

# High-Speed Visualization of Spray Breakup and Velocity Estimation in a Rotating Detonation Combustor Using Laser Induced Fluorescence

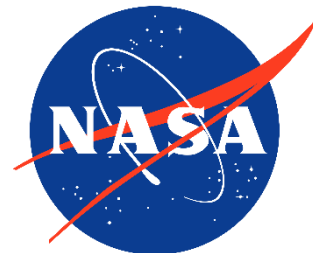
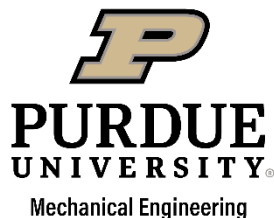
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# Motivation

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## Motivation:

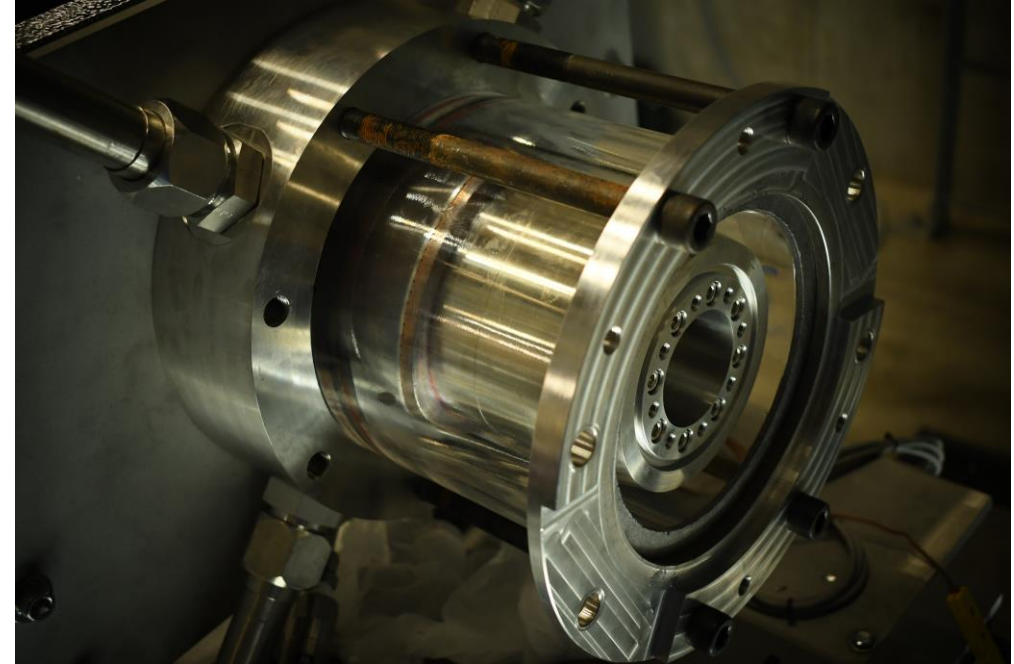
- Potential performance benefits of RDCs highly desired but many open questions remain; particularly for liquid fuel operation
- Quantifiable statistics regarding the recovery and refill process for liquid fuel injectors have not been previously reported
  - What are the driving factors?
  - How can a liquid fuel injector recover and promote sufficient mixing to support detonations in as little as 10s of  $\mu\text{s}$ ?

## Objective:

- Develop a test environment in an RDC where a **single liquid jet** can be studied
- **Directly visualize a liquid fuel spray** to study wave interaction and other dynamics
- Support model validation and generation

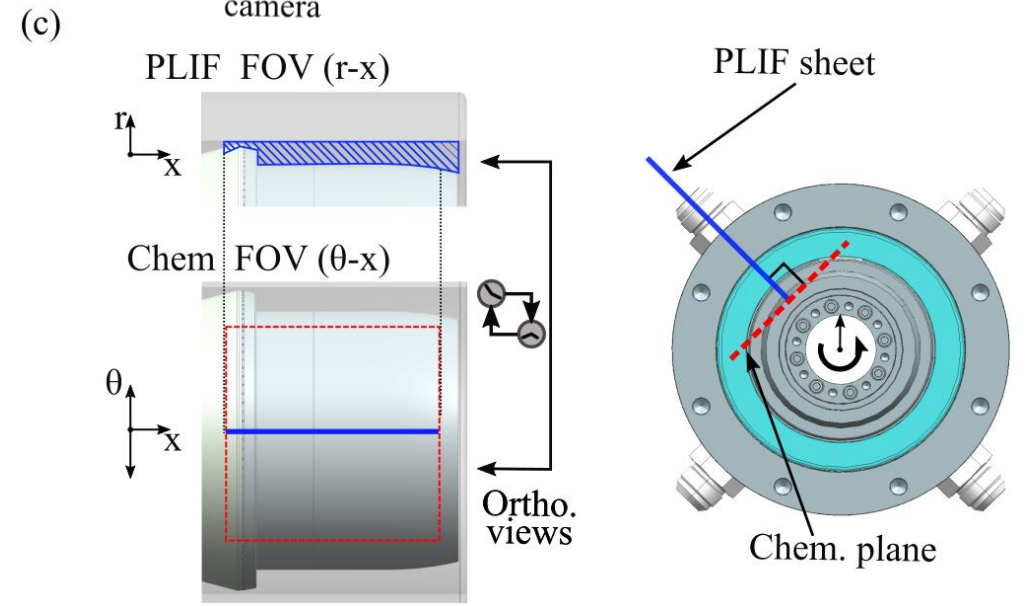
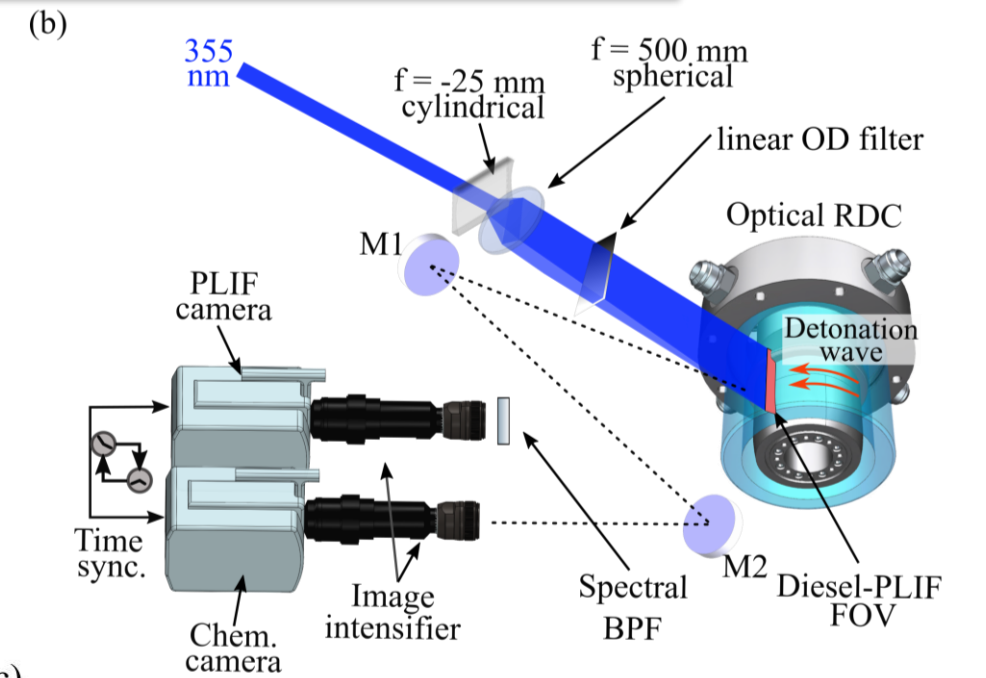
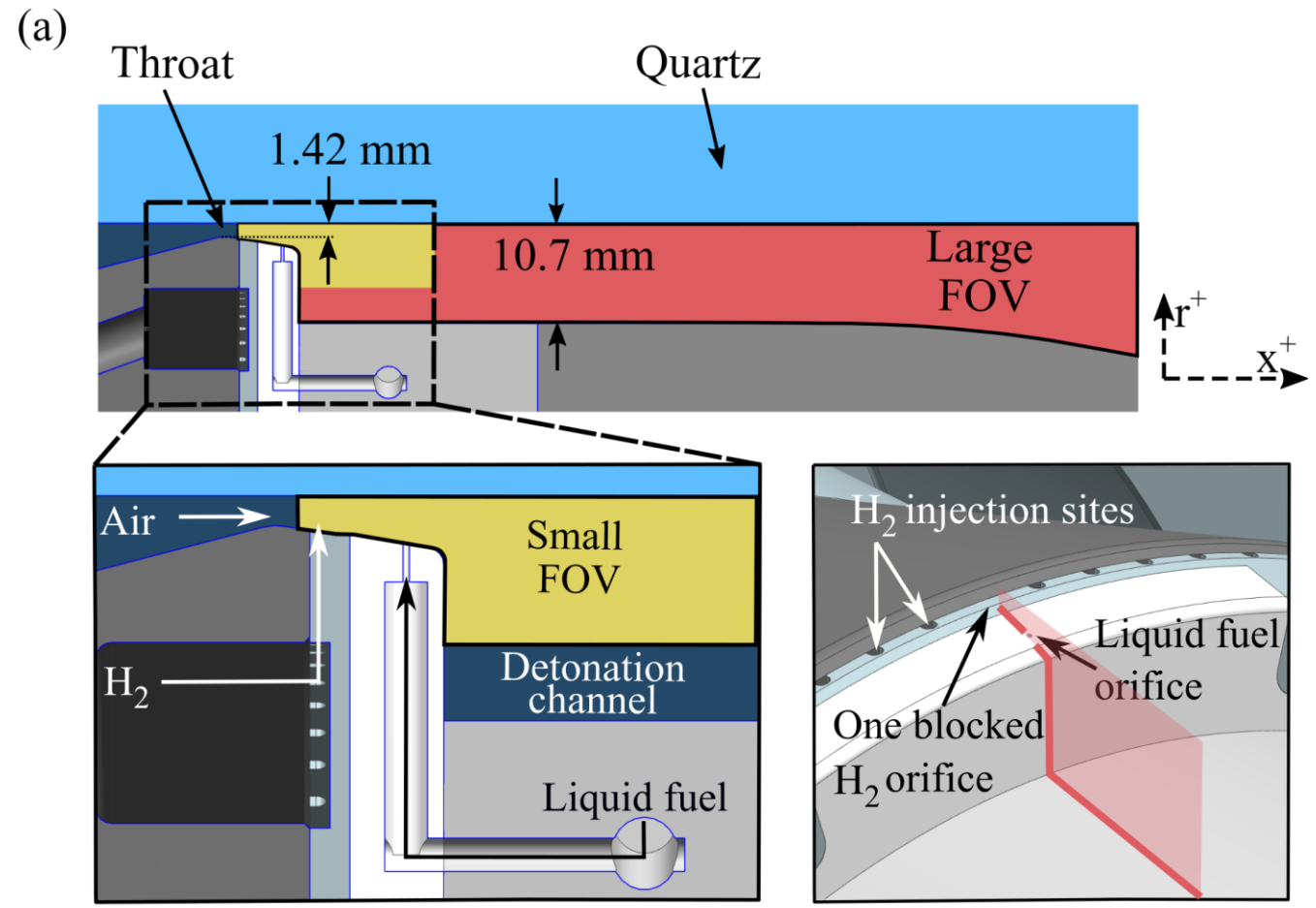
# Test Platform Overview

- 125 mm nominal chamber diameter with optical access
- Operates with non-premixed Hydrogen/Air
  - Axial slot air injection
  - 100 hydrogen radial injection sites
- The RDC platform is well studied and characterized for a plethora of operating conditions
  - “Standard” test condition of 0.23 or 0.46 kg/s,  $\Phi = 1$ , and single wave operating mode at 4 kHz
- For this work, RDC acts as a detonation driver to investigate liquid fuel spray breakup



THOR with optical outer body installed

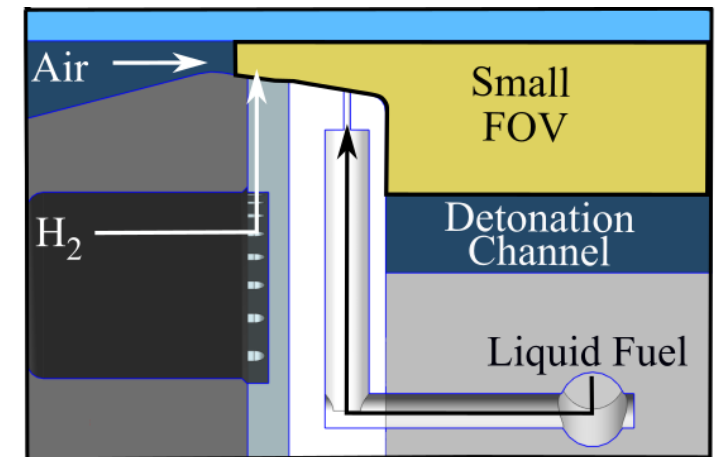
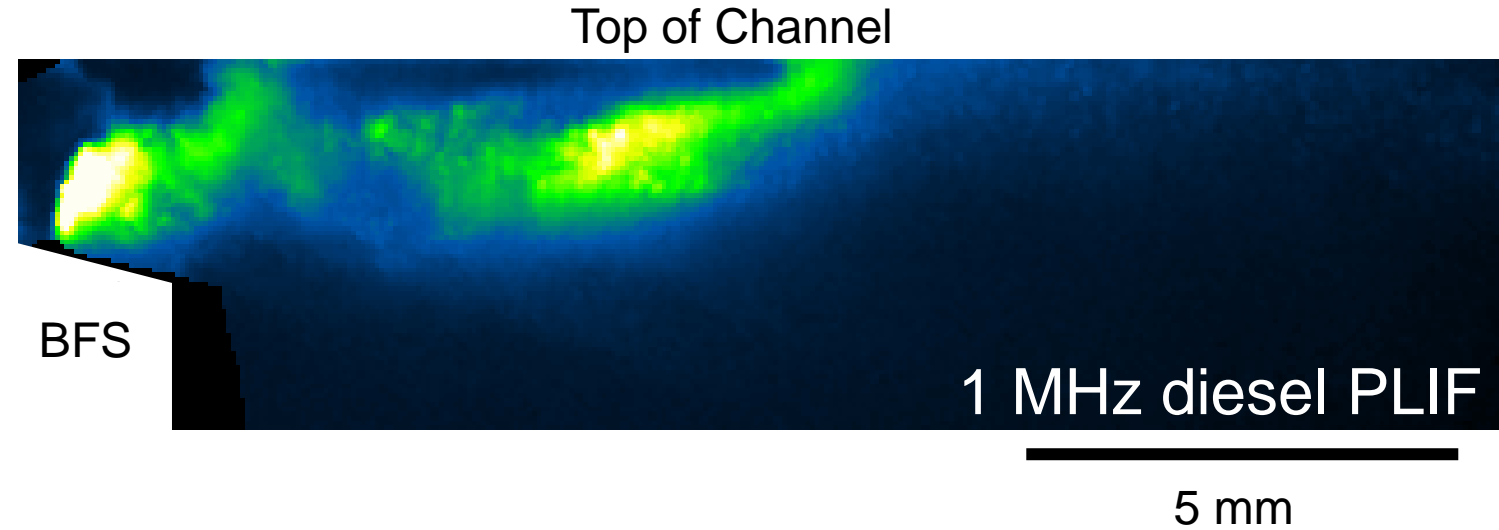
# A Look at Prior PLIF Work



Hoeper et al., "Liquid fuel refill dynamics in a rotating detonation combustor using megahertz planar laser-induced fluorescence," Proc. of the Comb. Inst., 2022

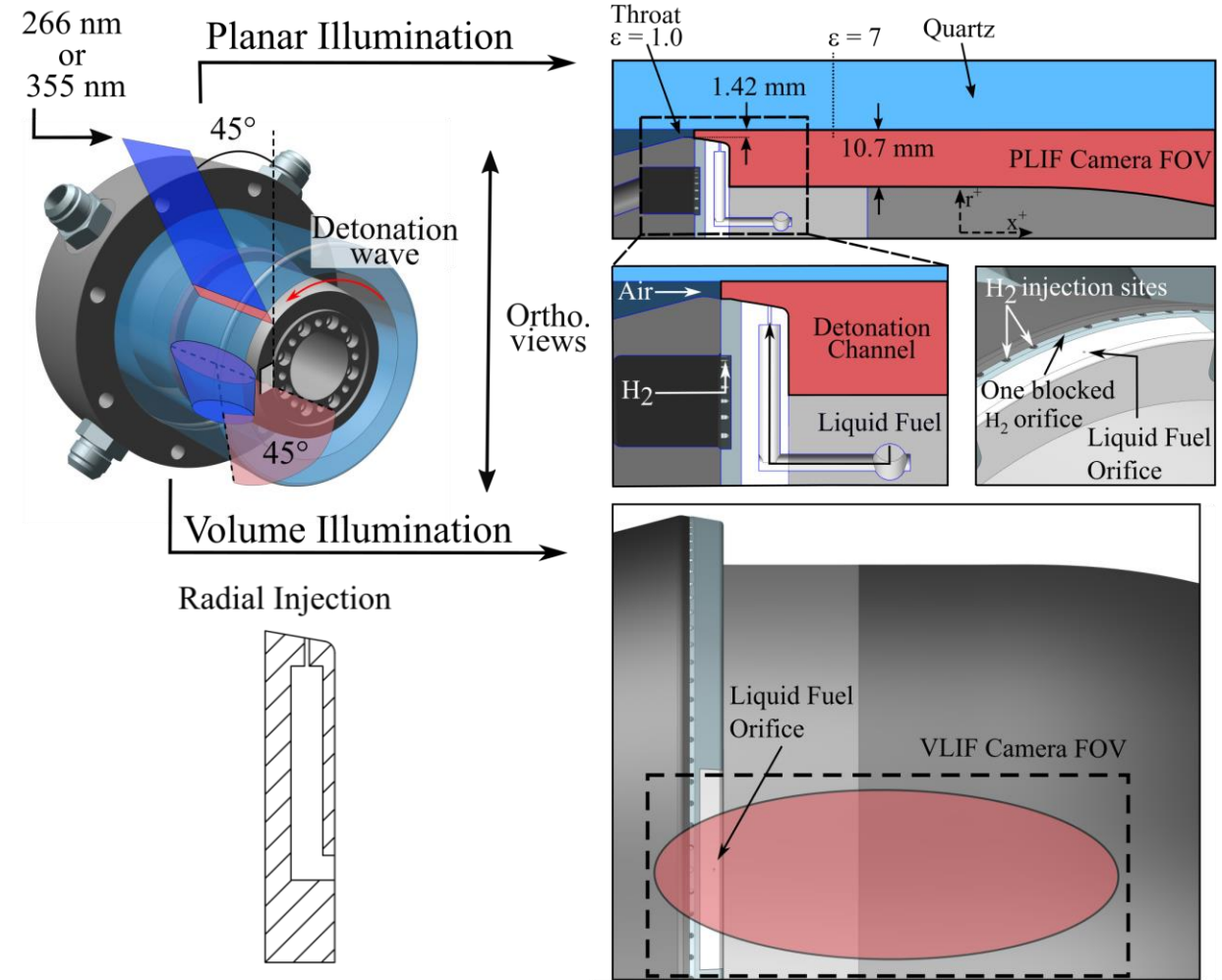
# A Look at Prior PLIF Work

- Example 1 MHz diesel PLIF data from previous work
- Imaging scheme is useful for monitoring near-field jet response in a spatio-temporal resolved manner
- Used to construct refill statistics across several conditions
- 430  $\mu\text{J}/\text{pulse}$  of 355 nm, 55  $\mu\text{m}/\text{pixel}$



# Volume Illumination Scheme (VLIF)

- The azimuthal spreading of the liquid fuel spray can not be captured with the PLIF setup
- In this case, the fuel spray was illuminated volumetrically to capture the axial-azimuthal directions
  - Radial direction information is lost
- The camera was position in a “top-down” view; looking at the PLIF sheet from the edge

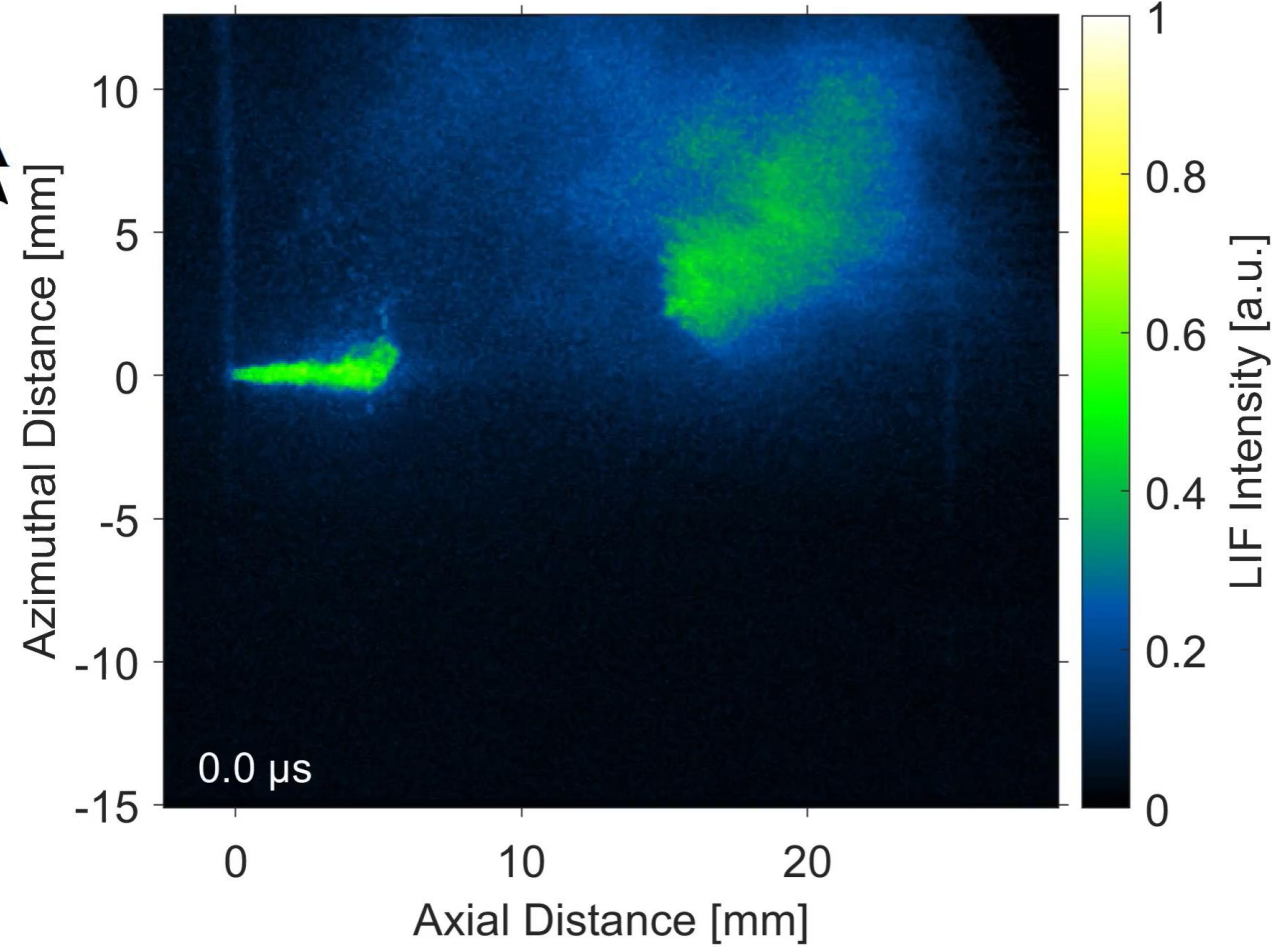
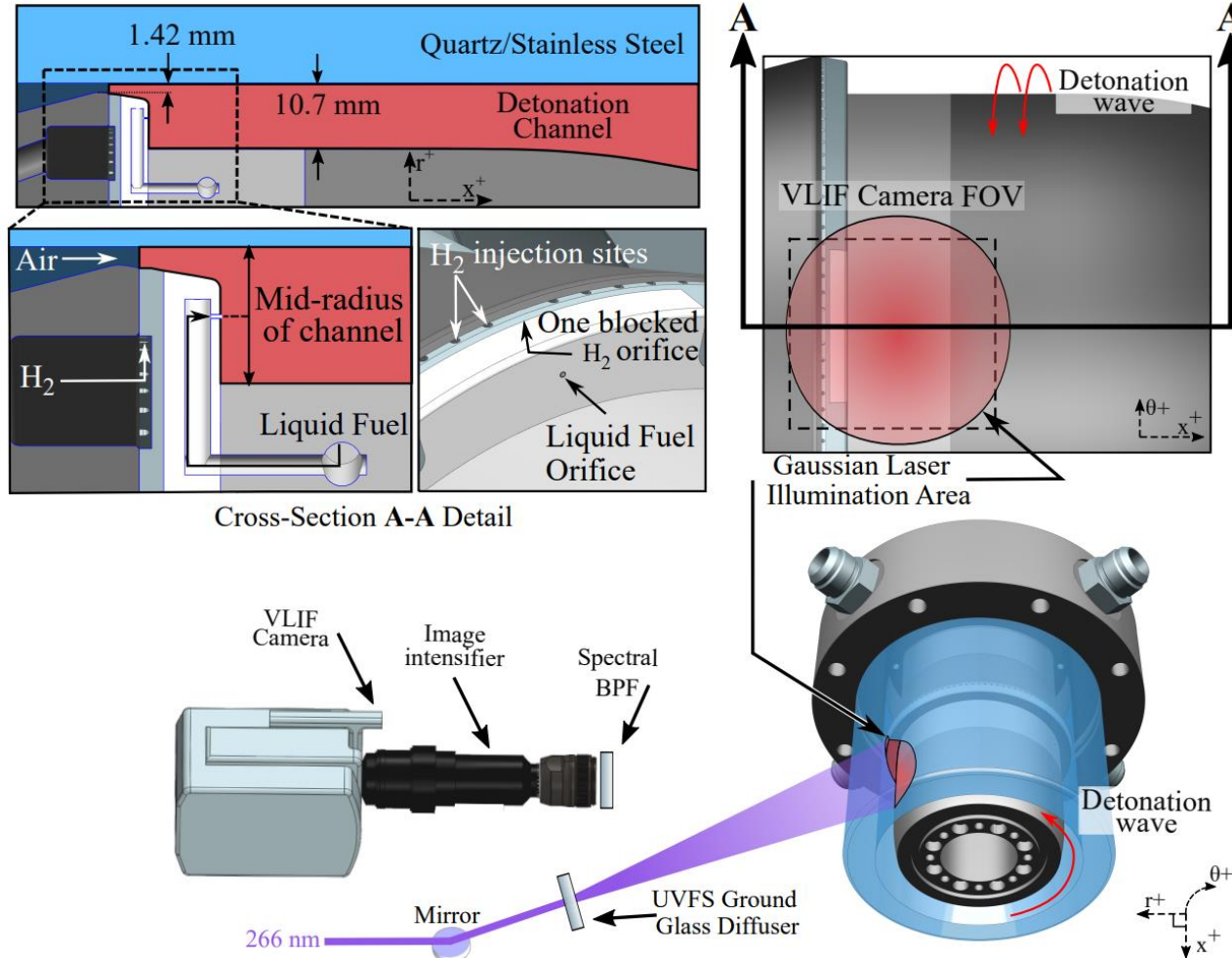


20 mm

# VLIF Sample Video Results

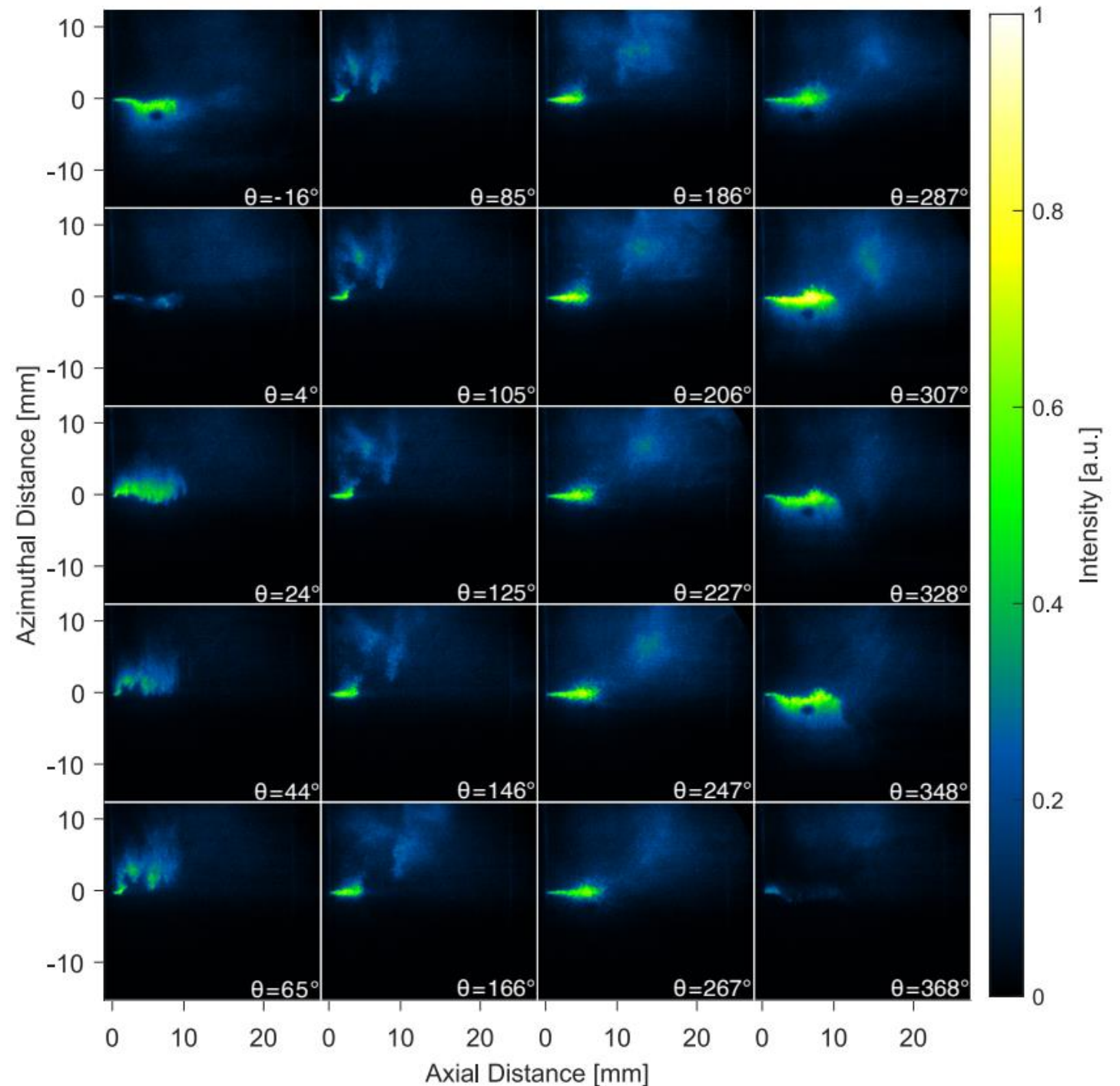
- 300 kHz Jet-A LIF, 10 ms burst length
- 300  $\mu$ J/pulse of 266 nm
- 68  $\mu$ m/pixel

300 kHz Jet-A LIF

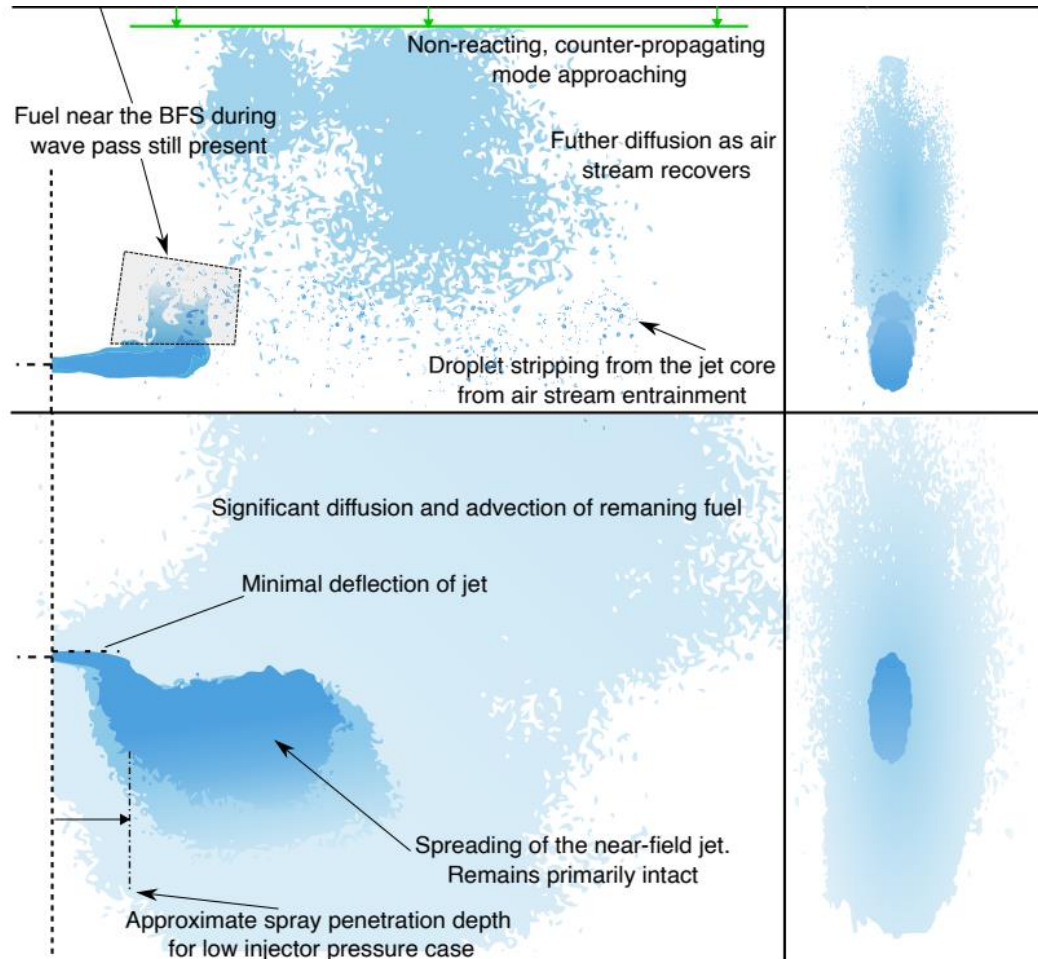
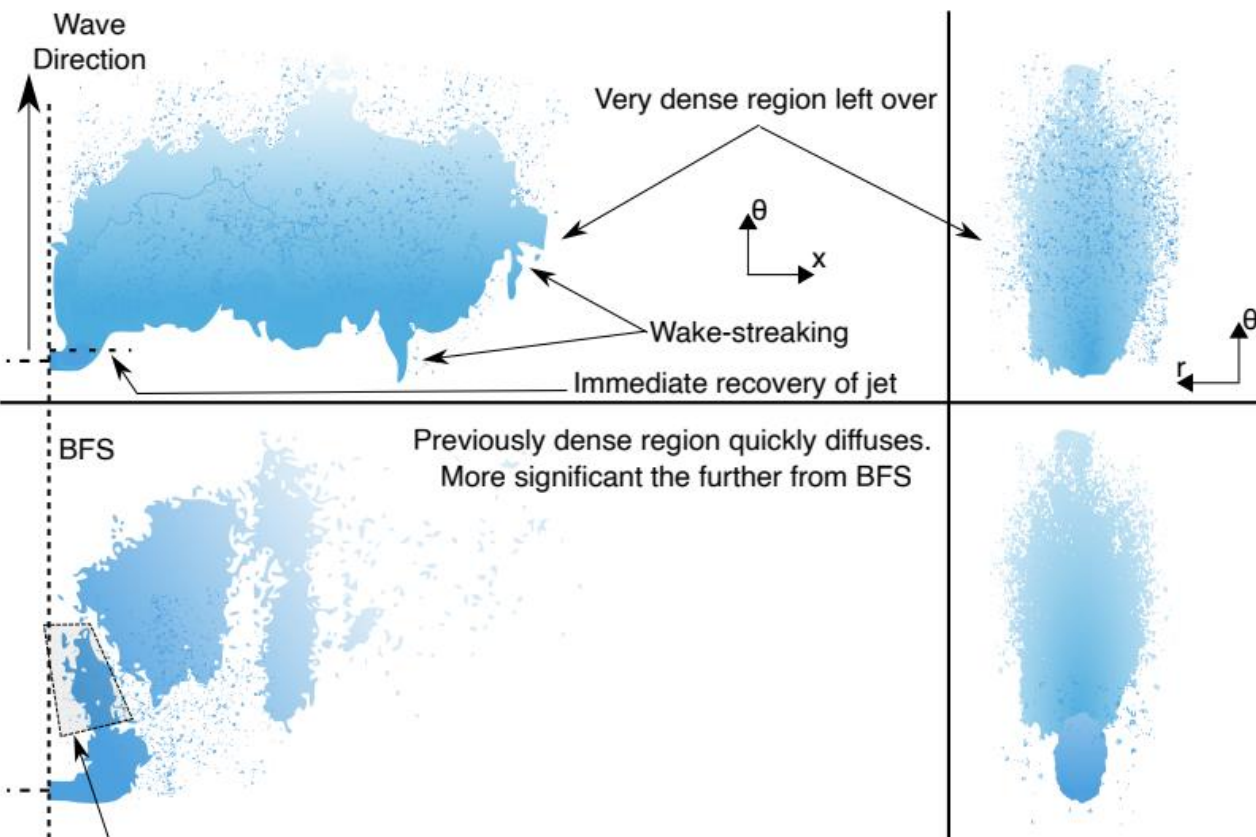


# VLIF Sample Video Results

- Detonation wave passes between the  $-16^\circ$  and  $4^\circ$  frames
- Apparent loss of signal but returns within  $6\ \mu\text{s}$
- After the wave pass, the jet core diffuses quickly
- Injector has no dwell period
- Before the detonation wave arrives, the spray is pushed in the opposite direction

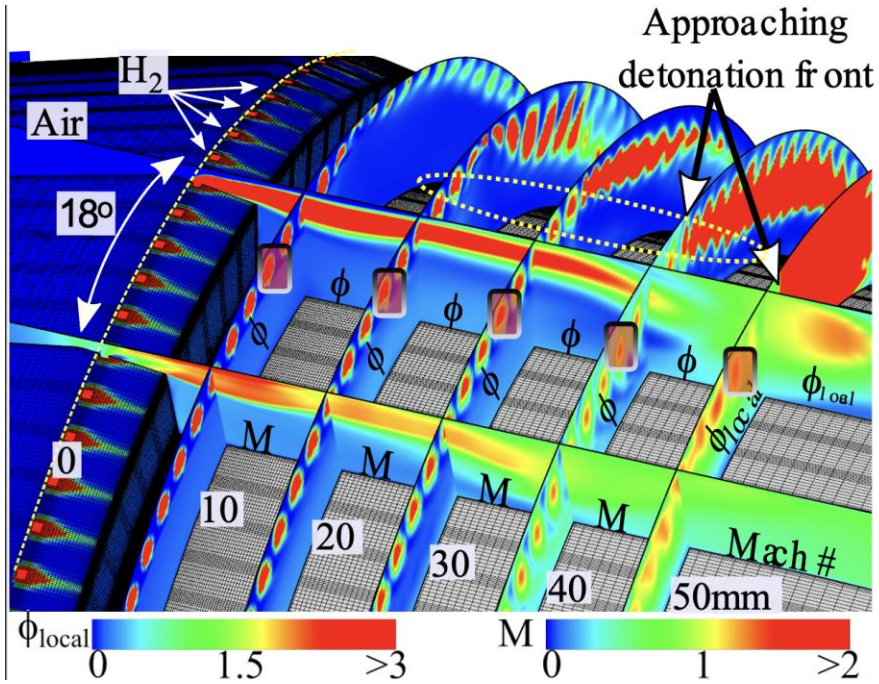


# Major Stages of Spray Evolution



# Comparison Between Chamber Conditions

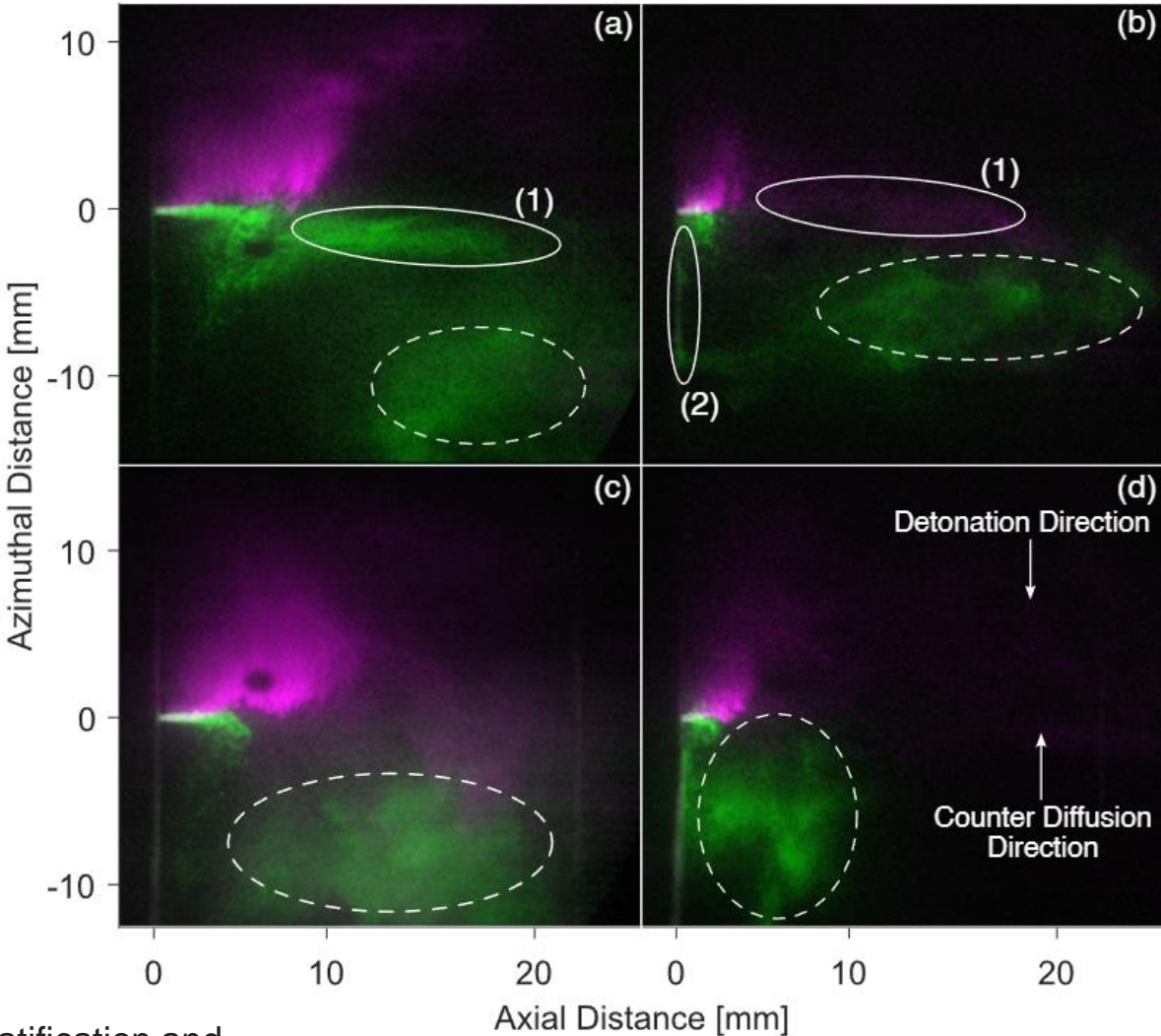
- Regardless of condition, the major features and processes are always present
- More subtle features occur for different conditions



Athmanathan et al., On the effects of reactant stratification and wall curvature in non-premixed rotating detonation combustors, Combs. Flame. (2022)

9 bar inj. pressure

2.7 bar inj. pressure

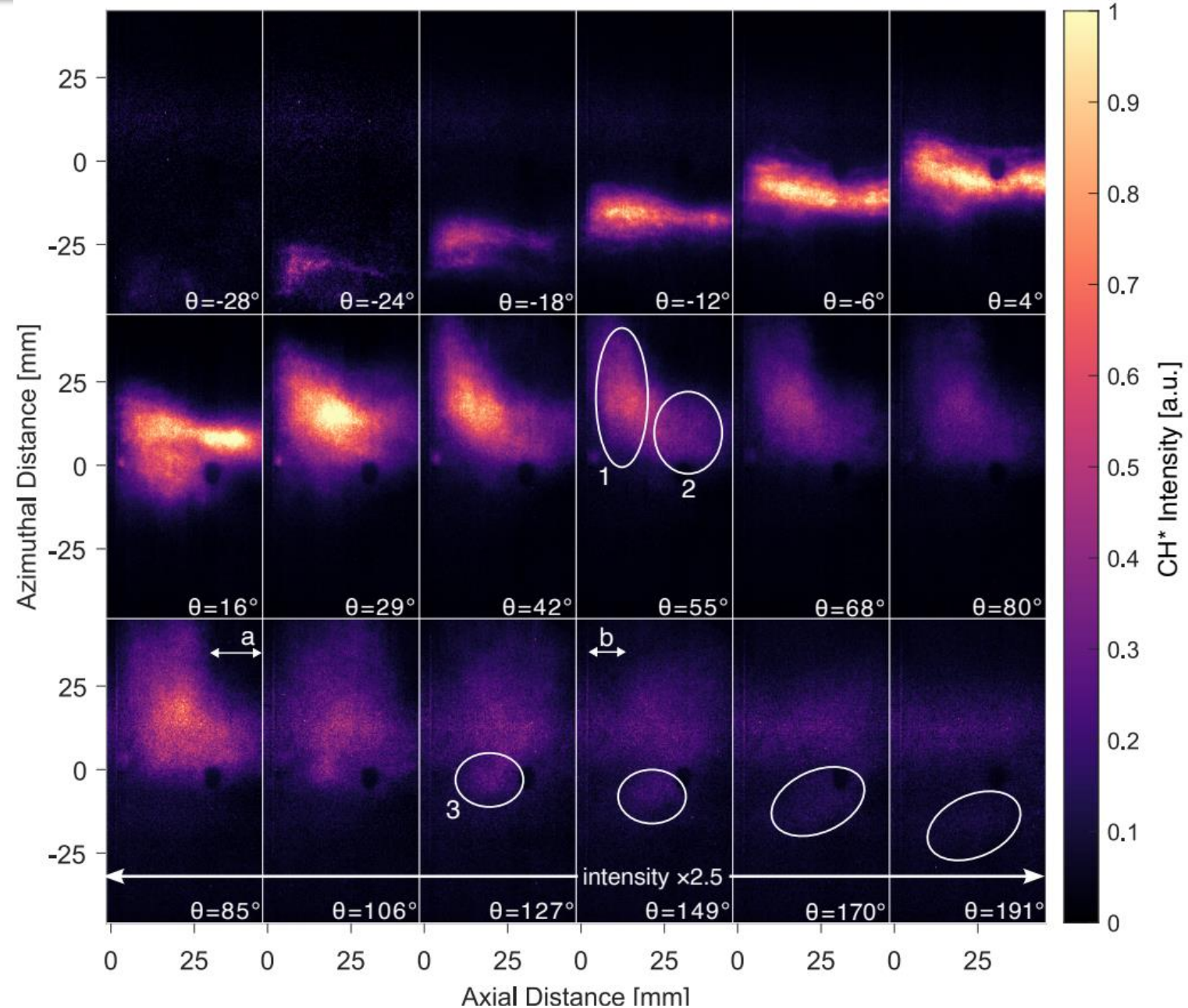


0.45 kg/s of air  
(~110 kg/m<sup>2</sup>/s)

0.23 kg/s of air  
(~55 kg/m<sup>2</sup>/s)

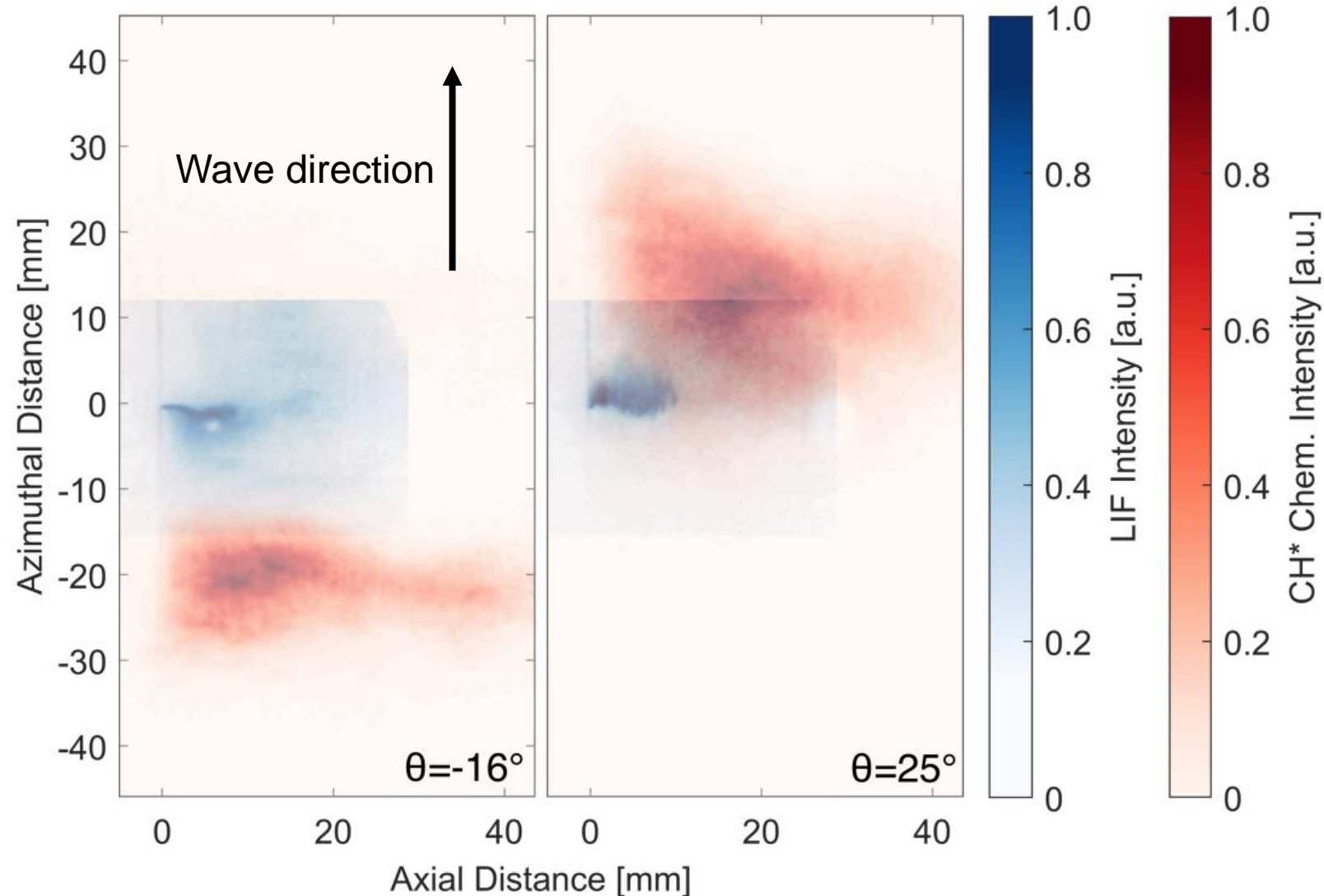
# Chemiluminescence Imaging

- Filtered CH\* chemiluminescence was also performed to support LIF data
- Field of view is slightly larger than the LIF frame
- Data was not taken simultaneously and so phase averaged results are used for comparison



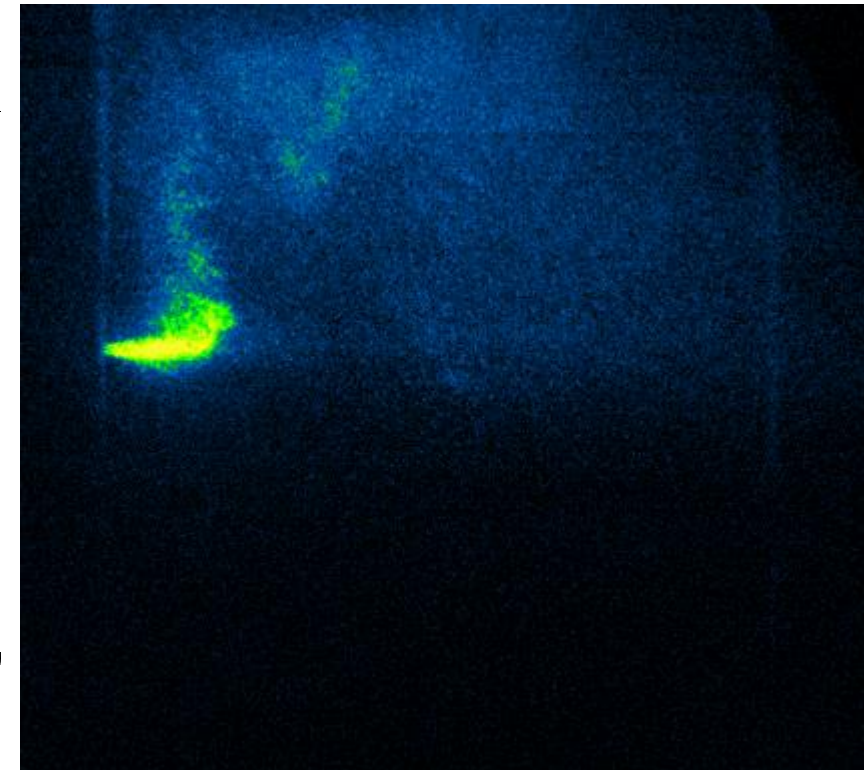
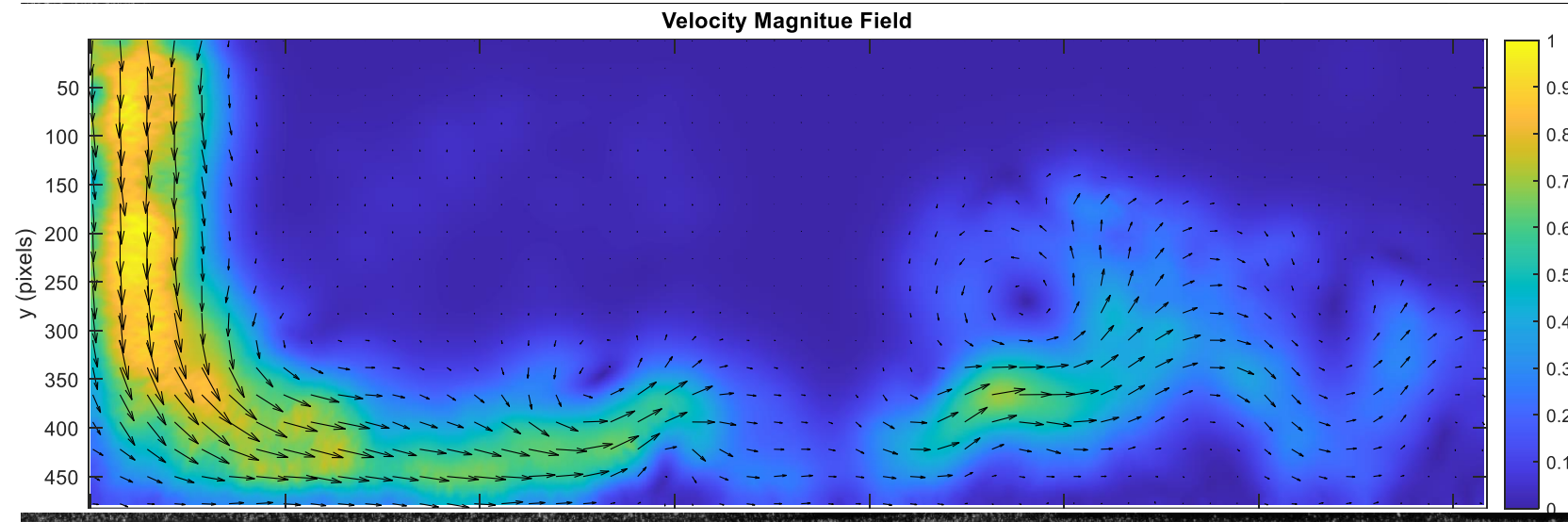
# Jet-A LIF vs. CH\* Images

- CH\* signal is present far away from the injection point. Much further than expected based on LIF images
- Other tests where the clocking between the camera and injection location was varied showed that CH\* does not exist beyond the field of view shown
- Based on the phase angles and the time difference, Jet-A droplets or vapor would have to travel at 200 m/s



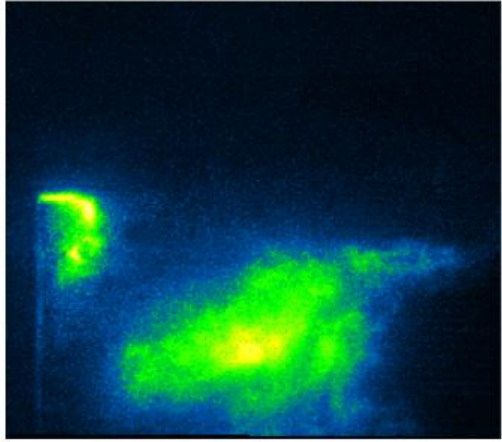
# Velocity Estimation Through Optical Flow

- Optical flow is an image analysis technique that can calculate velocity fields from a pair of images
- Due to the high temporal resolution in the LIF images, assuming the difference between two frames is small enough to be considered passive
- OpenOpticalFlow by Liu and Shen was used for computations. See Liu et al., OpenOpticalFlow, Journal of Research Software (2017)

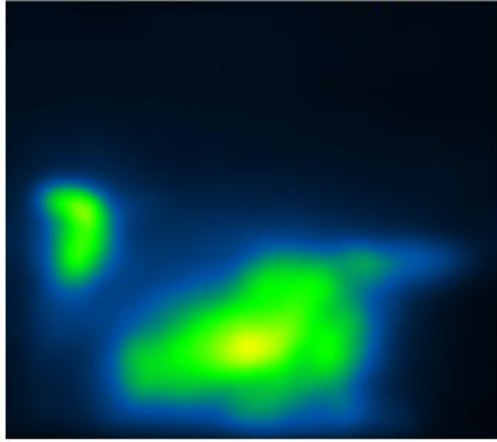


# Velocity Estimation

Original Image



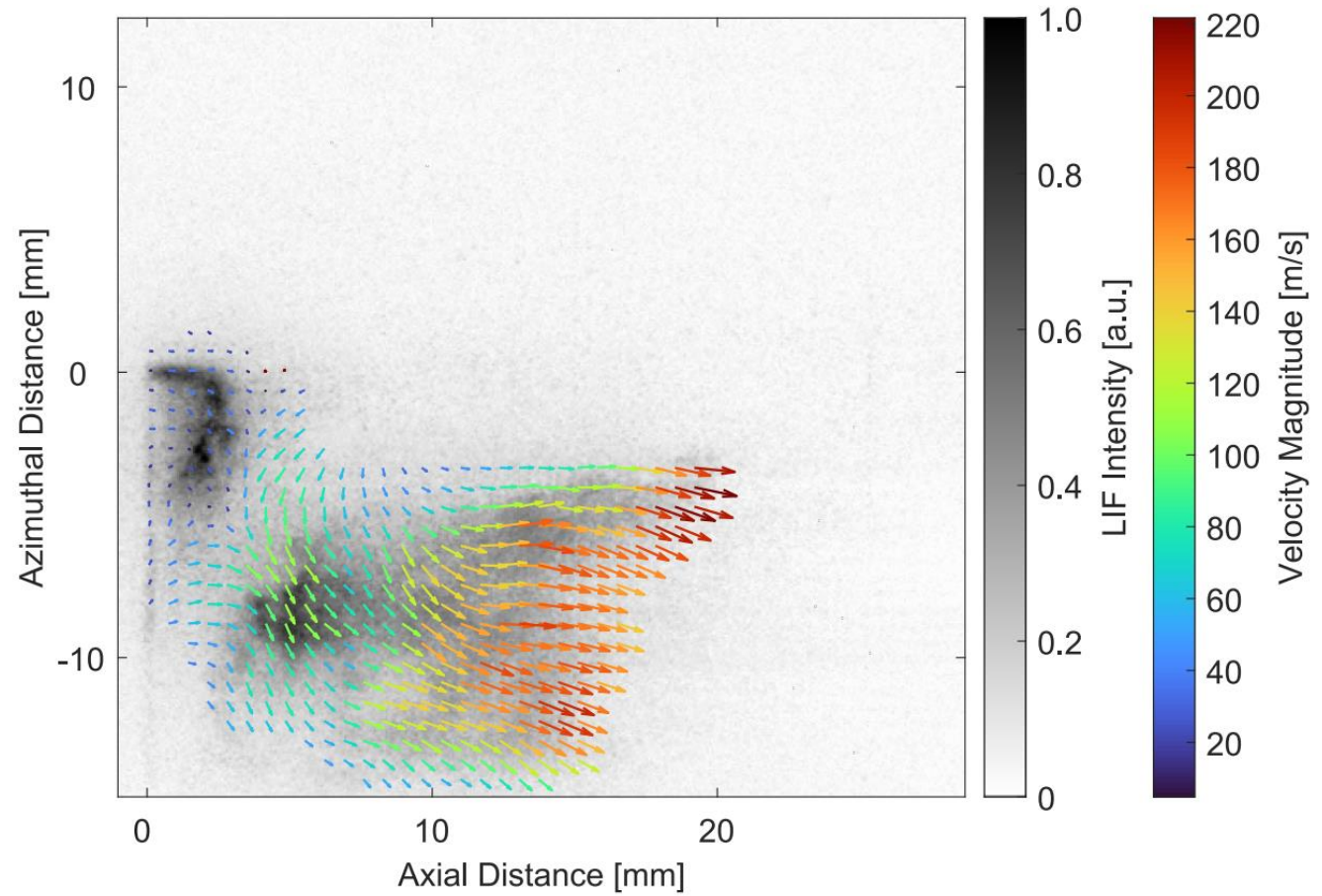
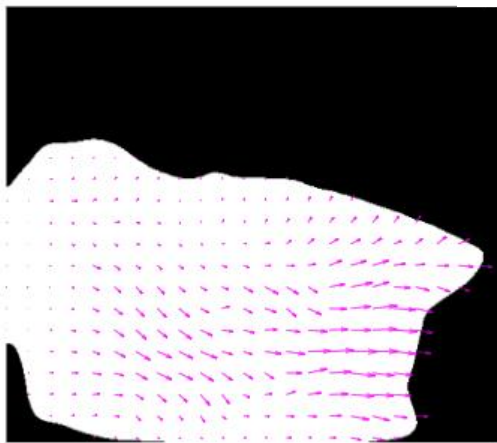
Gaussian Filter Applied



Binarized Image

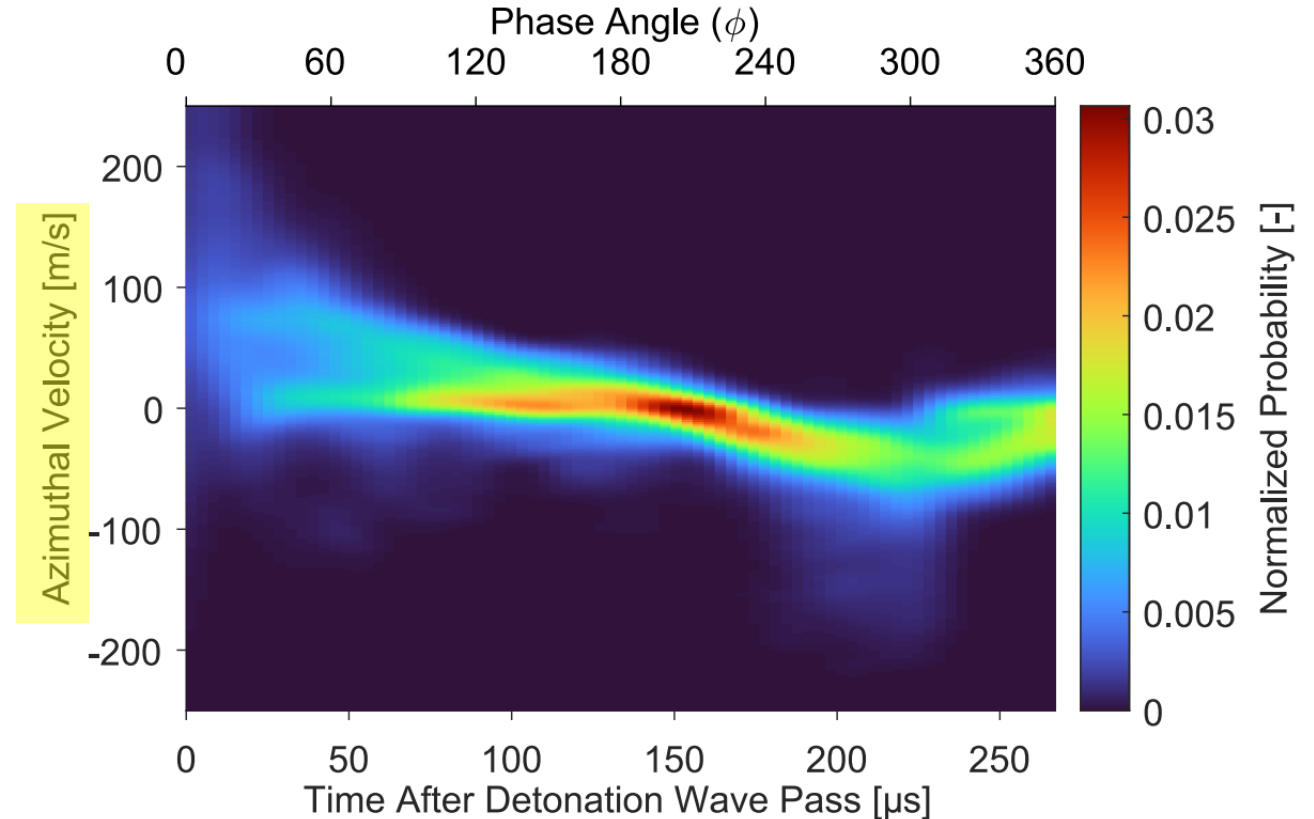
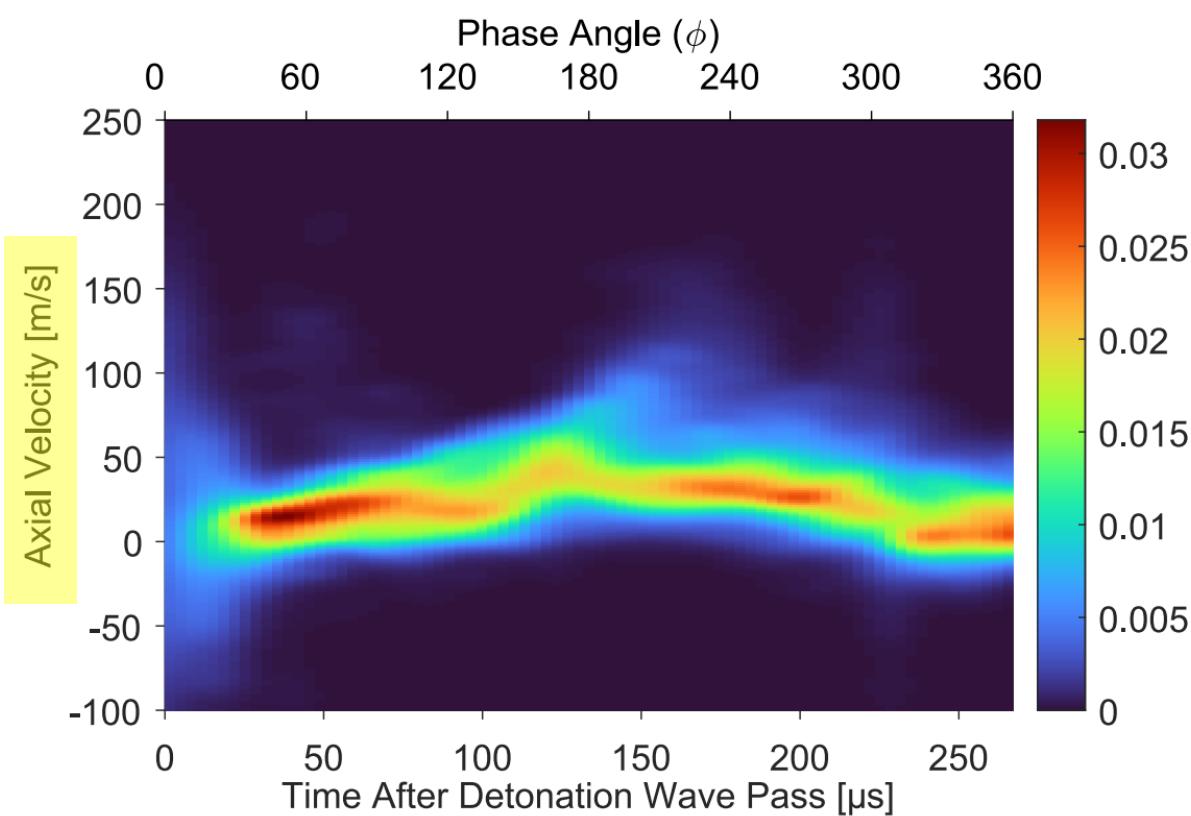


Masked Vector Field

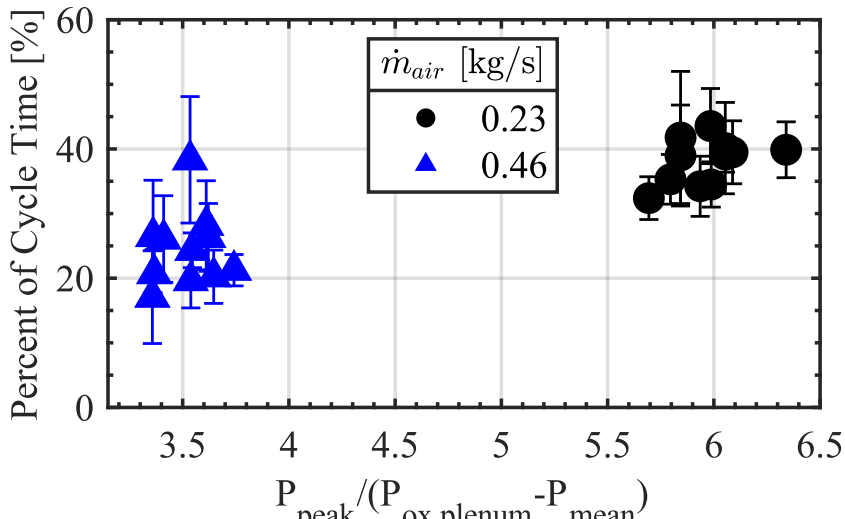
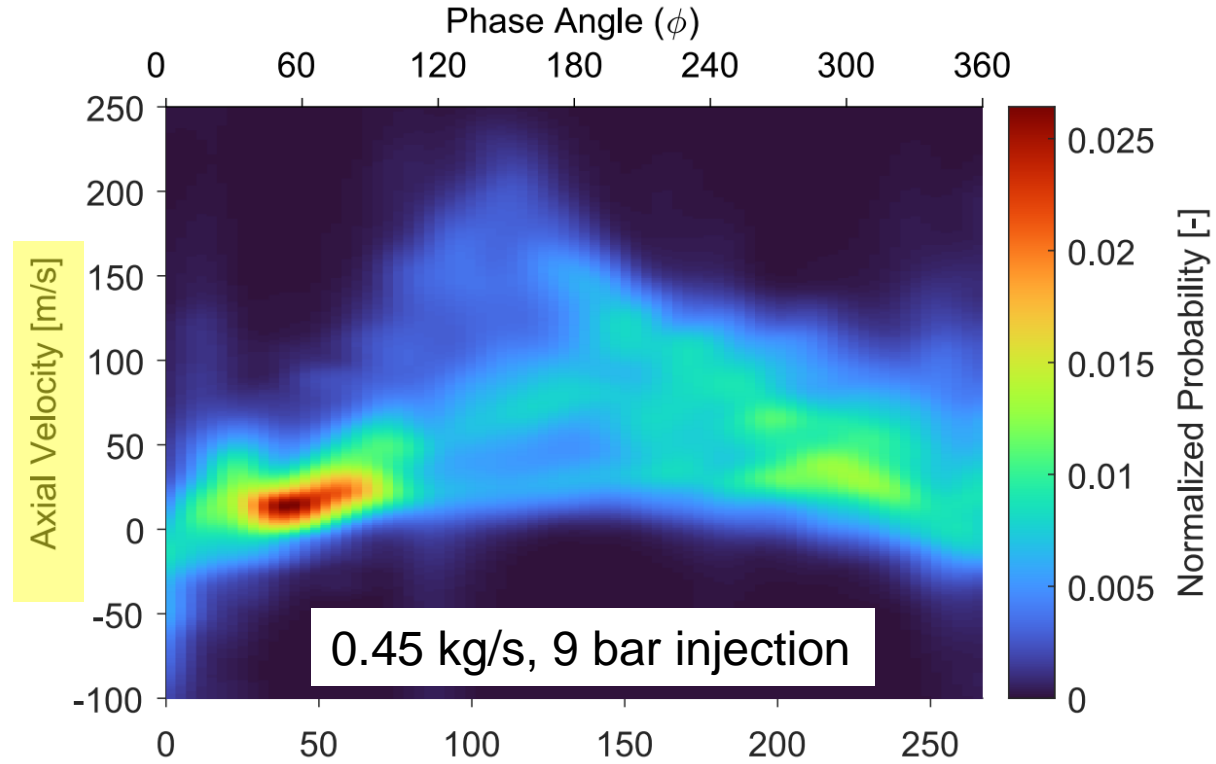
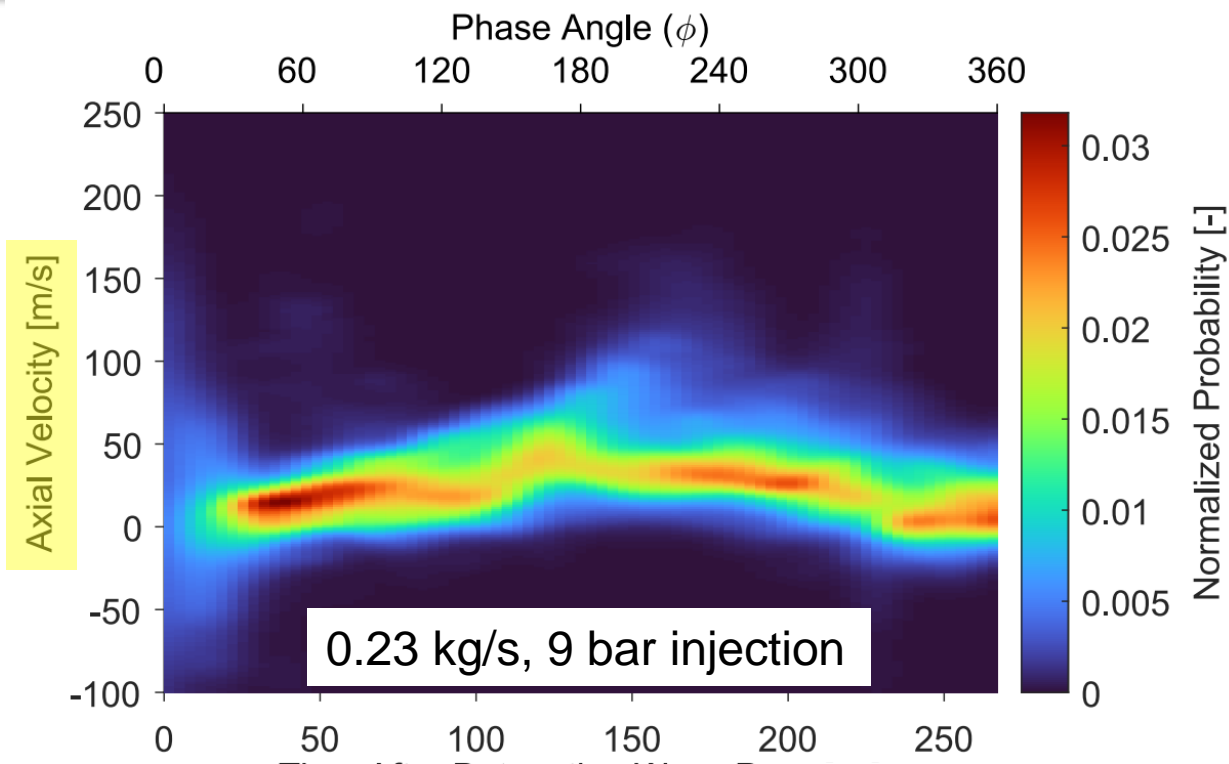


# Velocity Estimation

- Axial and azimuthal velocity components for the 0.23 kg/s, 9 bar injection case
- Optical flow suffers from noise so only 8 ms of the burst are used
- The first ~2 frames after the detonation wave pass typically have numerical instabilities
- The decrease in axial velocity is not a ‘deceleration’. Jet-A is leaving the field of view



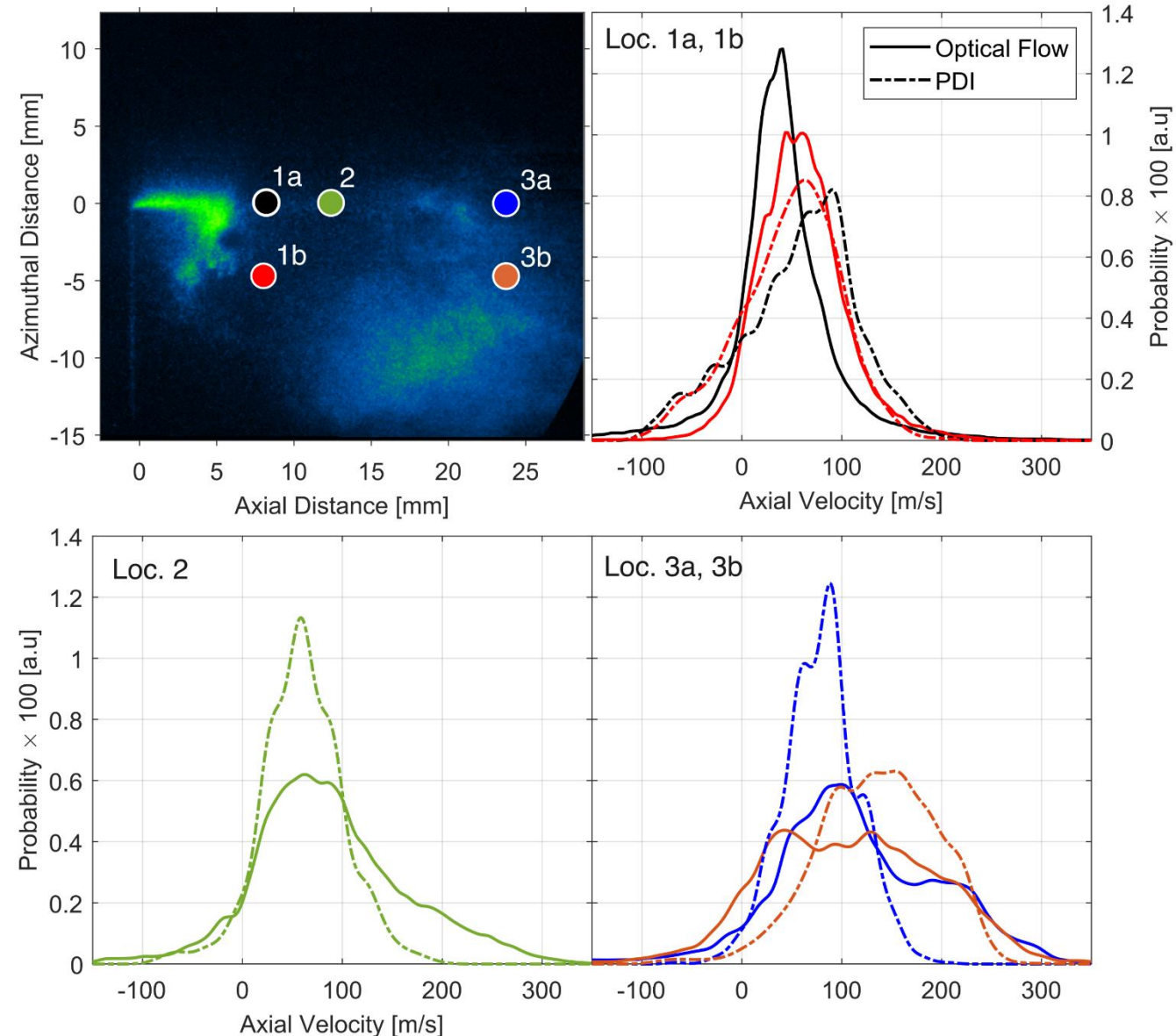
# Velocity Estimation



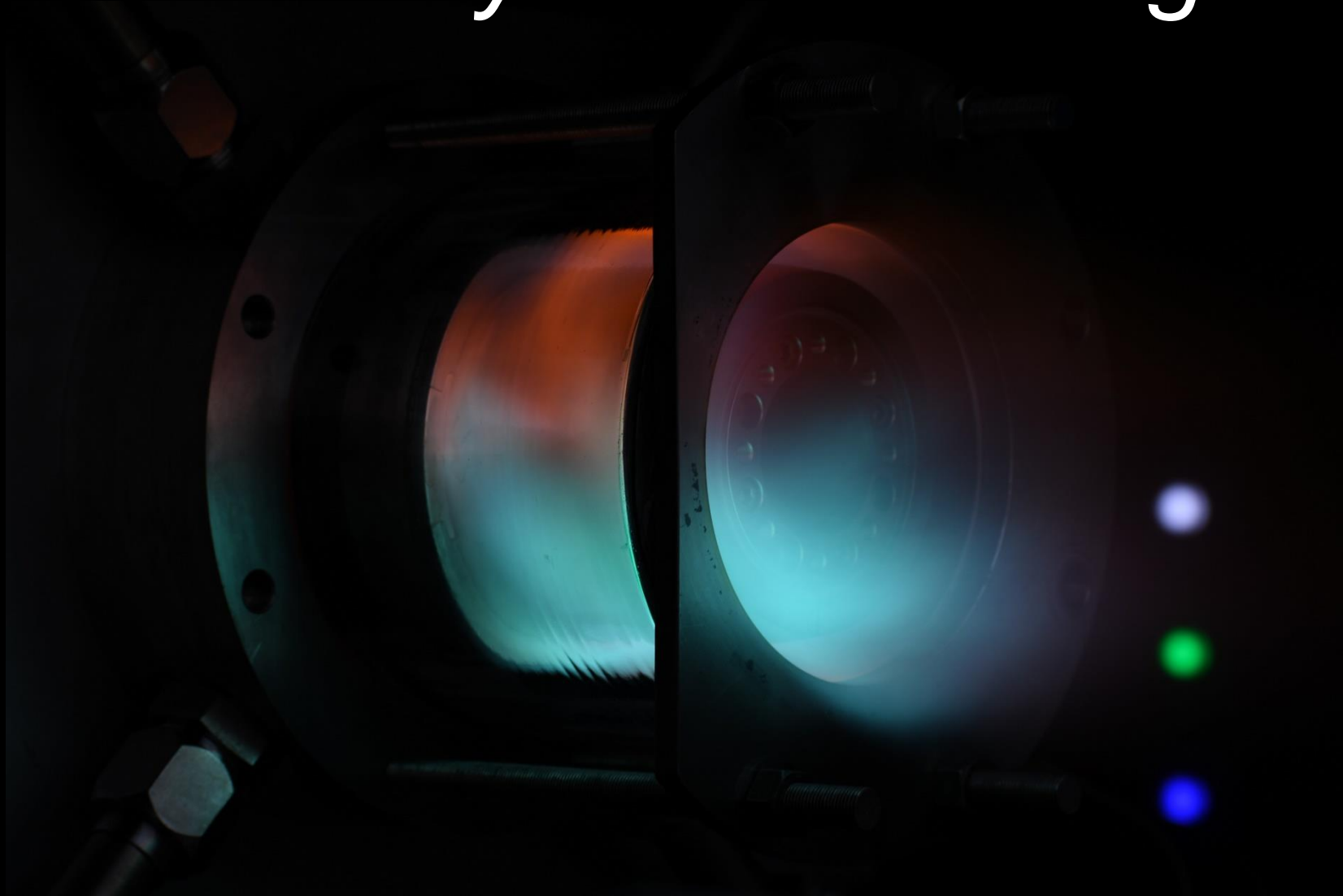
# Comparison of PDI and Optical Flow

- Previous optical flow sampling was performed over the entire image
  - Here, each PDI probe location is compared to optical flow in a  $1 \times 1$  mm box
- Good agreement at location 1a and 1b
  - 1a PDI is likely dominated by post-detonation advection. Late in the cycle, 1a sees the jet core which is too dense
- Other locations have similar median velocities
  - Location 2 and 3a has longer tails for optical flow. LIF is likely detecting some level of vapor, and this is pushing the velocity range higher.

0.23 kg/s, 9 bar injection pressure



*Thank you for listening*



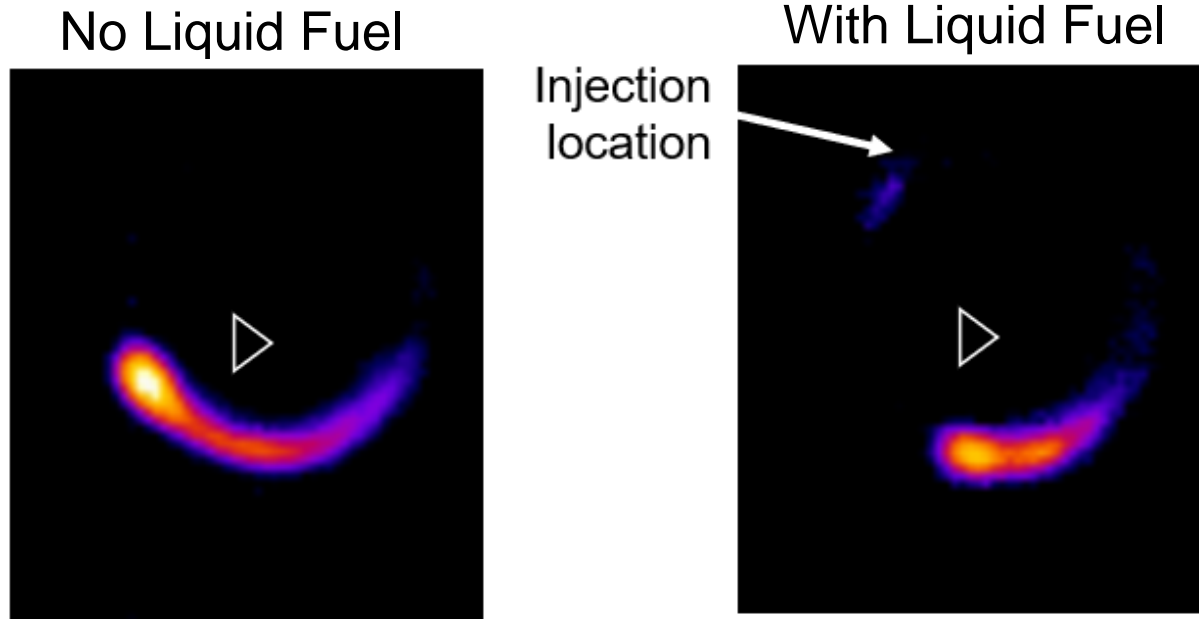
*Questions?*



*Supplementary Slides*

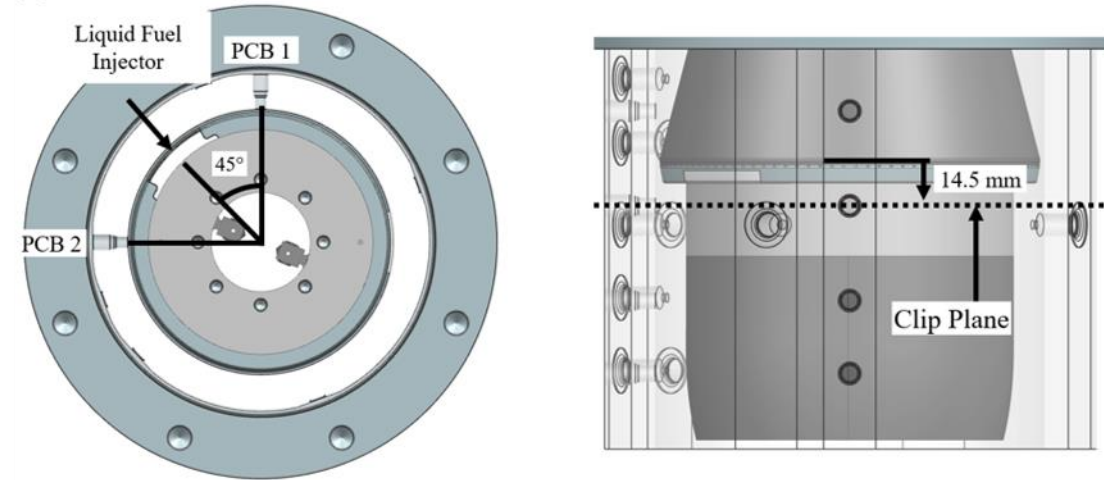
# Aft-End Image Comparison

- Needed to verify no significant detonation wave perturbation from diesel spray
- Identical chamber conditions ( $\dot{m}_{\text{air}}=0.46 \text{ kg/s}$ ,  $\Phi \sim 1$ )
- Corroborated with high frequency pressure measurements

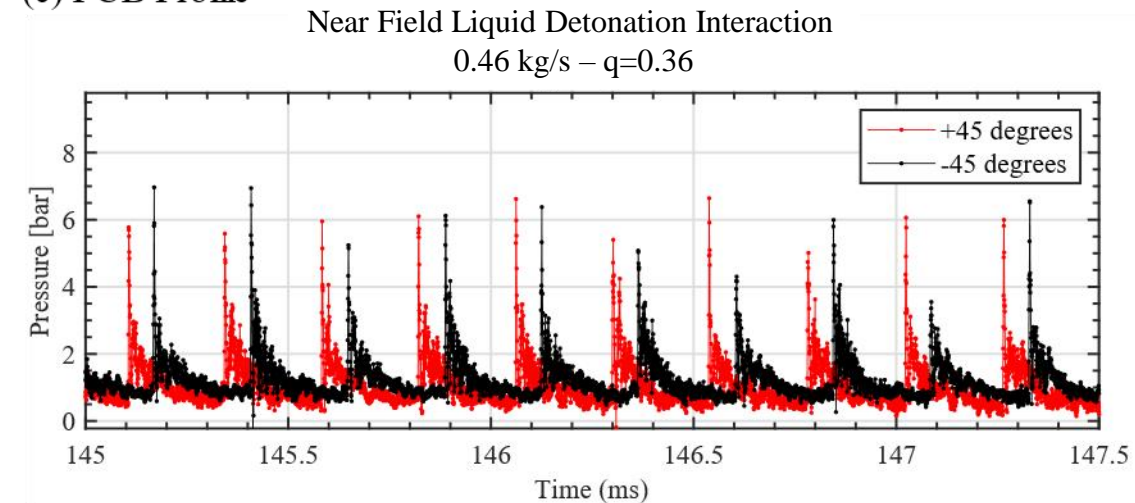


100 kHz Aft-End Chemiluminescence

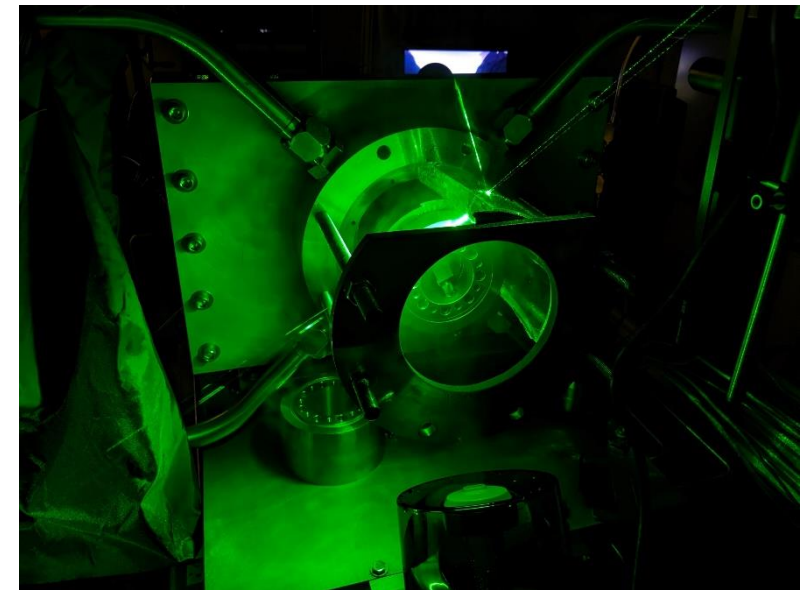
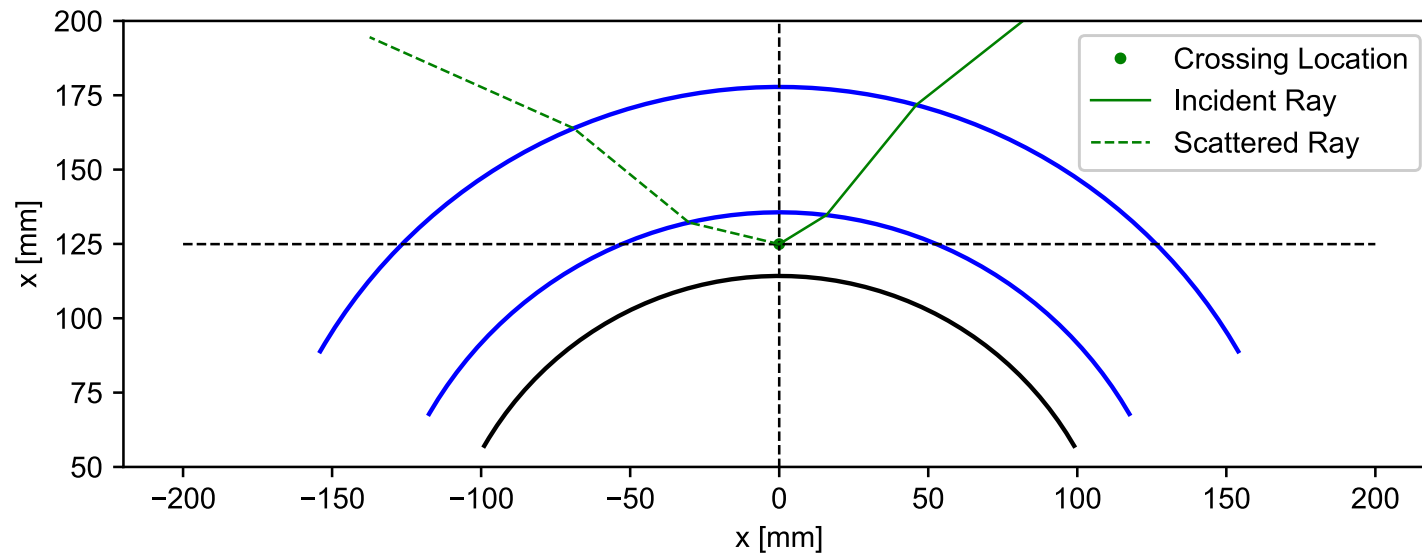
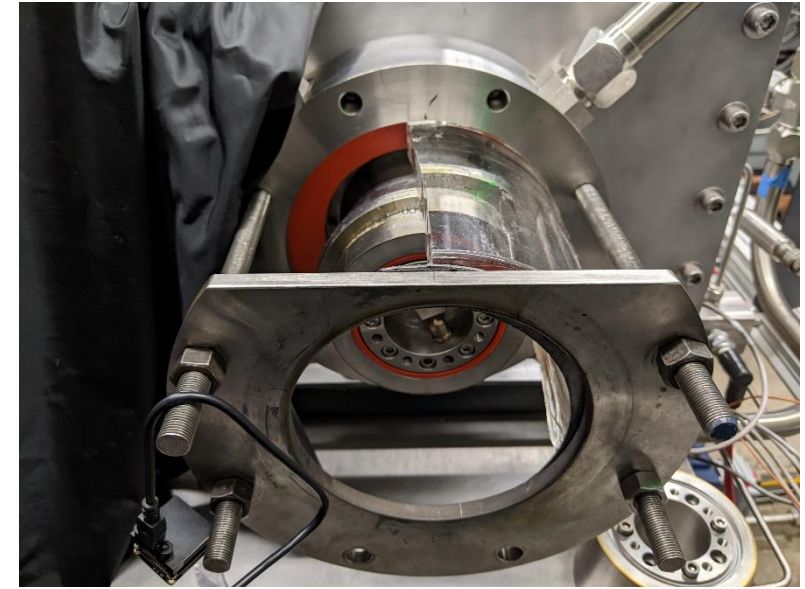
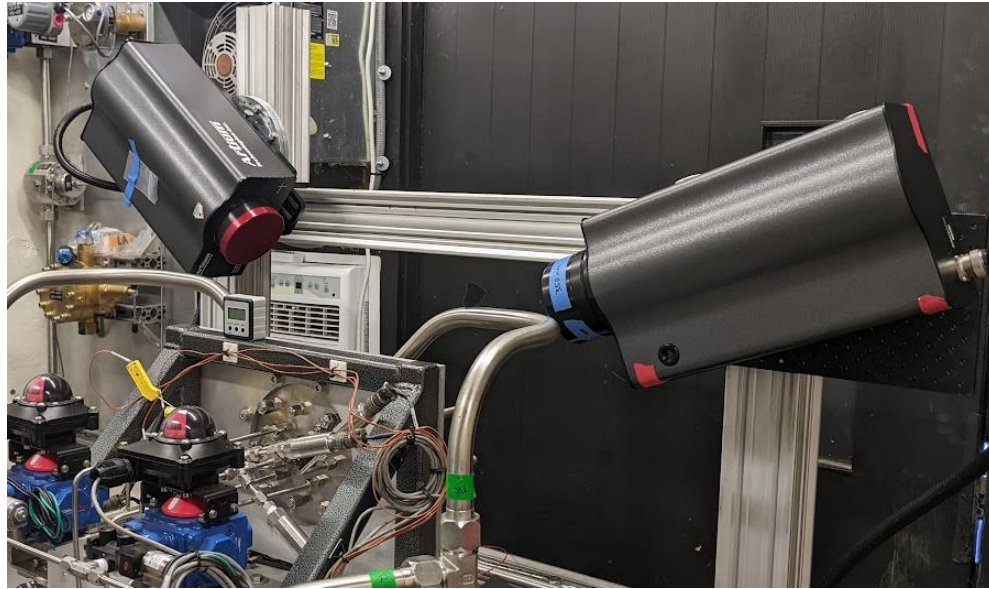
(b) PCB Arrangement



(c) PCB Profile

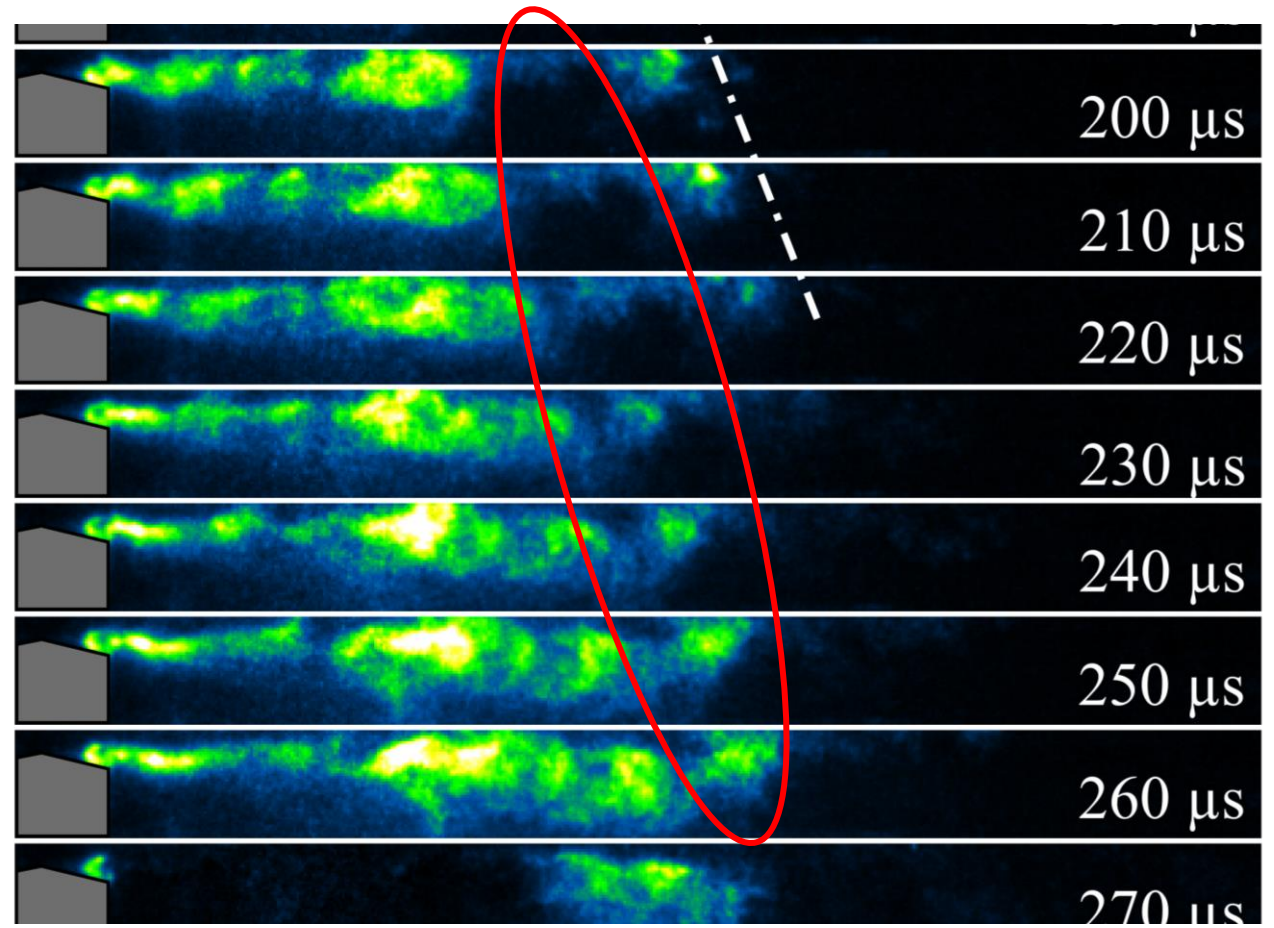
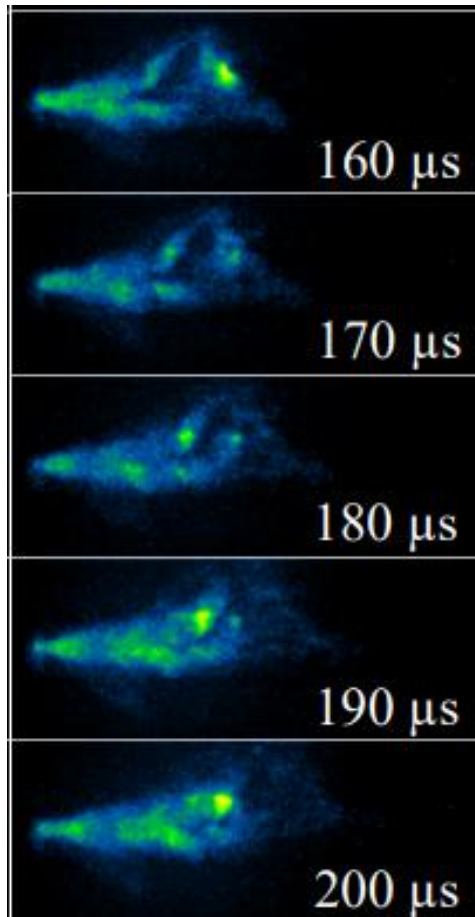


# PDA During Hot Fire



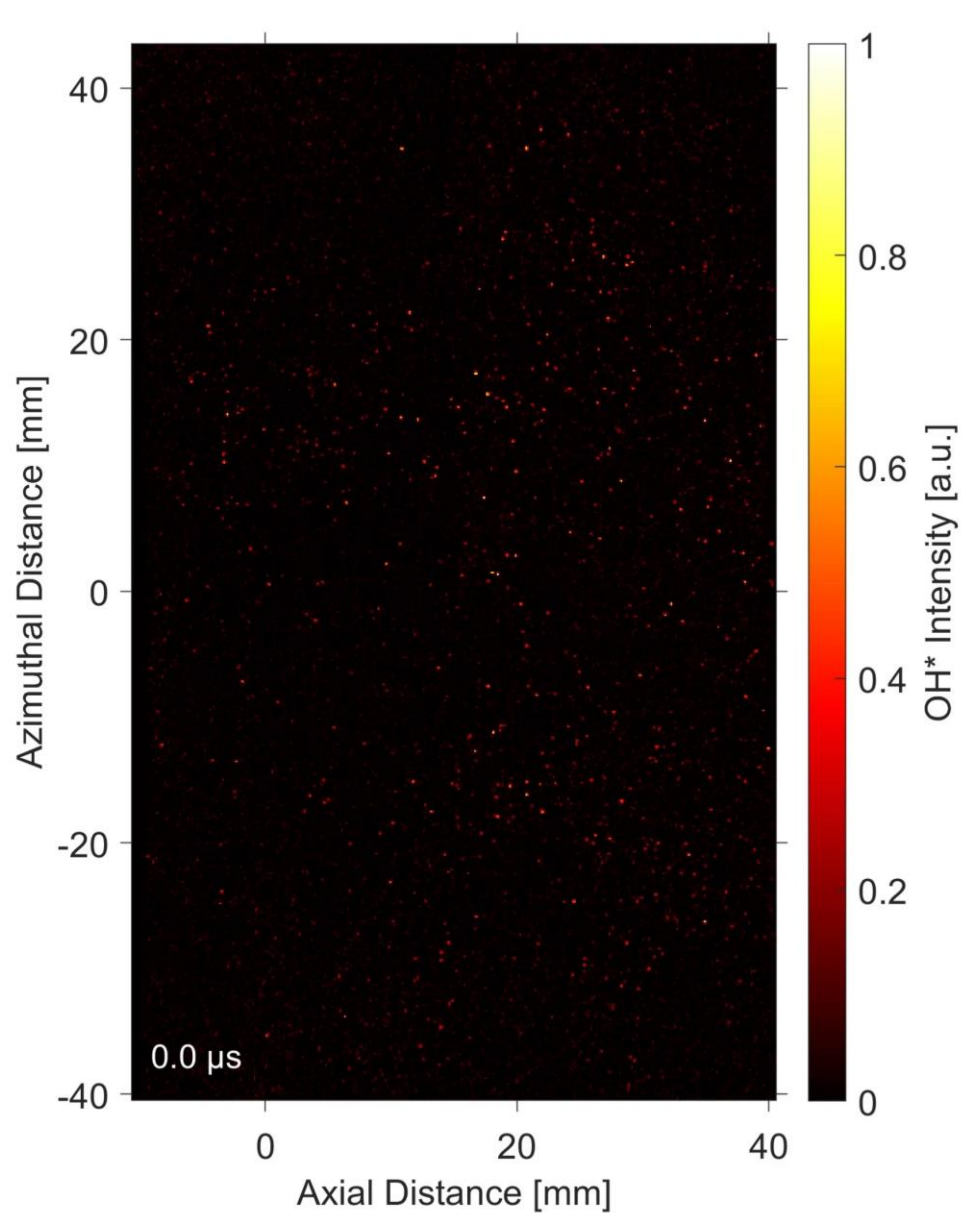
# Volume Illumination Scheme (VLIF)

- Dynamic evolution of fuel spray from the PLIF data set proven to be “out of plane” motion of flow structures
- Key insight into fuel spreading as it refills channel and how it spreads post detonation

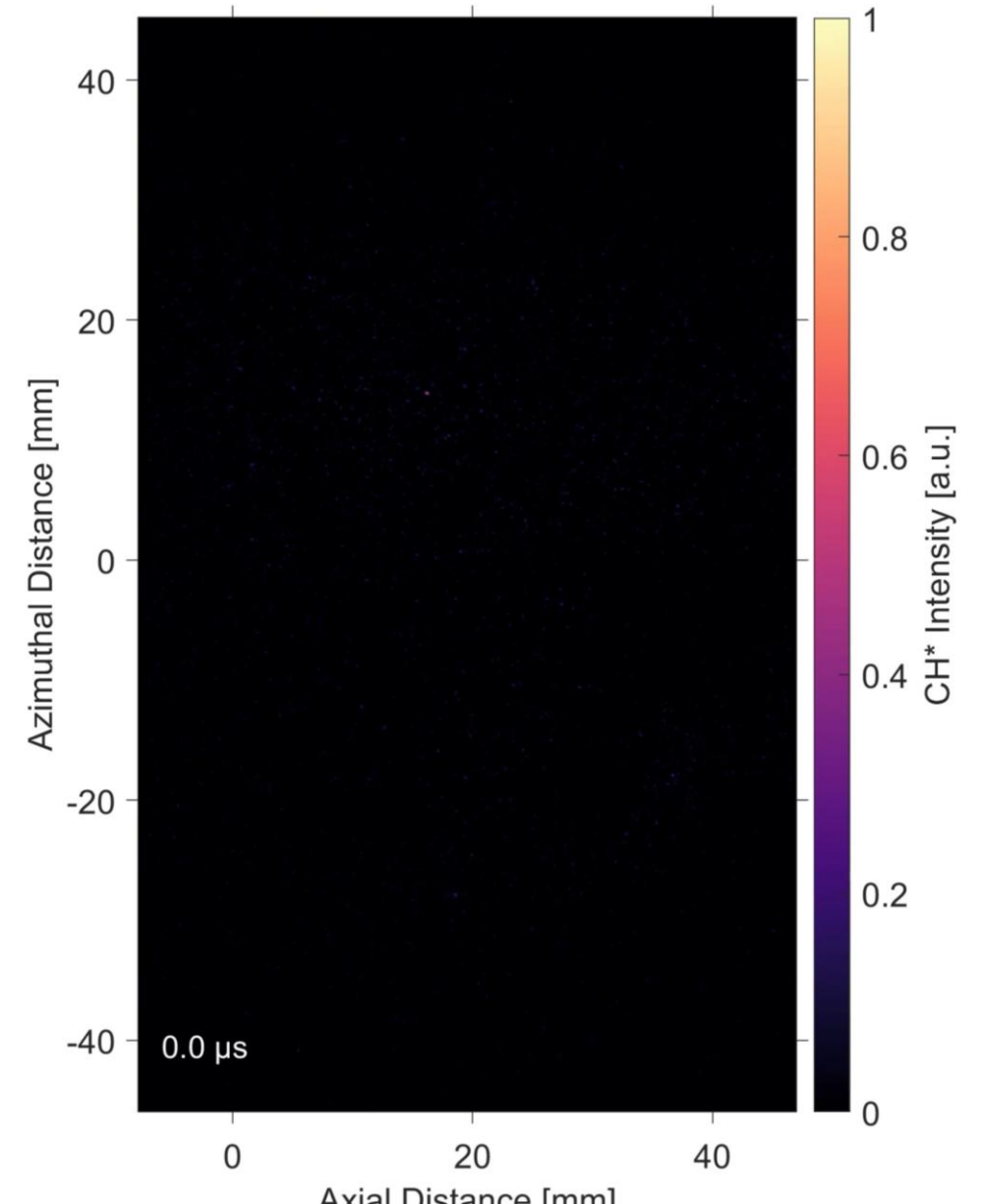


# Chemiluminescence Imaging

0.23 kg/s air with 9 bar injection pressure



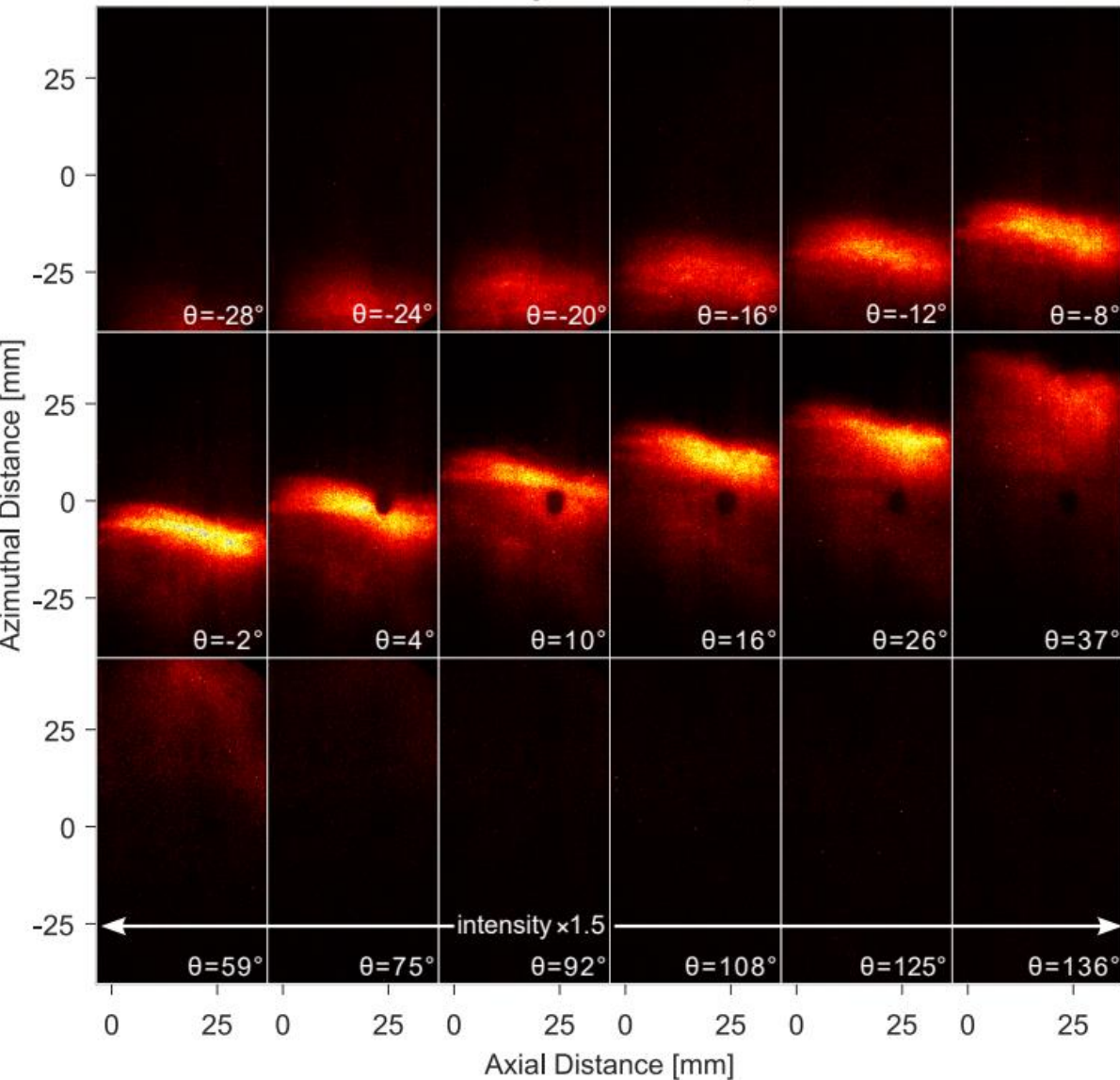
~120 μm/pixel



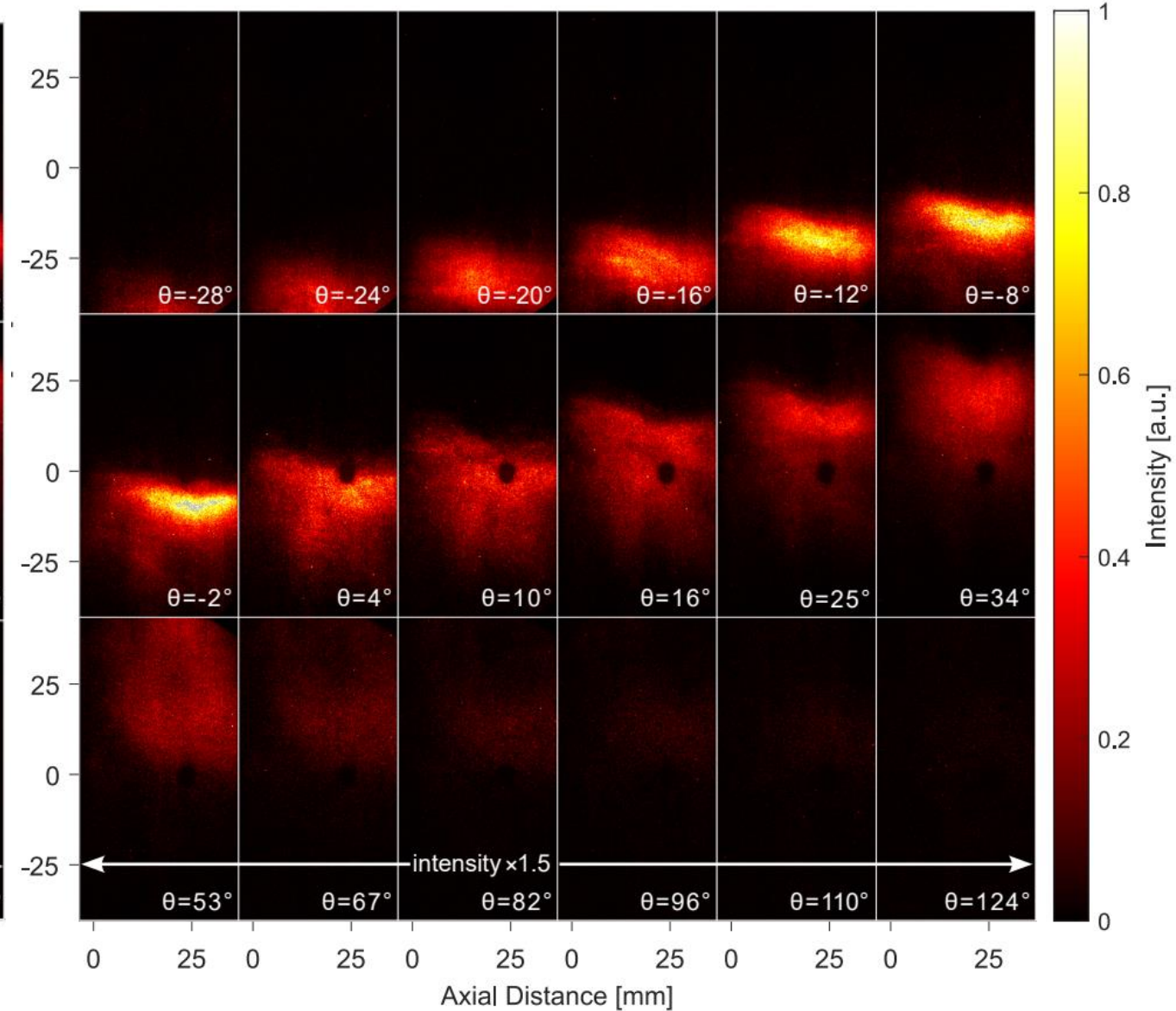
# Chemiluminescence Imaging

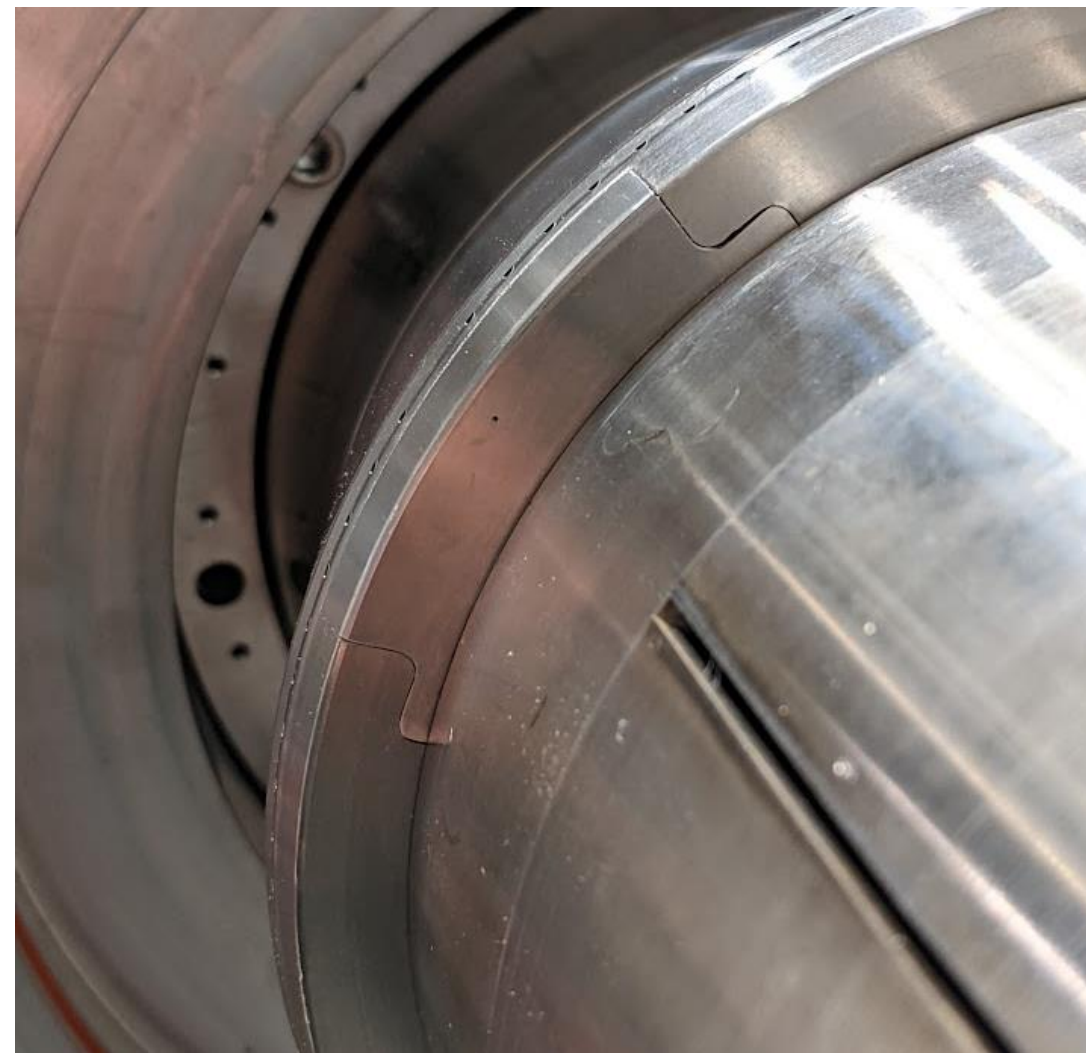
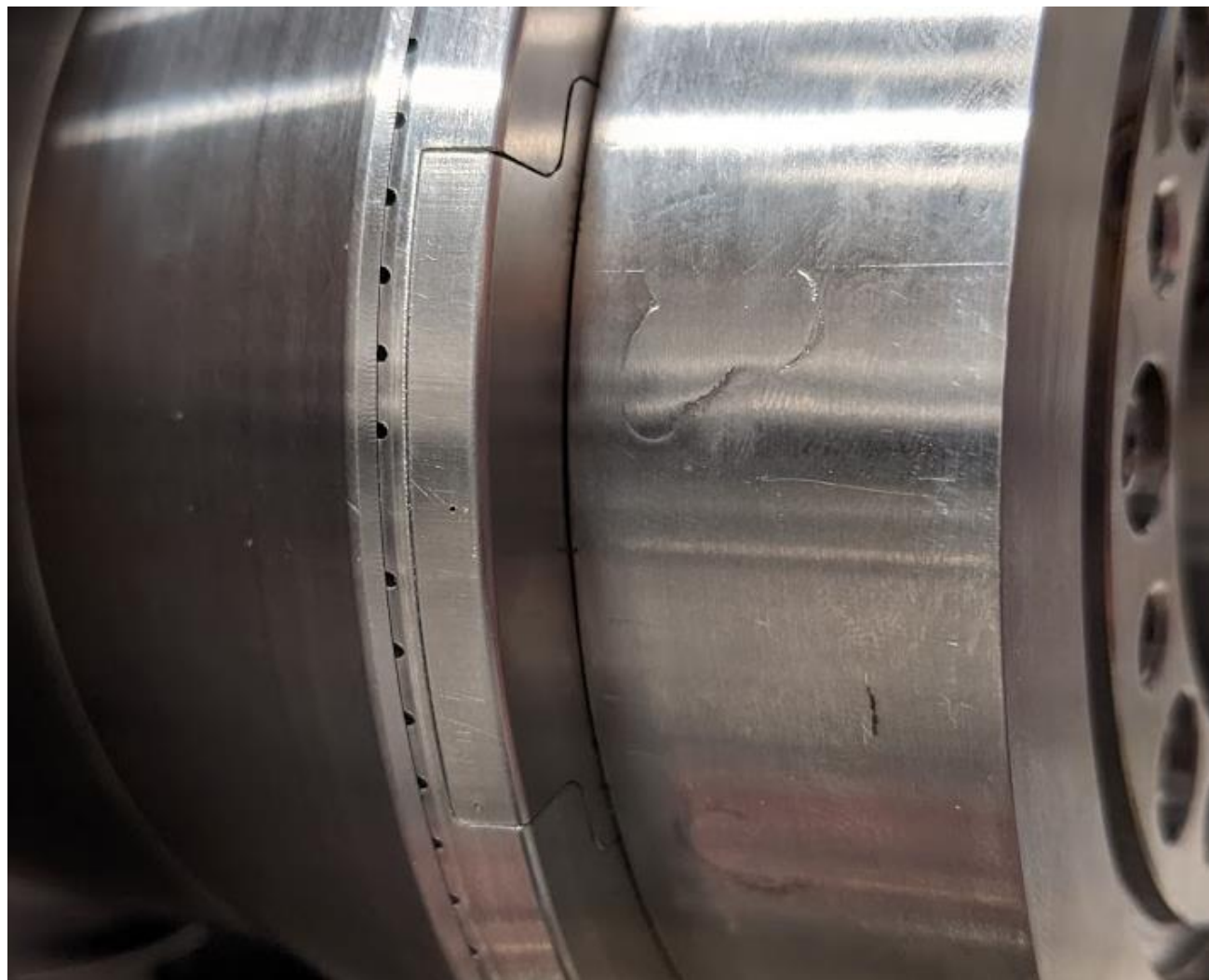


### No Liquid Fuel



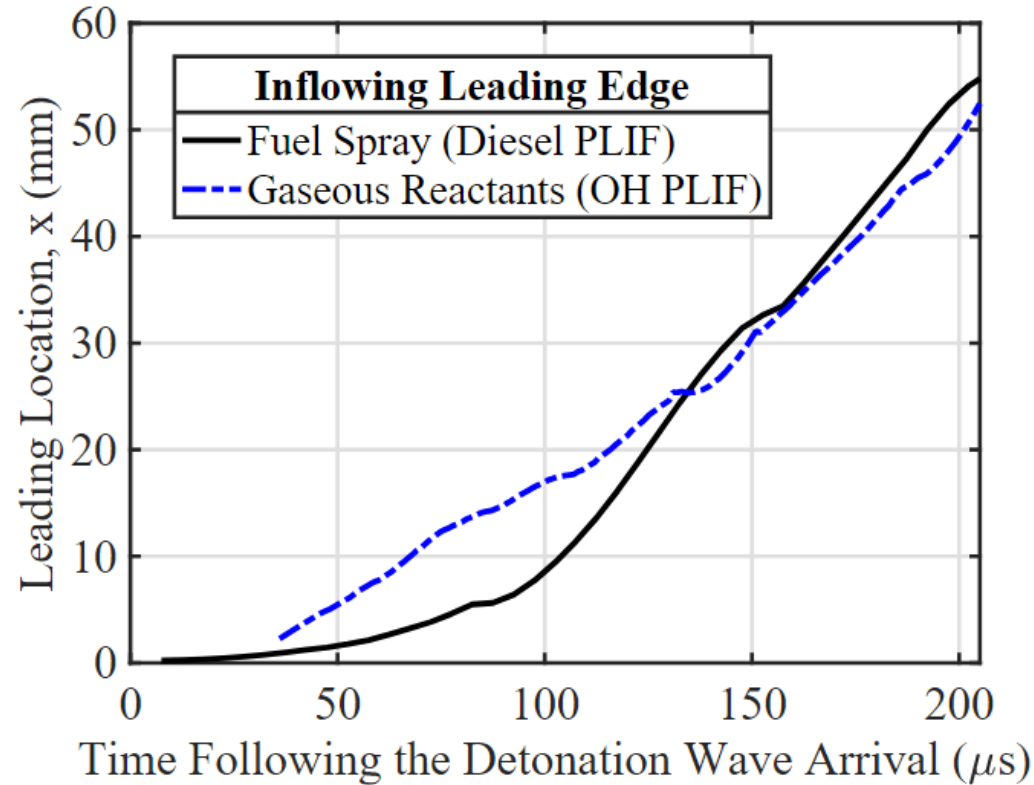
### With Liquid Fuel





# Refill of Liquid Fuel vs OH PLIF

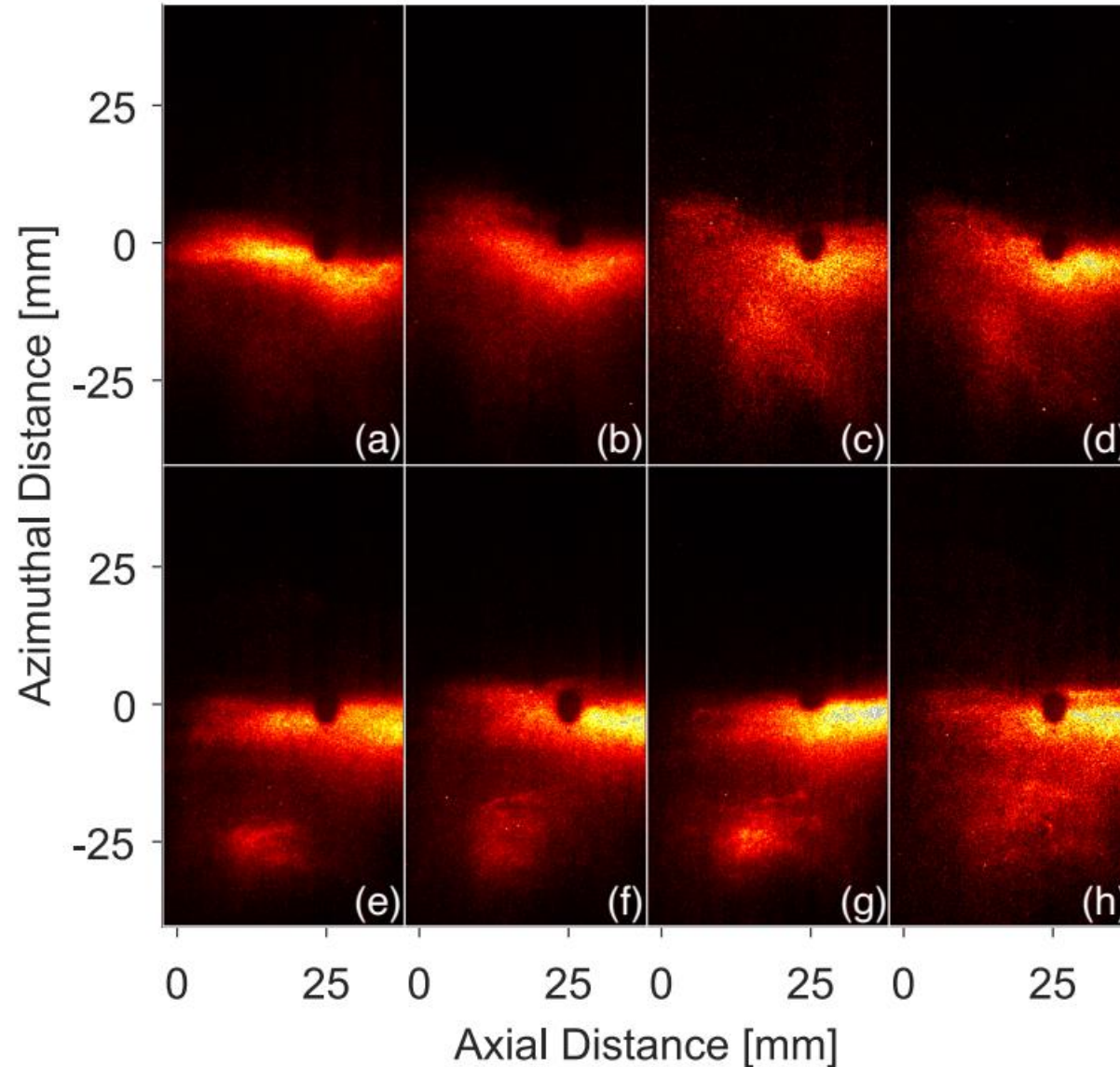
- A comparison between apparent leading edge (axial distance) of liquid fuel spray as it refills the channel and OH PLIF signal as fresh reactants enter the channel.



# OH\* For Different Conditions

Phase Angle  $\approx 0^\circ$

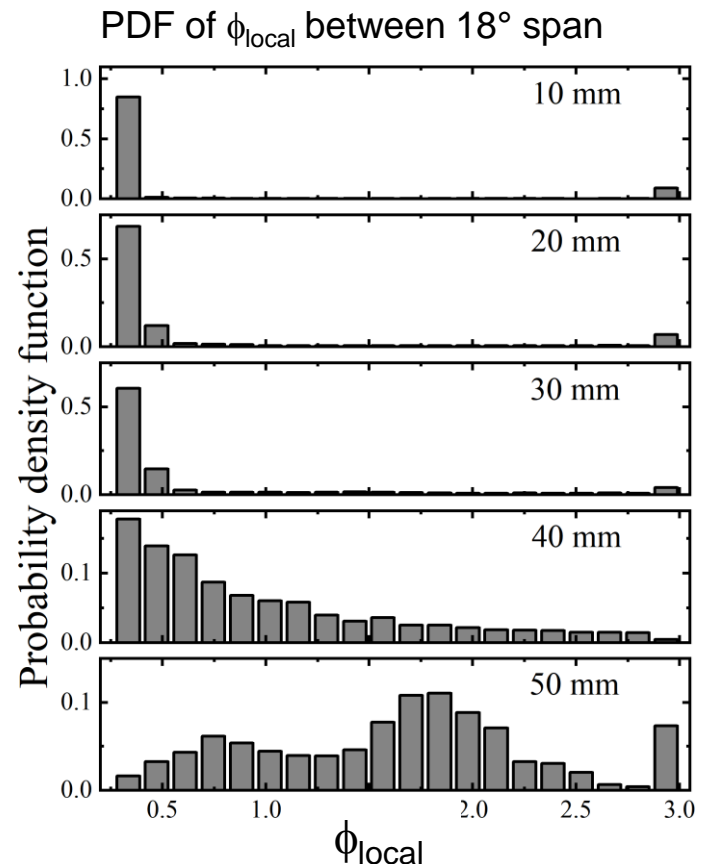
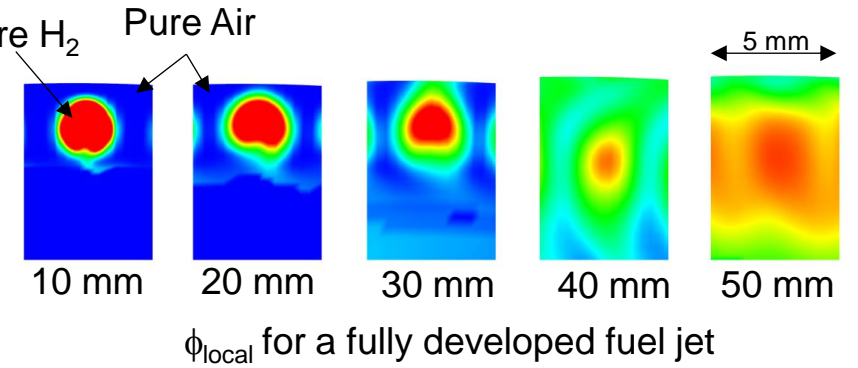
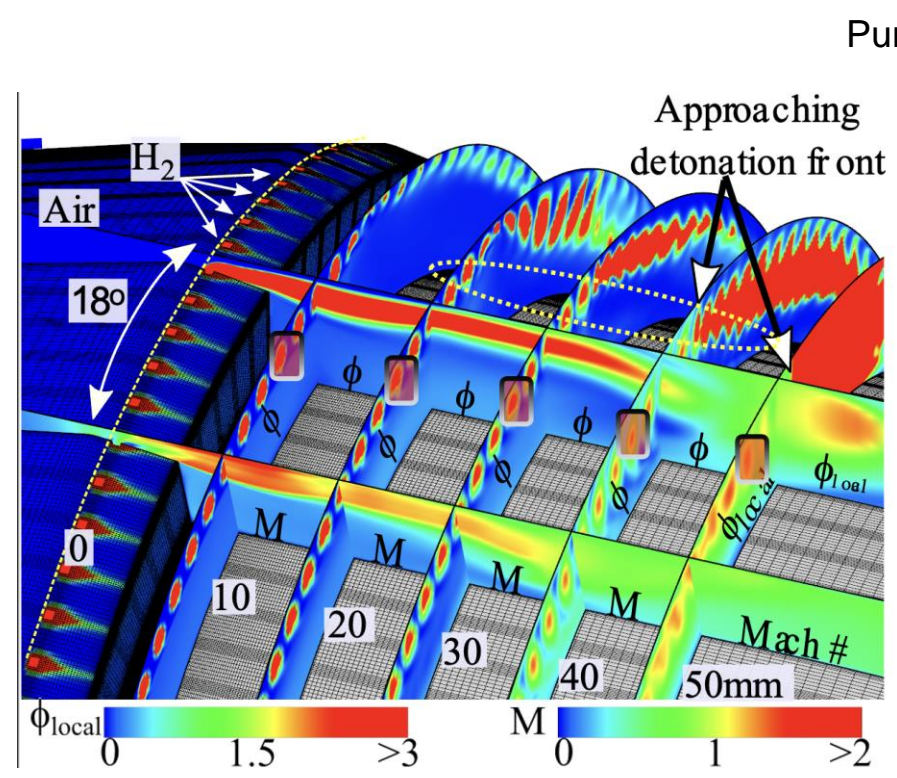
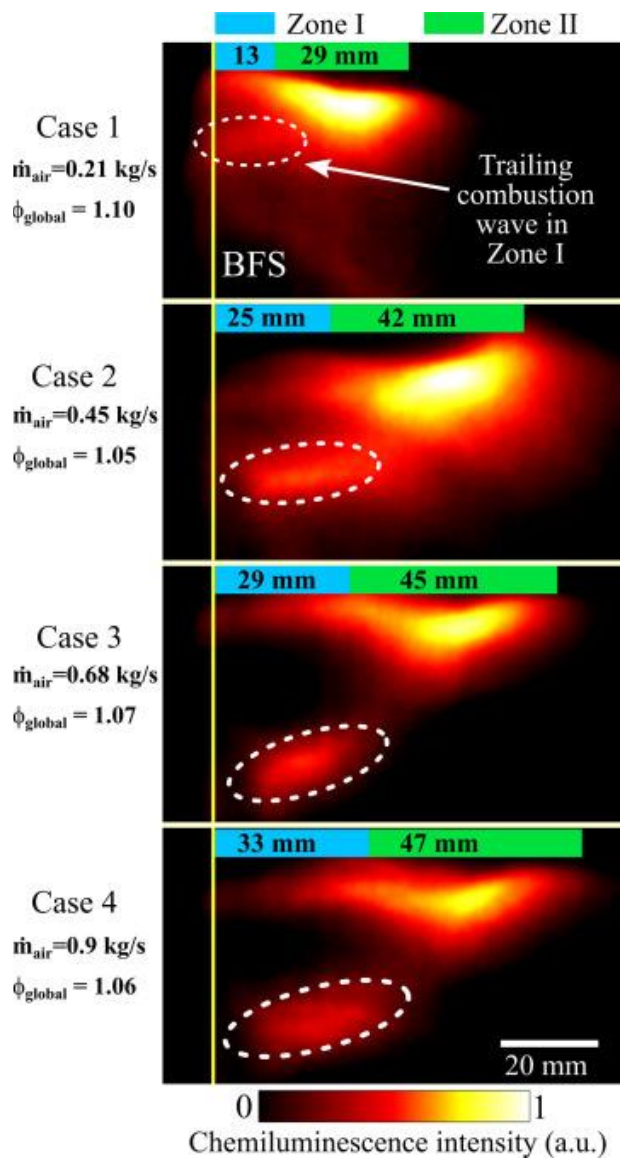
- (a) 0.5 lbm/s no liquid
- (b) 0.5 lbm/s, low P
- (c) 0.5 lbm/s, high P
- (d) 0.5 lbm/s, high P
  
- (e) 1.0 lbm/s, low P
- (f) 1.0 lbm/s, high P
- (g) 1.0 lbm/s, high P
- (h) 1.0 lbm/s, high P,  $\phi$  0.8



0.23 kg/s

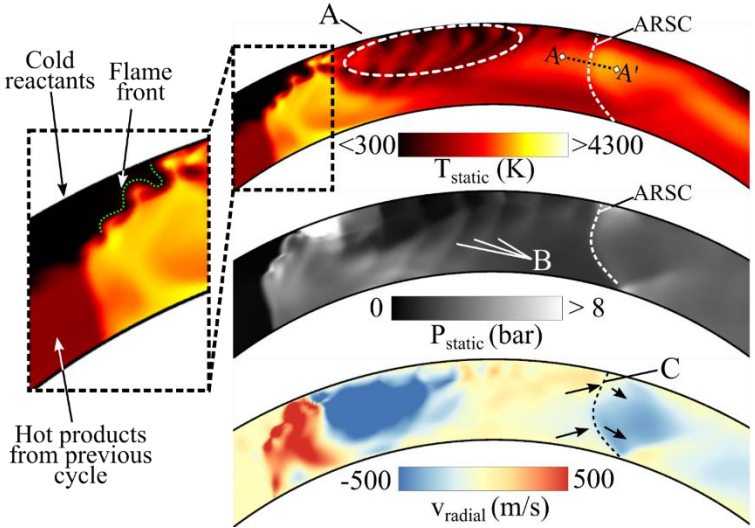
0.46 kg/s

# Numerical Simulations



Athmanathan et al., On the effects of reactant stratification and wall curvature in non-premixed rotating detonation combustors, Combs. Flame. (2022)

# OH PLIF Compared to URANS Simulation



Representative flow features in Zone I

