

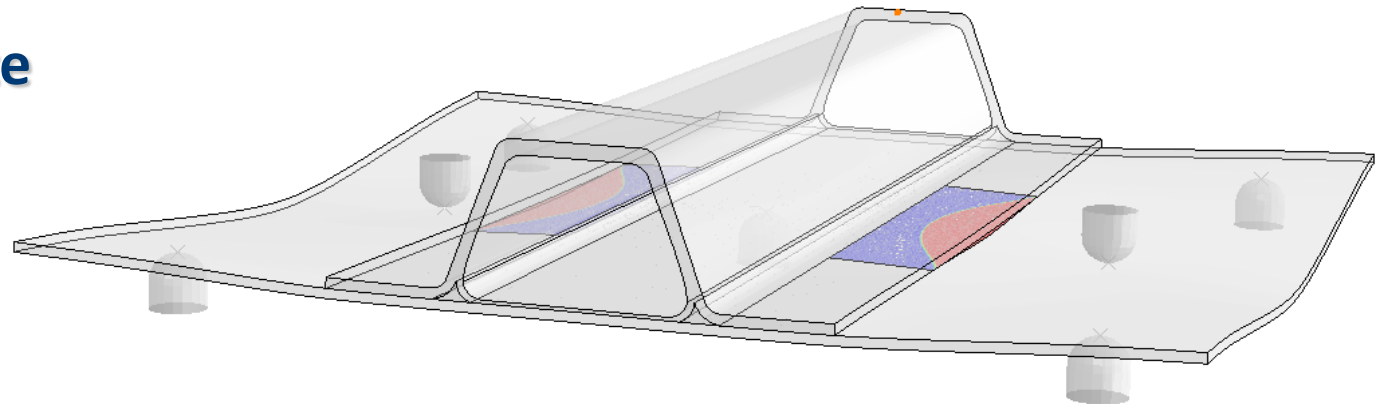
Softening the Gap between Wöhler and Paris

– New Approaches for Fatigue Analysis –

Carlos G. Dávila

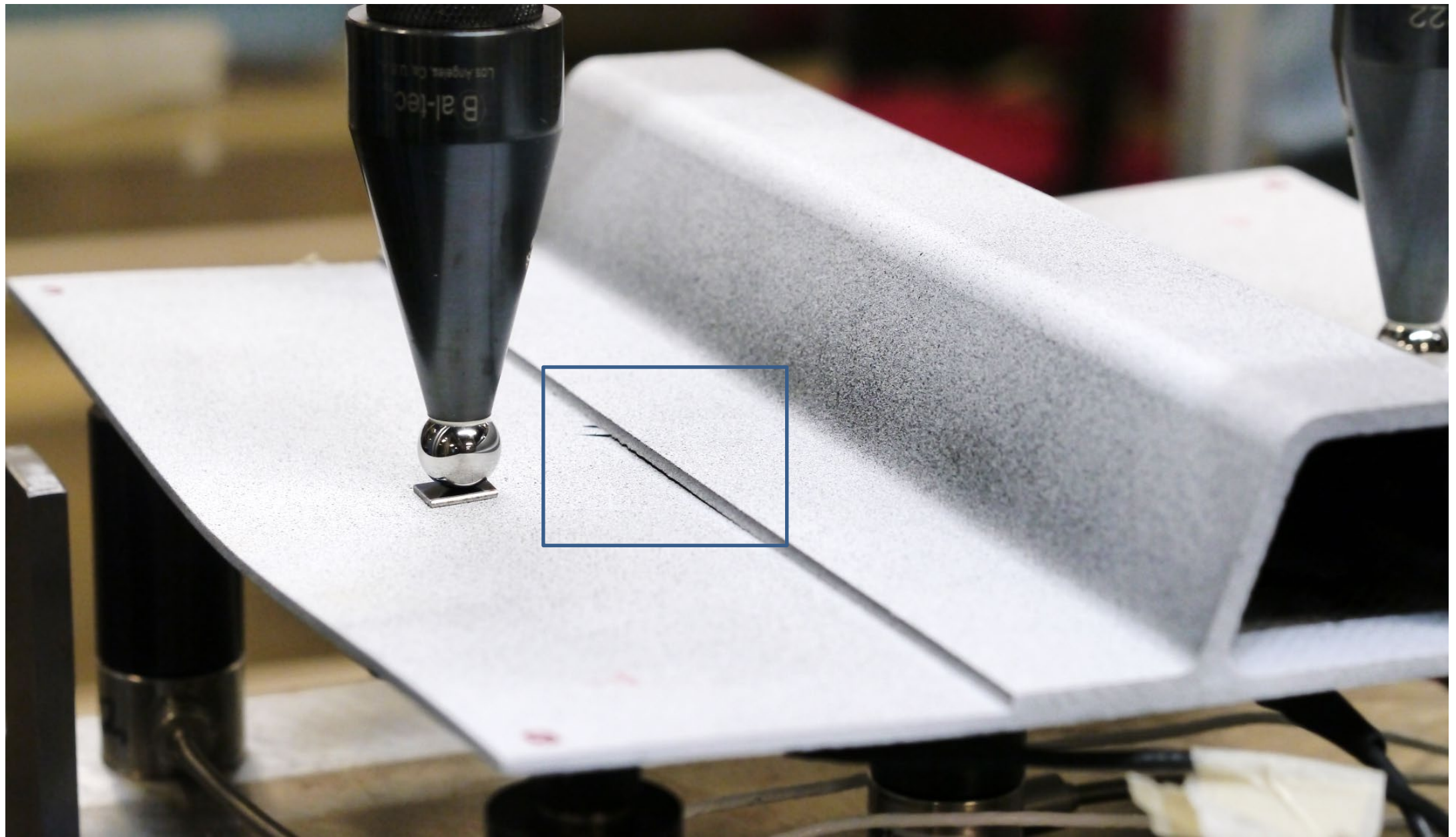
Emeritus Langley Associate

(NASA – retired)

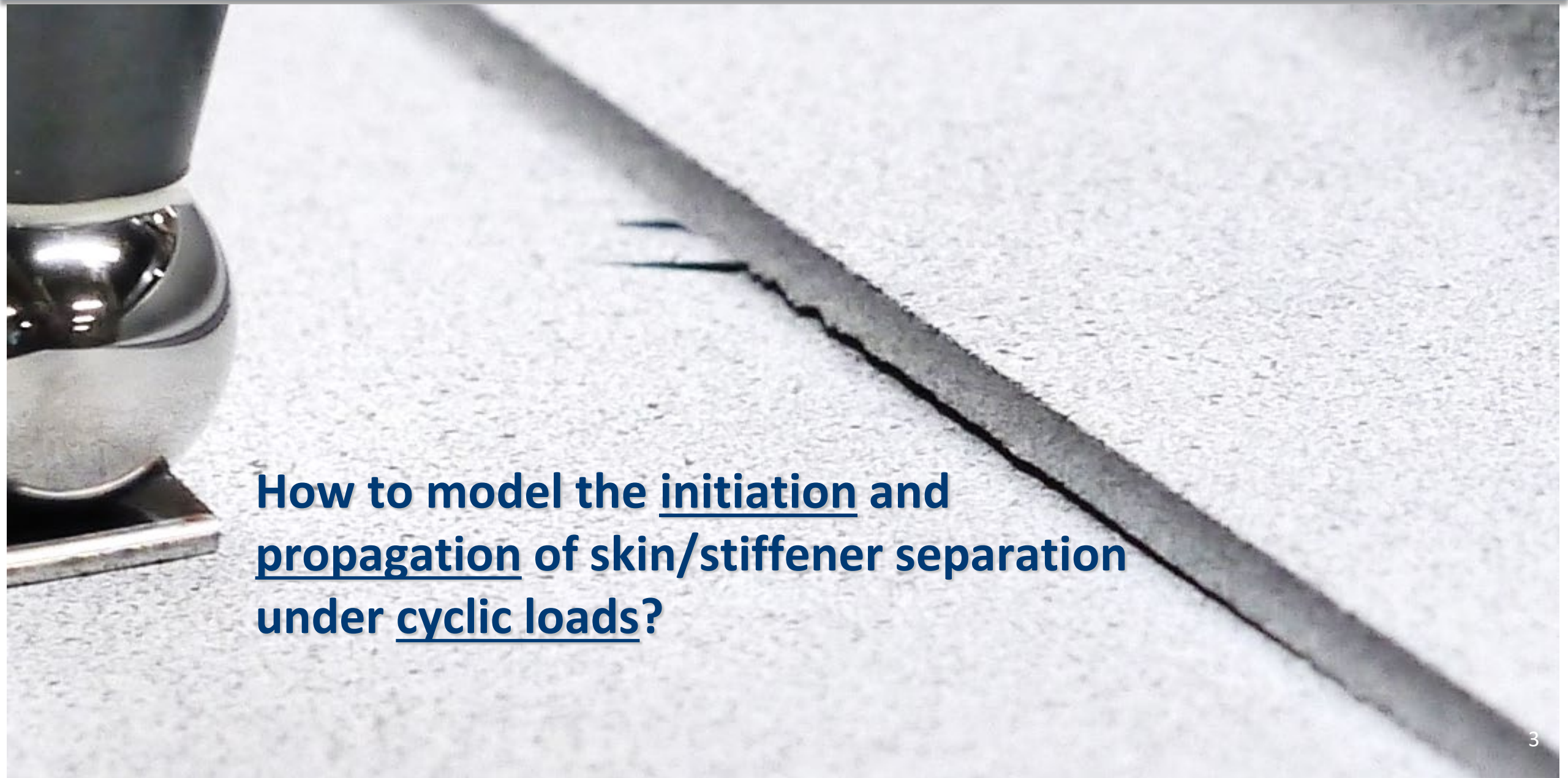


5th International Conference on Mechanics of Advanced Materials and Structures
1-3 July 2026, Institut Clément Ader, Toulouse, France

Motivation: Skin/Stiffener Separation



Motivation: Skin/Stiffener Separation



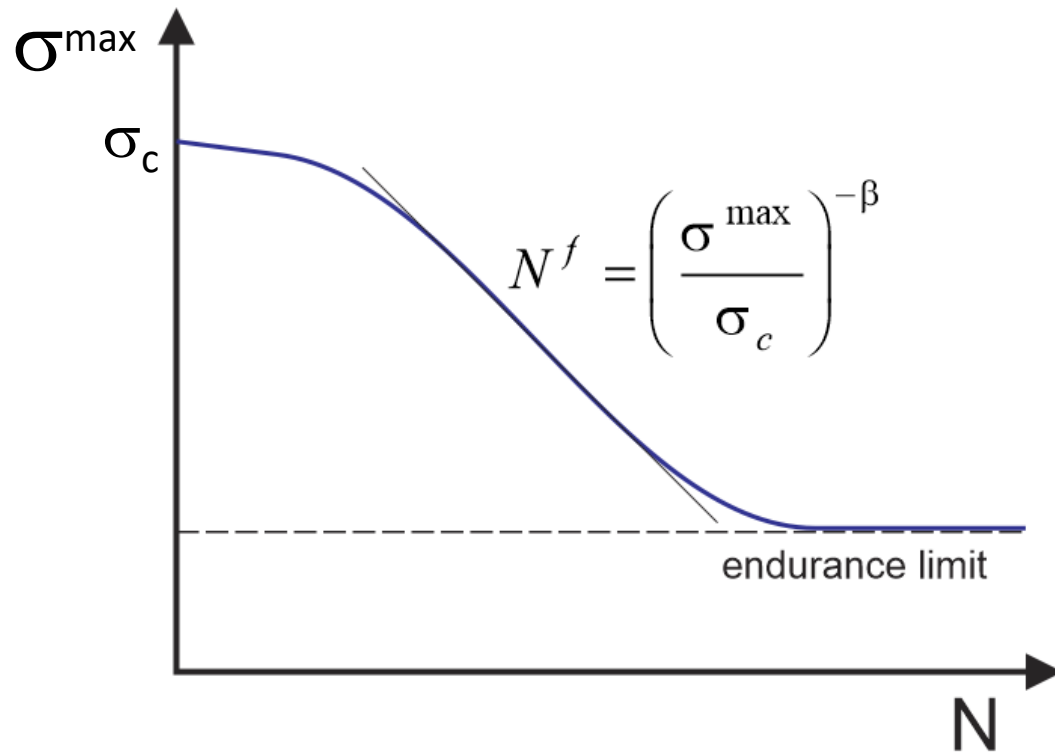
How to model the initiation and propagation of skin/stiffener separation under cyclic loads?

Fatigue Analysis

What fatigue analysis tools do you use?

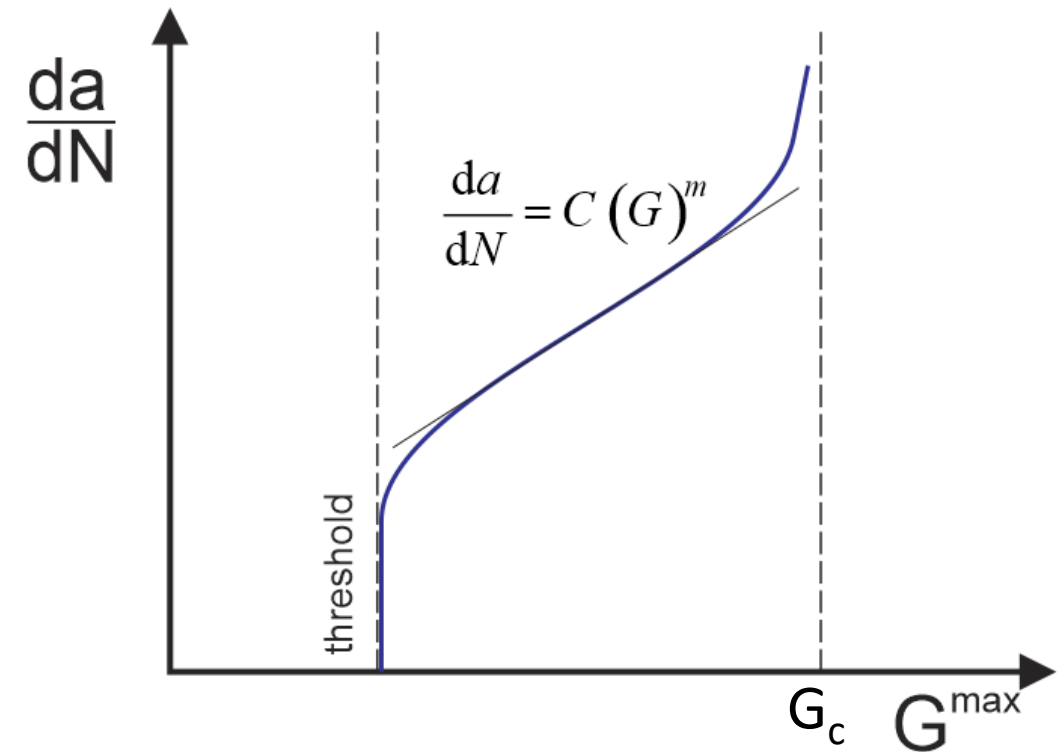
Fatigue: Strength or Fracture Mechanics?

Strength: Wöhler (S-N Curve)



- Safe-life design

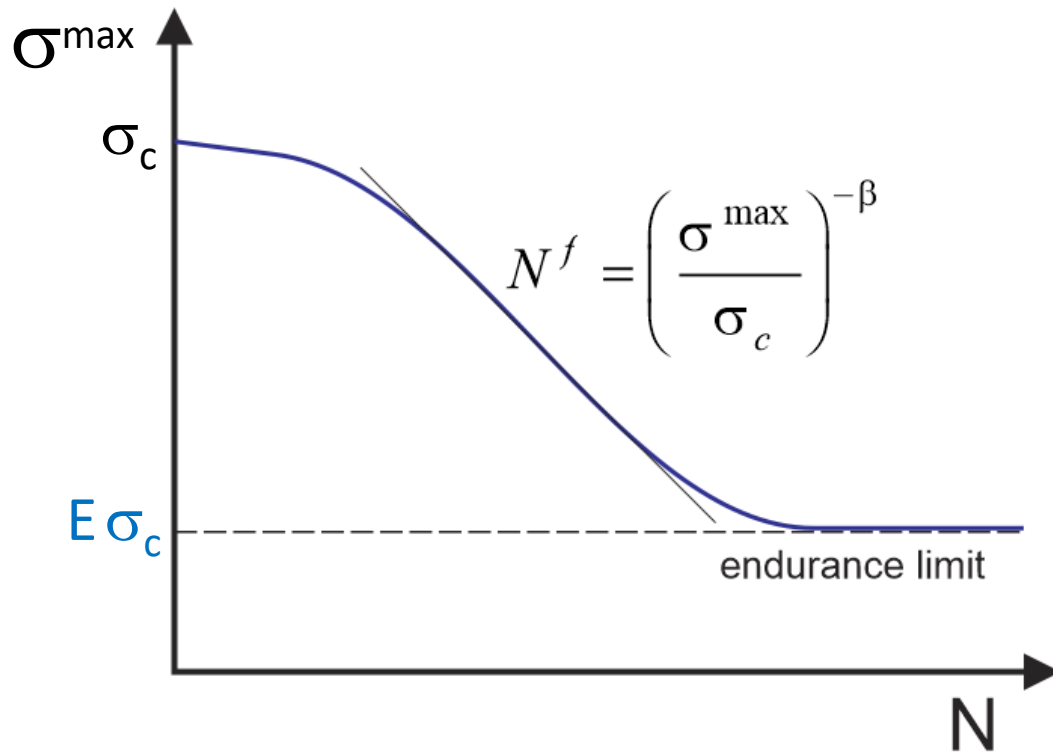
Fracture: Paris Law



- Damage tolerant design:
 - Slow-growth
 - Fail-safe
 - No-growth

Fatigue: Strength or Fracture Mechanics?

Strength: Wöhler (S-N Curve)

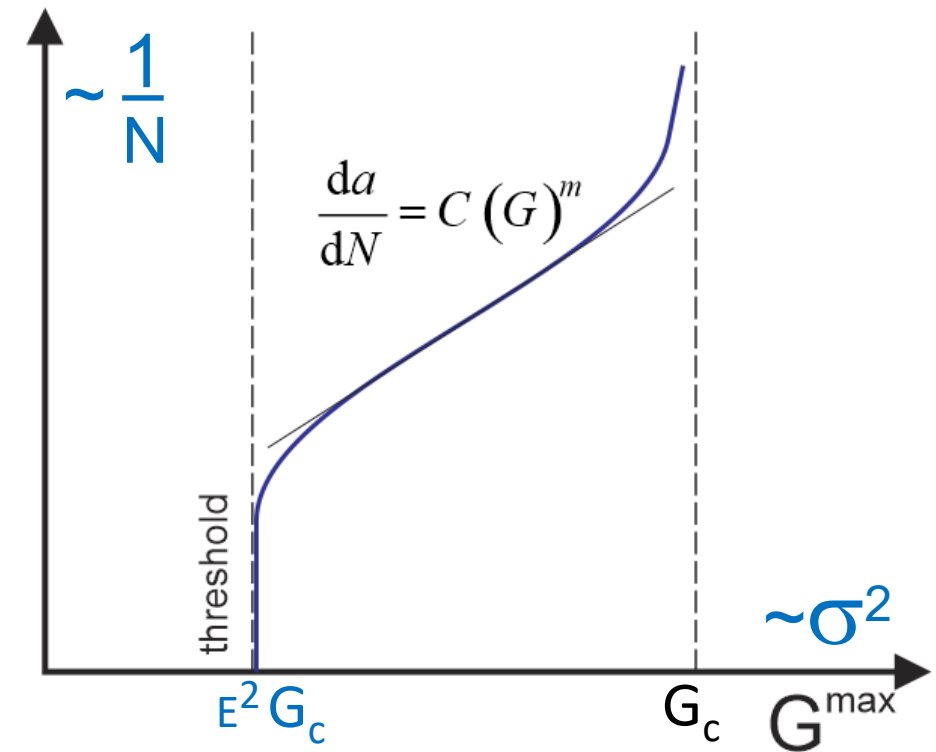


$\frac{da}{dN}$

← →

Allegri, 2013

Fracture: Paris Law



S-N Curve and Paris law are related: $\beta = 2m$

The Issue of Strength Scaling

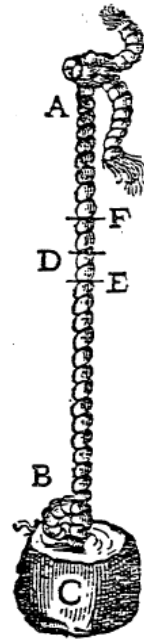
(when analysis tools were linear)

Scaling of Structural Strength

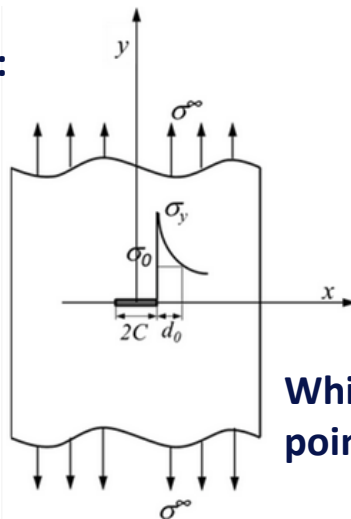
Strength of Materials

*"resistance increases
with cross-section"*

da Vinci, 1505
Galileo, 1638



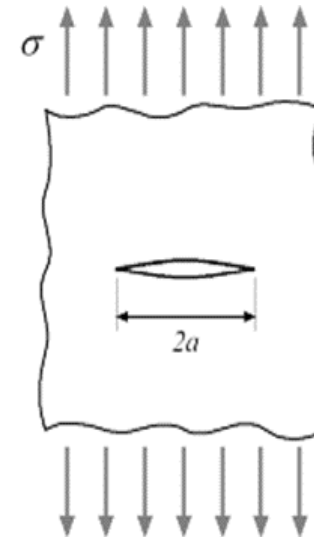
Notches:



Whitney-Nuismer
point stress criterion

Fracture Mechanics (Griffith, 1921)

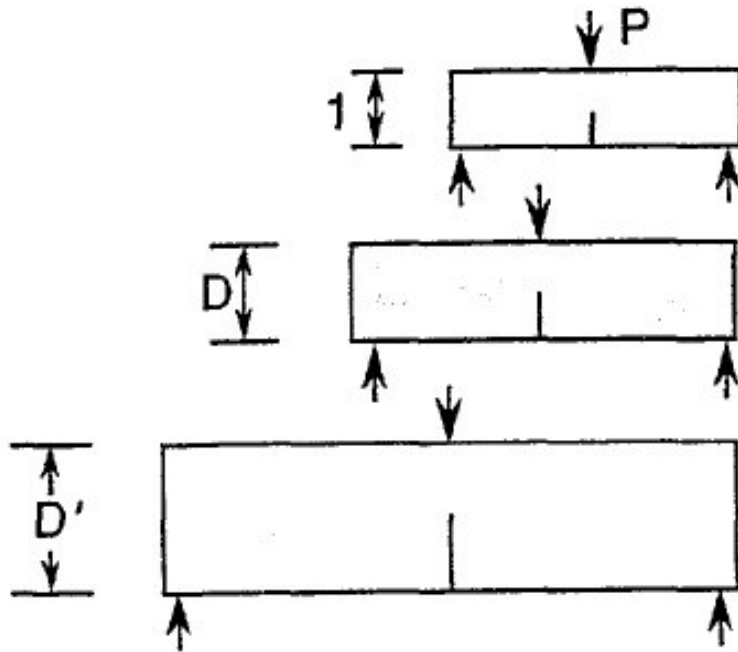
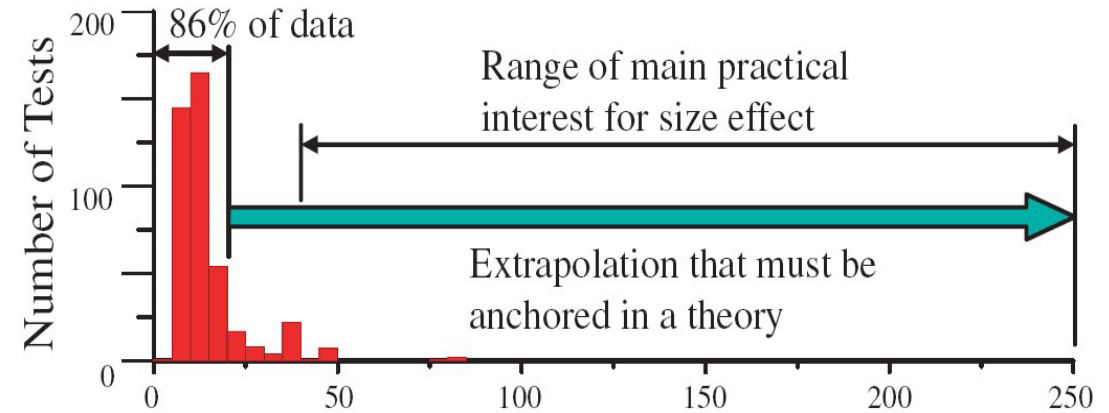
*"weakness is due to
the presence of flaws"*



$$\sigma_u = \sqrt{\frac{E G_c}{\pi a}}$$

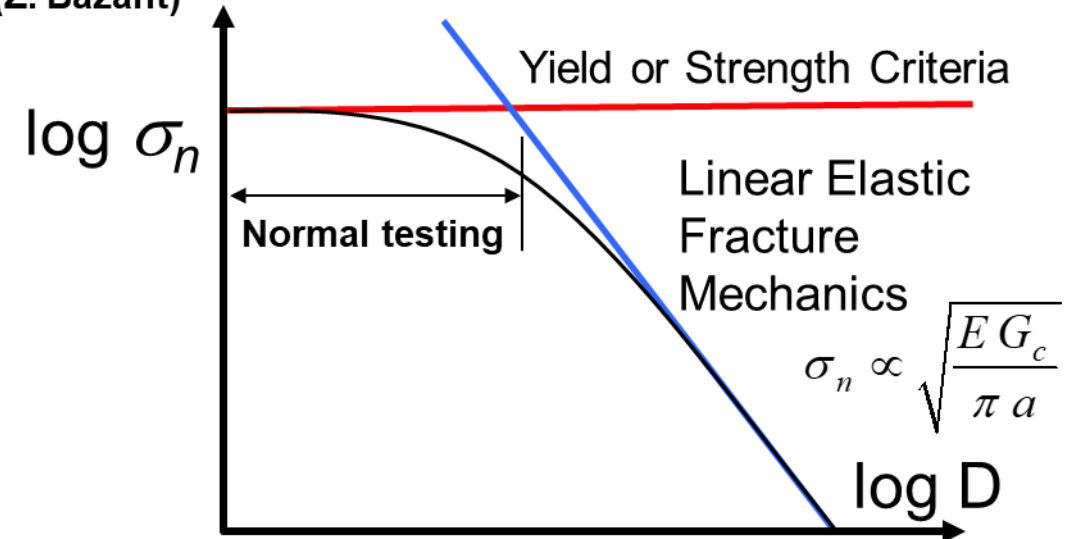
**While the aerospace engineers were arguing,
the civil engineers...**

Scaling: the Effect of Structure Size on Strength

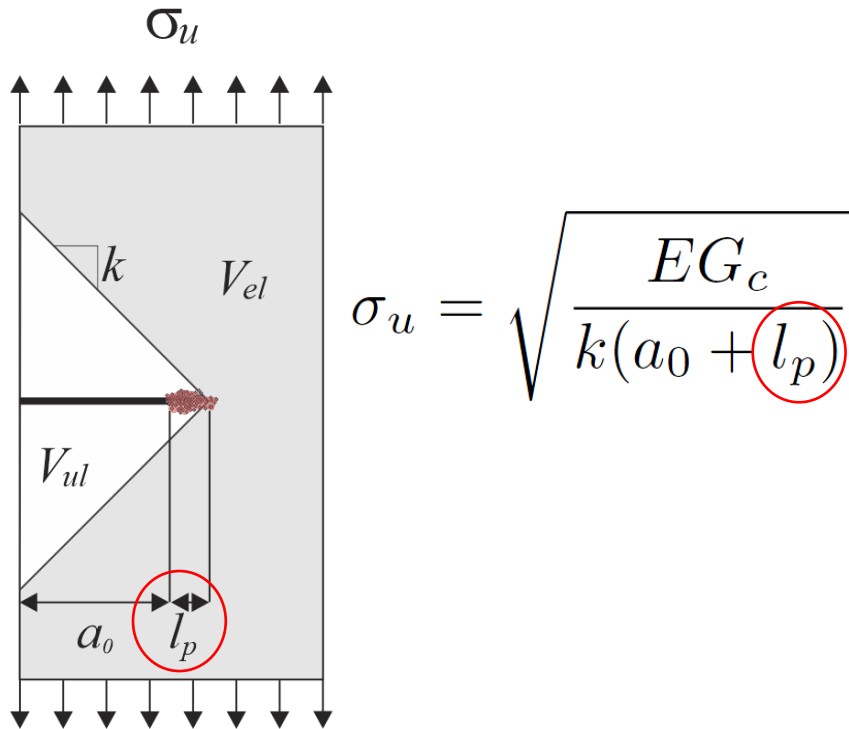


Z. Bažant, Scaling of Structural Failure, 1997

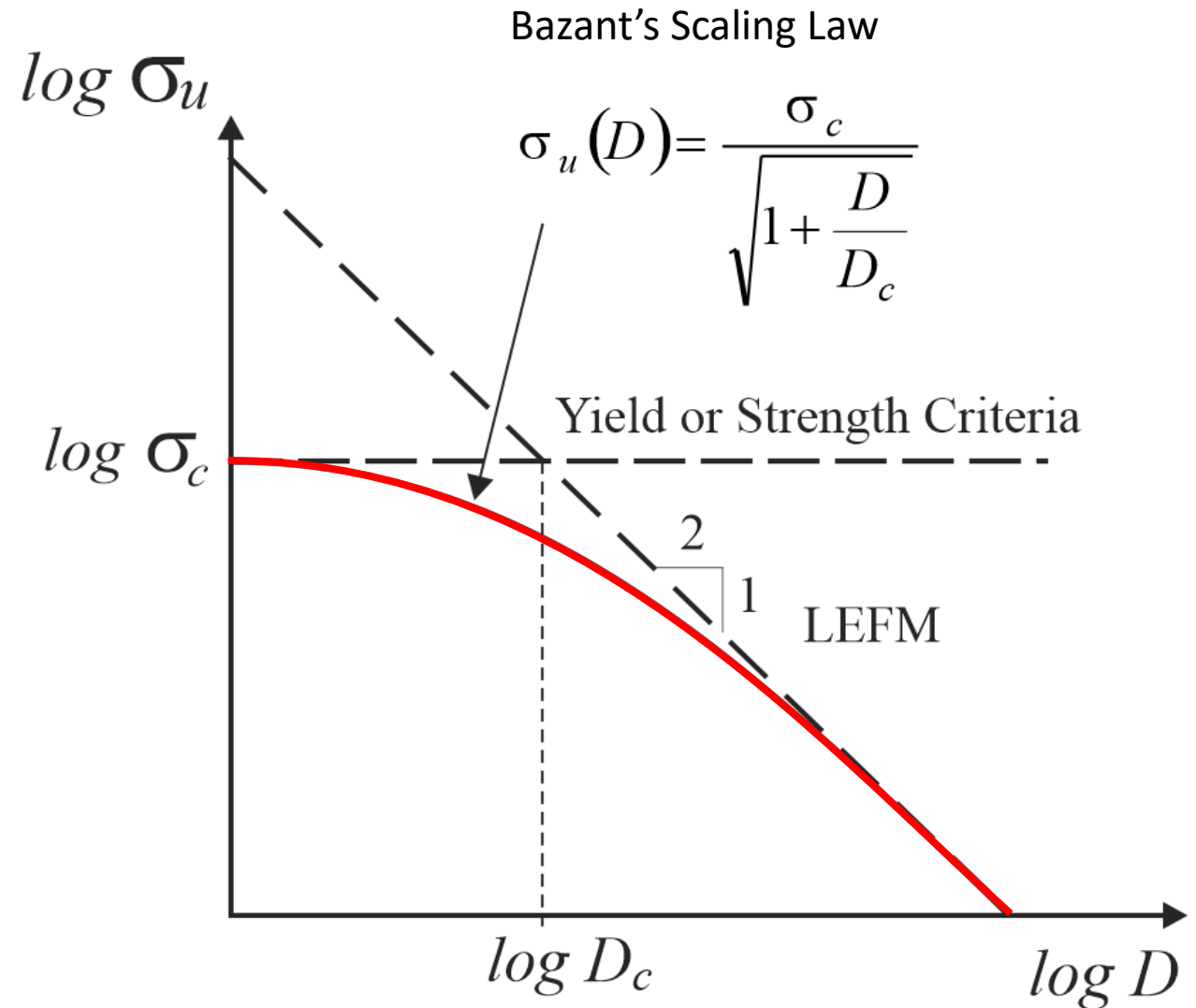
Scaling Laws (Z. Bažant)



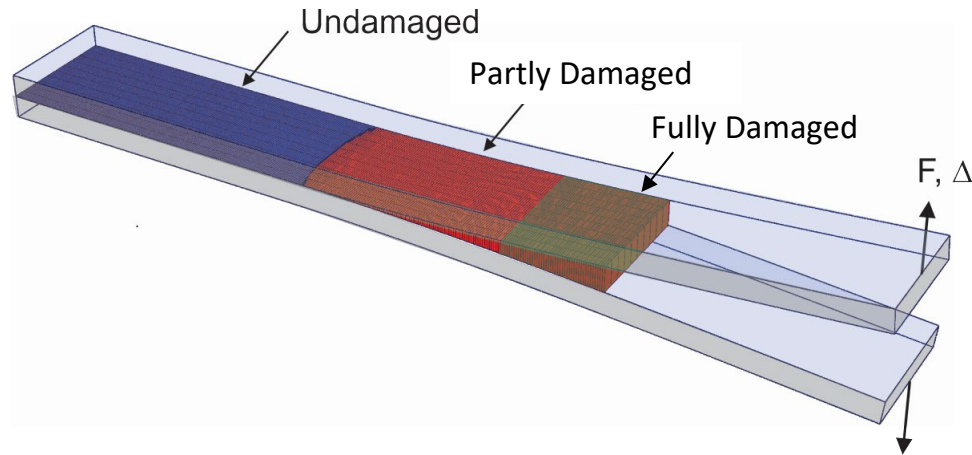
Scaling: the Effect of Structure Size on Strength



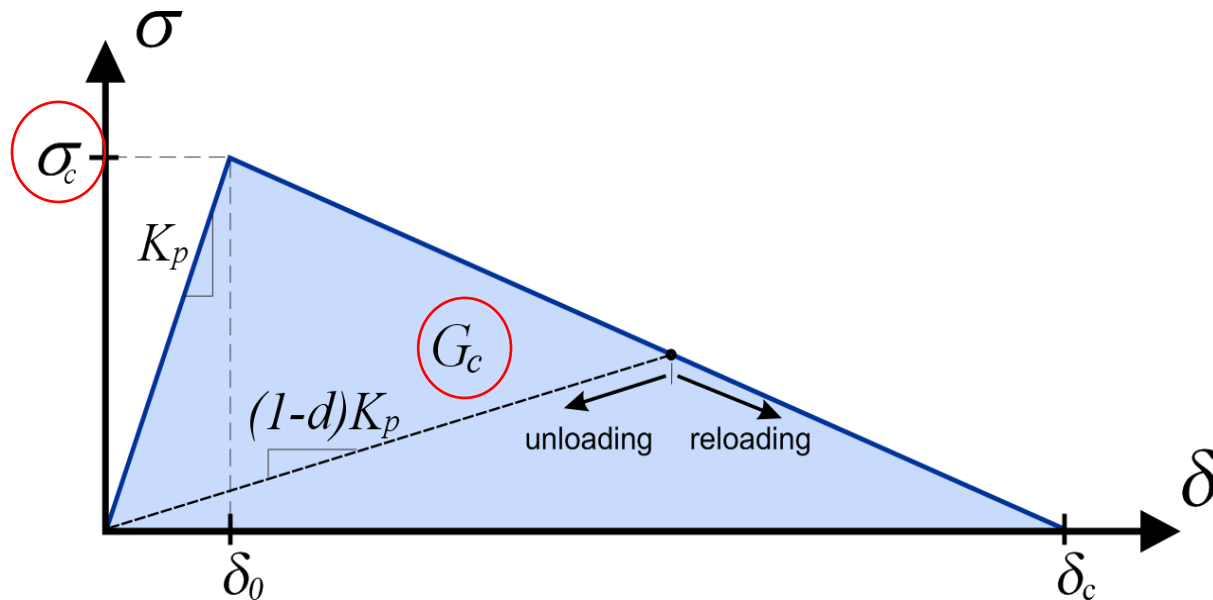
Softening is the bridge between strength scaling theories



Cohesive Laws: Two Criteria in One Softening Law

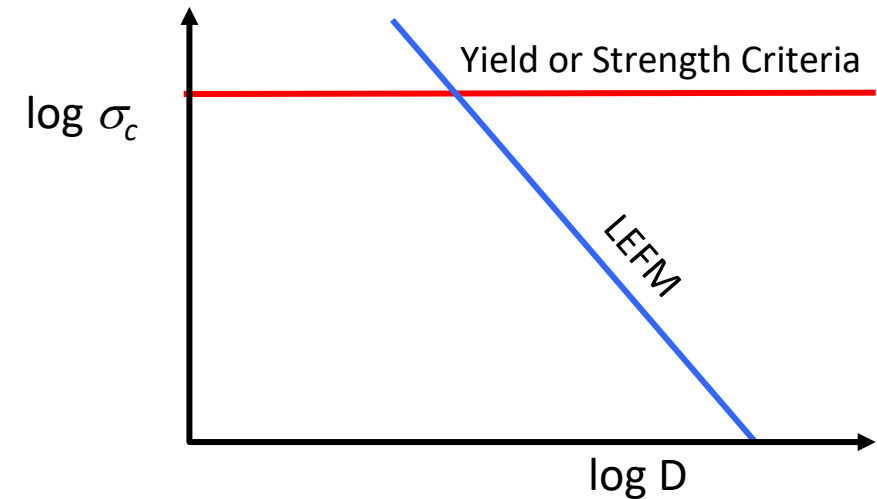


Bilinear Traction-Displacement Law



Two material properties:

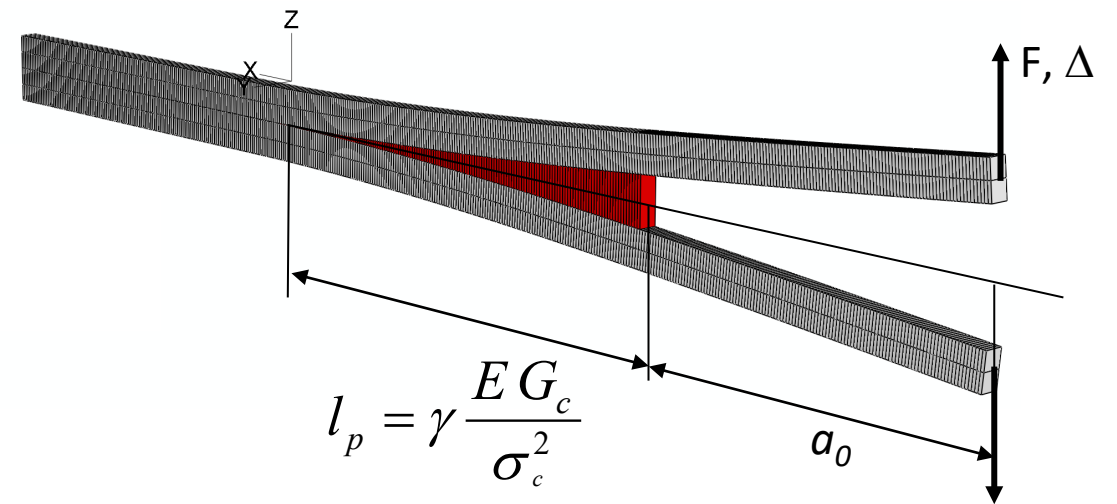
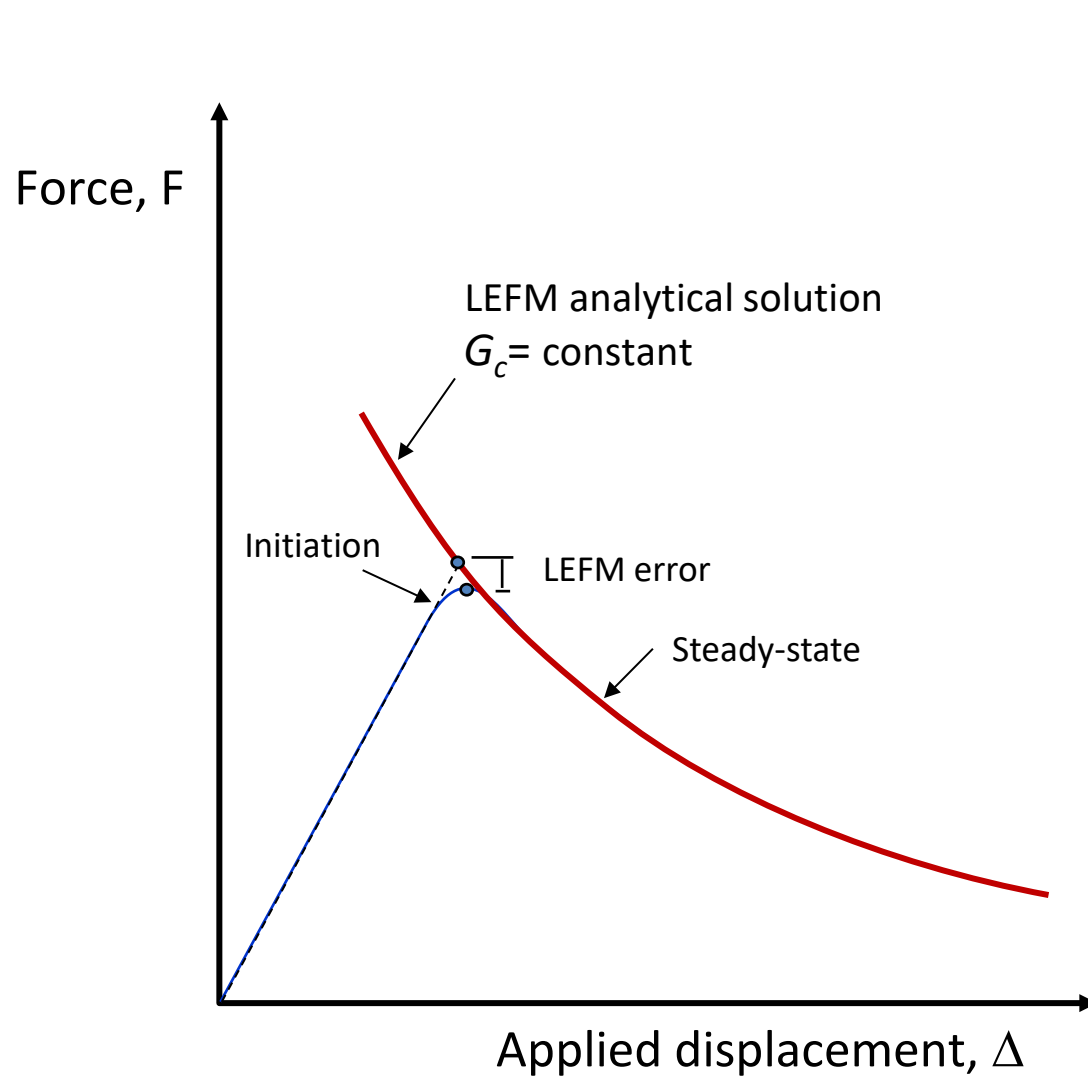
- G_c Fracture toughness
- σ_c Strength



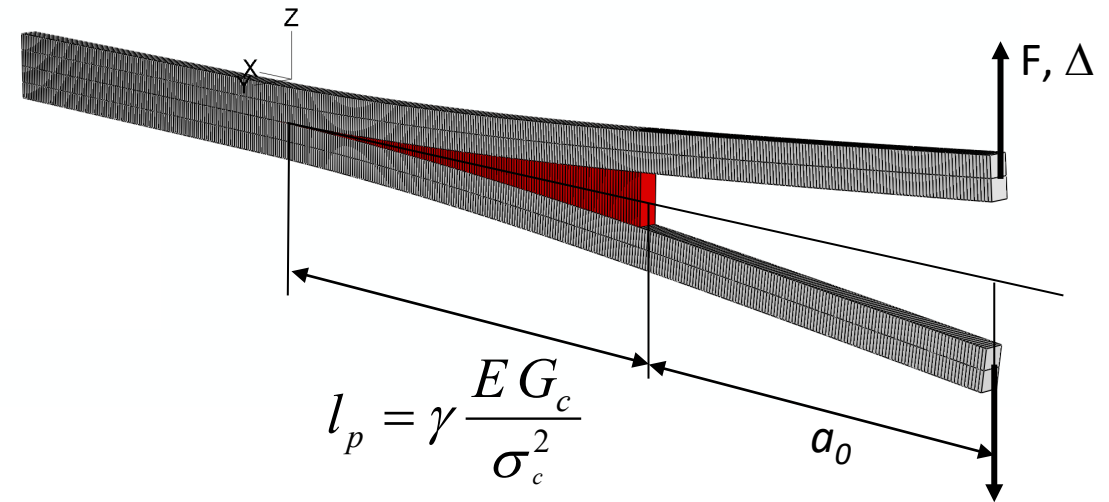
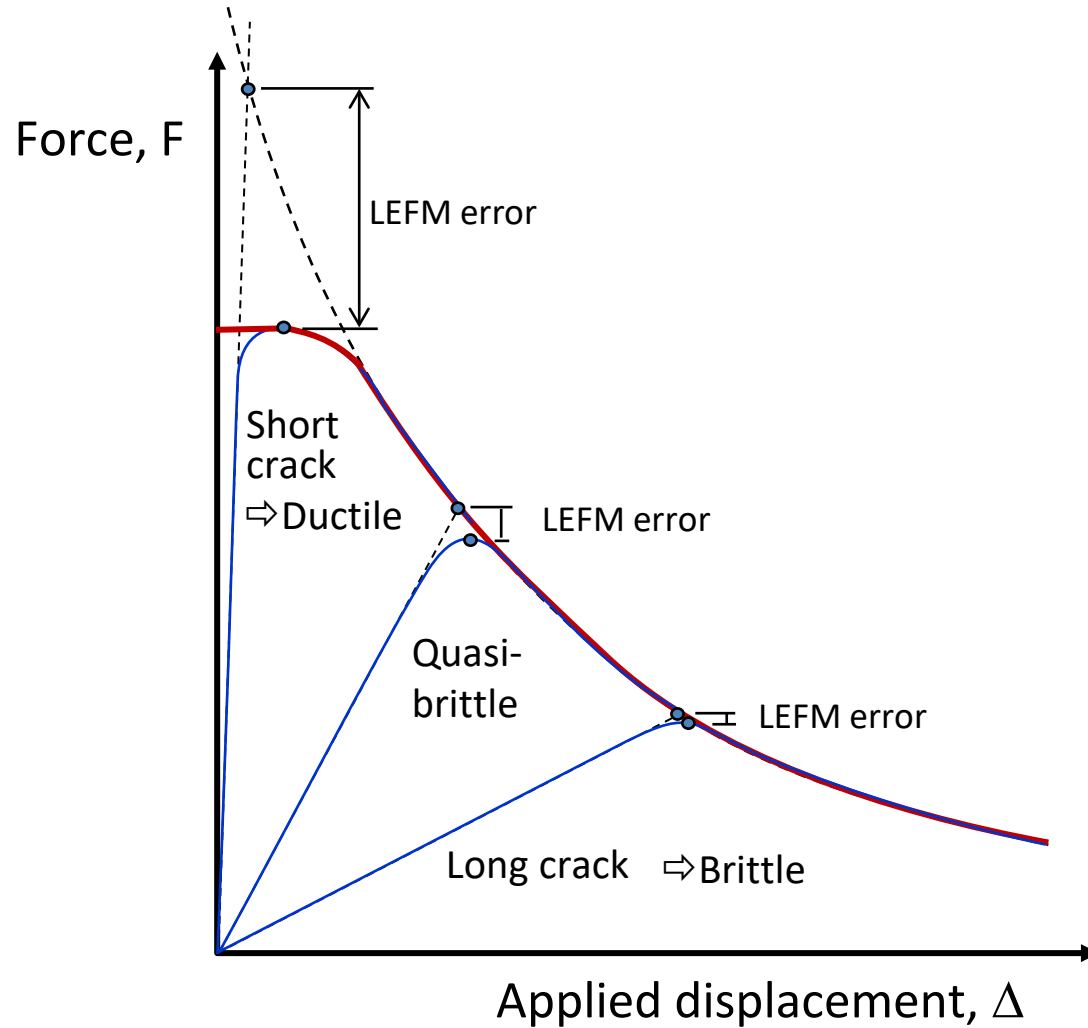
Characteristic Length:

$$l_c = \gamma \frac{E G_c}{\sigma_c^2}$$

Crack Length and Process Zone



Crack Length and Process Zone



Brittle:

$$a_0 > 100 l_p$$

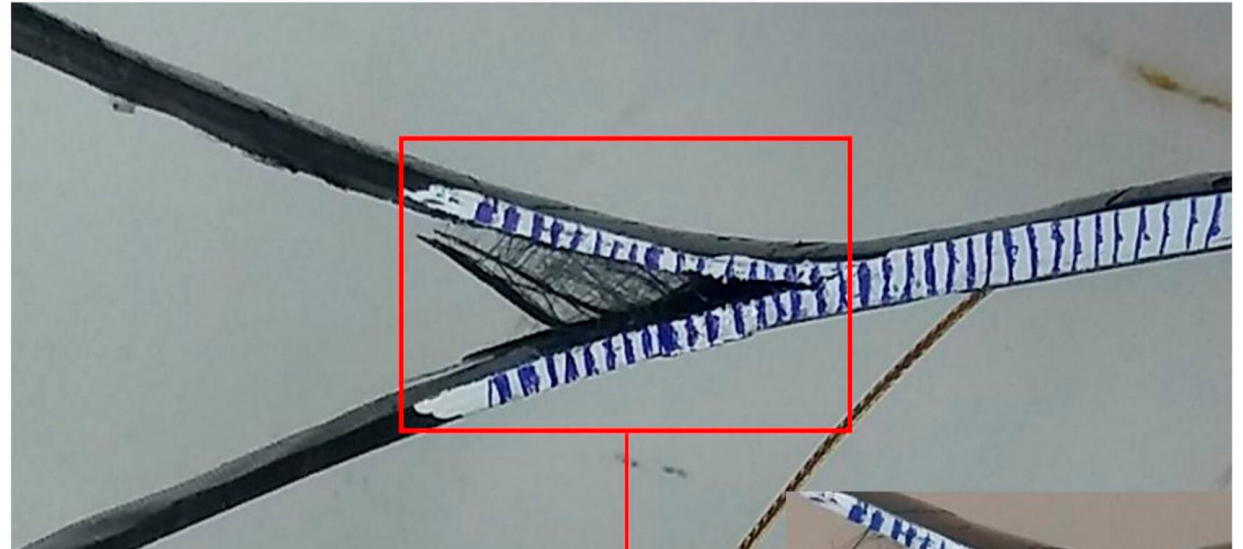
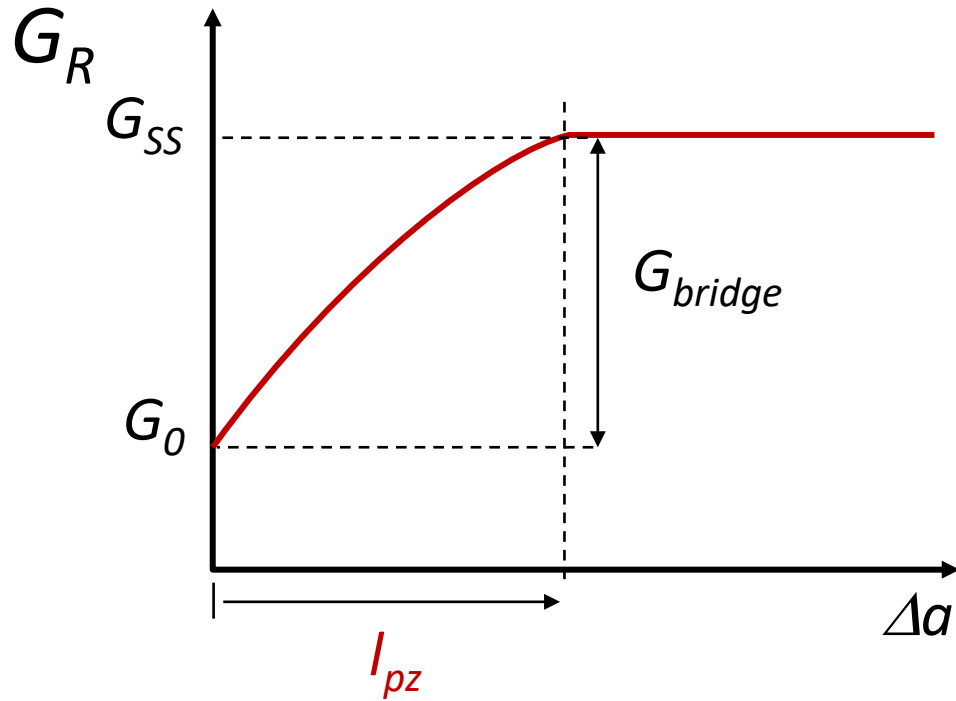
Quasi-brittle:

$$100 l_p \geq a_0 \geq 5 l_p$$

Ductile:

$$5 l_p > a_0$$

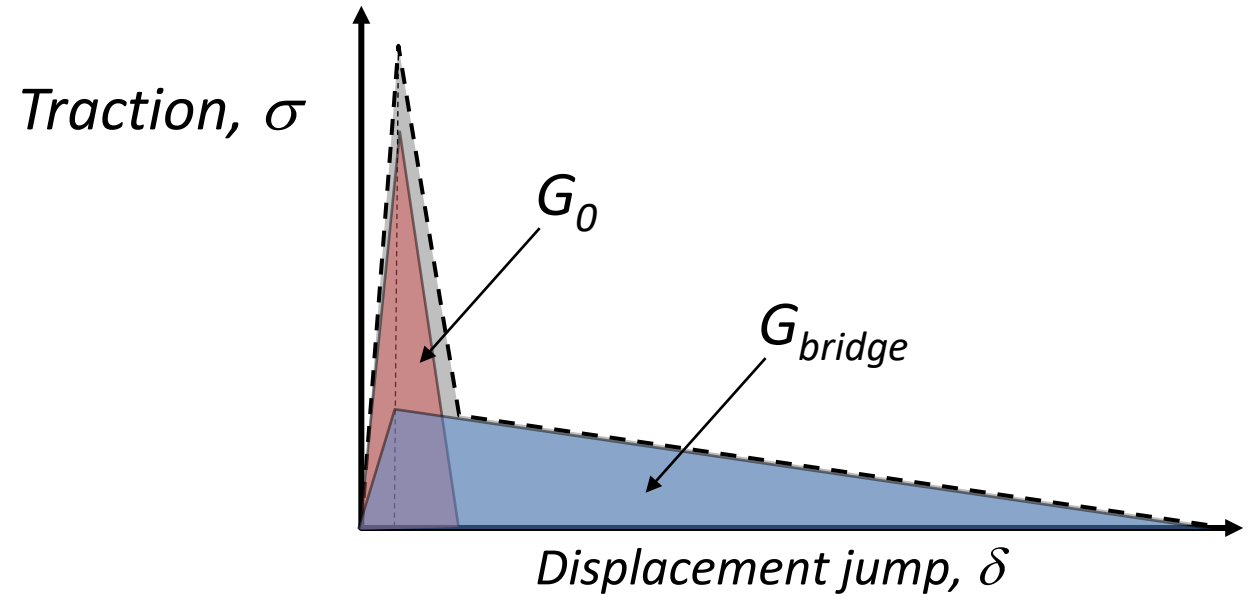
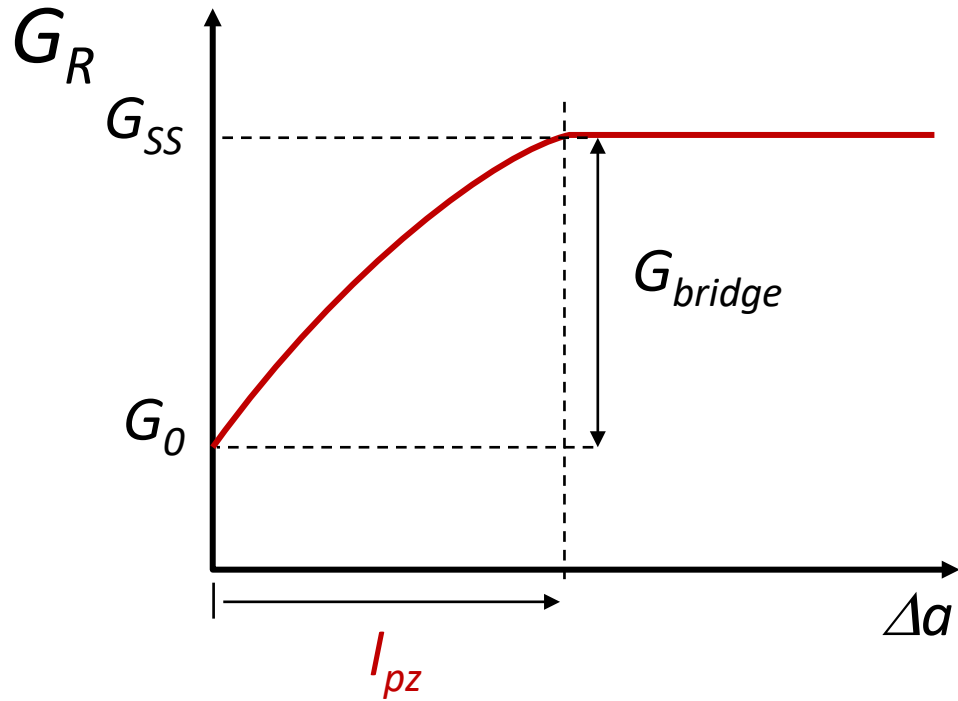
R-Curve Effects in Composites



M. Farajpour, JCM, 2023

Mechanisms such as fiber bridging can induce a gradual increase in the critical energy release rate, G_R . (R-curve effect)

Cohesive Model of R-Curve Effects



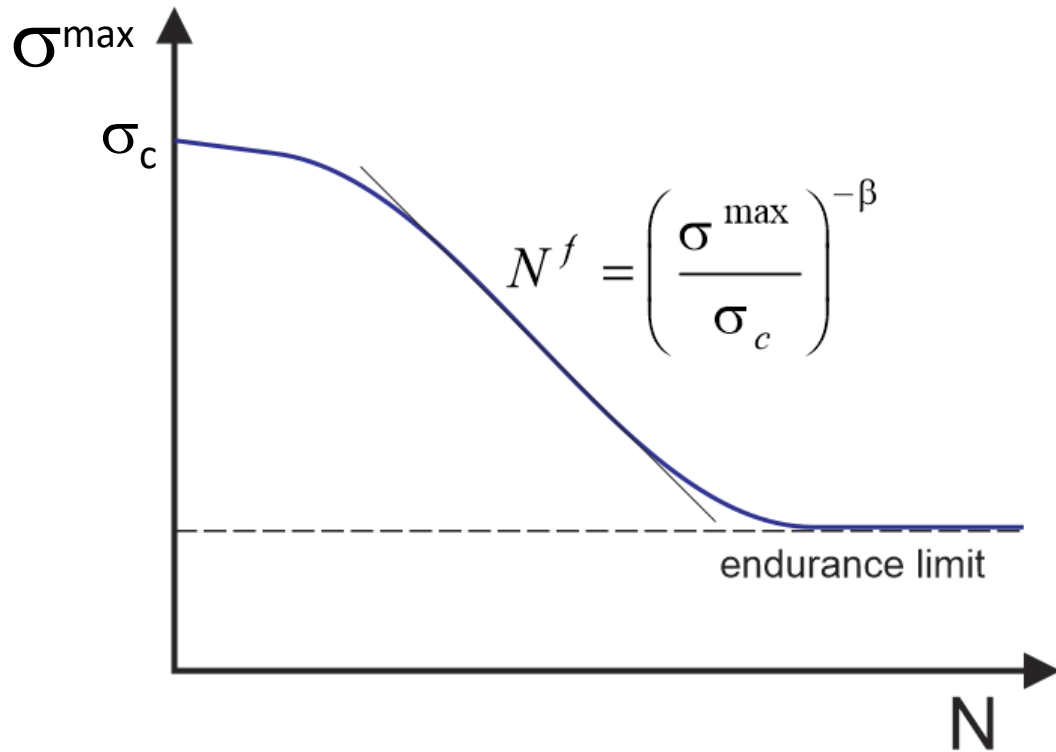
- The shape of the traction-separation (TS) induces different R-curves.
- TS with longer “tails” result in longer l_{pz} .

OK, material softening bridges the gap between strength and fracture theories...

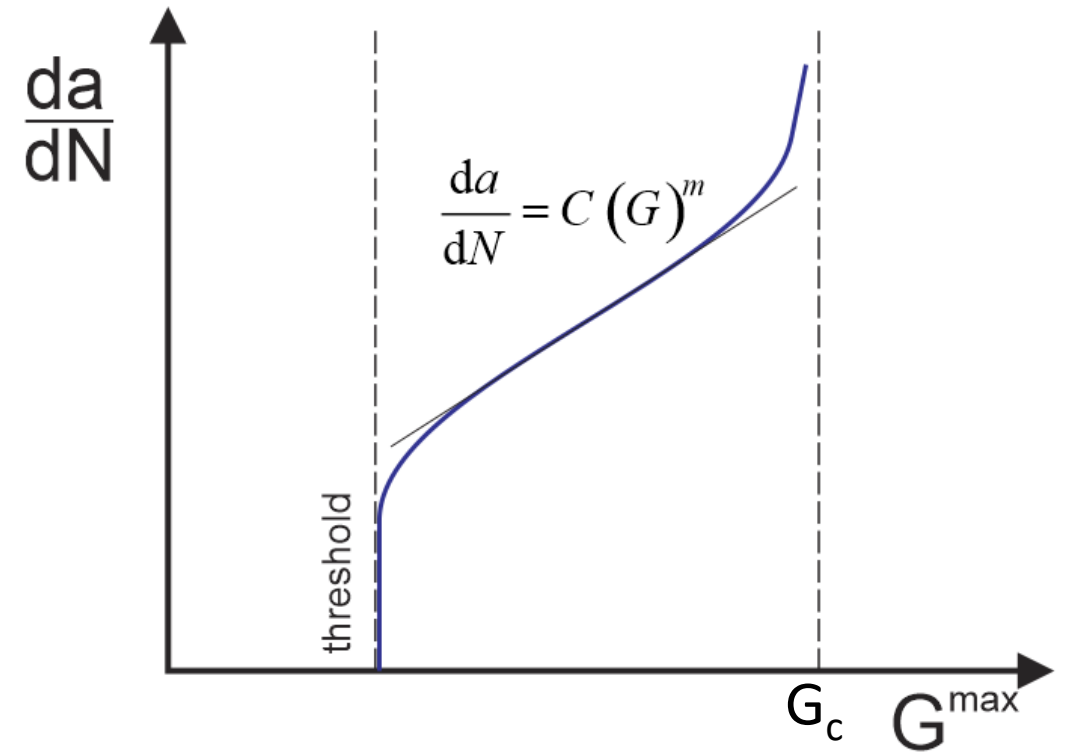
But what about fatigue?

Fatigue: Strength or Toughness?

Strength: Wöhler (S-N Curve)



Fracture: Paris Law

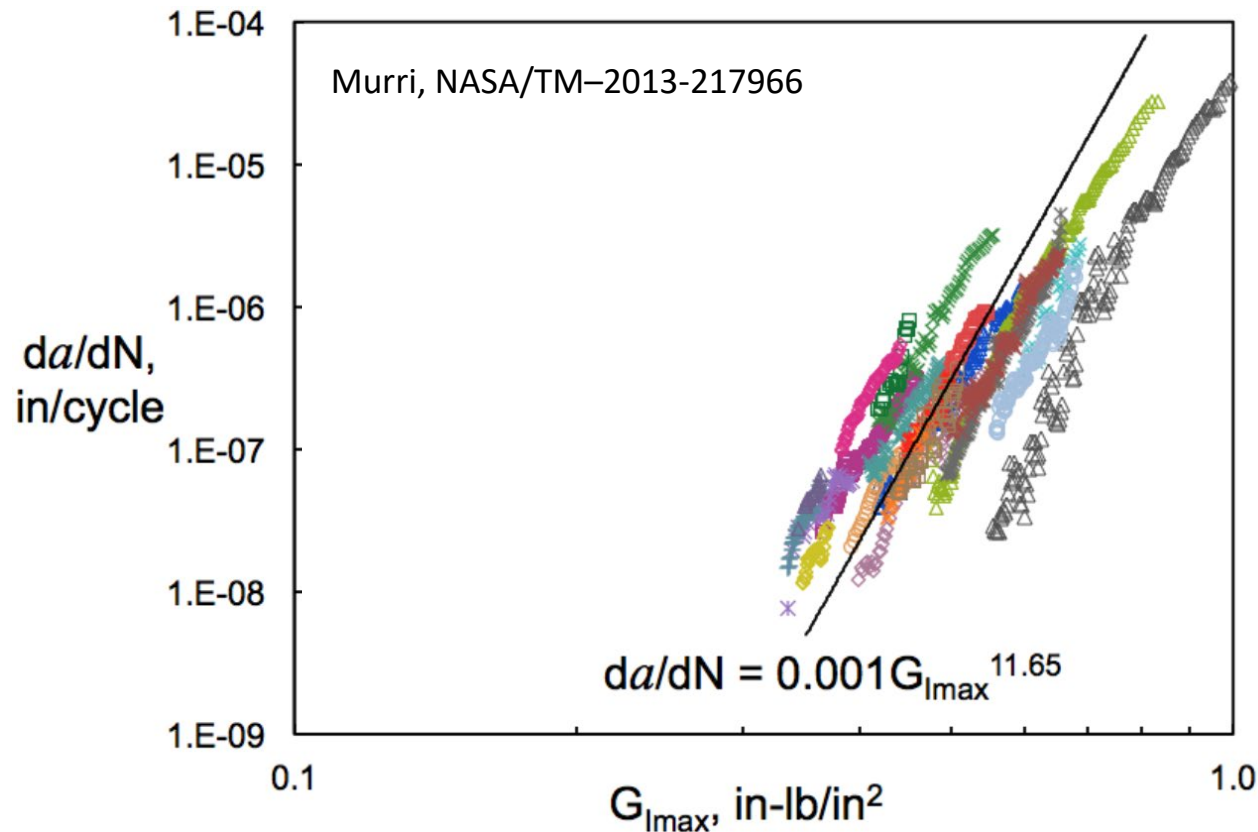


Propagation:

➡ Most fatigue cohesive constitutive models are based on Paris law

Drawbacks of Models Based on the Paris Law

Paris Law:
$$\frac{da}{dN} = C \left(G_{\max} \right)^m$$

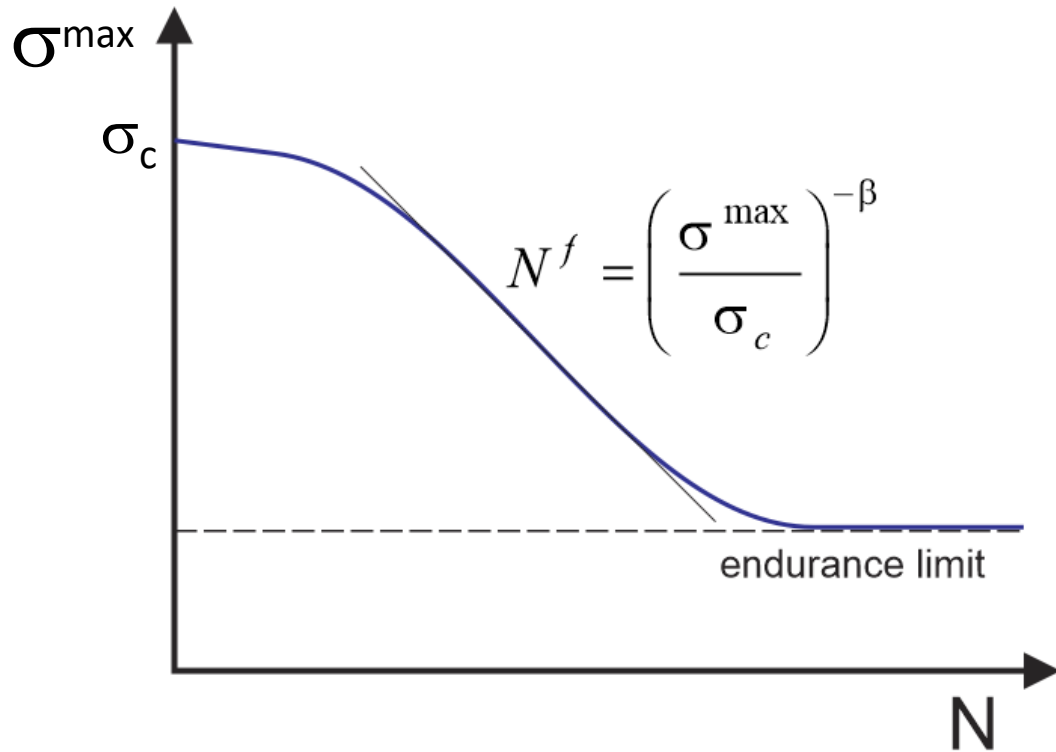


Model Limitations and Drawbacks:

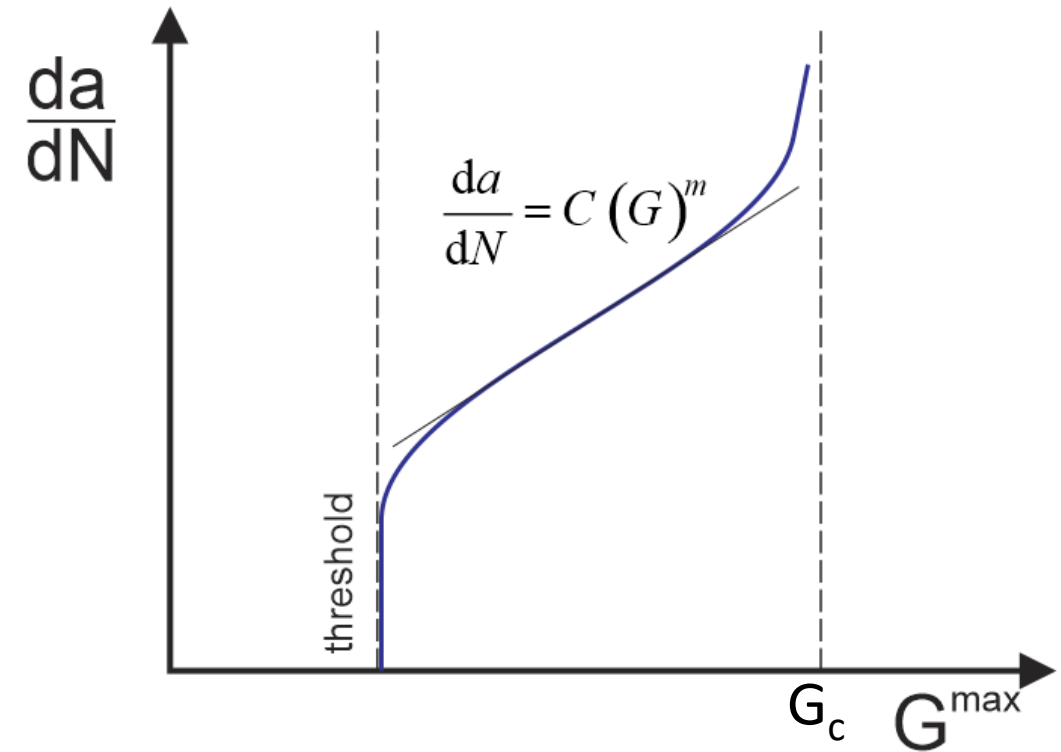
- Paris data (LEFM) does not apply to crack initiation.
- Characterization tests are expensive.
- Tests must be conducted at different stress ratios R and mode mixities B .
- R-curves induce multiple Paris laws.
- Implementation of Paris law into a cohesive law is difficult.

Fatigue: Strength or Toughness?

Strength: Wöhler (S-N Curve)



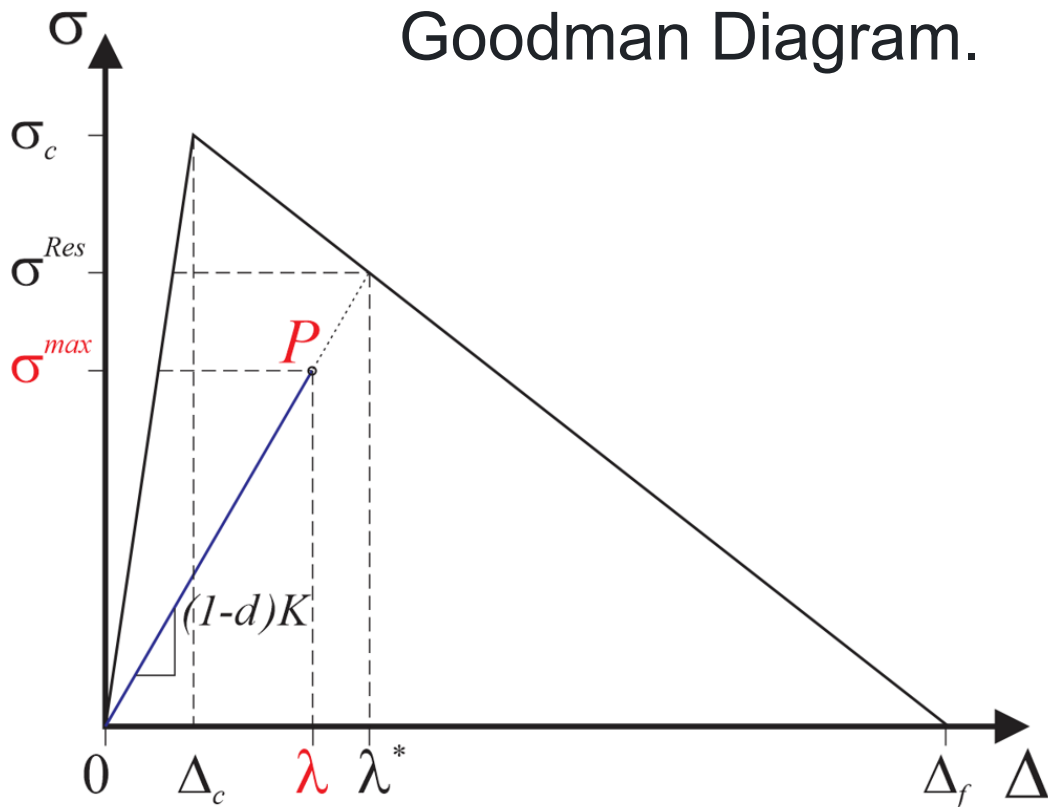
Fracture: Paris Law



Can we develop a cohesive model based on S-N that can also predict crack propagation?

CF22 Cohesive Fatigue Model

- CF22 is a reduced-input cohesive fatigue model that can predict the initiation and propagation of fatigue cracks.
- Relies on intrinsic relationships between S-N and da/dN .
- Effects of stress ratio and mode mixity are predicted using the Goodman Diagram.



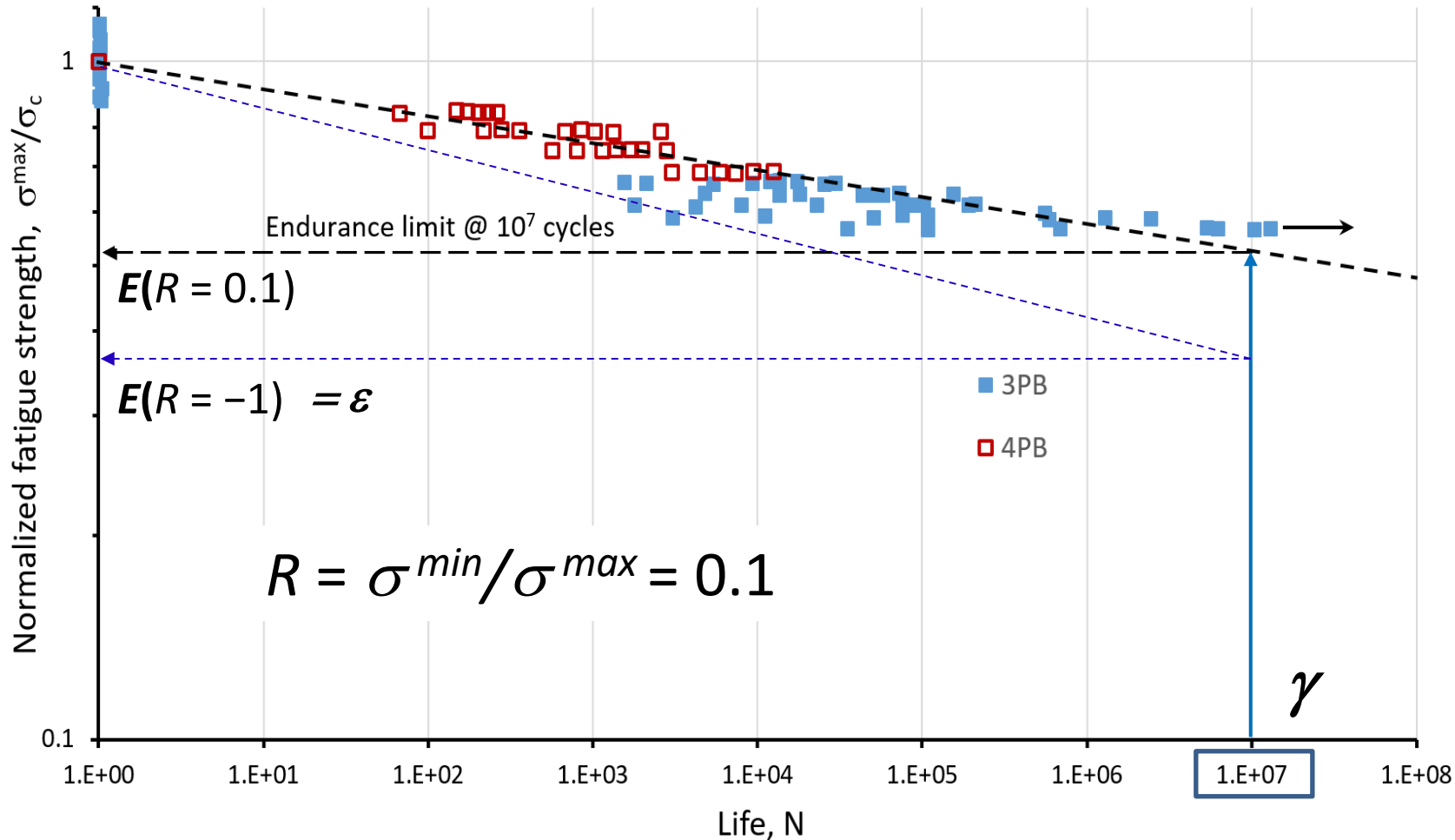
$$\frac{dD}{dN} = \frac{1}{\gamma} \frac{(1-D)^{-q}}{E^\beta (\beta + q + 1)} \left(\frac{\lambda}{\lambda^*} \right)^\beta$$

$$\text{Endurance: } E = \frac{2\varepsilon}{\varepsilon + 1 + (\varepsilon - 1)R}$$

$$\text{S-N exponent: } \beta = \frac{-\log \gamma}{\log E}$$

S-N Diagram for Delamination

- A single line fit the S-N curve from $N = 1$ to 10^7

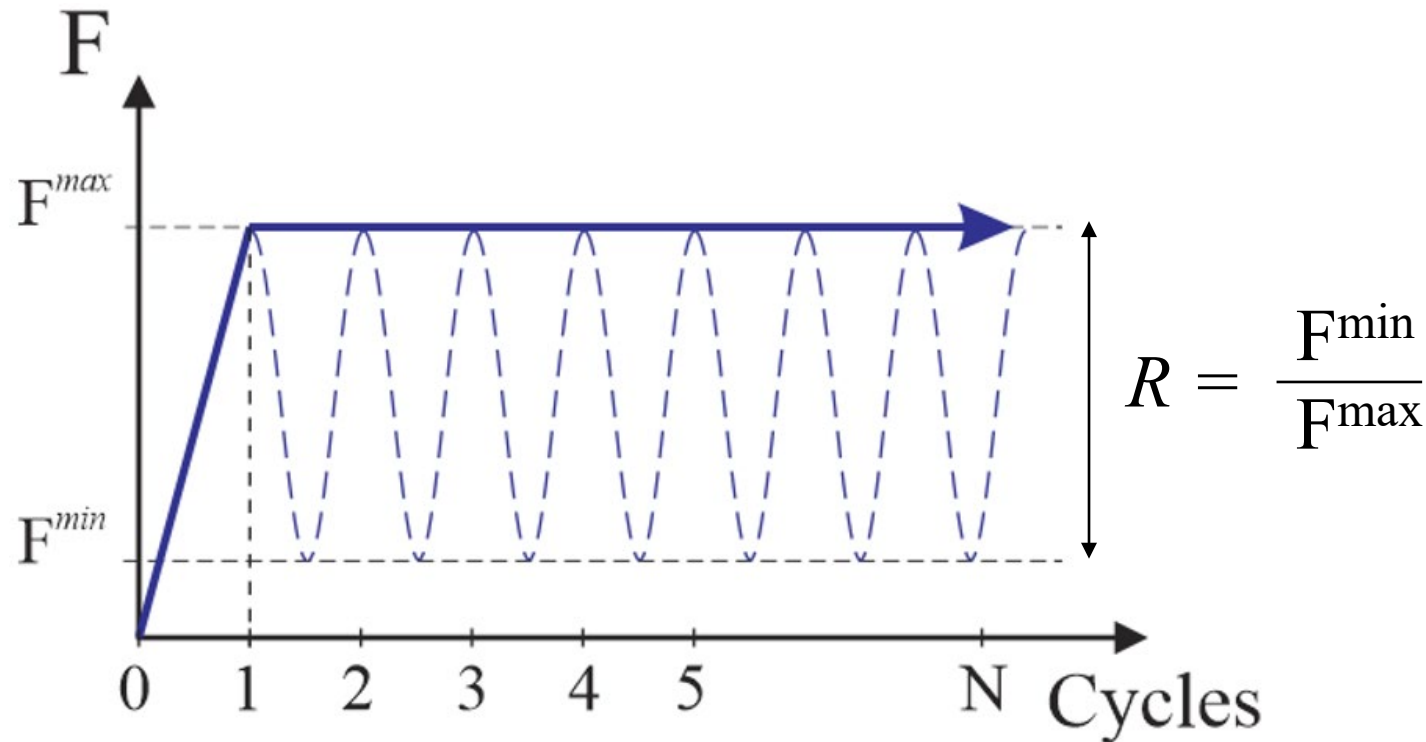
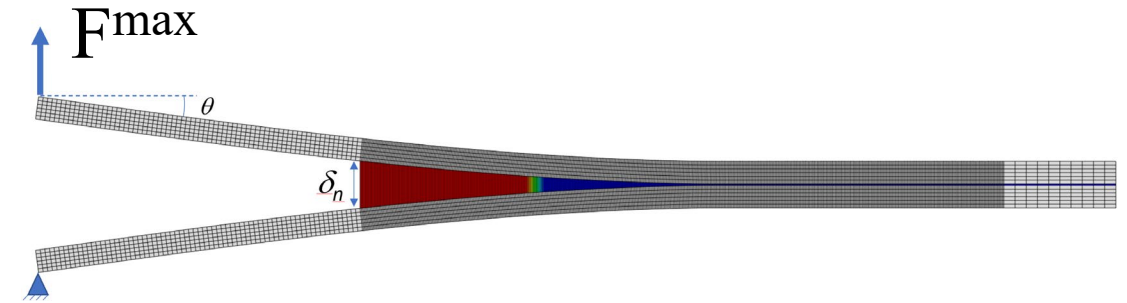


The S-N curve is anchored at point (γ, E) .

$E(R)$ can be calculated using Goodman Diagram.

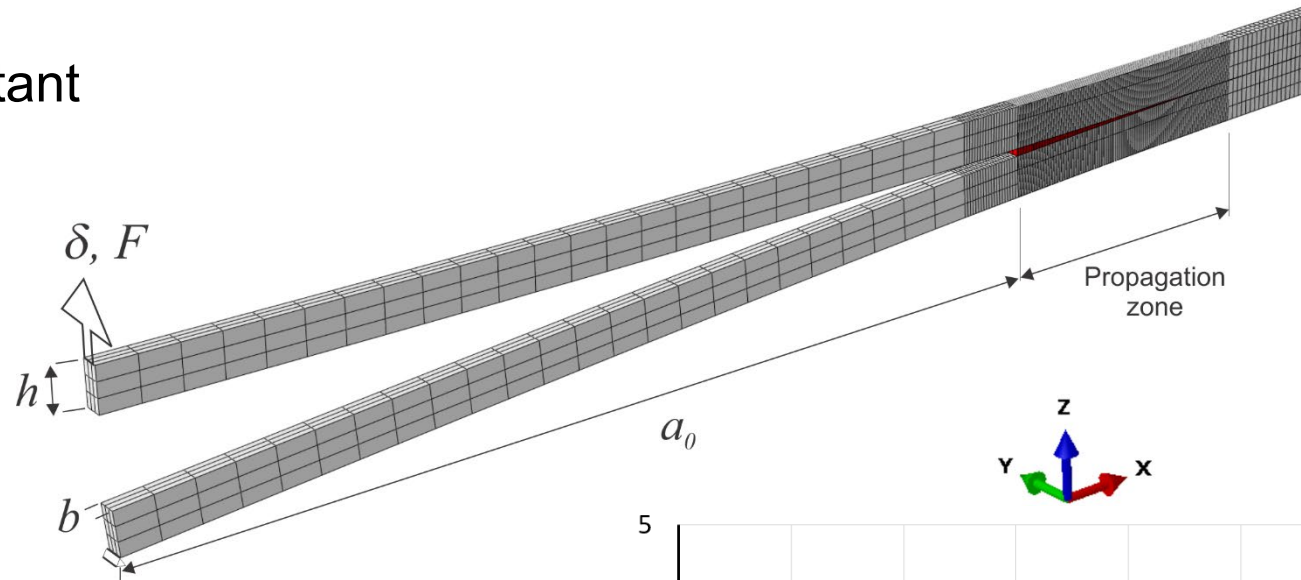
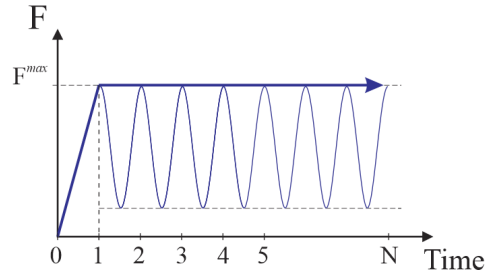
Fatigue Analysis - Simplified Cyclic Loading (SCL)

- $F^{\max}$ is held constant
- Constitutive model is informed of cyclic loading through value of R

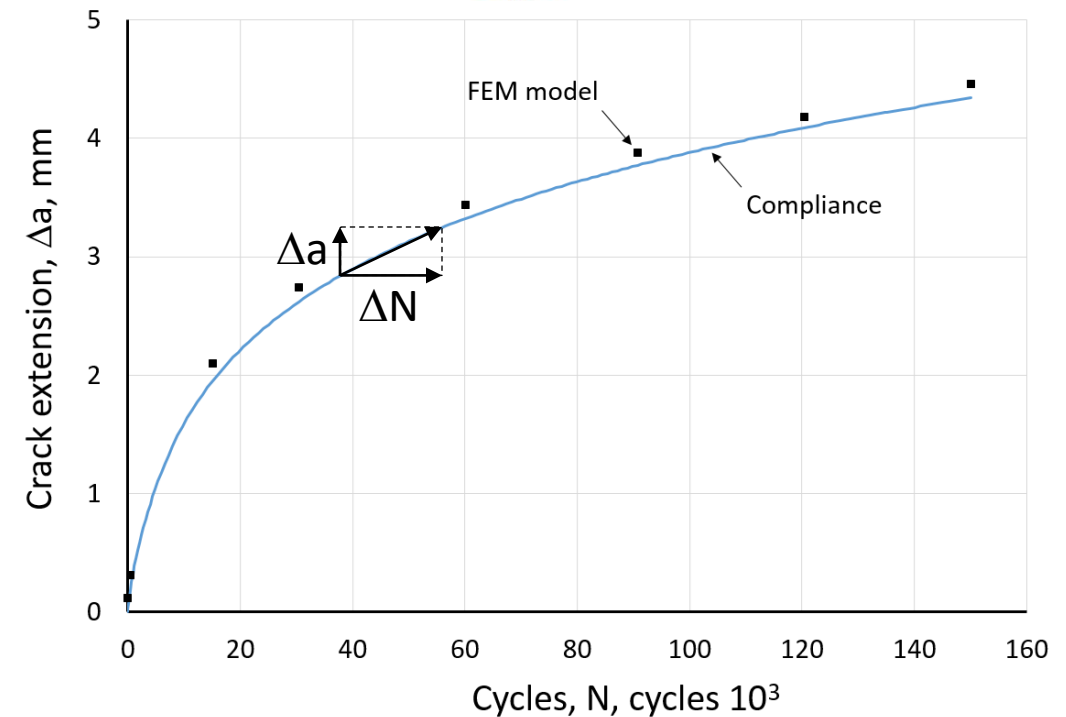
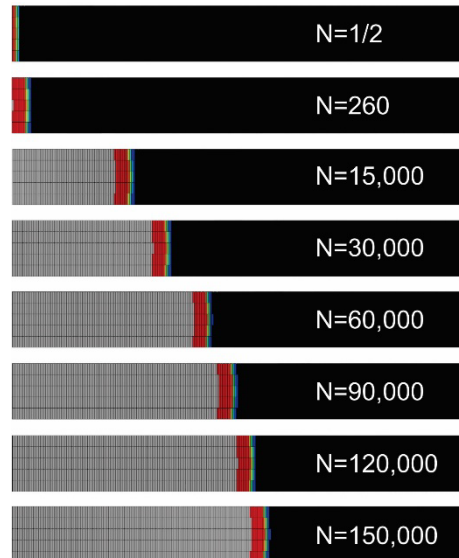


Analysis of Double Cantilever Beam Specimen (DCB)

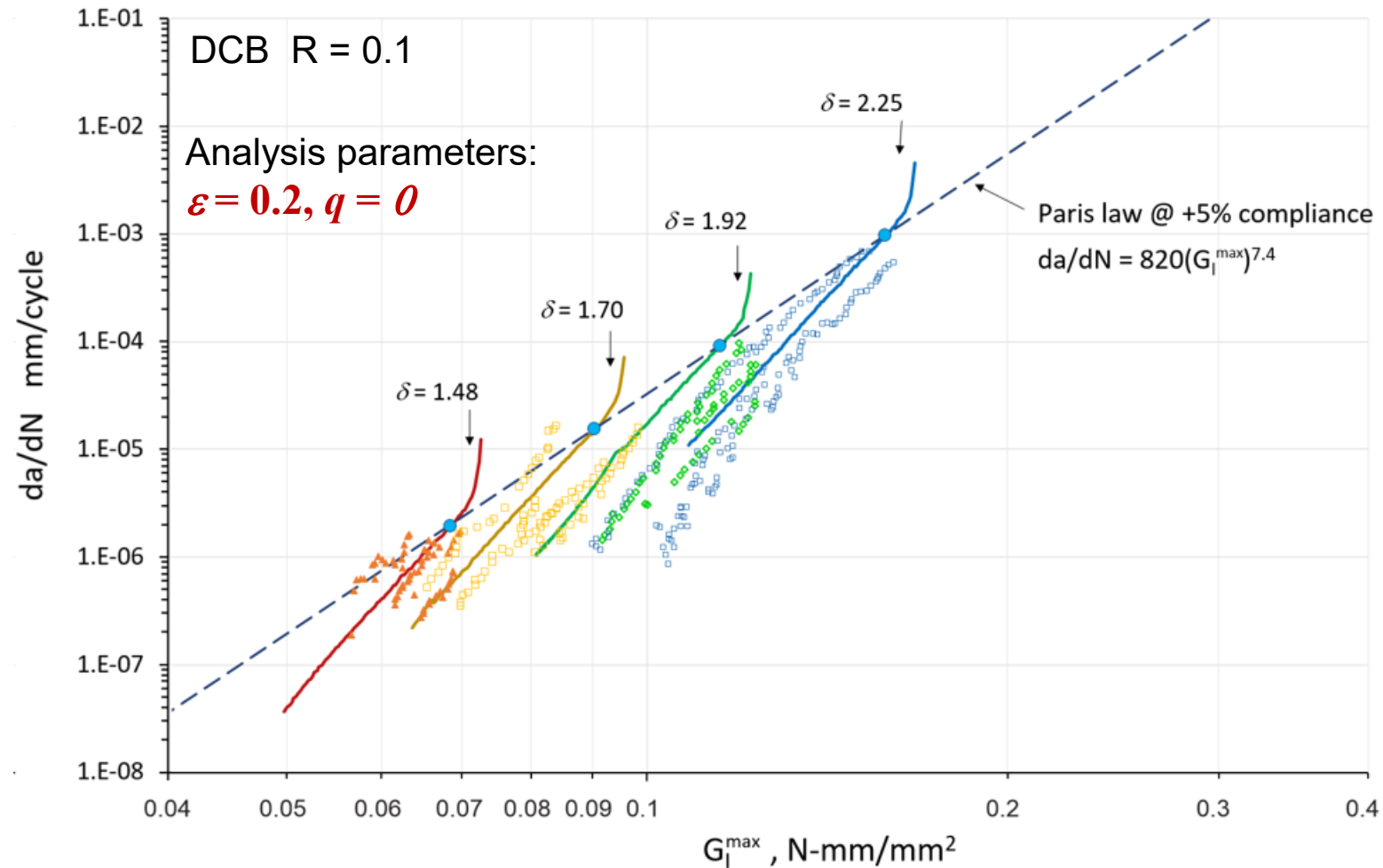
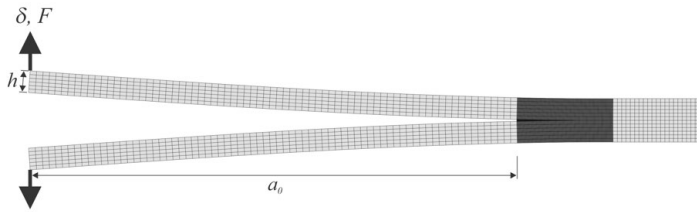
Applied load remains constant



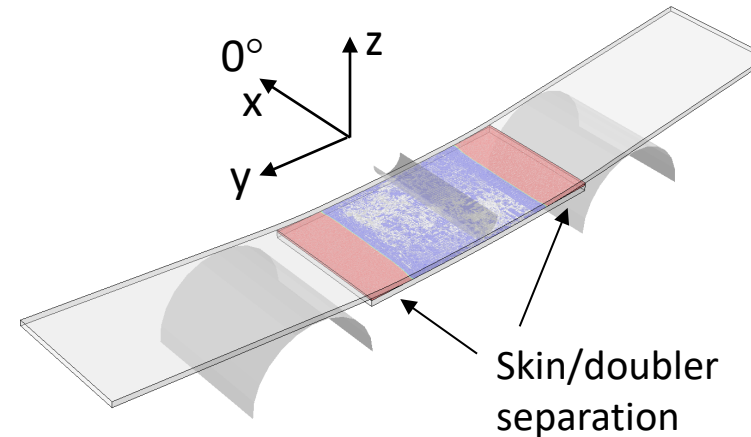
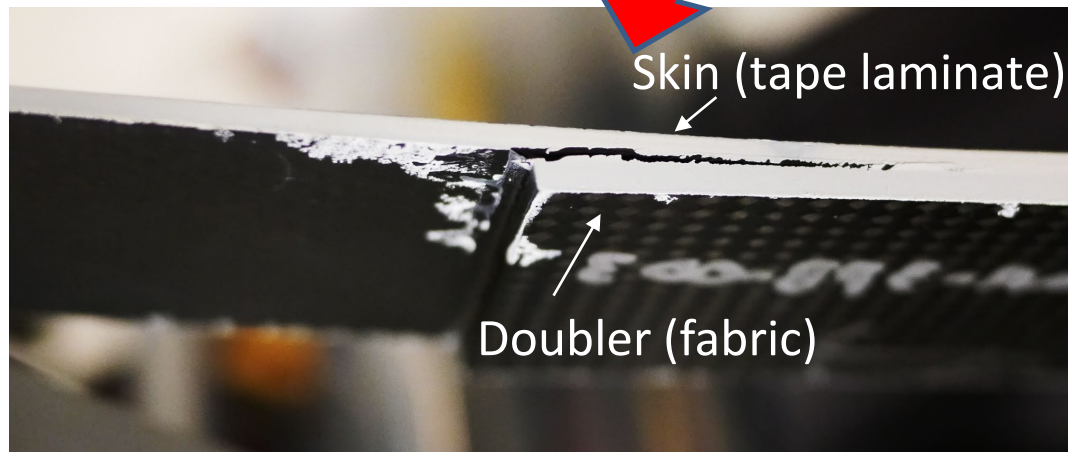
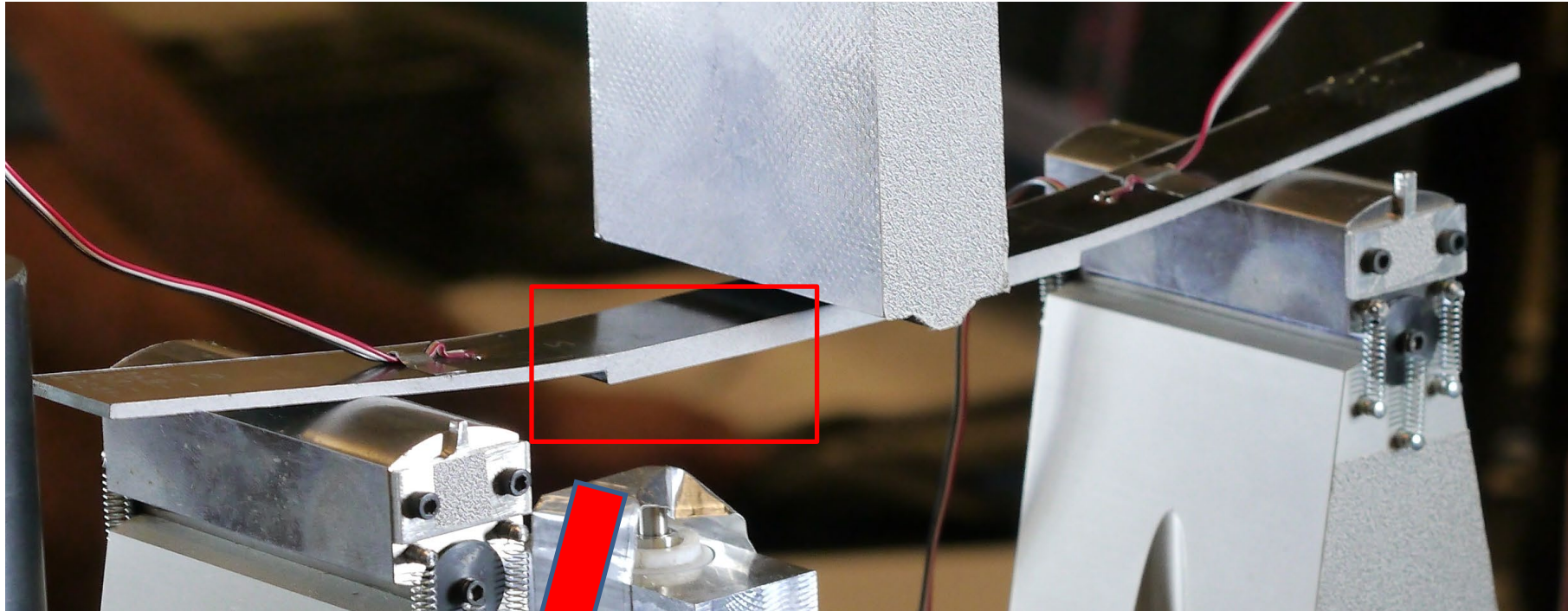
Detail of propagation zone



Fatigue Analysis of DCB Test with R-Curve Effect

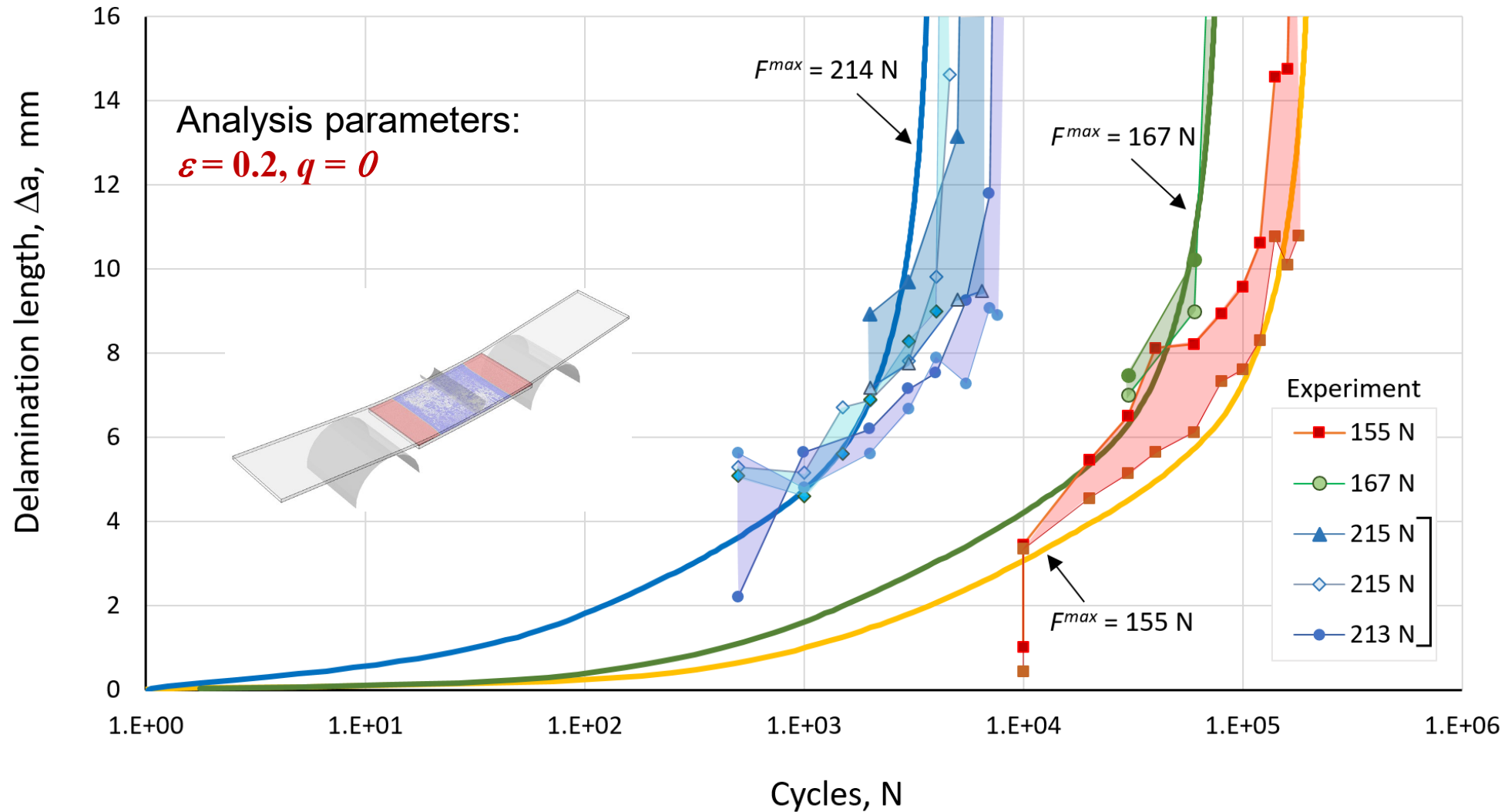


Three Point Bend (3PB) Doubler Specimen



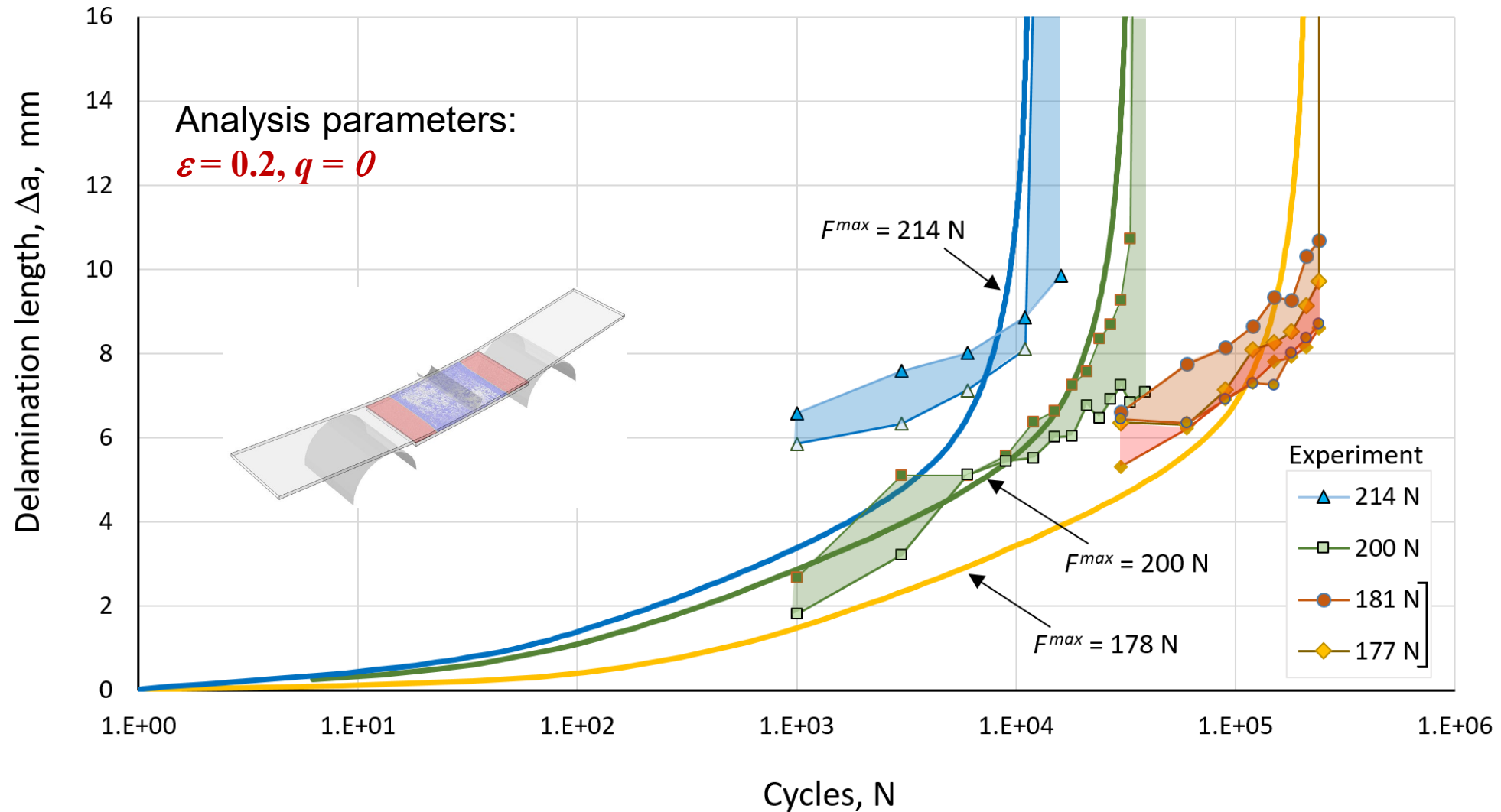
Delamination length in 3PB Doubler

3PB Doubler $R = 0.1$



Delamination length in 3PB Doubler

3PB Doubler $R = 0.4$



Softening the Gap between Wöhler and Paris

- Material softening blends strength and fracture theories.
- A common cohesive thread ties fatigue threshold, S-N, and the Paris rate.
- Transient rates of propagation can only be predicted with softening models.