



TFAWS INTERDISCIPLINARY SESSION



MOON BASE

Thermal & Fluids Analysis Workshop 2026
NASA Marshall Space Flight Center
Huntsville, AL
Aug 31 - Sept 4, 2026



MOON BASE TRANSPORTATION – DELIVERIES TO THE LUNAR SURFACE

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Deep Space Logistics: FLY | SUPPLY | EXPLORE

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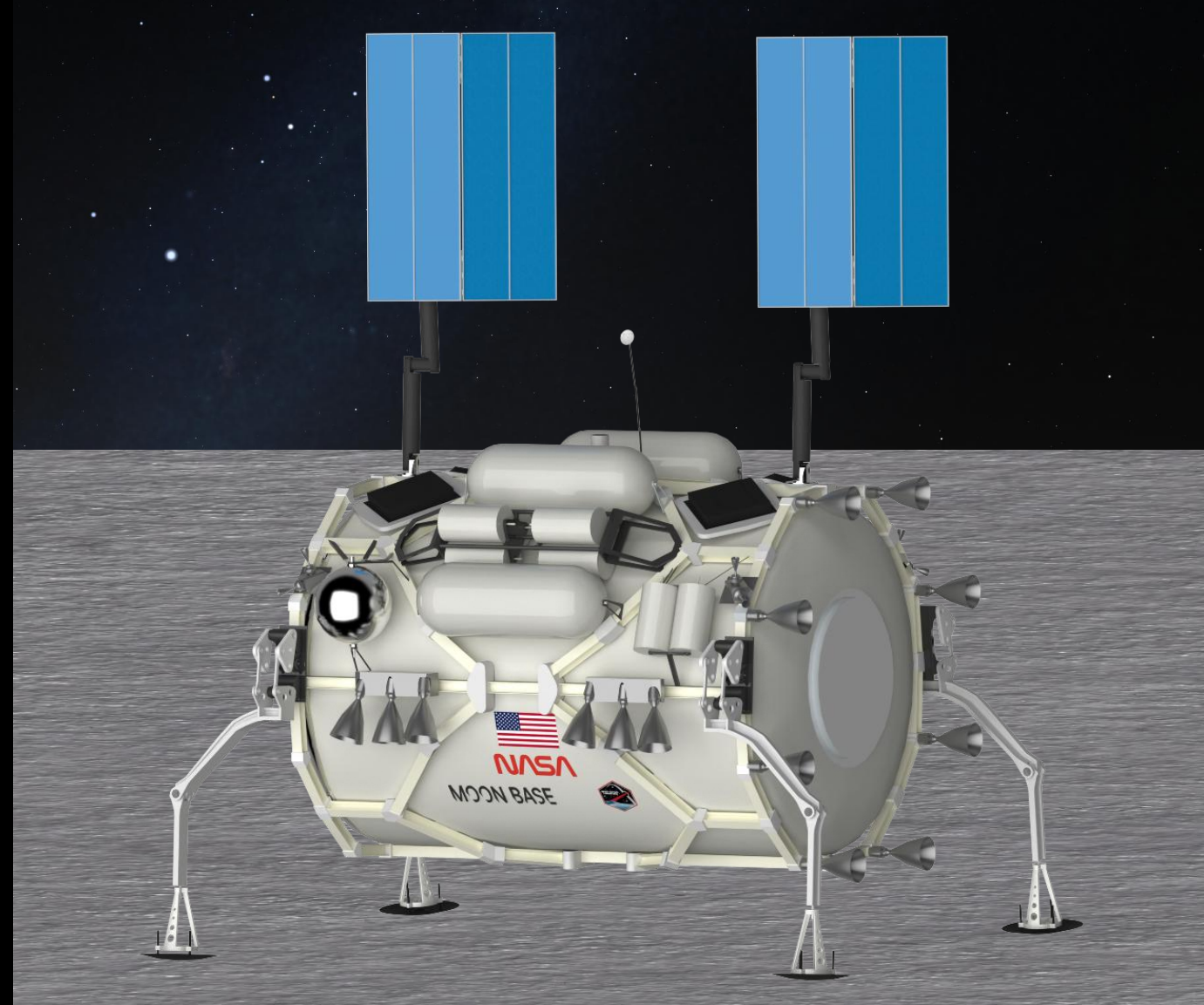


PRESENTATION OVERVIEW



MOON BASE

- Motivation & Objective
- Mission Overview
- Vehicle Architecture
- Key Elements of Mission Ops
- Conclusions





MOTIVATION



MOON BASE

SYSTEMS



TRANSPORTATION



AUTONOMY & ROBOTICS



LOGISTICS



COMMUNICATIONS
& POSITIONING,
NAVIGATION, AND
TIMING



HABITATION



POWER



MOBILITY



PHASE
01



PHASE
02



PHASE
03

PROGRESSION



LAUNCHES

- 25
- 27
- 29



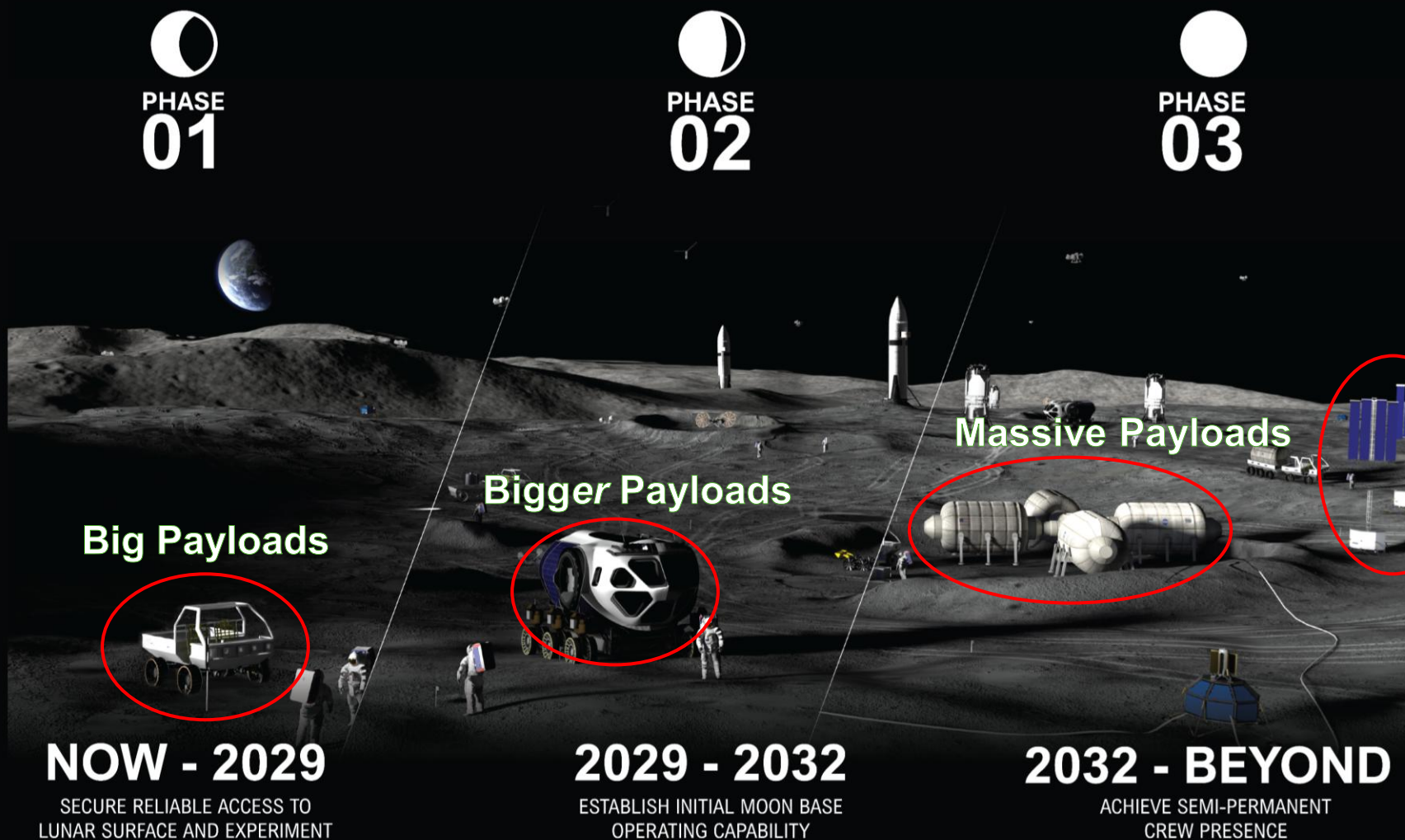
LANDINGS

- 21
- 24
- 28



CARGO TO SURFACE

- ~4,000 KG
- ~60,000 KG
- ~150,000 KG



BUILDING AN ENDURING LUNAR PRESENCE

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**Develop an end-to-end mission concept to transport large payloads
to the Lunar South Pole in support of Moon Base.**

**The transfer vehicle combines in space and landing capability with
jettisonable prop storage stages.**





MOON BASE

MISSION OVERVIEW

SYSTEM DESIGN IS AN
EXERCISE LEFT TO THE READER

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MISSION PHASES



MOON BASE

1. Launch and Launch Vehicle Separation

- Integrated vehicle stack of Lunar Lander (LL) + Payload in LV payload fairing

2. Trans Lunar Injection (TLI)

- Thrust to get out of Earth's gravity well

3. Mid Course Corrections (MCC)

- Heading updates and pointing maneuvers

4. Lunar Orbit Insertion (LOI)

- Entering the Moon's gravity well

5. LOI Corrections

6. Lunar Descent and Touchdown (LDT)

- Pre-Landing Navigation
 - High altitude tracking
 - Low altitude tracking
- Vertical Descent
 - Final site selection
 - *Hands off the controls & see what happens*

Launch Config Dependent dV (does LV supply?)

~Fixed dV (Lander must achieve)

Risk Tolerance Dependent dV

Earth (Launch Point)

Van Allen Belts

Moon

Figure Almost to Scale



GROUND RULES AND ASSUMPTIONS



Assumptions

- Launch/lunar phasing is optimal for mission
- Comms & ground tracking is sufficient/accommodating
- Space qualified (rad hard) hardware readily procurable
- Launch Vehicle (LV) with capability exists
- Launch loads and stack configurations are within dynamic envelope of fairing
 - Adapters are sufficiently stiff
- Landing site conditions are conducive to landing
 - More detail for vehicle needed to select max slope & surface feature sizes
 - No other assets in landing site (so far)

Ground Rules

- Slow roll in transit for thermal regulation and arrays point
- Sufficient lighting for TerRain based Nav (TRN) to work
- No insurmountable thruster limitations for landing and in space trajectory control
 - Selecting based on accelerations & life
- Sufficient electrical power to have no concern of eclipse/shadow in space

Make This Big!

Make This Feasible

$$m = m_{\text{payload}} + m_{\text{vehicle}} + \overbrace{m_{\text{Propellant}} + m_{\text{Pressurant}}}^{\text{Make This Feasible}}$$

???



"LANDER" DESIGN REQUIREMENTS

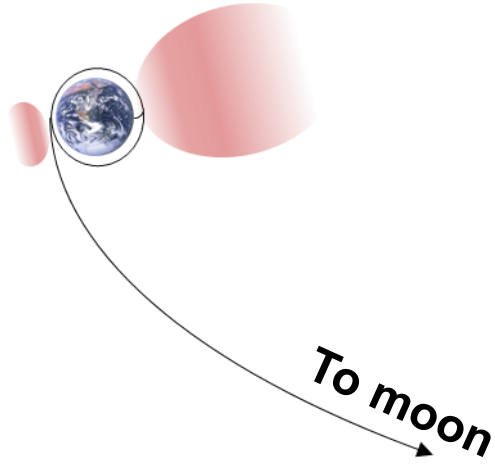


1. **Navigate in space & touchdown at desired location**
2. **Survive radiation/thermal environment(s)**
3. **Any jettisoned elements need separation analysis**
4. **Pyrotechnics (cutters/valves/etc.) need specific analysis**
5. **Adequate acceleration for Hohmann transfers/descent/touchdown**
6. **Not impose excessive loads into the payload (launch/landing/etc.)**
7. **Comm/instrumentation for the payload**

Desirable: avoid (Rendezvous, Proximity Operations, and Docking) RPOD & prop transfer

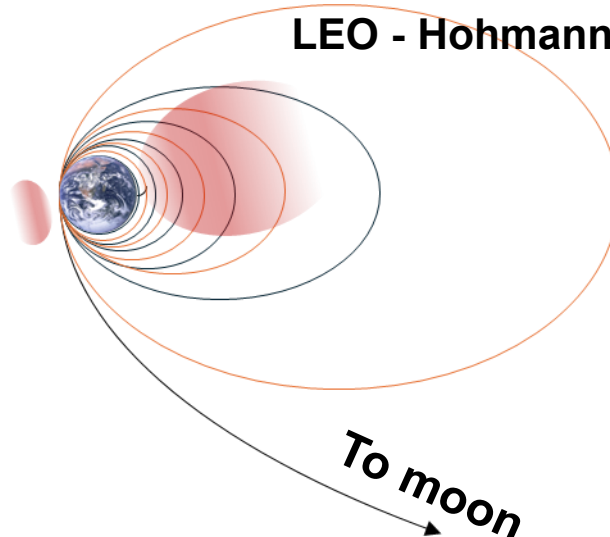
TRANSPORTATION FROM THE EARTH

Fast - Apollo



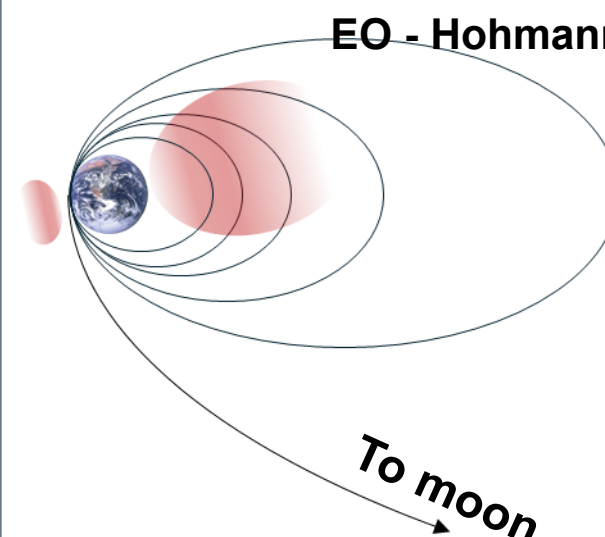
- Avoids Van Allen Belts
- ~5 day mission to the moon
- Facilitates cryo prop sys

LEO - Hohmann



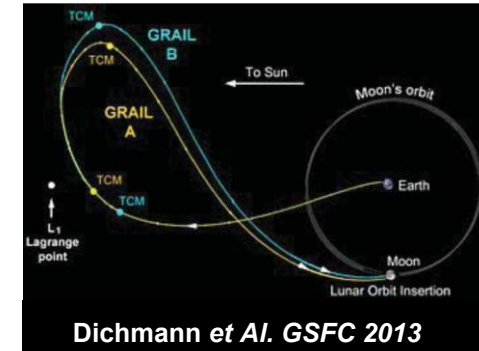
- Trade # of burns for time/thrust
- 300/600 m/s per burn for 10/5 burns
- ~10/15 days for 5/10 orbits

EO - Hohmann



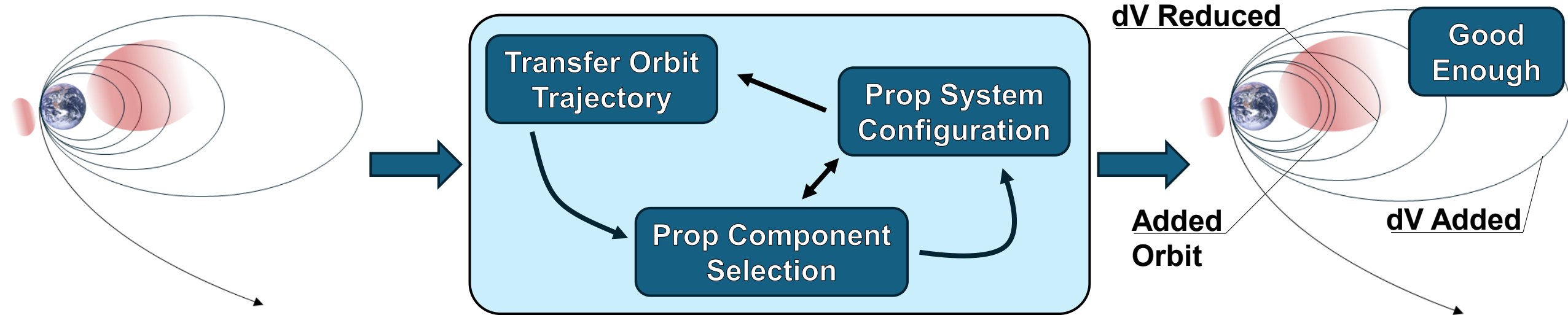
- Uses LV to provide dV, burn on first half orbit, then correction
- ~300 m/s per burn for 5 burns
- ~9 days

Ballistic Lunar Transfer



- Minimizes prop needs
- *Trade space to calculate dV, extended mission time – Good or bad*

Step	Apollo	10 Burn LEO Hohmann	5 Burn LEO Hohmann	EO Hohmann
1 – Launch to	Earth Parking Orbit	200 km Circular	200 km Circular	200 x 10,000 km Elliptical
2 – TLI	3.2 km/s	3.15 km/s	3.25 km/s	1.4 km/s
3 – MCC	0.05 km/s	0.05 km/s	0.08 km/s	0.08 km/s
4 – LOI	0.89 km/s	0.89 km/s	0.89 km/s	0.89 km/s
5 – LOI Corrections			0.05 km/s	
6 – LDT	2.45 km/s	2.25 km/s	2.25 km/s	2.25 km/s
Total dV [km/s]	6.59	6.39	6.52	4.67



- In space transit requires prop use, major dV burns & RCS use
 - For big transfers, optimize mass use
 - Primary prop tanks can be sized to be “for dV burns”
 - When the burn is complete, jettison the excess mass
 - Use pyro valves/cutters to safe systems prior
- Overall goals of
 - Making the mission more viable (success probability increase)
 - Reducing propellant consumption (cost reduction)
 - Increasing payload mass (cost reduction)

Pointing Losses

$$dV = ISP \cdot g_0 \cdot \cos(\theta) \cdot \ln\left(\frac{m_o}{m_f}\right)$$

$$dV = ISP \cdot g_0 \cdot \sum_k \cos(\theta_k) \cdot \ln\left(\frac{m_{o_k}}{m_{f_k}}\right)$$

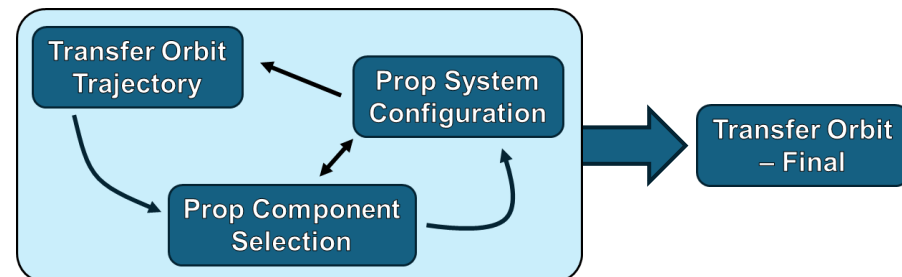
Per Stage Counting Index

BURN SCHEDULE & MISSION DESIGN

- 1.4 km/s equally across 5 burns ~ 285 m/s each
- Burn to 98.5% of tank capacity ~ 92,000 in³
- Assume 2 Prop tanks + 6 pressurant + structure per element

36 Pressurant tanks for 6 stages

- | | | |
|------------------------|----------|----------|
| • Burn 1 dV = 285 m/s, | Jettison | 285 m/s |
| • Burn 2 dV = 25 m/s, | | 308 m/s |
| • Burn 3 dV = 296 m/s, | Jettison | 604 m/s |
| • Burn 4 dV = 100 m/s, | | 704 m/s |
| • Burn 5 dV = 258 m/s, | Jettison | 962 m/s |
| • Burn 6 dV = 425 m/s, | Jettison | 1387 m/s |



$$m_{\text{payload}} + m_{\text{vehicle}} = 11,000 \text{ kg}$$

$$m_{\text{payload}} + m_{\text{vehicle}} = 10,700 \text{ kg}$$

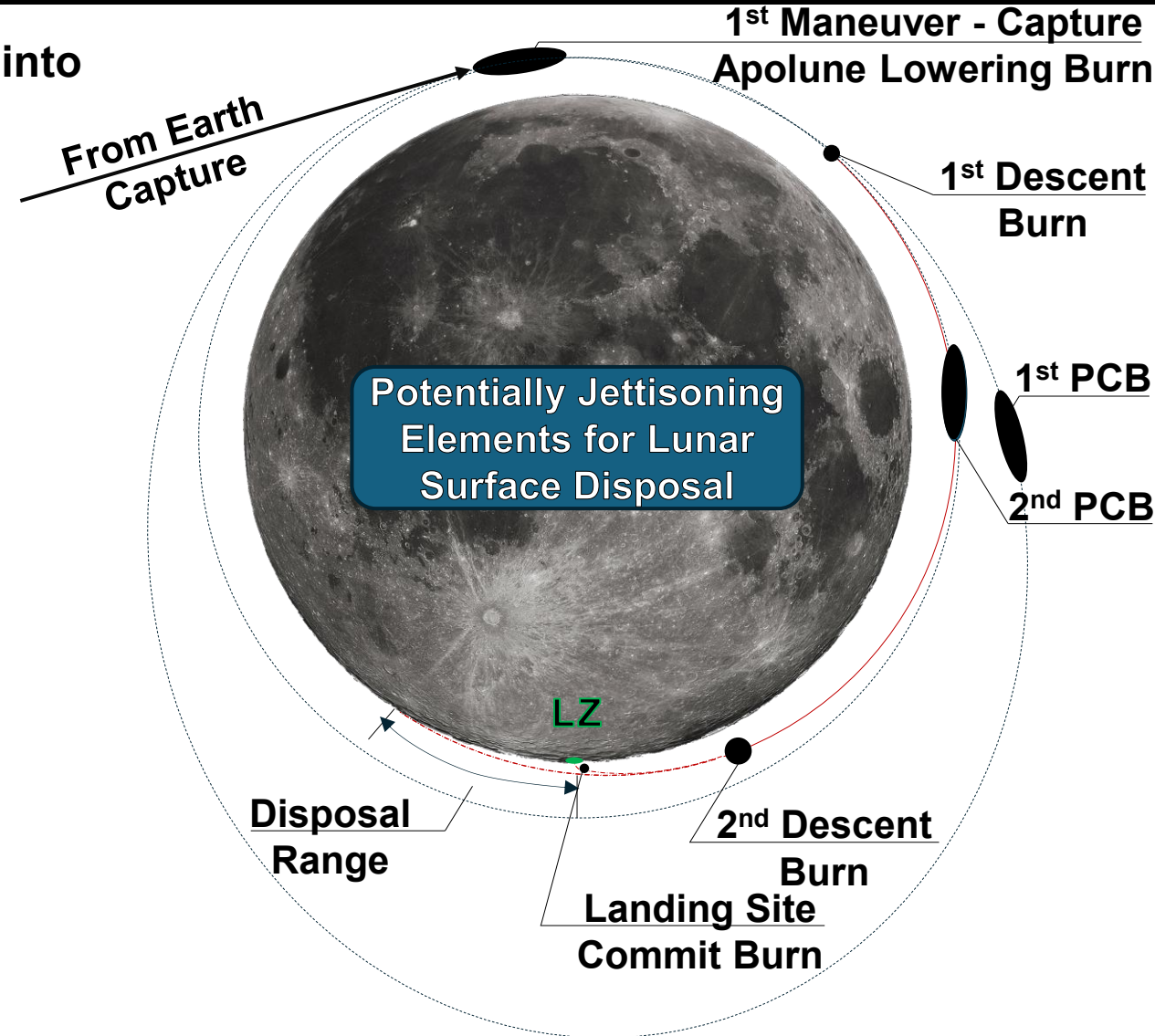
$$m_{\text{payload}} + m_{\text{vehicle}} = 10,400 \text{ kg}$$

$$m_{\text{payload}} + m_{\text{vehicle}} = 10,100 \text{ kg}$$

*It is accepted the
pressurant tank #
is obnoxious*

LUNAR TOUCHDOWN CONOPS

- **1st Maneuver – Capture, retrograde burn, puts Stack into polar elliptical lunar orbit 200 x 1400 km**
 - Capture somewhere in lunar north
 - Hold for 24 hours ~ 8 orbits for nav updating
 - Within 8 orbits, Plane Correction Burn (PCB)
- **Commit to retrograde circularization burn**
 - ~Same location as 1st maneuver
 - Lower to 200 km circular
 - Hold for 24 hours ~ 11 orbits for nav updating
 - Any high altitude GNC should be switched on
- **2nd Plane Change Burn**
 - “Final” landing trajectory selection
- **On subsequent rev, 1st Descent Burn**
 - Puts stack onto terminal path
- **2nd Descent burn, reduces horizontal velocity**
 - At 50 km altitude, start optical TRN
- **Landing Site Commit Burn**





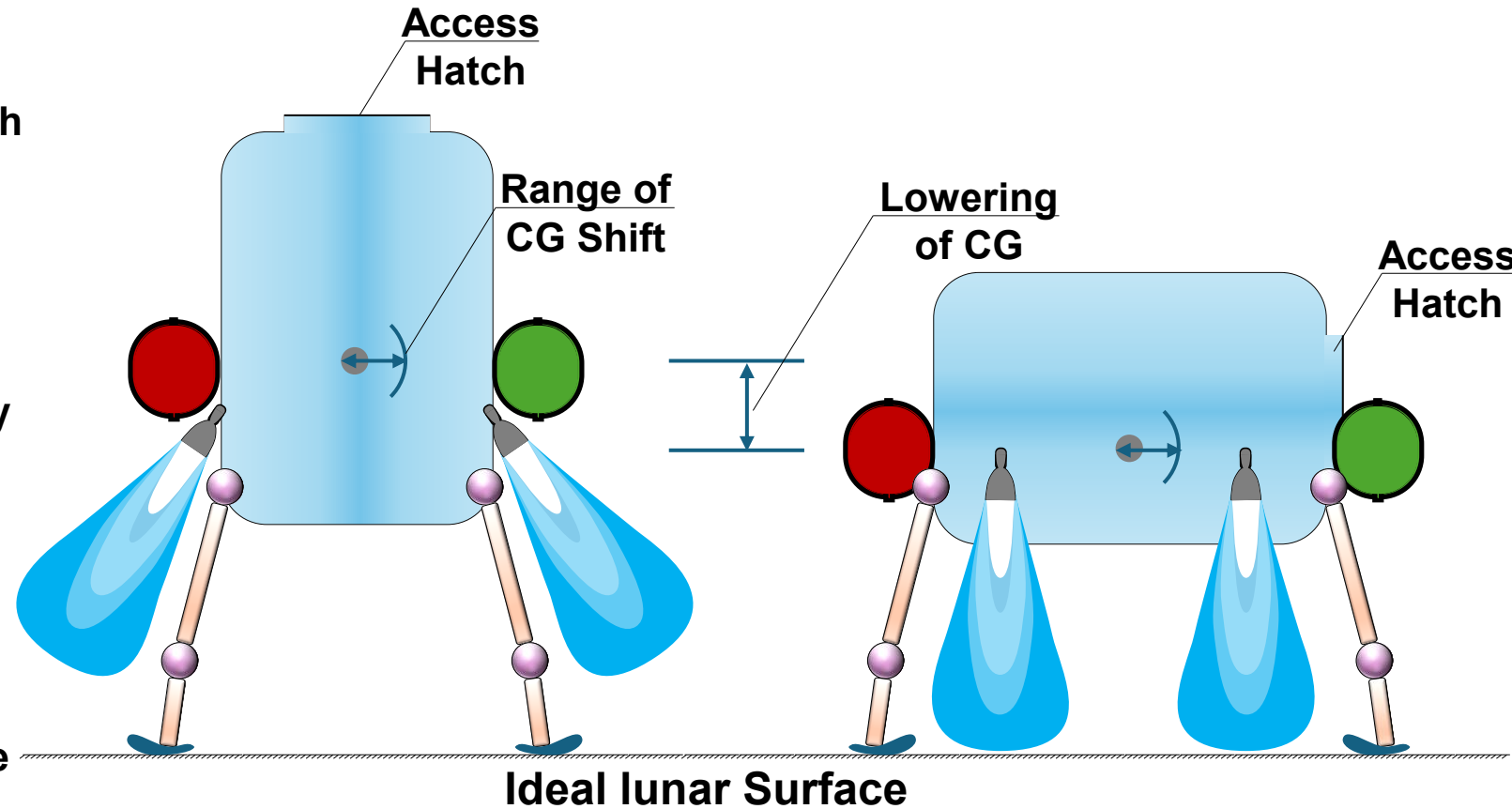
THRUSTER TRADE SPACE



MOON BASE

- ~ 2.4 km/s dV Needed for in space maneuvers
 - TLI + MCC + LDT
- Assume 300s ISP for MMH/NTO thrusters
- >20,000 kg of prop needed
- Thrusters must provide sufficient acceleration to complete transfer
 - Small thrusters would need more orbits & create burn time constraints
 - Big thrusters increase mass & create LV packing constraints
- *Optimal* thrusters enable redundancy and better attitude control
 - Thruster sets should be positioned to push through the mass center
- 900 lb_f (4.00 kN) class thrusters x8 ~ 0.9 m/s²
- 200 lb_f (0.89 kN) class thrusters x8 ~ 0.2 m/s²
- Similar considerations needed for landing
 - How much to arrest vertical velocity?
 - How much needed for attitude/lateral control?

- Payload is ~5.5m $\varnothing$ x 6.6m
- Landing of Vertical vs Horizontal Payload
- *We are part of Moon Base*
 - Current concepts show elements with long axis horizontal on the surface
- **Advantages of Horizontal**
 - Reduced height of access hatch
 - Lowered CG
 - Less off axis thrust (higher efficiency for descent)
 - Wider footprint on longitudinal axis
 - Easier launch packing config
- Prop use will shift cg laterally
 - $\rho_{MMH} \approx 885 \text{ kg/m}^3$, $\rho_{MON3} \approx 1440 \text{ kg/m}^3$
 - Fed at near equal volumetric flowrate



DESCENT TRAJECTORY PROFILE

- Thruster config 4x3, 12 total – 8 used for vertical

- Some off axis θ_j for thrusters

$$g(t_i) = \frac{G \cdot M_L}{(R_L + Alt(t_i))^2}$$

$$\dot{m}_j = \frac{F_{thrust_j}}{g_0 \cdot ISP}$$

Mass Flow Rate

$$a_{net_i} \approx -g(t_i) + \frac{\sum [F_{thrust_j} \cdot \cos(\theta_j)]}{m_i - \Delta t \cdot \sum \dot{m}_j}$$

$$\Delta V_{net_i} \approx a_{net_i} \cdot \Delta t, \quad V_{net}(t_{i+1}) \cong \Delta V_{net_i} + V_{net}(t_i)$$

$$\Delta Alt \approx \Delta V_{net} \cdot \Delta t, \quad Alt(t_{i+1}) \cong \Delta Alt + Alt(t_i)$$

- Assumes 1 Dof

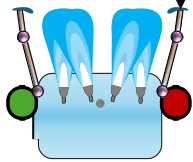
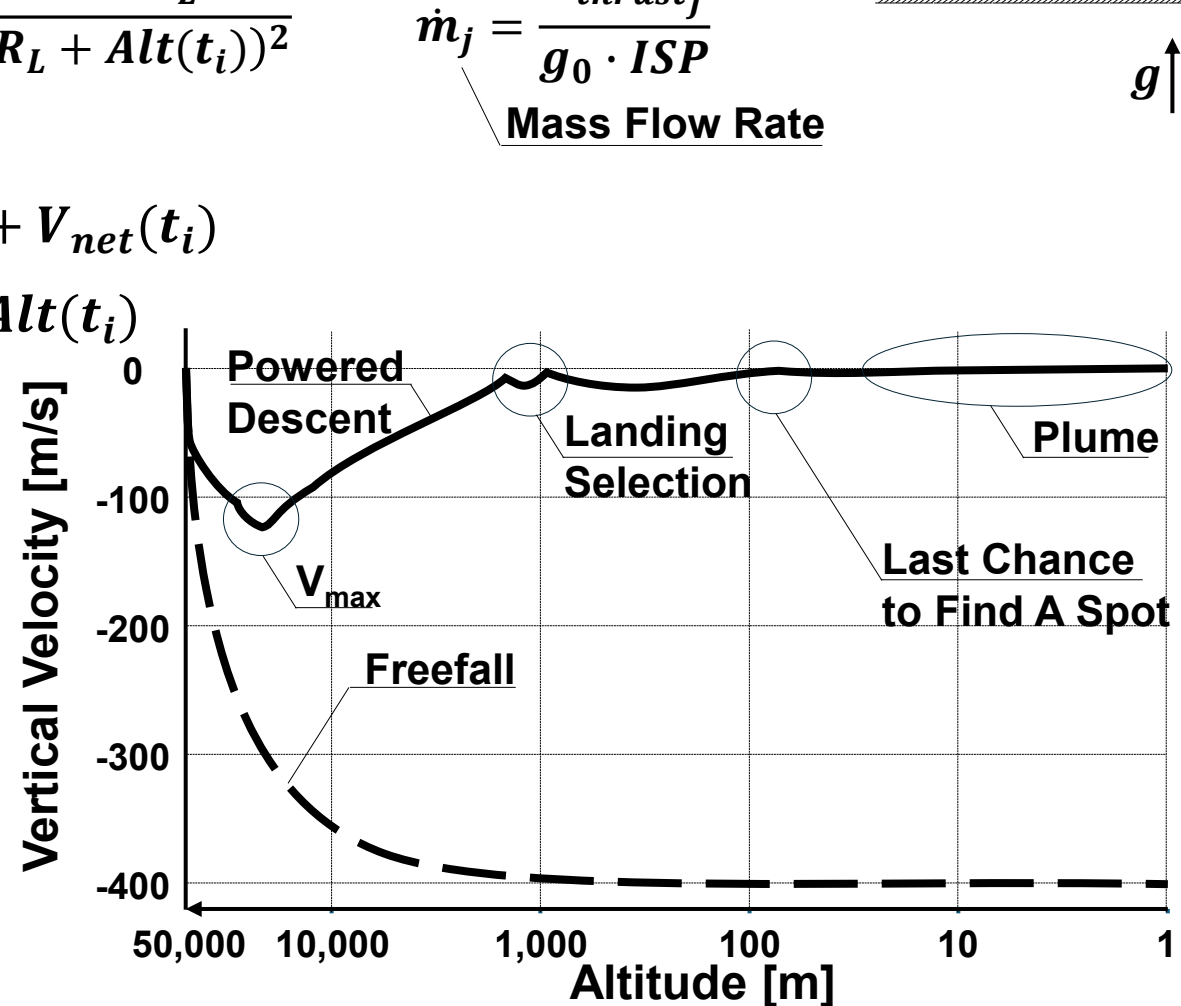
- Variable 2 body gravity
- Additional prop remaining for
 - Rotation & lateral displacement
 - Additional thrusters may be needed to control cg shift

- Velocity change reversal after V_{max}

- Two “hovering” periods occur

- ~1000 m & ~80m
- Optical/Radar navigation, negligible plume

Ideal lunar Surface
South Pole





MOON BASE

PROP HARDWARE LIMITATIONS

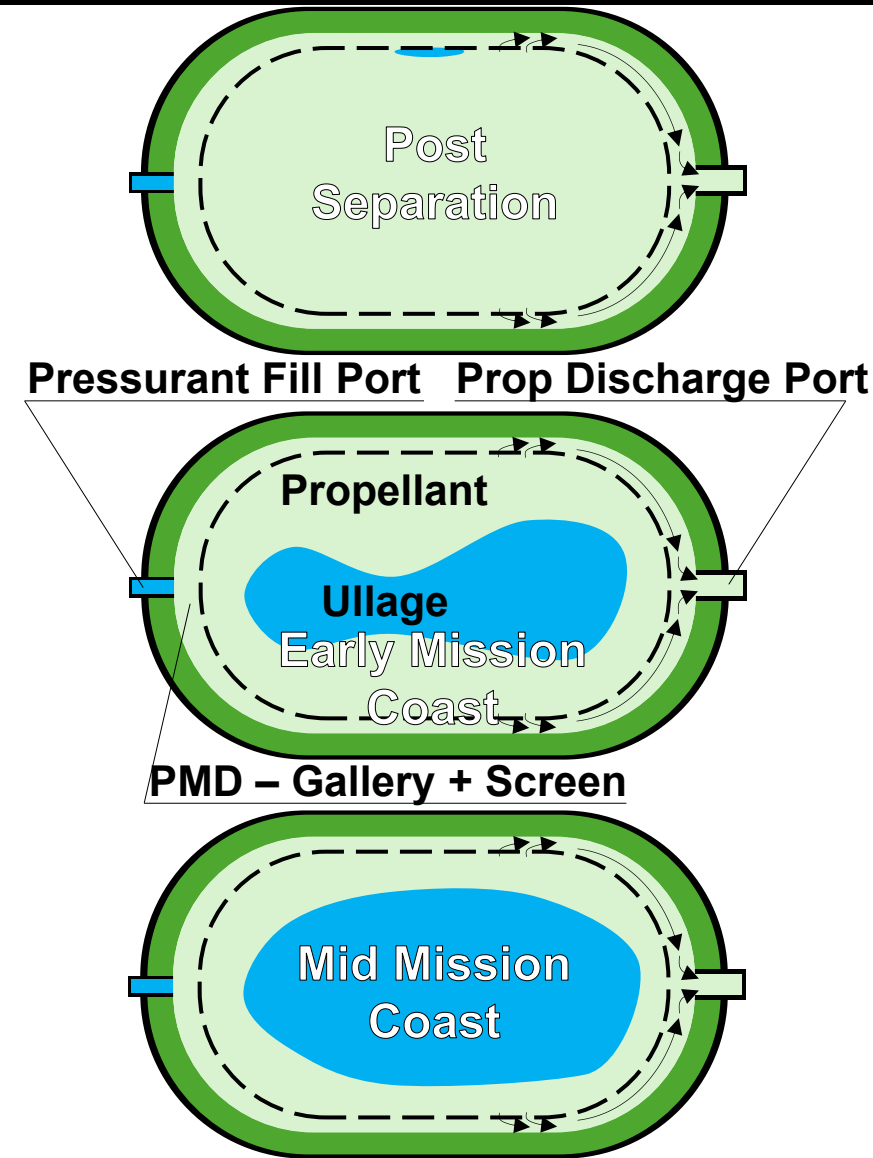
SETTLING PROPELLANT IS AN
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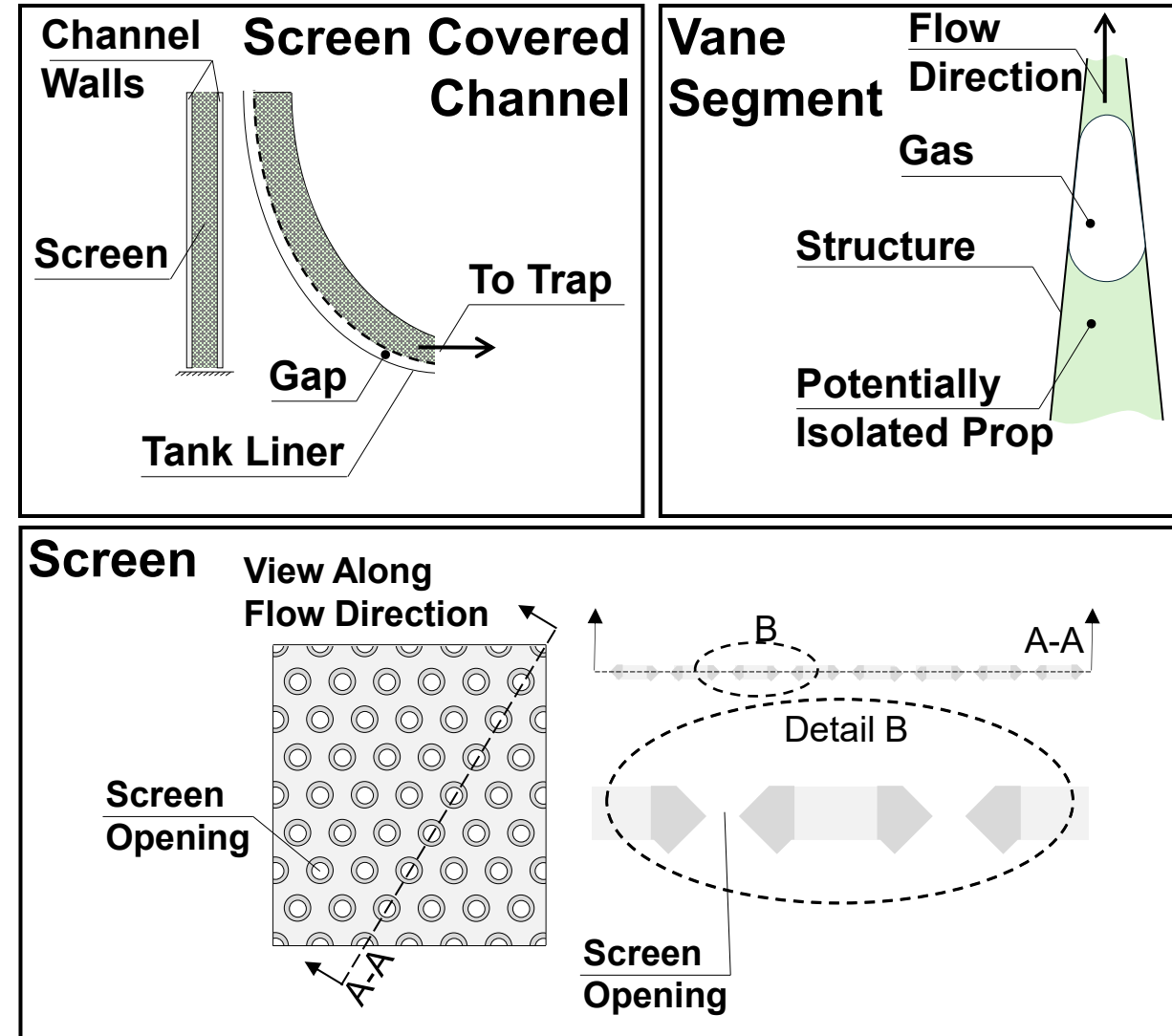
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PROP TANK SELECTION (STOREABLES)

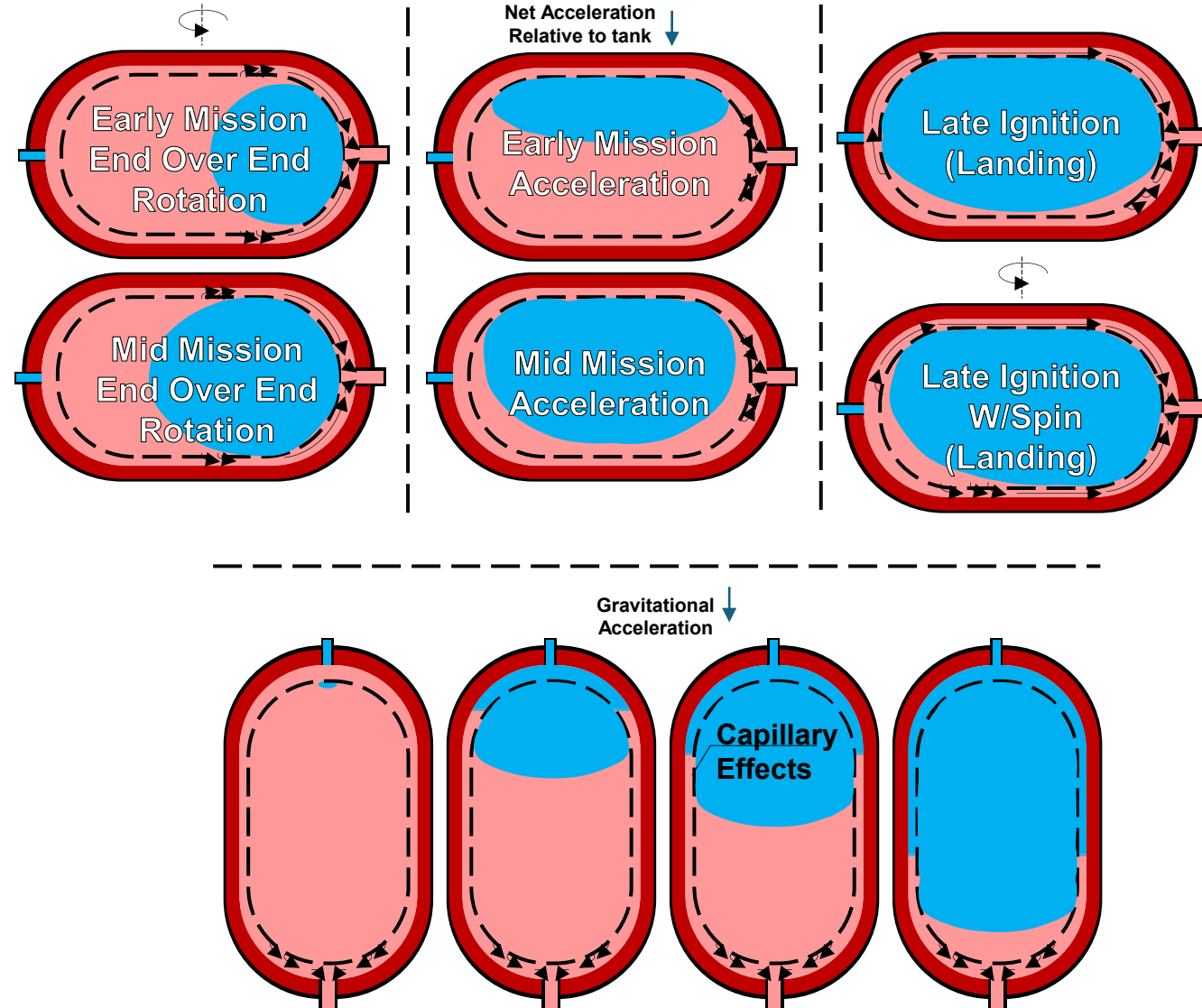
- Prop acquisition is handled by the tank, diaphragm or propellant management devices (PMDs)
 - Whole trade space to explore
- Thin wall structures, metal or COPV designs
 - Tank Volume, Fixed Maximum Expected Operating Pressure (MEOP), Fill Fraction (FF) on Launch are all controlled by tank
- Propellant tanks are developed and qualified, then manufactured
 - PMD's are designed for *in space - sans* gravity
 - Delta Qual is needed to verify performance requirements
- *Saturday Morning Science* Dr. Don Pettit (~47 min)
 - Experiments on the ISS for surface tension – Youtube



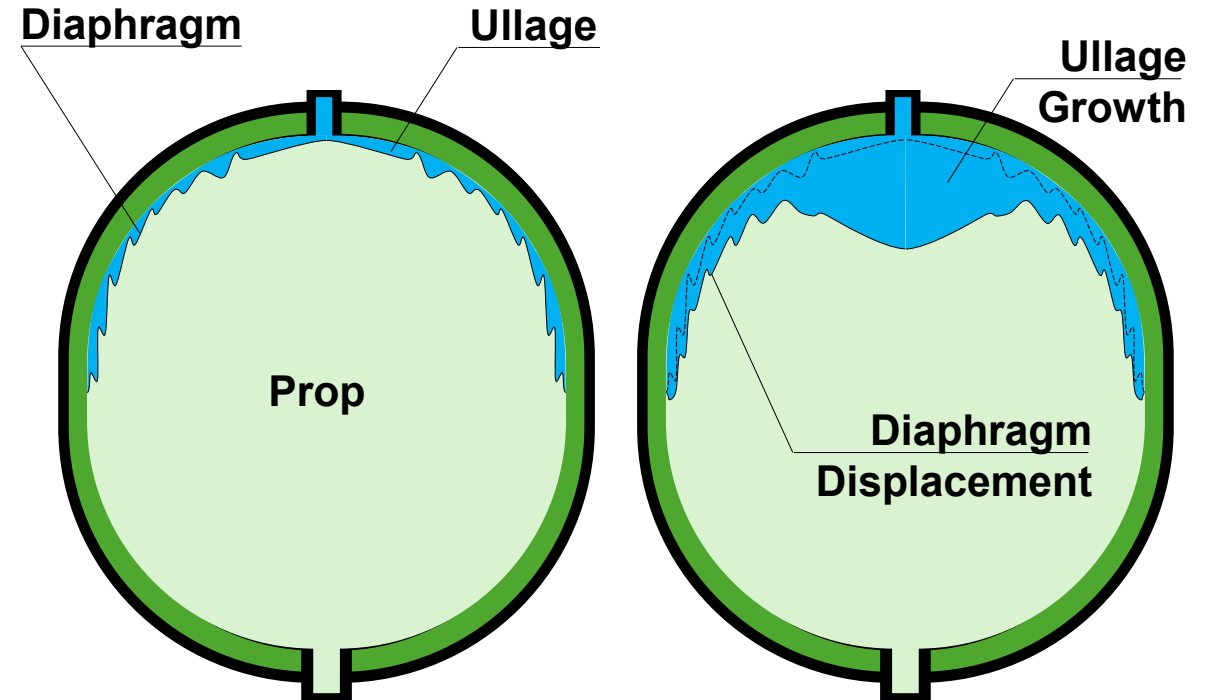
- PMDs ensure ullage (gas) free prop delivered
- PMDs control
 - Minimum Ignition characteristics, GNC flight restrictions, and more
- Geometry/manufacturing determines characteristics
 - Screens, Gallery, Traps, Vanes, Sponges, Channels, Troughs, Pickup assemblies
- NTO/MON3 has more stringent design limitations
 - Higher viscosity & freezing point
- Detail beyond scope of this work
 - D.E Jaekle Jr: AIAA-91-2172, AIAA-93-1970, AIAA-95-2531, AIAA-97-2811



- PMDs must account for linear & rotational movement of prop in flight
 - *Small* tank settling thrust pulse to move ullage - then fire thrusters full bore
- Tank orientation for landing determines ability to provide prop for thrusters
- Descent & Landing is a huge undertaking
 - 12 – 900 lb_f thrusters @ 300s isp 50% duty cycle
~ 55 gal per minute (GPM) of each commodity
 - ~ 8 minutes for those ~92,000 in³ tanks



- Diaphragm - membrane to separate ullage & prop
 - Moves as prop is consumed
- Cons
 - Heavy + Single use
 - Require extensive testing to get shape right
- Advantages
 - Easy to track both commodities
 - Omnidirectional acceleration compliance
 - Useful for high discharge rates





MOON BASE

FLIGHT HARDWARE SYSTEMS

ALSO, AN EXERCISE
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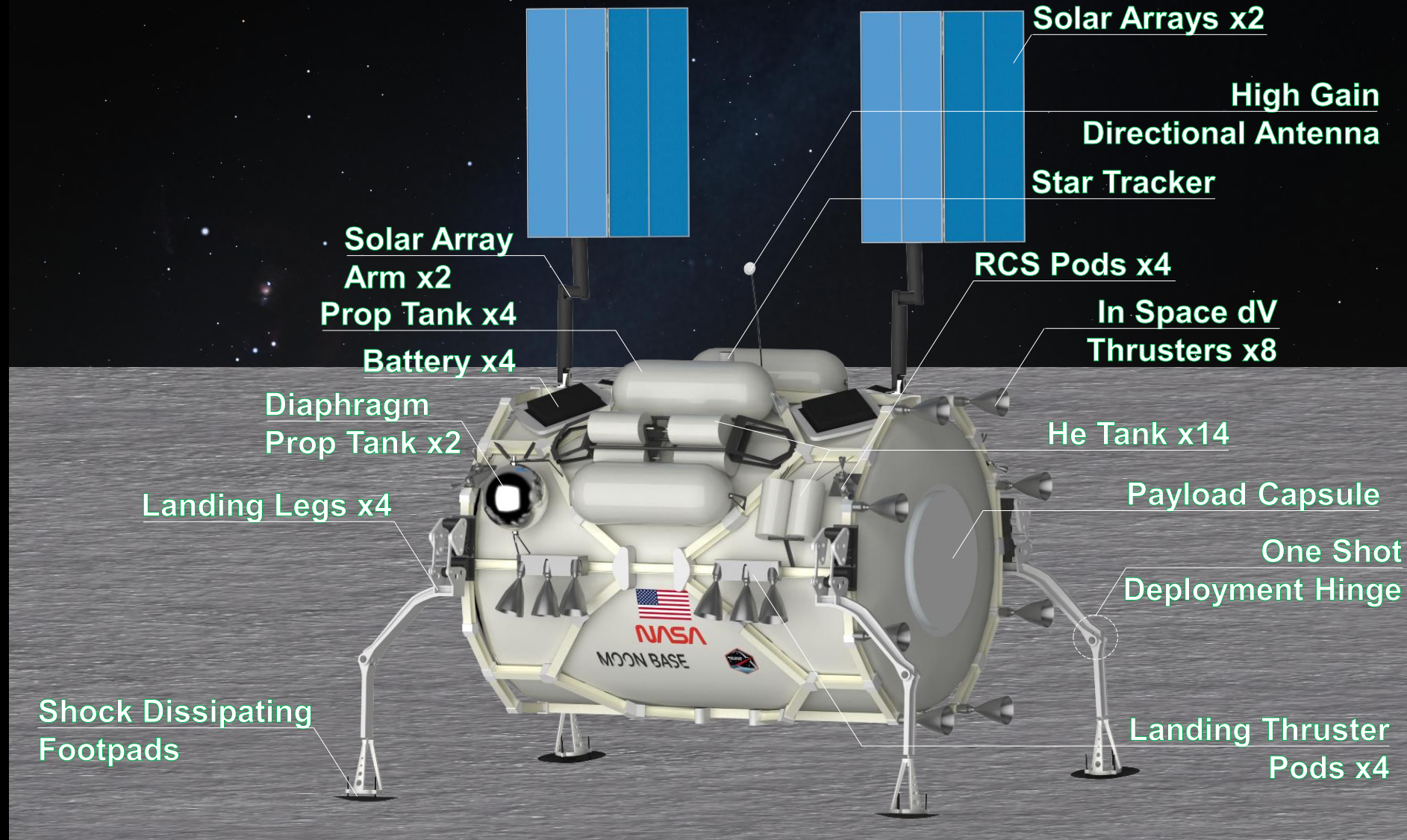
THE LANDER



MOON BASE

- **Not Shown**

- Flight computers
- Radios
- Ground tracking instruments
- Heaters
- Blankets
- Tubes & wires
- Prop manifolds
- Radiators
- Actuator drivers
- Thruster heat shields



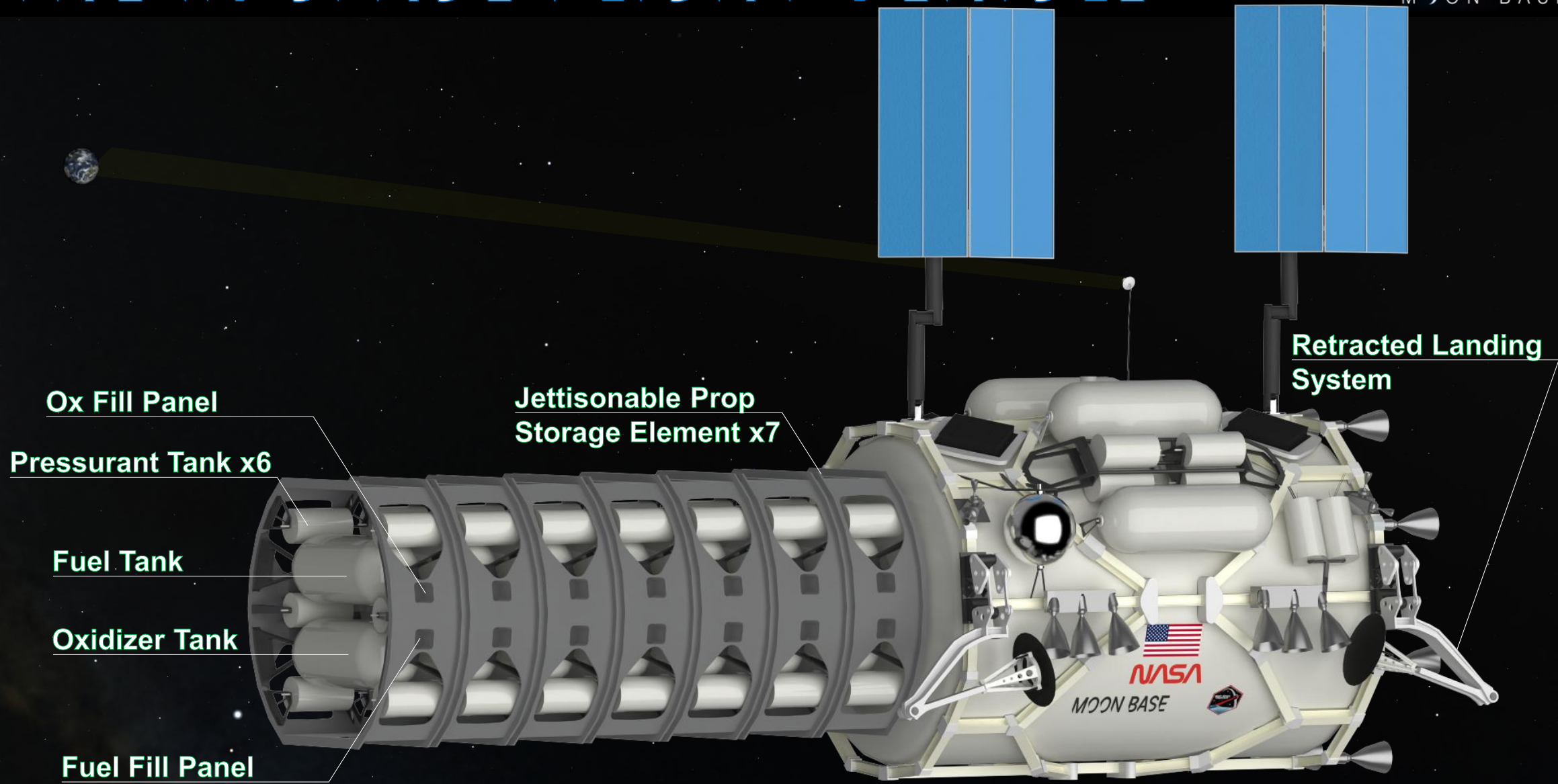
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MOON BASE

THE IN SPACE FLIGHT VEHICLE

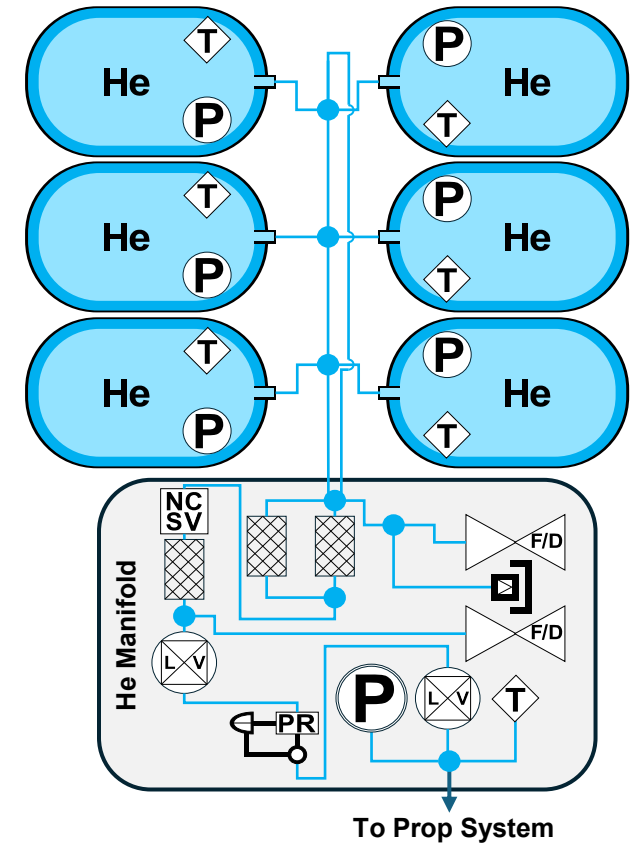
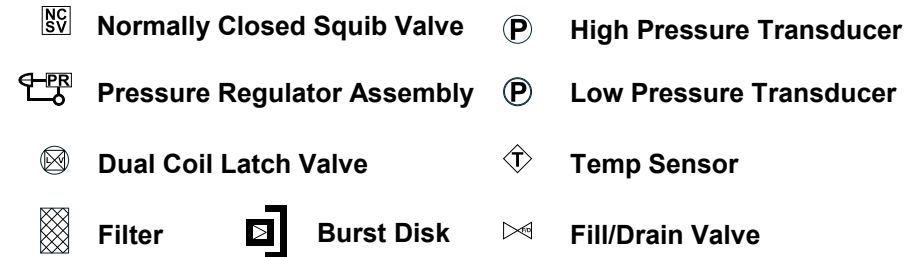




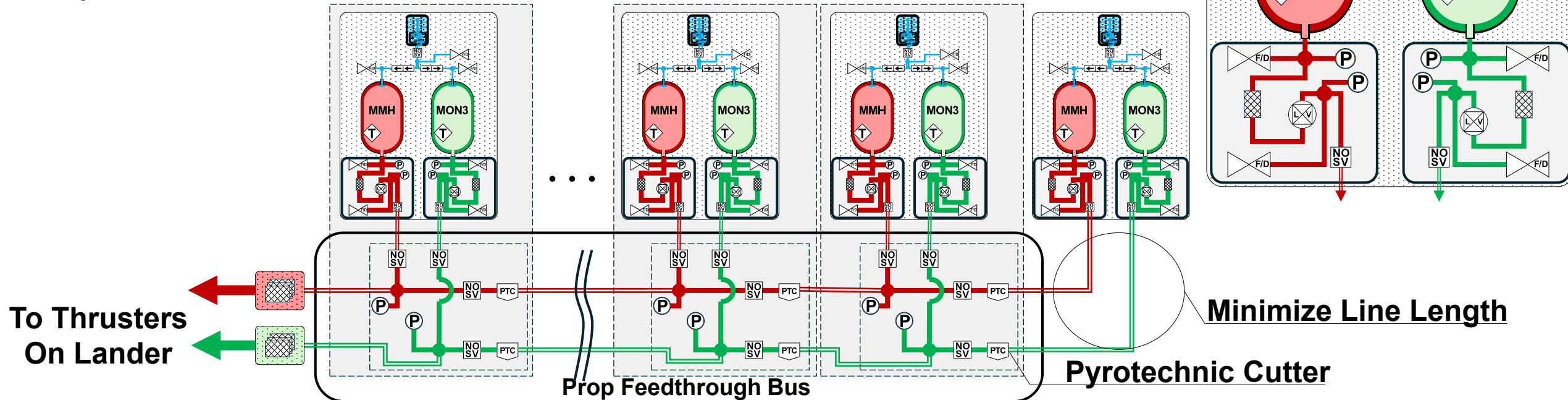
PRESSURANTS – PROP SUBSYSTEM



- He/Prop budgets Interdependent ~5,000/92,500 in³ tanks
- Iterate on number of tanks to what makes sense ~6
 - Pressure regulators must have upstream pressure at “empty” state, prop tanks must be full
 - Compressibility effects of high pressure He
 - Acoustic resonance/data frames/eclipses/etc.
 - double line from tank asy to control resonance
- Trade analysis to determine redundancy requirements on duplicity of elements (Valves/Regulators/etc.)



- From the staged Hohmann transfer orbit table
 - Several stages, ~300 kg (first pass estimate) of structure jettisonable per stage
- Each stage must have its own self test capabilities
- Check valves used for MMH/MON3 isolation & enable shared He
- Independent manufacture/assembly/test/prop load for jettisonable stages
 - “Fast” & scalable process – Big missions, small missions, change # of stages
- Spacecraft common connections minimizes hardware overhead





CONCLUSIONS



MOON BASE

- **A mission solution was presented to take a large payload from the Earth to the Lunar Surface in support of Moon Base**
 - Launch vehicle target orbits were shown
 - Transfer orbit ConOps
 - Landing Descent and Touchdown (LDT) ConOps was presented
- **TLI achieved through jettisonable prop stages**
 - Optimization of TLI burn schedule & vehicle configuration

The authors would like to thank the entirety of the DSL and LENS workforce for their contribution to this effort.

QUESTIONS?



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