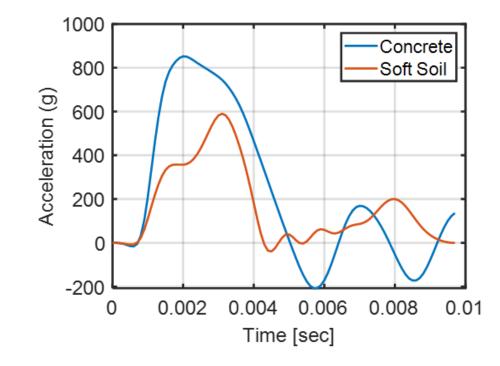
2500

#### **IMPACT SURFACES**

- Honeycomb design impact on two different representative surfaces was studied. Concrete surface and soil impact surface were explored.
- Representative soil model obtained from previous testing conducted at NASA.
- 50 ft/s vertical drop simulation compared for concrete vs soil surface.
- Soil impact surface acts as energy absorption rather than the honeycomb in this case.
- Design needs to consider how to optimize effectiveness in both landing surfaces.

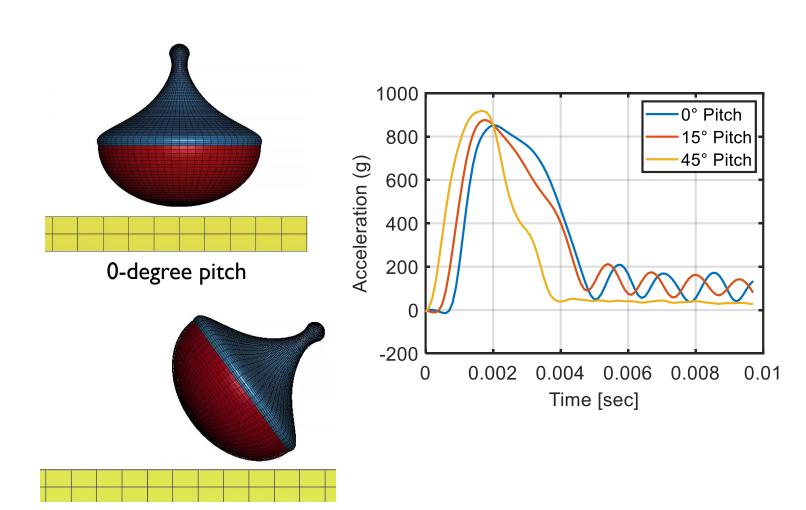






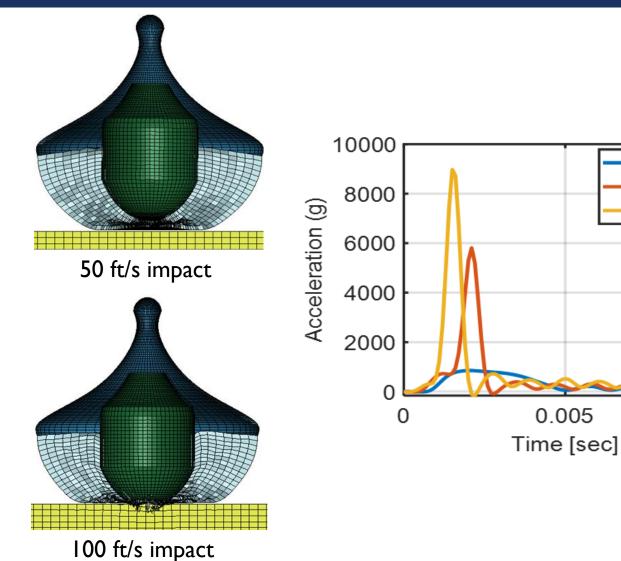
#### LANDER ORIENTATION

- Impact of pitch angle on the landing system was studied. Pitch angle was the orientation of the landing system velocity in relation to the surface. 0 degree is vertical drop of the lander.
- Z-direction acceleration measured along local coordinate system of the landing system.
- Pitch angle of 0, 15 and 45 degrees were studied using concrete landing surface to observe honeycomb structural response.
- Increased pitch angle caused slight increase in acceleration response of the lander indicating larger lateral stiffness in the design.



#### **IMPACT SPEED: CONCRETE**

- The speed at which the lander impacts the surface was explored for the concrete surfaces.
- 50 ft/s, 75 ft/s and 100 ft/s vertical drop simulation (0° pitch angle) were conducted.
- Increasing the impact speed above 50 ft/s caused the honeycomb structure to bottom out and allow the payload to impact the concrete surface leading to a spike in acceleration.



50 ft/s

75 ft/s

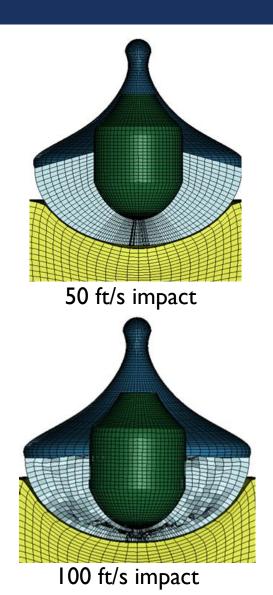
0.005

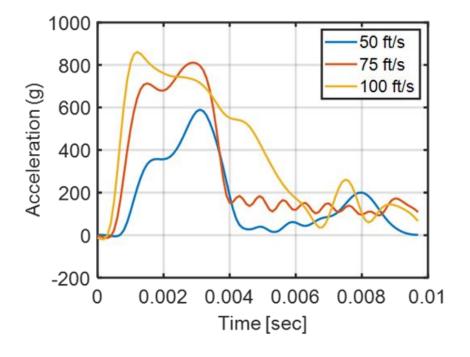
100 ft/s

0.01

#### **IMPACT SPEED: SOIL**

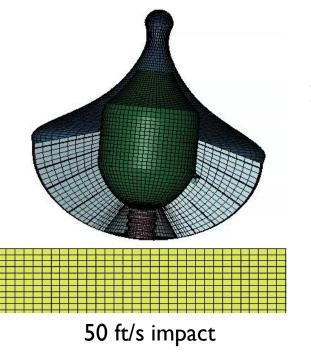
- 50 ft/s, 75 ft/s and 100 ft/s vertical drop simulation (0° pitch angle) were conducted on the soil landing surface.
- For the soil surface, impact speeds above 50 ft/s initiated crushing in the honeycomb structure maintaining acceleration levels of 800 g.
- Factors such as impact speed, landing condition, impact pitch angle must be explored simultaneously to design a lander suitable for all conditions.

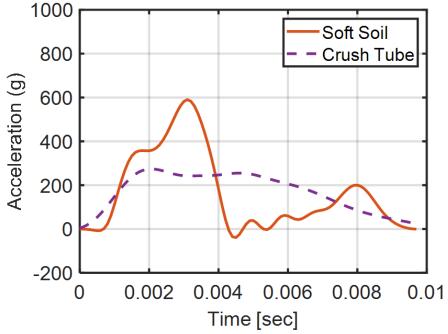




#### COMPOSITE CRUSH TUBE: SOIL

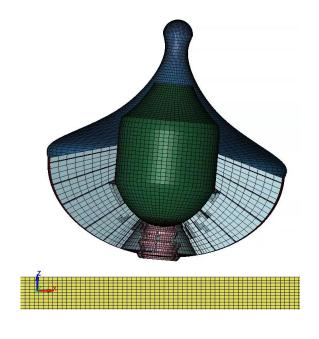
- In addition to honeycomb material, composite crush tube with corrugated sides used in energy absorption for seat designs was explored.
- Honeycomb and composite crush tube can be combined to optimize the design to limit accelerations in various conditions.
- Honeycomb cell size and composite crush tube size was adjusted to reduce previous acceleration peaks of 800 g.



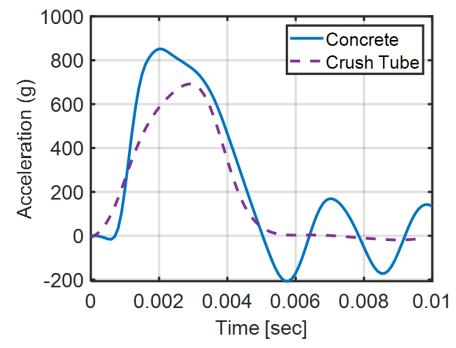


### COMPOSITE CRUSH TUBE: CONCRETE

- Composite crush tube design was also evaluated with the concrete landing surface.
- Initial design of composite tube bottoms out and impact concrete surface for impact speed of 50 ft/s.
- The diameter and thickness of the composite tube was adjusted to provide additional stiffness.

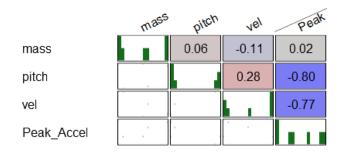


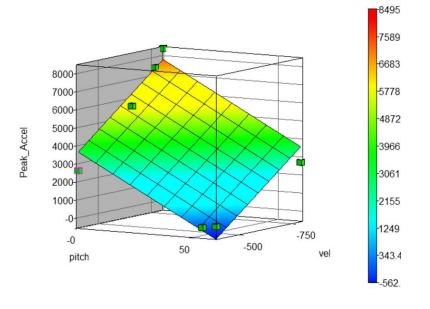
50 ft/s impact



#### PARAMETRIC STUDY

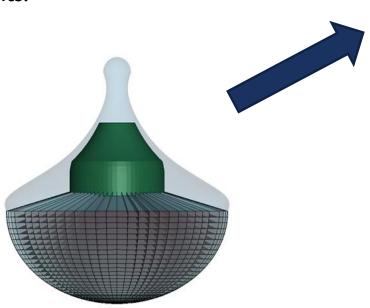
- Parametric study on the impact of speed, pitch angle and payload mass was studied using LS-OPT.
  - Multiple speeds (33.3 ft/s-66.7 ft/s)
  - Multiple pitch angle (0°-60°)
  - Multiple masses (15 23 lbs.)
- Seven points were selected to conduct the simulation. Linear response surface derived from the simulations.
- Peak acceleration in the concrete surface was mainly dependent on pitch angle and impact speed rather than mass.

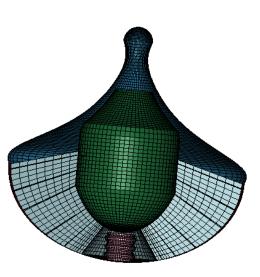




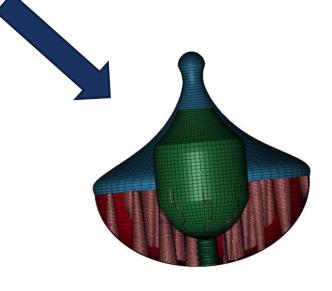
## **CONCLUSION**

- Passive energy attenuation is a viable means of design vehicle used for payload delivery.
- Several factors must be considered to optimize the design to ensure payload stays within acceptable limits.





Future designs can optimize the shape and size of the internal material through design iterations based on the known constraints such as landing location and impact speeds.





# **THANK YOU**

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