

NASA Revolutionary Vertical Lift Technology Project

# Acoustic Assessment of an MD530F Helicopter in Maneuvering Flight

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# Overview

Test Description & Data Reduction

**Snapshot Array for Maneuvers** 

**Pitching Maneuvers** 

**Rolling Maneuvers** 

Conclusions





# Objective

Investigate methods to capture, process, and analyze noise emissions from unsteady flight conditions in preparation for future UAM/FVL flight tests.





# Test Description & Data Reduction

## Flight Test Description

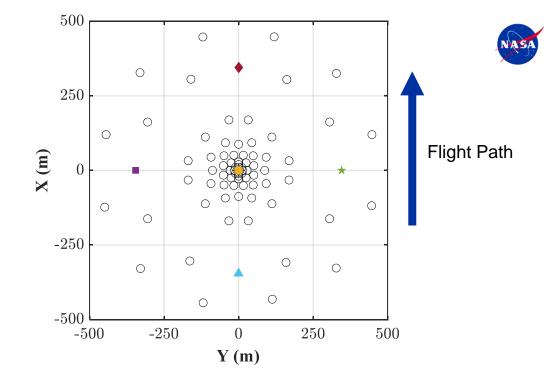
- Research methods for collecting UAM/FVL noise
- NASA/Army Comprehensive Rotorcraft Acoustic Flight Test Team (CRAFTT)
- Amedee Army Airfield at Sierra Army Depot
- 11 sorties over 6 flight days, total 21 flight hours
- MD530F helicopter
- 79-element microphone array
- Unsteady maneuvers flown
  - Initiated over array center
  - Two runs each
  - Pilot attempted 'single-input"
  - No adjustments to maintain speed or altitude

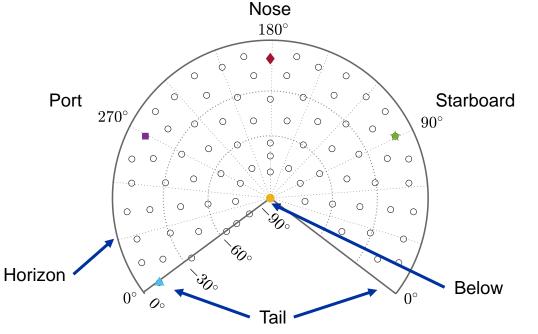


<b>Condition Code</b>	Description	Entry Speed	Entry Altitude
M1	Cyclic roll right, fast	75 kts	61 m AGL
M2	Cyclic roll left, fast	75 kts	61 m AGL
M3	Cyclic roll right, slow	75 kts	61 m AGL
M4	Cyclic roll left, slow	75 kts	61 m AGL
M5	Pitch up, cyclic	75 kts	61 m AGL
M6	Pitch up, collective	75 kts	61 m AGL
M7	Pitch up, cyclic and collective	75 kts	61 m AGL
L3	Steady, level flight	75 kts	61 m AGL

## Microphone Array

- Snapshot Array design
  - Mathematically defined distribution of points
  - Good hemispherical coverage at an instant in time
  - Does not rely on steady vehicle conditions throughout a flyover
- Ground-based coordinate system
  - +X: along flight path
  - +Y: to port (left)
  - +Z: up
- Vehicle state data collected by NASA's Aircraft Navigation and Tracking System (ANTS)
  - Vehicle position
  - Velocity
  - Accelerations
  - Pitch, roll, and heading





#### **Data Reduction**

#### NASA

#### - Timing

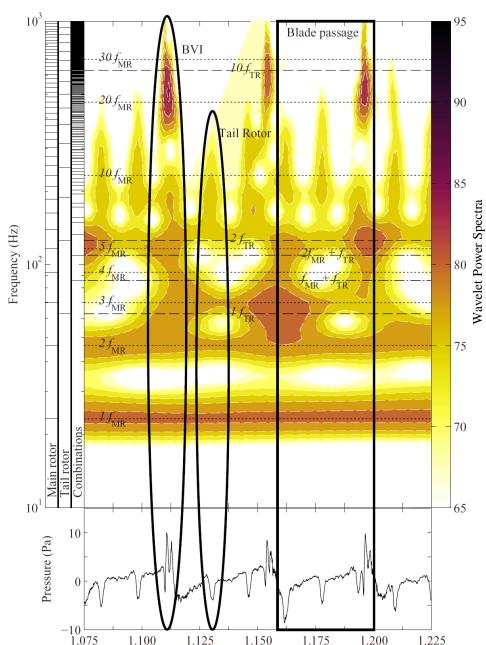
- All data recorded with UTC timestamps
- Acoustic, weather, and vehicle data time-synced
- Vehicle crosses center of array at t = 0 s

#### Vehicle state data

- Flight path angle (γ) and pitch (dα/dt) and roll (dφ/dt) rates calculated
- Effective flight path angle,  $\gamma_{eff}$ , accounting for acclerations

#### Acoustic data

- De-Dopplerized in time domain
- Pressure magnitudes distance-corrected to 30.48 m (100 ft) from vehicle
- Wavelet transform method used to extract Blade-Vortex Interaction (BVI) noise
  - Analyzes content in time domain
  - Converts pressure time history into wavelet power spectrum
  - Preserves content with:
    - Frequency > 6 x BPF of main rotor
    - Energy density > 6 dB of main rotor BPF



Time (s)

Stephenson (2014)

#### **Data Reduction**



#### - Timing

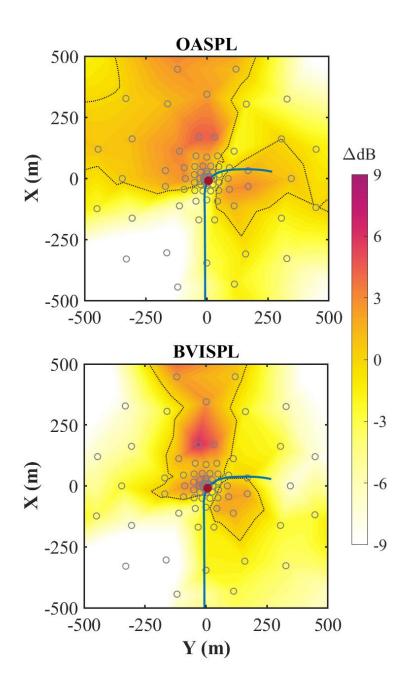
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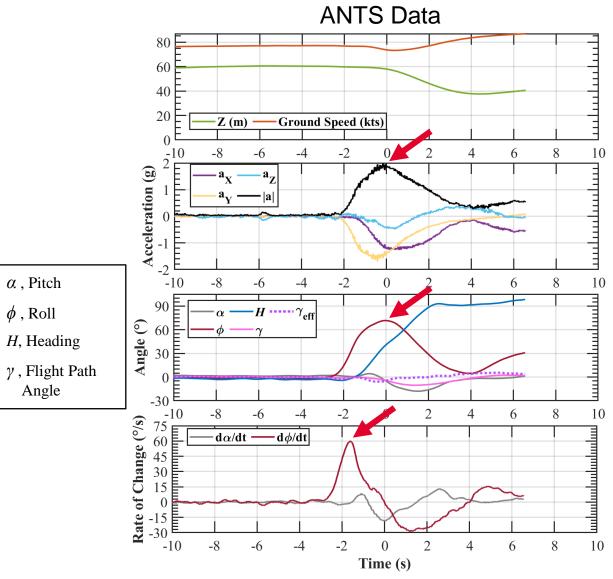
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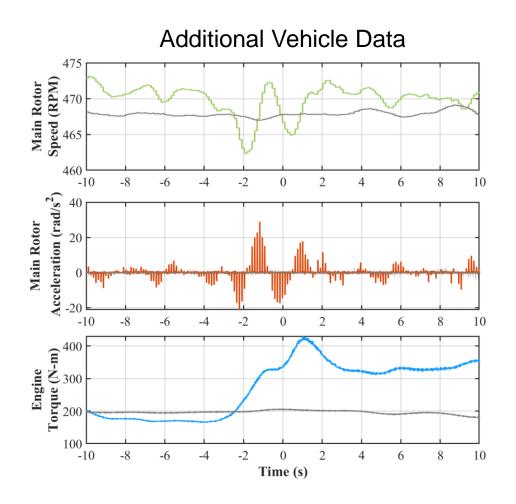
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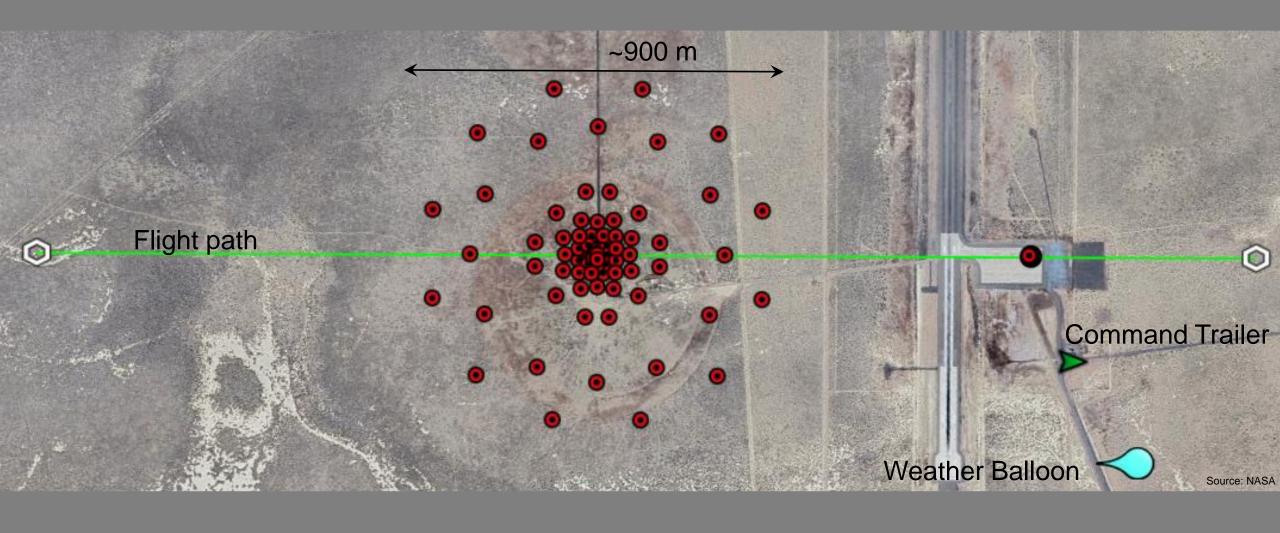


### Vehicle State Data – M1 Cyclic Roll Right





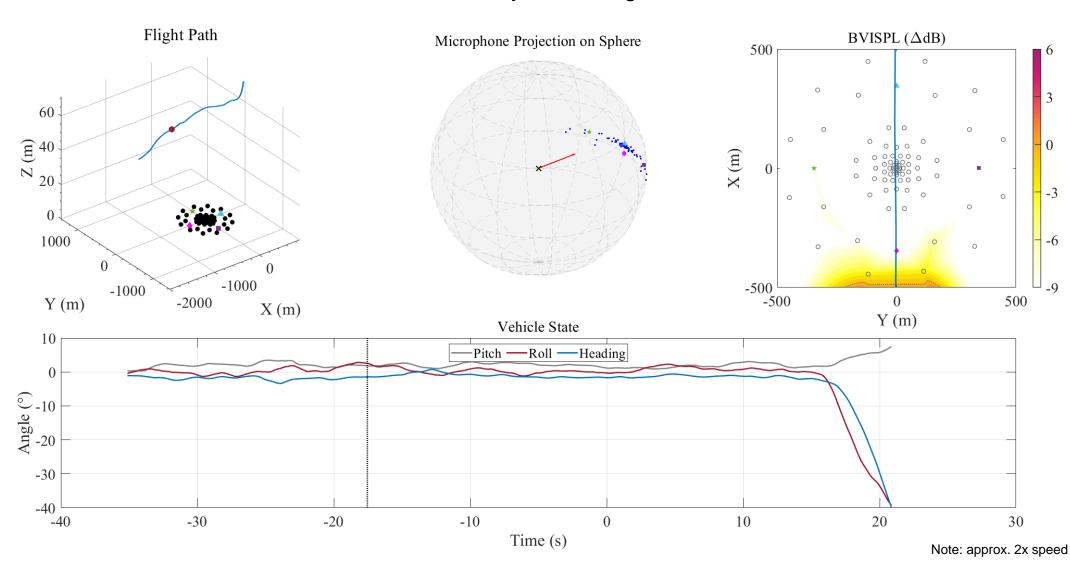




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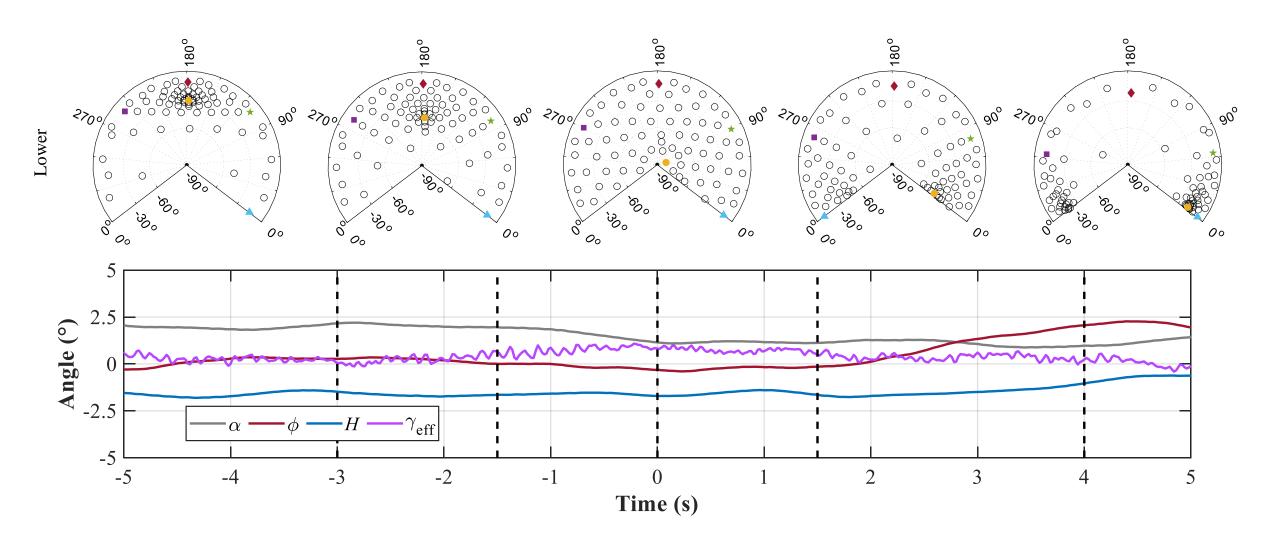


#### L3 – Steady, Level Flight



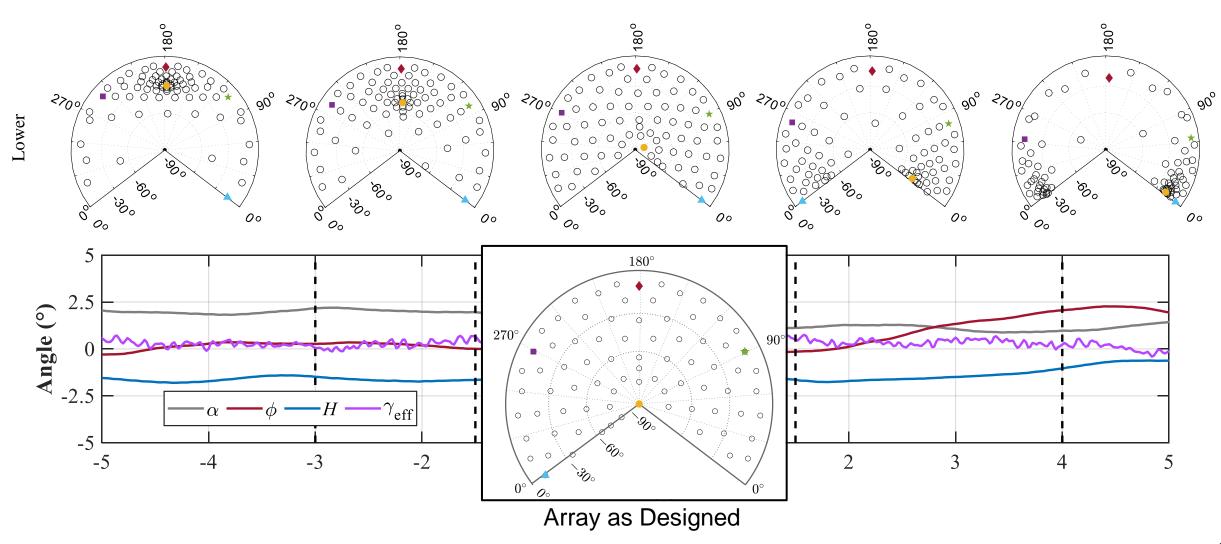


L3 – Steady, Level Flight



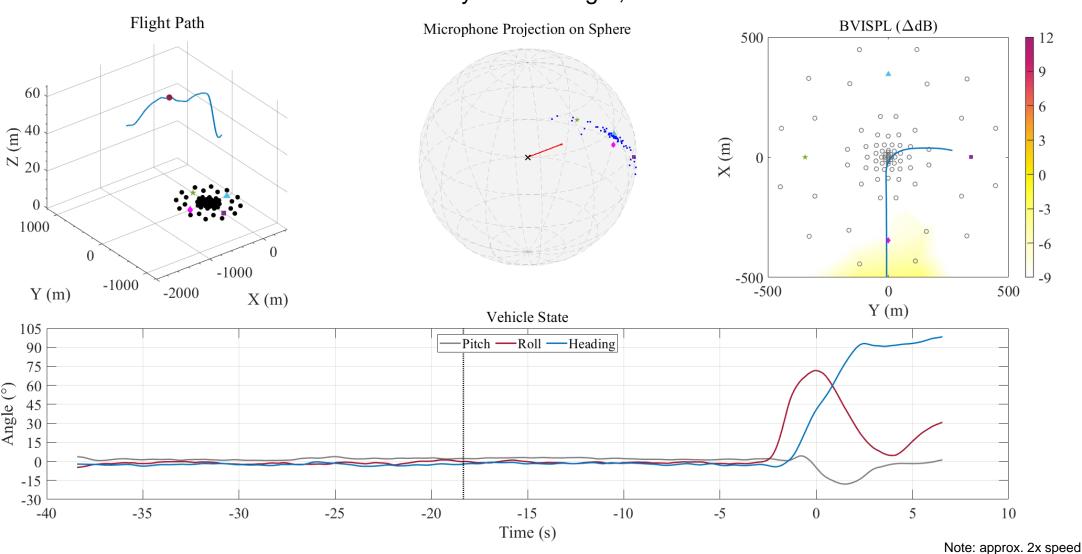


L3 – Steady, Level Flight



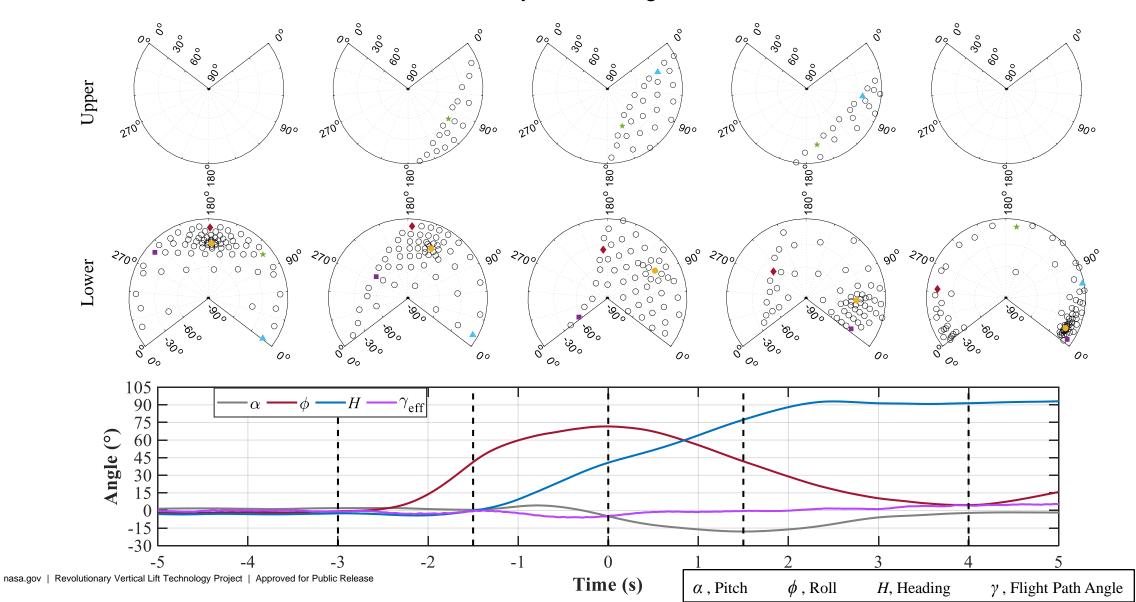


#### M1 – Cyclic Roll Right, Fast





L1 – Cyclic Roll Right, Fast





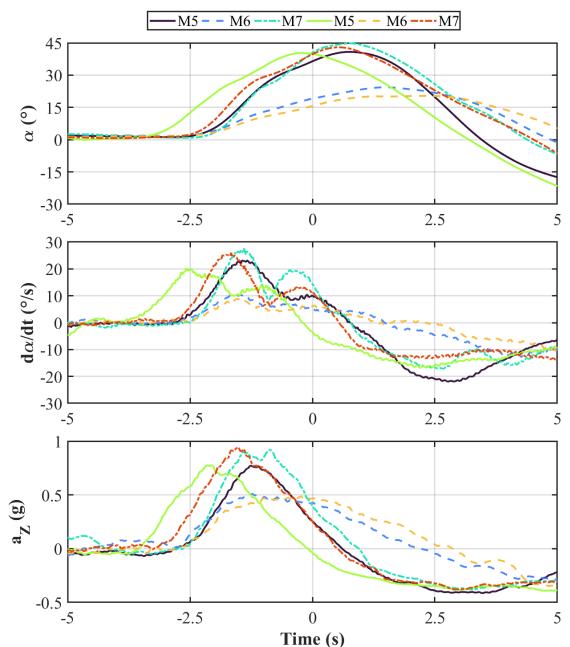
# Pitching Maneuvers

## Pitching Maneuvers



- Vehicle state data
  - Pitch-up maneuvers were fairly repeatable
  - Cyclic motion significantly more severe and dominated in combination flights
  - 'Double-hump' shape in  $d\alpha/dt$  likely due to thermals

M5	Cyclic
M6	Collective
M7	Cyclic & Collective



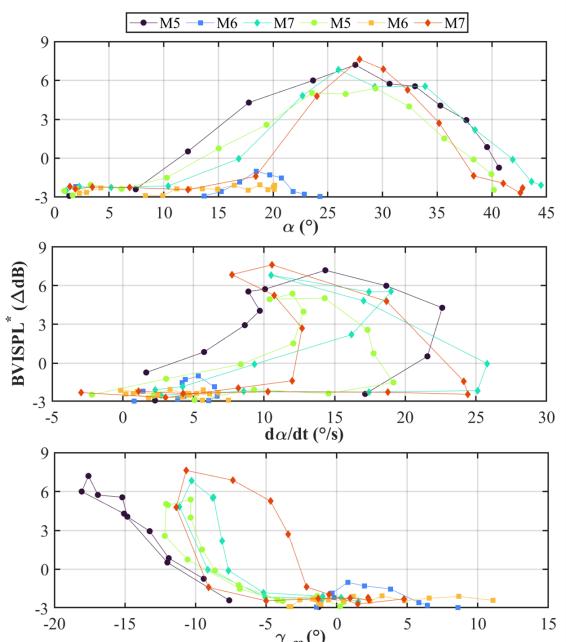
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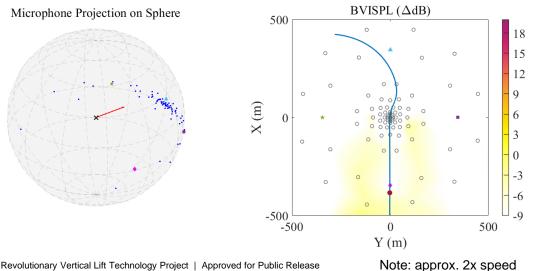
- Presence of BVI during pitching maneuver?
  - BVISPL\* is mean of BVISPL ≥ 3 dB across the array at a given time
  - Peak BVISPL\* did not occur at peak pitch angle or peak pitch rate
  - Peak BVISPL\* did occur at peak  $\gamma_{\it eff}$ , which accounts for accelerations

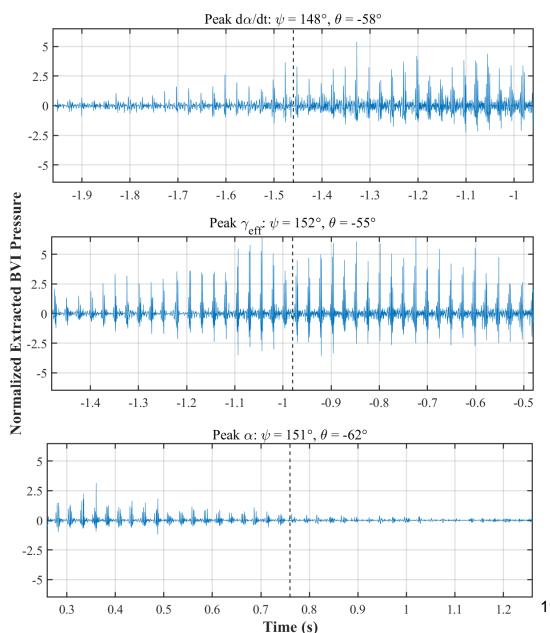
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M6	Collective	
M7	Cyclic & Collective	



## Pitching Maneuver – M5 Cyclic

- Identified directivity of peak BVISPL value
- Interrogated nearest mic to that emission angle at times of different peak values
  - Strong BVI presence at peak  $\gamma_{eff}$
  - Suggests acceleration is main driver of BVI
  - Weaker BVI presence *near* peak pitch rate
  - No discernable BVI around peak pitch angle
- Is wake above main rotor near the nose? Or is the rotor plane pitching fast enough to catch the wake near the tail?







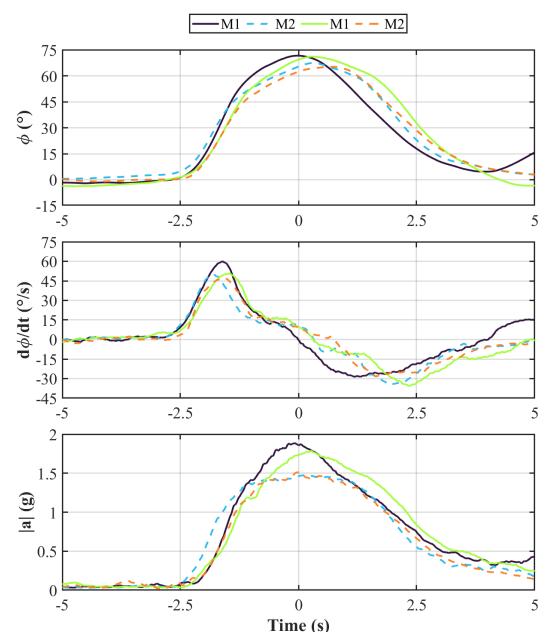
# Rolling Maneuvers

## Rolling Maneuvers



- Neglect slow rolls (M3, M4)
- Right vs. left turns repeatable and similar
- Effects on acoustics should be isolated to advancing vs. retreating side of the main rotor
- Expectation:
  - Strong BVI in rolls into advancing side
  - Weak to no BVI in rolls away from advancing side

M1	Roll right (into advancing side), fast
M2	Roll left (away from advancing side), fast

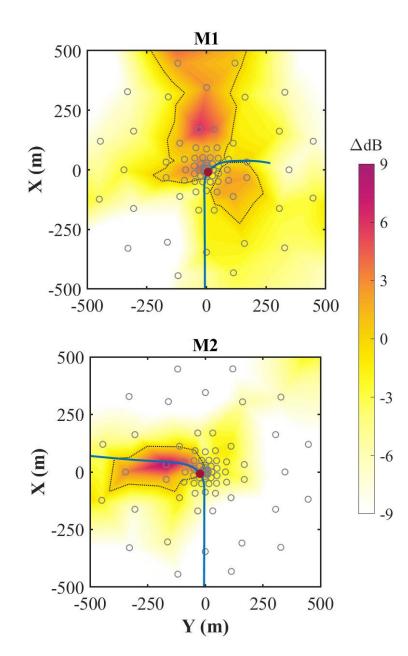


#### Rolling Maneuvers



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- Effects on acoustics should be isolated to advancing vs. retreating side of the main rotor
- Expectation:
  - Strong BVI in rolls into advancing side
  - Weak to no BVI in rolls away from advancing side
- Observed:
  - Similar BVI strength for both directions
  - More focused directivity for retreating-side roll

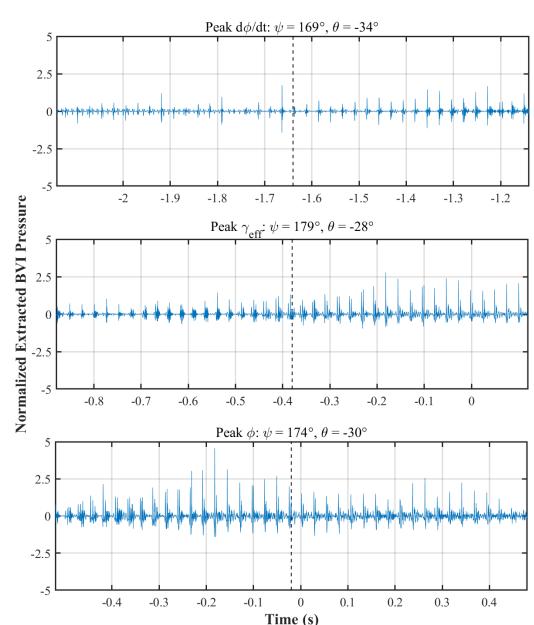
M1	Roll right (into advancing side), fast
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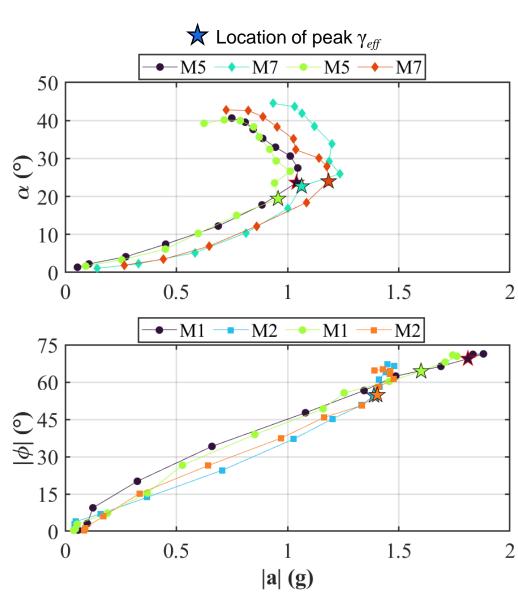
# Rolling Maneuver – M1 – Fast Right

- Same process as the pitching maneuver
  - Identified emission angle of peak BVISPL value
  - Interrogated nearest mic to that directivity at times of different peak values
- Different trends than pitch
  - No discernable BVI at peak roll rate
  - Weaker BVI presence *near*  $\gamma_{eff}$
  - Strongest BVI at peak roll angle, not associated with peak acceleration



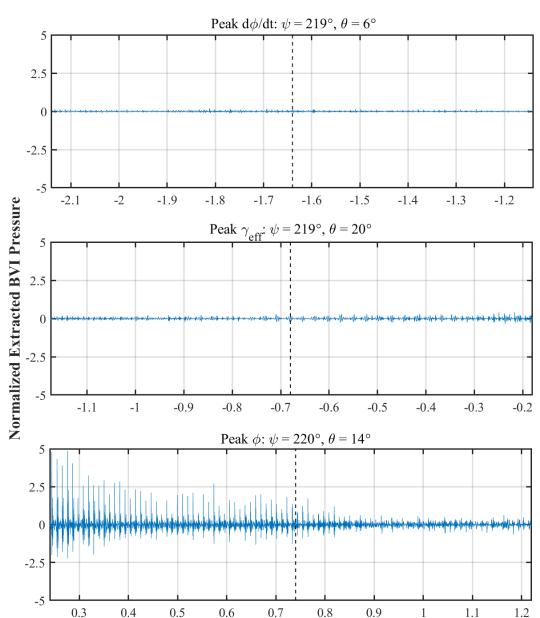
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- Same process as the pitching maneuver
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- Different trends than pitch
  - No discernable BVI at peak roll rate
  - Weaker BVI presence *near*  $\gamma_{eff}$
  - Strongest BVI at peak roll angle, not associated with peak acceleration
- Do these trends <u>disagree</u> with pitch?
  - Parabolic vs linear acceleration result of fighting gravity
  - M5 & M7: strongest BVI at peak  $\gamma_{eff}$
  - M1 & M2: strongest BVI at peak roll angle
  - Both correspond to peak total acceleration
  - Note, is close to peak |a| for M1 & M2, hence the weak BVI shortly after



#### Rolling Maneuver – M2 – Fast Left

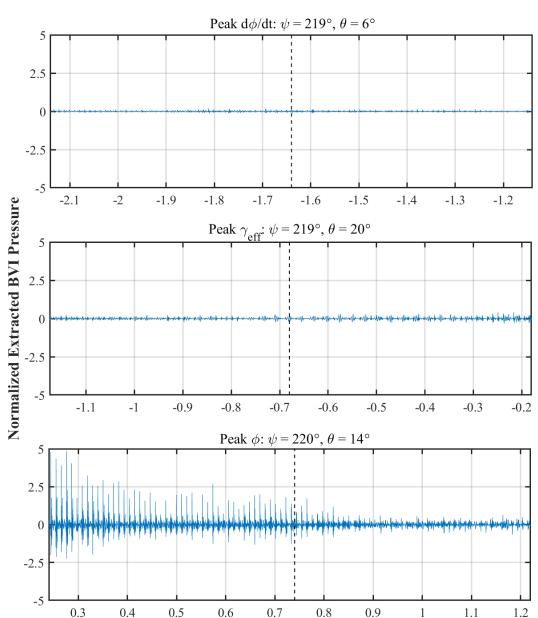
- Same process again
  - Identified emission angle of peak BVISPL value
  - Interrogated nearest mic to that directivity at times of different peak values
- Strong BVI present near peak roll angle



Time (s)

#### Rolling Maneuver – M2 – Fast Left

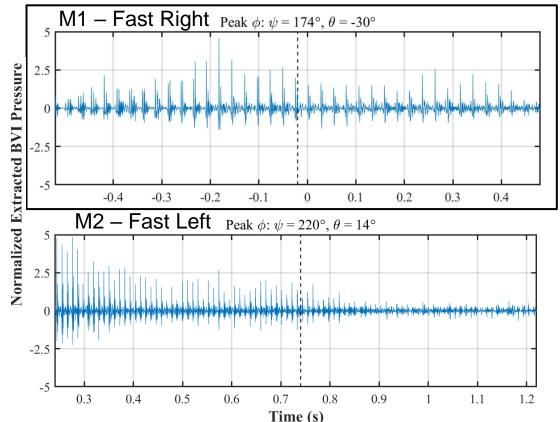
- Same process again
  - Identified emission angle of peak BVISPL value
  - Interrogated nearest mic to that directivity at times of different peak values
- Strong BVI present near peak roll angle
- Emission angle is wrong?
  - BVI expected to be ahead and below the vehicle, possibly favoring the advancing
  - M1 ✓
  - M2 **≭**



Time (s)

## Rolling Maneuver – M2 – Fast Left

- Same process again
  - Identified emission angle of peak BVISPL value
  - Interrogated nearest mic to that directivity at times of different peak values
- Strong BVI present near peak roll angle
- Emission angle is wrong?
  - BVI expected to be ahead and below the vehicle, possibly favoring the advancing
  - M1 ✓
  - M2 ×
- Period is wrong?
  - Main rotor BPF = 39.75 Hz  $\rightarrow$  T = 0.0252 s
  - Tail rotor BPF =  $94.9 \text{ Hz} \rightarrow \text{T} = 0.0105 \text{ s}$
- M2 is exhibiting BVI associated with the tail rotor
  - Directivity would be ahead and below from the tail rotor plane ✓
  - Tail rotor wake pushed towards starboard
  - Yawing motion during roll left could lead to tail rotor interacting with its own wake → BVI



#### Conclusions



- Snapshot Array
  - Well-suited to unsteady conditions
  - Limitations at large pitch/roll angles inherent in ground mics
- BVI present in all severe maneuvers (M1, M2, M5, & M7)
  - Main rotor BVI during rolls towards advancing side expected
  - Main rotor BVI during pitch-up maneuvers
  - Wake above rotor near nose during level flight?
  - Rotor plane pitches quickly enough to catch wake near tail?
  - BVI during roll towards retreating side appears to be tail rotor BVI
  - Strong BVI occurs at or near peak acceleration for all cases

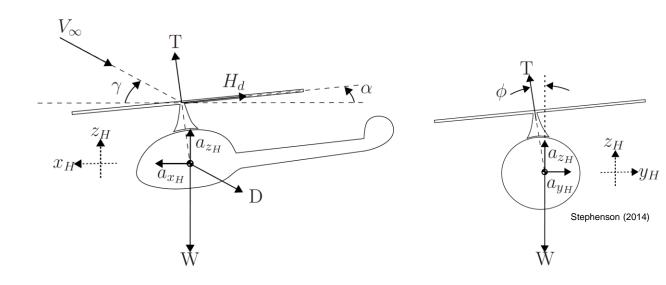
#### Questions?

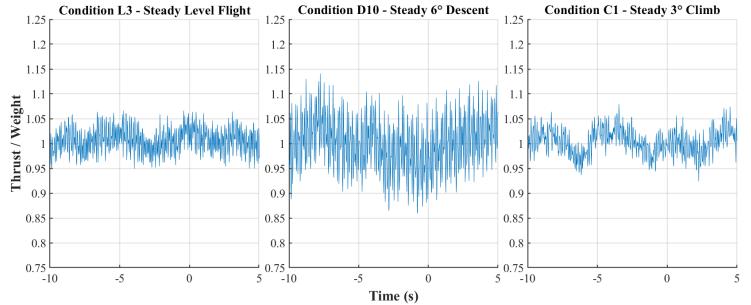


#### Calculating Main Rotor Thrust



- Goal was to use <u>only</u> ANTS data to estimate rotor thrust
  - Position, velocity, acceleration in (x, y, z)
  - Roll, pitch, and heading angles
- Applied to steady flight conditions
- Compared to CAMRAD II results with 3% -5% error





$$0 = T\cos\alpha\cos\varphi - Th\sin\alpha - Td\sin\gamma - W(1 - \frac{a_z}{g})$$
$$0 = T\sin\alpha\cos\varphi + Th\cos\alpha - Td\cos\gamma + W^{a_x}/g$$

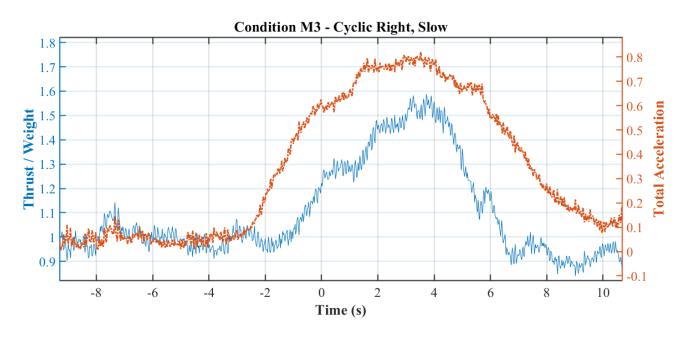
Stephenson (2014)

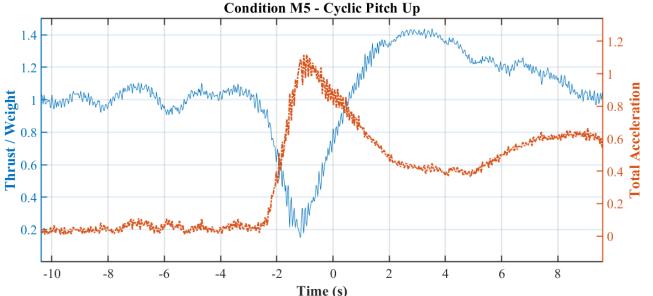
$$h = \frac{\sigma C_{d_0} \mu}{4} \qquad \qquad d = \frac{f_e \mu^2}{2A}$$

#### Calculating Main Rotor Thrust



- Applied method to unsteady maneuvers
- Still working on CAMRAD II inputs for maneuvers
- Comparison of T/W and |a|
  - F = ma
  - Additional force (thrust) should be proportional to additional acceleration
- Slow roll maneuvers appear reasonable
- Aggressive (cyclic) pitch-up maneuvers appear reasonable





## Calculating Main Rotor Thrust



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- Still working on CAMRAD II inputs for maneuvers
- Comparison of T/W and |a|
  - F = ma
  - Additional force (thrust) should be proportional to additional acceleration
- Slow roll maneuvers appear reasonable
- Aggressive (cyclic) pitch-up maneuvers appear reasonable
- Fast roll maneuvers appear incorrect
- Centripetal force due to roll?
  - Using center of roll as R is wildly wrong
  - Is it better modeled as hanging mass, so R is distance from  $c_a$  to center of rotor?

