

# Design of a Magnetically-Geared Actuator for Extremely Cold and Dusty Space Environments

Justin J. Scheidler<sup>1</sup>

**Aaron D. Anderson**<sup>1</sup>

Thomas F. Tallerico<sup>1</sup>

Peter A. Hoge<sup>2</sup>

George R. Harpster<sup>2</sup>

Kyle R. Whitling<sup>2</sup>

Jesse Hawk<sup>2</sup>

Malcolm Robbie<sup>2</sup>

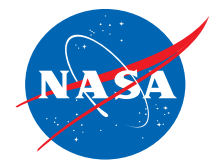


<sup>1</sup>NASA Glenn Research Center, Cleveland, USA



<sup>2</sup>HX5, LLC, Brook Park, USA

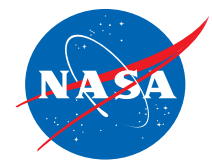
*Notice for Copyrighted Information This manuscript is a joint work of employees of the National Aeronautics and Space Administration and employees of HX5, LLC under Contract No. 80GRC020D0003 with the National Aeronautics and Space Administration. The United States Government may prepare derivative works, publish, or reproduce this manuscript and allow others to do so. Any publisher accepting this manuscript for publication acknowledges that the United States Government retains a non-exclusive, irrevocable, worldwide license to prepare derivative works, publish, or reproduce the published form of this manuscript, or allow others to do so, for United States government purposes.*



# Agenda

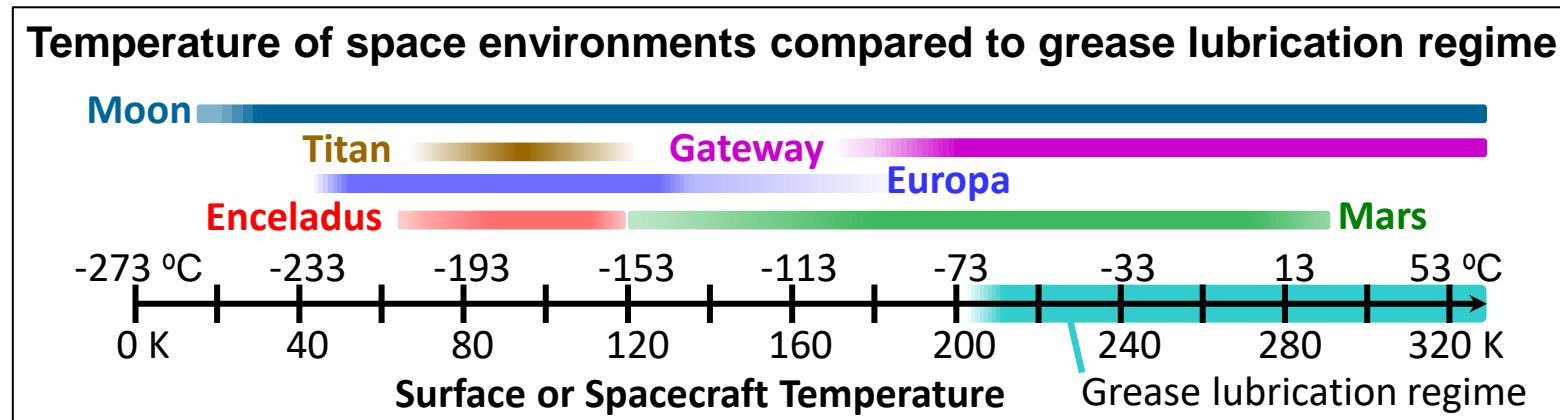
---

- Motivation
- Actuator overview
- Detailed design
  - Electromagnetic
  - Bearing
  - Thermal
  - Mechanical
- Predicted performance
- Conclusions



# Motivation

- Rotational actuators almost always require a mechanical gearbox to meet mass, volume requirements
- Challenging to lubricate a gearbox operating in cold environments
  - Pervasive problem – *potential for big impact*



- Objective: enable operation in cold to extremely cold environments...
  - Without the mass, complexity, & energy/efficiency penalties of heating actuators
  - Without the strict design constraints & life limitations of solid lubricated gears



# Motors for Dusty & Extremely Cold Environments (MDECE) Project

---

- **R&D & ground test project, 2020 – 2025**
- **Goal:** Develop 2 unheated rotational actuators that can operate for a long duration in extreme cold (ambient temperature of  $-243\text{ }^{\circ}\text{C}$  (30 K))
- **Approach:** Eliminate gear lubrication:
  - 1 magnetically-gearred actuator with non-contact gearing
  - 1 piezoelectric actuator with no gears (not discussed in this presentation) [1]
- **Relevant environment:** Broadly applicable, but focusing on permanently shadowed regions on lunar surface
- **Promising applications:** rover mobility ▪ in-situ resource utilization ▪ robotic arm joints (magnetic actuator) rotors for powered flight

This presentation only covers the magnetically-gearred actuator

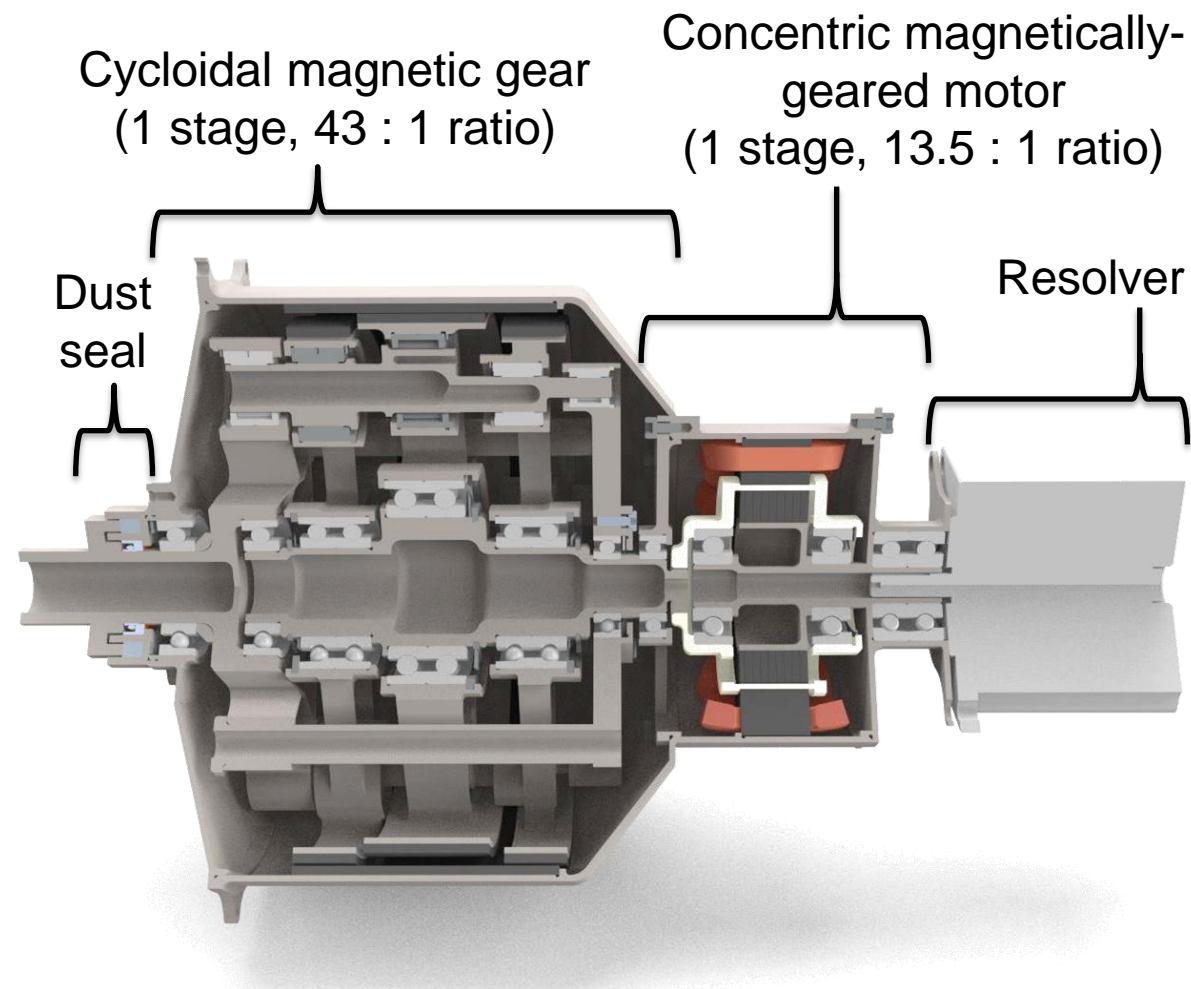
1. Badescu, M. et al., "Piezoelectric motor for cryogenic applications," Proc. SPIE Smart Structures + Nondestructive Evaluation, 2024.



# Actuator Overview

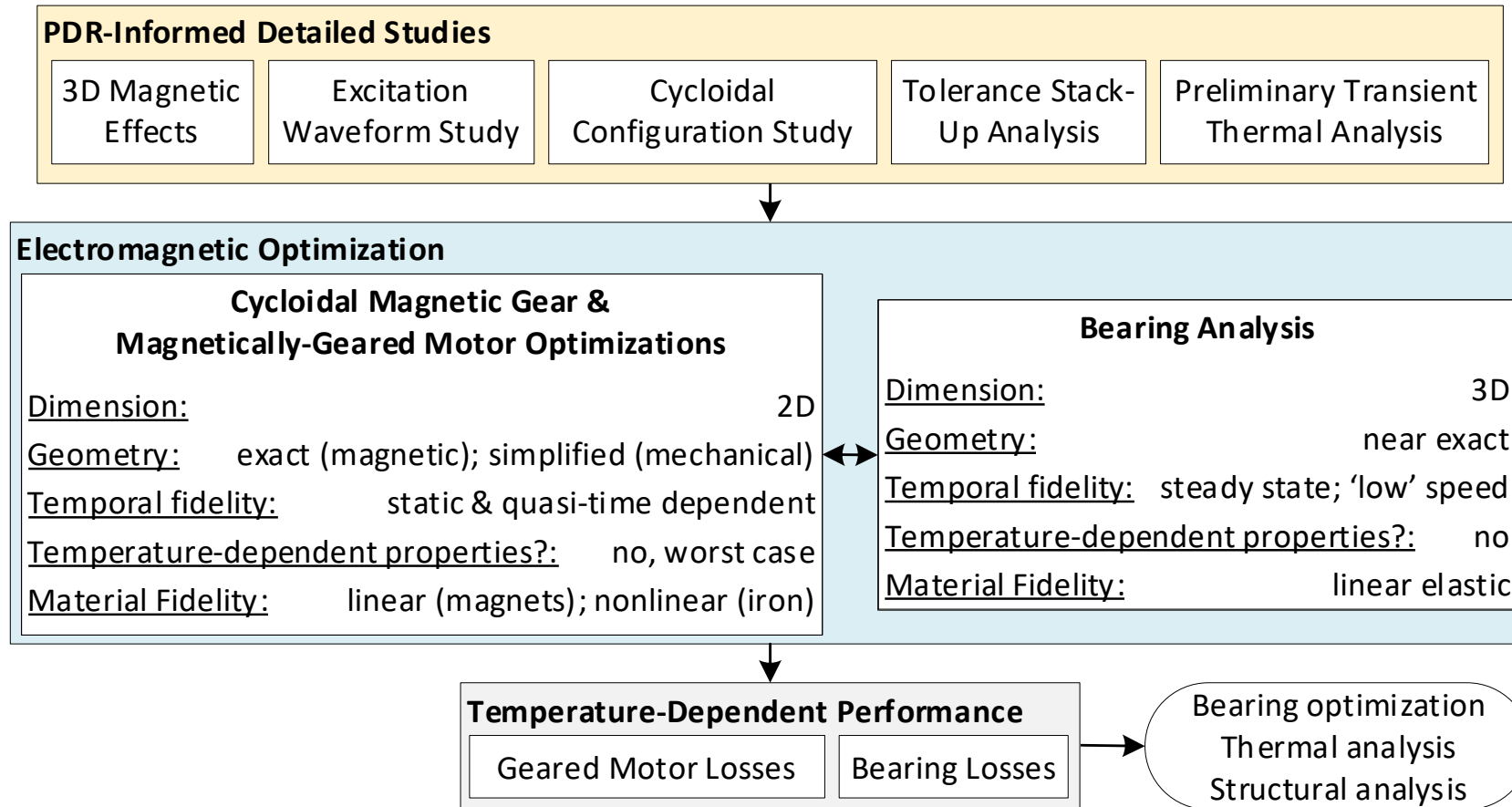
## Driving requirements

- **Thermal:** Operate unheated  
-165 °C to < -243 °C ambient surface
- **Mechanical:** 105 Nm at 2 rpm continuous (22 W)  
208 Nm at 1.5 rpm (33 W) for 60 s
- **Efficiency:** 60% to >80% continuous
- **Life:** 6k to > 50k output revolutions
- **Size/mass:** No strict requirements (TRL 2-5)  
4.73 kg to < 3.15 kg  
1440 cm<sup>3</sup> to < 960 cm<sup>3</sup> envelope





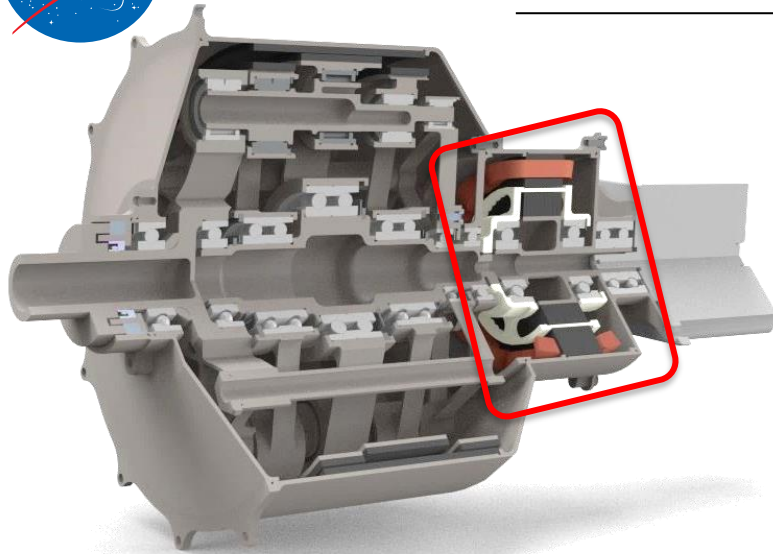
# Electromagnetic Design



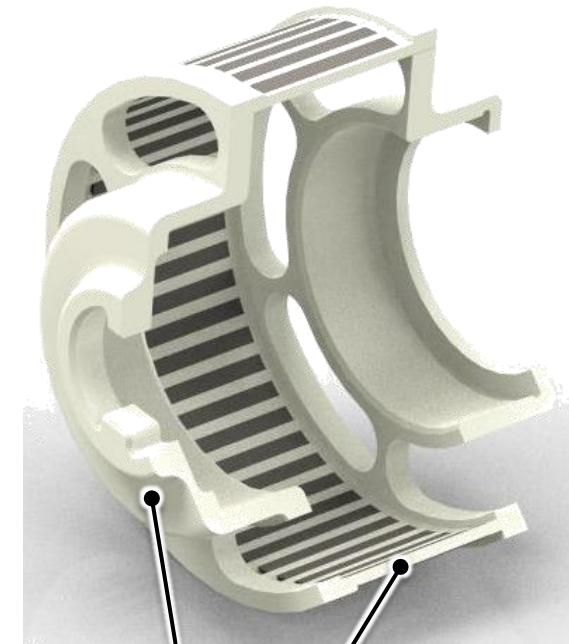
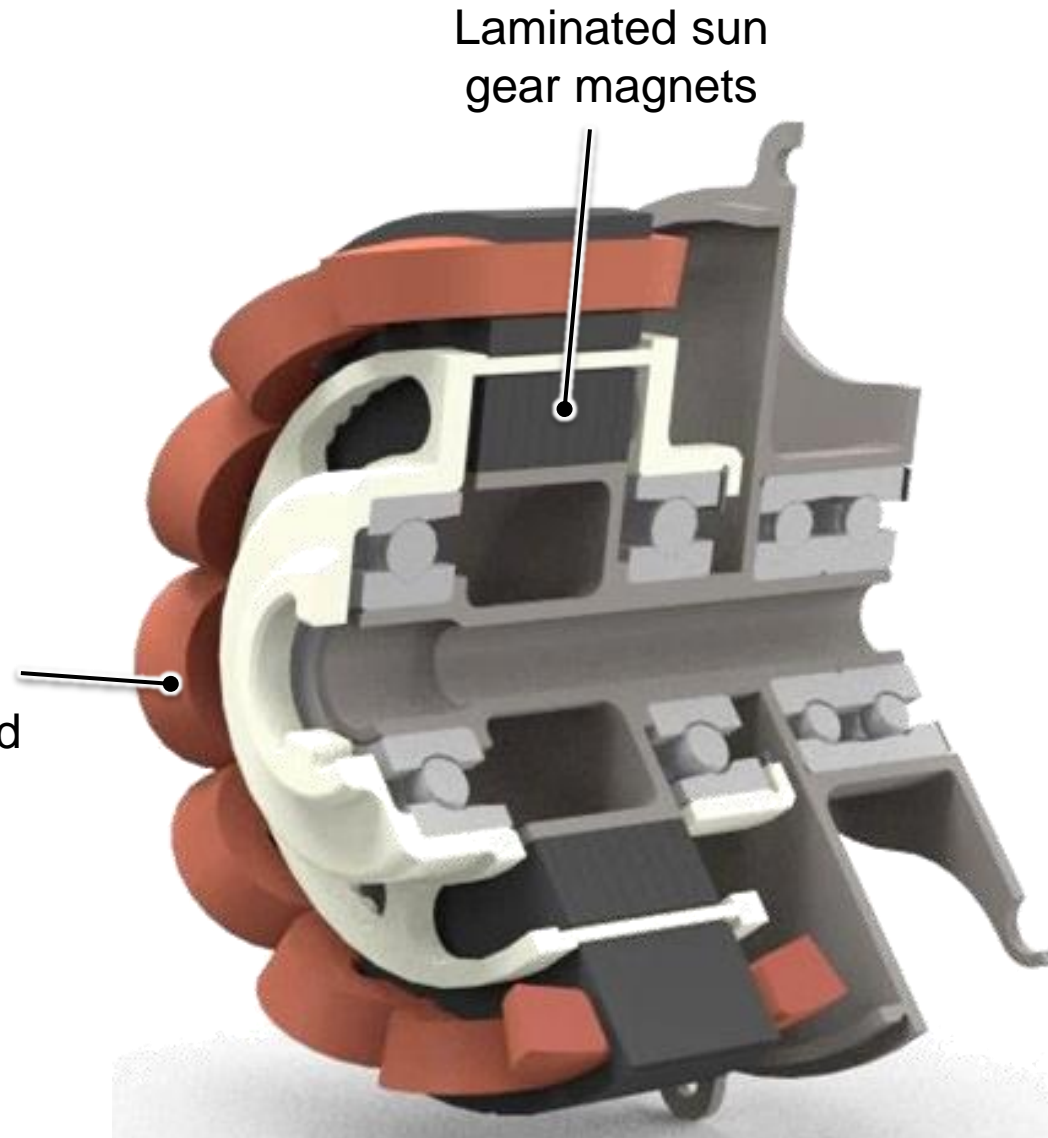
- Cycloidal gear optimized then its gear ratio & efficiency input to motor optimization
- 0.25 mm air gaps selected, but sized magnetically for 0.4 mm gaps based on initial prediction of air gap tolerance ( $\pm 0.15$  mm)
  - Additionally, 15% and 20% torque margin on gear and motor



# Electromagnetic Design



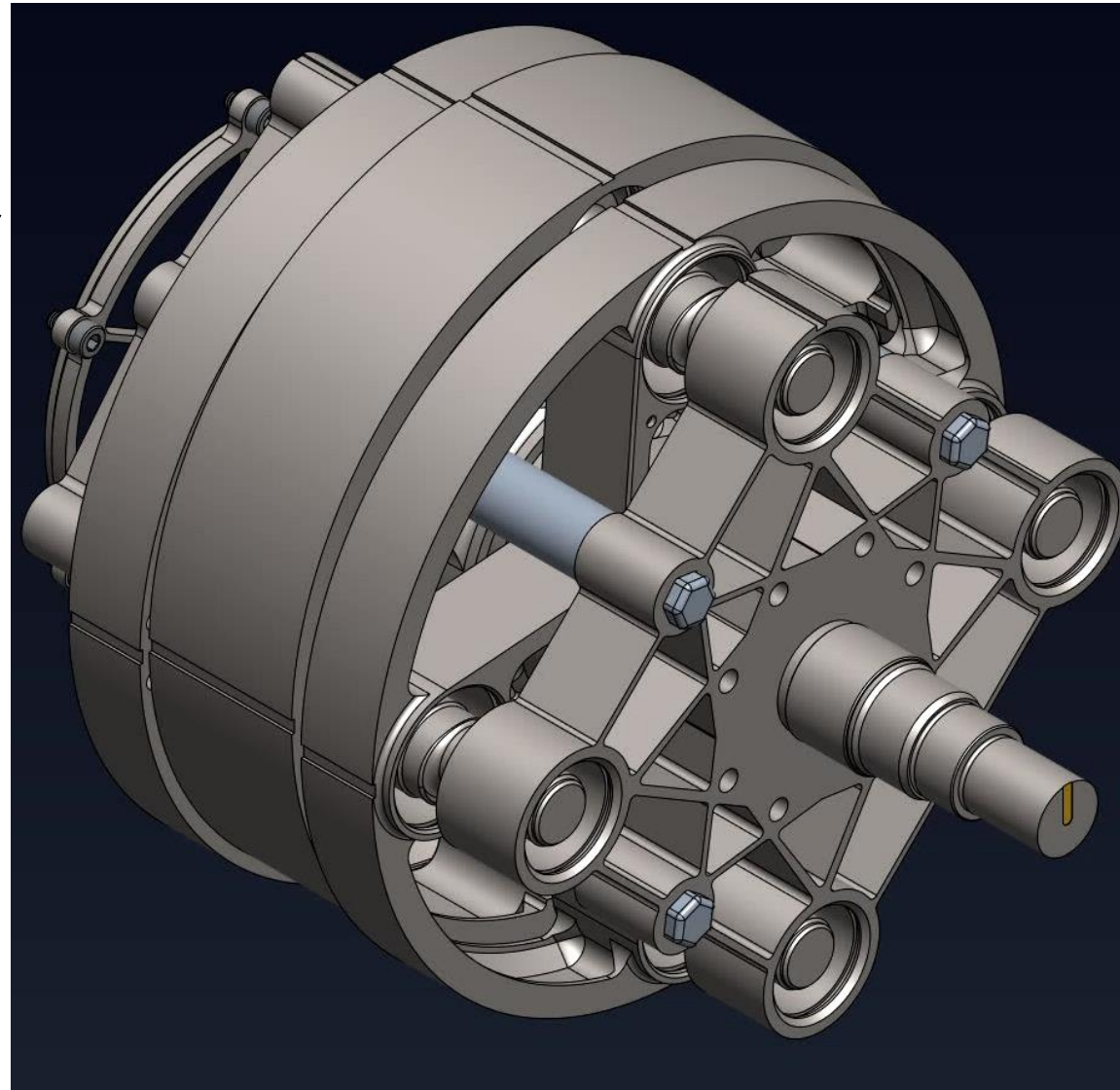
Concentrated winding for simplicity & higher efficiency  
+  
field oriented control for reduced resistive loss & torque ripple





# Electromagnetic Design

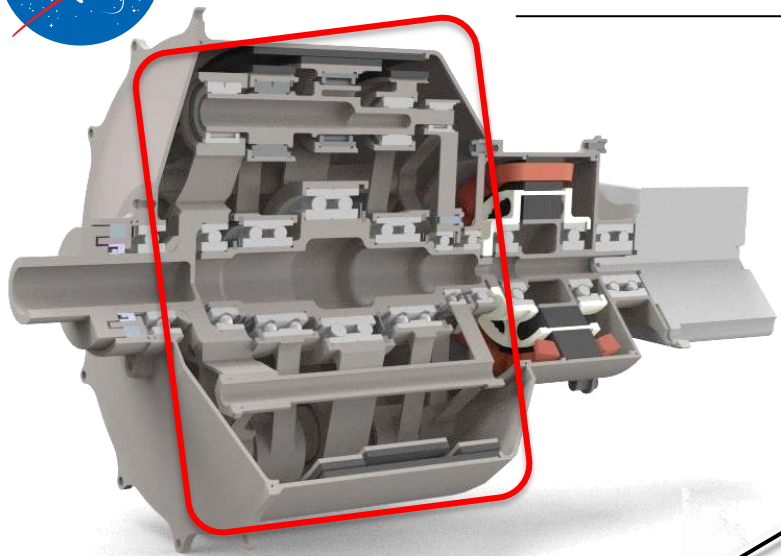
Input  
(not visible)  
86 rpm



Output  
2 rpm

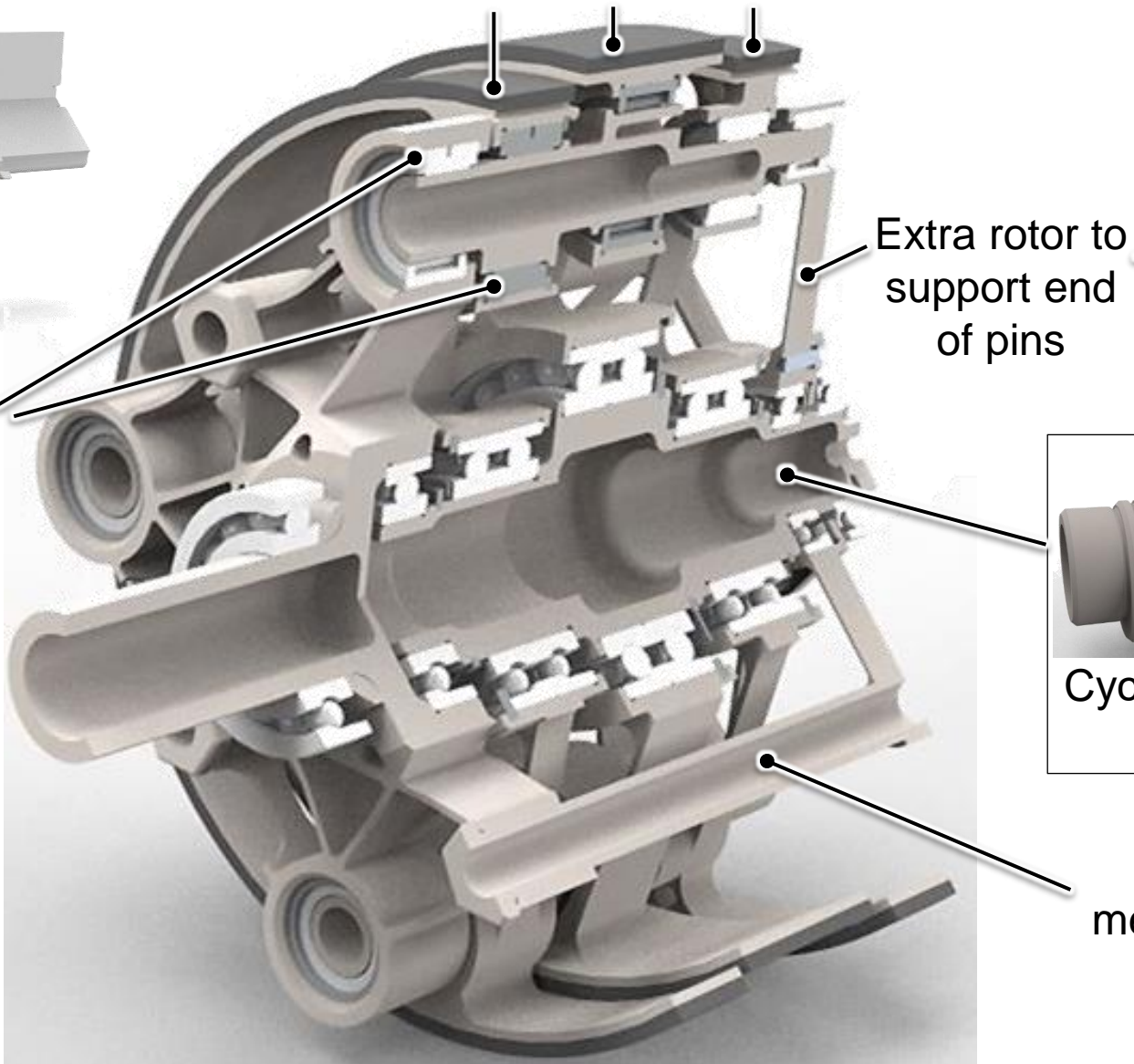


# Electromagnetic Design

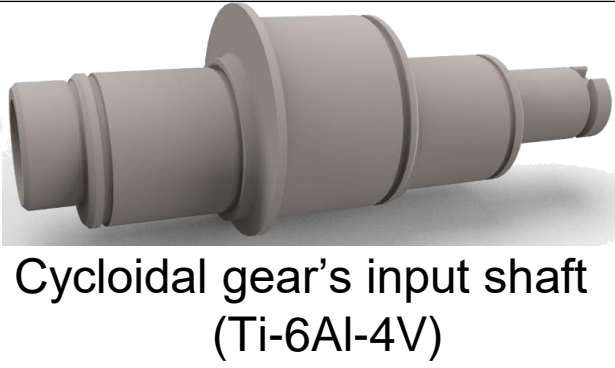
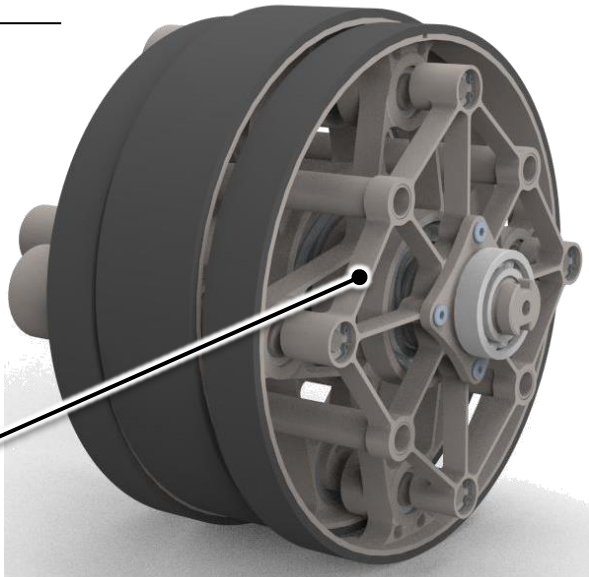


Needle bearings to reduce losses & mass

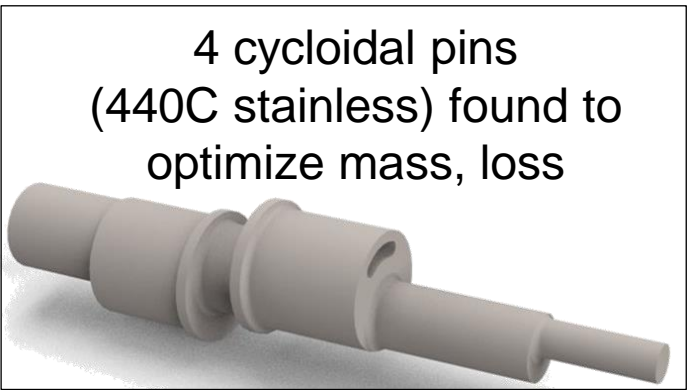
3 eccentric rotors to yield 1.3 kg reduction relative to 1 rotor



Extra rotor to support end of pins



Cycloidal gear's input shaft (Ti-6Al-4V)



4 cycloidal pins (440C stainless) found to optimize mass, loss

1 of 4 tie rods to mechanically link support rotor to output shaft



# Electromagnetic Design

## Magnetic losses & magnetic efficiency (continuous operation)

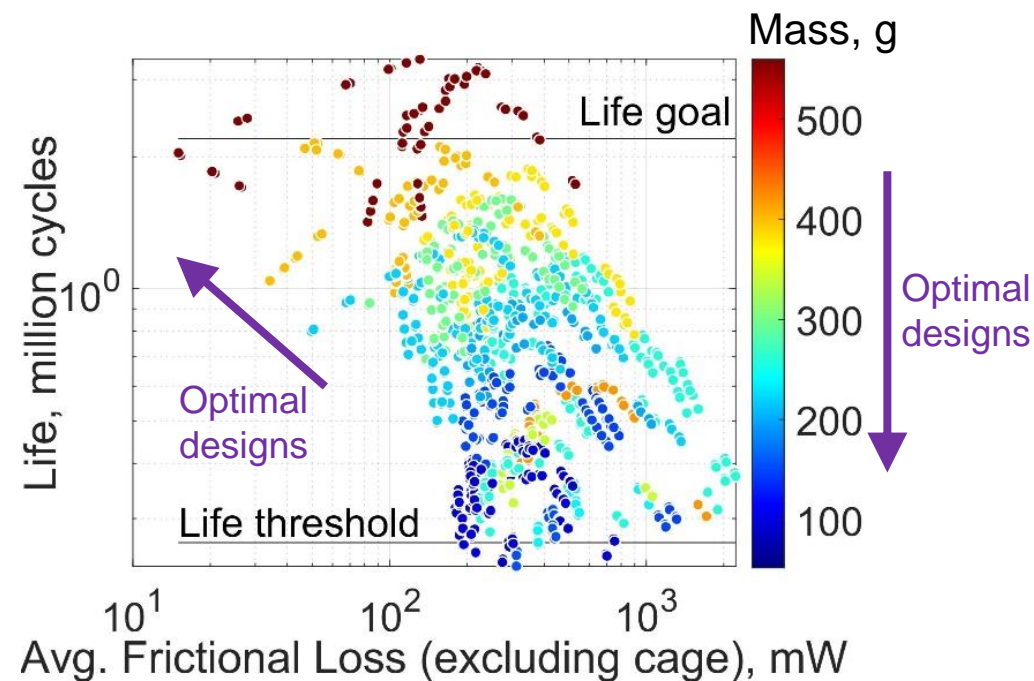
Loss [W]		Temperature [K]				
		50	150	250	350	450
Eddy currents	Sun magnets	0.1	0.09	0.08	0.07	0.06
	Modulator	0.15	0.14	0.14	0.14	0.13
	Ring magnets	0.07	0.07	0.06	0.05	0.05
	Stator iron	0.77	0.77	0.76	0.74	0.71
Winding losses	Proximity	0.86	0.05	0.03	0.02	0.01
	Ohmic	0.06	0.84	1.65	2.54	3.53
<b>Efficiency</b>		91.7%	92.0%	89.2%	86.3%	83.2%

- Magnetic forces simulated then input to bearing & structural analyses



# Bearing Design

- Bearing design dictated by life and sliding friction of the solid lubrication
- For each bearing in the actuator, the whole catalog of bearings was evaluated, and the best was selected
- Evaluation was based on time-dependent analytical calculation of:
  - Load distribution on each ball/roller
  - Contact area & contact stress
  - Sliding friction power loss
- Included effects of
  - Temperature-dependent material properties
  - Fits to mating hardware
  - Thermal expansion
  - Bearing preload variation
- Stiffness matrix of each bearing calculated & input to structural analysis

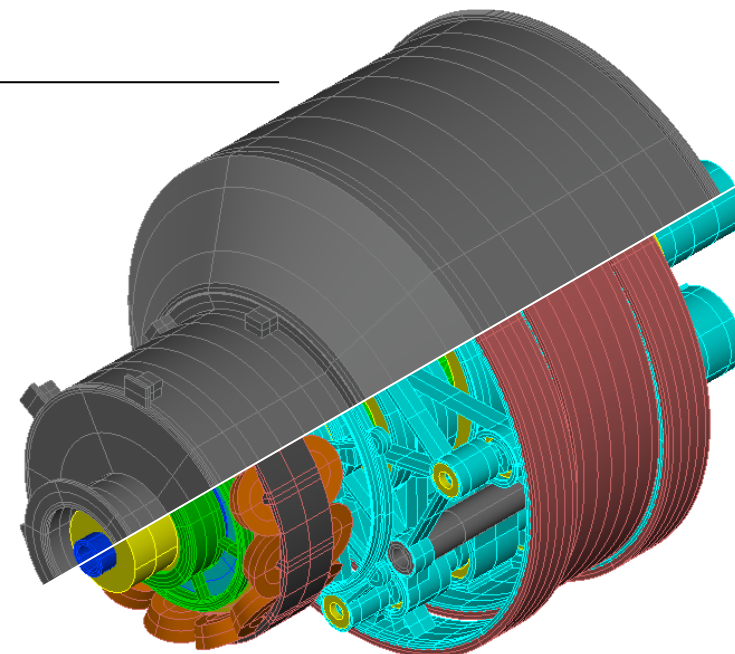


Example optimization of a heavily-loaded bearing

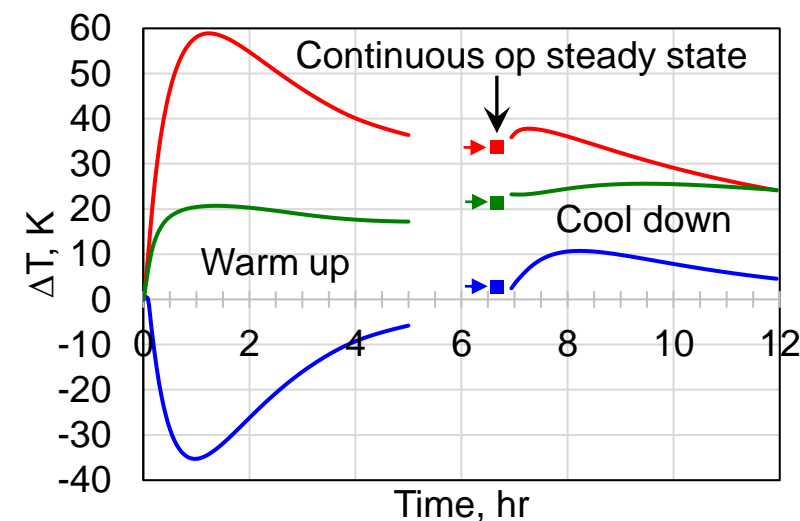


# Thermal Design

- Finite difference + finite element (FE) model of actuator used to predict steady state and transient responses
  - Only radiation to environment
  - Contact conductances of bearings & mechanical contacts
  - Temperature-dependent heat loads, thermal conductivity, and specific heat
  - Measured optical properties
- Ability to operate cold eliminates typical tradeoff with housing's external finish/coating → can optimize for hot, sun lit environments
- Predicted max internal temperature of 101 °C
  - Hot thermal margins >140 °C except cryo-vacuum rated epoxy (34 °C margin)
- Bearing & structural analyses use temperature distribution & gradient across bearings & air gaps

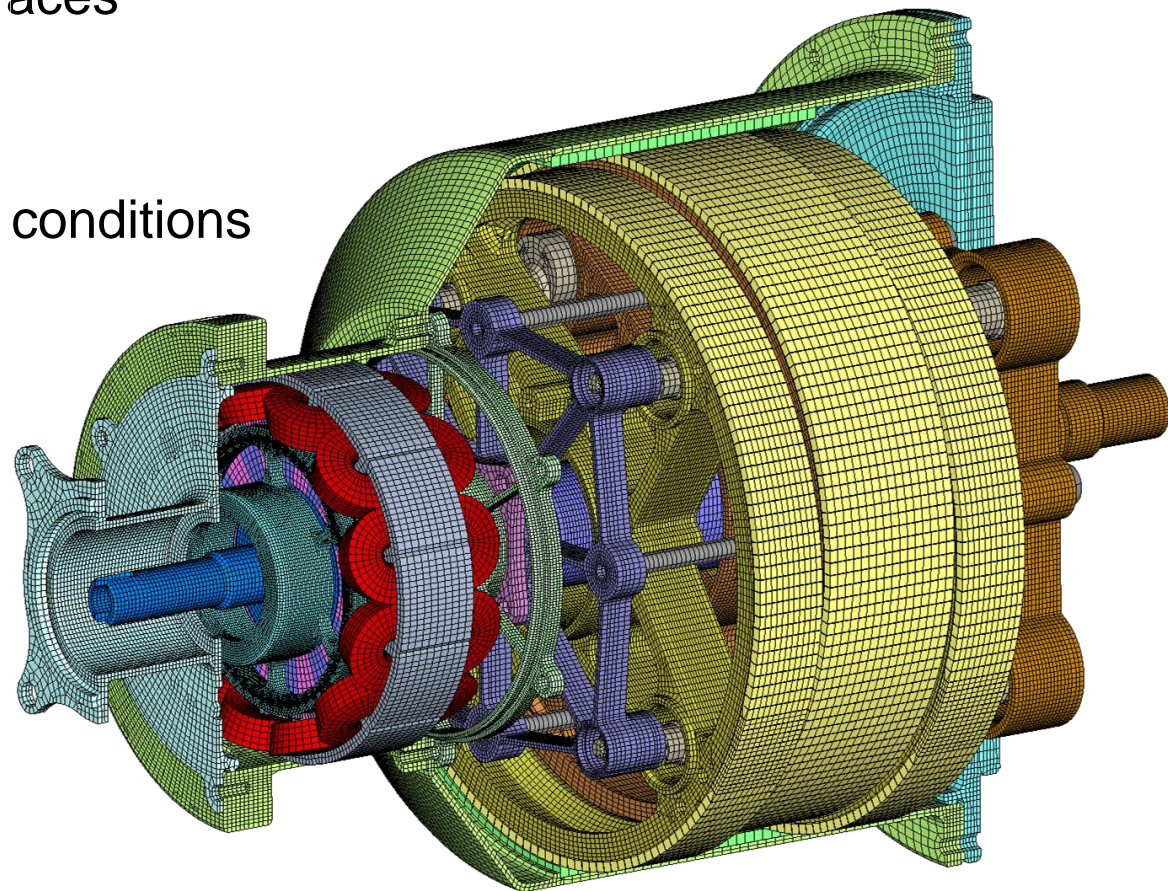


Thermal model



Temperature gradient across 3 air gaps 12

- Designed based on bearing design, tolerance stack-ups, manufacturability, & structural FE model
- Structural FE model
  - Mechanical contact at non-bolted, non-glued interfaces
  - Explicitly modeled epoxy around magnets
  - Thermal stress from temperature distribution & temperature-dependent expansion for 4 operating conditions
  - Worst-case magnetic forces (0.1 mm air gaps)
  - Worst-case position of eccentric rotors
- Predicted change in cycloidal's minimum air gaps
  - At peak torque: *increases* by 0.01 to 0.08 mm
  - At zero torque: *decreases* by 0.06 mm

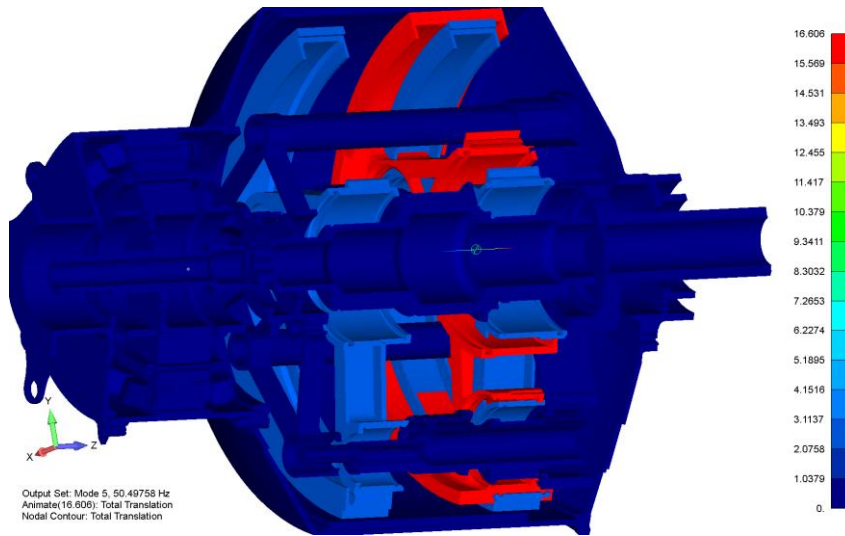


Structural model of as-built actuator

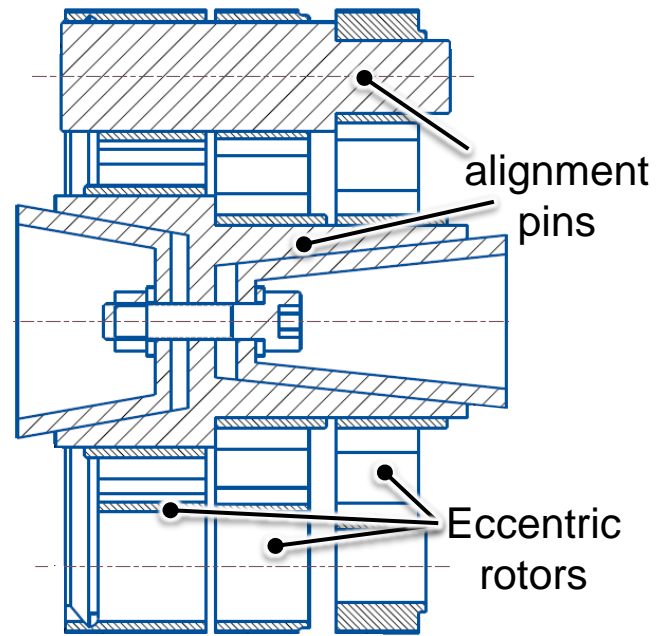


# Mechanical Design

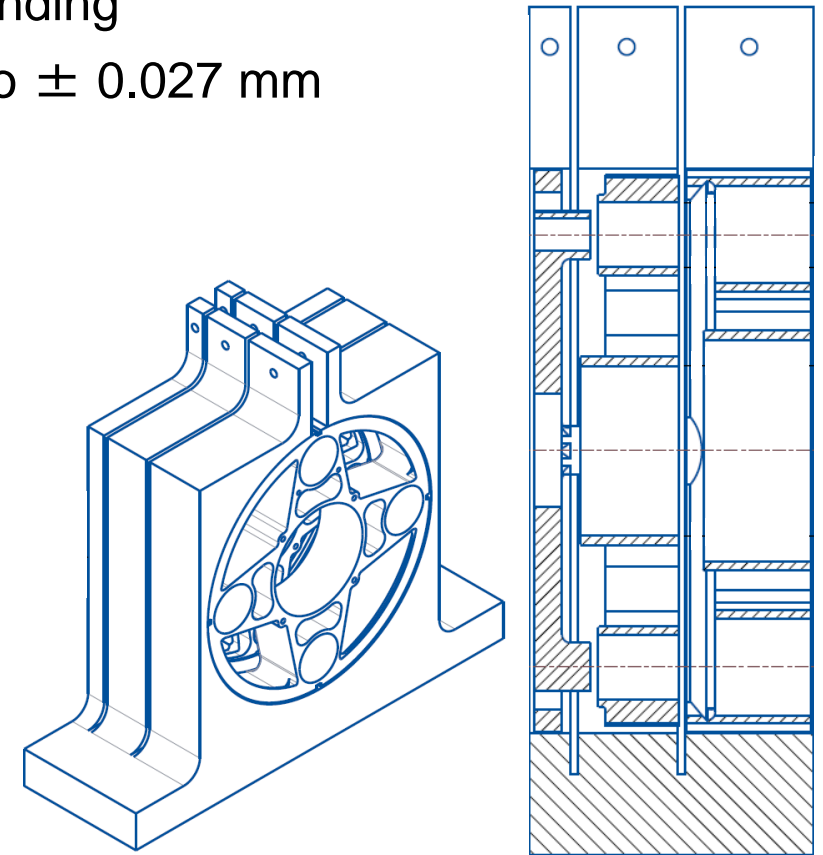
- Modal analysis confirmed that vibration modes can't be excited (bearing preload springs aren't too compliant)
- Challenges with 3 eccentric rotors addressed
  - Angular misalignment reduced using 4 grooves spaced 90° apart, 1 used as datum during match grinding
  - Match grinding to reduce air gap tolerance to  $\pm 0.027$  mm



Vibration mode with lowest frequency (51 Hz)



Fixturing to match grind OD of eccentric rotors

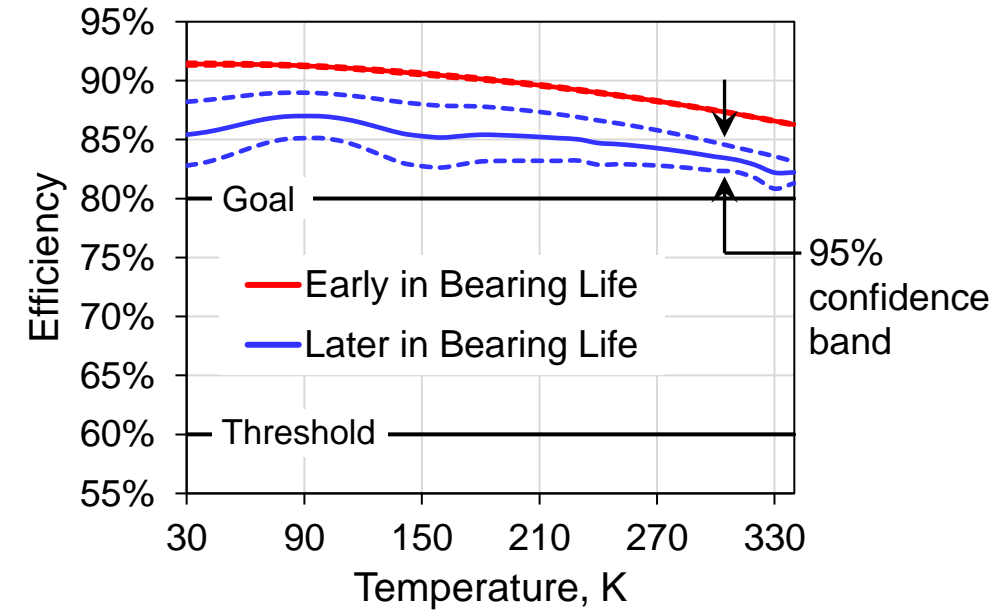


Fixturing to match grind bearing seats in 3 of 5 rotors



# Predicted Performance

Category	Description	Current model prediction	Objective
Thermal	Internal <i>operating</i> temperature range	-249 °C to +101 °C ✓	< -243 °C
Efficiency	Considering full temperature range & actuator life	81% to 91% ✓	>80%
Magnetic	Peak torque	252 to 262 Nm ✓	105 Nm continuous 208 Nm peak



## Impact of air gap on torque & specific torque

Air gap [mm]	Magnetic gear		Geared motor			Actuator		
	Peak torque [Nm]	Specific torque [Nm/kg]	Peak torque [Nm]	Specific torque [Nm/kg]		Peak torque [Nm]	Specific torque [Nm/kg]	
				With resolver	No resolver		With resolver	No resolver
0.1	282.6	78.7	-	-	-	282.6	53.3	62.1
0.25	257.0	71.6	7.56	4.4	7.9	257.0	48.5	56.5
0.4	231.2	64.4	5.62	3.3	5.9	231.2	43.6	50.8

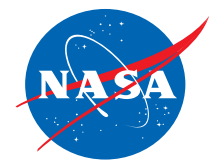


# Predicted Performance

Category	Description	Current model prediction	Objective
Mass	Total mass	4.55 kg ✓ (initial design script: 4.63 kg)	Target: <4.73 kg Stretch goal: < 3.15 kg
	Specific torque	47.5 to 49.5 Nm/kg	
Size	Envelope	153 mm dia, 240 mm length = 4,412 cm <sup>3</sup> ✗	Target: 1440 cm <sup>3</sup> Stretch goal: < 960 cm <sup>3</sup>
Life	Output revolutions, dust free	46,500 ✓	Required: 6,000 Goal: > 50,000

## Mass breakdown (without resolver)

Component	Magnetic (stator) [kg]	Magnetic (other) [kg]	Structure [kg]	Bearings [kg]	Hardware / other [kg]	Total [kg]
Geared motor	0.31	0.30	0.20	0.14	0.01	<b>0.96</b>
Magnetic gear	n/a	1.11	1.78	0.59	0.11	<b>3.59</b>
Actuator	0.31	1.41	1.98	0.73	0.12	<b>4.55</b>



# Conclusions

---

- Actuator predicted to operate at internal temperatures of  $-249\text{ }^{\circ}\text{C}$  to  $+101\text{ }^{\circ}\text{C}$ , have efficiency  $> 80\%$ , and a useful life
- Lightweight magnetic design enabled by 0.25 mm air gaps
  - Achieving this is difficult due to complexity of cycloidal gear, but solution found that achieves air gap tolerance of  $-.09 / +.11\text{ mm}$  across all operating conditions
- Actuator's size and mass largely driven by sizing of solid lubricated bearings



# Acknowledgements

---

This work was funded by the Motors for Dusty & Extremely Cold Environments (MDECE) Project

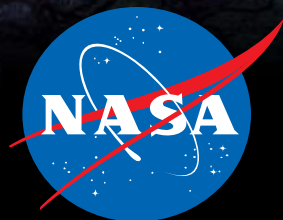
Space Technology Mission Directorate  
Game Changing Development Program  
MDECE Project

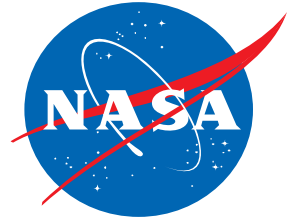
## Contact Info

---

{justin.j.scheidler, aaron.d.anderson-1, thomas.tallerico, peter.a.hoge,  
george.r.Harpster, kyle.r.whitling, jesse.hawk, malcolm.g.robbye}@nasa.gov

# THANK YOU



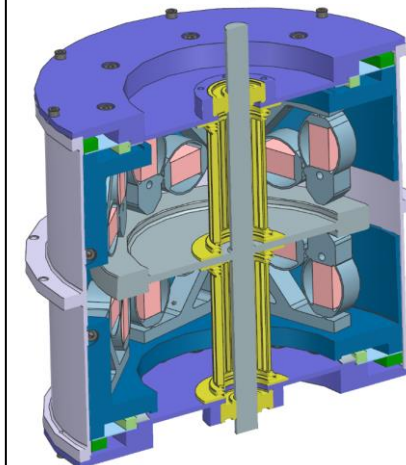
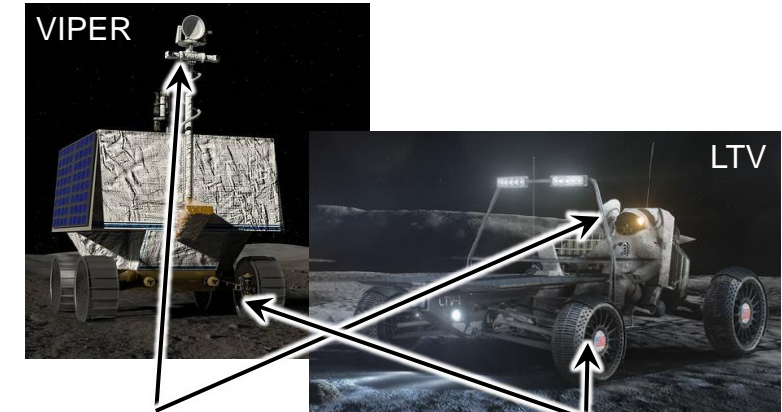




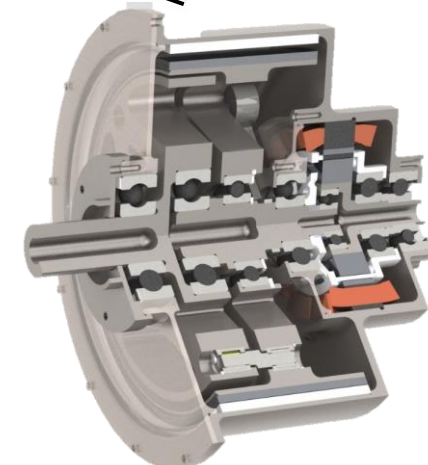
# Motors for Dusty & Extremely Cold Environments (MDECE) Project

- **R&D & ground test project, 2020 – 2025**
- **Goal:** Develop 2 unheated rotational actuators that can operate for a long duration in extreme cold (ambient temperature of  $-243\text{ }^{\circ}\text{C}$  (30 K))
  - Evaluate life in controlled, representative lunar dust environment with and without lunar simulant
- **Approach:** Eliminate gear lubrication – 1 actuator with non-contact gearing, 1 actuator with no gears
- **Key Performance Parameters:** Min. operating temperature • dust-free life • efficiency of magnetic actuator • output resolution of piezoelectric actuator
- **Relevant environment:** Broadly applicable; focusing on lunar PSR
- **Promising applications:**
  - Magnetic actuator: rover mobility • in-situ resource utilization • robotic arm joints • rotors for powered flight
  - Piezoelectric actuator: precision pointing (e.g., laser communication) • low power robotic arm joints

Example mechanisms for demonstrating prototypes (NASA KSC)



**Piezoelectric actuator**  
preliminary design  
(JPL)



**Magnetically-g geared actuator**  
preliminary design  
(NASA GRC & GSFC)

[graphic courtesy of NDEAA team / JPL / Caltech / NASA (Patent pending)]



# Driving Requirements

- Mechanical output**
  - Continuous 105 Nm at 2 rpm (22 W power)
  - Peak 208 Nm at up to 1.5 rpm (up to 33 W) for 60 seconds
- Life**
  - 6,000 output revolutions (min), 50,000 (goal) [dust free]
- Size / mass**
  - No strict requirements (TRL 2-5)
  - Mass 4.73 kg (max), < 3.15 kg (goal)
  - Envelope volume 1440 cm<sup>3</sup> (max), < 960 cm<sup>3</sup> (goal)
  - Aspect ratio (length / diameter) 0.5 to 1.75

} Match flight-qualified reference actuator

## Thermal specifications for operation

Parameter	Minimum		Maximum	
	Goal	Required	Required	Goal
Lunar surface temperature	30 K (-243 °C)	108 K (-165 °C)	293 K (20 °C)	313 K (40 °C)
Solar heating environment	Shadowed		–	Lunar 85° S