

# LTV-xEVA Applied Injury Biomechanics

Keegan Yates, PhD1

Aaron Drake1

Kristine Davis2

*Trade names are used in this presentation for identification only. Their usage does not constitute an official endorsement, either expressed or implied, by the National Aeronautics and Space Administration.*

1KBR, Human Health and Performance Contract, Houston, TX

2NASA Johnson Space Center, Houston, TX

## **Background**



- Operating a rover in reduced gravity while wearing a modern EVA suit is a loading condition with very few analogs
- The Apollo Lunar Roving Vehicle (LRV) is an obvious starting point
	- Apollo astronauts wore an EVA suit, though different from modern suits
	- The Apollo missions were in different terrain and lighting conditions than planned Artemis missions
	- Lunar Terrain Vehicles (LTVs) are different than the Apollo LRV
	- We don't know what the actual Artemis LTV will look like
- A short literature review was performed on the Apollo LRV

## Apollo Notes



- One injury noted (wrist laceration) due to suit<sup>1</sup>
- Obstacles constantly encountered
- Visibility difficult
- "Vehicle traverse cross slope caused discomfort to the crewman on the down-slope side and was avoided whenever possible"<sup>2</sup>



<sup>1</sup> https://www.nasa.gov/wp-content/uploads/static/history/alsj/a16/A16\_MissionReport.pdf <sup>2</sup> https://ntrs.nasa.gov/api/citations/19730025089/downloads/19730025089.pdf

## **Background**

- LTV operation has potential to cause injury
	- EVA suit inertia
	- Rollover risk
	- Blunt loading from suit rigid components
	- Restraints can't interface with body directly
	- Obstacles may be difficult to see
- LTV injury probability difficult to predict with standard tools
	- Anthropomorphic test devices (ATDs) likely wont fit in an EVA suit
	- Brinkley ground rules are broken by presence of EVA suit
	- Types of injury most likely (bruising, abrasions, point loading) not considered by existing dynamic injury tools
- **Human body models (HBM) are compatible with EVA suits, and have potential to be used to predict LTV injury**

## **Methods**



- Human body models placed into model of occupant facing xEMU suit hard goods
- Models positioned into two postures
- Models simulated through "worst-case allowable" loading conditions
- Model outputs compared to injury metrics



## Human Body Models

- Global Human Body Models Consortium (GHBMC) 5<sup>th</sup> female, 50<sup>th</sup> male, and 95<sup>th</sup> male occupant models used
- Can be positioned like a human
- Provides outputs similar to ATDs (accelerations, forces, etc.)
- Can provide contact forces with suit components



## Suit Model



- xEMU model used for all simulations
- M95 uses the large HUT
- Model consists of only the rigid suit components that face the occupant
	- Harness shoulder pads used in all cases
	- Back pad used for F05 model
- HBMs placed in suit in roughly the right posture
- Final positioning done as a pre-simulation
	- Allows HBM to come to final position with natural contact with the suit
	- Allows for deformation of the HBM flesh



## LTV Agnostic Model



- Restraints were modeled as a rigid attachment of the HUT to a seat and feet to floor
- Greatly simplifies modeling effort
	- Non-rigid restraints require modeling of seat, restraint system, and pressurized suit
	- Interaction between seat, restraint, and suit is also crucial to capture
- Rigid attachment may be the worst case for single events
	- Immediate transfer of loading from vehicle to suit
	- Only single events modeled in this effort
	- Non-rigid attachment may be better for single events
	- Repeated events with non-rigid attachment may cause amplification of loading
	- Non-rigid restraints could represent an injury risk not covered in this work

 $\blacktriangleright$ 

#### **Postures**



- Models placed in a seated posture as well a semi-standing "Leaning Post" configuration
	- Based on NASA Ground Test Unit designs
- Settling of occupant within suit performed as beginning of simulation



## Loading Conditions



- Realistic lunar loading conditions currently unknown
- Requirements<sup>1</sup> specify maximum accelerations in all directions and maximum acceleration rate-of-change (jerk)
- "Worst-case allowable" impact starts at the maximum acceleration in one direction, then switches to the maximum acceleration in the other direction
- This process was applied to each direction and combination of directions
- **These are not representative of any particular LTV operation**



<sup>1</sup> Dolick, Kevin R., et al. "Lunar Transport Vehicle Occupant Protection Requirements." (2022).

## Loading Conditions



- Developed curves starting at 0, reaching a steady state in one direction, then reversing
- Steady -state is held for 100 ms
- There are 17 total combinations of these inputs





## Simulation Outputs



- Traditional injury metrics
	- Forces and moments in neck, shoulders, humeri, elbows, wrists, femurs, knees, and tibias
	- Accelerations in head, spine, and pelvis
	- Deflection of the chest
- Contact force between specific bony locations of concern and suit components
	- Able to be used for comparison with requirements
	- Intended to prevent blunt trauma
	- Not traditional



#### Simulations - Directionality





#### Simulations – Size Variation





Leaning post, S9



#### Simulations – Posture Variation





### Simulation Results - General



- Very short duration head impact spikes seen when head contacts the hut
- Energy of impact relatively low

Head Rotational Acceleration – M50 Leaning Post



#### Head Acceleration – M50 Leaning Post



#### Simulation Results - General



• Traditional injury metrics low in all cases, but some contact forces high

Head Injury Criterion\* (unitless), M50 Leaning Post



\* Limit is 340

Head to HUT contact Force



#### Simulation Results - General



- Some simulations passed blunt trauma limits in some body parts
- Limits primarily passed in the acromions, clavicles, and scapular spines
	- F05 primarily passed in acromions and clavicles
	- M50 primarily passed in acromions, clavicles, scapular spines
	- M95 primarily passed in scapular spines



### Simulation Results - Posture



- For most injury metrics, posture affected phase of responses
- Peak loads largely the same
- Position of head/torso within suit largely the same in both postures\*
- Metrics in lower extremities different, but still low for all cases



#### Force in Left Femur



Head Acceleration



#### Simulation Results – Model Size



- All model sizes stayed clear of traditional injury metric limits
- M50 model showed the most cases passing blunt trauma limit
- Only three conditions did not pass any blunt trauma limit for at least one model



#### Head Acceleration

## **Limitations**



- This work focused on rigid restraints only
	- May not fully capture injury risk to lower extremities
- Models used in these studies do not respond to loading with active muscle
- Elements inside of the suit other than the harness not modeled
- All cases modeled are allowable during nominal operation of the LTV
	- Off nominal cases not modeled
- Rigid suit components in other parts of the body not modeled

## **Limitations**



- Suit/LTV designs and loading conditions not representative of Artemis
	- Techniques developed intended to be design agnostic
	- Loading conditions were all purely linear, i.e. no rotational component
- HBM sizes not all encompassing
	- HBMs can be resized to any particular size
- Model positioning idealized
- Effects of repeated events not captured by this work
	- Repetition can cause amplification
	- Repeated loading on a body part could cause injury

### **Conclusions**



- Traditional injury metrics (e.g., head injury criterion, neck and spine loads) show a low risk of injury
- Blunt loading limits are occasionally passed
	- Limits based on half of force required to fracture the weakest clavicle in a set of cadavers
	- The clavicle was deemed to be the "weakest link" in the torso
	- Model contained no padding other than harness pad (and back pad for F05)
- Head contact forces high, but it is unclear if the short duration could be responsible for injury
	- Study on boxer punches showed similar impulse, but more head acceleration<sup>1</sup>
- Poorest performance relative to the blunt loading requirements seen in M50
	- Back pad in F05 model may have helped to prevent high closing velocities
- The data don't show a preference between seated and the semi-standing posture

1Walilko, Timothy J., David C. Viano, and Cynthia A. Bir. "Biomechanics of the head for Olympic boxer punches to the face." *British journal of sports medicine* 39.10 (2005)

### Acknowledgements



- Many people contributed to this work from across NASA
- This work was funded by the NASA Extravehicular Activity and Human Surface Mobility Program (EHP)

#### Questions?



• keegan.m.yates@nasa.gov