

# Establishing an In-Space Joining Ecosystem at NASA Marshall via Laser Beam Welding

Andrew O'Connor, Jonathan M Bonebrake, Thomas C Bryan, Zachary S Courtright, Charles T Cowen, Ellis R Crabtree, William C Evans, Emma K Jaynes, John C Ivester, Louise S Littles, Christopher S Protz, Benjamin L Rupp, Parker D Shake, Raju Subedi, Jeffrey W Sowards

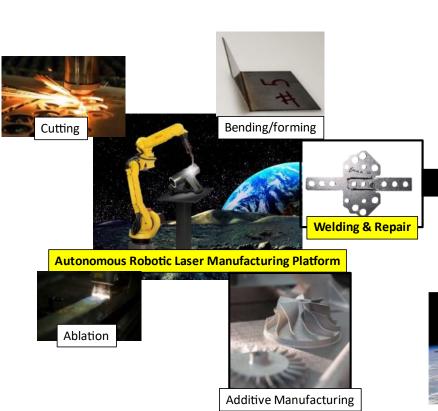
NASA Marshall Space Flight Center



# In-space welding enables space infrastructure



Method → ↓ Criteria	Fasteners/ rivets	In–Space Welding (ISW)
Joint strength & rigidity	•	0
Joint hermeticity	•	0
Joint mass	•	0
Joint design & manufacturing simplicity	•	0
Joint reliability	•	0
Repair versatility	•	0
Associated cost & upmass	•	0
● - Poor 👄 -	- Satisfactory	O - Good



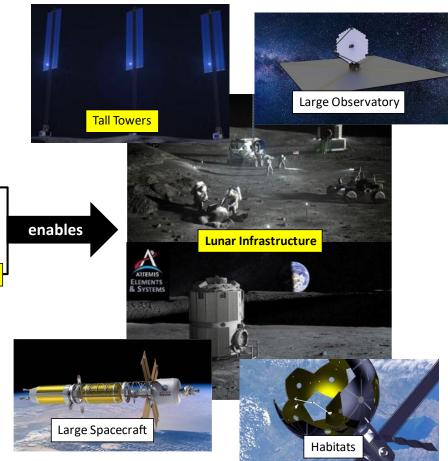
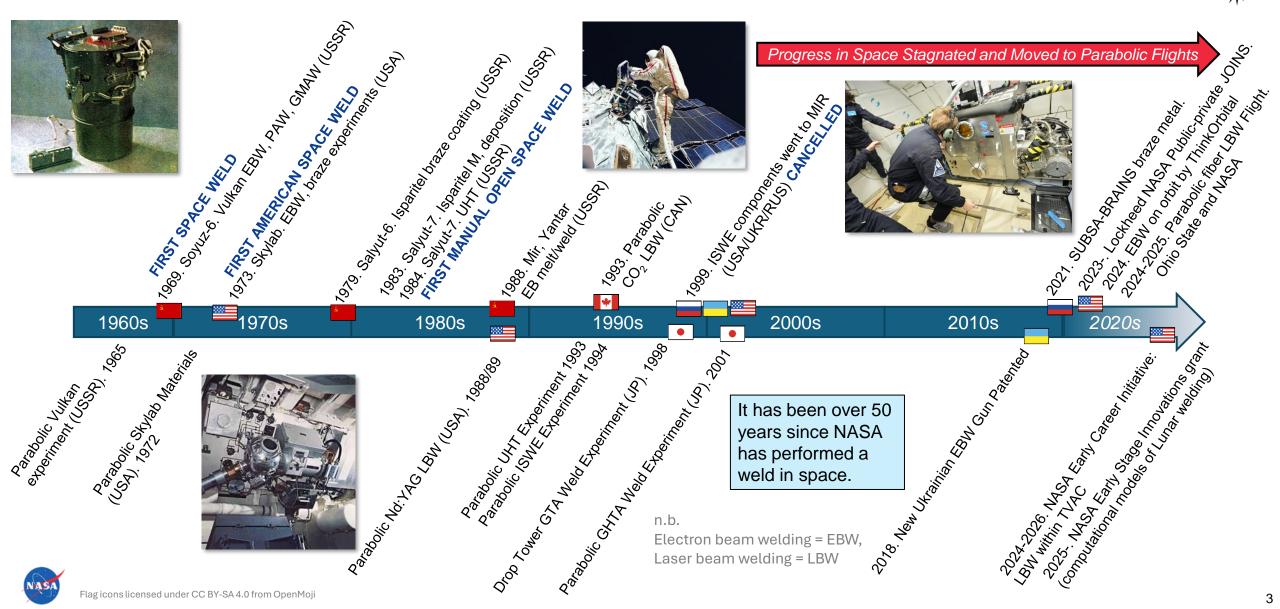


Image credit: ThinkOrbital, www.mechanicalcaveman.com



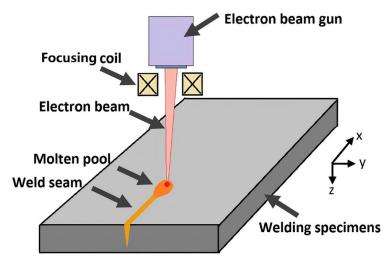
# Timeline of In-Space Welding and Joining



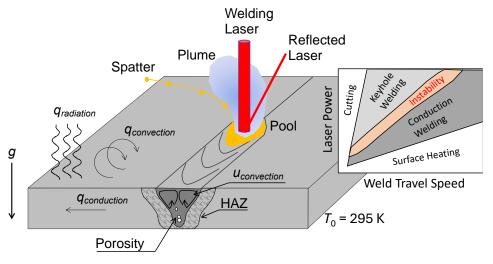


## Why laser beam welding in space?





Licensed under CC BY from Yin et al., 2023, doi: 10.1007/s00170-022-10682-6.



High-energy Beam Process →  ↓ Criteria	Electron	Laser	Status
IVA flexibility (e.g. in habitat) & EVA			
flexibility (e.g. in vacuum, Lunar	•	0	
surface, on Mars)			
Workpiece variety (e.g. geometry,		0	Capability
material)			available after
Suitable for operation on end effector			planned
of robotic arm (e.g. EMI, mass, power	•	0	development
delivery, heat rejection)			
Compatible with inspection tools &			
able to repair welds			
Power requirements & energy	$\cap$		Commercial
efficiency			lasers
Suitable for additive manufacturing	<b>-</b>	0	
Perform subtractive manufacturing –			Future work
cutting, drilling, etc.			(GCD, etc.)
Capable of bending/forming structures	•	0	
● - Poor ← - Satisfa	ctory	O - Goo	d



## In-space effects that influence welding



Variable	Case 1: In Space	Case 2: Chamber Inside Space Habitat	Case 3: Inside Space Habitat	Case 4: Lunar Surface	Case 5: Martian Surface	Baseline: Earth	Capabilities Needed at Present
Gravity	μg	μg	μg	0.17 g	0.38 g	1 g	µg to 0.38 g
Atmosphere	Vacuum (10 <sup>-19</sup> Pa)	Vacuum (10 <sup>-4</sup> Pa)	>21% O <sub>2</sub> , <101 kPa	Vacuum (10 <sup>-9</sup> Pa) or habitat	$95CO_2$ -2.6N <sub>2</sub> - 1.9Ar-0.2O <sub>2</sub> - 0.06CO (0.6 kPa) or habitat	78N <sub>2</sub> -21O <sub>2</sub> - 0.9Ar- 0.1other, 101 kPa	HV (10 <sup>-1</sup> Pa) UHV (10 <sup>-5</sup> Pa) XUHV (10 <sup>-9</sup> Pa)
Temperature	Extremely low ISS Exterior: 120 K – 395 K	~ 293 K	~ 293 K	40 K – 400 K	133 K – 300 K	~ 293 K	40 K – 400 K
Space Suit	Yes	No	No	Yes	Yes	No	

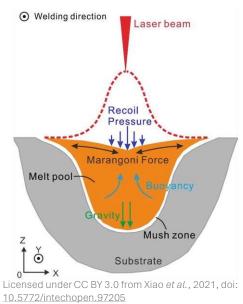
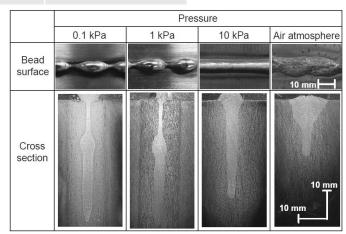


Table adapted and expanded from original source: Masubuchi, 1990, doi: 10.2207/qijws1943.59.421

Reduced gravity is unique among the above effects in that it cannot be reproduced for prolonged periods on earth.

**Current Work**: Integrate existing capabilities across academia, government, and industry to investigate space environmental effects on welding processes to inform computational models, and to create public-private partnerships to develop and implement space welding technologies.



Licensed under CC BY-NC-ND 3.0 from Katayama et al., 2011, doi: 10.1016/j.phpro.2011.03.010.



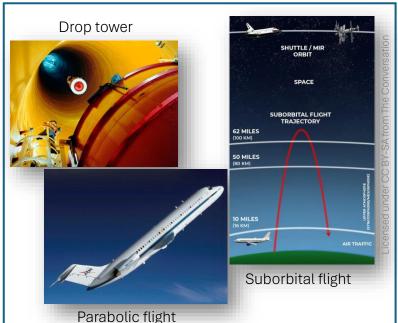
## Simulating space conditions for welding

Low Earth Orbit (LEO)

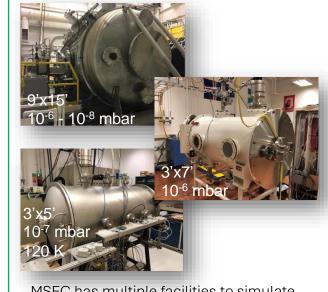


Experimental platform →  ↓ Criteria	Drop tower	Parabolic flight	Suborbital flight
Length of microgravity [s]	<5	20-25	>180
Gravity (quality) [g]	10 <sup>-5</sup>	10 <sup>-3</sup> -10 <sup>-2</sup> (up to 2.0)	10 <sup>-4</sup>
Mass allowed [kg]	10 <sup>2</sup>	10 <sup>2</sup>	10 <sup>1</sup>
Cost [\$]	\$	\$\$	\$\$\$

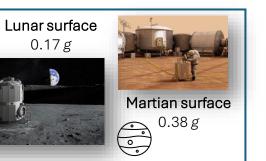
#### **Microgravity / Reduced Gravity**

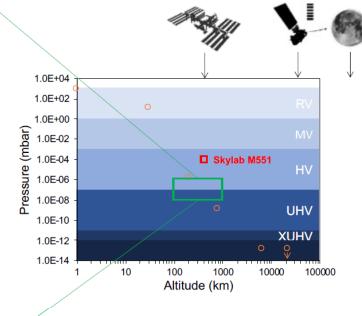


#### **Vacuum and Reduced Temperature**



MSFC has multiple facilities to simulate vacuum and reduced pressure, including variable atmospheric composition





Numerous experiments with welding systems in vacuum chambers on parabolic flights



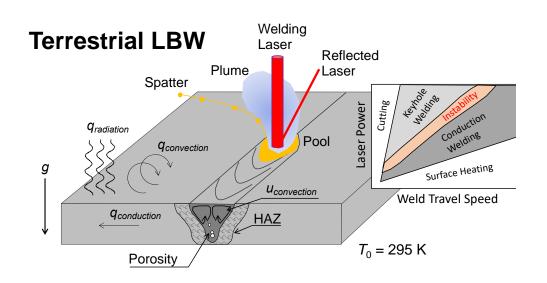


Mladenov, Koleva, and Trushnikov, *E+E*, 2019.

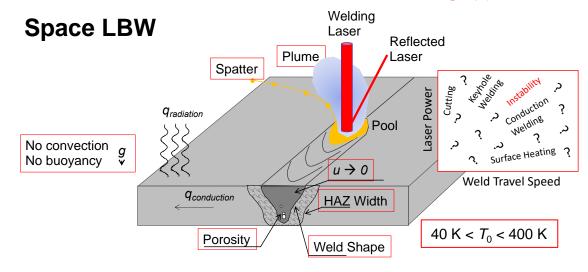


## **Key effects to consider for in-space LBW**





Red boxes indicate instrumentation and modeling opportunities.



**Issue #1** Weld heat transport has profound effect on size of a weld and its metallurgical transformations and hence weld properties:

Temperature gradient and cooling rate are proportional to thermal conductivity and  $T_0^2$ 

Issue #2 Reduced gravity reduces buoyancy-induced convection:

Development of weld pool shape and porosity evolution are altered, and chemical effects become dominant, e.g., surface-active elements influence weld penetration due to thermocapillary flow. (minute alloy chemistry changes are important)

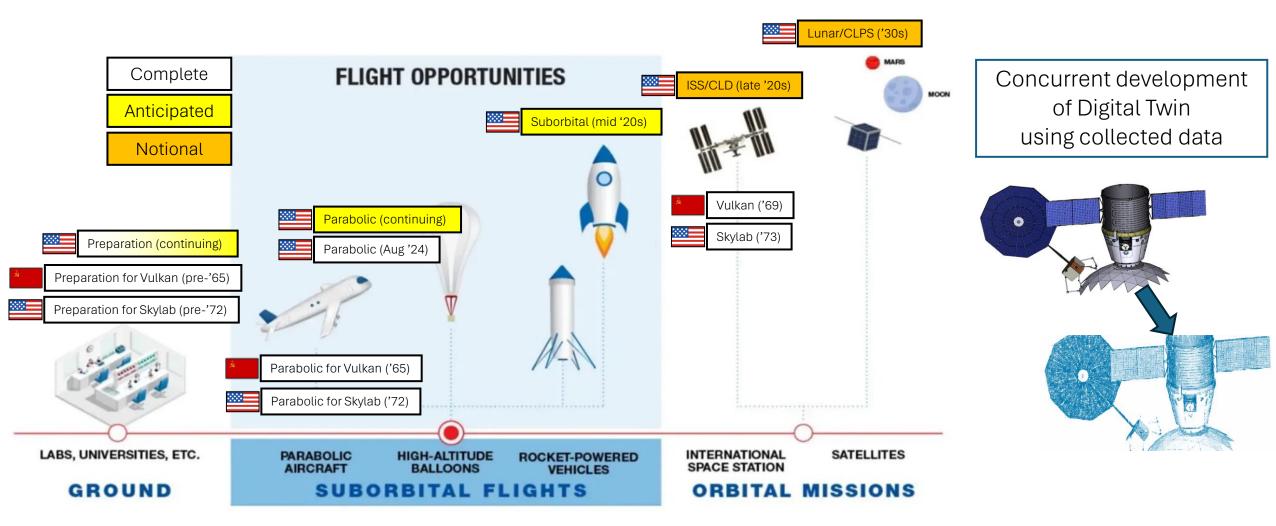
Issue #3 Reduced pressure/vacuum in space:

Heat transport is dominated by radiation and conduction rather than by convection. Weld shape and width, and weld strength will be influenced by change in weld cooling.

Reduced pressure influences laser beam keyhole stability, evaporation of volatile species, safety issues, etc.

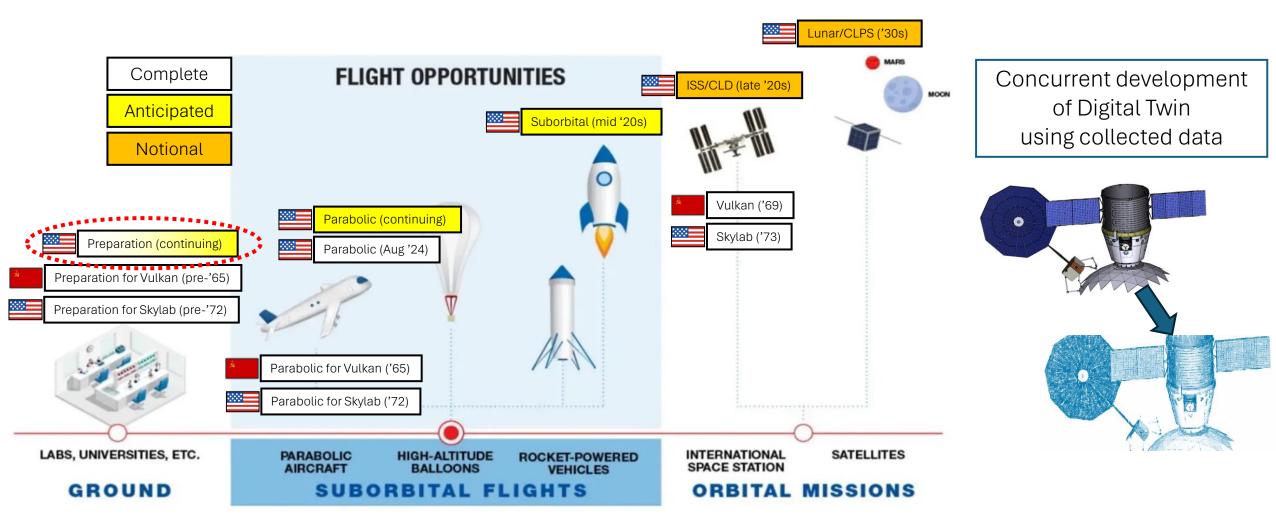












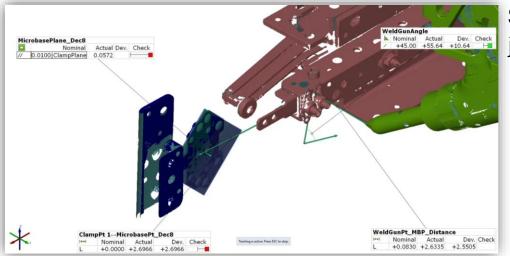


# Ground testing LBW on 3-DOF "Flat Floor"



Enclosed LBW station for rapid parameter development



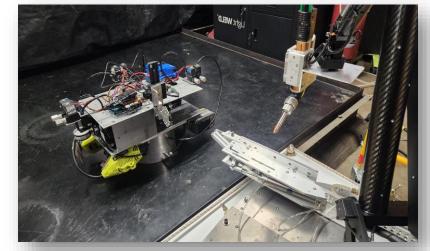


Structured light scan of joint fit-up on Flat Floor

Half of joint on mobile base, other half on floating robotic arm;
LBW from side;
in situ videography and thermography

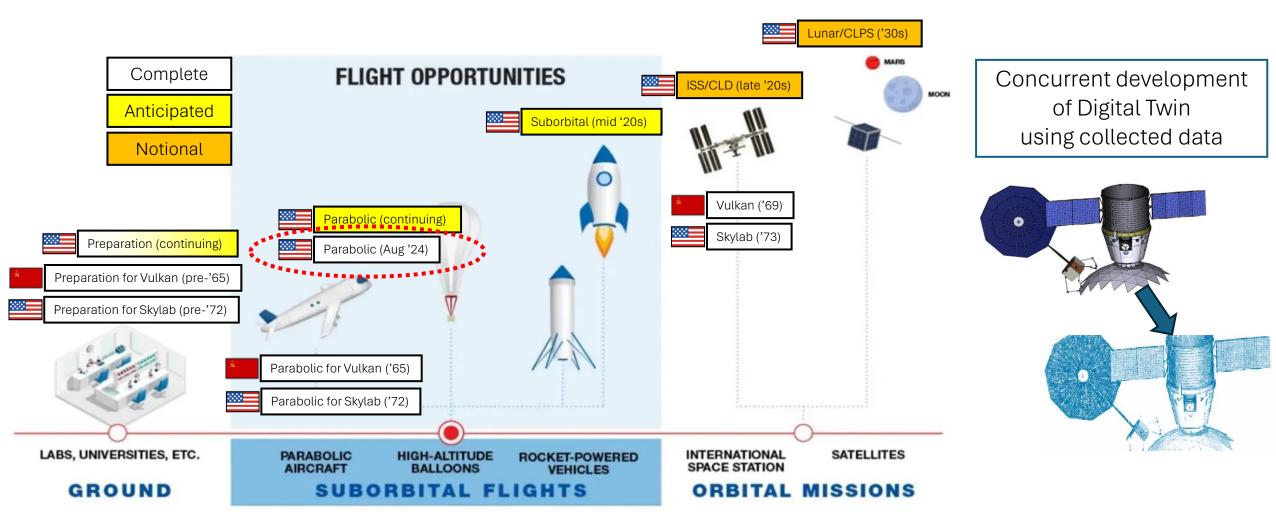
Ongoing:

Glovebox capable of variable composition atmosphere and with regolith simulant (Lunar, Martian, etc.) via handheld LBW











## Collaboration with the Ohio State University on parabolic flight



### Integration and Ground Demonstration of Self-contained Laser Welding System for Parabolic Microgravity Experiments.

- OSU. Profs: Ramirez, Panton, Horack, Nassiri, Williams, Nate Ames, Bob Rhoads. Undergrad capstone team. Grad students: Eugene Choi, Aaron Brimmer, Will McAuley.
- NASA. Jeff Sowards, Karen Taminger (LaRC), Will Evans, Zach Courtright, Louise Littles, Andrew O'Connor, Emma Jaynes, Ben Rupp, Tom Bryan.

Heritage parabolic vacuum chamber from NASA/LaRC



Generate Model Calibration Data



OSU-NASA CAN



**Materials** 

Integrated Computational Materials
Engineering (ICME)

Laser Beam Welding



Modern high-power fiber lasers enable LBW for space; Welding times within microgravity parabola length (15-20 seconds) Leverage LBW expertise and workforce development at OSU



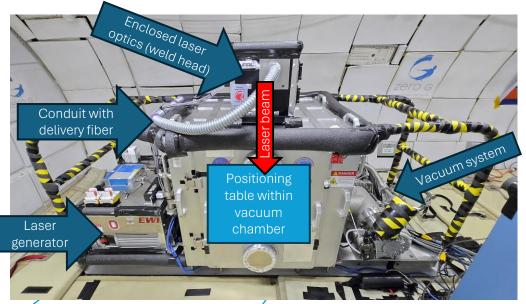


Retrofitted vacuum chamber in flight on Zero-G 727 aircraft

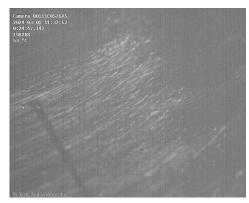


## Post-flight data analysis ongoing and preparing for re-flight









in situ thermal data and videography

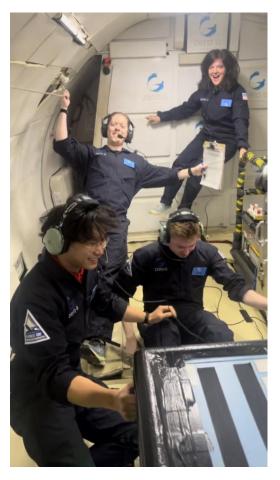
Successfully welded during 69 out of 70 total parabolas – including both Lunar and microgravity profiles

Characterization in progress:

- X-ray radiography, micro-CT scans
- Metallography and hardness testing

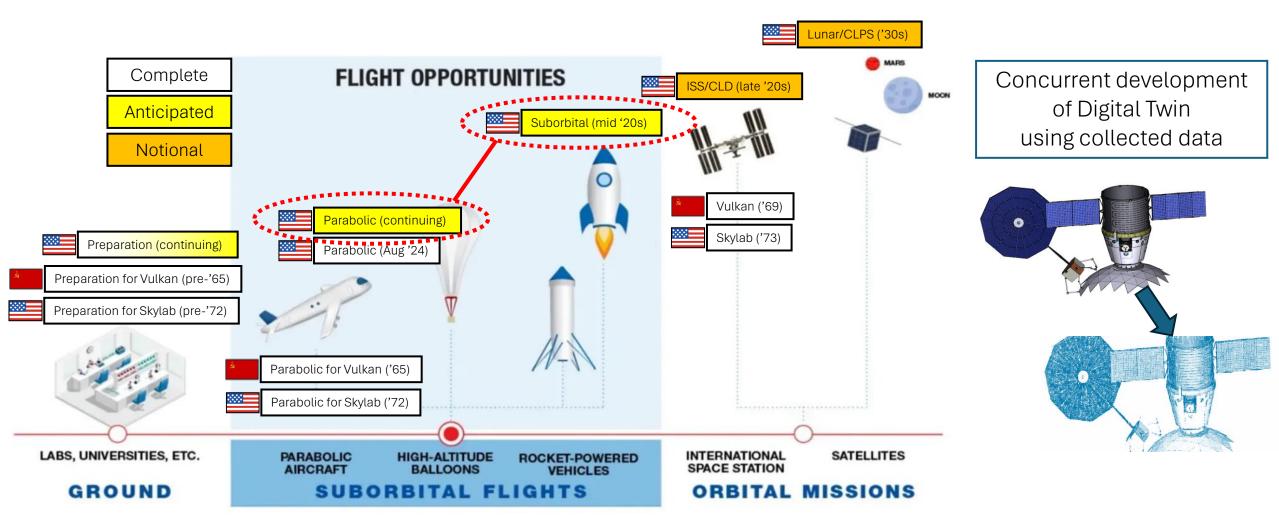
Upcoming flight tentatively scheduled for May 2025:

- Hermetic welds (pressure vessels, etc.) and realistic joints (lap, butt-lap, etc.)
- Continuous melt pools established and maintained through gravity transitions
  - Reduced order alloys (e.g. Al-Cu for Al 2219) to ease computational modeling











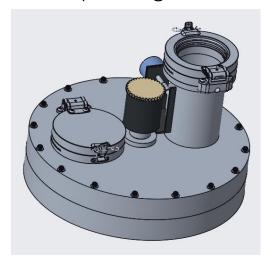
#### **Evolve from parabolic to suborbital flight experiments**

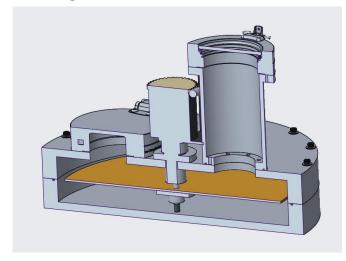


Parabolic	Suborbital
Tens of seconds in reduced or µg	Minutes in reduced or µg
Two-g during pull out (weld solidified?)	Hi-g only before welding (launch)
g-jitter complicates effect of gravity	Reduced g-jitter

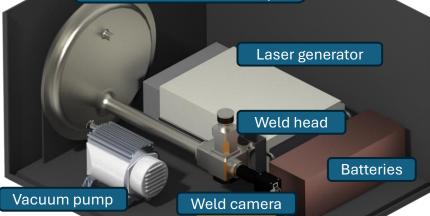


#### Initial protoflight hardware design



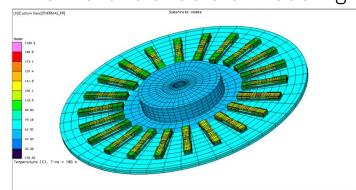


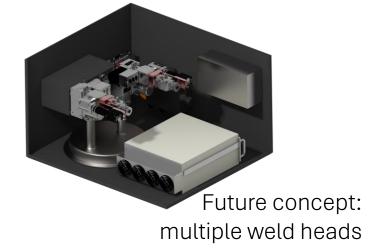
Conformal vacuum chamber (coupons to be welded mounted on disc inside)



Conceptual design developed with MSFC Advanced Concepts Office

#### Thermal and structural modeling







#### **Practicalities of suborbital LBW**



Laser module selected: 1500 W peak pulsed power, 1070 nm, Yb fiber

Requires batteries (excessive power draw from flight platform)

Fully automated control

Investigating (via ground testing) concerns re:

- Vapor deposition and spatter on vacuum window
- Loss of vacuum due to offgassing

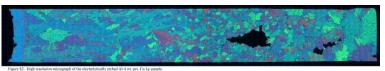


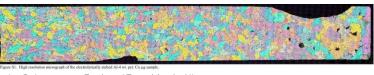
Courtesy: IPG Photonics

Materials selected: stainless steel 316L, aluminum 2219-T87, Ti64

### Also considering Al-Cu binaries:

- More tractable for computational models
- Previous flight experiments investigated solidification (Al-4wt%Cu in 1 g and µg shown below)







## Data collection to anchor computational models



- Weld camera: 140+ dB HDR imaging for weld bead size & morphology
  - Coxial mount onto weld head for on-line alignment with specimens
- Thermal/weld camera: short-wave infrared (InGaAs) thermography of weld
  - Reduced effect of emissivity shifts on thermal data
  - Enhanced view through weld fumes
- Thermocouples: provide calibration for thermography
  - Establish workpiece starting temperature (collateral heating)
  - Require slip ring (or similar) and pass-through into vacuum
- Plume characterization (ground only)
  - Spectrometer for chemistry, mid-wave infrared or Schlieren for morphology



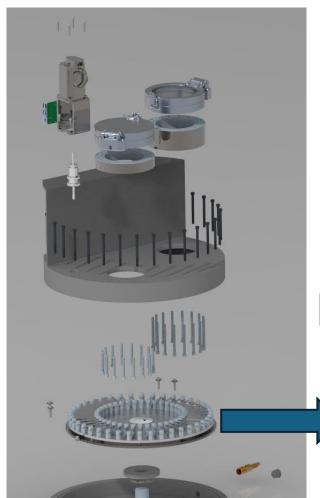


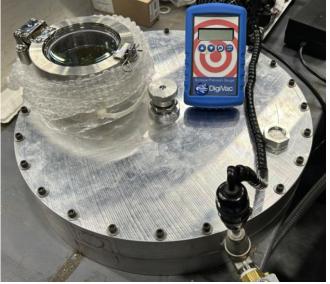
## Latest prototype status – design and fabrication





- Switched from central spindle to turntable driven by belt (o-ring)
- Added additional access door
- Reduced length of "stovepipe"
- Provided mounting plane for weld head, etc.

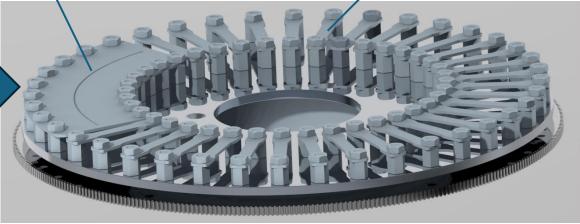




- Vacuum
   chamber robust
   and maintains
   <100 Pa</li>
- Initial operating capability (spot welds without thermography) achieved

Linear weld for hermetic seals

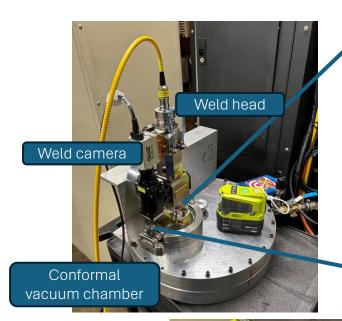
Spot welds for truss structures





## Latest prototype status – initial operating capability

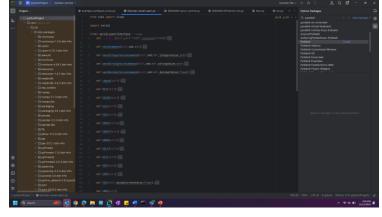




View through window into vacuum

Spot weld

Programmatic control of coupon positioning/movement and laser expected shortly



Coaxial weld camera in operation; thermal to follow

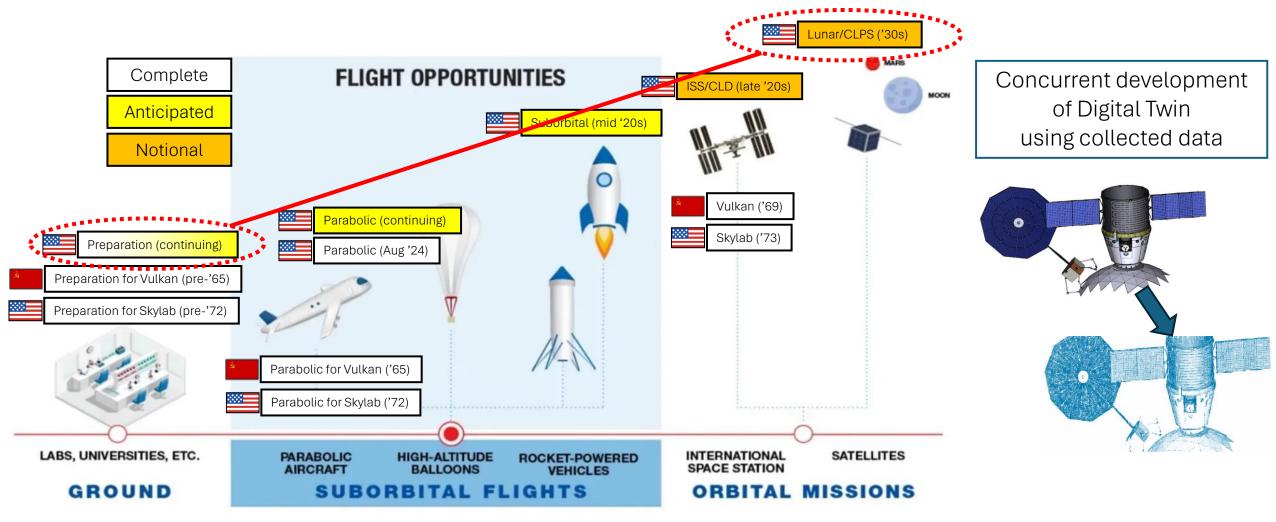
> Rapid access to coupons



Concern: metal vapor coating, also spatter
Current mitigation: cover glass (sacrificial)

FY25 SBIR Pre-release –
"Space-Capable Laser Beam
Welding Component and
Subsystem Development"





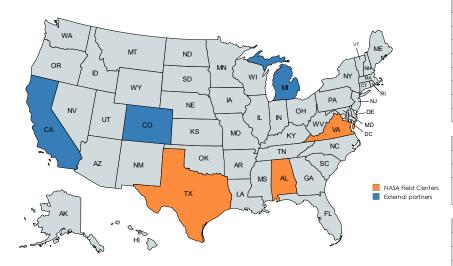


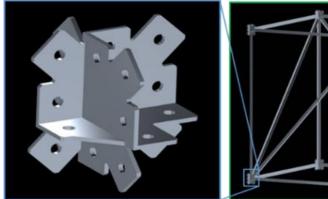
## **Lunar Assembly and Servicing by Autonomous Robotics (LASAR)**

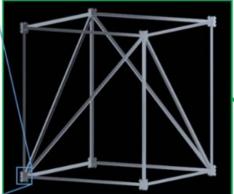


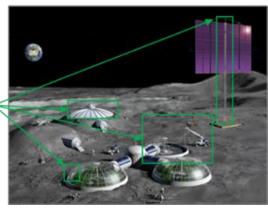
NASA-funded Early Career Initiative project: Mature LBW and associated robotics & NDE (non-destructive evaluation) for Lunar infrastructure applications

- Ruggedized laser optics and robotic arm suitable for thermal vacuum
- Supervised autonomous LBW of innovative "Snowflake" joint geometry
- Non-contact NDE of welds









Visualization of innovative "snowflake" joint geometry constructing Tall Lunar Tower

PI: Andrew O'Connor; PM: Zach Courtright (both NASA/MSFC)

#### **NASA Core Team Members**

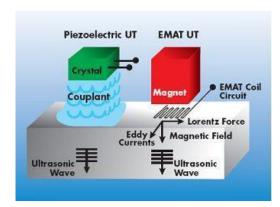
Name	Center
Emma Jaynes	NASA/MSFC
Alex Sowell	NASA/JSC
Raju Subedi	NASA/MSFC
Brace White	NASA/LaRC
Si	upported by:
William Evans	NASA/MSFC
Matthew Mahlin	NASA/LaRC
Parker Shake	NASA/MSFC

J	Exte	rnai	Partn	ers	
ne					Rol
4.1					

Name	Role
Laserline	Laser Processing Partner
Motiv Space Systems	Robotics Hardware Partner
PickNik Robotics	Robotics Software & Autonomy
	Partner

M	[er	ıto	rs

Name	Role
Shaun Azimi	JSC Robotics SME
Bill Doggett, PhD	LaRC In-Space Assembly SME
John Fikes	MSFC Management SME
Jeffrey Sowards, PhD	MSFC Laser Welding SME



Electromagnetic acoustic transduction (EMAT) for NDE



## LASAR: Laser Processing sub-team





Initial mounting and welding trials on UR10e robotic arm in ambient conditions

Laser optics and delivery fiber to be placed within thermal vacuum representing Lunar surface

> Components within dashed lines are within V-20 TVAC at MSFC (shown to right)

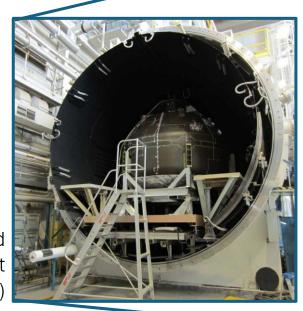
Laser generator, diode (outside TVAC)\*

> \*Future opportunity: ruggedization of laser generator

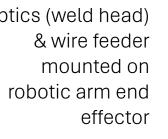


Post-weld characterization:

- Metallography and chemistry
- Mechanical testing
- TVAC compatibility



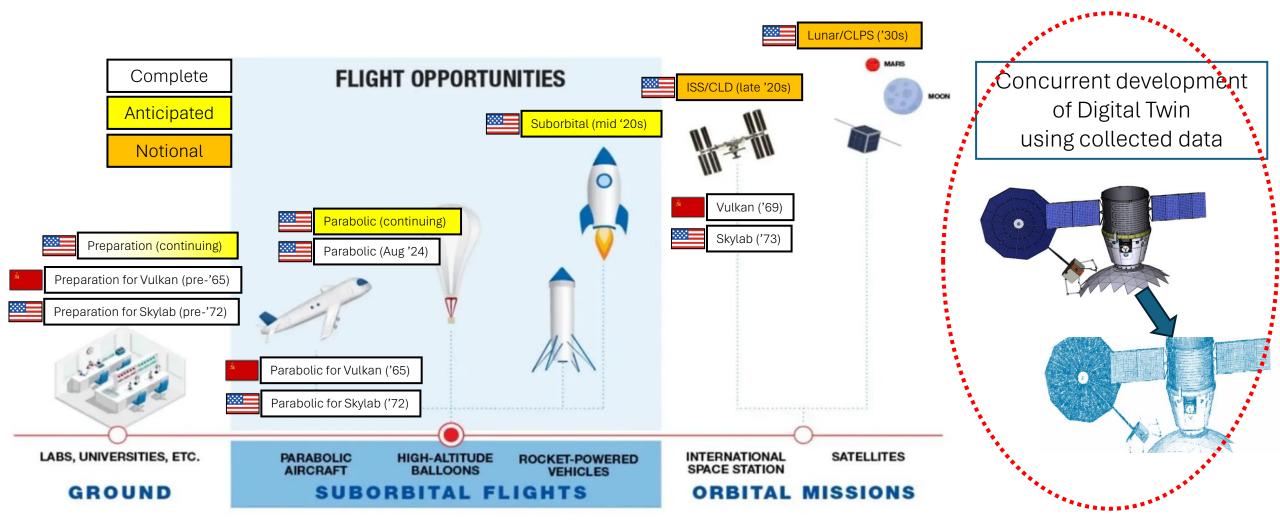
Laser focusing optics (weld head) & wire feeder mounted on robotic arm end effector







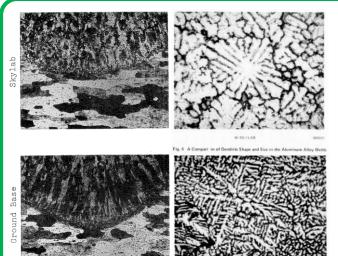






## Skylab Electron Beam Welds: Structure-Property-Processing

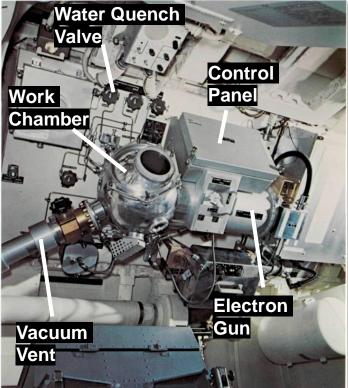




2219-T87 Aluminum, 1003

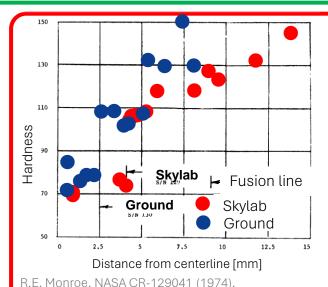
- In the ground-based samples, the dendrites are much larger at the root region than at the crown region. For Skylab samples, reduced difference in size.
- Concluded some unknown combination of *G* (temperature gradient) and *R* (solidification range) varied between ground and flight
- G. Busch. Grumman Report (1976). <a href="https://ntrs.nasa.gov/citations/19770024270">https://ntrs.nasa.gov/citations/19770024270</a>





**Processing** 

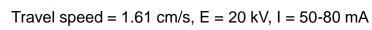
#### Structure



https://ntrs.nasa.gov/citations/19750002046

#### **Properties**

- Monroe (1974) produced hardness plots for full penetration Skylab and Ground welds.
- Li et al. (1976) concluded that no significant differences in hardness were observed between the ground-based and Skylab samples of 2219. Tantalum discs did show a significant difference, but no explanation was provided.



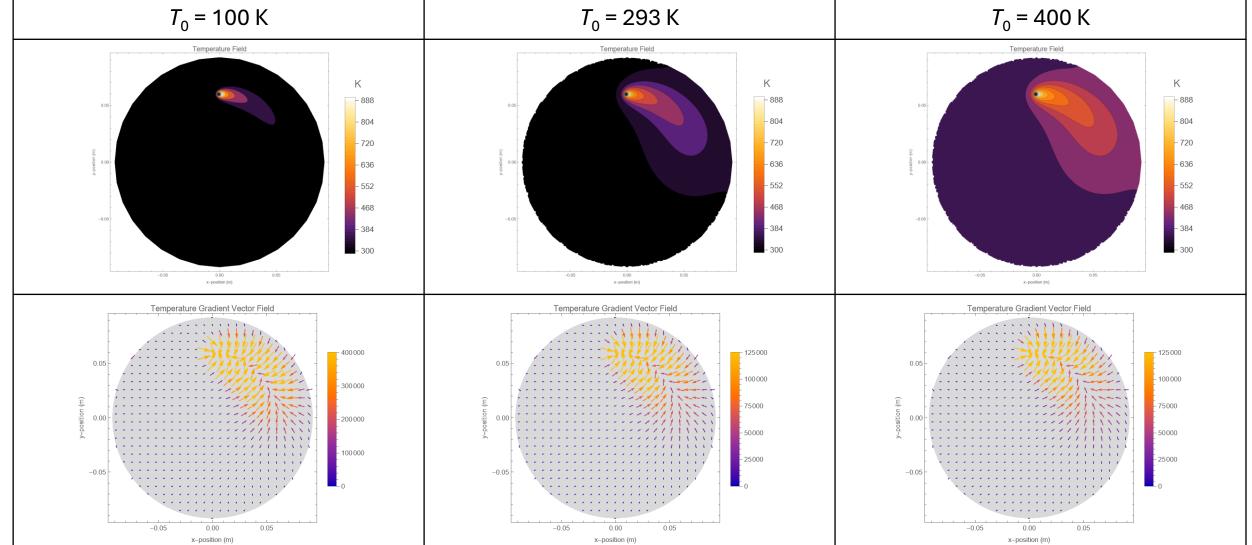
Alloys: Stainless Steel (304), Aluminum (2219-T87), CP Tantalum.

After 2 hr space vent, Vacuum =  $10^{-4}$  Torr (~ $10^{-2}$  Pa)

Computational and Physics-Based Modeling for the Development of in-Space Welding Technology - NASA Technical Reports Server (NTRS)

# Temperature and gradient maps of Skylab 2219 Al disc at 100K, 293K, 400K

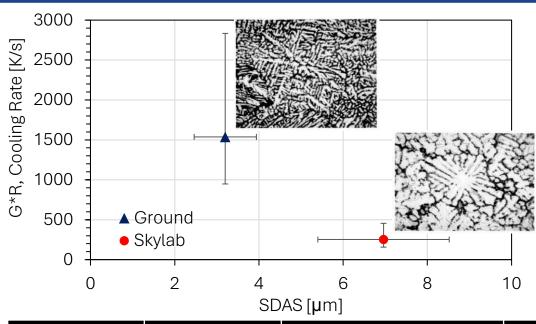






## Comparison of Model and Empirical G\*R





$$\lambda_2 = (143.73 \text{x}^{-0.356}) (\text{G*R})^{-0.43}$$

Brice and Dennis. *Met Trans A* 46 2015: 2304-2308.

DOI: 10.1007/s11661-015-2775-x (Wirefed electron beam additive

manufacturing process on Al-Cu)

 $\lambda_2$ , Secondary dendrite arm spacing [ $\mu$ m]

x, Cu content of AA2219 Skylab discs (6.2 wt.%)

G, Thermal gradient [K/m]

R, Growth rate [m/s] (Ground ~Travel speed = 0.015 m/s)

G\*R, Cooling rate through solidification interval [K/s]

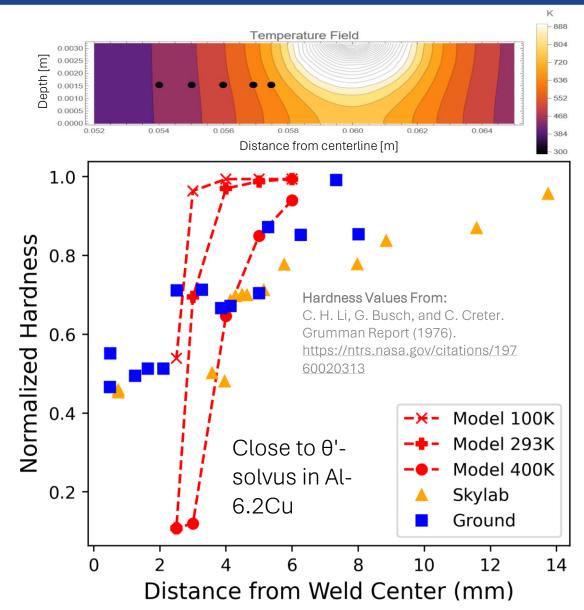
Condition	SDAS [µm]	Empirical GR [K/s] (from equation above)	Empirical G [K/m] (from equation above)	R [m/s]	Macro Gradient [K/m]
Ground	3.2 ± 0.74 (N = 26)	1537	104·10 <sup>3</sup>	0.015	125·10 <sup>3</sup>
Skylab	6.96 ± 1.56 (N = 22)	252	17·10 <sup>3</sup>	Unknown due to microgravity solidification	Fluid transport neglected in model

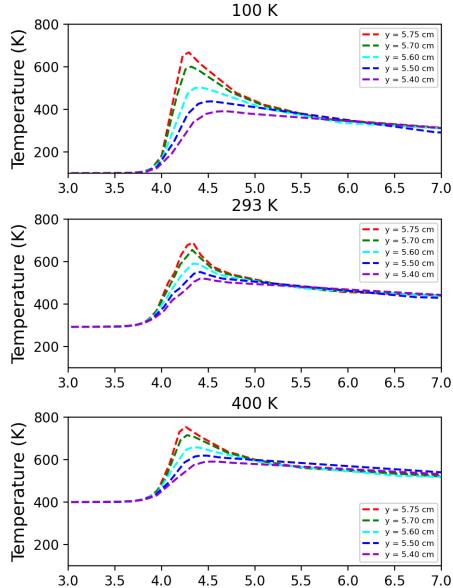
The lack of convective currents in microgravity means heat and solute are removed from the solidification front primarily by diffusion, resulting in slower growth rates and larger dendrite arms.



# Properties: Hardness by Starting Disc Temperature



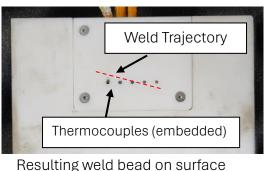




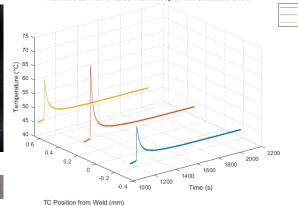


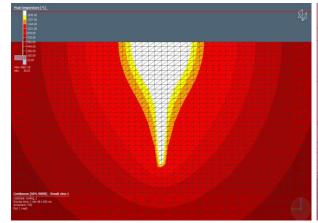
# Leveraging ICME modeling to link laser absorptivity, thermophysical properties of material, laser parameters, etc.

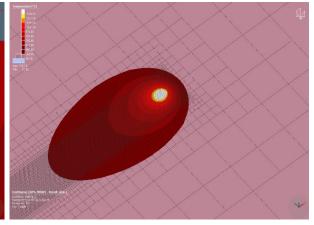




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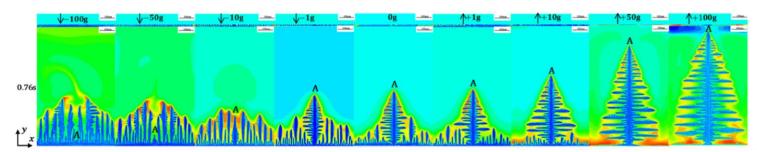


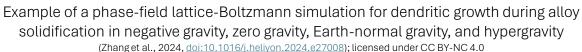


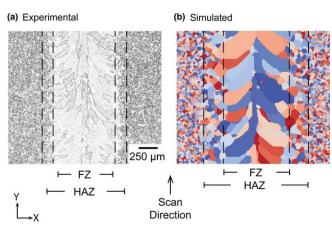


Validating LBW thermal models with thermocouples and thermography; enhances confidence in ICME approach

To do: link thermal & thermodynamic/precipitation model to solidification, fluid flow, and grain structure







Example of a Monte Carlo Potts model in SPPARKS code to simulate grain growth in e-beam welding

(Rodgers et al., 2016, doi:10.1007/s11837-016-1863-8); licensed under CC BY 4.0



#### **Conclusions**



- NASA and partners are progressing experiments from ground to flight
- Demonstration of LBW in space-like environments will enable:
  - Understand combined effects of reduced gravity, reduced pressure, varied temperatures
  - Provide validation datasets to anchor computational models
  - Mature ISW technology to enable joining structures in space
- Building ISW ecosystem of hardware, expertise, and partnering opps.
  - Suborbital flight unit hardware
  - Parabolic and suborbital flight experiment know-how
  - Computational models anchored by collected data
  - Network of academic, government, and industrial collaborators



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