

# Amplifier Output Power, Gain, Efficiency, and Bandwidth: A Comparative Study of GaN HEMT MMIC Multi-Stage Power Amplifiers versus Distributed Power Amplifiers

Rainee.N. Simons, Ph.D., *Life Fellow, IEEE*  
Marie T. Piasecki, Joseph A. Downey and Bryan L. Schoenholz

NASA Glenn Research Center, MS 54-1  
21000 Brookpark Road, Cleveland, OH 44135  
*e-mail: [Rainee.N.Simons@nasa.gov](mailto:Rainee.N.Simons@nasa.gov)*

2024 IEEE International Symposium on Antennas & Propagation and ITNC-  
USNC-URSI Radio Science Meeting

Florence, Italy, July 14-19, 2024

Session MO-UB.1A: Devices, Systems, Applications: Part I, Mon, July 15, 2024,

Paper # MO-UB.1A.1, presentation at 8:40-9:00 am



# Abstract

- In this paper we present first, the results of a study conducted to investigate the microwave performance of a wideband (25-31 GHz) GaN MMIC distributed high power amplifier (HPA)
- Second, we compare and contrast the above performance with that of an alternate architecture that relies on two HPAs to provide contiguous 25-31 GHz coverage. The two HPAs operate across 25-28 GHz and 27-31 GHz, respectively, and can be switched in and out depending on the need at any given time
- The parameters investigated includes the output power, gain, power added efficiency, bandwidth, RMS error vector magnitude for offset-QPSK, 8PSK, 16APSK, and 32 APSK waveforms, 3rd-order intermodulation distortion products, noise figure, and single sideband phase noise



# Outline

- Introduction & Benefits of GaN MMIC Technology for HPAs
- Design Approaches for Wideband HPA & Brief Set of Specifications
  - Wideband (25-31 GHz) Distributed HPA
  - Switched HPAs for two contiguous frequency bands (25-28 & 27-31 GHz)
- Wideband Distributed HPA Characterization
  - Output Power & Power Added Efficiency (PAE) vs. Input Drive Power
  - Error Vector Magnitude (EVM) for OQPSK, 8PSK, 16APSK, & 32APSK Waveforms
  - Output Spectrum & Spectral Regrowth
  - Third-Order Intermodulation Distortion (IMD) Products
  - Noise Figure
  - SSB Phase Noise
- Performance Comparison of the above two approaches
- Conclusions & Discussions



# Introduction

- NASA plans to transition the space relay communication services provided by TDRSS in a phased manner to U.S. commercial service provider networks
- This requires developing user spacecraft terminals capable of roaming and having performance flexibility to interoperate between multiple U.S. commercial service provider networks and space networks owned by U.S. government agencies
- However, legacy systems operate over different frequency bands within the Ka-band spectrum
- Hence, there is a need to develop wideband microwave components and HPAs



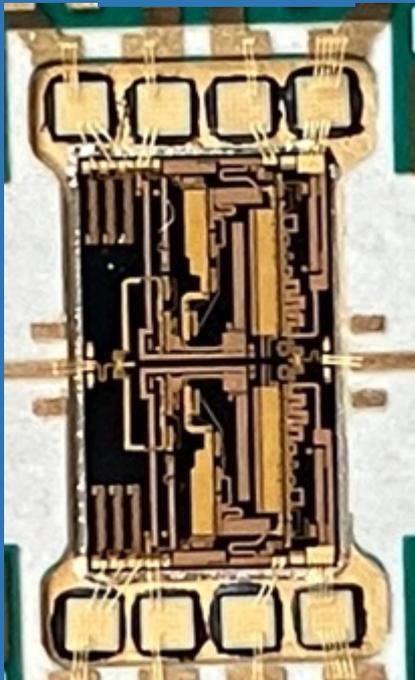
# Benefits of GaN Technology for Microwave High Power Amplifiers



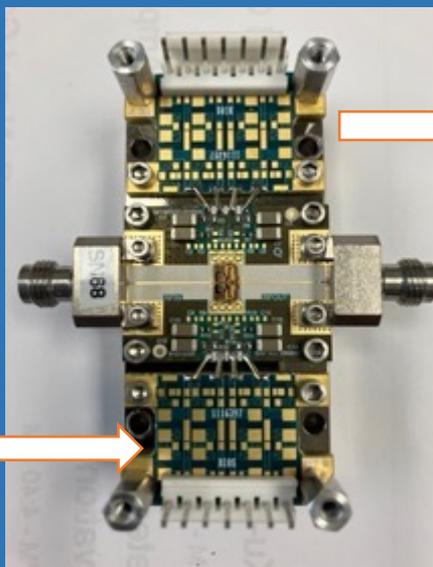
- Gallium nitride (GaN) has large bandgap, high electron saturation velocity, excellent thermal properties, & good chemical stability
- Consequently, high electron mobility transistors (HEMTs) fabricated on epitaxially grown GaN-on-SiC wafers can
  - Operate at high frequencies
  - Deliver high RF output power hence fewer devices for a target output power – smaller size, lower mass
  - Offer good linearity
  - Provide high power added efficiency
  - Perform at elevated temperatures
  - Operate in high radiation environment

# 1<sup>st</sup> Design Approach — GaN Wideband Distributed HPA Proof-of-Concept Demonstration Model

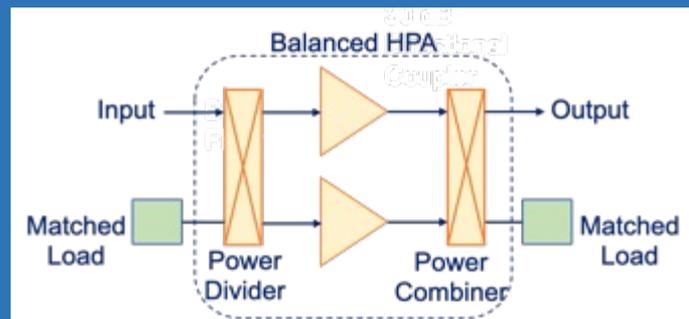
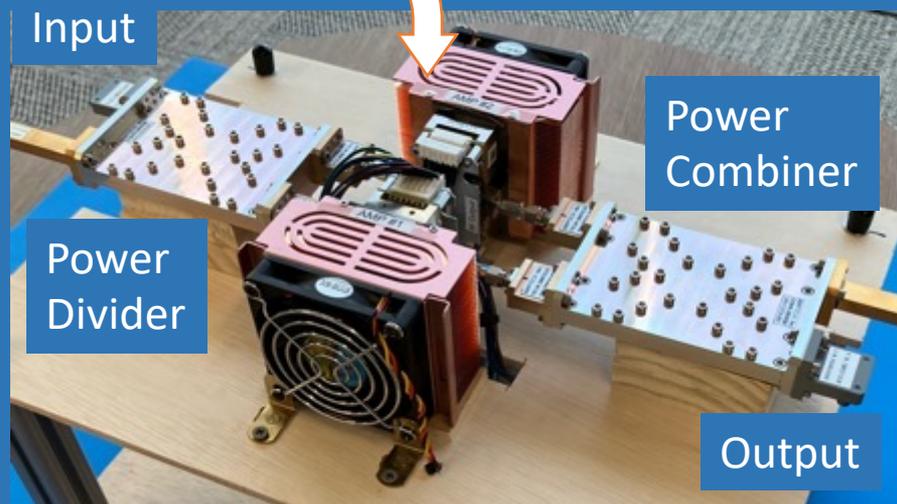
GaN MMIC



GaN MMIC In Test Fixture

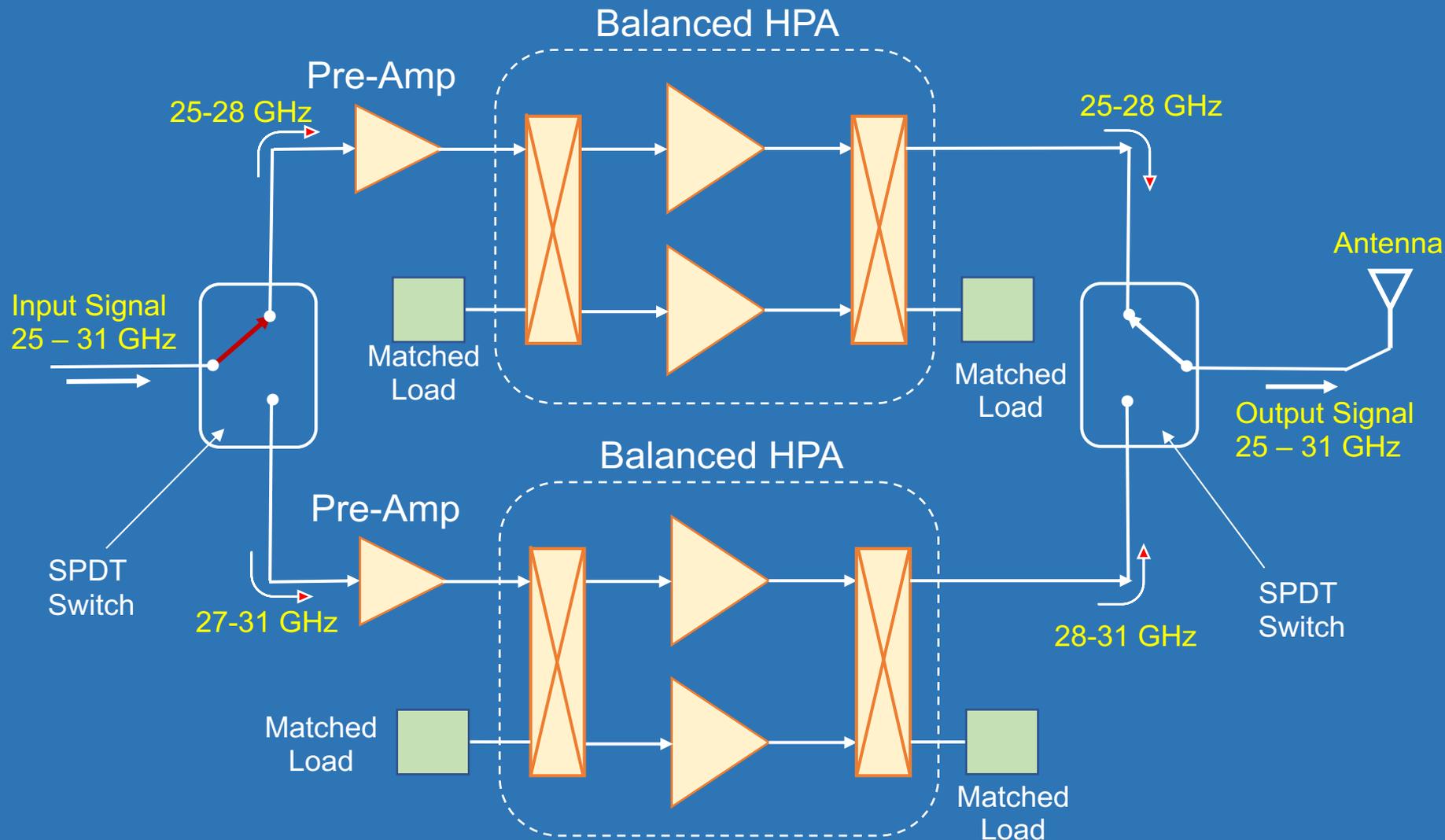


Test Fixture attached to a Heat Sink with Fan





# 2<sup>nd</sup> Design Approach — GaN Switched HPAs for Two Contiguous Frequency Bands (25-28 GHz & 27-31 GHz)





# Brief Set of Specifications for GaN Wideband Distributed & Switched HPAs



- Saturated output power ( $P_{\text{sat}}$ ) (Single Amp): 8 to 10 W (CW)
  - ~3dB higher for Balanced Amplifier
- Bandwidth: 25 to 31 GHz
- PAE: 15 to 20 percent
- Small signal gain: 15 to 20 dB
- Input/output return loss:  $< -10.0$  dB
- Gain flatness over full bandwidth:  $\pm 1$  dB

# Test Setup for GaN Wideband Distributed HPA Characterization

R&S SMW200A Vector Signal Generator



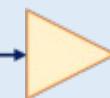
R&S FSW Signal & Spectrum Analyzer



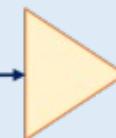
Keysight N6705C DC Power Analyzer for Gate & Drain Voltages/Currents



Pre-Amp



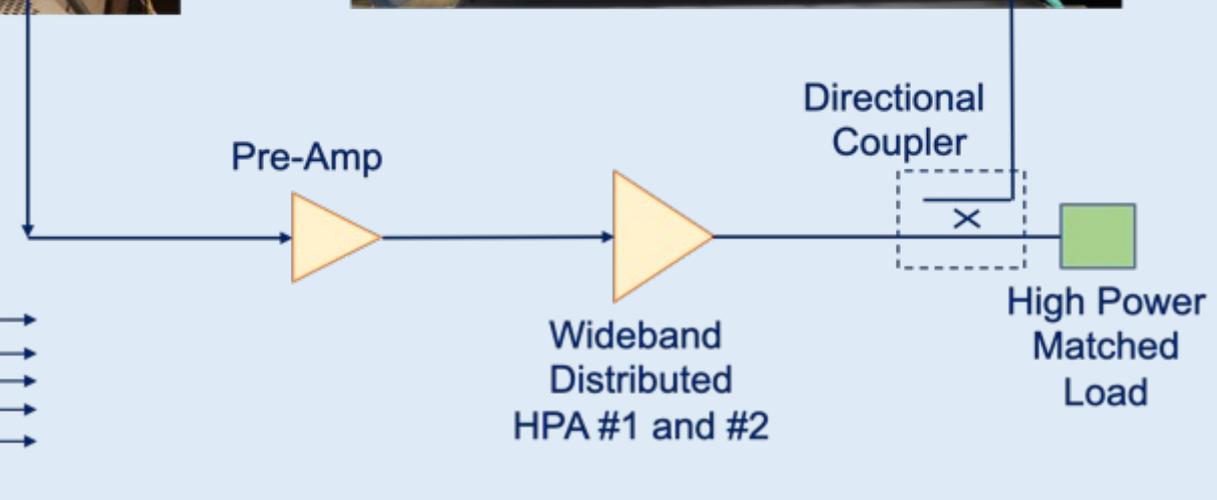
Wideband Distributed HPA #1 and #2



Directional Coupler



High Power Matched Load

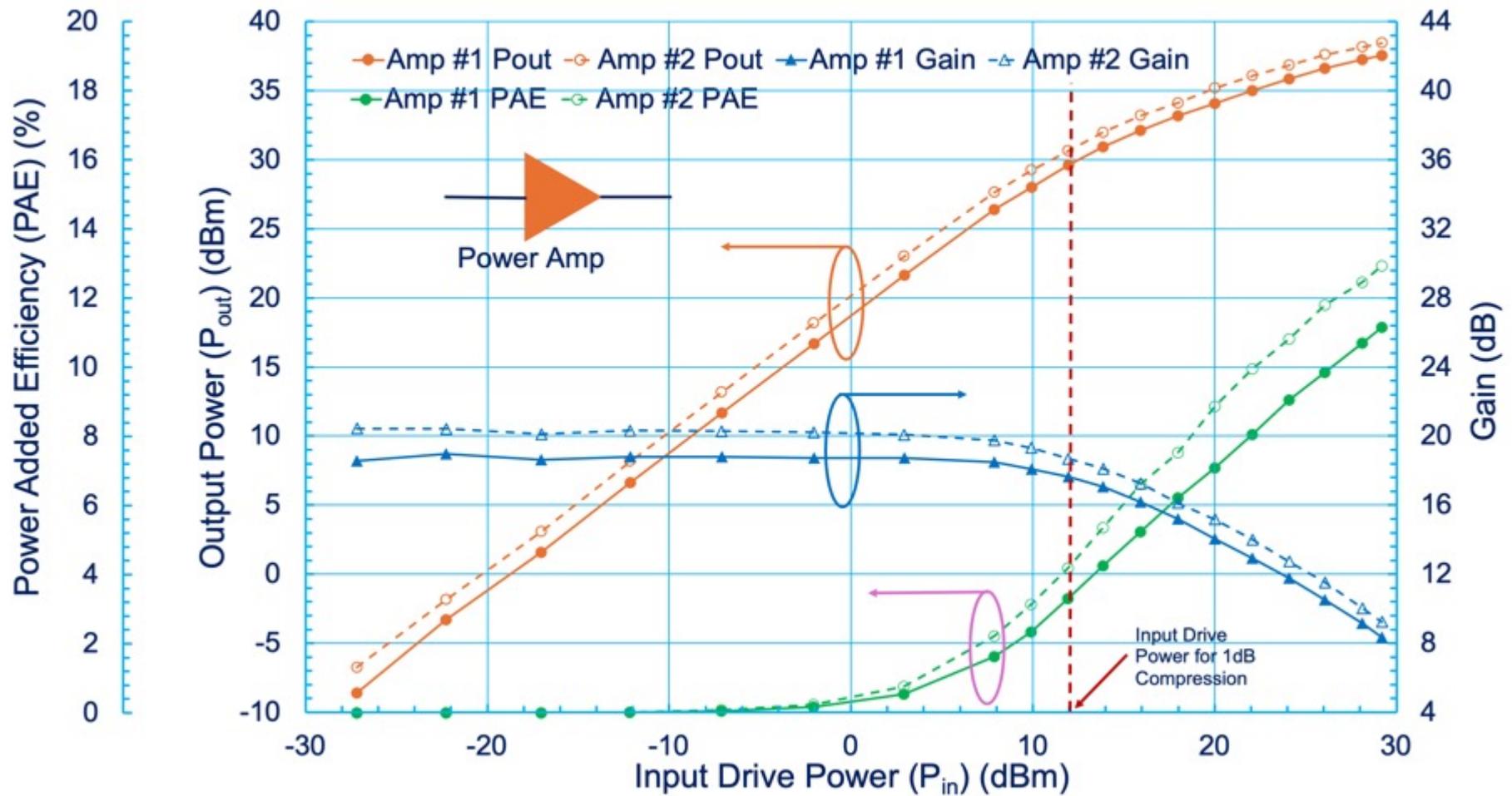




# Measured $P_{out}$ , Gain, & PAE vs. $P_{in}$

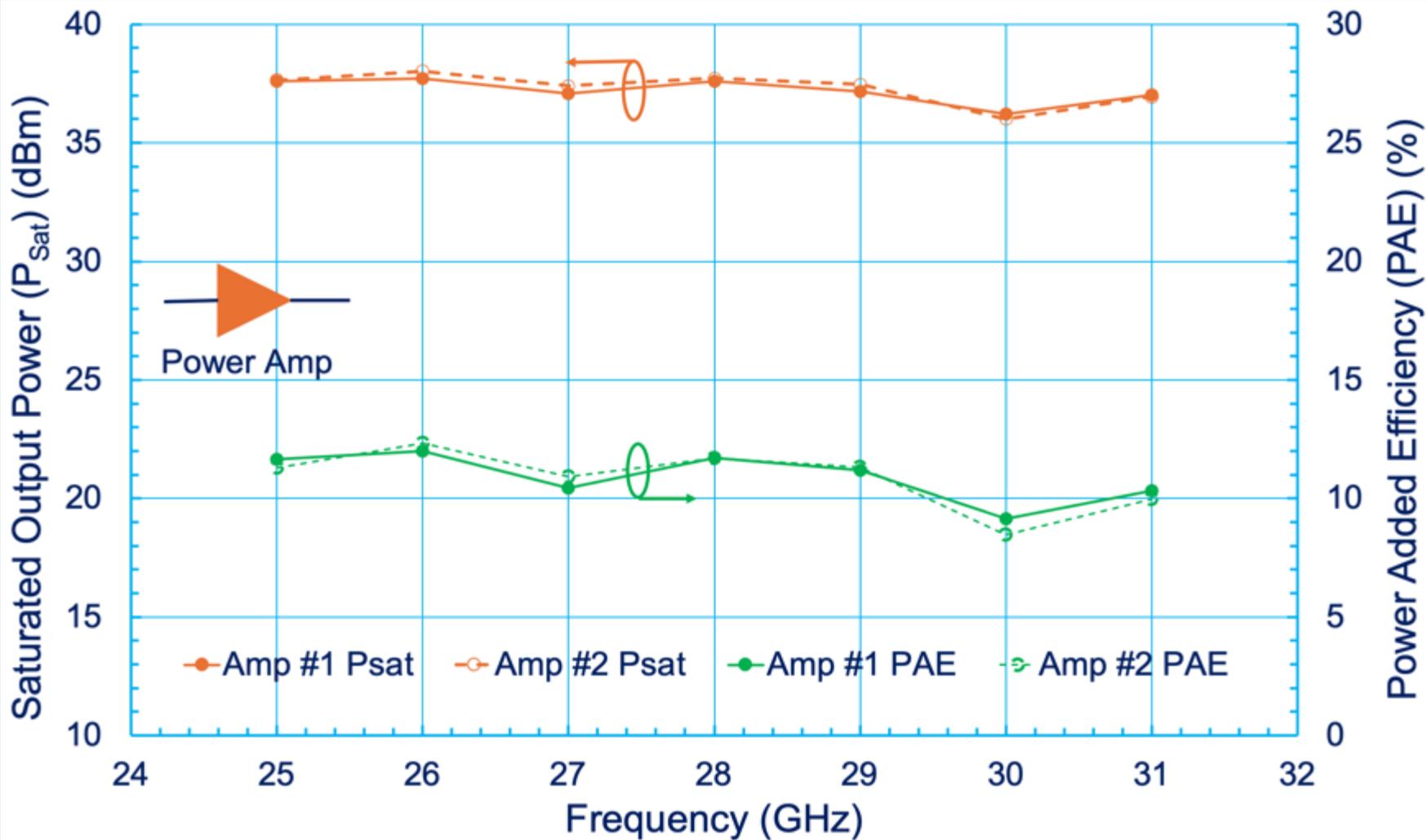


$(f_0 = 28.0 \text{ GHz}, V_{d1} = V_{d2} = 18 \text{ V}, V_{g1} = -2.0 \text{ V}, V_{g2} = -2.04 \text{ V}, T = 25^\circ \text{ C})$



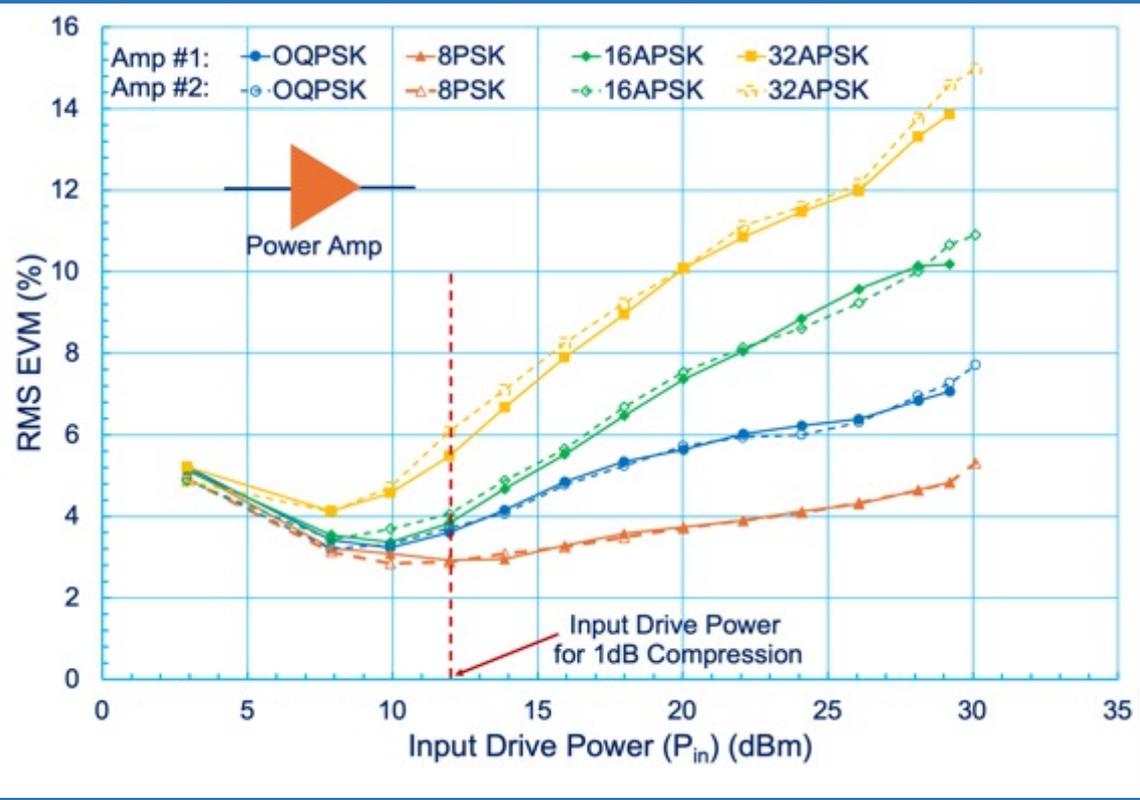
# Measured $P_{\text{sat}}$ & PAE vs. Frequency

( $f_0 = 28.0$  GHz,  $V_{d1} = V_{d2} = 18$  V,  $V_{g1} = -2.0$  V,  
 $V_{g2} = -2.04$  V,  $T = 25^\circ$  C)

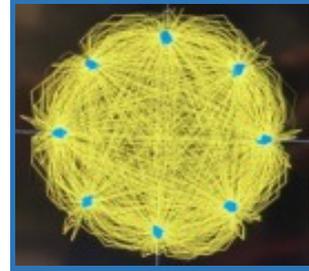


# Measured RMS EVM vs. $P_{in}$

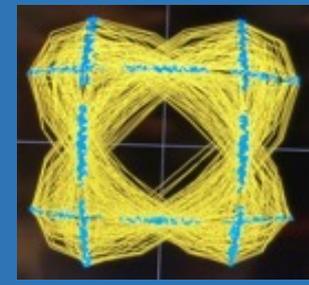
( $F_0 = 28$  GHz, Symbol Rate: 180 Msymbols/second & Square Root Raised Cosine (SRRC) filter set to 0.35)



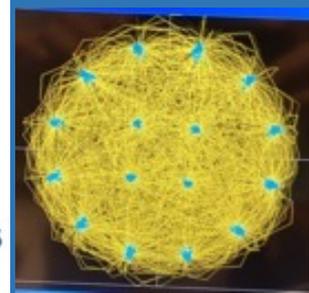
## Waveforms & Constellations



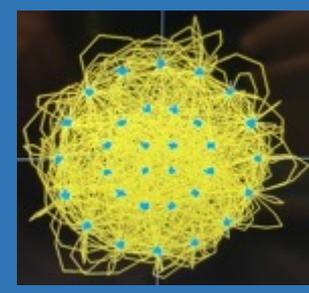
8PSK



Offset-QPSK



16APSK

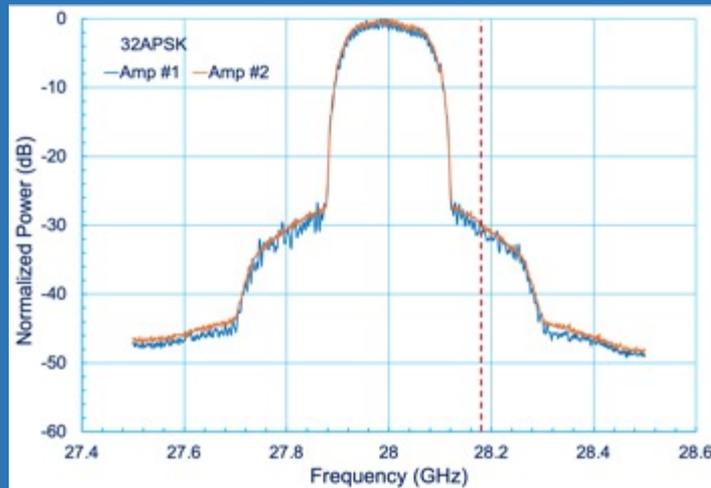
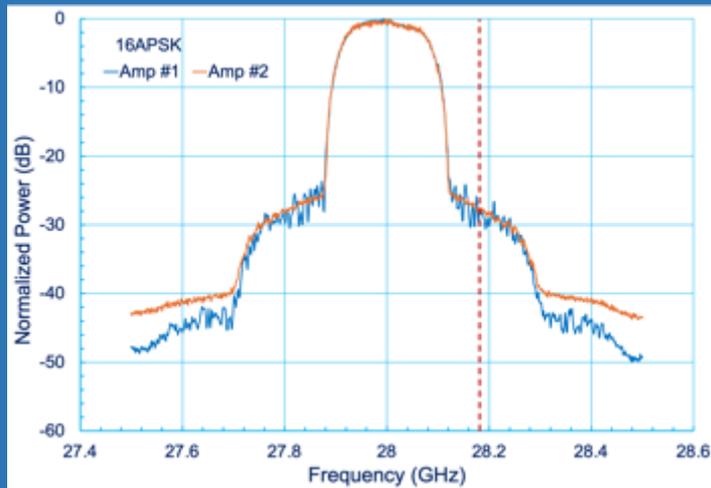
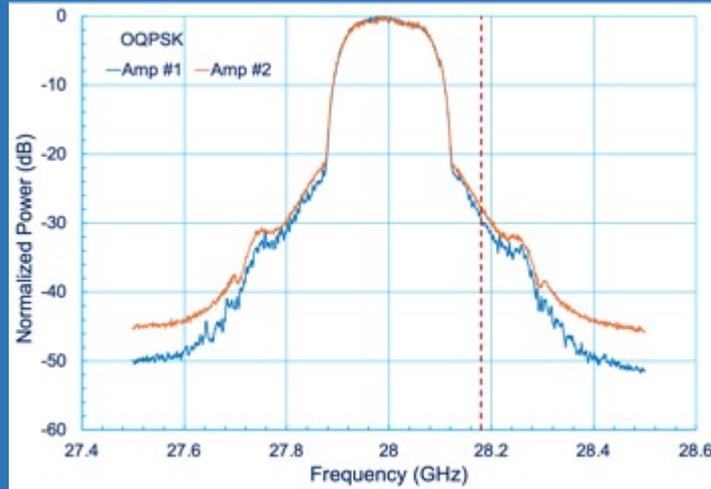
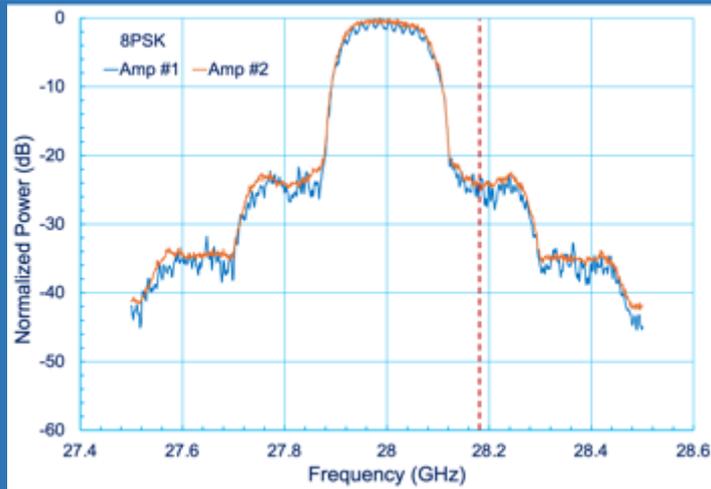


32APSK

✓ Low RMS EVM ( $\leq 6\%$ ) up to the 1-dB compression point demonstrates excellent linearity, which enables amplifying higher-order modulation waveforms, such as 8PSK, 16APSK, & 32APSK. This feature enables the spacecraft radios to support both CCSDS compliant waveforms used by NASA missions, as well as, DVB-S2 waveforms typically used by commercial service providers

# Measured Spectrum @ ~5% EVM

( $F_0 = 28$  GHz, Symbol Rate: 180 Msymbols/second, SRRC filter: 0.35, & Channel Bandwidth: 225 MHz)



- ✓ For a fixed bandwidth the spectral efficiency improves from 2bits/s/Hz (OQPSK) to 5bits/s/Hz (32APSK) & can be exploited by spacecraft radios to enhance throughput



# Measured Out-of-Band Spectral Regrowth



- ✓ The out of band spectral regrowth is measured at 1-symbol rate (180 MHz) away from the center frequency or carrier frequency (28 GHz) for all four waveforms and the results are summarized below

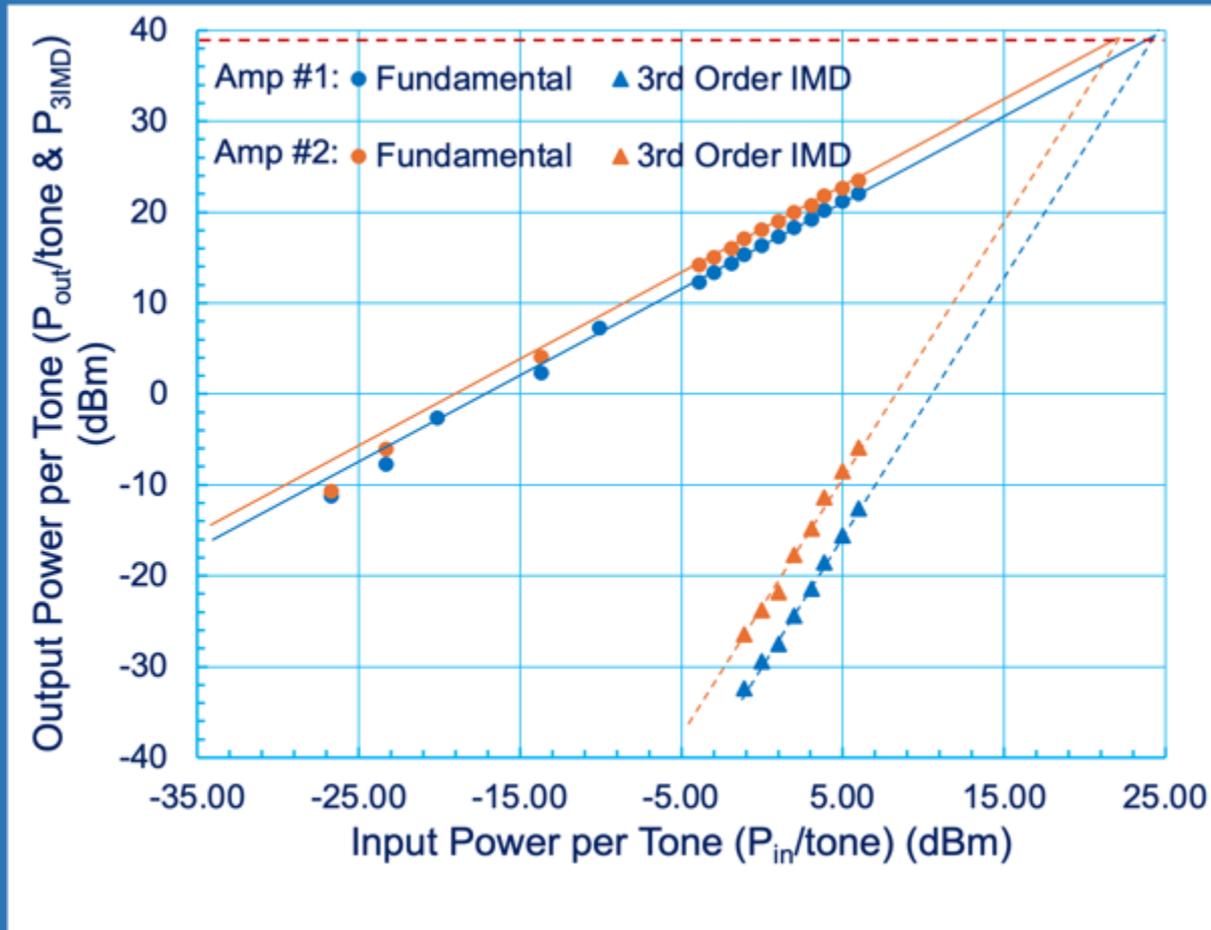
Waveform	Spectral Regrowth (dBc) (@28.18 GHz)	
	Amp #1	Amp #2
8PSK	-26.1	-24.3
OQPSK	-29.6	-27.9
16APSK	-29.5	-27.6
32APSK	-29.4	-30.0

- ✓ The data indicate spectral regrowth  $\leq -20$  dBc, which demonstrates low adjacent channel interference or adjacent channel power ratio (ACPR). A spacecraft radio with this capability enables roaming & interoperability

# Measured 3rd-Order Intermodulation Distortion (IMD) vs. $P_{in}$ per Tone

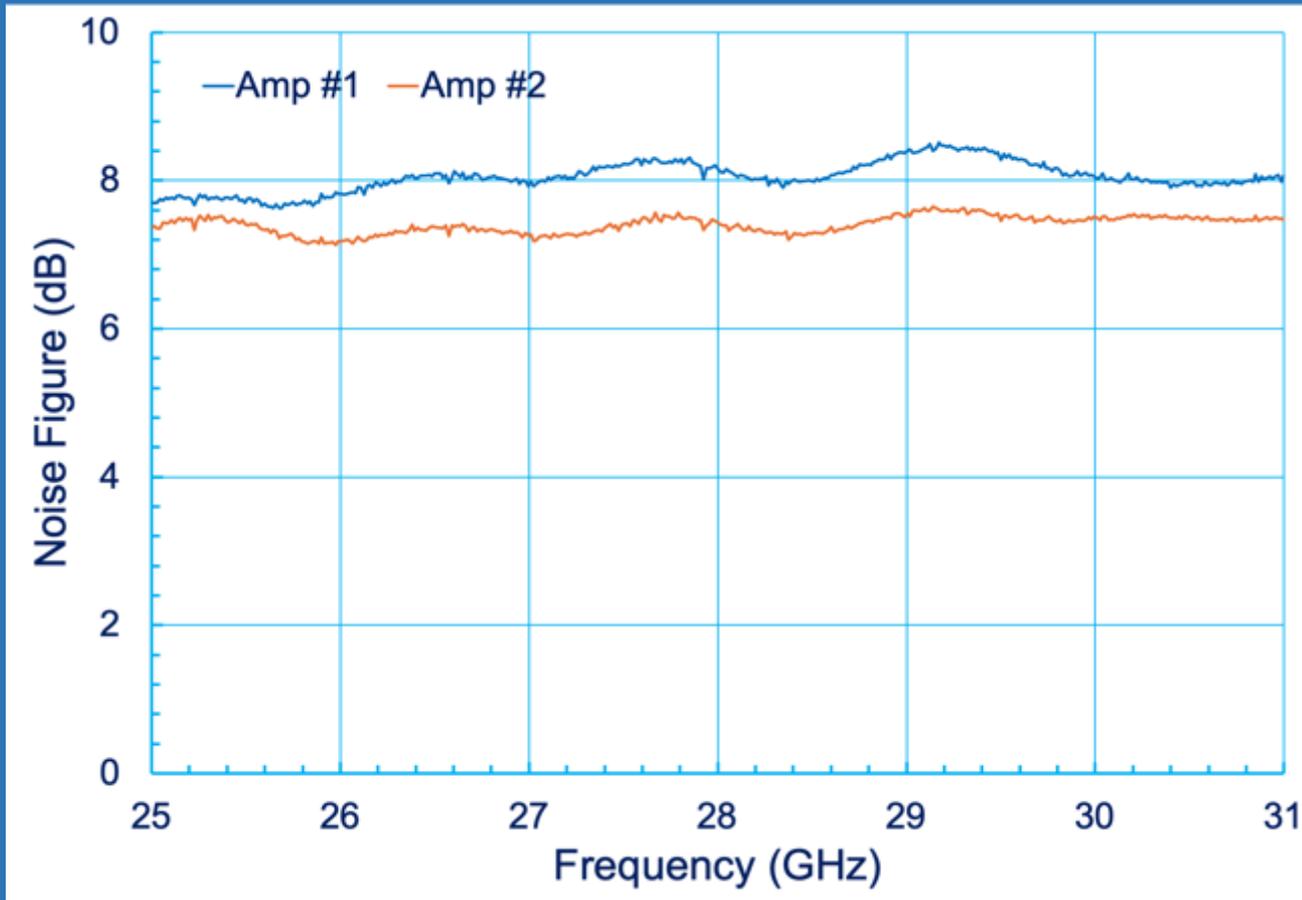


(Tone Frequencies: 28 GHz  $\pm$  2.5 MHz & Tone Spacing: 5 MHz)



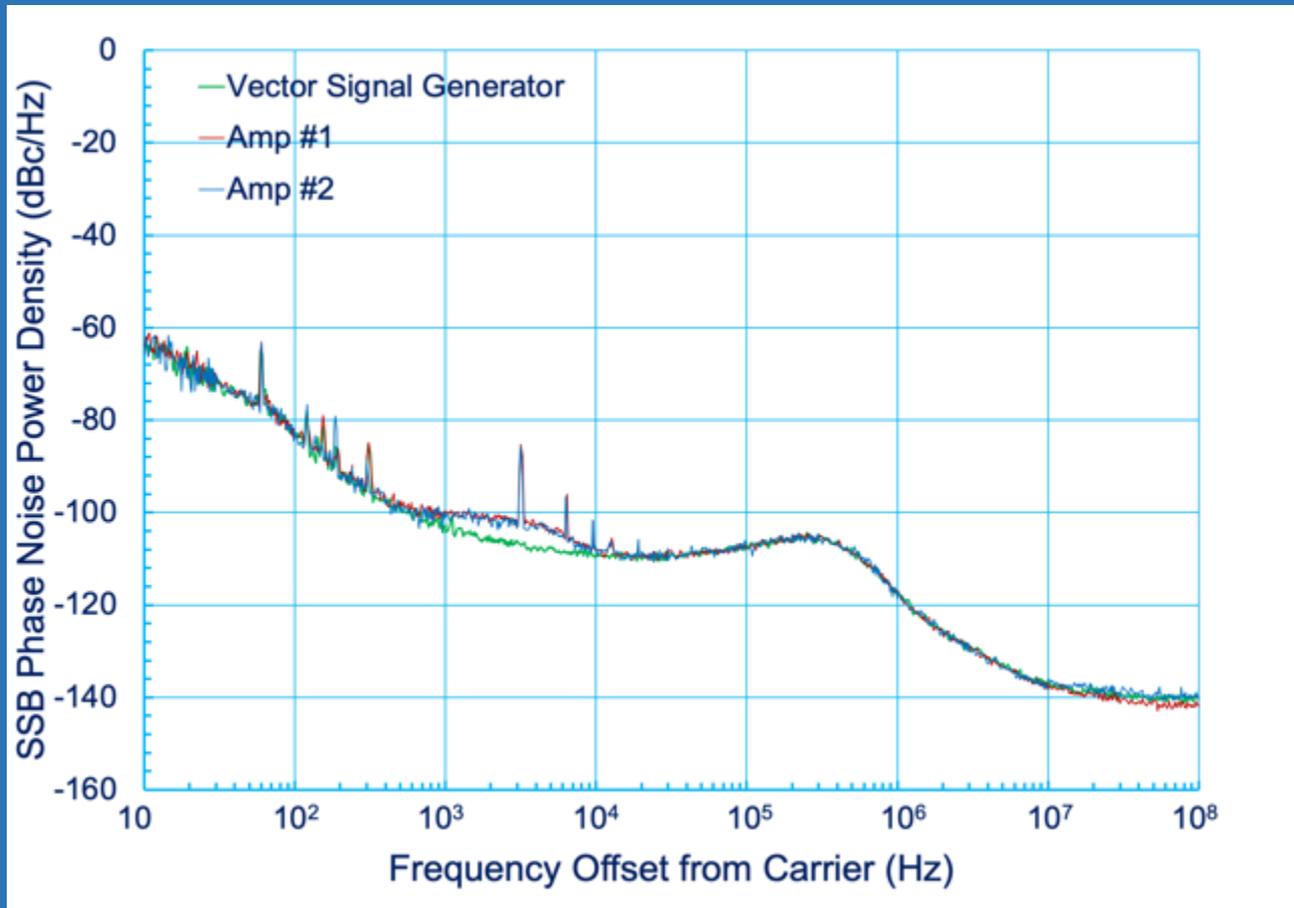
- ✓ The high OIP3 of 39 dBm demonstrated that the 3rd-order IMD products generated is small. Hence, interference signals generated within the spacecraft radio channel bandwidth due to HPA nonlinearity is also small

# Measured Noise Figure vs. Frequency



- ✓ Low noise figure ( $\leq 9.0$  dB), while the spacecraft radio is transmitting, implies less S/N ratio degradation of the adjacent channels

# Measured SSB Phase Noise Spectral Power Density vs. Frequency Offset from $f_0 = 28$ GHz



- ✓ Low HPA phase noise implies less rotation of the waveform constellation points which improves BER performance of the spacecraft radio



# GaN Wideband Distributed HPA Performance Summary



Parameter	Amp #1 Measured Value	Amp #2 Measured Value
Frequency Range (GHz)	$28 \pm 3.0$	$28 \pm 3.0$
Output Power ( $P_{\text{sat}}$ ) (dBm)	$37 \pm 0.75$ ( $5.1 \pm 0.9$ W)	$37 \pm 1$ ( $5.15 \pm 1.15$ W)
Small Signal Gain (dB)	$19.0 \pm 0.4$	$19.4 \pm 0.7$
Peak PAE (%)	$10.5 \pm 1.5$	$10.4 \pm 2$
Gain at peak PAE (dB)	$8.2 \pm 0.2$	$8.6 \pm 0.6$
Return Loss (dB)	$< -10.0$	$< -10.0$
RMS EVM Offset-QPSK, 8PSK, 16APSK, and 32APSK (Drive at 1-dB compression point and carrier frequency of 28 GHz)	$\leq 6\%$	$\leq 6\%$
Out-of-Band Spectral Regrowth (dBc), @ 28.18 GHz	$< -26.0$ dBc	$< -24.0$ dBc
OIP3 (dBm) at carrier frequency of 28 GHz	39	39
Noise Figure (dB) across the above frequency range	$< 8.6$	$< 7.7$



# GaN Switched HPAs Performance Summary

Parameter	Measured Value (25–28 GHz Driver & Power Amp)			Measured Value (28–31 GHz Driver & Power Amp)		
	25.0	26.5	28.0	28.0	29.5	31.0
Frequency ( $f_0$ and $f_0 \pm 1.5$ GHz)	25.0	26.5	28.0	28.0	29.5	31.0
Output Power (dBm) ( $P_{sat}$ )	39.1	37.7	37.9	37.5	38.4	37.0
Small Signal Gain (dB)	30.9	29.6	30.4	30.5	31.4	29.7
PAE (%)	22.8	18.9	19.0	21.5	23.3	20.6
Return Loss (dB)	< -10.0			< -10.0		
RMS EVM (%) (drive at 1- dB compression point) (QPSK, Offset-QPSK, 8PSK, 16APSK, & 16QAM)	5 (All but 16QAM)			5 (QPSK & 8PSK)		
	7 (16QAM)			6 (Offset-QPSK & 16APSK)		
				10 (16QAM)		
Out-of-Band Spectral Regrowth (dBc)	< -30			< -30		
OIP3 (dBm)	48			53		
Noise Figure (dB)	9 (Higher NF due to stabilizing gate resistor)			7		
SSB Phase Noise Power Density (dBc/Hz) (drive at 1-dB compression point)	Compliant with MIL-STD Mask			Compliant with MIL-STD Mask		
	Added Phase Noise is insignificant			Added Phase Noise is insignificant		



# Conclusions & Discussions

- Characterization of the Wideband Distributed HPA and the Switched HPA indicates:
  - Both HPA design approaches are capable of providing wideband performance
  - The linearity, spectrum, spectral regrowth, noise figure and SSB phase noise characteristics are comparable for both approaches
  - The PAE of the wideband distributed HPA is lower than the switched HPAs
- The single wideband distributed HPA approach requires few components — simplifies HPA design, manufacturing, & testing — lower size, mass, & cost