

Acoustic Characterization of the NASA Langley 14- by 22-Foot Subsonic Tunnel Using a Phased Array

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Outline

- Motivation
- Experimental Setup
 - Facility
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 - Static Runs
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- Conclusion



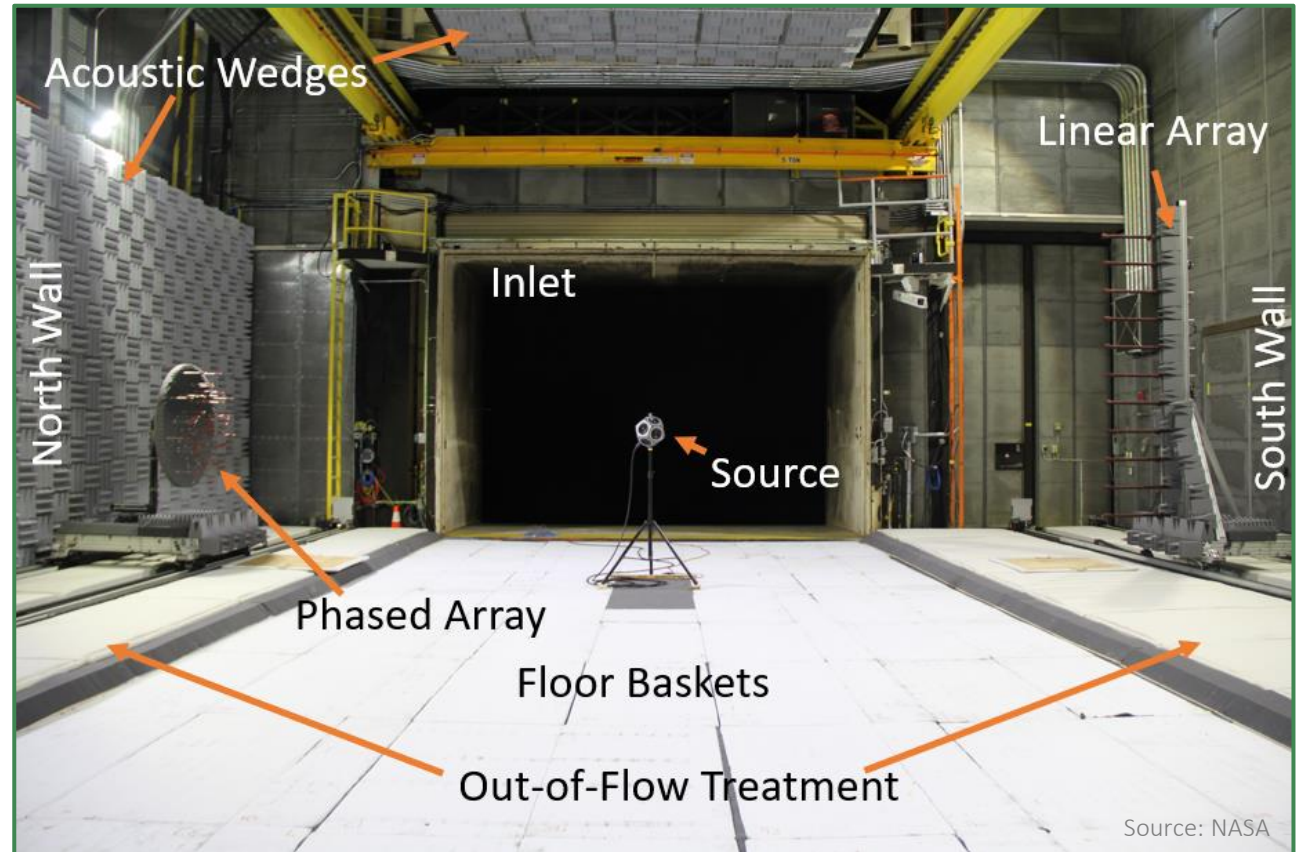
Motivation

- Characterize acoustic treatment of large wind tunnel
- Past acoustic testing
 - High frequency (airframe noise and propulsion-airframe aeroacoustics)
 - Periodic impulsive (large rotor)
- Sound from scale-model UAM/AAM vehicles may blend into tunnel background noise
- Need to capture signal in low signal-to-noise (SNR) environments



Experimental Setup - Facility

- NASA Langley 14- by 22-Foot Subsonic Tunnel (14x22)
 - Closed circuit, atmospheric
 - Up to Mach 0.12 in this analysis
 - Run in open-jet configuration
- Acoustic treatment of tunnel
 - Walls of open-jet have some permanent treatment
 - Acoustic wedges on north wall and ceiling
 - Walls and ceiling out of flow
 - Floor in flow
 - Floor treated with acoustic floor baskets

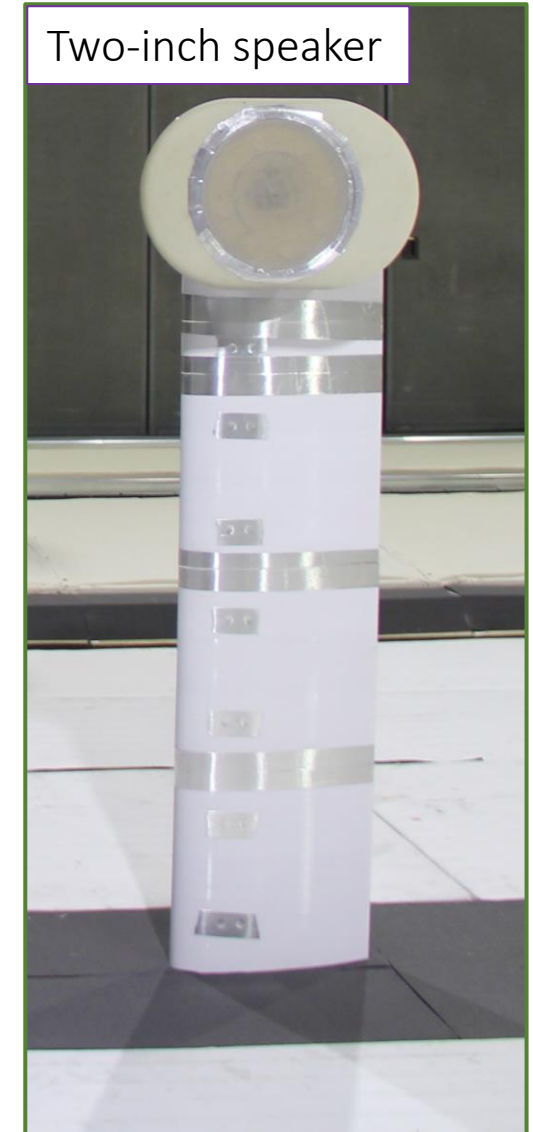


Discussion of linear array results in Stutz et al. 2024

Discussion of floor baskets in Zawodny et al. 2024

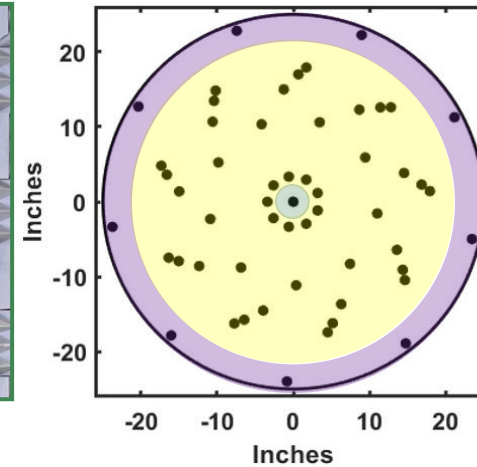
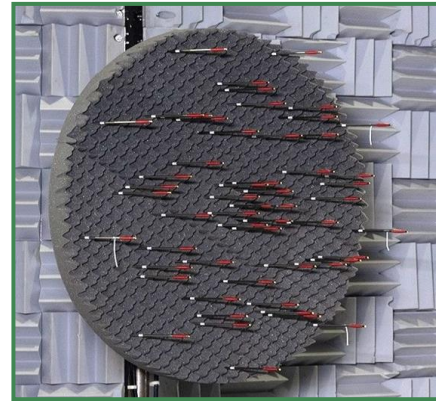
Experimental Setup – Noise Source

- Source located halfway across test section and 60 in above floor, 16 ft downstream from inlet
- Two static (no-flow) noise sources
 - **Cabinet speaker (directional)**
 - Dodecahedron speaker (omnidirectional)
- Two inflow noise sources
 - **Two-inch speaker (directional)**
 - Air source (high frequency stochastic)
 - Both embedded in aerodynamic fairing

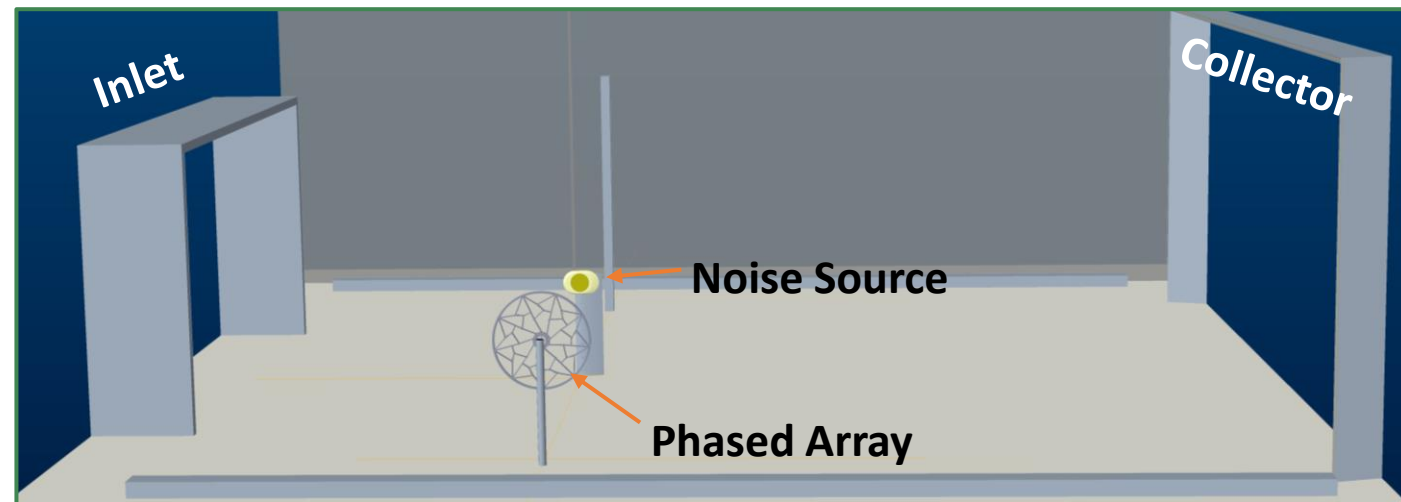


Experimental Setup – Phased Array

- 54 elements
- ¼-in microphones
- Inner array
 - 45 elements in reverse-log distribution
 - 36-in diameter
- Outer ring
 - Nine elements
 - 48-in diameter
 - Improves low frequency resolution
- Single reference microphone
- Microphone diaphragms 187 in away from noise source in lateral direction

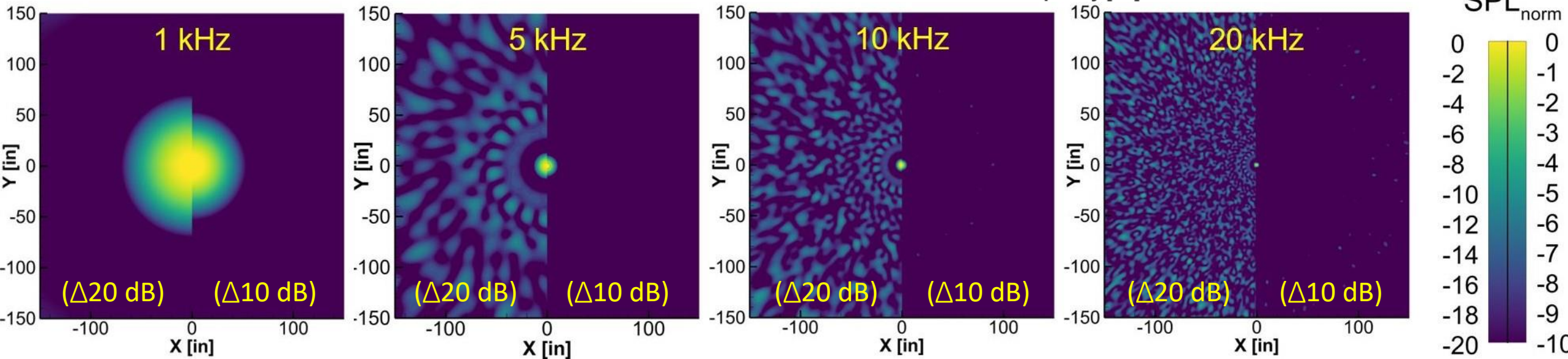
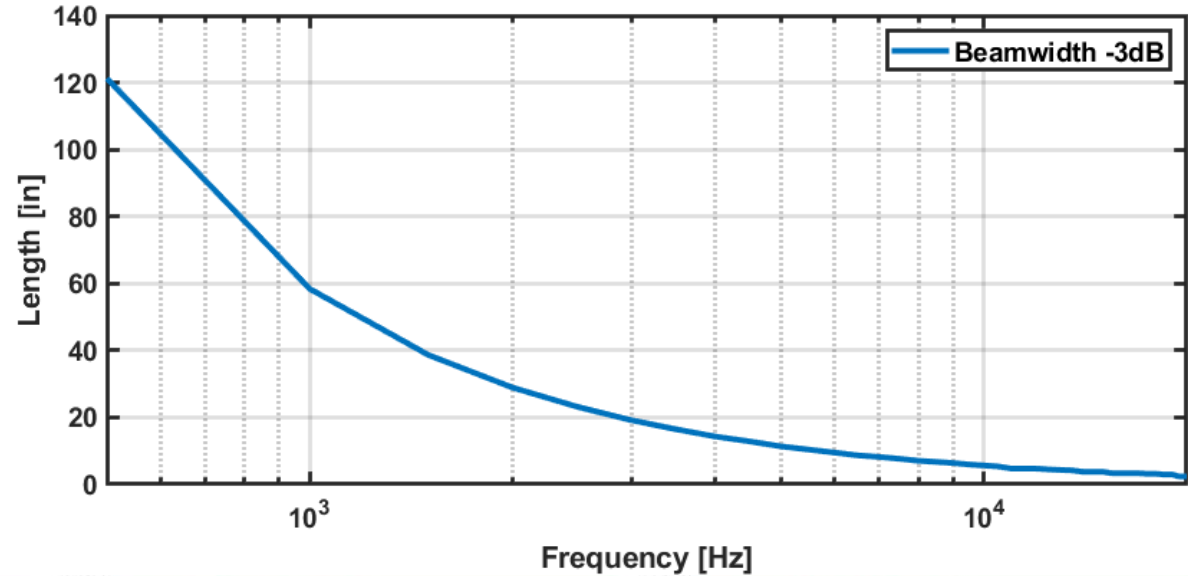


Source: NASA



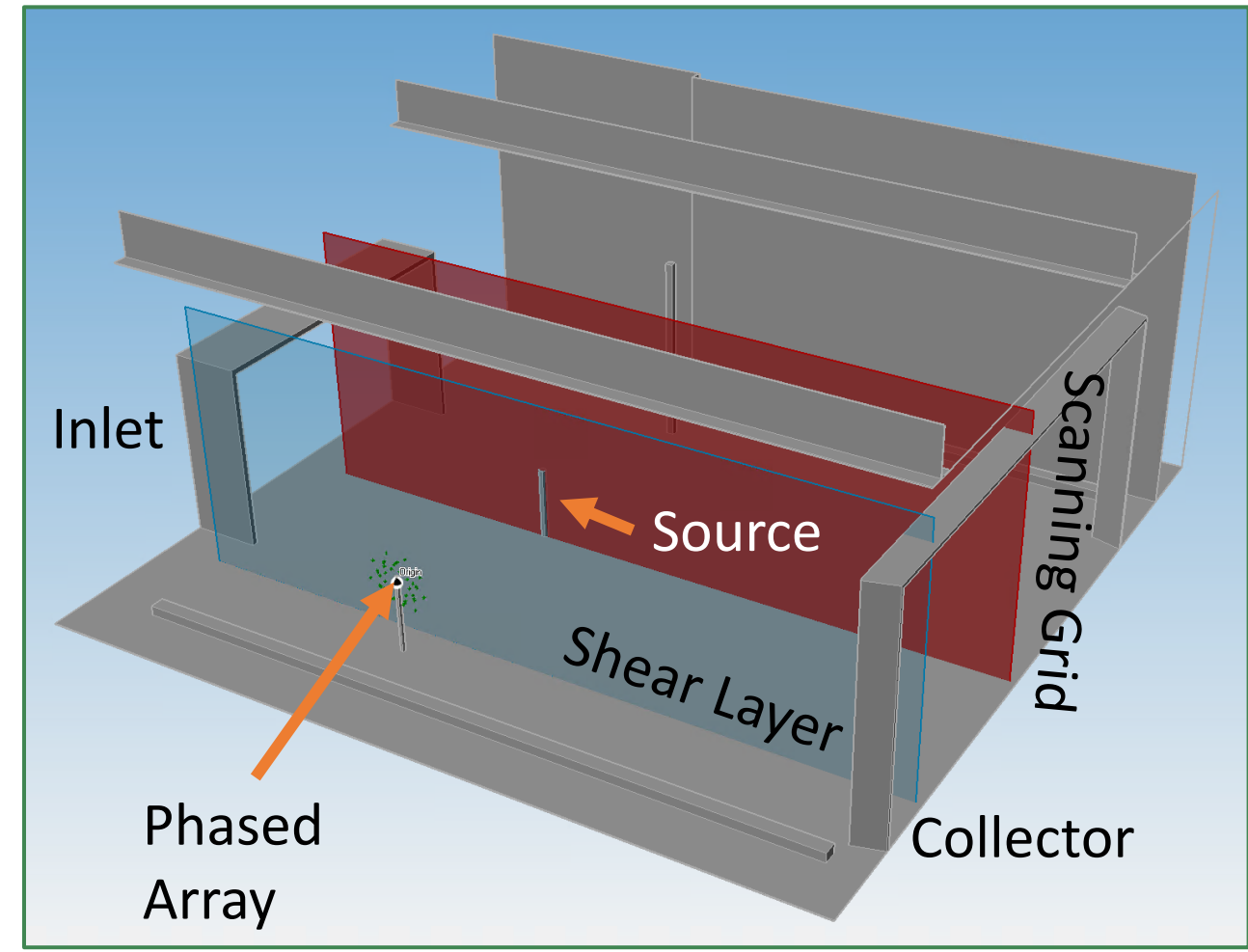
Experimental Setup - Phased Array Response

- Minimizes 3-dB beamwidth
- Sidelobes more than 10 dB below main lobe from 1 to 16 kHz
- Simulated Point Spread Functions (PSF)



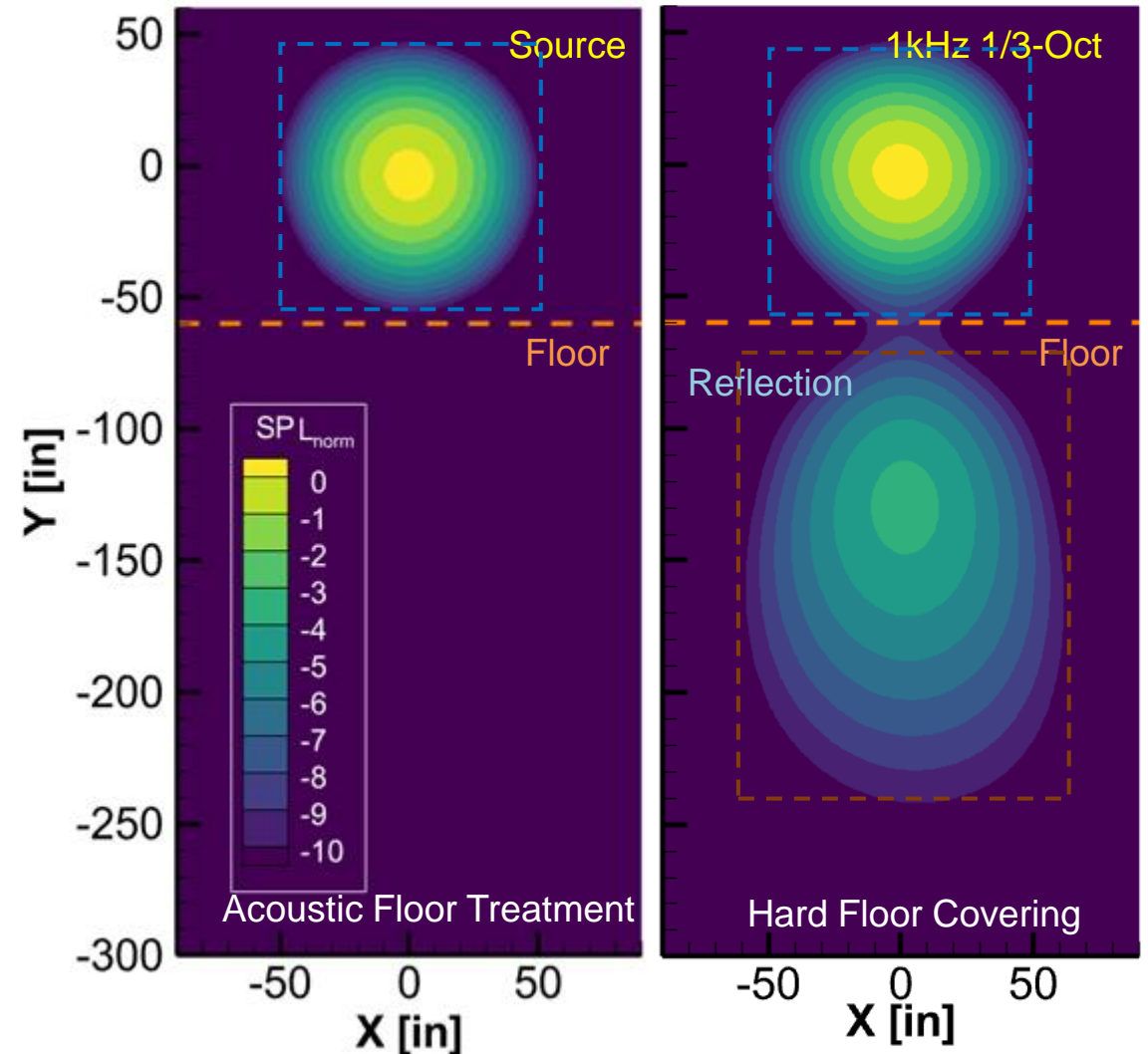
Beamforming

- Conventional frequency-domain beamforming (CFDBF)
- CLEAN deconvolution
- Static runs to identify reflection
- Flow-on runs to identify noise sources
- Integration for background noise rejection
- Correction for flow convection and shear layer refraction

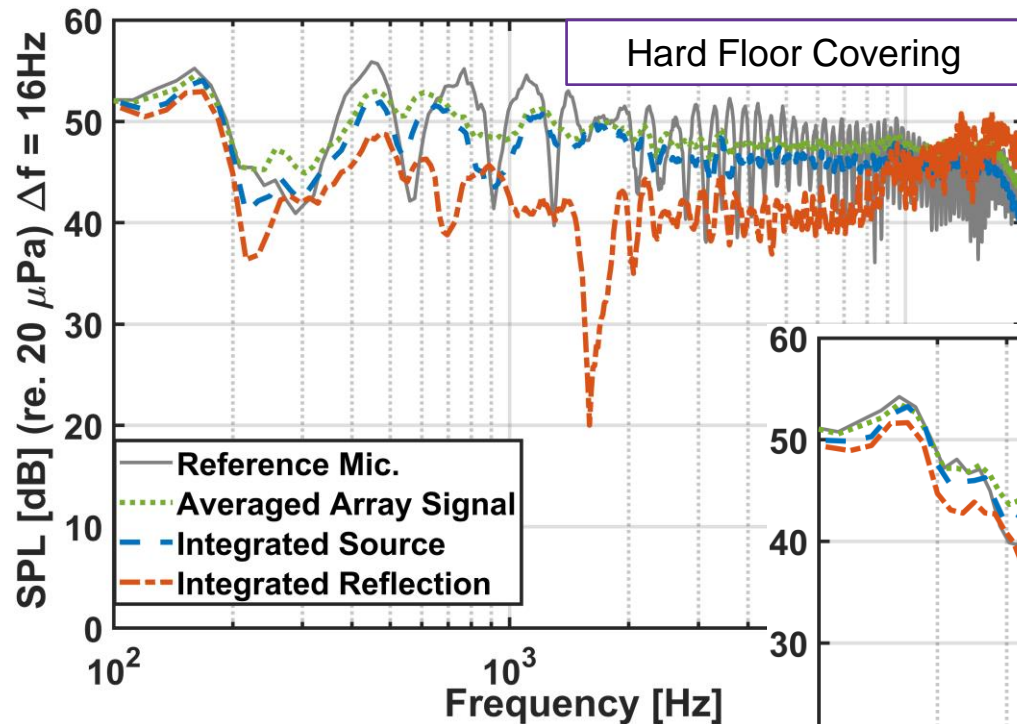


Results – Static (No-Flow)

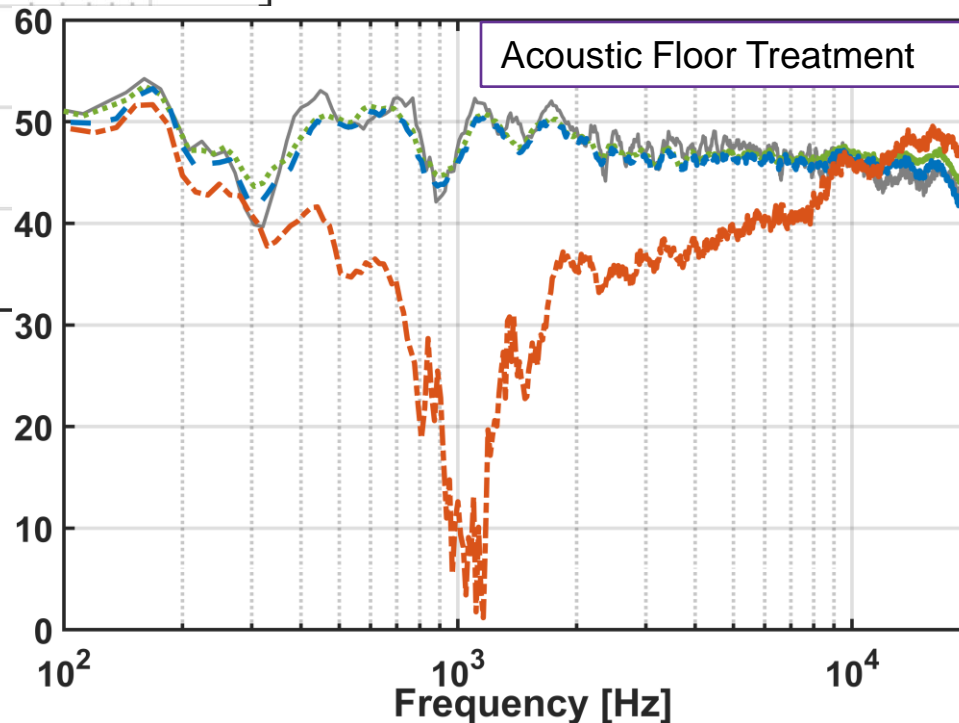
- Demonstrate lower reflectivity of acoustic floor treatments
- Able to identify source reflected off hard floor covering
- Reflection captured as “image source” below floor
- Could not identify other sources of reflection
- Extract spectra by integrating around source/ reflection



Results – Static (No Flow)



- Averaged signal across all array microphones higher in presence of reflection
- Integrating around source brings level closer to true level

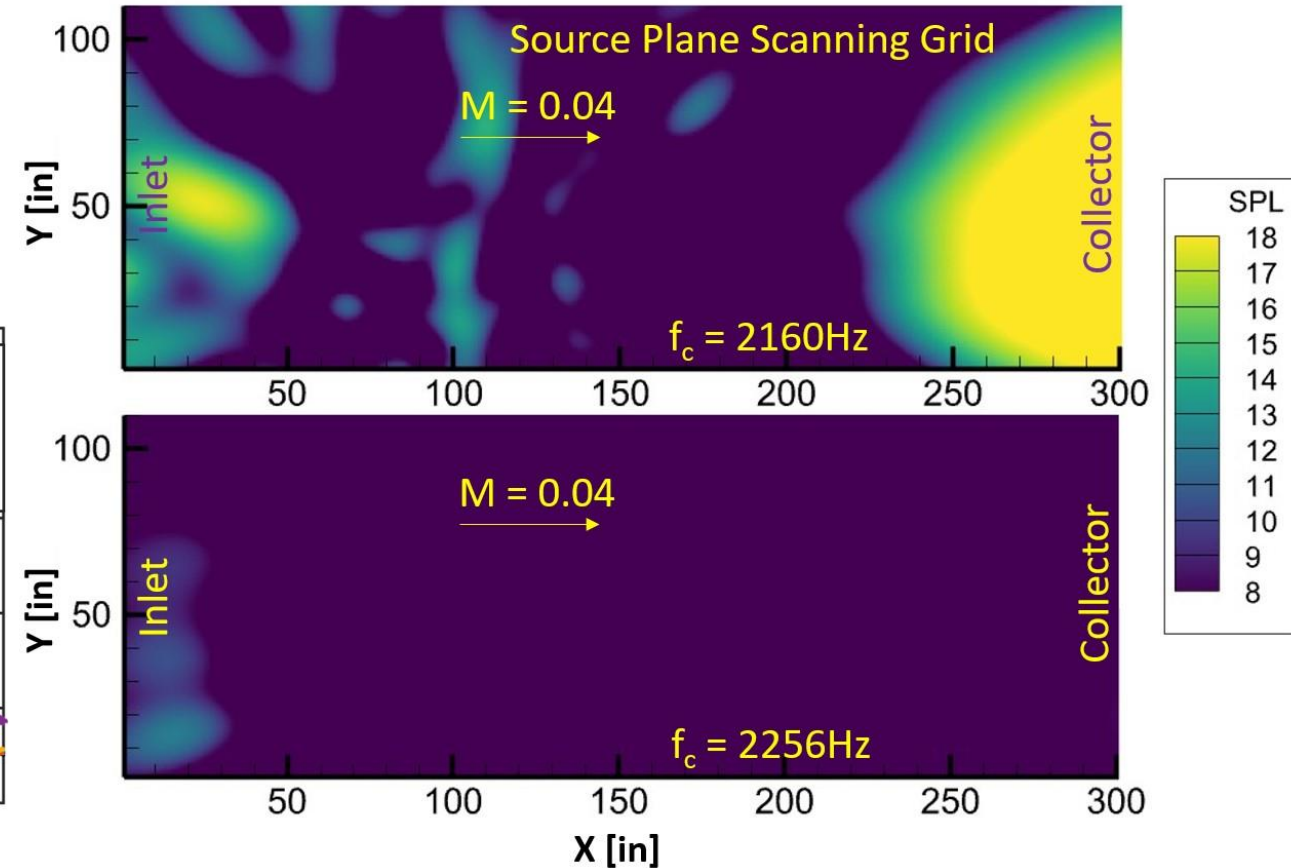
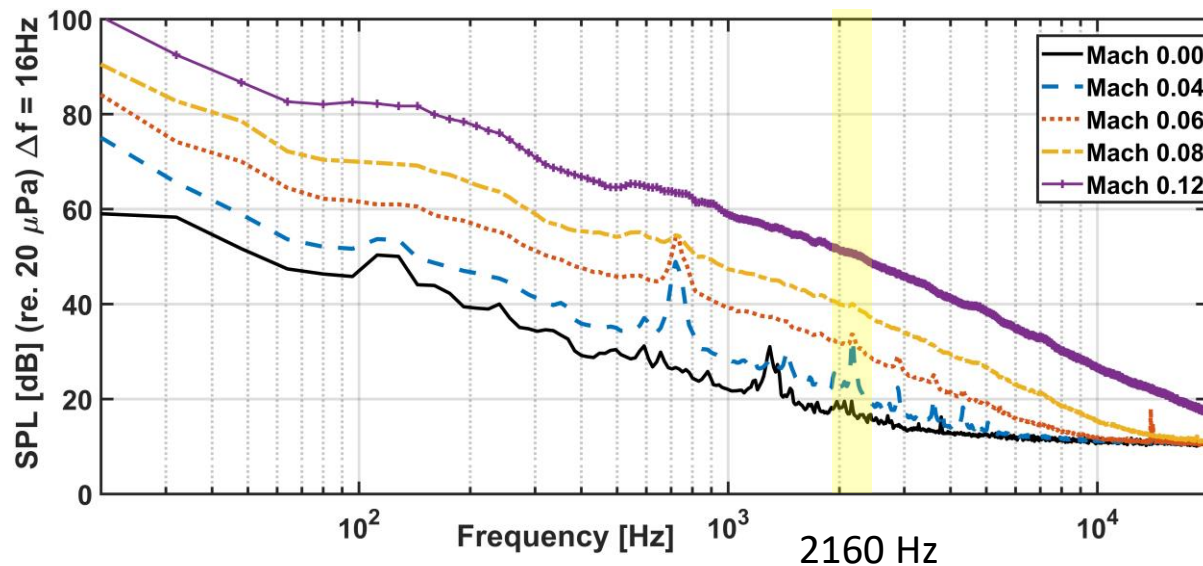


Details regarding floor reflectivity
in Zawodny et al. 2024

- Averaged signal same as integrated signal with acoustic floor treatment
- Reflected data impacted by source directivity
- Reflected data above 10 kHz likely incorrect

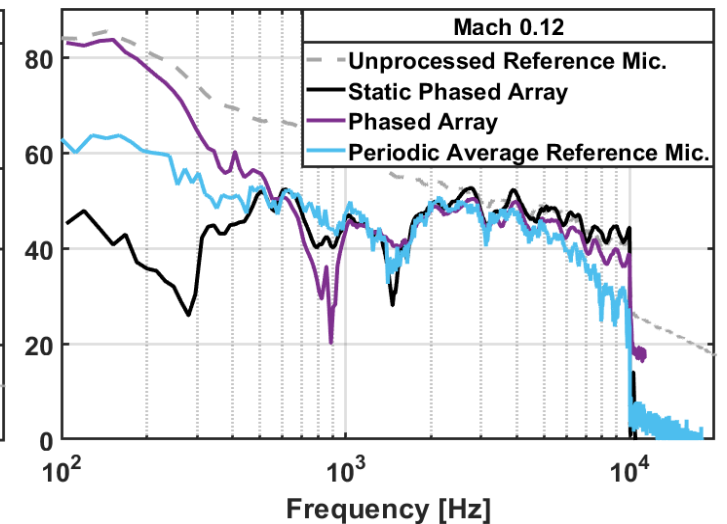
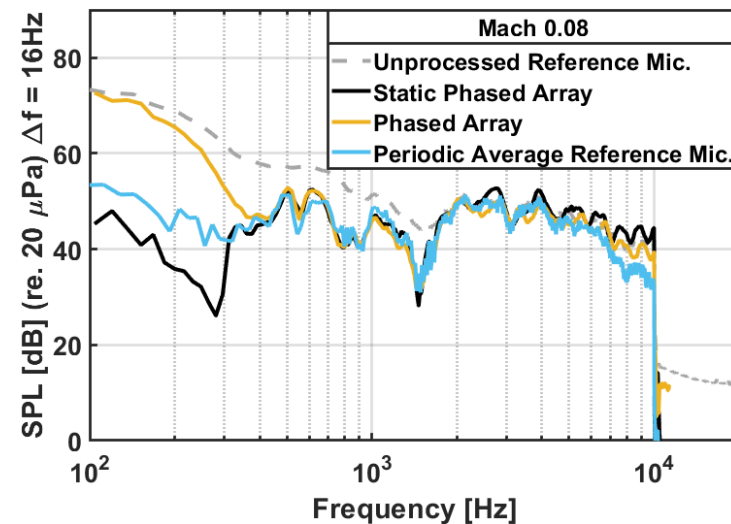
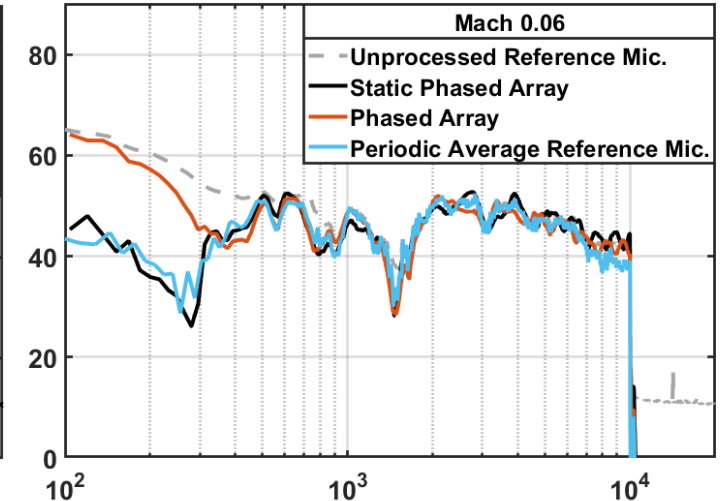
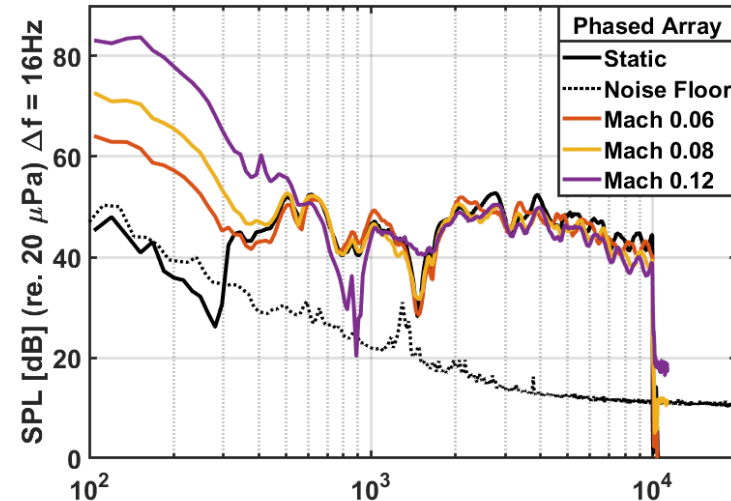
Results – Flow-On

- Background noise source identification
 - Identified direction of 2160 Hz peak in Mach 0.04 data
 - 720 Hz peak in spectra too low for array to resolve clearly
 - Both peaks likely harmonics of fan cooling unit



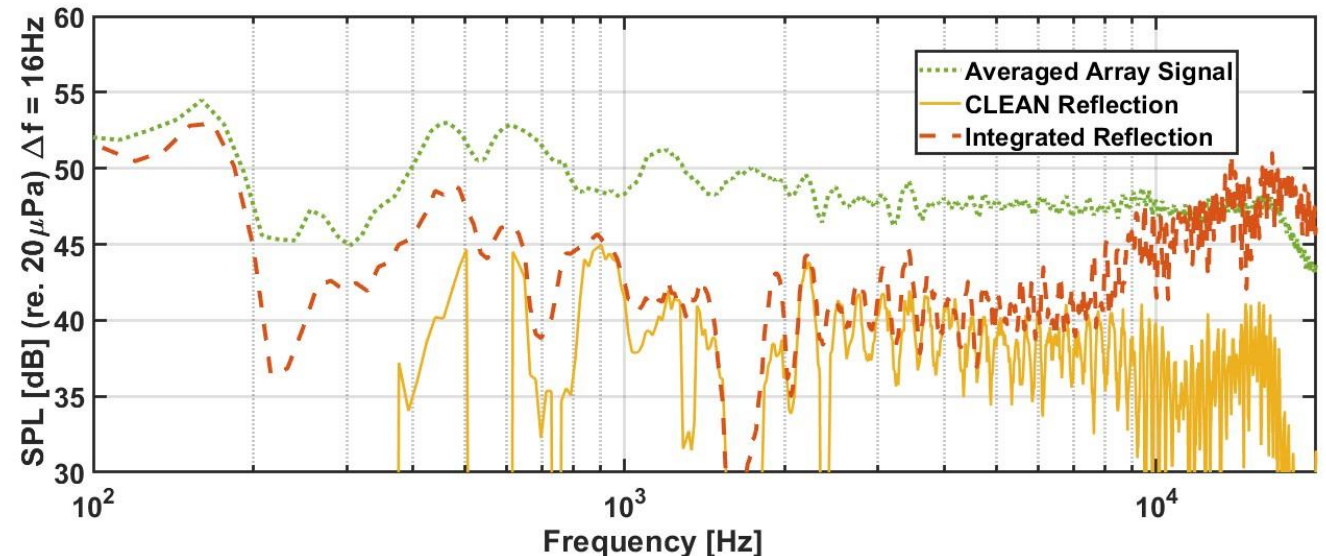
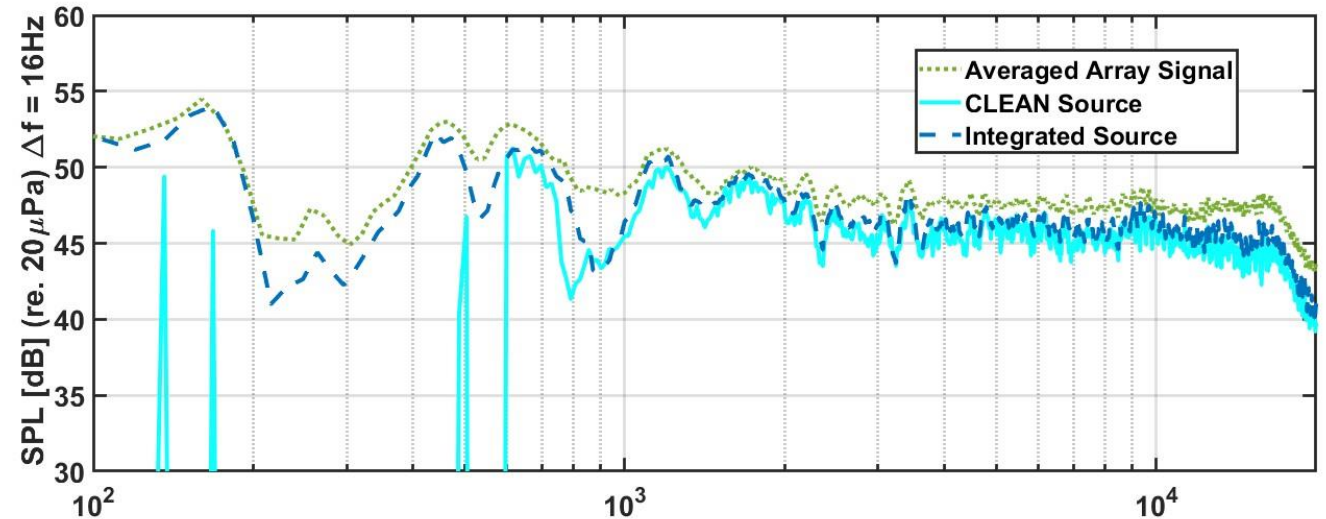
Results – Flow-On

- Background noise rejection
- Captures high frequency better than periodic averaging of single microphone
- Does not require periodic signal
- Periodic averaging better at low frequency where the array response is poor



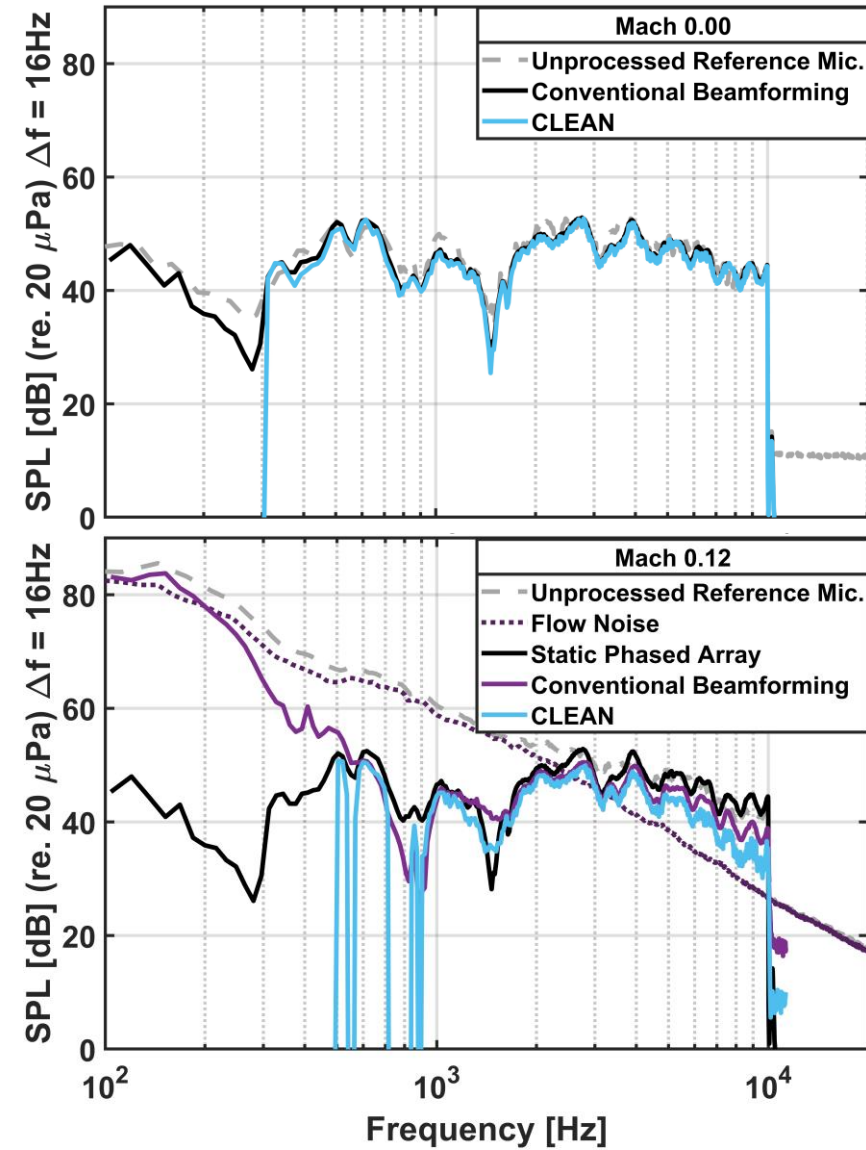
Results – Deconvolution (Static)

- CLEAN deconvolution removes effects of scanning grid
- Struggles at frequencies below array design level ($f = 1$ kHz)
- Further reduces integrated source below averaged signal level
- Applicable to reflection because it is sufficiently separated from main source
- Reduces amplitude of reflected spectra for $f > 10$ kHz
- Difficult to measure true level of reflected signal



Results – Deconvolution (Flow-on)

- SPL dropouts at low frequency
- Impaired high frequency response through shear layer
- Sensitive to decorrelation through turbulent shear layer



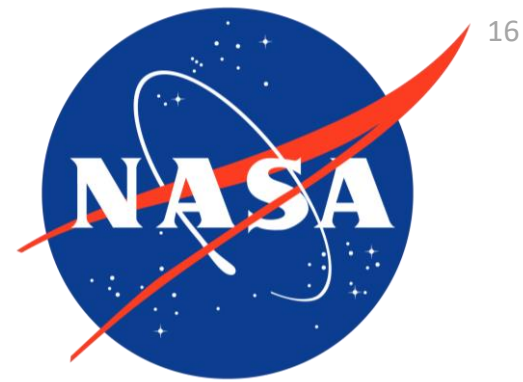


Conclusions

- Testing with known acoustic sources will allow better interpretation of results from unknown sources
- Single microphone measurements overestimate source strength when reflective floor is present
- Integrating around source in beammap rejects contributions from reflections
- Conventional Frequency Domain Beamforming (CFDBF)
 - Reflection from acoustically treated floor not observed in beammap
 - Able to determine direction of 2160 Hz peak present at certain flow speeds
 - Captures high frequency content passing through the shear layer better than periodically averaged single microphone
- CLEAN
 - Deconvolution impairs high frequency capture through shear layer
 - CLEAN deconvolution may improve low frequency response below designed limits but also exhibits frequency dropouts



Acknowledgments



The authors thank the LSAWT and 14x22 test engineers and technicians, M. Galles for assistance designing new floor treatments.

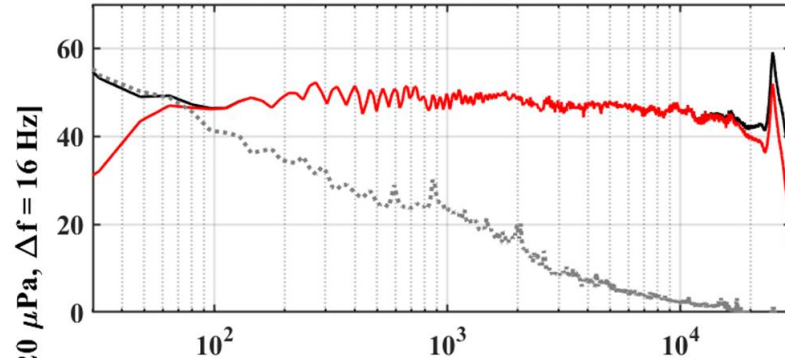
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Broadband Output of Sources

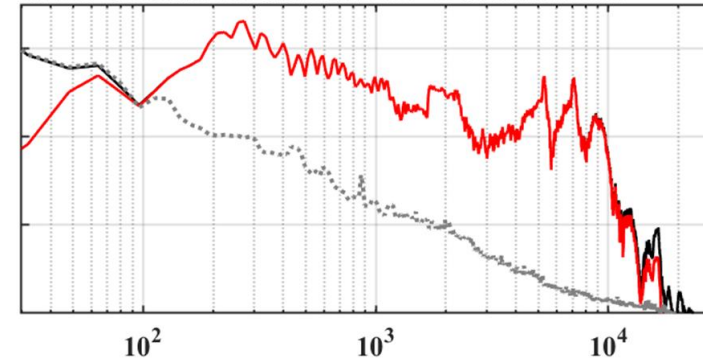


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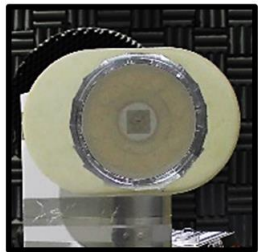
Static Directional Source - Mackie



Static Omnidirectional Source - Dodecahedron

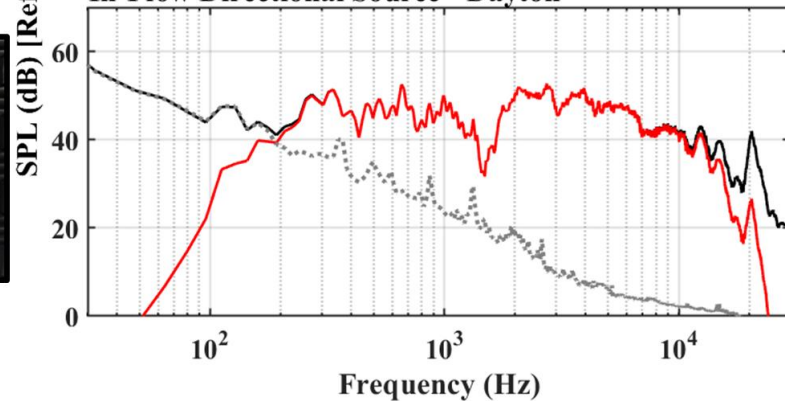


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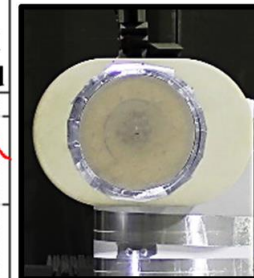
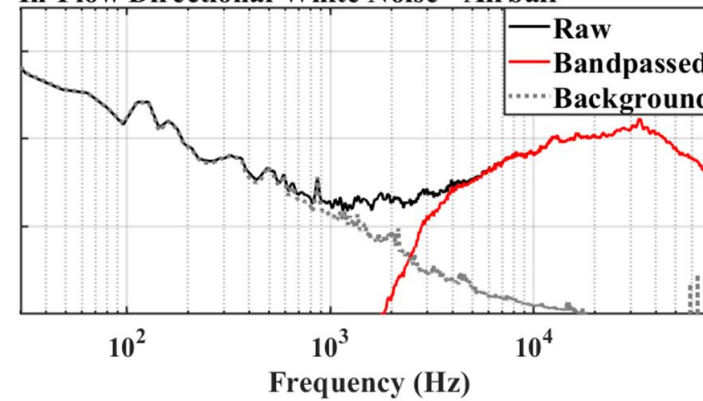


Source: NASA

In-Flow Directional Source - Dayton



In-Flow Directional White Noise - Airball



Source: NASA