



back part of the voltage across  $Q_1$  and  $R_e$  to the base of  $Q_2$ . When  $Q_1$  is saturated, and with normal load current through  $R_e$ ,  $Q_2$  is biased off. The current limit is controllable within 1 mA by variation of  $R_e$ .

As load current through  $R_e$  increases above the selected safe level, the voltage at the base of  $Q_2$  rises, causing  $Q_2$  to turn on; thus  $Q_1$  is turned off, and regeneration then keeps  $Q_2$  on and  $Q_1$  off. By switching of the high resistance of  $R_{C2}$  in the path of the load current, both load and power supply are protected.

The circuit automatically resets to the on state when the supply voltage is dropped to zero and raised again; capacitor  $C_2$  ensures that  $Q_1$  turns on first when voltage is reapplied. By use of two stages and bypass diodes  $D1$ , this circuit limits current for direct current of either polarity or for a non-dc type of supply.

In this particular case, the load of the transformer's primary is considerably inductive; therefore, zeners  $Z_1$  and  $Z_2$  are used to limit inductive spikes that would occur if the circuit limited. The collector-to-emitter breakdown voltage of  $Q_1$  and power rating of  $R_{C2}$  are chosen so that even with a worst-case power-supply failure, resulting in a supply output of 120 V rms (170-V peak), the transformer is not damaged.

The circuit also protects the power supply and eliminates the chance of fire resulting from direct shorting of the outputs; it is capable of limiting continuously more than 120 V rms supplied to a direct short at the output. The switch's limiting speed for this circuit is about 5  $\mu$ sec; therefore it can be used for supply-voltage frequencies from direct current to about 100 kHz. The frequency range could be increased, if desired, by use of high-frequency transistors if the high collector-to-emitter breakdown voltage were not required.

**Note:**

Requests for further information may be directed to:  
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