



## NASA's Horizontal Planar Near-Field Facility:

A Large-Scale, High-Accuracy System for Spaceborne Antenna Testing

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# Near-Field Planar Scanner

Made for Space-Borne Antennas / Vehicle Mounted Antennas

SCANNER DIMENSIONS: 10M X 10M

## Technology

- > Horizontal Planar Near-field Scanner:
  - > Better for deployable to prevent distortions to the parabolic shape.
  - > Can drive in large vehicles for insitu-measurements for upper-hemisphere measurements
  - > E.g. Lunar Vehicles or UAVs

## Measurement capabilities

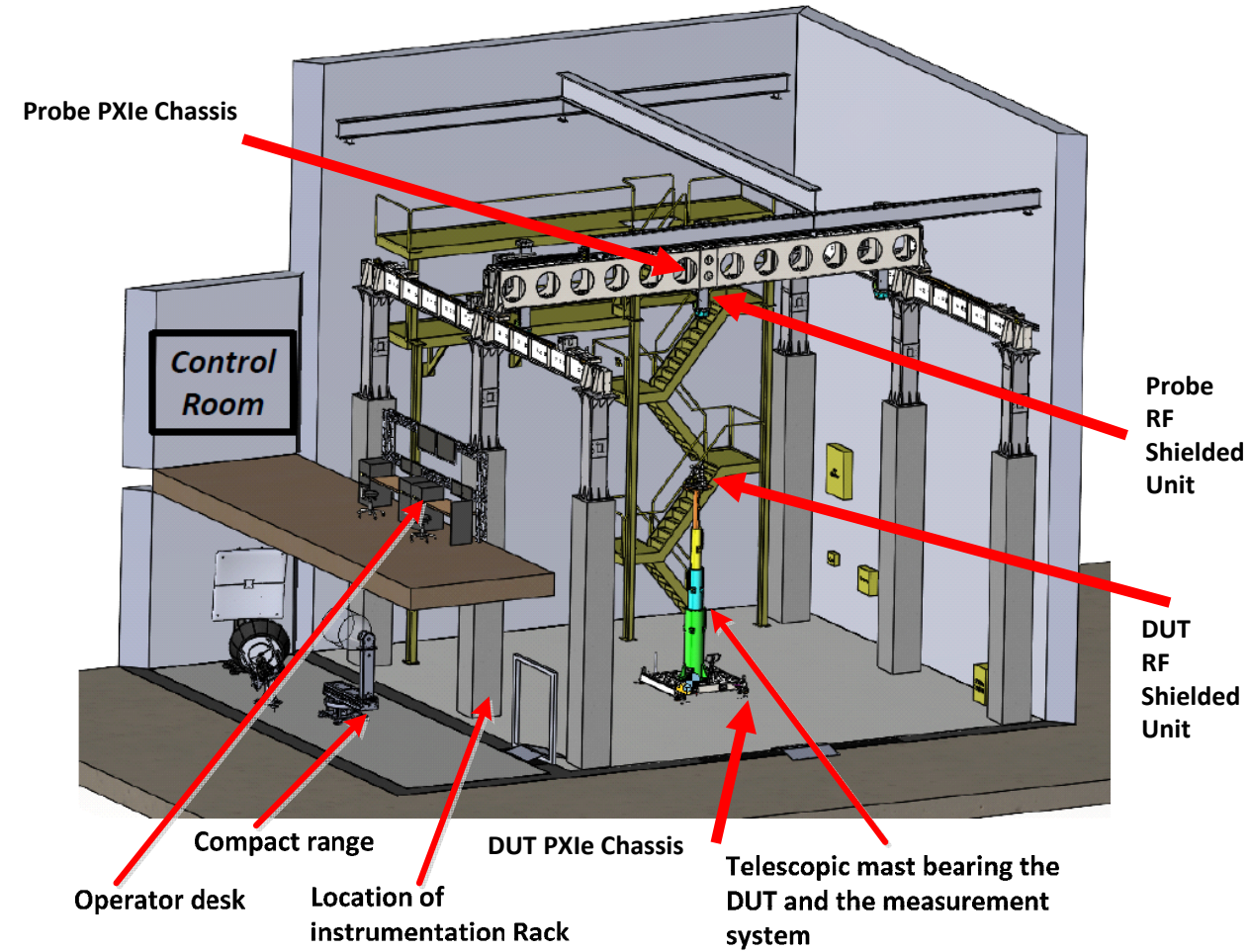
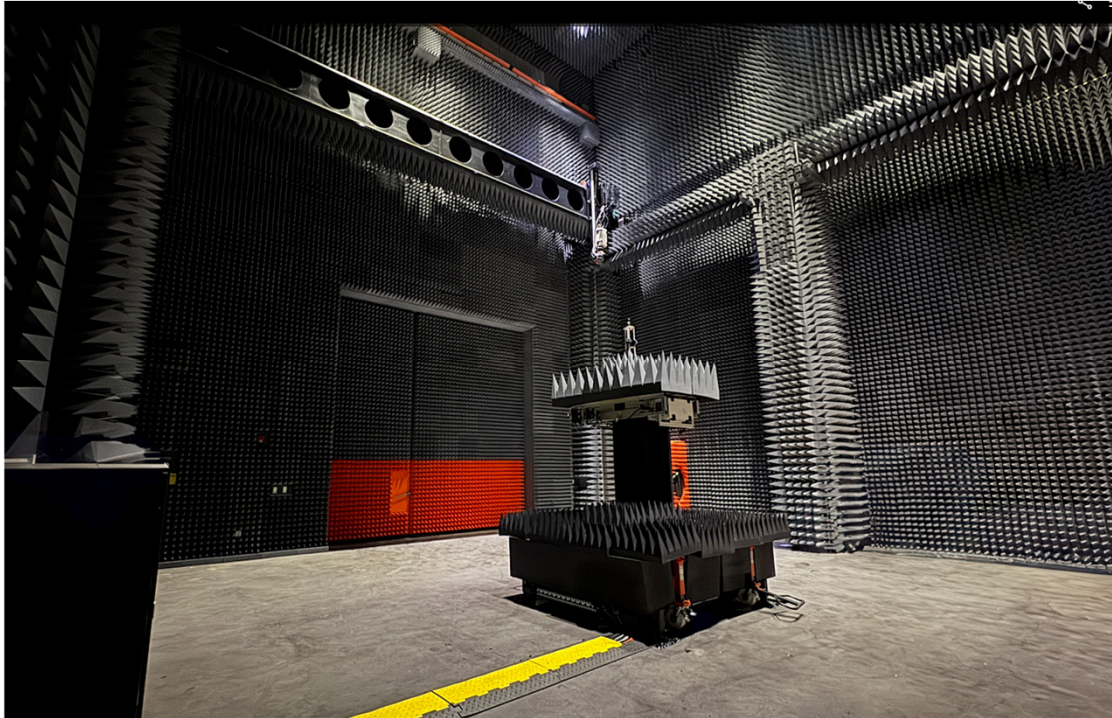
- |                                                                                                                                                                                                                                                |                                                                                                                                                                                                                                                                                 |
|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| <ul style="list-style-type: none"> <li>&gt; Gain</li> <li>&gt; Beamwidth</li> <li>&gt; Sidelobe levels</li> <li>&gt; Radiation pattern in any polarizations - (linear)</li> <li>&gt; Multi beam antenna measurement and calibration</li> </ul> | <ul style="list-style-type: none"> <li>&gt; Directivity</li> <li>&gt; 3D radiation patterns</li> <li>&gt; Beam pointing properties</li> <li>&gt; Full payload testing</li> <li>&gt; EIRP, G/T, IMD,</li> <li>&gt; Pulsed Measurements</li> <li>&gt; Gain Compression</li> </ul> |
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## Frequency bands

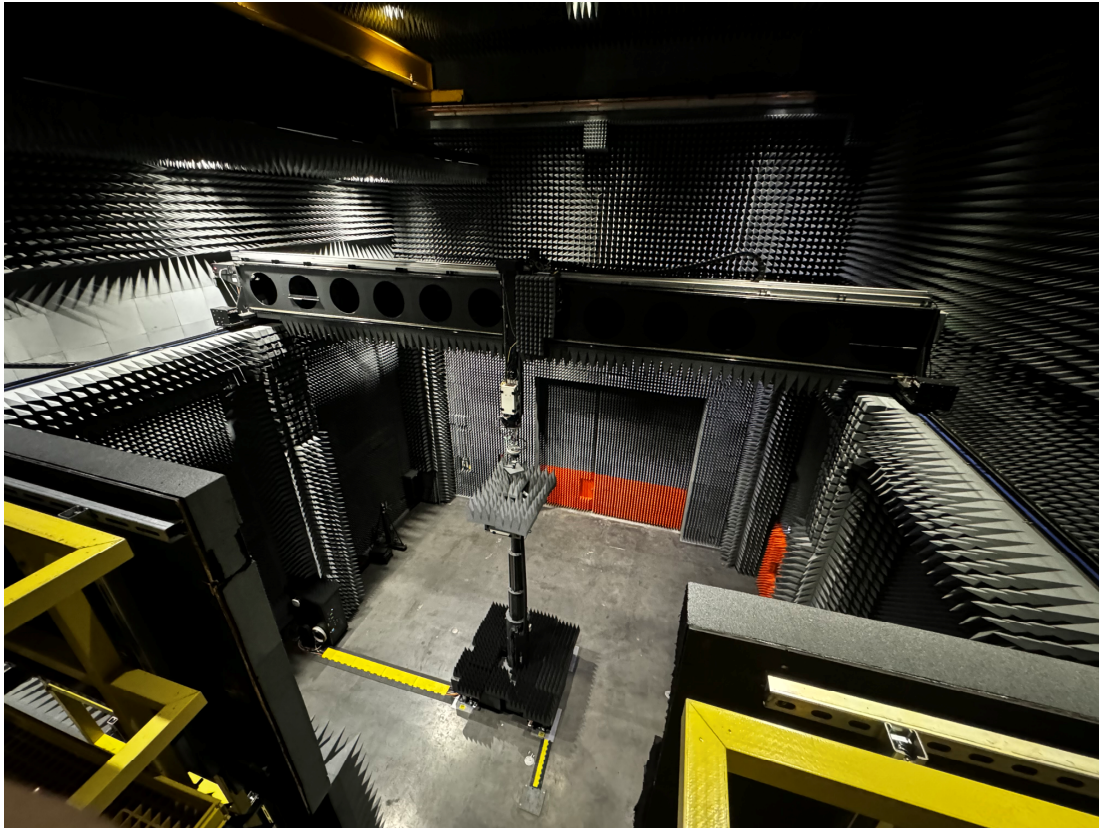
1 to 110 GHz (and beyond?)







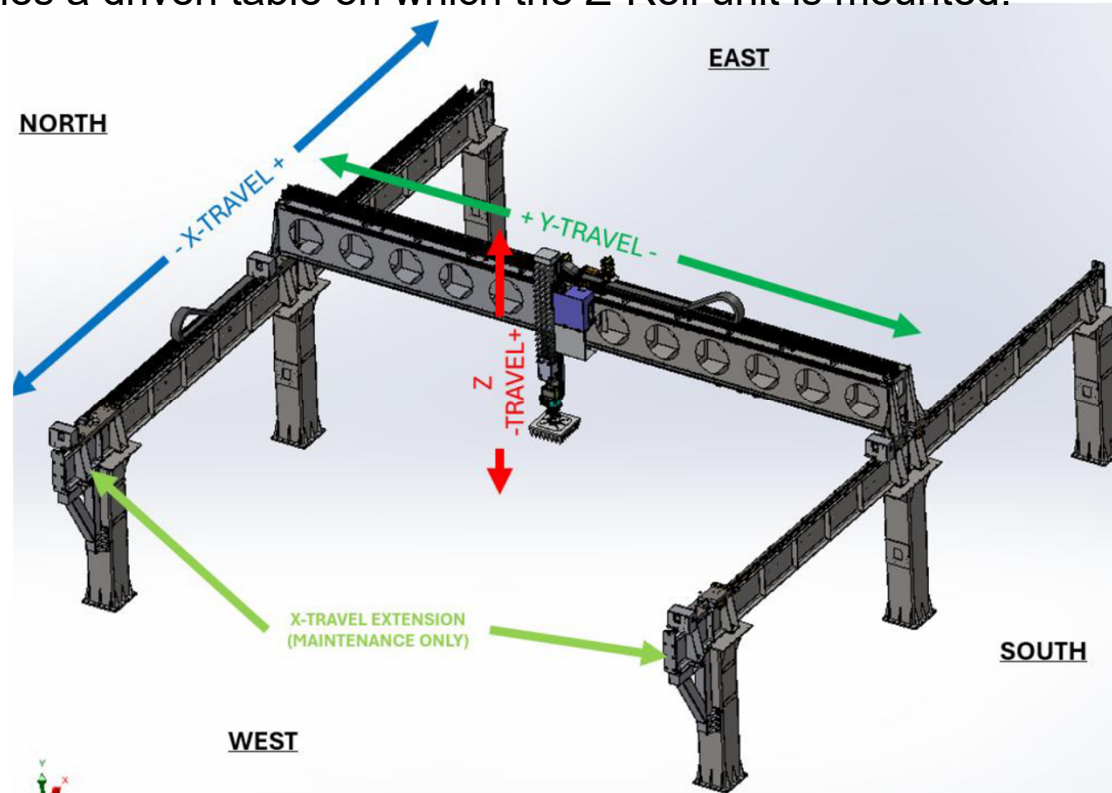






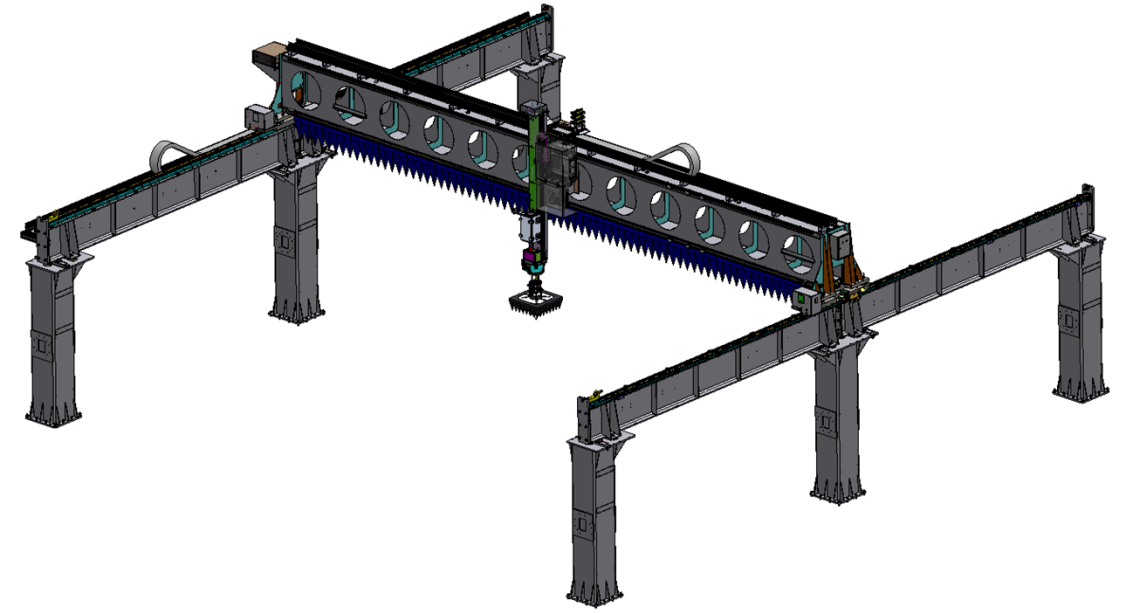
# Structural Description

- The scanner is built from two X-axis linear slides and a Y-axis beam moving in the horizontal plane.
- The X-axis linear slide is constructed of two modular sections, which are securely mounted on six supporting masts fixed to the floor and are leveled to it as one integral unit.
- The Y-axis linear slide is mounted on top of the X-axis linear slides and moves along them. The Y-axis carries a driven table on which the Z-Roll unit is mounted.



## Scanning Area & Motion

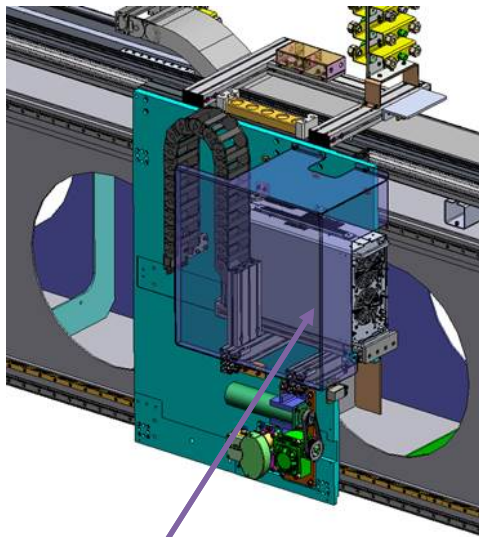
- Scan area of **10m x 10m x 1.5m** (X / Y / Z).
- Probe mounting location has roll / polarization alignment.
- Probe aperture can be located at a height of ~9.1m – ~7.6m.
- Overall Dimensions: 13.64m x 13.25m x 12m



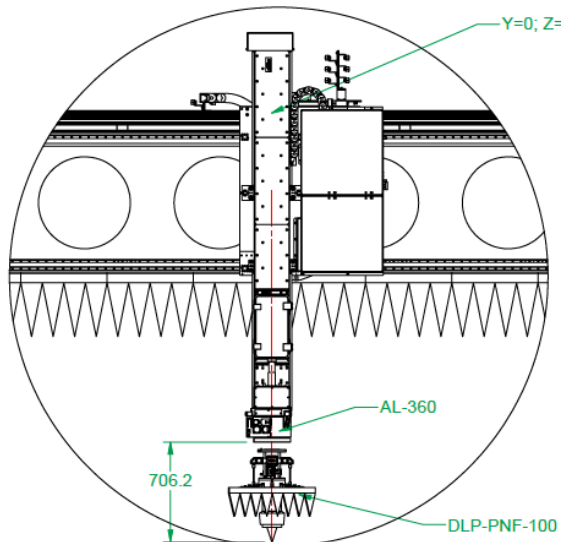
Parameter	X-axis	Y-axis	Z-axis	Polarization AXIS
Travel range	10000mm	10000mm	1500 mm	360 deg
Scan speed	250 mm/sec.	500 mm/sec.	10 mm/sec.	1rpm
Load	N/A	N/A	80 Kg	N/A
Resolution	0.001 mm	0.001 mm	0.003 mm	0.001 deg
Accuracy (corrected)	+/- 0.06 mm	+/- 0.06 mm	+/- 0.06 mm	+/- 0.02 deg
Planarity	0.035 RMS mm corrected			



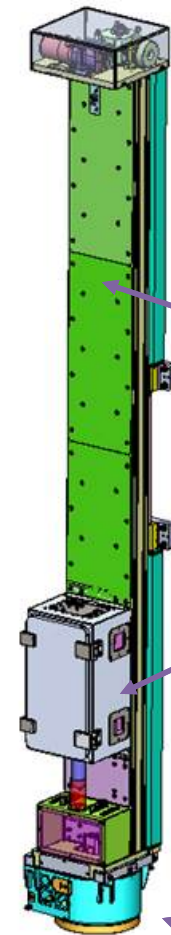
# RF Unit Locations on Z-Axis



PXIe unit



DETAIL D  
SCALE 1 : 25

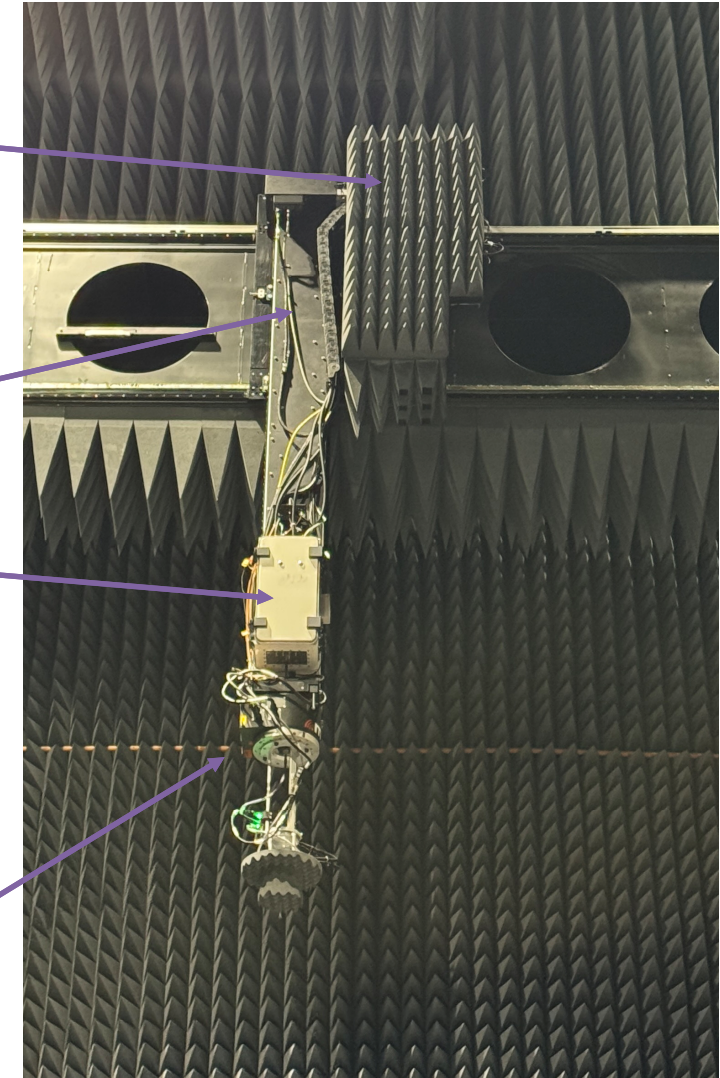


PXIe unit

Z-Axis Positioner

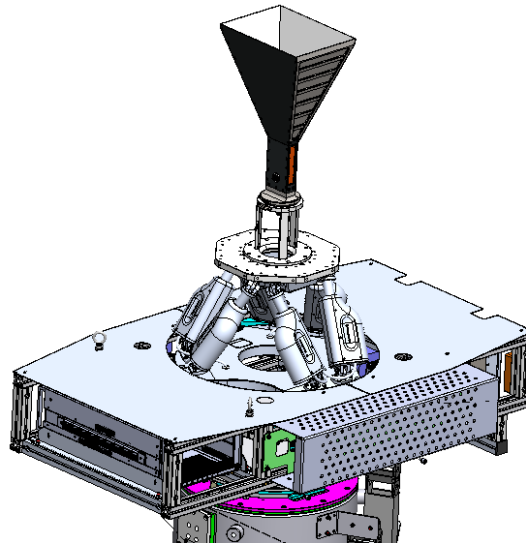
RF shielded enclosure

Roll Positioner



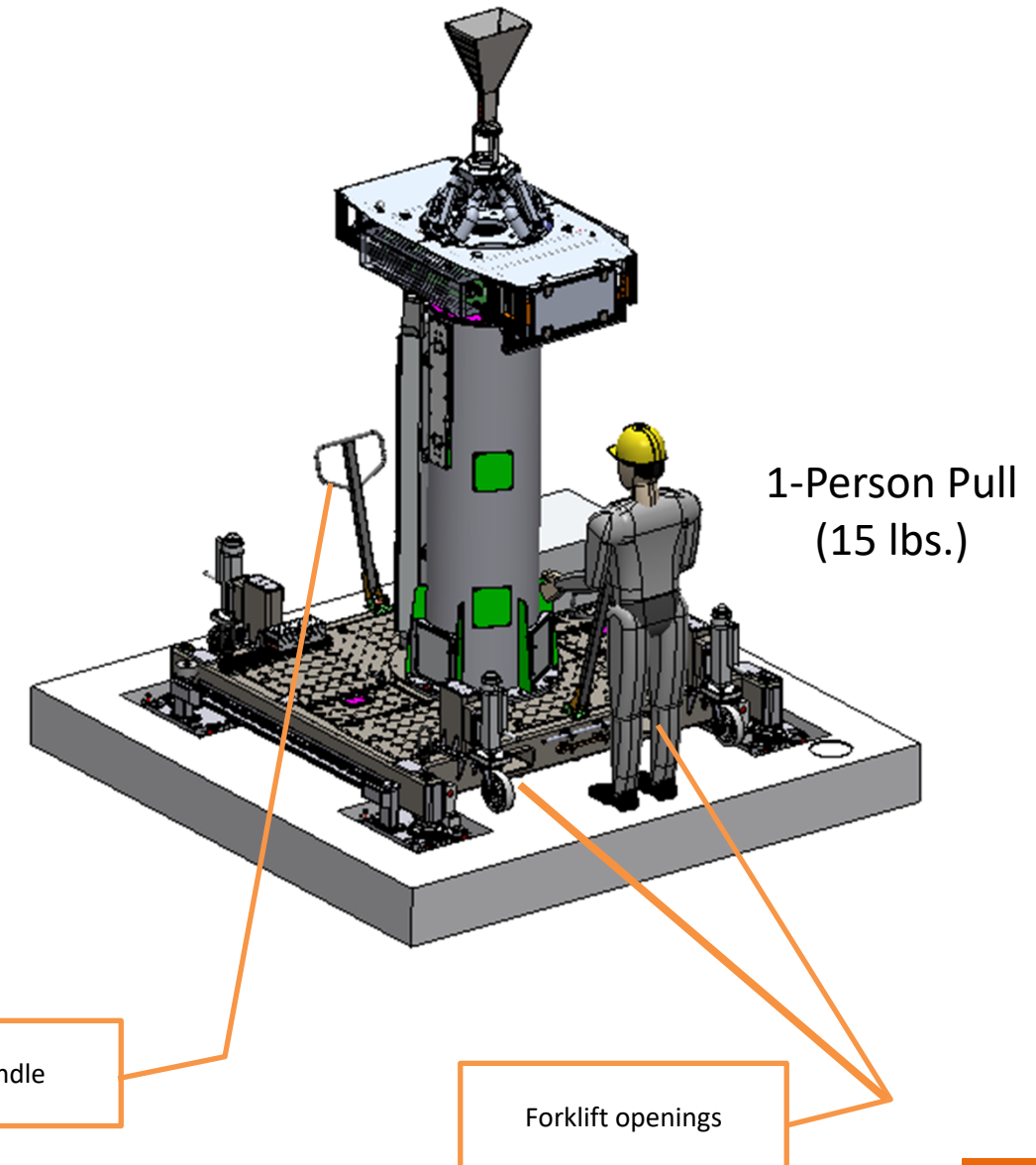
# / DUT Positioner– General

- / DUT Mast has telescoping height from 3m to 6m
- / Cart dimensions: 2m x 2m
- / Top of the DUT Cart is a Symmetrie BREVA Hexapod used for precision DUT alignment
  - / Sized to be able to support a group 3 drones ( 55 – 1320 lbs)
  - / Precision alignment for mm-Wave measurements
- / DUT mounting face/sides includes holes for SMR targets for DUT alignment





- / Positioner cart is pushed by hand over tapered locating features and lowered into testing position with jack wheels
- / Allows for it to be moved in and out of the chamber
  - / Repeatability:  $\sim .02\text{mm}$
- / Allows for rolling in large antennas that cannot be otherwise mounted
- / Can drive in large vehicles for insitu-measurements for upper-hemisphere measurements
- / E.g. Lunar Vehicles or UAVs



- A Laser tracker was used for initial alignment and positioner corrections (MV-Cor)
  - HNF scanner
    - Corrected X- Axis as a function (X,Y)
    - Corrected Y-Axis as a function (X,Y)
    - Correction of Z Planarity as a function (X,Y)
    - Roll Pointing aligned to scan plane
  - DUT Mounting
    - X,Y, Z rotation errors and translation
- Long term goal is to also allow for
  - Surface metrology aligned to the near-field data
    - For back projection of the data to Ideally correlate the defects
  - Characterization of parabolic surfaces
    - Directly mounting a laser scanner on the probe positioner mounts



# RF Subsystem

## Features a Dual PXI Architecture

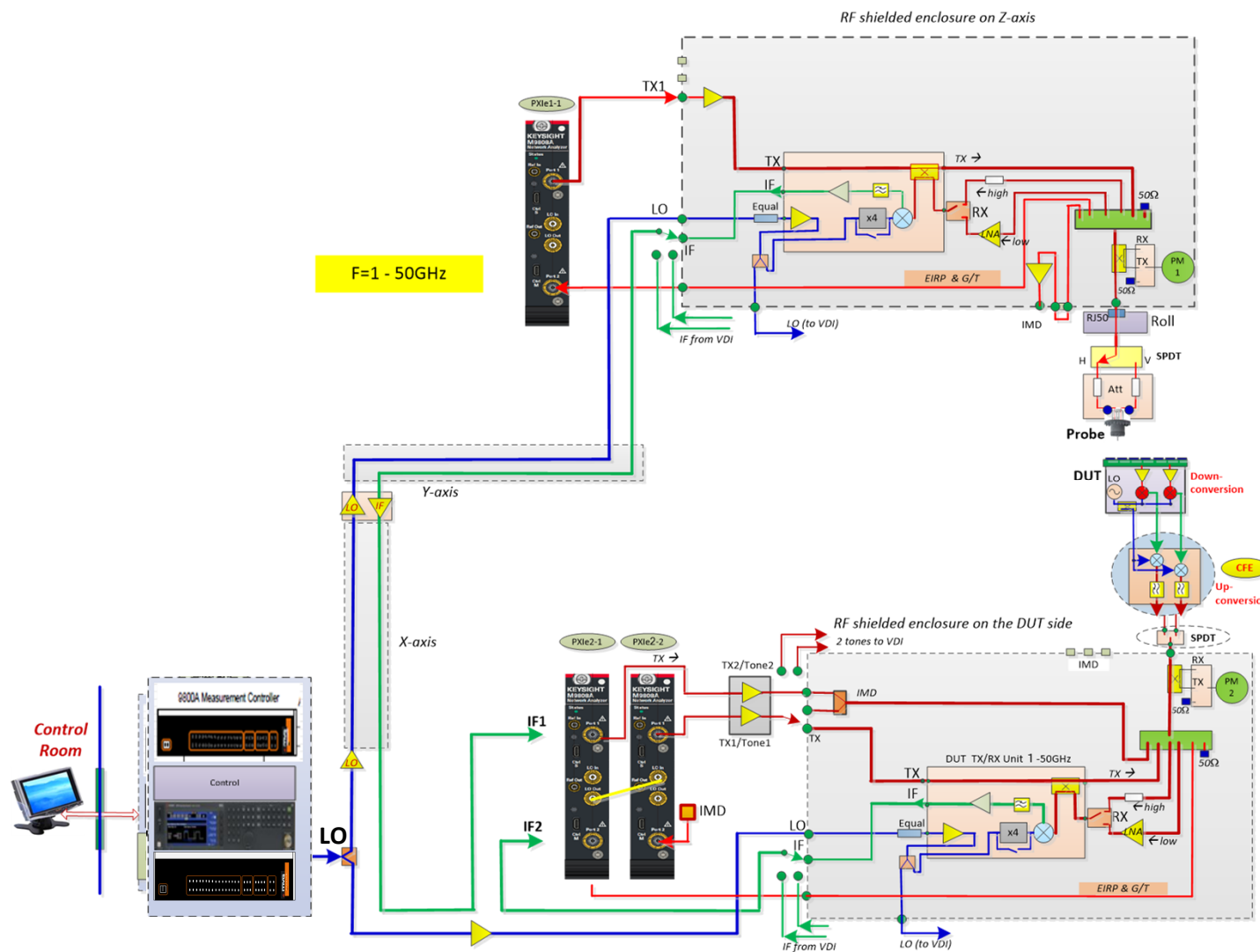
- 1 PXIe at the DUT and one on the Scanner
- Direct RF 1-50 GHz

## Phase Coherency through an MXG located in a rack on the ground

## Shielded RF Enclosures

- Down-convert test and reference signals to an IF
- Multiplier is used for down-conversion above 20 GHz

## LO runs up from the rack through Scanner and DUT tower



## 2x M9010A 10-Slot PXIe Chassis

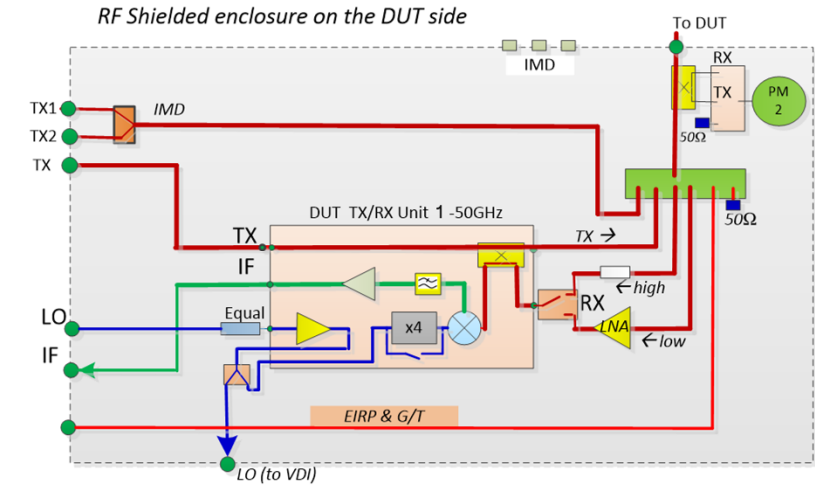
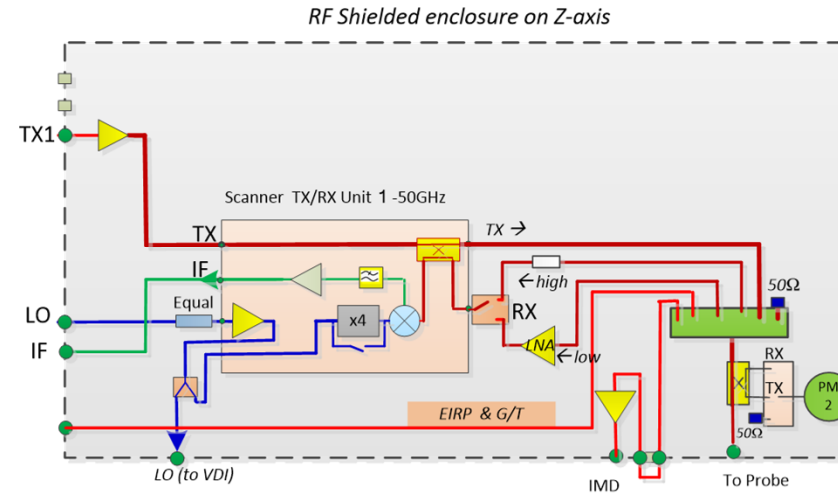
- Keysight M9808A-200 100 kHz to 53 GHz PXIe Vector Network Analyzer

## System will include (2) Chassis

- DUT Chassis, configured with (2) M9808A modules
- Probe Chassis, configured with (1) M9808A module
  - Spectrum Analyzer Hardware/Software
  - Intermodulation Distortion (IMD) Software
  - Pulse Modulation Hardware and Software

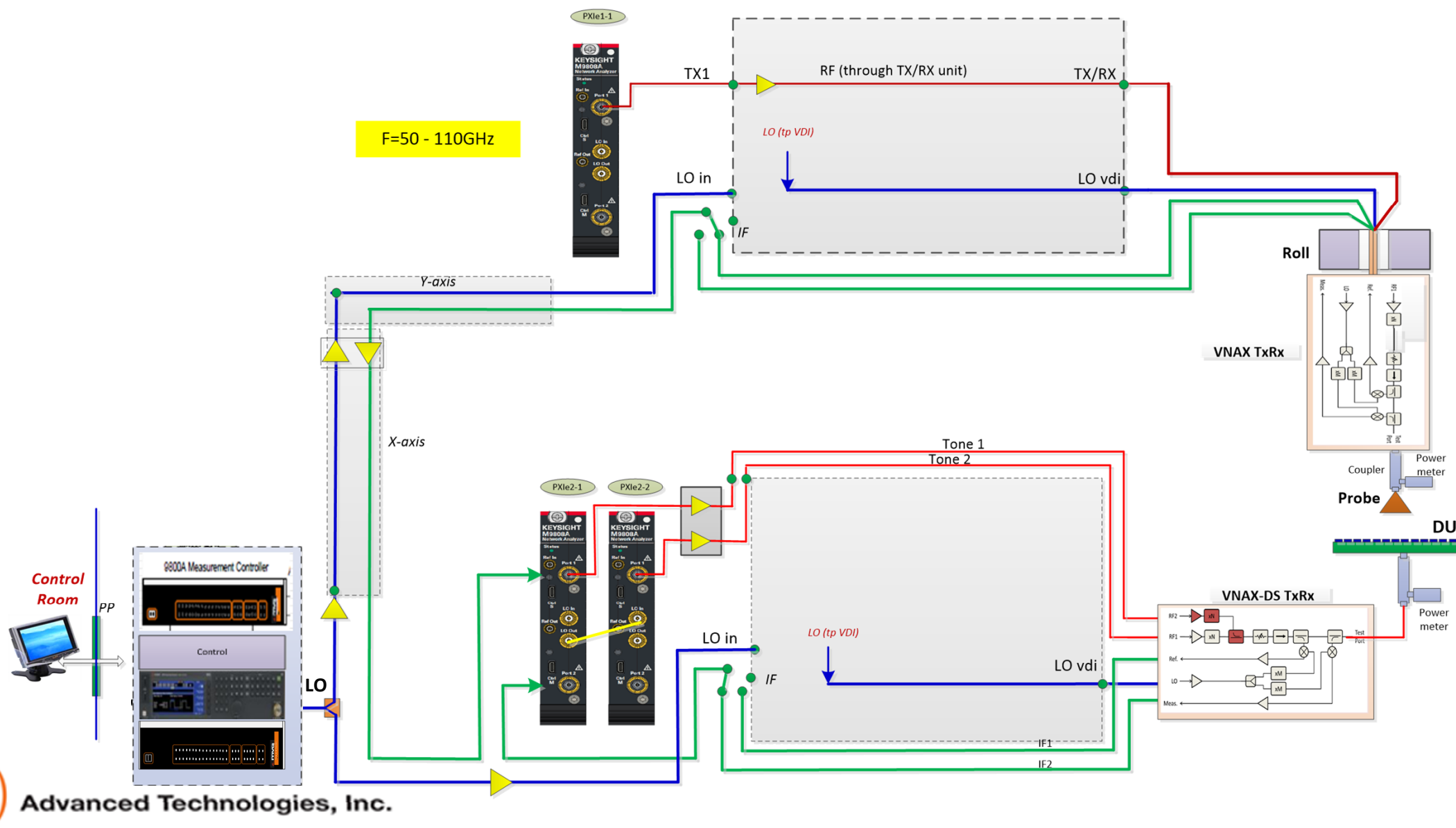






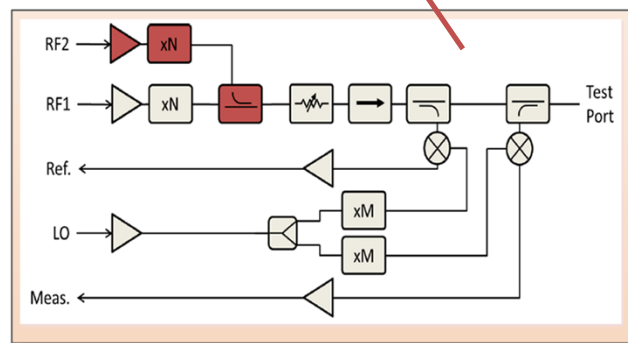
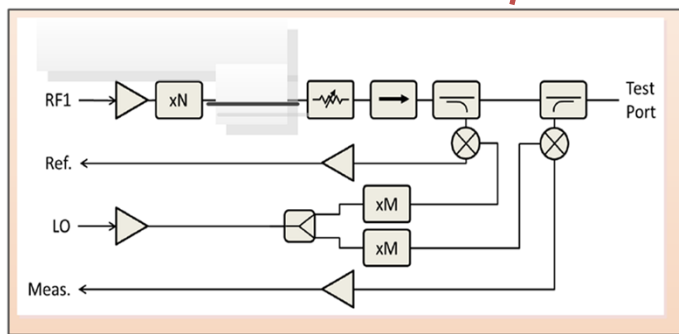
Shielded enclosure Specification	
Frequency Range	0.5-50 GHz
Shielding effectiveness	-80dB @ 1-10 GHz -65dB @ 10-50 GHz
Dimensions	500/250/200 mm
Input power	24V DC

# RF System Configuration (50-110GHz)



# VDI Frequency Extender Modules

#	Freq Band	Probe Side	DUT Side	Required in Addition	Comments
1	V (50-75GHz) WR15	TxRx WR15VNATxRxM	TxRx-DS WR15VNATxRxM-DS	V281CS WR15 to 1mm(F) adaptor	TxRx-DS with attenuator
2	E (60-90GHz) WR12	TxRx WR12VNATxRxM	TxRx-DS WR12VNATxRxM-DS	E281CS WR12 to 1mm(F) adaptor	
3	W (75-110GHz) WR10	TxRx WR10VNATxRxM	TxRx-DS WR10VNATxRxM-DS	W281CS WR10 to 1mm(F) adaptor	







## Integrated power sensors for RF and mmWave Modes


Utilized for EIRP and G/T measurement modes.

Alternatively, the PXI can be used in Spectrum Analyzer mode if more sensitivity is needed, but required a manual setup.

	Unit	P/N	Probe side	DUT side	Description	Comments	
2	Power sensor 10MHz-54GHz	U2056XA	1	1	Average power -70...+20dBm	U2056XA-100 Connector 1.85mm Accuracy: +/-0.24dB @50GHz	
1	Power sensor DC-120GHz	U8489A	1	-----	Thermocouple, -35...+20dBm	U8489A-200 Connector 1.0mm Accuracy: 7.6% @110GHz	

## Each probe assembly includes:

- Mechanical drawing
- AEP Absorber Collar
- Standoff cage and mounting plate
- Probe pattern correction coefficients (CST generated)
- Gain calibration at UPM
- Simulated Probe Correction Files

P/N	Freq (GHz)	Freq. Band	Polarization	Connector	
DLP-PNF-100	0.8 - 2.0	L	Dual Linear	3.5mm (f)	
DLP-PNF-200	2.0 - 4.5	S	Dual Linear	3.5mm (f)	
DLP-PNF-400	4.0 - 8.0	C	Dual Linear	3.5mm (f)	
DLP-PNF-800	8.0 - 18.0	Ku	Dual Linear	3.5mm (f)	
DLP-PNF-1800	18.0 - 40.0	Ka	Dual Linear	2.92mm (f)	
DLP-PNF-3300	33.0 - 55.0	Q	Dual Linear	2.4mm (f)	
OEW5000	50.0 - 75.0	WR15	Single Linear	w/g	
OEW6000	60.0 - 90.0	WR12	Single Linear	w/g	
OEW7500	75.0 - 110.0	WR10	Single Linear	w/g	

Measurements Below 50 GHz are dual Polarized

mmWave Bands must rotate the roll axis of the probe

## / Each SGH assembly includes:

- ▮ Mechanical drawing
- ▮ AEP Absorber Collar
- ▮ Standoff cage and mounting plate
- ▮ On-axis gain calibration performed at NPL



P/N	Freq (GHz)	WG Band	Connector
SGH112	1.12 – 1.7	WR650	N (f)
SGH170-A	1.7 – 2.6	WR430	N (f)
SGH260	2.6 – 3.95	WR284	N (f)
SGH395	3.95 – 5.85	WR187	N (f)
SGH585	5.85 – 8.2	WR137	N (f)
SGH820	8.2 – 12.4	WR90	N (f)
SGH1000	10.0 – 15.0	WR75	SMA (f)
SGH1240	12.4 – 18.0	WR62	N (f)
SGH1800	18.0 – 26.5	WR42	SMA (f)
SGH2200	22.0 – 33.0	WR34	2.9mm (f)
SGH2650	26.5 – 40.0	WR28	2.9mm (f)
SGH3300	33.0 – 55.0	WR22	w/g
SGH5000	50.0 – 75.0	WR15	w/g
SGH6000	60.0 – 90.0	WR12	w/g
SGH7500	75.0 – 110.0	WR10	w/g



# System Performance

# RF Mode Dynamic Range Measurements

## Sample Dynamic Range Measurements taken Over the Air

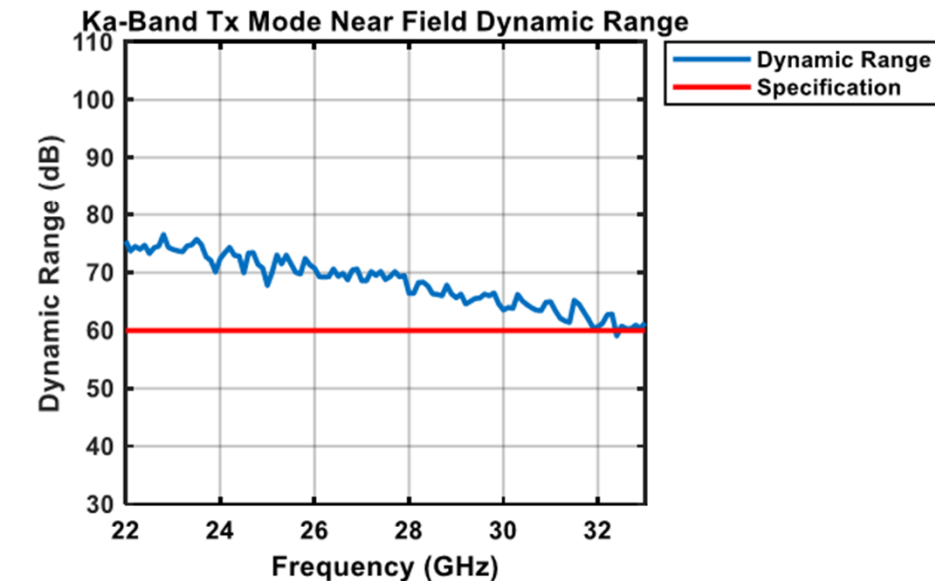
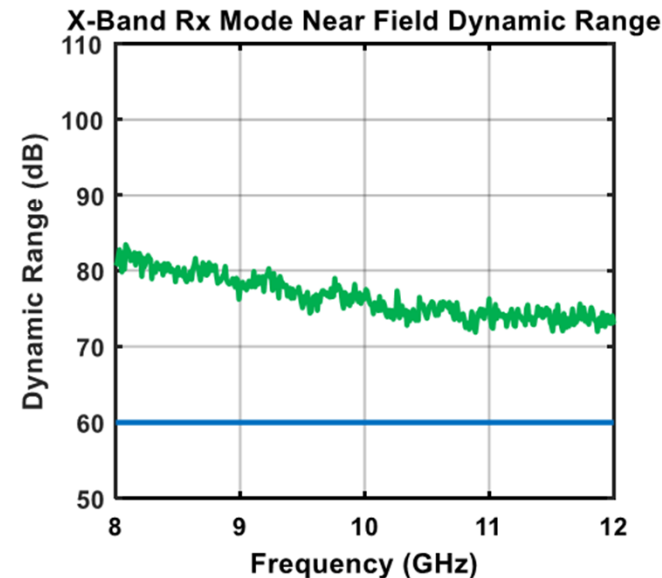
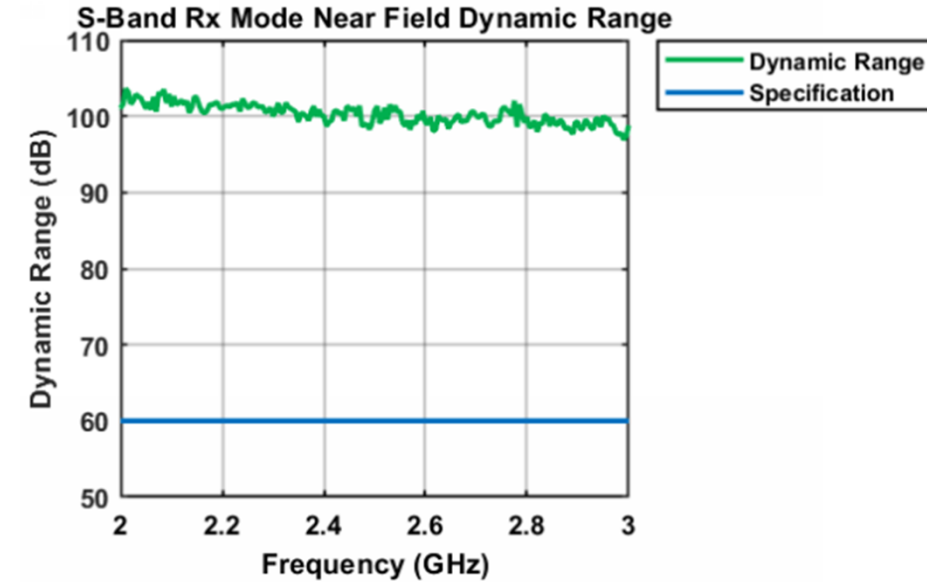
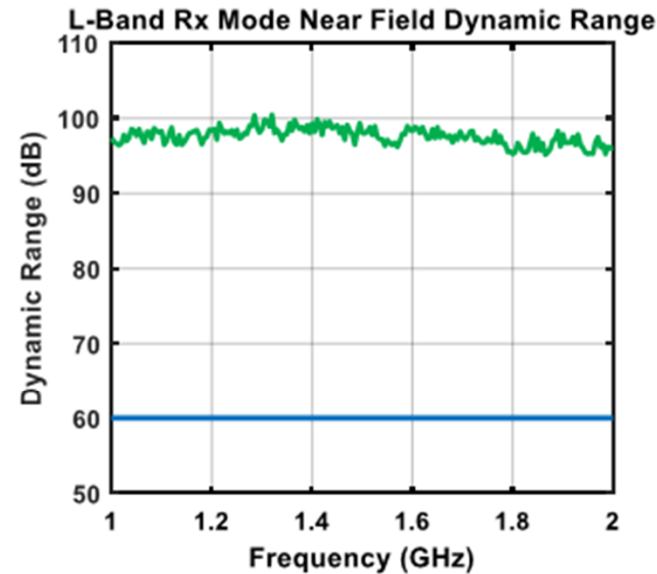
- Data taken at boresight coordinates X=0,Y=0
- 50 Frequency sweeps performed
- RMS of Signal and Noise computed.
- 1 KHz IFBW

## With DLP Probes and SGHs

- L-Band
- S-Band
- X-Band
- Ka-Band

## System Requirements for nearfield dynamic range were >60 dB.

- Stepped attenuator used to prove system is linear.



# RF Mode Dynamic Range Measurements

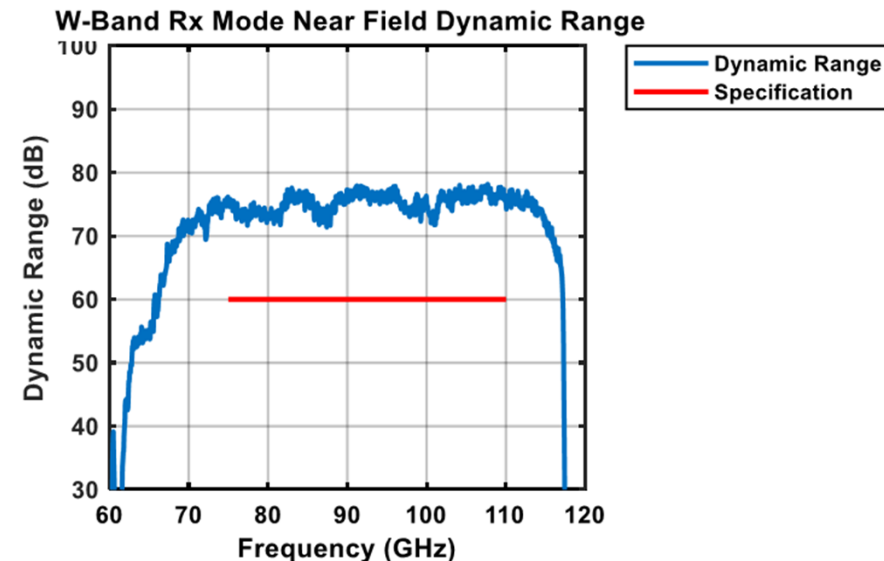
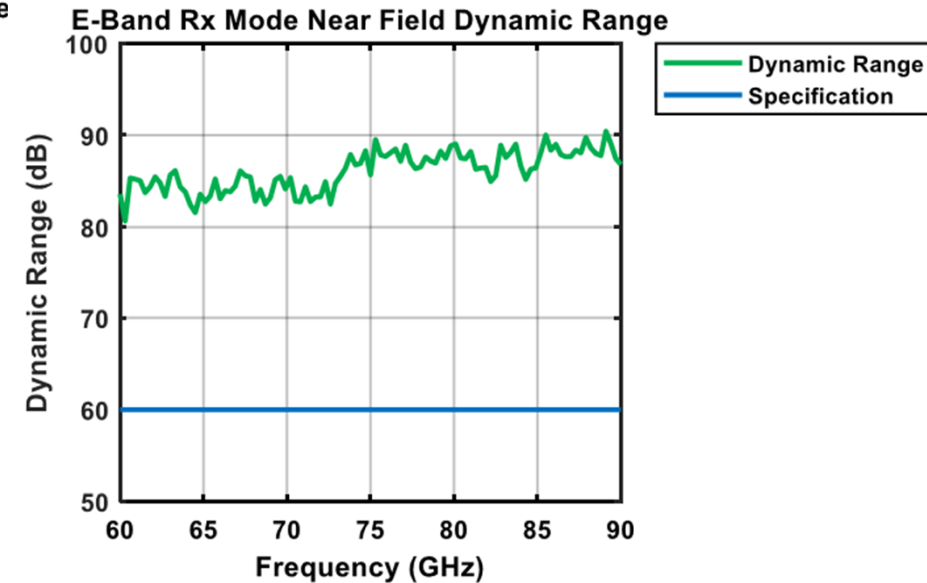
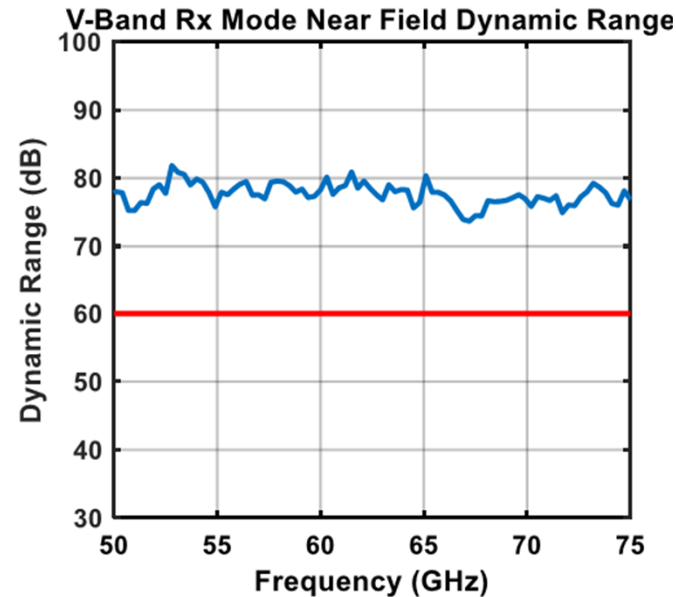
## Sample Dynamic Range Measurements taken Over the Air

- Data taken at boresight coordinates X=0,Y=0
- 50 Frequency sweeps performed
- RMS of Signal and Noise computed.
- 1 KHz IFBW

## With OEW Probes and SGHs

- V-Band
- E-Band
- W-Band

## System Requirements for nearfield dynamic range were >60 dB.





# Special Test Modes

- // EIRP
- // G/T
- // Gain Compression Testing
- // IMD
- // Pulsed RF
- // Park & Probe

## Active DUT measurements

The following tests will be performed:

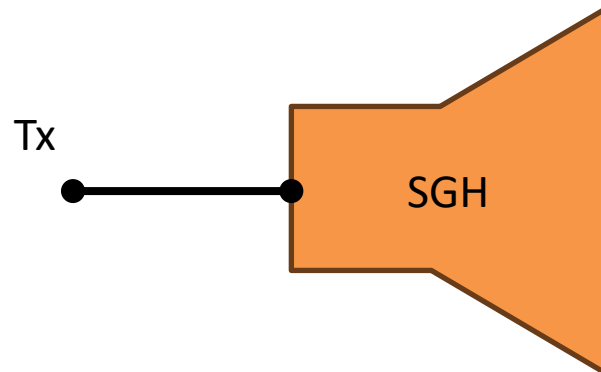
- Active Antenna patterns for G/T, and IMD

- Note: Pulsed RF, EIRP and Gain Compression do not require the Amplifier

- Separable Antenna (SGH and Amplifier required)

- Ka-Band SGH2200 (22 – 33 GHz)

Case 1: Gain Reference Baseline

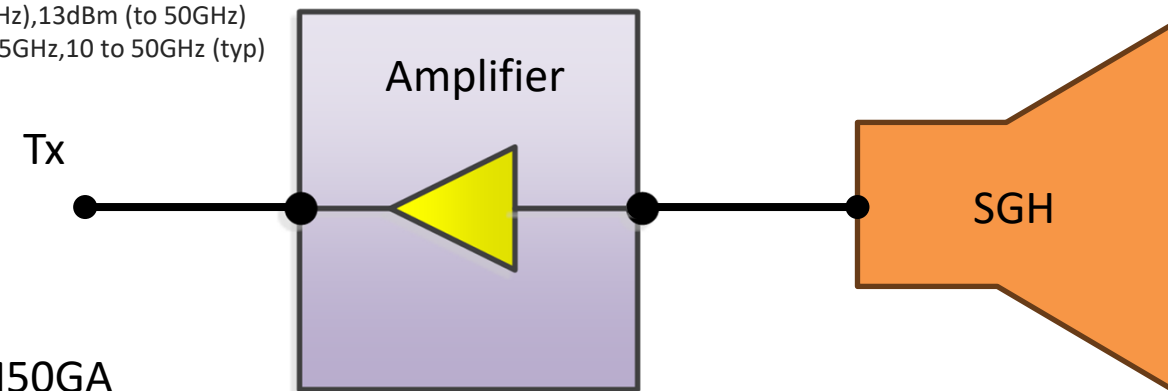


- Gain of more than 21dB
- P1dB of more than 15dBm (to 40GHz), 13dBm (to 50GHz)
- Noise figure of less than 6dB to 26.5GHz, 10 to 50GHz (typ)



RF-Lambda RAMP00M50GA

Case 2: Active DUT





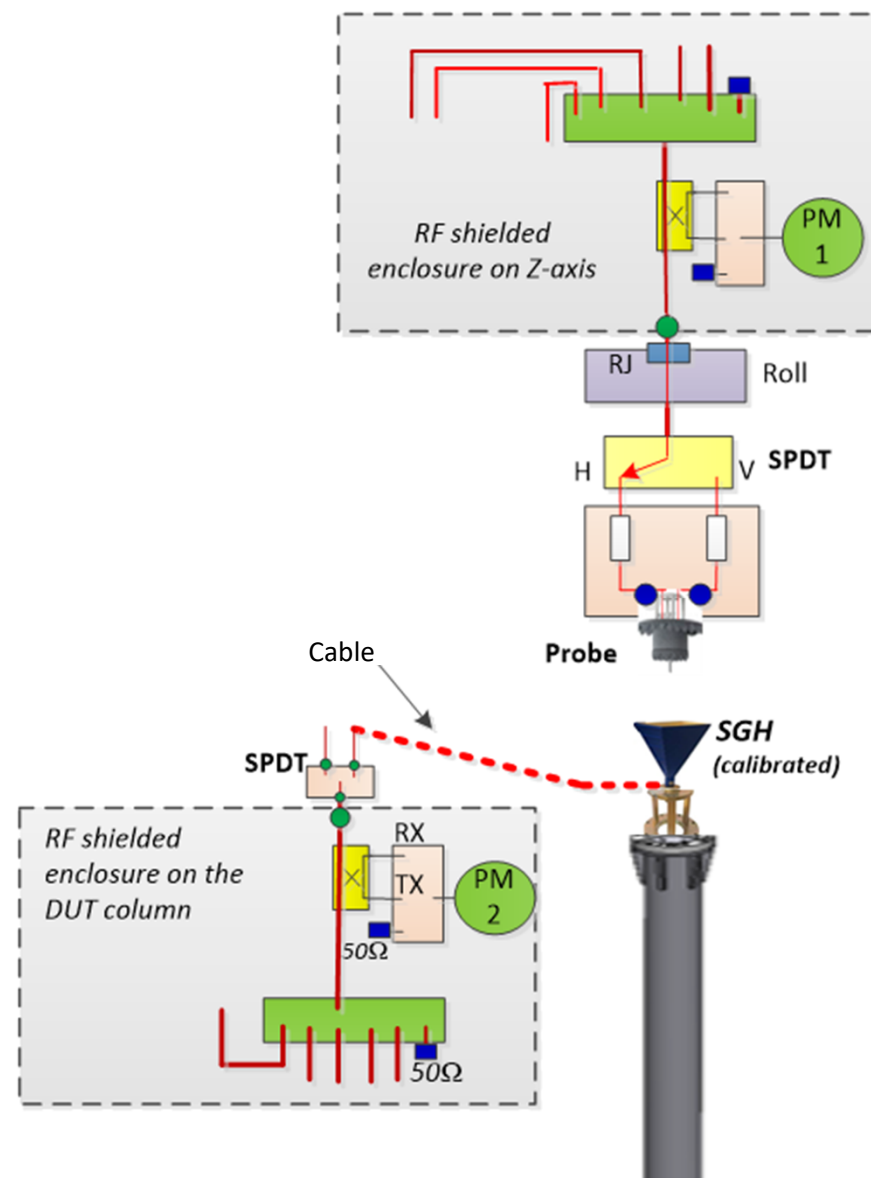
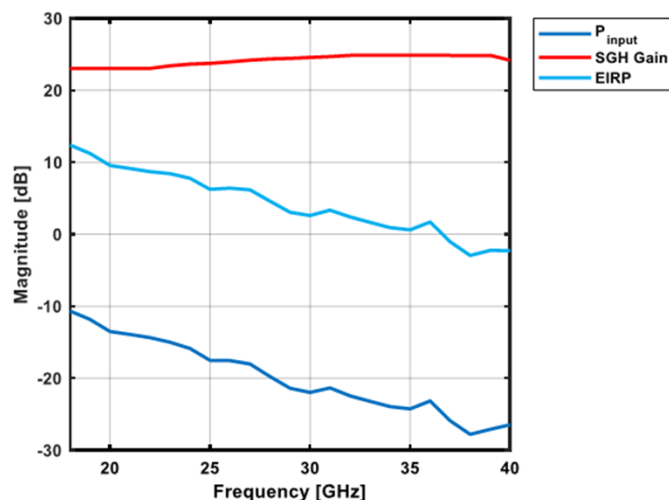
## EIRP measurements

- ▮ NF to FF far-field transform is used to determine the DUT Gain
- ▮ Input power is computed by either:
  - ▮ Direct Connection of the Cable with PXI in SA mode
    - ▮ Required cable to calibrated out
  - ▮ Power Meter measurement at PM2
    - ▮ Requires calibration path through the coupler.

EIRP is computed as:

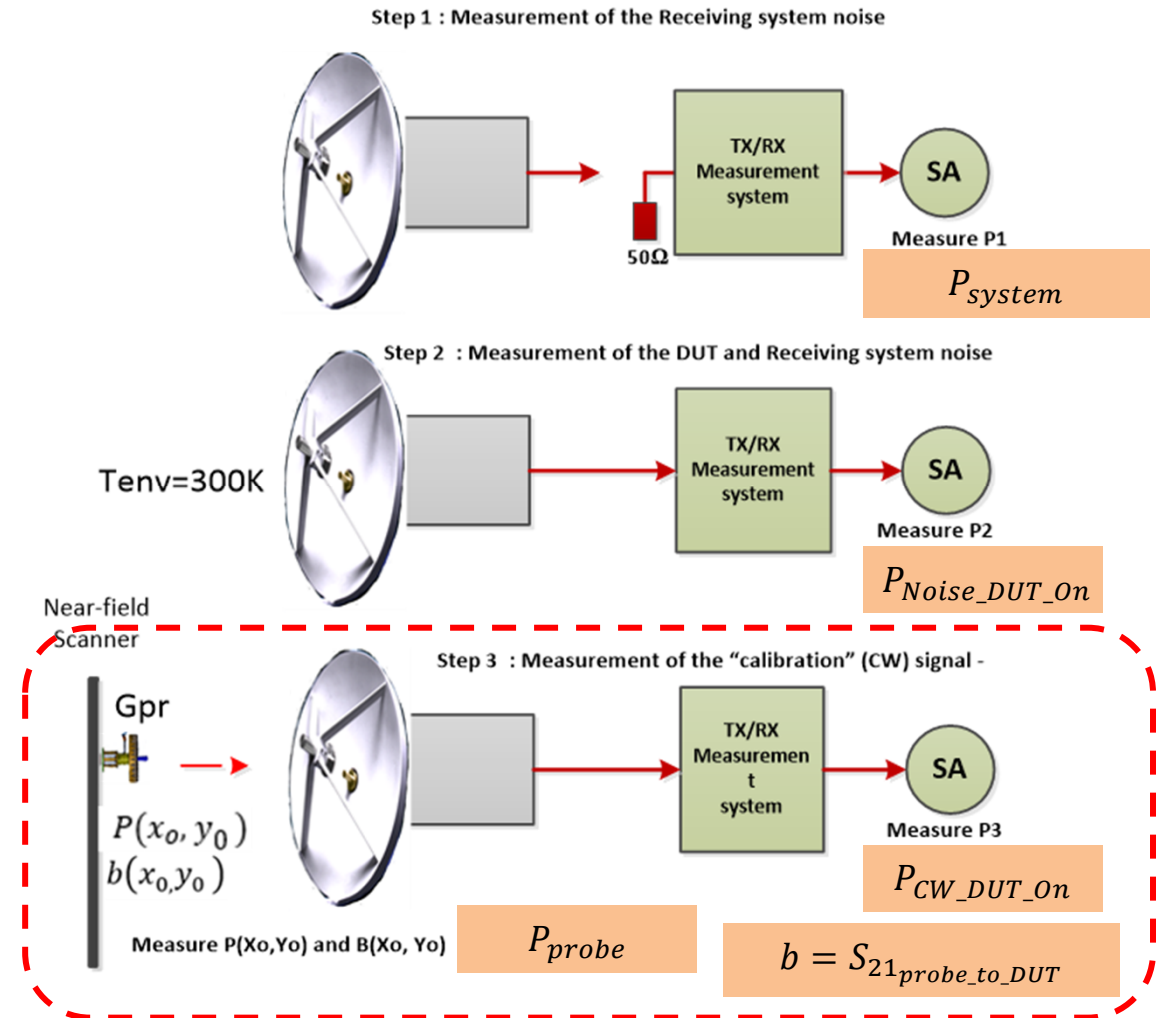
$$EIRP = G_{DUT} P_{in}$$

Example EIRP Measurement at Ka-Band using an SGH 2200



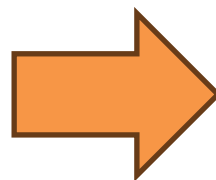
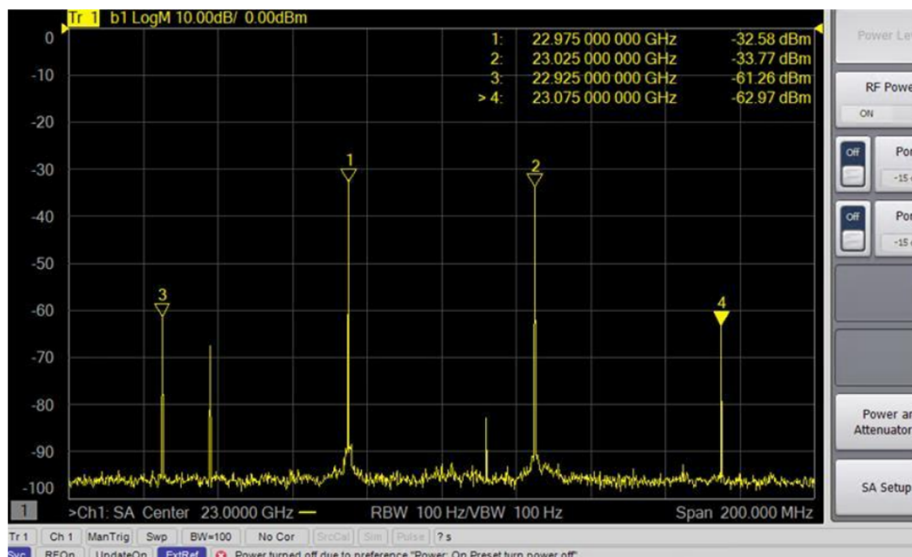
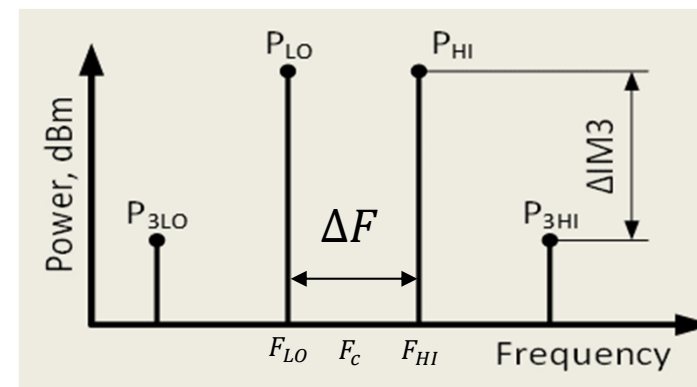
- ❑ Perform NF Acquisition
  - ❑ Perform NF-to-FF Transform: **FF(K)**
- ❑ Use  $b_0$  finder to get peak-near field  $x_0, y_0$ 
  - ❑ Store  **$b(x_0, y_0)$**  value from near-field data
- ❑ Move Probe into  $(x_0, y_0)$  position, collect Probe Side Power Meter Measurement ( **$P_{pr}(x_0, y_0)$** ) (**RF Source is ON**)
  - ❑ Power meter measurement assumes it is calibrated through the coupler path properly with a correction table.
  - ❑ Transmit amp should have low harmonic content.
- ❑ Collect Measured DUT received power with Spectrum Analyzer (**P3**) (**RF Source is ON**)
- ❑ **Turn RF source off**, collect DUT (and test equipment) noise power with Spectrum Analyzer (**P2**)
- ❑ **Turn DUT power off** (or connect a load to the SA input), collect noise power of test equipment with Spectrum analyzer (**P1**).
- ❑ Compute G/T metric
  - ❑ **B** = 1 Hz, **k** =  $1.380649 \times 10^{-23}$  joule per kelvin
  - ❑  **$M_{G/T}$**  = 1 (or can be measured, optionally)

$$G/T = \frac{kB}{M_{G/T} \cdot P_{pr}(x_0, y_0)} \cdot \frac{1}{b^2(x_0, y_0)} \cdot \left( \frac{P_3 - P_2}{P_2 - P_1} \right) \cdot FF(K)$$

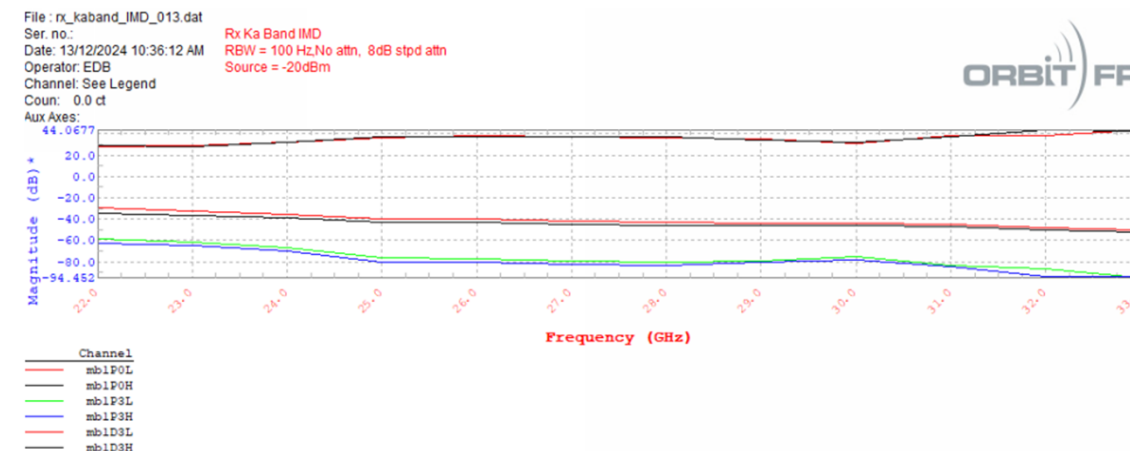


# Intermodulation Distortion (IMD) Mode

- ΔIM3 using OTA measurements can be performed using the Dual PXI-Setup
  - DUT PXI using IMD Mode
  - Scanner PXI in SA mode
- These measurement can be performed in two modes:
  - Swept Frequency, Fixed Delta
  - Swept Delta, Fixed Center Frequency



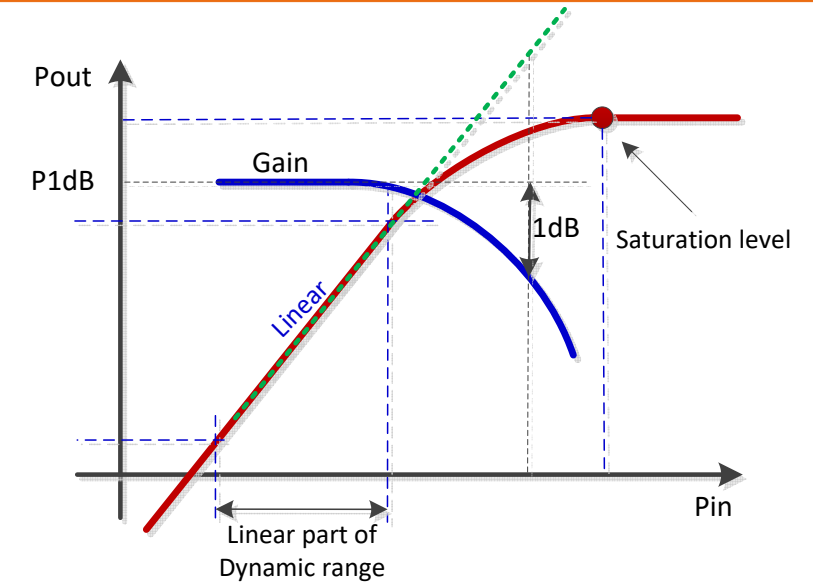
Swept Data Reported in 959 Spectrum



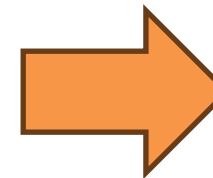
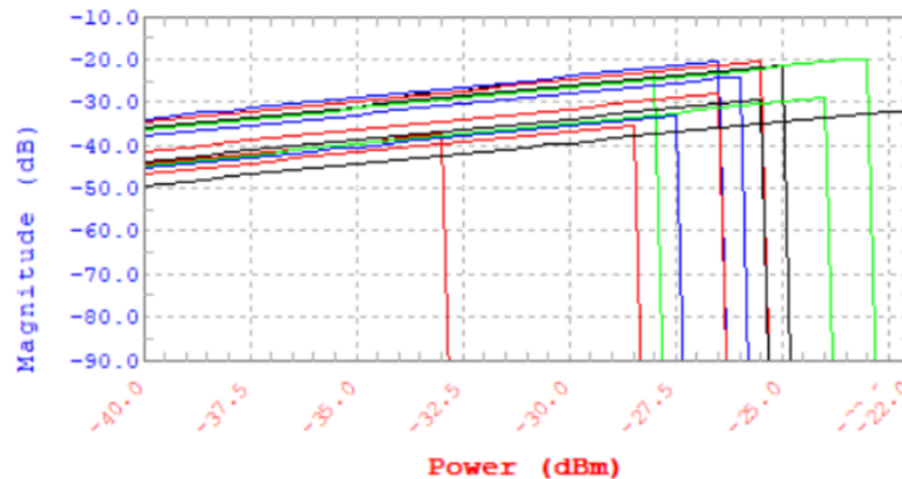


# Gain Compression (P1dB) Parameter

- Gain Compression is performed by sweeping the input power of the DUT until a compression point is hit.
  - Power increment and compression point is specified by the user.
- Data collection is automated using 959 Spectrum
  - Power sweeps are conducted to find compression point
  - The Next frequency is measured



Swept Data Reported in 959 Spectrum



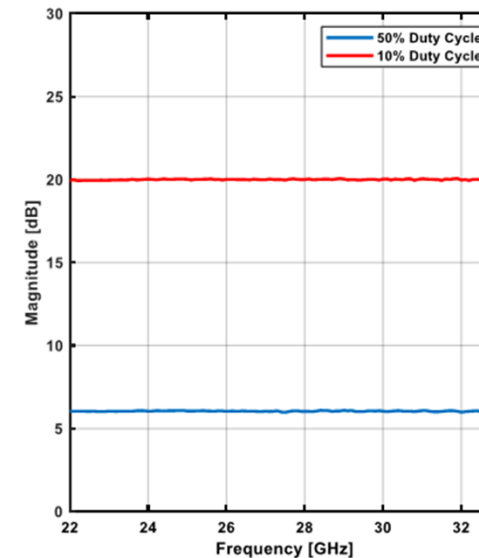
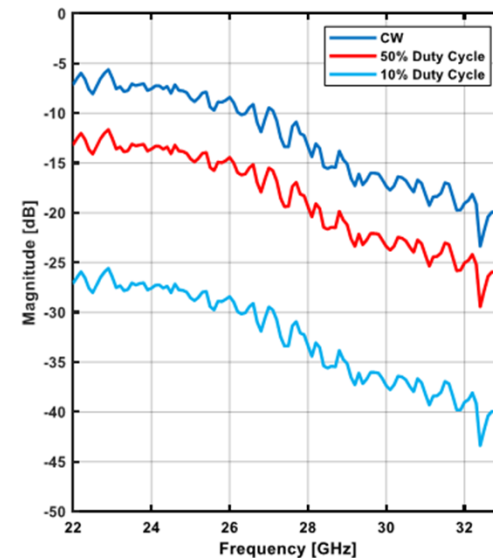
Frequency (GHz)	IP1dB
21	-26.5
22	-28
23	-26.5
24	-25.5
25	-25
26	-23
27	-26
28	-26.5
29	-25.5
30	-24
31	-27.5
32	-28.5

## Pulsed RF can be performed in two ways

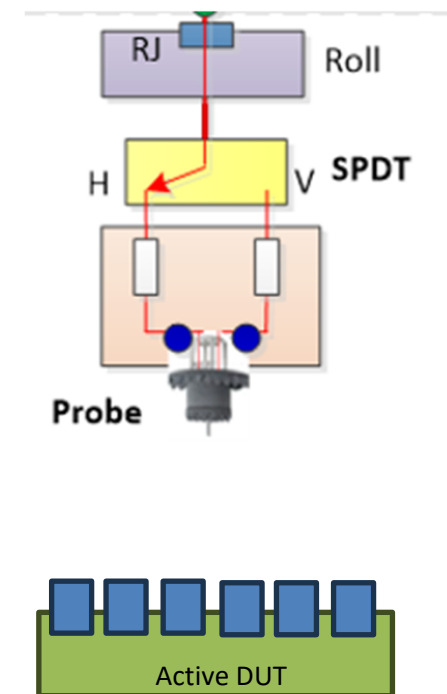
- With PXI internal pulsing Hardware
  - Test and Reference Paths are both pulsed
    - Due to down conversion hardware.
- External Pulsing Switch with PXI as pulse modulator
  - Test Path Pulse, Reference Path is not.

Description	Typical
Minimum pulse width	200 ns
Minimum pulse period	1 $\mu$ s
Maximum pulse period	10 s

Example Boresight Measurement Showing Duty Cycle Hits Due to Pulsing



- / Primarily for active antenna array calibrations
- / Probe moves to designated X,Y Coordinate and performs test
  - / Each X,Y coordinate has a list of unique DUT coordinates
    - / This enables the measurement unique DUT states
    - / Probe parks over an active antenna element
      - / Cycles through the phase shifter or attenuator states
    - / Moves to next element and does an repeats





# Uncertainty Analysis

- Uncertainty Analysis was Conducted at 8 Different frequency bands at the following frequencies
- Uncertainty based on NIST nearfield 18-term error model [3] and IEEE STD 1720
- Values computed inside the valid angle

Band	Frequency Band	OTA Test Frequency	Source Frequency	DUT	Probe	Uncertainty Main Beam ( $2\sigma$ )	Uncertainty -30 dB SLL ( $2\sigma$ )
L	1-2 GHz	1.5 GHz	1.5 GHz	SGH112	DLP-PNF-100	-	-
S	2-4 GHz	3 GHz	2.5 GHz	SGH260	DLP-PNF-200	$\pm 0.277$	$\pm 1.379$
C	4-8 GHz	5.5 GHz	5 GHz	SGH395	DLP-PNF-400	$\pm 0.230$	$\pm 0.997$
Ku	8-18 GHz	8.5 GHz	8.5 and	SGH820	DLP-PNF-800	$\pm 0.444$	$\pm 1.060$
		15 GHz	15 GHz			$\pm 0.410$	$\pm 0.706$
Ka	18-40 GHz	23 GHz	23 and	SGH2650	DLP-PNF-1800	$\pm 0.442$	$\pm 0.855$
		30 GHz	30 GHz			$\pm 0.519$	$\pm 1.562$
Q	33-50 GHz	40 GHz	40 GHz	SGH3300	DLP-PNF-3300	-	-
V	50-75 GHz	60 GHz	10 GHz	SGH5000	OEW5000	$\pm 0.388$	$\pm 0.994$
W	75-110 GHz	90 GHz	15 GHz	SGH7500	OEW7500	$\pm 0.426$	$\pm 1.315$

- Probe Calibrations (1-4) and DUT calibrations (5,6)
  - Analysis based on UPM calibration data
- Alias (8) and Truncation (9)
  - Processing Errors due sampling and scan size
- Positioner Errors (10,11)
  - Laser tracker data used to perturb ideal data to run through the transform
- Probe-DUT Coupling Room Reflections (12)
  - $\frac{1}{4}$  wavelength offsets DUT offset from Probe
- Receiver Linearity (13)
  - Boresight Roll Method and Attenuator Checks

#	Uncertainty Term	Method of Evaluating
1	Probe relative pattern	Analysis, Probe Calibration Data
2	Probe polarization ratio	Analysis, Probe Calibration Data
3	Probe gain measurement	Analysis, Probe Calibration Data
4	Probe alignment error	Analysis, Mechanical SAT
5	Normalization constant	Analysis, SGH calibration data
6	Impedance mismatch factor	Analysis
7	DUT alignment error	Analysis, Hexapod Specs
8	Data point spacing (aliasing)	Measurement
9	Measurement area truncation	Measurement
10	Probe x, y-position errors	Analysis, Mechanical SAT
11	Probe z-position errors	Analysis, Mechanical SAT
12	Multiple reflections (probe/DUT)	Measurement
13	Receiver amplitude nonlinearity	Measurement
14	System phase error due to receiver phase errors, flexing cables/rotary joints, and temperature effects	Analysis from RF FAT Drift Measurements
15	Receiver dynamic range	Measurement
16	Room scattering	Measurement
17	Leakage and crosstalk	Measurement
18	Repeatability /Random errors in amplitude/phase	Measurement

## System Phase Errors (14)

- Drift testing

## Receiver Dynamic Range (15)

- Boresight Dynamic range measurements

## Chamber Scattering (16)

- Fixed DUT offset from Probe with  $\frac{1}{4}$  movement of probe and DUT Mast

## Leakage/Cross Talk (17)

- Near-Field Scan with terminated cable that attaches to DUT

## Repeatability/Random Errors (18)

- Back-to-Back measurement taken.

#	Uncertainty Term	Method of Evaluating
1	Probe relative pattern	Analysis, Probe Calibration Data
2	Probe polarization ratio	Analysis, Probe Calibration Data
3	Probe gain measurement	Analysis, Probe Calibration Data
4	Probe alignment error	Analysis, Mechanical SAT
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15	Receiver dynamic range	Measurement
16	Room scattering	Measurement
17	Leakage and crosstalk	Measurement
18	Repeatability /Random errors in amplitude/phase	Measurement



# Sample Uncertainty Analysis Results ( 2σ Results)

## Uncertainty Analysis at 5 GHz

Term #	Term Name	Δ Gain [dB]	Main Beam [dB]	Side-lobe@-30 [dB]	Side-lobe@-45 [dB]	Side-lobe ESS [dB]	Source of Data
Frequency/Polarization		5 GHz EΦ Polarization					
1	Probe Relative Pattern	N/A	N/A	±0.30	±0.45	N/A	Probe Calibration Data
2	Probe Polarization Ratio	NE	N/A	±0.002	±0.196	N/A	Probe Calibration Data
3	Probe Gain Measurement	±0.13	N/A	N/A	N/A	N/A	Probe Calibration Data
4	Probe Alignment Error	N/A	NE	±0.009	±0.012	N/A	Mechanical SAT
5	Normalization Constant	±0.12	N/A	N/A	N/A	N/A	SGH Calibration Data
6	Impedance Mismatch Factor	±0.138	N/A	N/A	N/A	N/A	Analysis
7	DUT Alignment Error	N/A	±0.001	±0.002	±0.012	-102.000	Hexapod Specifications
8	Data Point Spacing (Aliasing)	±0.008	±0.040	±0.190	±1.020	-63.090	Measurement
9	Measurement Area Truncation	±0.002	±0.193	±0.309	±1.608	-58.833	Measurement
10	Probe x,y-position errors	NE	±0.003	±0.027	±0.153	-79.991	Mechanical SAT/Analysis
11	Probe z-position errors	±0.003	±0.004	±0.016	±0.091	-84.533	Mechanical SAT/Analysis
12	Multiple Reflections (Probe/DUT)	±0.040	±0.068	±0.549	±2.713	-53.715	Measurement
13	Receiver Amplitude Nonlinearity	±0.026	N/A	N/A	N/A	N/A	Measurement
14	System Phase Error	NE	NE	±0.003	±0.015	-100.348	Measurement
15	Receiver Dynamic Range	N/A	NE	NE	±0.002	-120.188	Measurement
16	Room Scattering	±0.028	±0.050	±0.595	±2.916	-52.981	Measurement
17	Leakage and Crosstalk	±0.001	±0.001	±0.029	±0.112	N/A	Measurement
18	Random Errors	±0.012	±0.052	±0.420	±2.137	-56.090	Measurement
Total Error		±0.230	±0.220	±0.997	±4.389		

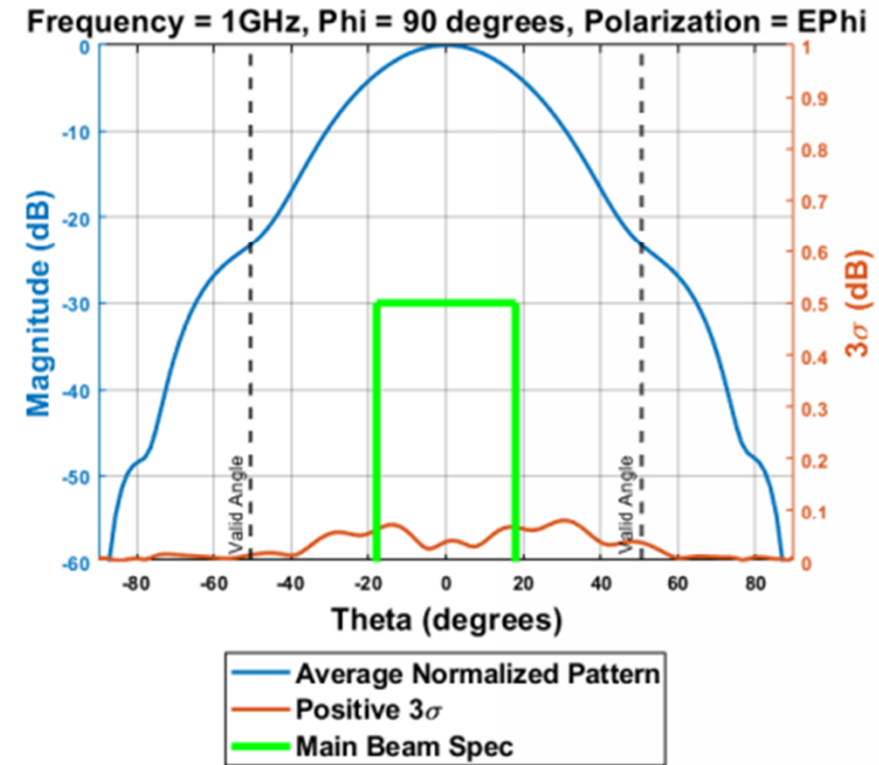
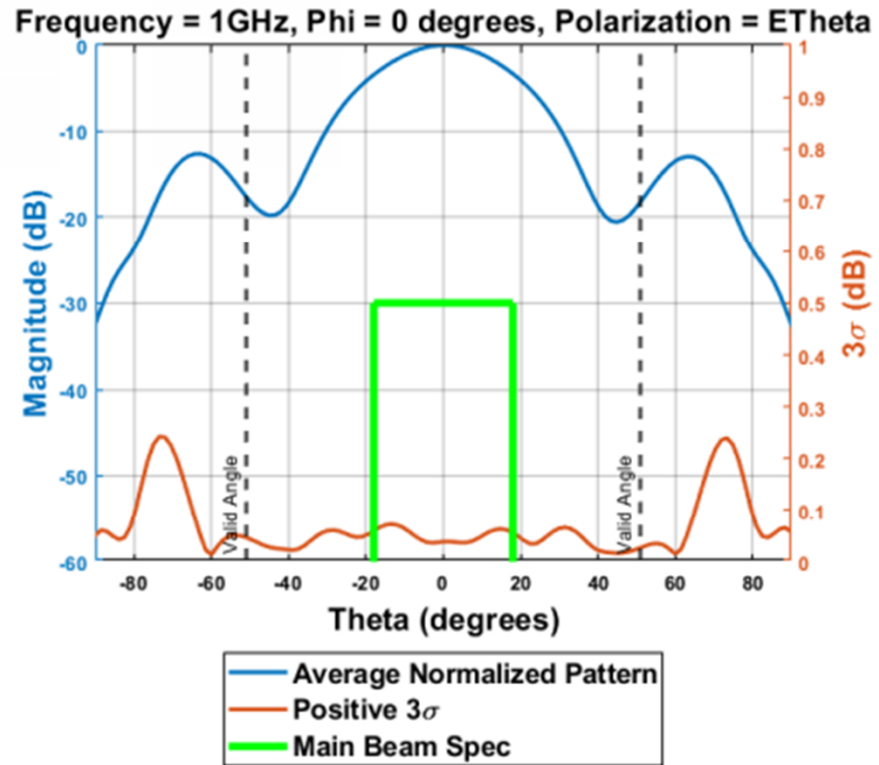
## Uncertainty Analysis at 90 GHz

Term #	Term Name	Δ Gain [dB]	Main Beam [dB]	Side-lobe@-30 [dB]	Side-lobe@-45 [dB]	Side-lobe ESS [dB]	Source of Data
Frequency/Polarization		90 GHz EΦ Polarization					
1	Probe Relative Pattern	N/A	N/A	±0.30	±0.45	N/A	Probe Calibration Data
2	Probe Polarization Ratio	NE	N/A	±0.007	±0.116	N/A	Probe Calibration Data
3	Probe Gain Measurement	±0.31	N/A	N/A	N/A	N/A	Probe Calibration Data
4	Probe Alignment Error	N/A	NE	±0.010	±0.016	N/A	Mechanical SAT
5	Normalization Constant	±0.15	N/A	N/A	N/A	N/A	SGH Calibration Data
6	Impedance Mismatch Factor	±0.129	N/A	N/A	N/A	N/A	Analysis
7	DUT Alignment Error	N/A	±0.001	±0.001	±0.008	-105.688	Hexapod Specifications
8	Data Point Spacing (Aliasing)	±0.013	±0.053	±0.285	±1.493	-59.540	Measurement
9	Measurement Area Truncation	±0.006	±0.066	±0.160	±0.865	-64.596	Measurement
10	Probe x,y-position errors	±0.014	±0.056	±0.389	±1.989	-56.789	Mechanical SAT/Analysis
11	Probe z-position errors	±0.006	±0.016	±0.044	±0.243	-75.957	Mechanical SAT/Analysis
12	Multiple Reflections (Probe/DUT)	±0.216	±0.185	±1.086	±4.854	-47.516	Measurement
13	Receiver Amplitude Nonlinearity	±0.009	N/A	N/A	N/A	N/A	Measurement
14	System Phase Error	±0.013	±0.020	±0.060	±0.335	-73.111	Measurement
15	Receiver Dynamic Range	N/A	NE	±0.003	±0.014	-100.802	Measurement
16	Room Scattering	±0.044	±0.046	±0.311	±1.620	-58.762	Measurement
17	Leakage and Crosstalk	±0.002	±0.093	±0.176	±0.913	N/A	Measurement
18	Random Errors	±0.024	±0.019	±0.413	±2.102	-56.25	Measurement
Total Error (RSS)		±0.426	±0.236	±1.315	±5.569		

# Antenna Gain Measurements

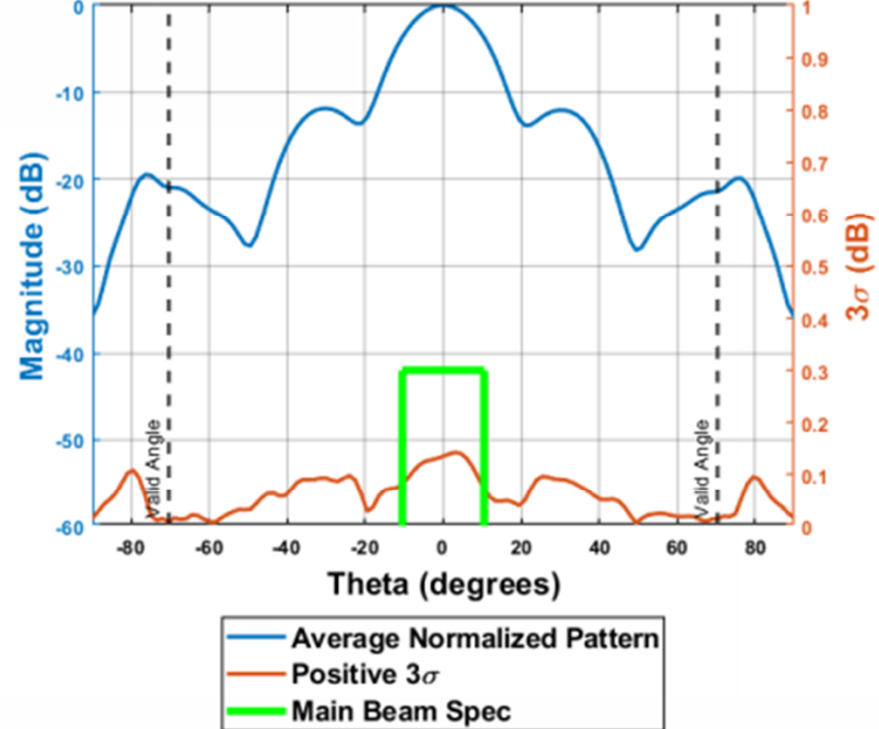
- 5 antenna measurements were taken at 1/8 wavelength Z-axis steps at each band
  - A mean of the 5 patterns was taken to determine the “Truth”
  - 3 $\sigma$  STD taken within the 3dB mean with was taken to determine a main beam metric
- Worst Case values for reported for Theta/Phi polarizations and band overlaps
  - Statement of work had a requirement to measure the 3 $\sigma$  gain accuracy
  - Compared 2 $\sigma$  values from the uncertainty analysis with the 3 $\sigma$  from the gain accuracy measurements
    - 3 $\sigma$  (99.7% confidence) should fall within the 2 $\sigma$  (95.4% confidence) interval

Band	Frequency Band	OTA Test Frequency	Source Frequency	DUT	Probe	Uncertainty Main Beam 2 $\sigma$ [dB]	Main Beam Gain Accuracy 2 $\sigma$ [dB]	Main Beam Gain Accuracy 3 $\sigma$ [dB]
L	1-2 GHz	1.5 GHz	1.5 GHz	SGH112	DLP-PNF-100	-	±0.089	±0.133
S	2-4 GHz	2.5 GHz	2.5 GHz	SGH260	DLP-PNF-200	±0.277	±0.095	±0.142
C	4-8 GHz	5 GHz	5 GHz	SGH395	DLP-PNF-400	±0.230	±0.095	±0.143
X	8-12 GHz	8.5 GHz	8.5 GHz	SGH820	DLP-PNF-800	±0.444	±0.061	±0.092
Ku	12.5-18 GHz	15 GHz	15 GHz	SGH1240	DLP-PNF-800	±0.410	±0.125	±0.187
Ka	18-40 GHz	23 GHz	23 GHz	SGH2650	DLP-PNF-1800	±0.442	±0.110	±0.165
		30 GHz	30 GHz			±0.519	±0.029	±0.348
Q	33-50 GHz	40 GHz	40 GHz	SGH3300	DLP-PNF-3300	-	±0.102	±0.153
V	50-75 GHz	60 GHz	10 GHz	SGH5000	OEW5000	±0.388	±0.102	±0.263
W	75-110 GHz	90 GHz	15 GHz	SGH7500	OEW7500	±0.426	±0.178	±0.267

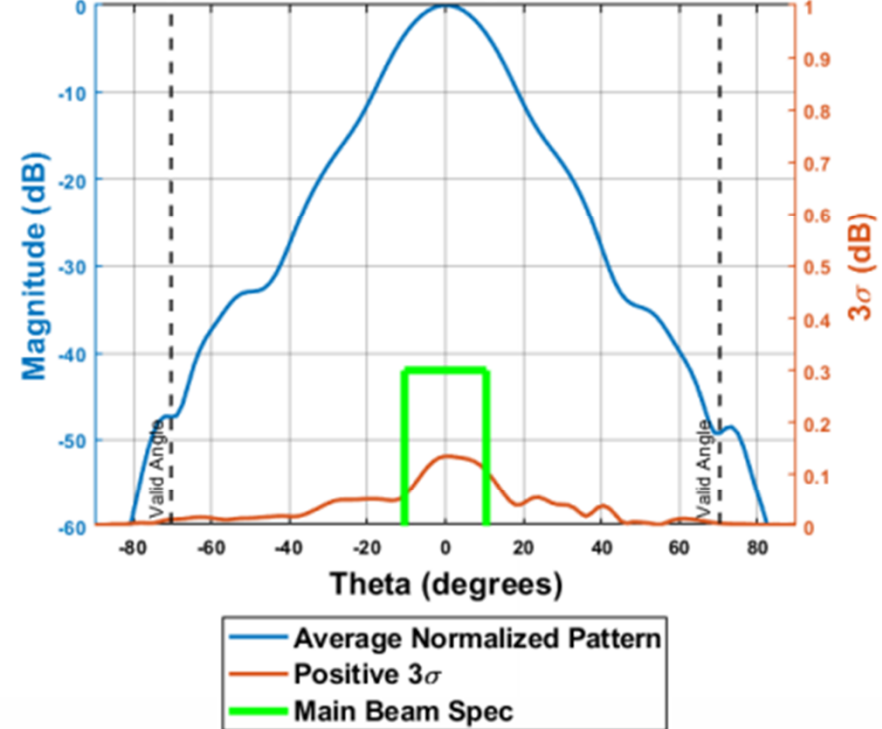




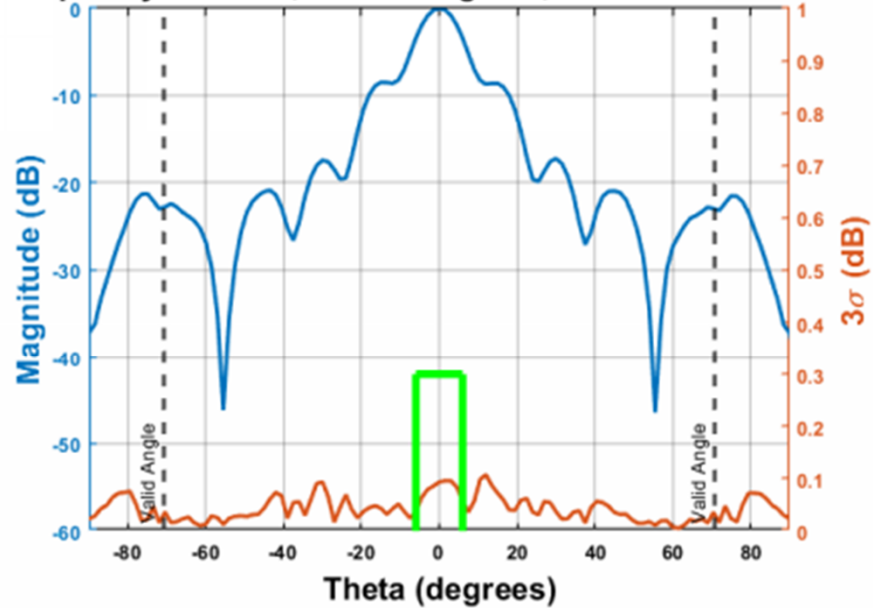
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Frequency = 5GHz, Phi = 90 degrees, Polarization = EPhi

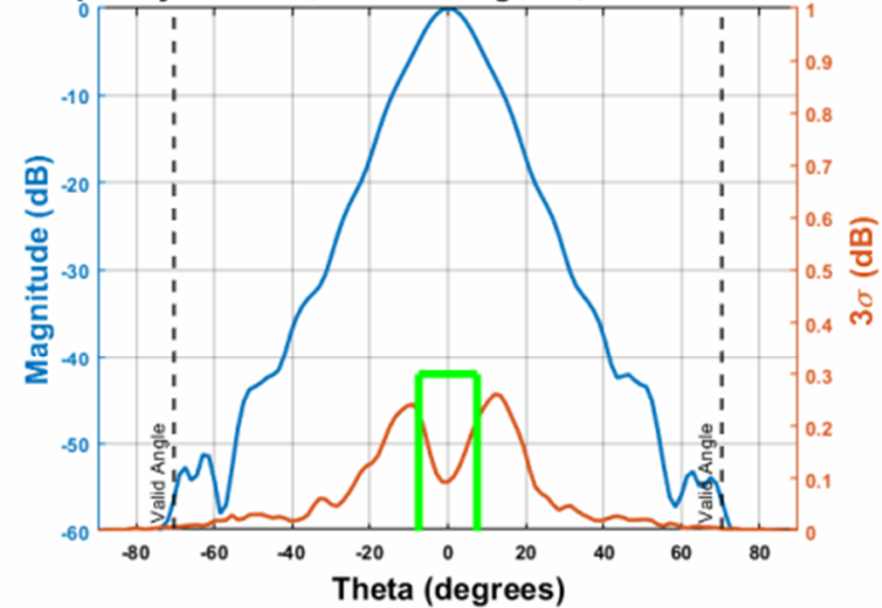


Frequency = 10GHz, Phi = 0 degrees, Polarization = ETheta



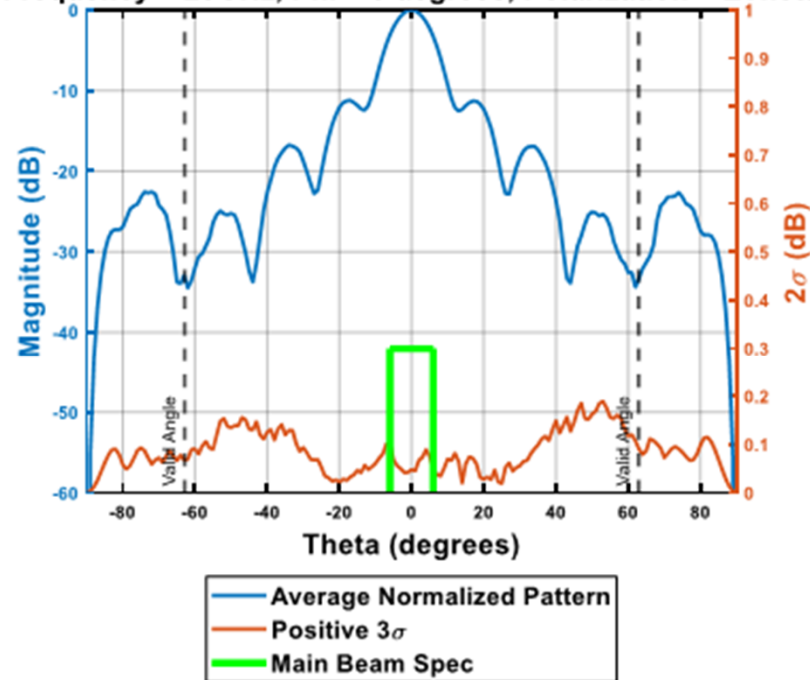
— Average Normalized Pattern  
— Positive 3σ  
— Main Beam Spec

Frequency = 10GHz, Phi = 90 degrees, Polarization = EPhi

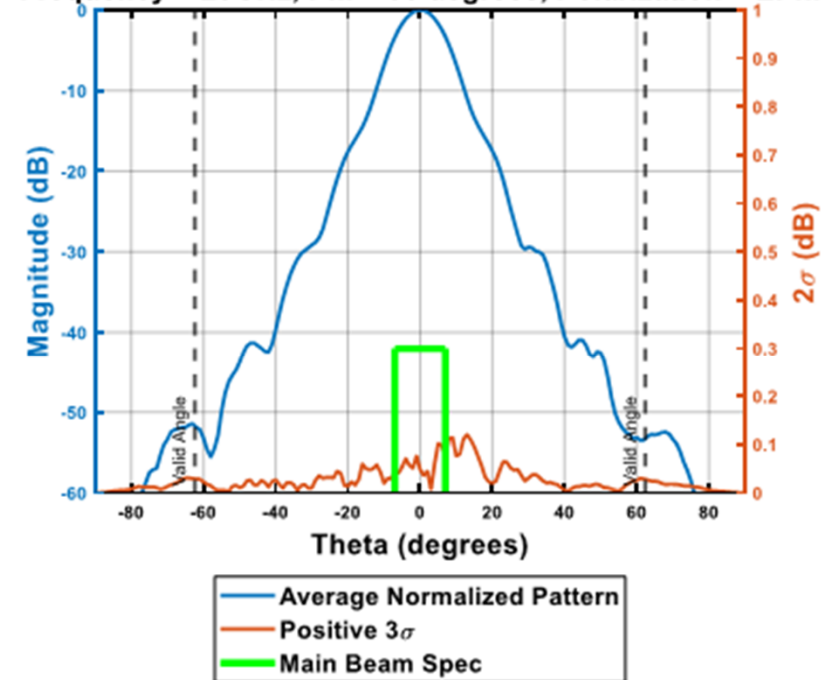


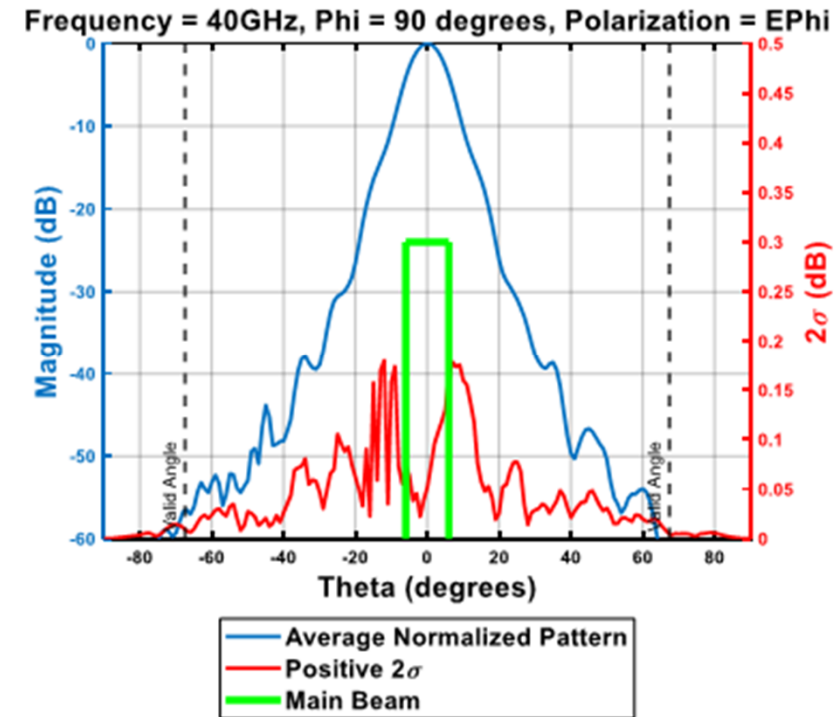
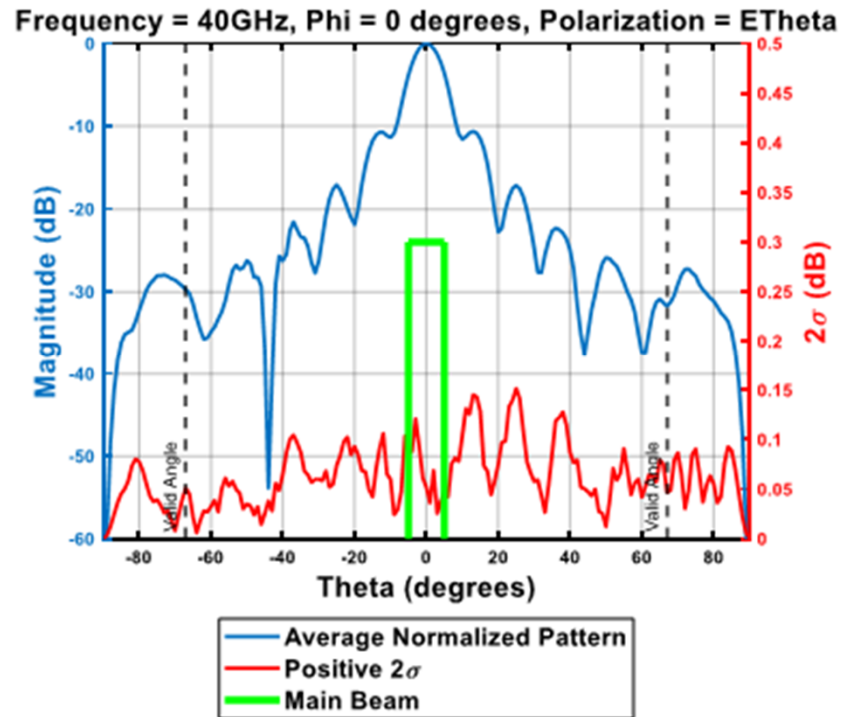
— Average Normalized Pattern  
— Positive 3σ  
— Main Beam Spec

Frequency = 20GHz, Phi = 0 degrees, Polarization = ETheta

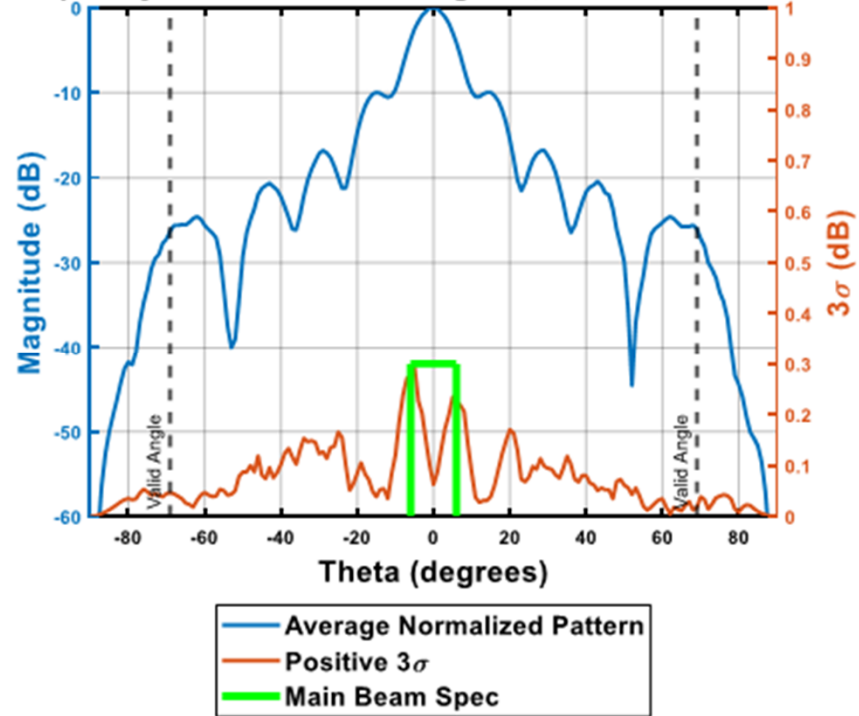


Frequency = 20GHz, Phi = 90 degrees, Polarization = EPhi

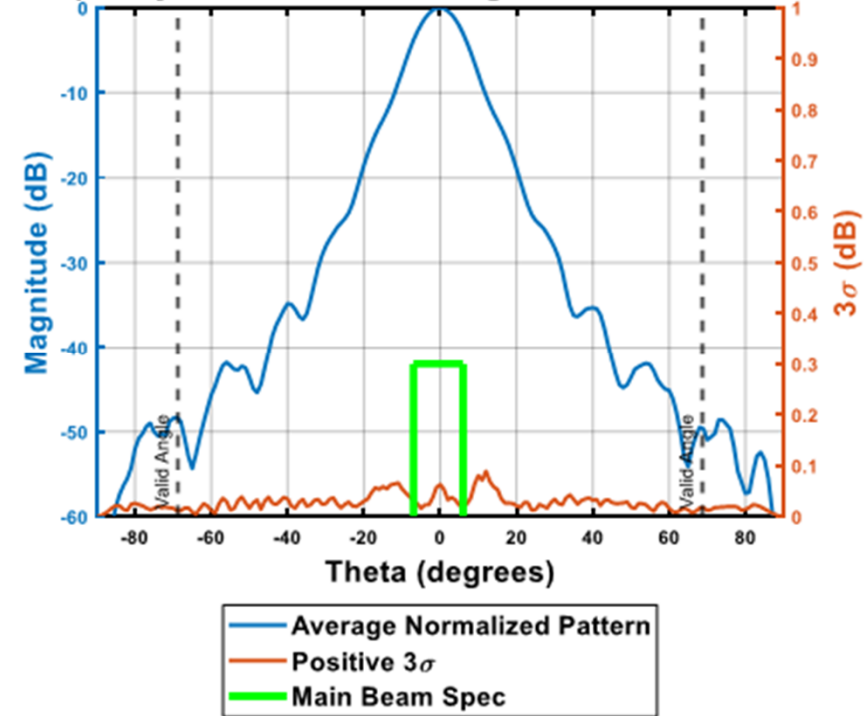




Frequency = 75GHz, Phi = 0 degrees, Polarization = ETheta

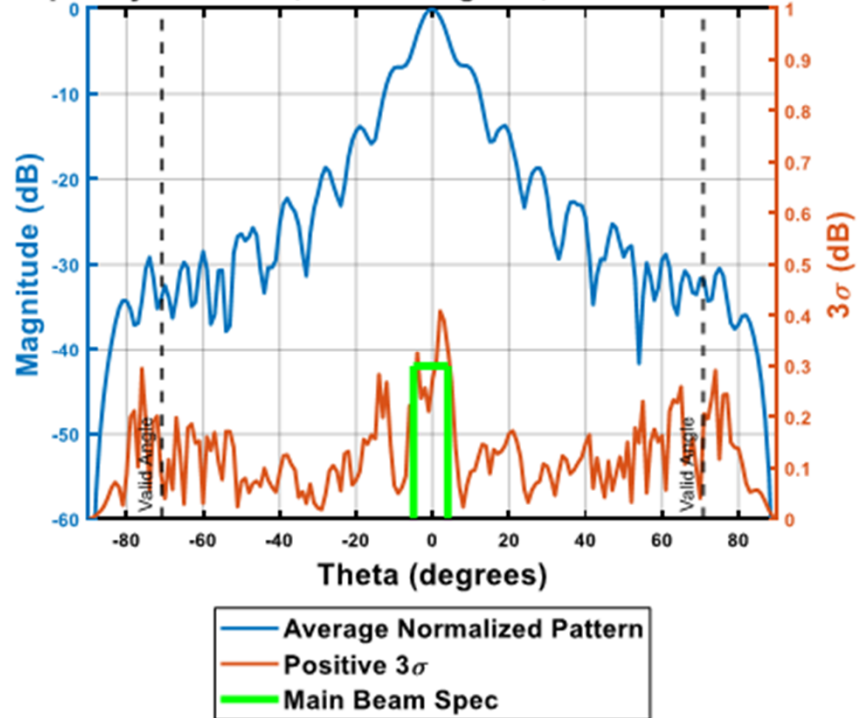


Frequency = 75GHz, Phi = 90 degrees, Polarization = EPhi

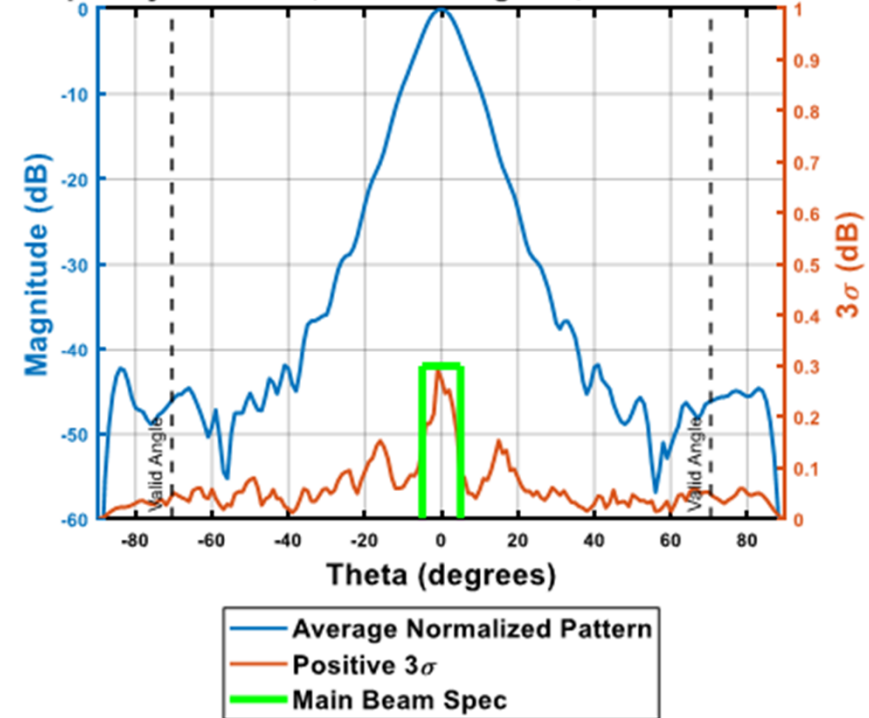




Frequency = 110GHz, Phi = 0 degrees, Polarization = ETheta



Frequency = 110GHz, Phi = 90 degrees, Polarization = EPhi



- NASA Commissioned a Large HPNF Measurement Facility
  - 10 m x 10 m Scan plane
  - 1 – 110 GHz
  - Antenna Gain Measurements and Radiation Patterns
  - Special Test modes
    - EIRP, G/T, IMD, Gain Compression, Pulsed Mode, Park and Probe
- Antenna Range is capable of measurement of very large antennas
  - DUT mast can be removed to allow for very heavy payloads on the floor
- Higher Frequency VDI units can further extend the maximum frequency range
- Future work can include integration of k-corrections for improvement on the measurement accuracies

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# Thank you Questions ?



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