



**TFAWS**  
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## Initial Computational Analysis of Helium Subsurface Pressurization

Jacob Brodnick – NASA MSFC ER42  
Jason Hartwig – NASA GRC LTF0

Presented By  
Jacob Brodnick

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# Background

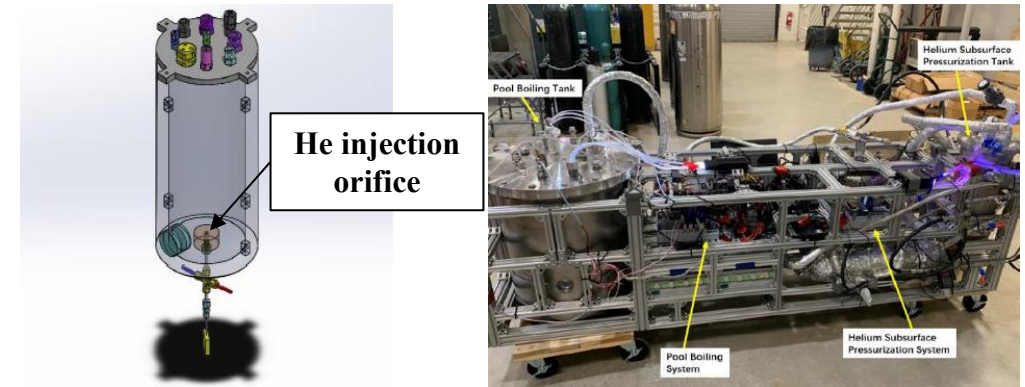


- Helium subsurface pressurization (HSP) in low gravity was simulated using computational fluid dynamics (CFD) analysis.
- Pressurant flow regime characteristics were compared to imagery taken from a parabolic flight experiment conducted under a NASA Flight Opportunities grant, FO 244-P [1].
- Initial results are shown herein while a more comprehensive validation effort will be documented in the future.
- Validation of HSP dynamics is intended to help inform future trade studies of tank pressurization for spacecraft engine restarts and propellant transfer.
  - Efficient methods of pressurizing directly into a cryogenic propellant are sought.
  - Additionally, HSP has been shown to thermally condition cryogenic propellants which may be leveraged in future in-space operations.

- HSP was conducted on the ground and in flight using the hardware shown
  - 30 parabolas were flown over two flights
- Pressurant was injected into an 8.34 L liquid nitrogen (LN2) tank via an orifice
  - Pressurant flow rate and temperature along with orifice diameter were varied
- Tank was filled and continuously vented to 101.3 kPa prior to flight
- A viewport was used to directly image the bubble dynamics during pressurization
- Pressurant dynamics were categorized into flow regimes

## Submerged Pressurization Test Configuration [1]

Left: Tank CAD / Right: Parabolic Flight Test Article



## Measured Flow Regime Map [1]

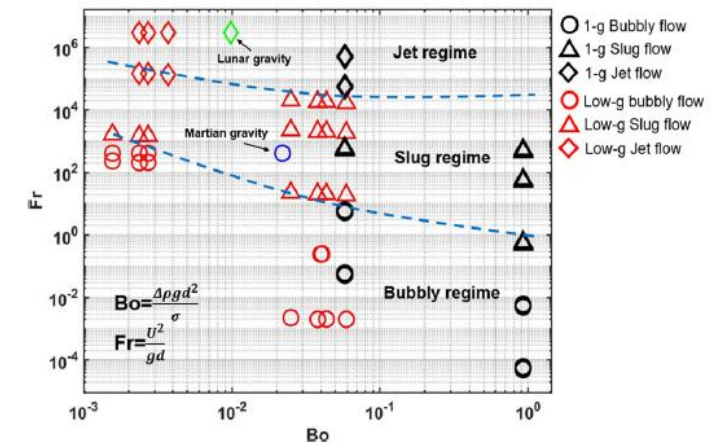


Fig. 12 | Two-phase flow regime map. All gravity levels two-phase flow regime map.

- **Loci-Stream-VoF solver [2]**
  - All-speed pressure-based solver
- **Solver settings:**
  - Unsteady 1<sup>st</sup> order spatial and temporal accuracy
  - Compressible gas with incompressible liquid
  - Boussinesq approximation of natural convection
  - Turbulent RANS k- $\omega$  SST 2003 with interfacial turbulent damping
  - Surface tension and contact angle
  - Volume of Fluid (VoF) model with geometric reconstruction type of interface tracking
  - Phase change excluded in initial simulations, may be impactful in flow regime transitions

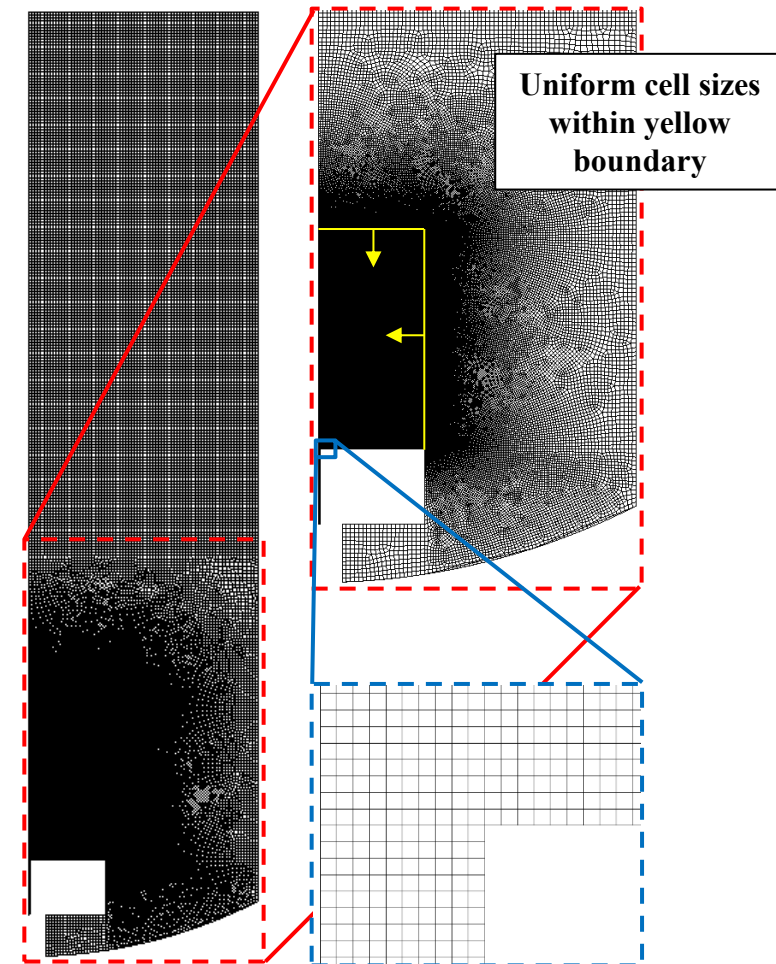
## Model Geometry

Modeled tank was smaller than test article, correcting model for future validation



## Computational Mesh

Initial simulations were axisymmetric to facilitate rapid sensitivity study



## Flight Test Matrix [1]

- Two test cases were selected initially to begin identifying modeling methodology and numerical convergence criteria for capture of HSP dynamics
- A high and middle flow rate condition are highlighted in the reported flight test matrix [1]

| Test Number | Orifice Diameter (mm) | Gravity Level (g/g <sub>o</sub> ) | Inlet Temp (K) | Inlet Mass Flow Rate (kg/s) |
|-------------|-----------------------|-----------------------------------|----------------|-----------------------------|
| 2-1         | 1                     | 0.038                             | 185            | 2.73E-07                    |
| 2-2         | 1                     | 0.042                             | 186            | 2.73E-06                    |
| 2-3         | 1                     | 0.035                             | 247            | 8.18E-06                    |
| 2-4         | 1                     | 0.043                             | 200            | 2.73E-08                    |
| 2-5         | 1                     | 0.031                             | 214            | 2.73E-06                    |
| 2-6         | 1                     | 0.041                             | 255            | 8.18E-06                    |
| 2-7         | 1                     | 0.041                             | 230            | 2.73E-09                    |
| 2-8         | 1                     | 0.029                             | 172            | 2.73E-07                    |
| 2-9         | 1                     | 0.047                             | 218            | 2.73E-09                    |
| 2-10        | 1                     | 0.044                             | 198            | 2.73E-08                    |
| 2-11        | 1                     | 0.025                             | 260            | 8.18E-06                    |
| 2-12        | 1                     | 0.027                             | 208            | 2.73E-09                    |
| 2-13        | 1                     | 0.032                             | 182            | 2.73E-07                    |
| <b>2-14</b> | <b>1</b>              | <b>0.046</b>                      | <b>208</b>     | <b>2.73E-06</b>             |
| 2-15        | 1                     | 0.064                             | 230            | 2.73E-09                    |
| <b>2-16</b> | <b>1</b>              | <b>0.051</b>                      | <b>170</b>     | <b>2.73E-07</b>             |
| 2-17        | 0.25                  | 0.031                             | 196            | 2.73E-09                    |
| 2-18        | 0.25                  | 0.039                             | 215            | 2.73E-07                    |
| 2-19        | 0.25                  | 0.045                             | 207            | 8.18E-06                    |

**Simulated Conditions**

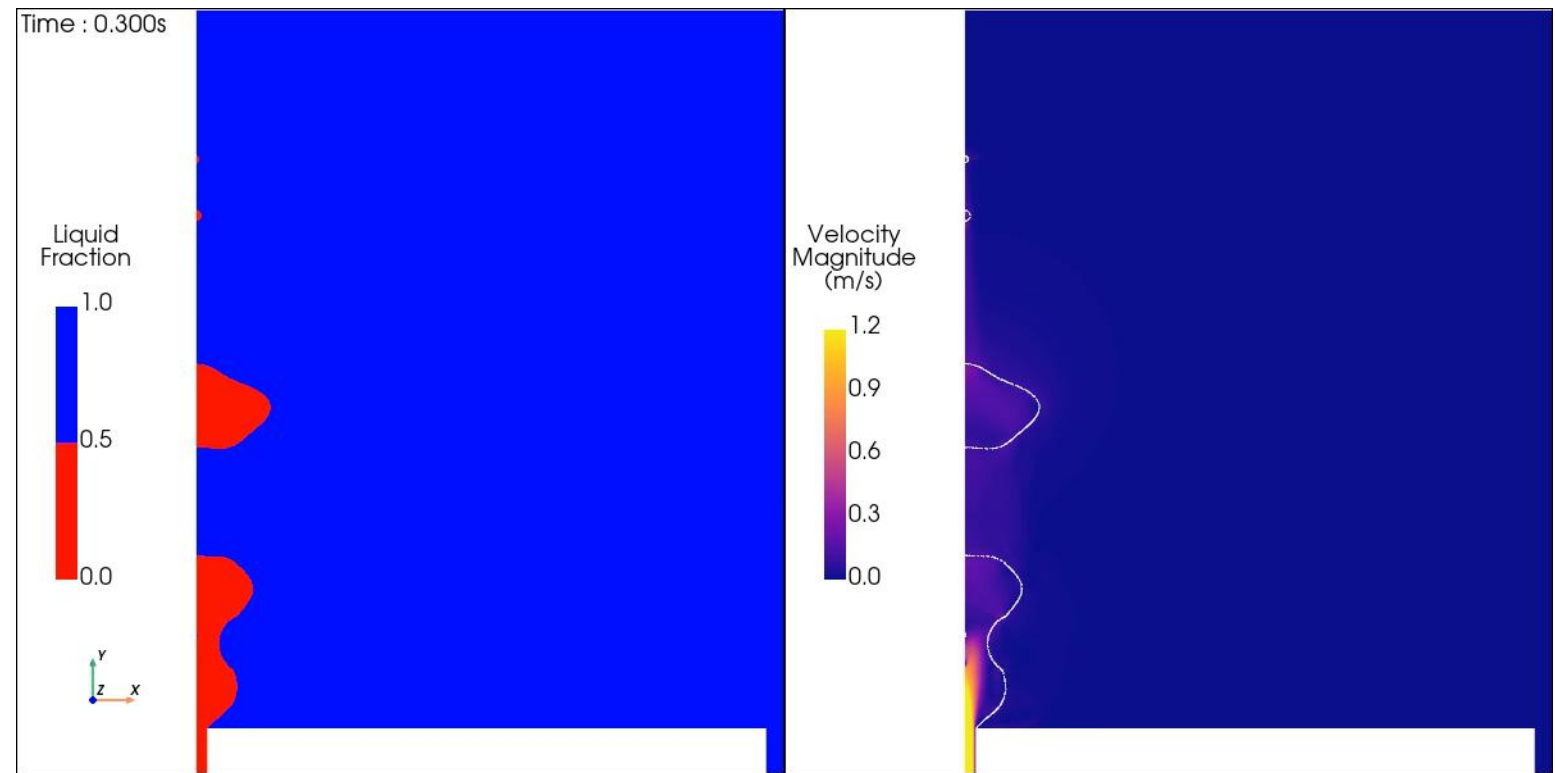
High Flow Rate Case

Middle Flow Rate Case

- Nominal simulation results for test case 2-16 are shown
- Distinct bubbles form and detach as buoyancy overcomes surface tension near the orifice-tank interface
- Following detachment, bubble growth from the orifice can exceed detached bubble convection causing two bubbles of combine
- The resulting dynamics often imparted momentum into the combined bubble such that further bubble combination was not observed

## Animation of Simulated Pressurant Dynamics

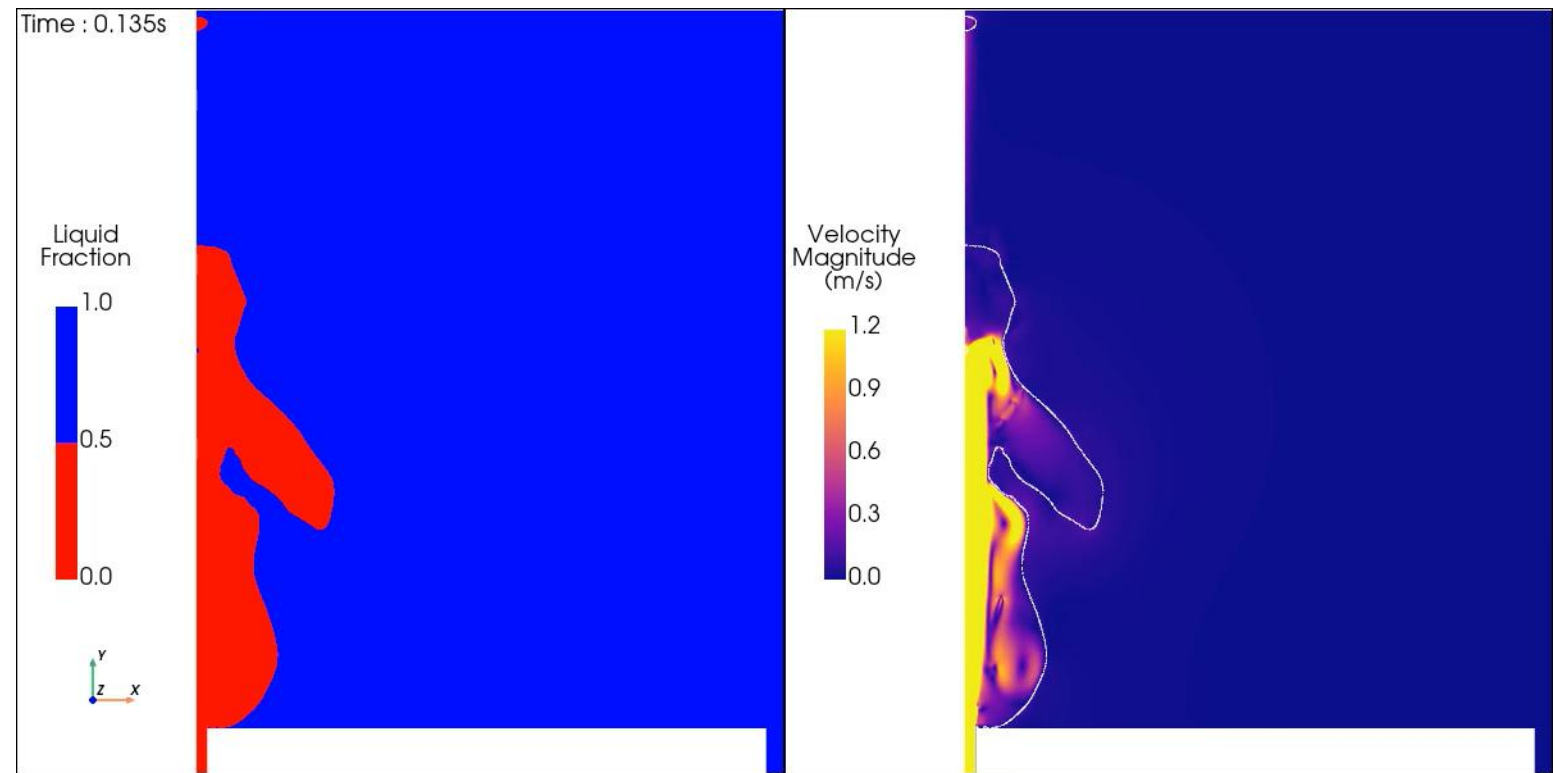
Case 2-16



- Nominal simulation results for test case 2-14 are shown
- No distinct bubble formation was observed
- Pressurant momentum significantly exceeded buoyancy driven convection resulting in more chaotic bubble formation, detachment, and combination
- Periodic bubble detachment was observed but rapid bubble recombination makes the resulting structure look continuous with periodic bulges

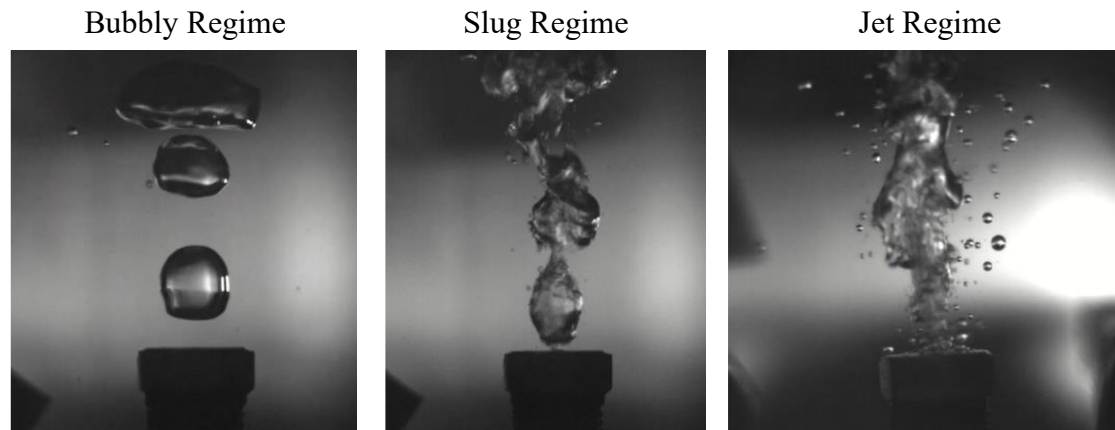
## Animation of Simulated Pressurant Dynamics

Case 2-14

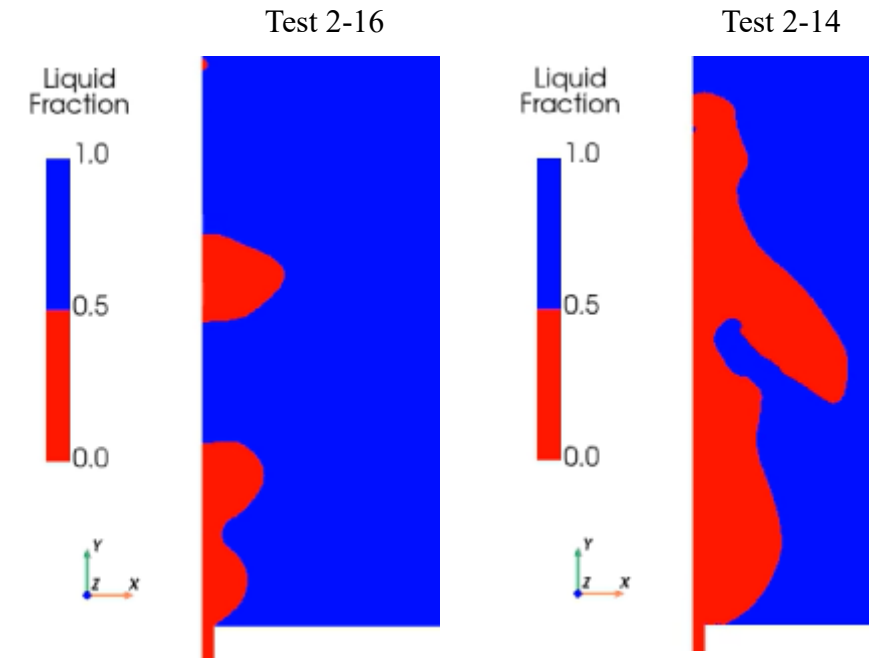


- Multiple flow regimes were identified in testing which are shown below
- Predicted flow regimes correspond well to experimental observations, but quantitative comparison of transition regions is still in-work
  - Case 2-16 (middle flow rate): bubbly-to-slug flow transition
  - Case 2-14 (high flow rate): slug regime

## Low-g Bubble Detachment Visualization Data [1]



## Low-g Bubble Detachment Analysis Snapshots



# Conclusion

- Initial CFD simulation results of low-g HSP in a small LN2 tank were predicted.
- Predicted flow regimes included (1) distinct bubble formation and (2) periodic bubble detachment and combination which correspond well to experimental observations.
- Quantitative comparison of transition regions between flow regimes is still in-work.
- The present analysis is a part of a concerted effort to better understand if subsurface pressurization is viable or optimal for any applications or parameter spaces in future NASA missions.



# Forward Work

- Include phase change in CFD simulations
- Demonstrate mesh and mass transfer convergence
- Demonstrate contact angle sensitivity
- Expand the simulated set of test conditions
- Compare bulk liquid cooling predictions to test measurements



# References

1. Jinze Yu, et. al., "Cryogenic helium subsurface pressurization in terrestrial and low-gravity: experiments and flow visualization," Microgravity Journal Paper, 2025.
2. <https://www.snumerics.com/>