

Recommended Practice for Use of ExB Probes in Electric Propulsion Testing

IEPC-2025-483

Joshua L. Rovey and Toyofumi Yamauchi

University of Illinois Urbana-Champaign, Urbana, Illinois, 61801, USA

Wensheng Huang and Robert E. Thomas

NASA Glenn Research Center, Cleveland, Ohio, 44135, USA

William J. Hurley

University of Michigan, Ann Arbor, Michigan, 48109, USA

Shawn C. Farnell, Seth J. Thompson, Cody C. Farnell, and Casey C. Farnell

Colorado State University / Plasma Controls LLC, Fort Collins, Colorado, 80523, USA

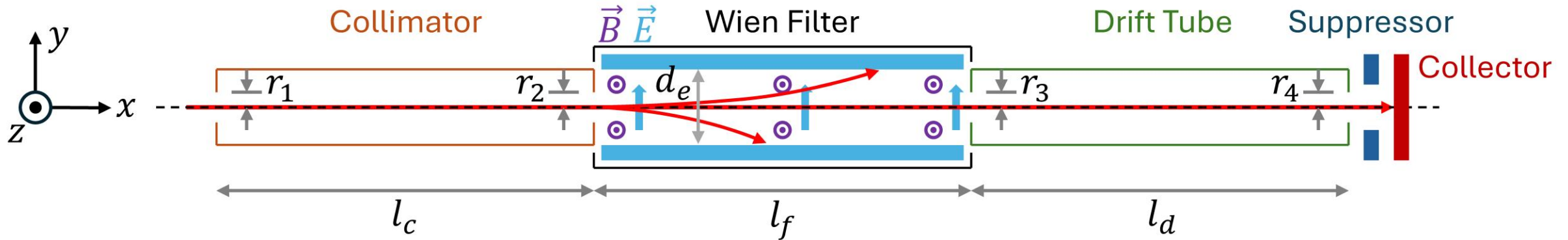
William P. Brabston

Georgia Institute of Technology, Atlanta, Georgia, 30318, USA

Jason A. Young

Aerospace Corporation, California, USA

Theory – First Principles



$$\vec{F} = q(\vec{E} + \vec{v} \times \vec{B}) = 0$$

$$\vec{E} = -\vec{v} \times \vec{B}$$

$$v = -\frac{E}{B} = v_{Wien}$$

$$E = \frac{V_{plates}}{d}$$

$$v = v_{Wien} = -\frac{V_{plates}}{Bd}$$

$$v = \sqrt{\frac{2qV_{accel}}{m}}$$

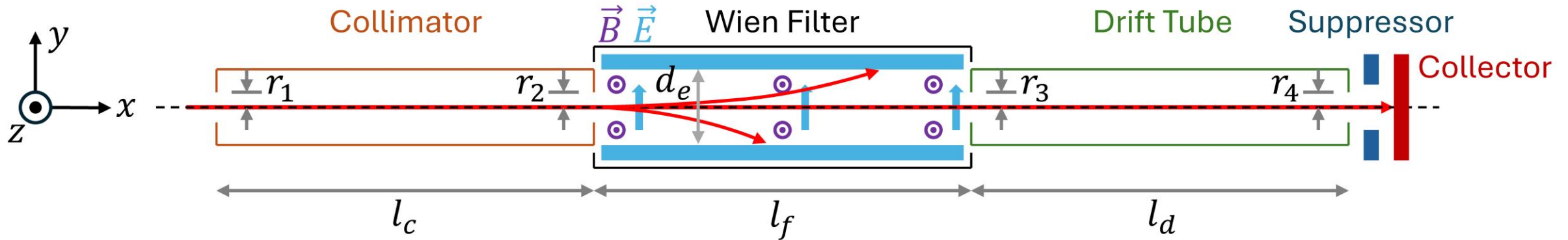
Mass-to-charge ratio filter

$$\frac{q}{m} = \frac{1}{2V_{accel}} \left(\frac{V_{plates}}{Bd} \right)^2$$

Charge state filter (const. m)

$$Z = \frac{m}{2eV_{accel}} \left(\frac{V_{plates}}{Bd} \right)^2$$

Theory – First Principles



$$\vec{F} = q(\vec{E} + \vec{v} \times \vec{B}) = 0$$

$$\vec{E} = -\vec{v} \times \vec{B}$$

$$v = -\frac{E}{B} = v_{Wien}$$

$$E = \frac{V_{plates}}{d}$$

$$v = v_{Wien} = -\frac{V_{plates}}{Bd}$$

$$v = \sqrt{\frac{2qV_{accel}}{m}}$$

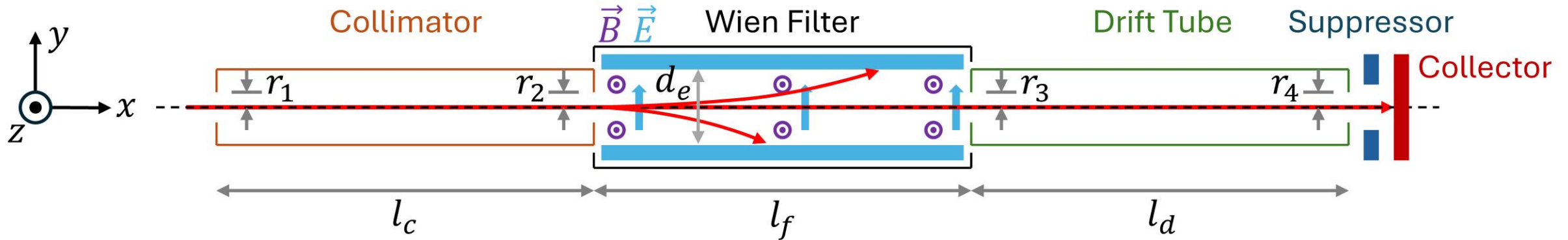
Mass-to-charge ratio filter

$$\frac{q}{m} = \frac{1}{2V_{accel}} \left(\frac{V_{plates}}{Bd} \right)^2$$

Charge state filter (const. m)

$$Z = \frac{m}{2eV_{accel}} \left(\frac{V_{plates}}{Bd} \right)^2$$

Theory – First Principles



$$\vec{F} = q(\vec{E} + \vec{v} \times \vec{B}) = 0$$

$$\vec{E} = -\vec{v} \times \vec{B}$$

$$v = -\frac{E}{B} = v_{Wien}$$

$$E = \frac{V_{plates}}{d}$$

$$v = v_{Wien} = -\frac{V_{plates}}{Bd}$$

$$v = \sqrt{\frac{2qV_{accel}}{m}}$$

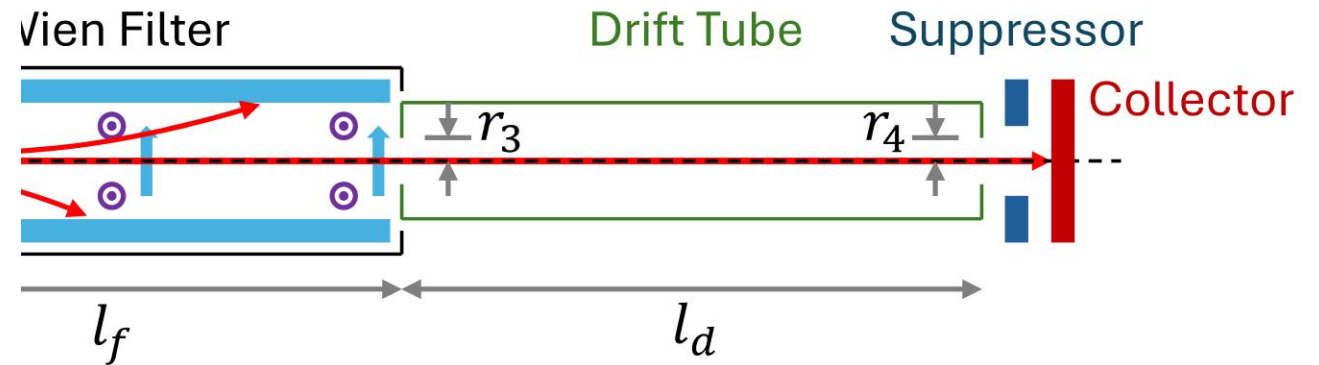
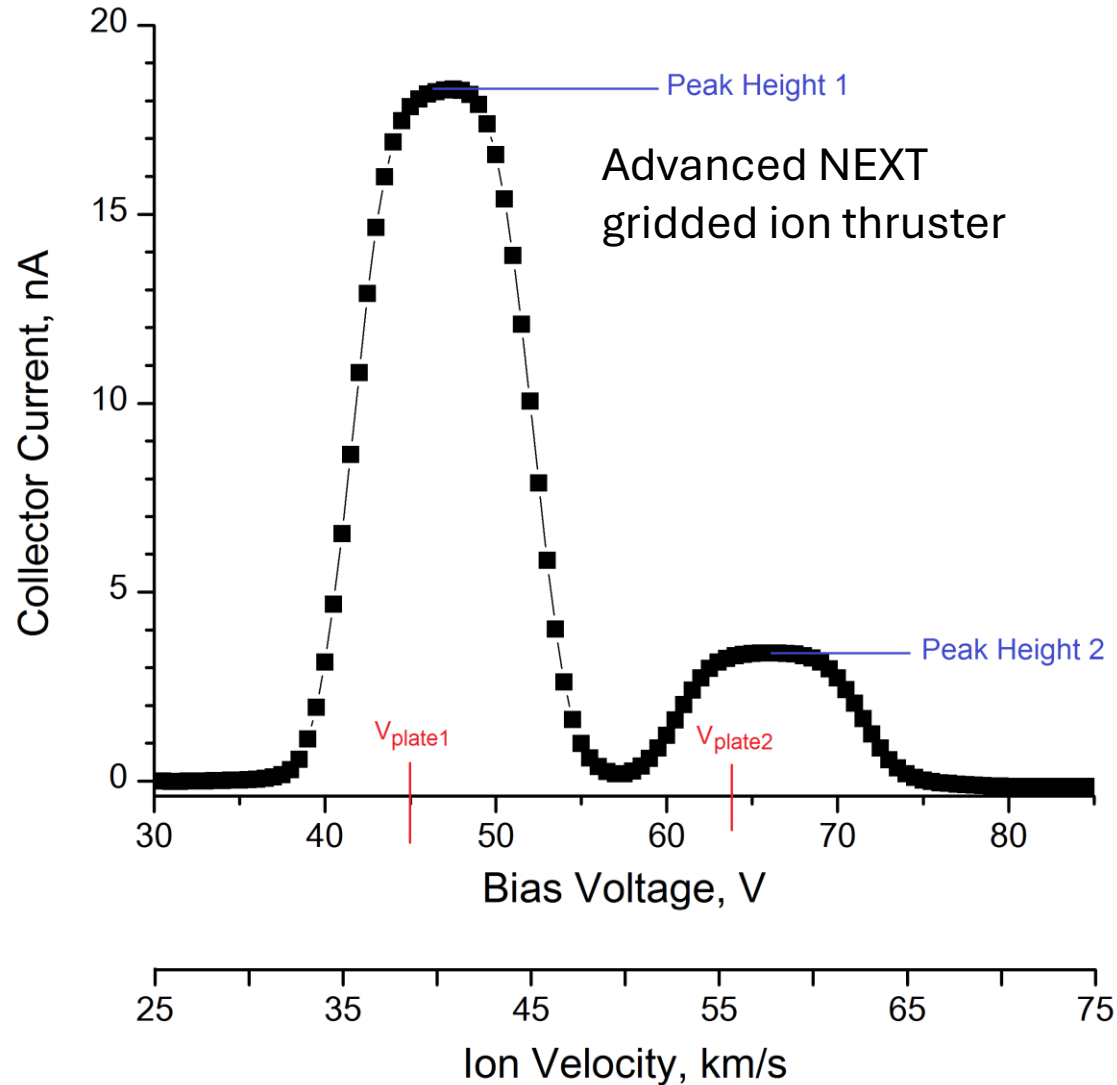
Mass-to-charge ratio filter

$$\frac{q}{m} = \frac{1}{2V_{accel}} \left(\frac{V_{plates}}{Bd} \right)^2$$

Charge state filter (const. m)

$$Z = \frac{m}{2eV_{accel}} \left(\frac{V_{plates}}{Bd} \right)^2$$

Theory – First Principles



$$\frac{V_{plates}}{d} = - \frac{V_{plates}}{Bd}$$

$$\frac{lV_{accel}}{m}$$

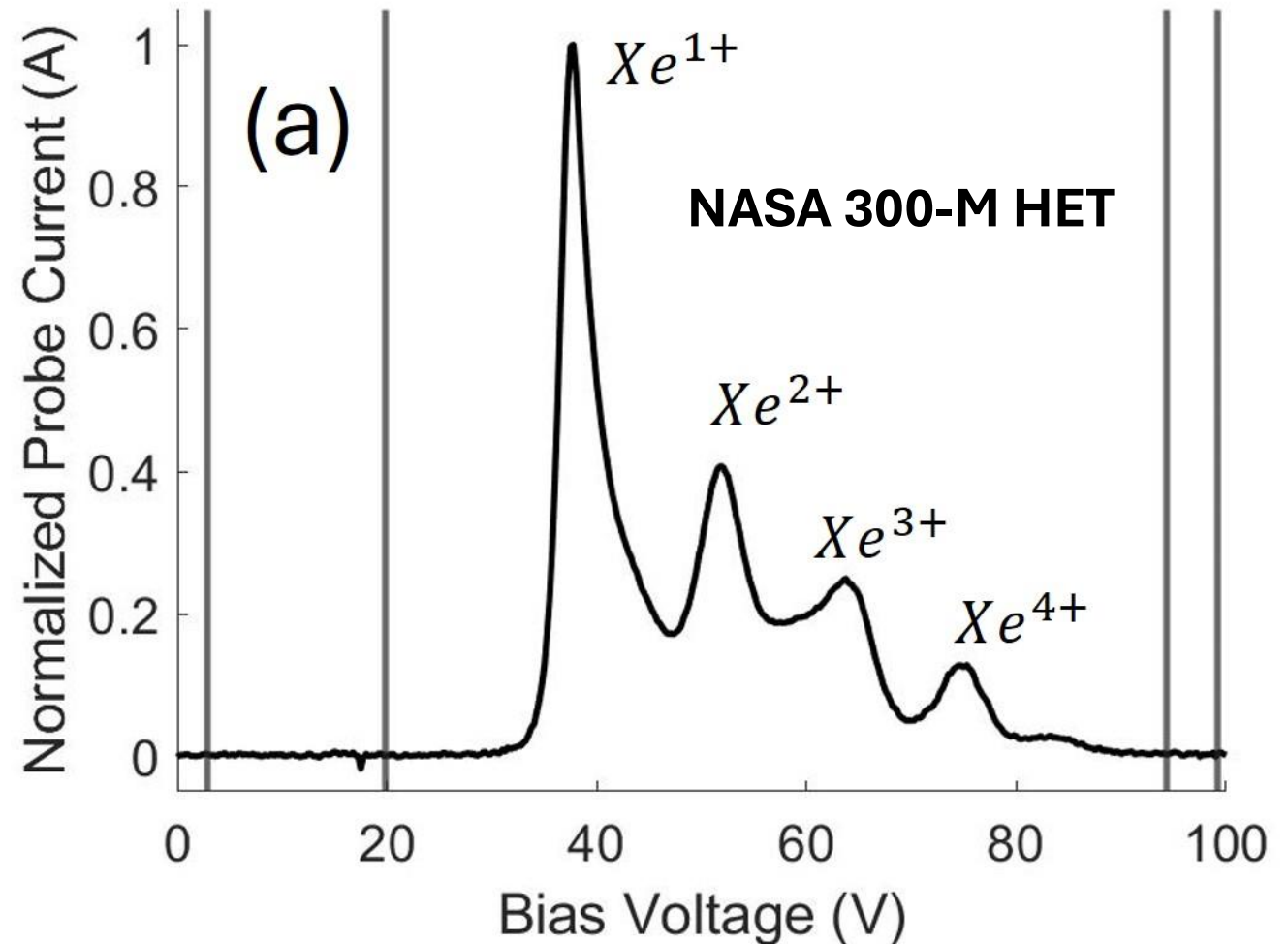
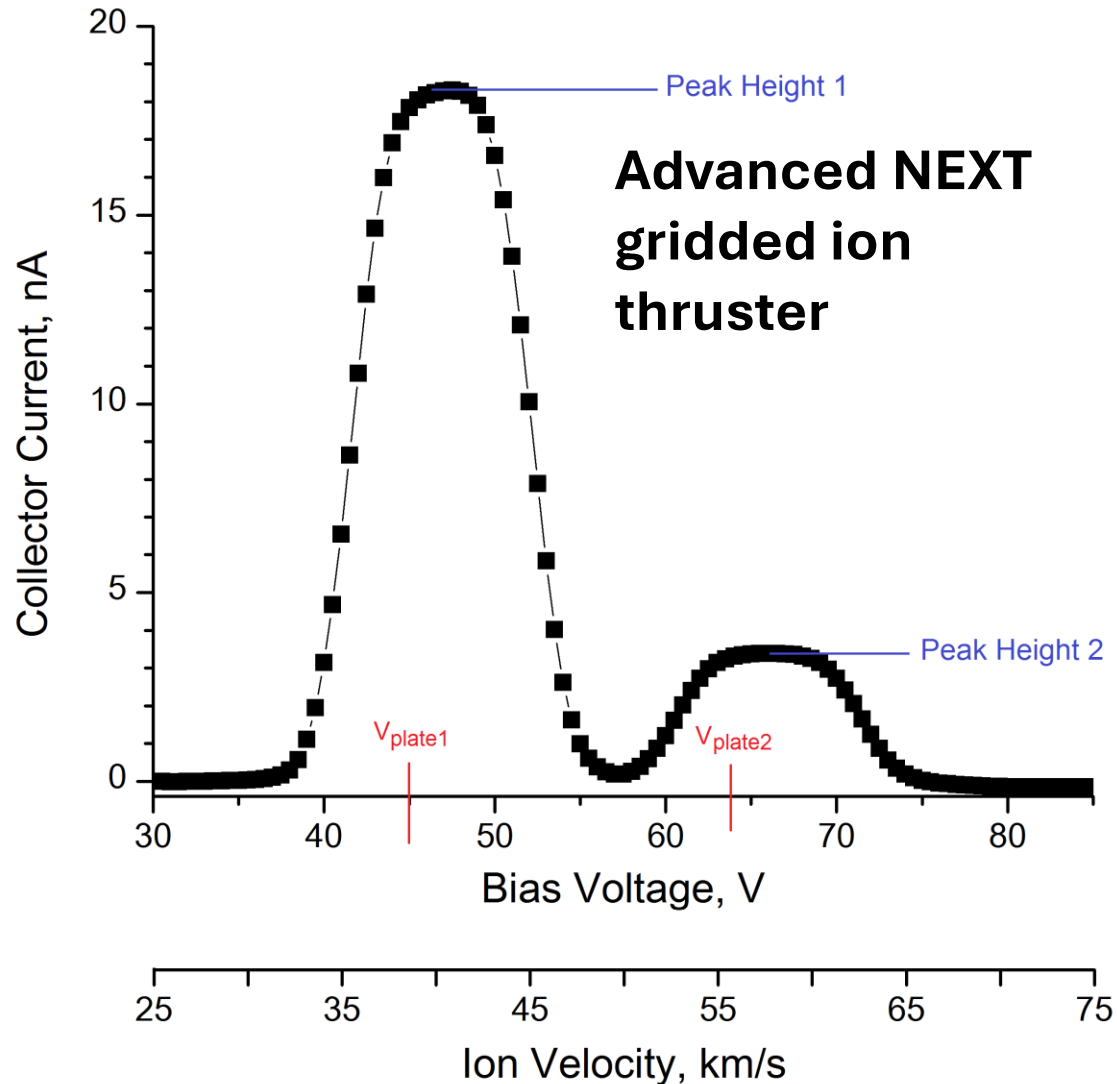
Mass-to-charge ratio filter

$$\frac{q}{m} = \frac{1}{2V_{accel}} \left(\frac{V_{plates}}{Bd} \right)^2$$

Charge state filter (const. m)

$$Z = \frac{m}{2eV_{accel}} \left(\frac{V_{plates}}{Bd} \right)^2$$

Theory – First Principles



Velocity Resolution

$$\Delta v = \frac{mv_{Wien}^2}{ZeB} G$$
$$\frac{\Delta v}{v_{Wien}} = \frac{mv_{Wien}}{ZeB} G$$

Where G is dependent
on probe dimensions

$$G = \left[\frac{a_2 + a_3 + (a_1 + a_2)(L_f + L_d)/L_c}{L_f^2 + 2L_dL_f} \right]$$

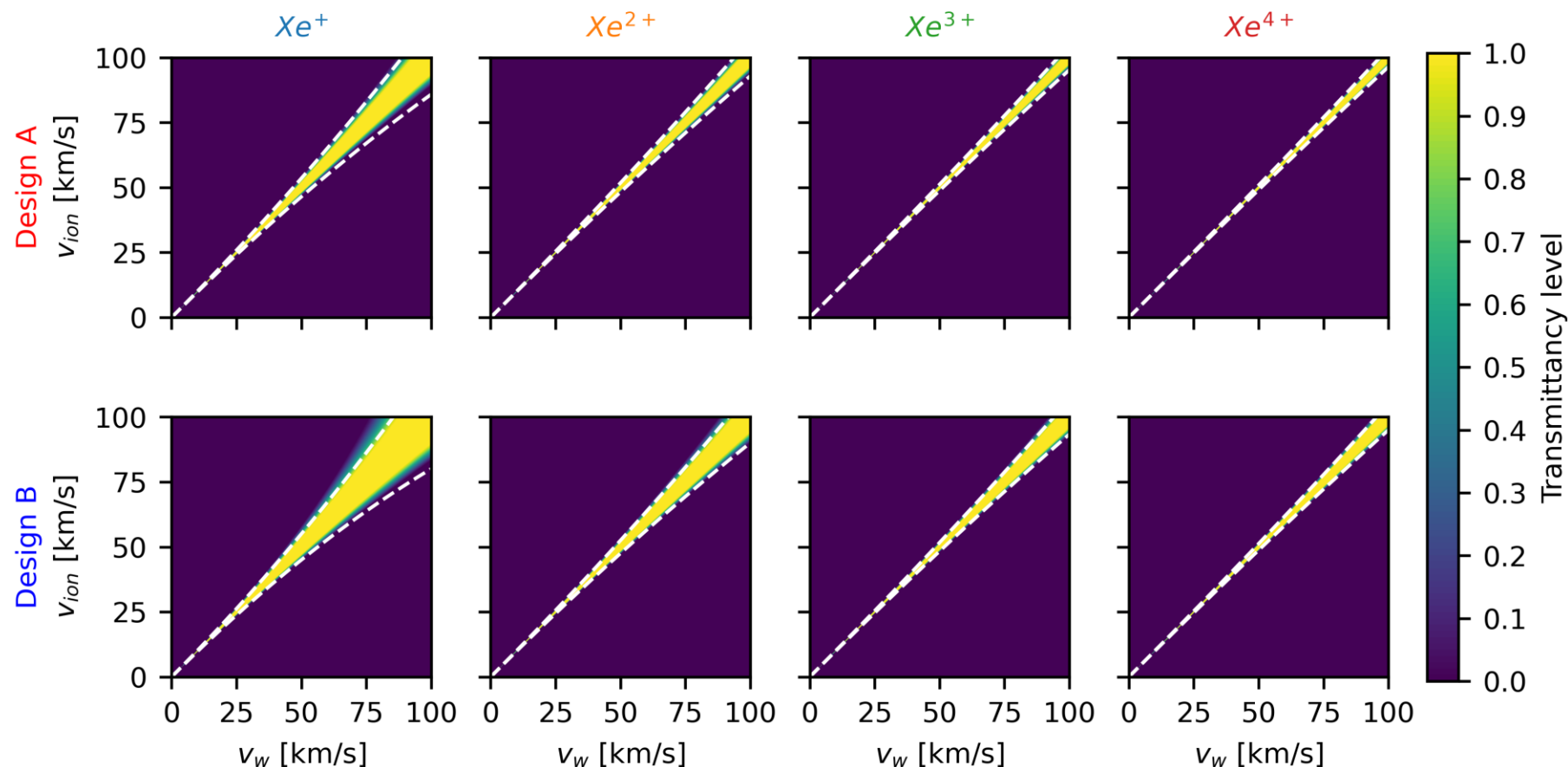
Velocity Resolution

$$\Delta v = \frac{mv_{Wien}^2}{ZeB} G$$

$$\frac{\Delta v}{v_{Wien}} = \frac{mv_{Wien}}{ZeB} G$$

$$G = \left[\frac{a_2 + a_3 + (a_1 + a_2)(L_f + L_d)/L_c}{L_f^2 + 2L_dL_f} \right]$$

	Aperture Radius (mm)				Length (mm)			Plate Sep. (mm)	Magnetic Field (T)	(1/m)
Probe	r1	r2	r3	r4	lc	lf	ld	de	B	G
A	1	2	3	4	100	200	50	10	0.2	0.208
B	1	2	3	4	100	125	50	10	0.2	0.364



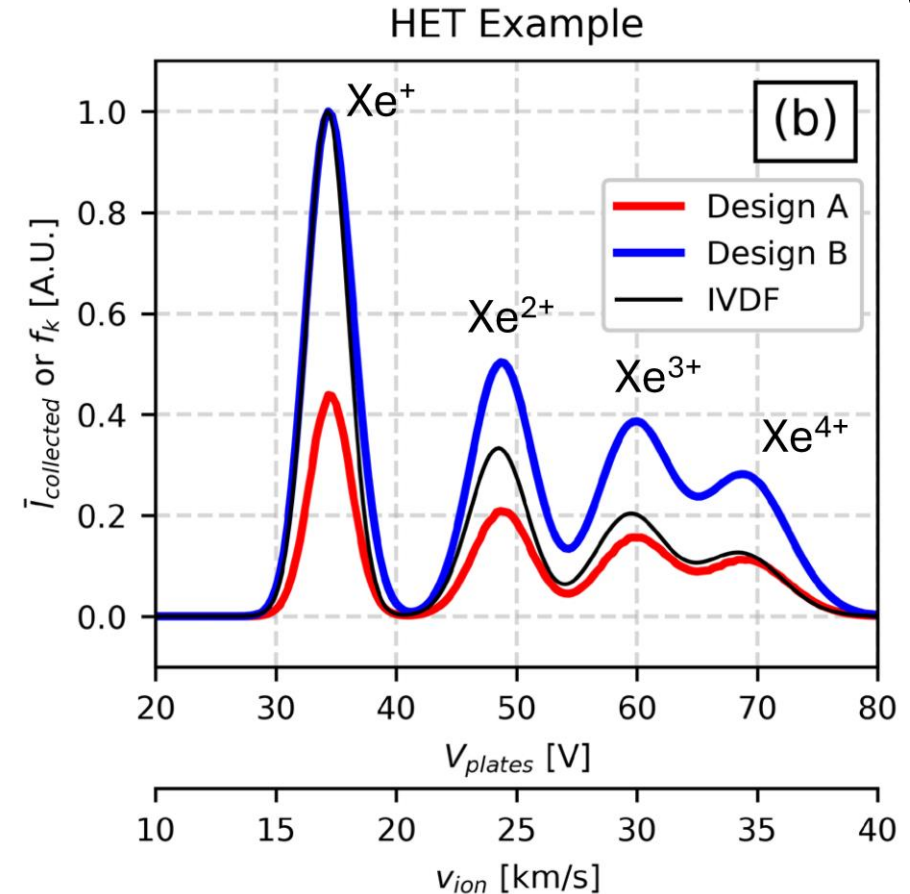
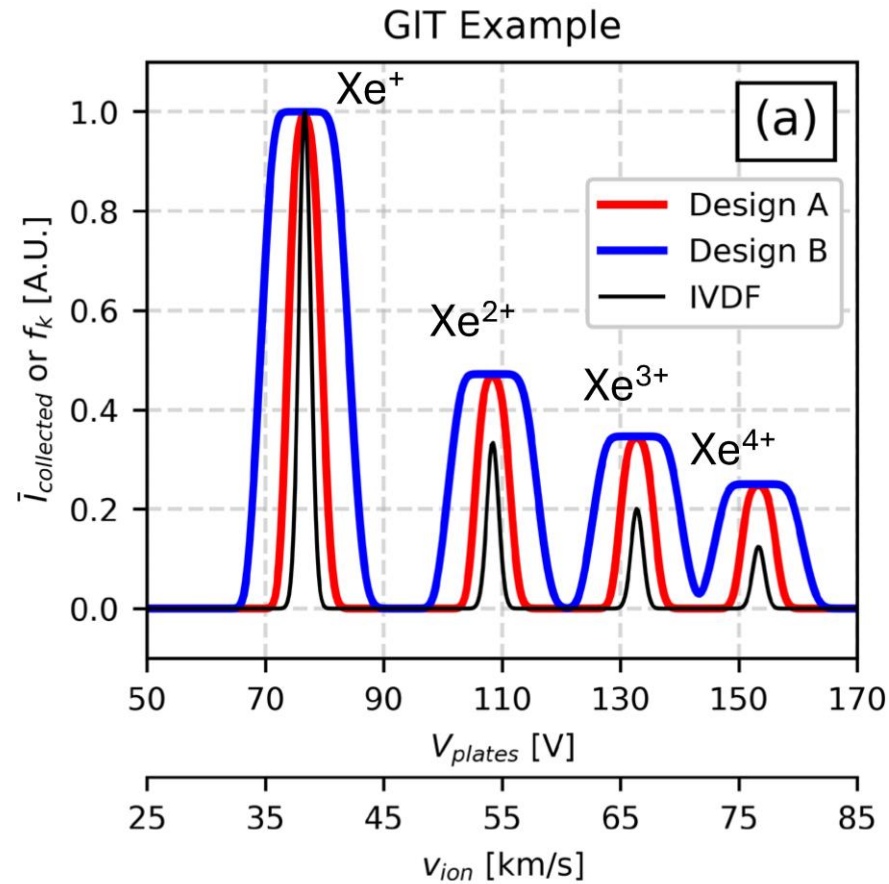
Velocity Resolution

$$\Delta v = \frac{mv_{Wien}^2}{ZeB} G$$

$$\frac{\Delta v}{v_{Wien}} = \frac{ZeB}{mv_{Wien}} G$$

$$G = \left[\frac{a_2 + a_3 + (a_1 + a_2)(L_f + L_d)/L_c}{L_f^2 + 2L_dL_f} \right]$$

	Aperture Radius (mm)				Length (mm)			Plate Sep. (mm)	Magnetic Field (T)	(1/m)
Probe	r1	r2	r3	r4	lc	lf	ld	de	B	G
A	1	2	3	4	100	200	50	10	0.2	0.208
B	1	2	3	4	100	125	50	10	0.2	0.364



Design

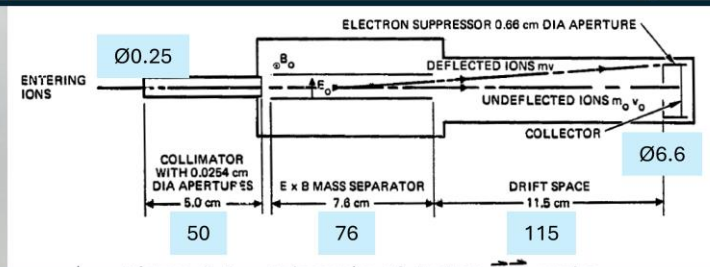
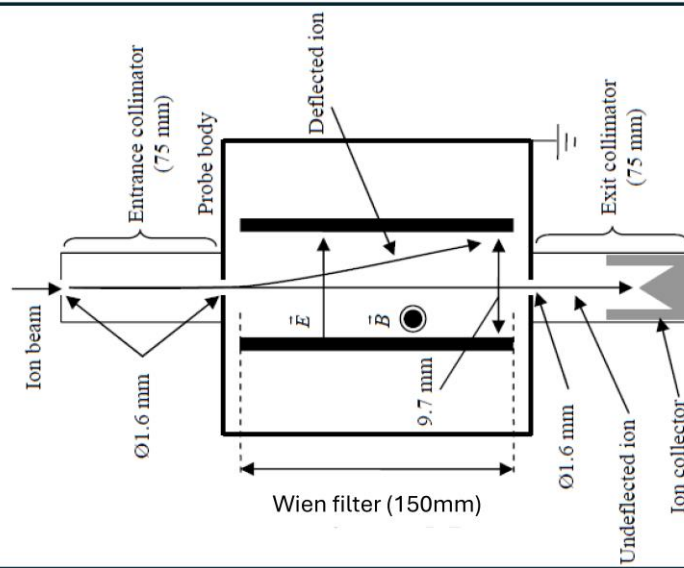
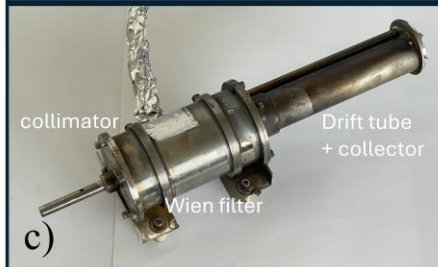
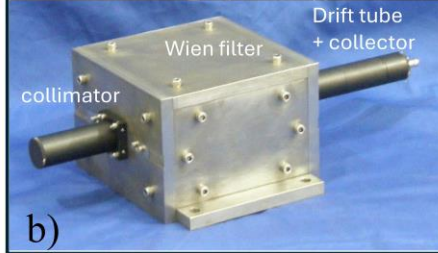
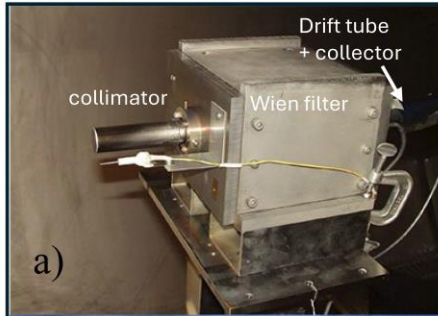
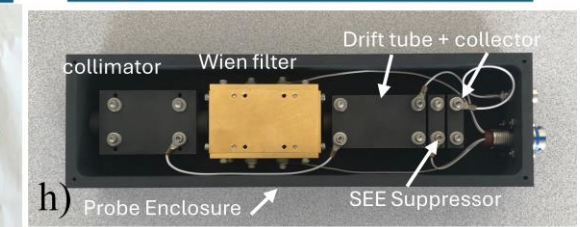
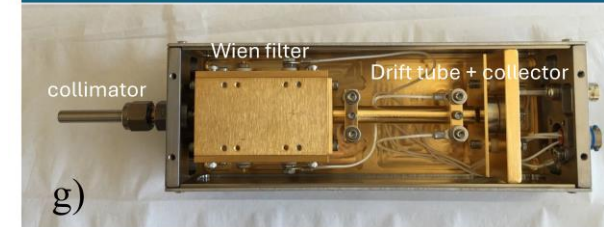
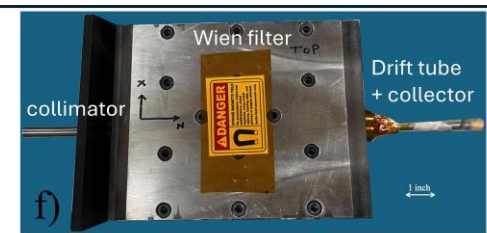
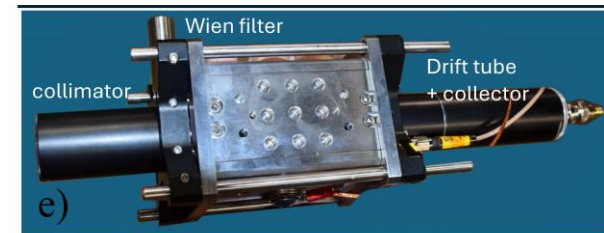
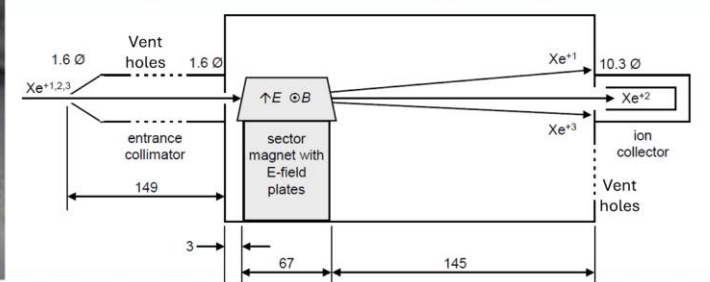
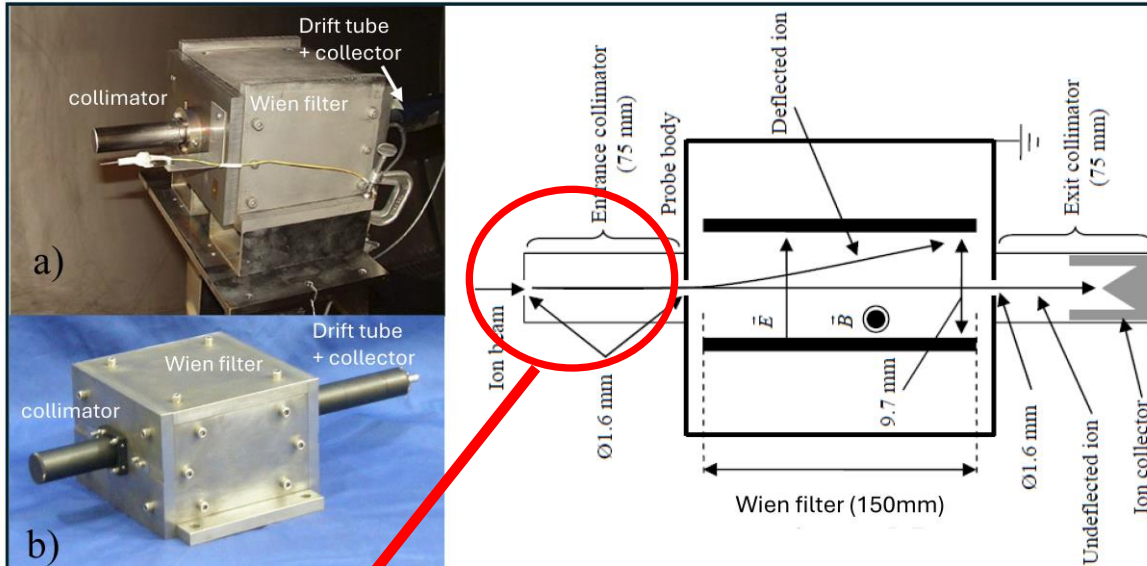


Figure 7-5 Schematic of Hughes $E \times B$ probe



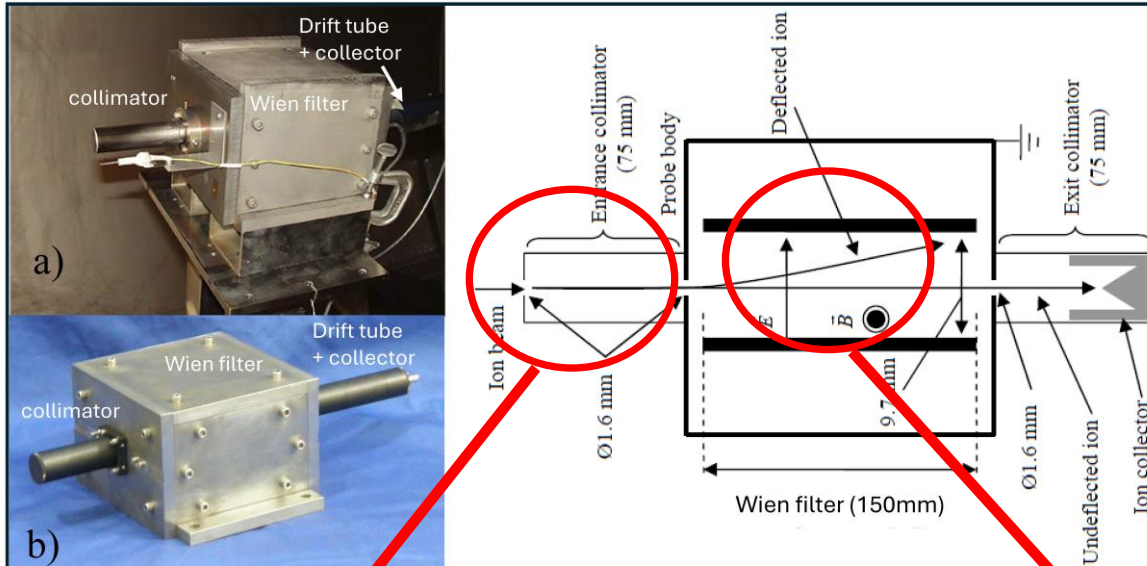
Design



Collimator:

- Entrance orifice size to Debye length ratio: $r_1/\lambda_d \ll 1$
- Collimator OD to orifice ratio for flat sheath: $r_1/r_{collimator} \ll 1$
- Longer improved angular filtering but reduces signal: $\alpha_{max} = \tan^{-1} \left(\frac{r_1 + r_2}{l_c} \right)$

Design



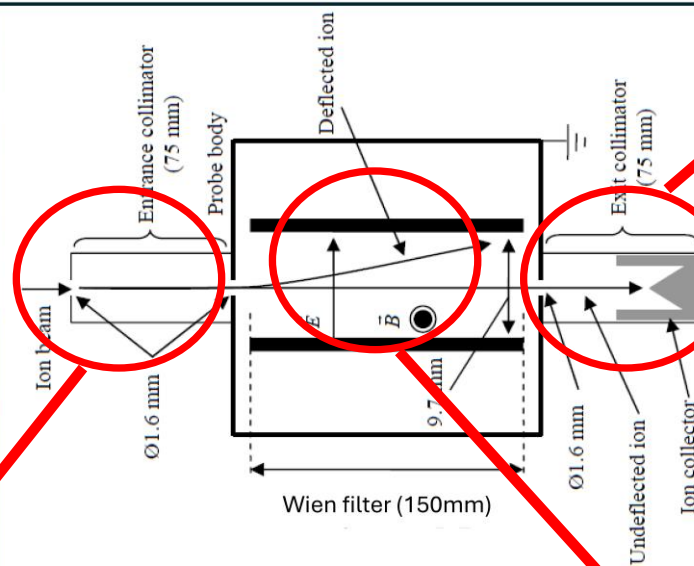
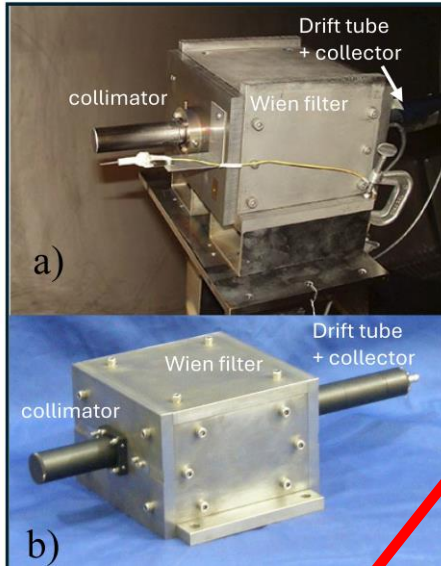
Collimator:

- Entrance orifice size to Debye length ratio: $r_1/\lambda_d \ll 1$
- Collimator OD to orifice ratio for flat sheath: $r_1/r_{collimator} \ll 1$
- Longer improved angular filtering but reduces signal: $\alpha_{max} = \tan^{-1} \left(\frac{r_1 + r_2}{l_c} \right)$

Wien Filter Region:

- Bfield – high temp. SmCo permanent magnets – 0.15 – 0.4 T
- SS or Mo electrodes – some gold plating
- Housing – shapes field (low-carbon steel, 430SS) or passive (alum, graphite)
- Electrical isolation – high temp ceramic insulators (alumina, macor, BN)

Design



Collector:

- Secondary electron emission mitigation with cone-in-cylinder design, low SEE material, (e.g., Mo, W), SEE suppression electrode
- SEE correction with known SEE yield

$$I_k = q_k n_k v_k A_c (1 + \gamma_k)$$

Xenon Charge State	Molybdenum	Tungsten
1	0.022	0.016
2	0.20	0.20
3	0.70* est. from W	0.71

Collimator:

- Entrance orifice size to Debye length ratio: $r_1/\lambda_d \ll 1$
- Collimator OD to orifice ratio for flat sheath: $r_1/r_{collimator} \ll 1$
- Longer improved angular filtering but reduces signal: $\alpha_{max} = \tan^{-1} \left(\frac{r_1 + r_2}{l_c} \right)$

Wien Filter Region:

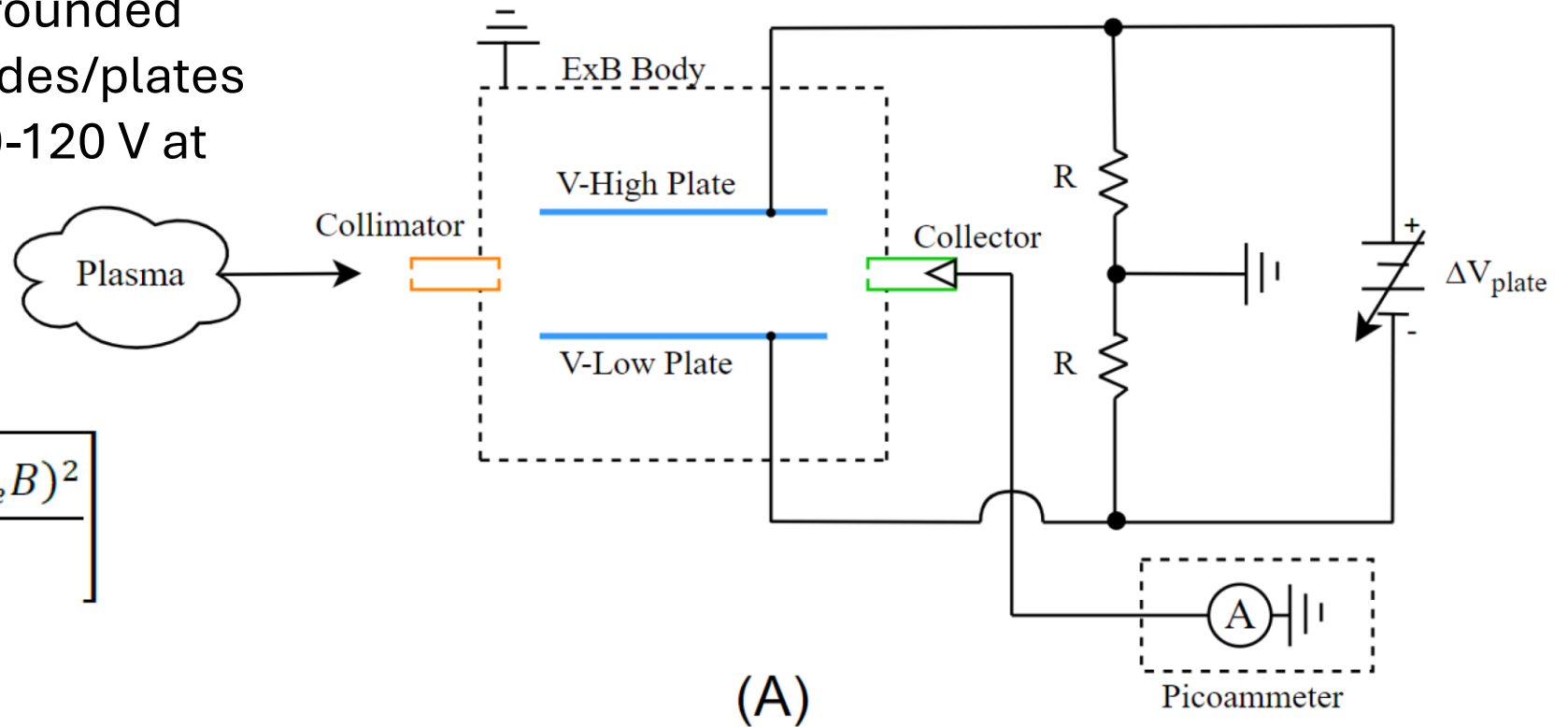
- Bfield – high temp. SmCo permanent magnets – 0.15 – 0.4 T
- SS or Mo electrodes – some gold plating
- Housing – shapes field (low-carbon steel, 430SS) or passive (alum, graphite)
- Electrical isolation – high temp ceramic insulators (alumina, macor, BN)

Implementation and Operation

Electrical:

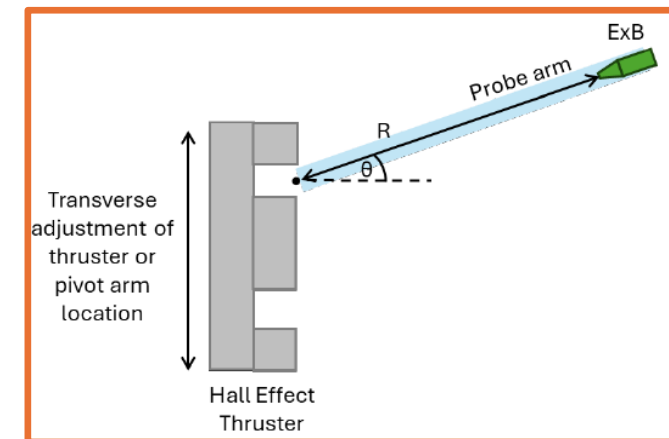
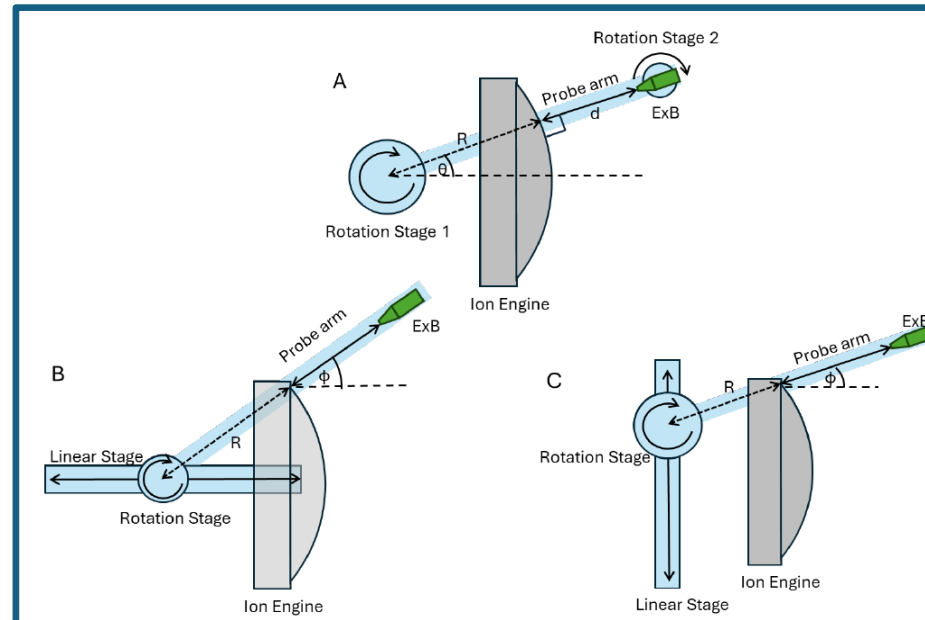
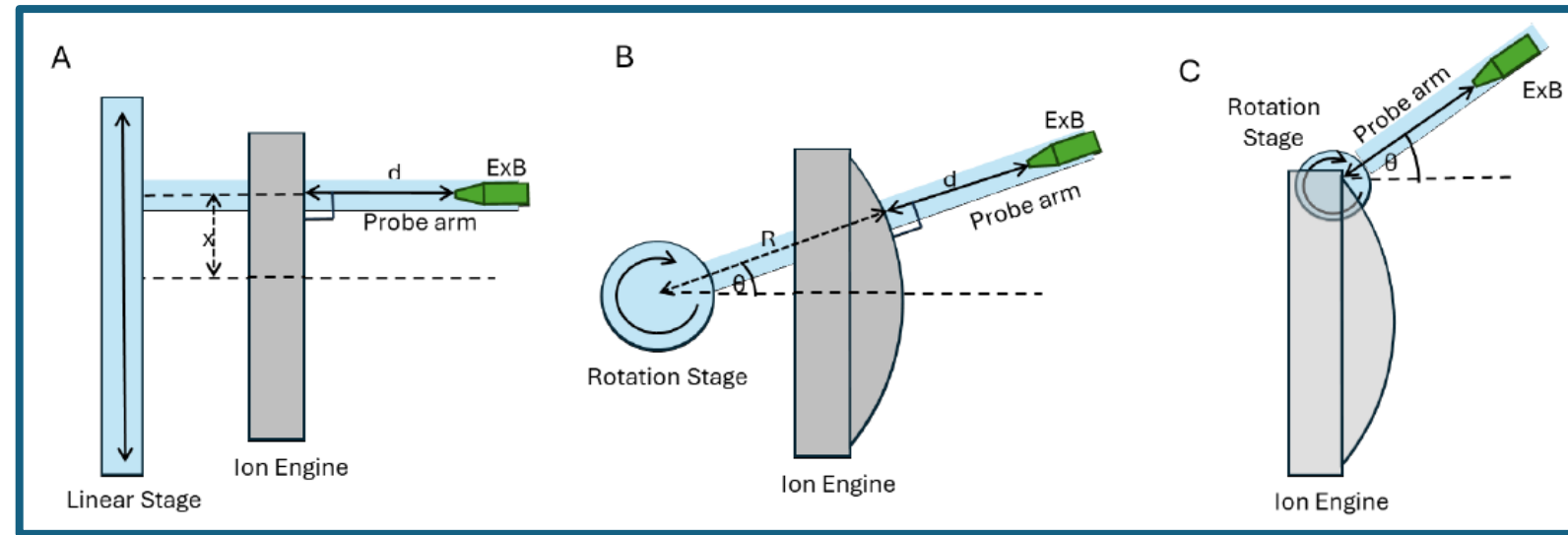
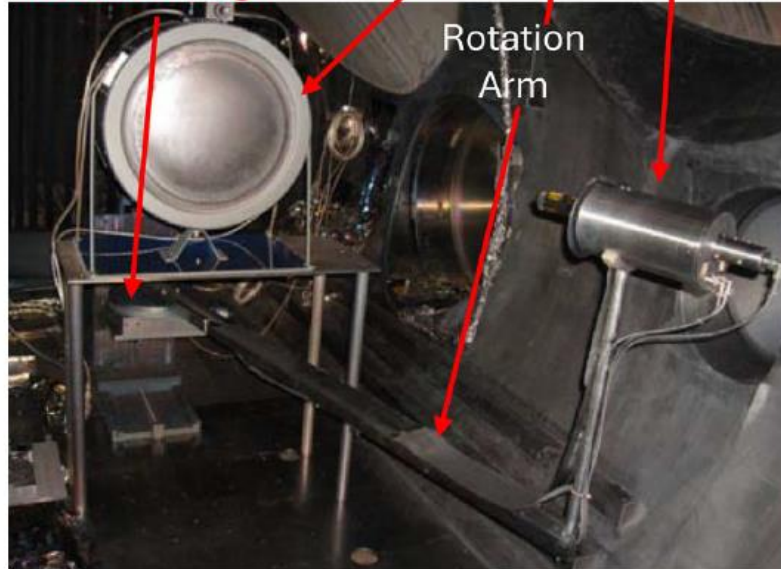
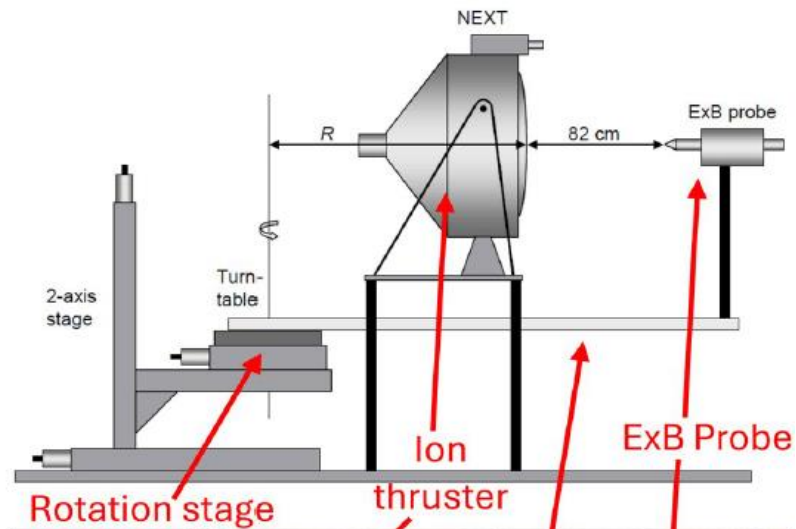
- Grounded probe body – exterior surfaces in contact with plasma are grounded
- Symmetric biasing of electrodes/plates
- Plates biasing range typical 0-120 V at typical 1 V increments

$$V_{plates,range} = \left[0, 1.5 \sqrt{\frac{2eZV_{accel}(d_e B)^2}{m}} \right]$$



Implementation and Operation

Physical Setup:



Data Analysis

Peak Height Analysis:

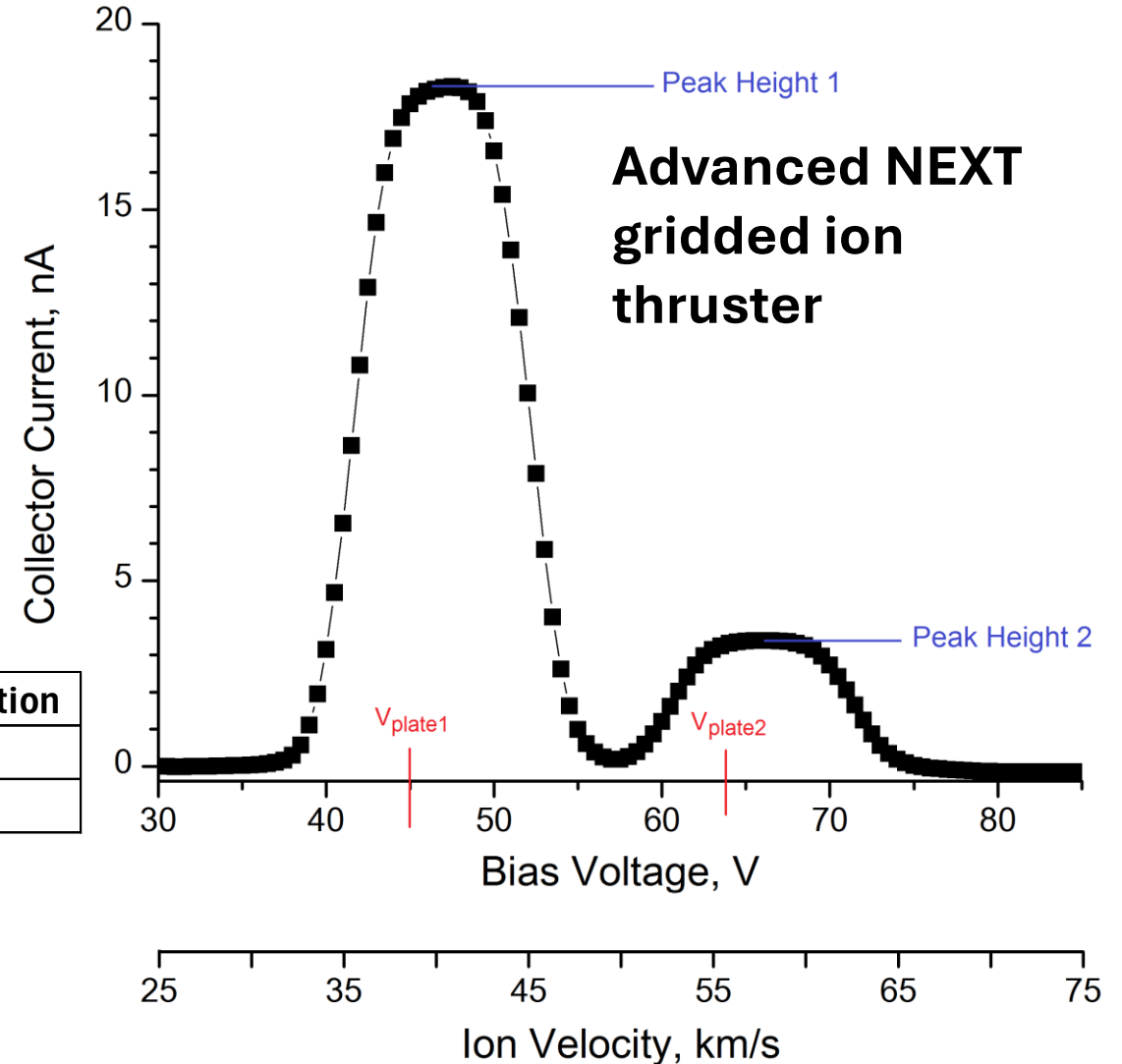
- Recommended for:
 - Narrow monoenergetic ion beams (all ions same V_{accel})
 - Relatively wide velocity resolution probe
 - Clearly separated species mass spectrum
- Typical in GIT current ratio and species ratio analysis

Species fraction $\zeta_j \approx \frac{\Omega_j / Z_j^{3/2}}{\sum_j \Omega_j / Z_j^{3/2}}$

j species	Z charge-state	I (nA)	Ω (-) Current Fraction	ζ (-) Species Fraction
1	1	18.5	0.841	0.937
2	2	3.5	0.159	0.063

Doubles-to-Singles
Current Ratio

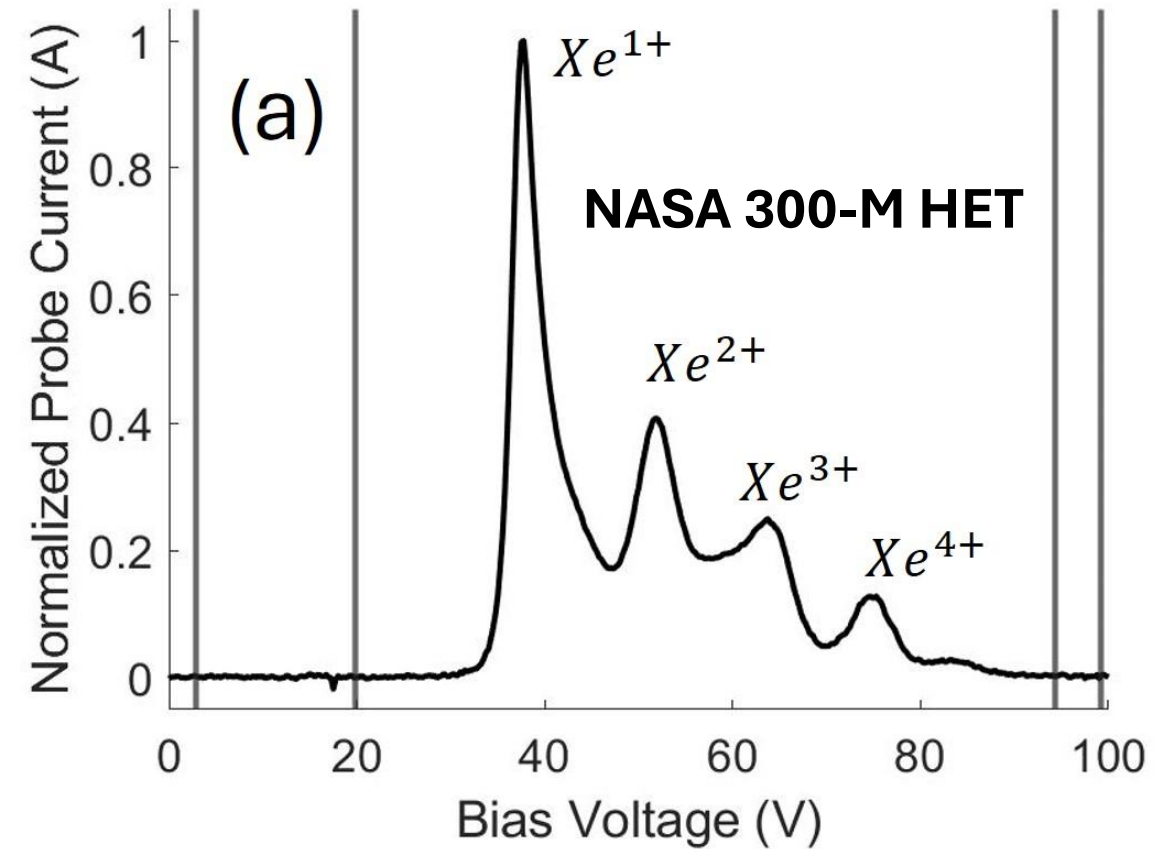
19%



Data Analysis

Simplified Integration:

- Recommended for:
 - Broader energy ion beams
 - Identifiable, but overlapping species mass spectrum
- Directly fit an assumed IVDF shape to the measured IV curve from the probe
- Ignores velocity resolution scaling with Wien velocity, $I_j(V_{\text{plates}}) = K_1 n_j V_{\text{plates}}^3 f_j(K_2 V_{\text{plates}})$
- HET current ratio and species ratio analysis



Triangle:

$$f_j(v) = \begin{cases} (-a/b)|v - c| + a, & c - b < v < c + b \\ 0, & \text{else} \end{cases}$$

Gaussian:

$$f_j(v) = a \exp[-b(v - c)^2]$$

Variable Exponent:

$$f_j(v) = a \exp[-b|v - c|^n]$$

Twin/Bi Gaussian:

$$f_j(v) = a_1 \exp[-b_1(v - c_1)^2] + a_2 \exp[-b_2(v - c_2)^2]$$

Skew-Normal:

$$f_j(v) = a \exp\left[-\frac{(v - c)^2}{2b^2}\right] \left\{ 1 + \operatorname{erf}\left[-\frac{d * (v - c)}{\sqrt{2}b^2}\right] \right\}$$

Current Ratio

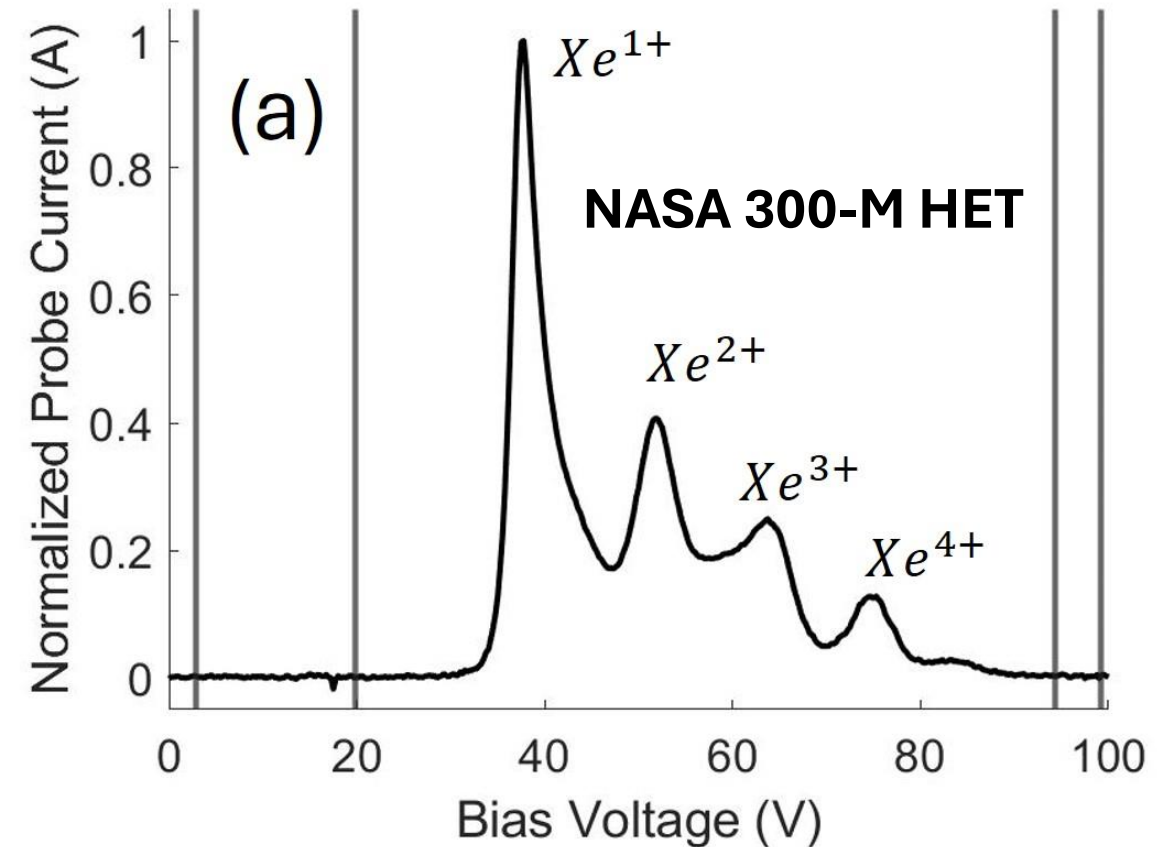
“Area under the curve”

$$\Omega_j = \frac{\int_0^\infty I_j(V_{\text{plates}}) dV_{\text{plates}}}{\sum_j \int_0^\infty I_j(V_{\text{plates}}) dV_{\text{plates}}}$$

Data Analysis

Simplified Integration:

- Recommended for:
 - Broader energy ion beams
 - Identifiable, but overlapping species mass spectrum
- Directly fit an assumed IVDF shape to the measured IV curve from the probe
- Ignores velocity resolution scaling with Wien velocity, $I_j(V_{\text{plates}}) = K_1 n_j V_{\text{plates}}^3 f_j(K_2 V_{\text{plates}})$
- HET current ratio and species ratio analysis



Triangle:

$$f_j(v) = \begin{cases} (-a/b)|v - c| + a, & c - b < v < c + b \\ 0, & \text{else} \end{cases}$$

Gaussian:

$$f_j(v) = a \exp[-b(v - c)^2]$$

Variable Exponent:

$$f_j(v) = a \exp[-b|v - c|^n]$$

Twin/Bi Gaussian:

$$f_j(v) = a_1 \exp[-b_1(v - c_1)^2] + a_2 \exp[-b_2(v - c_2)^2]$$

Skew-Normal:

$$f_j(v) = a \exp\left[-\frac{(v - c)^2}{2b^2}\right] \left\{ 1 + \operatorname{erf}\left[-\frac{d * (v - c)}{\sqrt{2}b^2}\right] \right\}$$

Current Ratio

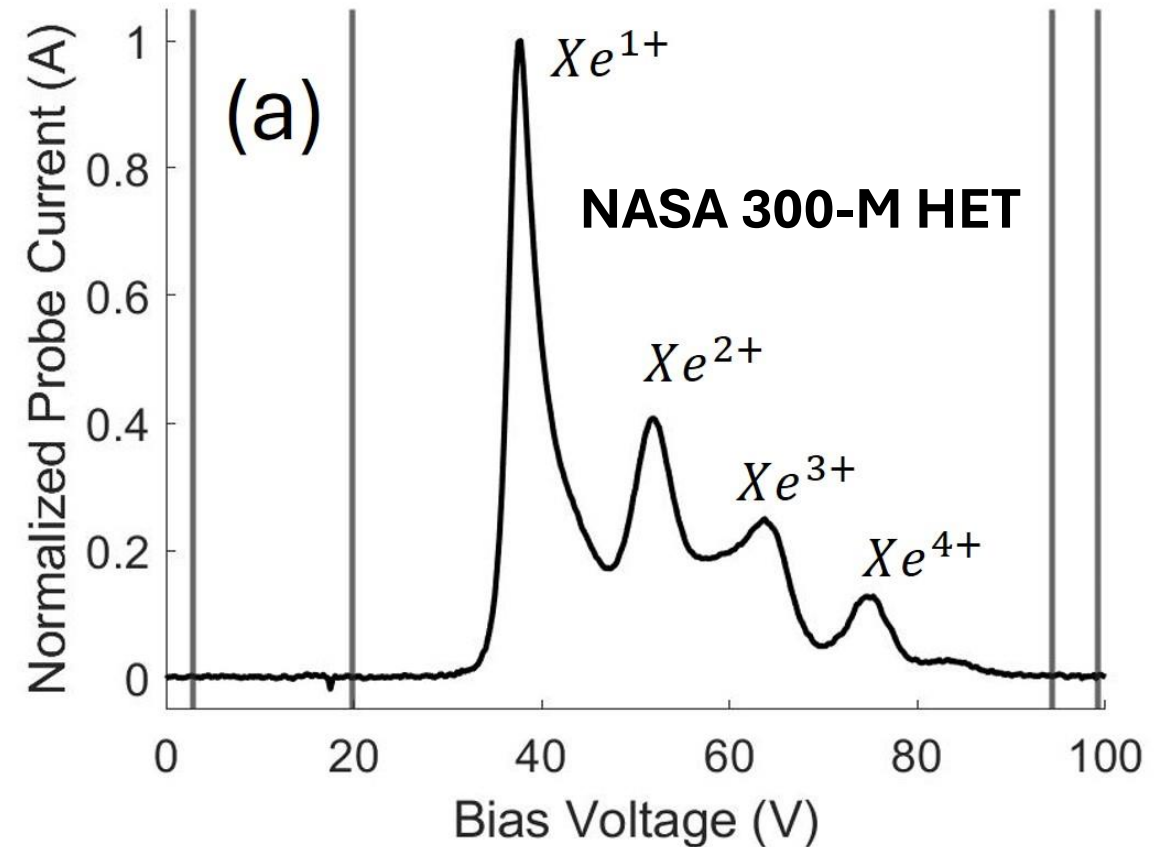
“Area under the curve”

$$\Omega_j = \frac{\int_0^\infty I_j(V_{\text{plates}}) dV_{\text{plates}}}{\sum_j \int_0^\infty I_j(V_{\text{plates}}) dV_{\text{plates}}}$$

Data Analysis

Simplified Integration:

- Recommended for:
 - Broader energy ion beams
 - Identifiable, but overlapping species mass spectrum
- Directly fit an assumed IVDF shape to the measured IV curve from the probe
- Ignores velocity resolution scaling with Wien velocity, $I_j(V_{\text{plates}}) = K_1 n_j V_{\text{plates}}^3 f_j(K_2 V_{\text{plates}})$
- HET current ratio and species ratio analysis



Triangle:

$$f_j(v) = \begin{cases} (-a/b)|v - c| + a, & c - b < v < c + b \\ 0, & \text{else} \end{cases}$$

Gaussian:

$$f_j(v) = a \exp[-b(v - c)^2]$$

Variable Exponent:

$$f_j(v) = a \exp[-b|v - c|^n]$$

Twin/Bi Gaussian:

$$f_j(v) = a_1 \exp[-b_1(v - c_1)^2] + a_2 \exp[-b_2(v - c_2)^2]$$

Skew-Normal:

$$f_j(v) = a \exp\left[-\frac{(v - c)^2}{2b^2}\right] \left\{ 1 + \operatorname{erf}\left[-\frac{d * (v - c)}{\sqrt{2}b^2}\right] \right\}$$

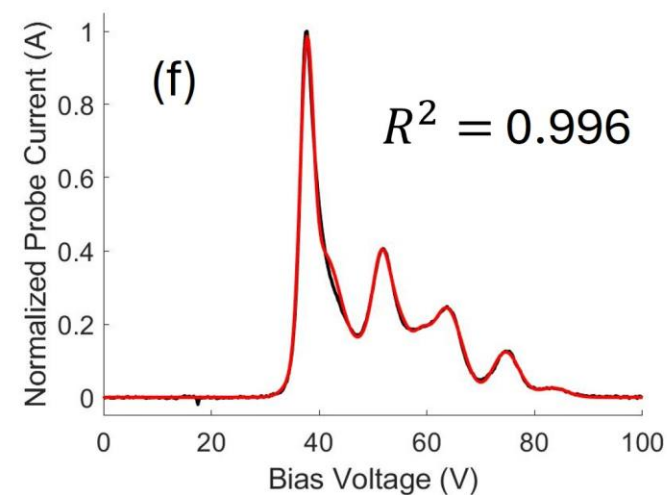
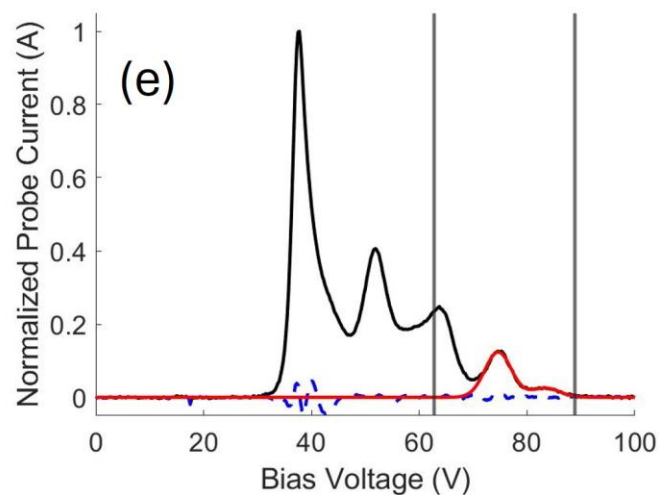
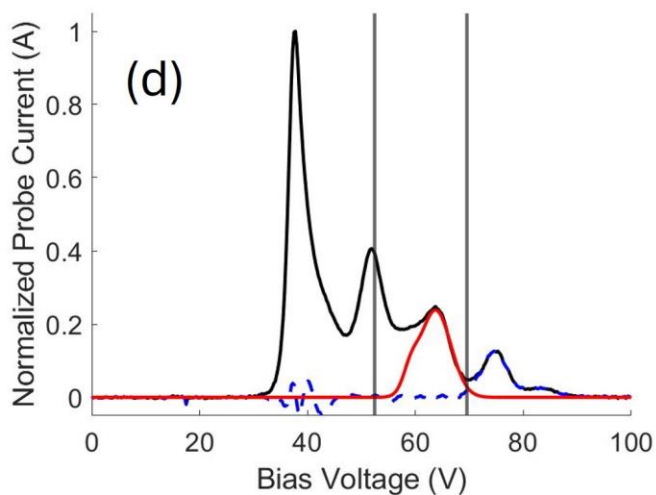
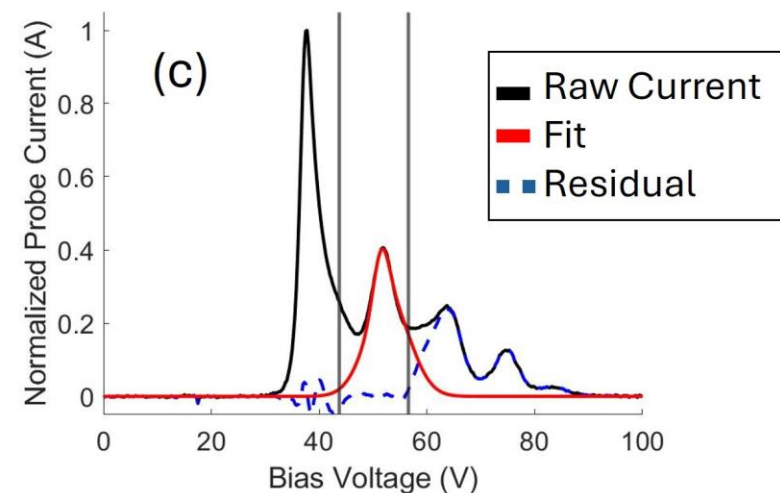
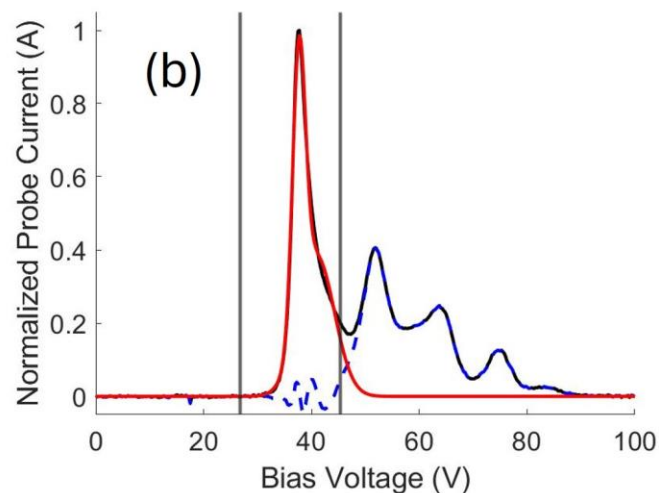
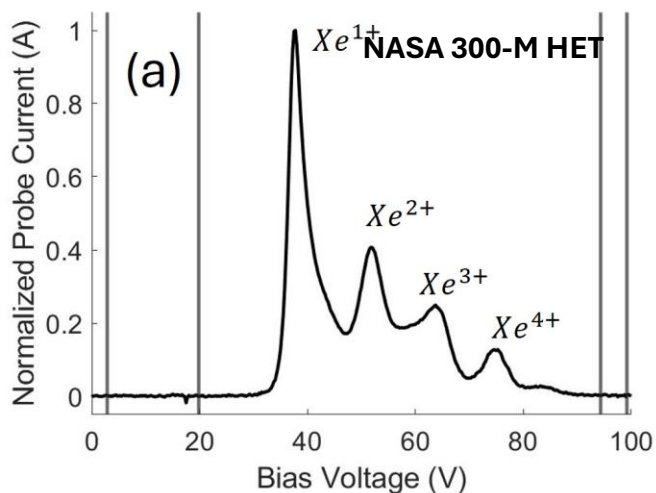
Current Ratio

“Area under the curve”

$$\Omega_j = \frac{\int_0^\infty I_j(V_{\text{plates}}) dV_{\text{plates}}}{\sum_j \int_0^\infty I_j(V_{\text{plates}}) dV_{\text{plates}}}$$

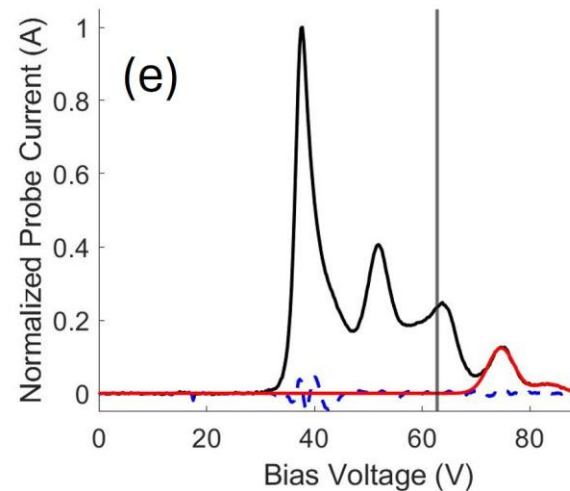
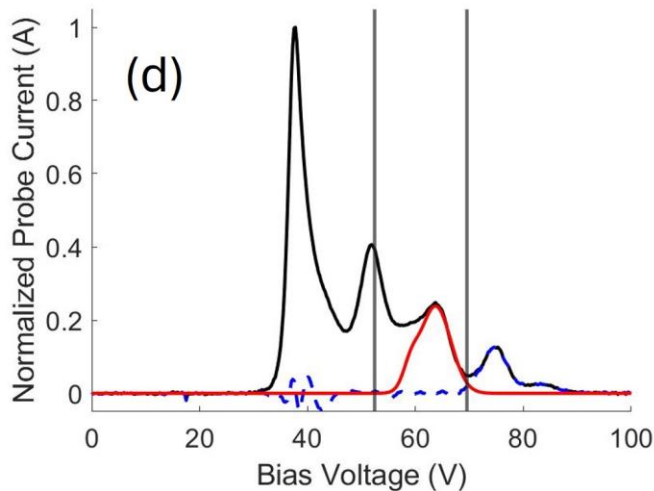
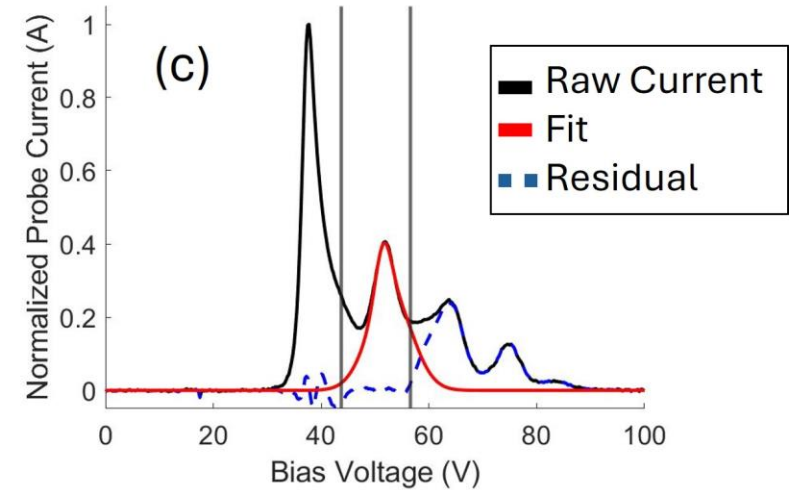
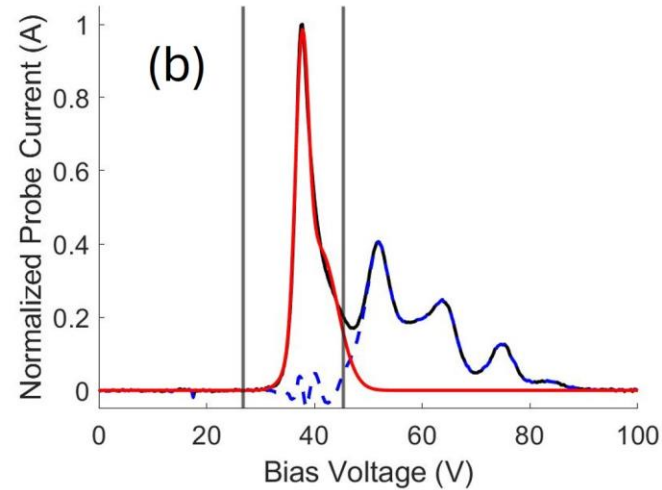
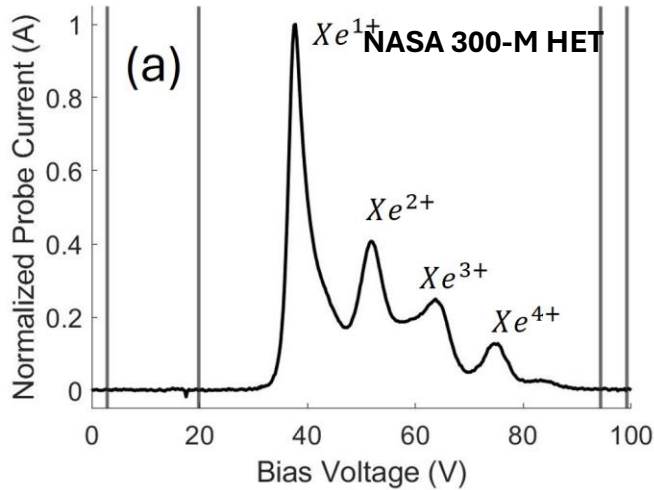
Data Analysis

Simplified Integration:



Data Analysis

Simplified Integration:



Species	Current fraction (Ω)	Species fraction (ζ)
Xe^{+}	0.48	0.78
Xe^{2+}	0.24	0.14
Xe^{3+}	0.19	0.06
Xe^{4+}	0.09	0.02

Data Analysis

Charge Exchange Correction:

- Recommended that ExB data always be corrected for CEX
- Current density at the probe is lower/attenuated due to CEX collisions with background gas
- Attenuation is different for different species

$$\begin{aligned} (I/I_0)_1 &= \exp(-n_0 \sigma_1 z), & \sigma_1 &= [87.3 - 13.6 \log(V_1)] \times 10^{-20} \text{m}^2 \\ (I/I_0)_2 &= \exp(-n_0 \sigma_2 z), & \sigma_2 &= [45.7 - 8.9 \log(2V_2)] \times 10^{-20} \text{m}^2 \\ (I/I_0)_3 &= \exp(-n_0 \sigma_3 z), & \sigma_3 &= [16.9 - 3.0 \log(3V_3)] \times 10^{-20} \text{m}^2 \end{aligned}$$

CEX Corrected
Current Fraction

$$\Omega_j^c = \frac{\Omega_j [(I/I_0)_j]^{-1}}{\sum_{j=1,2,3} \Omega_j [(I/I_0)_j]^{-1}}$$

Current Fraction from Peak
Height or Simplified Integration

Conclusion

Recommendations Include:

- Sizing the probe velocity resolution for the application with resolution 10x smaller than IVDF width
- Probe component scaling and material considerations are recommended:
 - Collimator OD and orifice size
 - Collector SEE effects mitigation and correction
- ExB measurements should be accompanied by Langmuir probe or emissive probe measurements to correct for sheath ion acceleration by plasma potential
- An ExB plate bias voltage range and resolution is recommended.
- Data analysis:
 - Peak Height data analysis is recommended for ion sources with narrow IVDF (e.g., GIT)
 - Simplified Integration analysis is recommended for broader energy ion sources (e.g., HET)
 - When used in this way, other sources of uncertainty dominate over the analysis
 - Data must be corrected for charge-exchange attenuation
- Additional recommendations regarding probe Transmittancy and IVDF reconstruction are provided in the paper