RATES OF HYDROGEN-GRAPHITE REACTION Between 1550° AND 2260° C

by William A. Sanders

Lewis Research Center
Cleveland, Ohio

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION • WASHINGTON, D. C. • APRIL 1965
RATES OF HYDROGEN-GRAPHITE REACTION
BETWEEN 1550° AND 2260° C

By William A. Sanders
Lewis Research Center
Cleveland, Ohio

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

For sale by the Office of Technical Services, Department of Commerce,
Washington, D.C. 20230 -- Price $1.00
RATES OF HYDROGEN-GRAPHITE REACTION
BETWEEN 1550° AND 2260° C
by William A. Sanders
Lewis Research Center

SUMMARY

The rates of reaction of a pitch-free, petroleum coke-base graphite with purified hydrogen were determined in the temperature range 1550° to 2260° C. Experimental weight losses agree very well above 1800° C with calculations based on thermodynamic data for the hydrogen-graphite theoretical equilibrium compositions, where acetylene is calculated to be the major reaction product. Although the experimental curve and the theoretical curve diverge below 1800° C, equilibrium might be achieved at temperatures below 1800° C if slower hydrogen flow rates were employed.

INTRODUCTION

Past experimental investigations of the thermal equilibrium between hydrogen and carbon agree reasonably well with the results obtained by calculation to about 1000° C (ref. 1) and indicate that methane (CH₄) is essentially the sole reaction product, the equilibrium concentration of CH₄ decreasing with increasing temperature. One investigator, however, reports a minimum methane concentration at 1450° C followed by an increase in methane concentration with increase in temperature to 2000° C (ref. 2). Up to 1450° C, the methane concentrations measured were somewhat higher than the calculated equilibrium concentrations. Reference 2 suggested that this disagreement was possibly due to a thermal diffusion effect and that the increase in CH₄ concentration between 1450° and 2000° C resulted from the increasing production (with increasing temperature) of radicals, such as methenyl (CH), methylene (CH₂) or methyl (CH₃), that diffuse away from the hot zone and react with hydrogen to form CH₄ (ref. 2). In this same study acetylene (C₂H₂) and ethylene (C₂H₄) were found to form above 1750° C. Other investigators report that C₂H₂ is the major product at 2050° C (ref. 3).

The work reported herein concerns the determination of the graphite weight loss due to the reaction of a graphite surface with flowing hydrogen in the temperature range 1550° to 2260° C. The goal of the investigation was to approximate equilibrium conditions and compare experimental weight losses with those calculated from thermodynamic data. The work was prompted by disagreements noted between some experimental weight-loss measurements made at this
laboratory and losses predicted by assuming CH₄ formation only.

Graphite test shapes were spherical to eliminate sharp edges and to provide a uniform hydrogen flow around the test piece. The low hydrogen flow of 0.1 standard cubic foot per minute (0.031 lb/hr, 0.38 ft/sec) was chosen in an effort to achieve equilibrium.

MATERIALS

The test graphite was a moldable, pitch-free, petroleum coke-base graphite. Molded bodies are graphitized at about 2500°C and exhibit isotropic properties. For this study the graphite test shapes were 1.48-inch-diameter spheres with a density of 1.65 grams per cubic centimeter. The as-received spheres were machined, outgassed, and weighed before testing.

Tank hydrogen was purified with a palladium tube purifier. Water content of the purified hydrogen was less than 1 part per million by volume (analyzer detection limit).

APPARATUS

The induction furnace used to heat the graphite spheres is described in reference 4. Figure 1 shows the furnace and the loaded tungsten susceptor detail. The graphite sphere was supported on a tripod stand constructed of 1/8-inch tantalum rod positioned within a 1 3/4-inch-diameter, 0.050-inch-wall tungsten susceptor 3 1/2 inches long. The susceptor had a 5/8-inch hole both in its base and in its removable lid for hydrogen gas exit and entrance.

Temperature was determined with a disappearing filament optical pyrometer, which, along with the furnace sighting prism, had been calibrated against a National Bureau of Standards certified standard lamp. Curves of induction-coil voltage setting against temperature were plotted for sighting on a tungsten button at the bottom of the susceptor and for sighting on the top of a graphite sphere in the test position, which was 1/2-inch below the susceptor lid. These determinations were made under hydrogen test flow conditions and provided a relation between tungsten button temperature and graphite sphere temperature for the same coil voltage settings. The tungsten button within the susceptor was under approximately blackbody conditions, and the test temperatures reported were determined from the measured ball temperature and the established relation between ball temperature and tungsten button temperature (true temperature). The reported temperatures are believed accurate within ±25°C.

Hydrogen flow into the induction furnace was measured with a flowmeter, which was calibrated for the flow range 0.02 to 0.20 standard cubic foot per minute at 770 millimeters of mercury (1.01 atm) and 22°C. The graphite-sphere - susceptor geometry resulted in a minimum annular cross-sectional area for hydrogen gas flow of 4.37x10⁻³ square foot. For a test flow of 0.1 standard
Figure 1. Schematic view of induction furnace.
cubic foot per minute, the maximum hydrogen flow velocity is then 0.38 foot per second. The hydrogen flow could be read directly to 0.005 standard cubic foot per minute and estimated to 0.001 standard cubic foot per minute.

EXPERIMENTAL PROCEDURE

The graphite spheres were first machined to remove molding bands and then outgassed in vacuum at 2320° C for 1 hour. They were then weighed and stored in a vacuum desiccator. Weighing was done with a direct-reading analytical balance having a precision of ±0.05 milligram. To perform a test, a weighed sphere was loaded into the induction furnace, which was then evacuated to about 5x10^-6 millimeter of mercury, and blanked off. High-purity helium was bled into the furnace to a static pressure of 550 millimeters of mercury, and heating was begun. An inert gas blanket was used while heating in order to suppress graphite evaporation. Helium, having a heat conductivity close to that of hydrogen, was chosen to minimize the power correction necessary to maintain the desired test temperature once the hydrogen flow was started. The heating time to test temperature varied from 22 to 36 minutes, depending on the temperature. When the test temperature was reached, hydrogen flow was started at the rate of 0.10 standard cubic foot per minute, and power was adjusted so that in 4 minutes the desired constant temperature was attained. The test period of 1 hour began at this point. The furnace pressure remained constant at the slightly positive pressure of 770 millimeters of mercury (1.01 atm).

At the conclusion of the 1-hour test period, the hydrogen flow was stopped, the power was shut off, and the furnace was evacuated and then filled with helium. When the furnace had cooled, the graphite sphere was removed and weighed. Weight loss was determined from the weights before and after the test and compared with the losses predicted by calculations based on thermodynamic data.

DISCUSSION OF RESULTS

The results of the weight-loss study are presented in figure 2. The weight-loss data were plotted on a log scale against the reciprocal of the absolute temperature. A straight line determined by the least-squares method was found to fit the data points well. Thermodynamic property data for 1-atmosphere equilibrium compositions in the hydrogen-graphite system (ref. 5) were used to calculate the theoretical graphite weight losses for CH₄ formation and also for the formation of other hydrocarbons. The equilibrium constants for several hydrocarbons and the computed amounts of graphite consumed as a result of the formation of each hydrocarbon for the temperatures 1527° C (1800° K) and 2327° C (2600° K) are presented in table I. The computations were for the following test conditions: hydrogen flow, 0.1 standard cubic foot per minute; hydrogen pressure, 1 atmosphere; graphite sphere area, 44.6 square centimeters. It can be seen that the contributions to graphite consumption by hydrocarbons other than CH₄ and C₂H₂ are negligible at 1527° C (1800° K), while at 2327° C (2600° K) only C₂H₂ is a significant contributor to graphite loss. A sample calculation is presented in the appendix. The relations between calculated graphite weight loss rate and reciprocal temperature for CH₄ formation, for C₂H₂ formation, and for both CH₄ and C₂H₂ formation combined are also plotted in
Comparison of the experimental and theoretical curves of figure 2 indicates that the experimental curve compares very well above $1800^\circ$ C with the calculated summation curve for CH$_4$ and C$_2$H$_2$ formation. Formation of C$_2$H$_2$, the major reaction product above $1800^\circ$ C, accounts for 10 times as much graphite loss as does CH$_4$ formation at $1800^\circ$ C and 200 times as much at $2260^\circ$ C. Because of the good overall agreement between the experimental curve and the theoretical curve for graphite weight loss due to C$_2$H$_2$ formation, it might be concluded that C$_2$H$_2$ formation is the principal reaction over the entire range of test temperatures. Such a conclusion would be highly questionable, however, since it precludes the formation of any CH$_4$ in a temperature region where significant quantities of CH$_4$ are reported to form. The achievement of equilibrium at temperatures below $1800^\circ$ C might be possible if a slower flow rate were employed.

**Table I. - Equilibrium Constants for Various Hydrocarbons and Computed Amounts of Carbon Consumed by Formation of Each**

<table>
<thead>
<tr>
<th>Hydrocarbon</th>
<th>Temperature</th>
<th>Equilibrium constant, K</th>
<th>Carbon consumed, (g/sq cm)/sec</th>
<th>Equilibrium constant, K</th>
<th>Carbon consumed, (g/sq cm)/sec</th>
</tr>
</thead>
<tbody>
<tr>
<td>Methane (CH$_4$)</td>
<td>1527°C (1800 K)</td>
<td>7.54x10^-4</td>
<td>3.98x10^-7</td>
<td>1.19x10^-4</td>
<td>6.26x10^-8</td>
</tr>
<tr>
<td>Acetylene (C$_2$H$_2$)</td>
<td></td>
<td>1.98x10^-4</td>
<td>2.09x10^-7</td>
<td>1.81x10^-2</td>
<td>1.91x10^-5</td>
</tr>
<tr>
<td>Ethylene (C$_2$H$_4$)</td>
<td></td>
<td>4.76x10^-6</td>
<td>5.03x10^-9</td>
<td>9.91x10^-6</td>
<td>1.04x10^-8</td>
</tr>
<tr>
<td>Methyl radical (CH$_3$)</td>
<td></td>
<td>9.47x10^-6</td>
<td>5.00x10^-9</td>
<td>1.30x10^-4</td>
<td>6.85x10^-8</td>
</tr>
<tr>
<td>Methylene radical (CH$_2$)</td>
<td></td>
<td>3.50x10^-7</td>
<td>1.85x10^-10</td>
<td>1.06x10^-4</td>
<td>5.59x10^-8</td>
</tr>
<tr>
<td>Methenyl radical (CH)</td>
<td></td>
<td>3.67x10^-12</td>
<td>1.93x10^-15</td>
<td>7.08x10^-7</td>
<td>3.73x10^-10</td>
</tr>
</tbody>
</table>
CONCLUSIONS

An investigation was conducted concerning the reaction of graphite and hydrogen in the temperature range 1550° to 2260° C. In this temperature range the reaction had not been well defined. The experimental data agree very well with theoretical calculations based on thermodynamic data for temperatures above 1800° C, which indicates that acetylene is the major reaction product.

Since equilibrium is apparently achieved above 1800° C at the hydrogen flow rate employed (0.1 standard cu ft/min), any lesser flow would also be expected to yield equilibrium conditions in the apparatus employed and would permit the attainment of equilibrium below 1800° C.

Lewis Research Center,
National Aeronautics and Space Administration,
Cleveland, Ohio, January 12, 1965.
APPENDIX - SAMPLE CALCULATION OF THEORETICAL GRAPHITE LOSS CALCULATED FROM THERMODYNAMIC PROPERTY DATA FOR 1-ATMOSPHERE EQUILIBRIUM COMPOSITIONS IN HYDROGEN-GRAPHITE SYSTEM

The theoretical equilibrium constants for CH₄ and for C₂H₂ for the temperature range 1527° to 2327° C (1800° to 2600° K) given in reference 5 were used to determine the quantity of CH₄ or C₂H₂ formed.

For methane

\[
C(s) + 2H_2(g) \rightarrow CH_4(g)
\]

\[
K_{CH_4} = \frac{p_{CH_4}}{(p_{H_2})^2}
\]

(1)

For acetylene

\[
2C(s) + H_2(g) \rightarrow C_2H_2(g)
\]

\[
K_{C_2H_2} = \frac{p_{C_2H_2}}{p_{H_2}}
\]

(2)

where

K  equilibrium constant
p  partial pressure
H₂  molecular hydrogen

At 1 atmosphere of hydrogen pressure, equations (1) and (2) become

\[
p_{CH_4} = K_{CH_4}
\]

(3)

\[
p_{C_2H_2} = K_{C_2H_2}
\]

(4)

From the equilibrium data of reference 5 for 1827° C (2100° K)

\[
K_{CH_4} = 3.17 \times 10^{-4} = p_{CH_4}
\]

\[
K_{C_2H_2} = 1.63 \times 10^{-3} = p_{C_2H_2}
\]
For a 1-atmosphere hydrogen pressure at a hydrogen flow rate of 0.00196 gram-mole per second (0.1 standard cu ft/min), the quantity of hydrocarbon formed is

For methane

\[ \text{CH}_4 = \frac{P_{\text{CH}_4}}{P_{\text{H}_2}} \times 0.00196 = \frac{3.17 \times 10^{-4}}{1} \times 0.00196 = 6.21 \times 10^{-7} \text{ moles/sec} \]

For acetylene

\[ \text{C}_2\text{H}_2 = \frac{P_{\text{C}_2\text{H}_2}}{P_{\text{H}_2}} \times 0.00196 = \frac{1.63 \times 10^{-3}}{1} \times 0.00196 = 3.19 \times 10^{-6} \text{ moles/sec} \]

The moles of hydrocarbon formed per second are then converted to grams of carbon lost per square centimeter per second by assuming a graphite surface area of 44.6 square centimeters (the surface area of a graphite test sphere):

\[ \text{C loss for CH}_4 = \frac{6.21 \times 10^{-7} \text{(moles/sec)CH}_4}{44.6 \text{ sq cm}} \frac{12 \text{ g C}}{\text{mole CH}_4} = 1.67 \times 10^{-7} \text{(g/sq cm)/sec} \]

\[ \text{C loss for C}_2\text{H}_2 = \frac{3.10 \times 10^{-6} \text{(moles/sec)C}_2\text{H}_2}{44.6 \text{ sq cm}} \frac{24 \text{ g C}}{\text{mole C}_2\text{H}_2} = 1.72 \times 10^{-6} \text{(g/sq cm)/sec} \]

\[ \text{C loss for CH}_4 + \text{C}_2\text{H}_2 = 0.17 \times 10^{-6} + 1.72 \times 10^{-6} = 1.89 \times 10^{-6} \text{(g/sq cm)/sec} \]

These computed equilibrium losses are plotted against the reciprocal of 2100° K, 4.76 \times 10^{-4} in figure 2.
REFERENCES


"The aeronautical and space activities of the United States shall be conducted so as to contribute . . . to the expansion of human knowledge of phenomena in the atmosphere and space. The Administration shall provide for the widest practicable and appropriate dissemination of information concerning its activities and the results thereof."

—National Aeronautics and Space Act of 1958

NASA SCIENTIFIC AND TECHNICAL PUBLICATIONS

TECHNICAL REPORTS: Scientific and technical information considered important, complete, and a lasting contribution to existing knowledge.

TECHNICAL NOTES: Information less broad in scope but nevertheless of importance as a contribution to existing knowledge.

TECHNICAL MEMORANDUMS: Information receiving limited distribution because of preliminary data, security classification, or other reasons.

CONTRACTOR REPORTS: Technical information generated in connection with a NASA contract or grant and released under NASA auspices.

TECHNICAL TRANSLATIONS: Information published in a foreign language considered to merit NASA distribution in English.

TECHNICAL REPRINTS: Information derived from NASA activities and initially published in the form of journal articles.

SPECIAL PUBLICATIONS: Information derived from or of value to NASA activities but not necessarily reporting the results of individual NASA-programmed scientific efforts. Publications include conference proceedings, monographs, data compilations, handbooks, sourcebooks, and special bibliographies.

Details on the availability of these publications may be obtained from:

SCIENTIFIC AND TECHNICAL INFORMATION DIVISION
NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
Washington, D.C. 20546