TECHNICAL INFORMATION SUMMARY

APOLLO-11 (AS-506)

APOLLO SATURN V
SPACE VEHICLE

PREPARED BY:
S&E-ASTR-5
S&E-ASTN-ESD
S&E-AERO-P

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

S&H-ASTR-5-101-69
June 25, 1969
### ABBREVIATIONS AND ACRONYMS

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<td>ac (AC)</td>
<td>Alternating Current</td>
<td>H₂</td>
<td>Hydrogen</td>
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<td>Accel</td>
<td>Accelometer</td>
<td>He</td>
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<td>AM</td>
<td>Amplitude Modulation</td>
<td>HP</td>
<td>High Pressure</td>
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<td>amp</td>
<td>Ampere</td>
<td>HOSC</td>
<td>Huntsville Operations Support Center</td>
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<td>APS</td>
<td>Auxiliary Propulsion System</td>
<td>Hr</td>
<td>Hour</td>
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<tr>
<td>AUTO</td>
<td>Automatic</td>
<td>Hz</td>
<td>Hertz (one cycle per second)</td>
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<td>C.O.</td>
<td>Cutoff</td>
<td>IBM</td>
<td>International Business Machines</td>
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<td>Counterclockwise</td>
<td>IGM</td>
<td>Interactive Guidance Mode</td>
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<td>Command Communication System</td>
<td>in</td>
<td>Inch</td>
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<td>Center Engine Cutoff</td>
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<td>Center of Gravity</td>
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<td>Kennedy Space Center</td>
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<td>Computer Interface Unit</td>
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<td>Direct Current</td>
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<td>Diameter</td>
<td>LOX</td>
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<td>Launch Vehicle Digital Computer</td>
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<td>EBW</td>
<td>exploding Bridgewire</td>
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<td>Maximum dynamic pressure</td>
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<td>Environmental Control Assembly</td>
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<td>EMR</td>
<td>Engine Mixture Ratio</td>
<td>MH₃</td>
<td>Mega Hertz (1 Million Hertz)</td>
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<td>Gal</td>
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<td>GN₂</td>
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<td>Number</td>
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<td>NM (n.m.)</td>
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<td>55</td>
<td>Lunar Surface Communication</td>
<td>91</td>
</tr>
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AS-506

MISSION SUMMARY

This document is prepared jointly by the Marshall Space Flight Center Laboratories S&G-ASTR-S, S&G-AERO-P, and S&G-ASTN-ED. The document presents a brief and concise description of the AS-506 Apollo Saturn Space Vehicle and the AS-506 mission. Where necessary, for clarification, additional related information has been included.

It is not intended that this document completely define the Space Vehicle, its systems or subsystems in detail. The information presented herein by text and sketches, describe launch preparation, ground support activities, and the space vehicle. This information permits the reader to follow the sequence of events beginning a few hours before liftoff to mission completion.

1. Mission Purpose:

AS-506, Apollo 11, Mission G-1, is the first manned Lunar Landing Mission. It uses Launch Vehicle SA-506; Command/Service Module 107, Lunar Module 5; Launch Complex 39A; Mobile Launcher #1 and LCC Firing Room #1.

The purpose is (1) to perform a successful lunar landing (2) assess the capabilities and limitations of the astronauts and their equipment in a lunar surface environment, (3) perform inspection of the lunar surface and obtain soil samples, and (4) to safely return the crew to earth. The crew consists of Neil A. Armstrong, Spacecraft Commander, Edwin E. Aldrin, Lunar Module Pilot, and Michael Collins, Command Module Pilot.

2. Launch Vehicle Objectives:

Demonstrate launch vehicle capability to inject the spacecraft onto a free-return, translunar trajectory.

3. Mission Description:

AS-506, (Apollo 11), has a flight duration of approximately 8 days.

The AS-506 mission profile, illustrated in Figures 2 through 5, consists of the following phases: Launch and boost to earth parking orbit, coast in earth parking orbit, translunar injection, translunar coast, S-IVB "slingshot", lunar orbit insertion, lunar module descent, lunar surface activities, lunar module ascent, transearth injection, transearth coast, reentry, splashdown and recovery.

Launch and Boost to Earth Parking Orbit (EPO). AS-506 will be launched from Kennedy Space Center, Complex 39A on a launch azimuth of 90° East of North. The launch days and the earliest liftoff time, for each day, for the month of July are:

<table>
<thead>
<tr>
<th>Day</th>
<th>Earliest Liftoff Time</th>
<th>Flight Azimuth</th>
</tr>
</thead>
<tbody>
<tr>
<td>July 16</td>
<td>8:32 a.m. CDT</td>
<td>72° - 108°</td>
</tr>
<tr>
<td>July 18</td>
<td>10:30 a.m. CDT</td>
<td>89° - 108°</td>
</tr>
<tr>
<td>July 21</td>
<td>11:09 a.m. CDT</td>
<td>94° - 108°</td>
</tr>
</tbody>
</table>
As the vehicle rises from the launch pad, a yaw maneuver is executed to ensure that the vehicle does not collide with the tower in the event of high winds or a single engine failure. Once tower clearance has been accomplished, a pitch and roll maneuver is initiated to achieve proper flight attitude and a flight azimuth orientation of between 72 and 108 degrees.

A successful boost sequence, as illustrated in Figure 3, will insert the S-IVB/IU/SC into a 100 NMI circular earth parking orbit.

Coast in Earth Parking Orbit (EPO). The vehicle will coast in earth parking orbit while space vehicle subsystems checkout is performed. Preparation for translunar injection takes place during this period. The reignition time and orbital position of the S-IVB injection burn will depend on lunar declination and upon the injection window opportunity to be selected. The first injection opportunity occurs midway through the second parking orbit revolution while the second opportunity occurs midway through the third revolution.

Translunar injection. Following the selection of one of the two injection opportunities described above, the S-IVB stage reignites to provide translunar injection. The nominal injection provides a free return trajectory to earth if the deboost to the lunar parking orbit is not initiated.

Translunar Coast. Shortly after translunar injection, the Transposition, Docking, and Extraction (TD&E) of the Command and Service Module (CSM) and the Lunar Module (LM) will take place. To initiate this maneuver, the CSM, assisted by the service module's reaction control system, will separate from the S-IVB. Spacecraft Lunar-Module Adapter (SLA) panels are then jettisoned to expose the docking mechanism of the lunar module. Following separation, the CSM will translate approximately 50 feet, pitch 180 degrees, roll 60 degrees and move to docking interface with the lunar module. As soon as the crew has completed verification that docking latches are engaged, and that CSM/LM tunnel pressure has been equalized, the LM/SLA attach points are severed and the LM is extracted and moved approximately 100 ft. from the S-IVB. During translunar coast (approximately 75 hours), midcourse corrections are made if required.

S-IVB "slingshot". In order to minimize the probability of spacecraft and launch vehicle collision, and to avert S-IVB earth or lunar impact, a S-IVB "slingshot" procedure is executed. To initiate this maneuver, the launch vehicle (S-IVB/IU/SLA) will move to a predetermined attitude and execute a retrograde dump of residual propellants. This will reduce vehicle velocity by approximately 115 feet per second. Following retrograde propellant dumping, the S-IVB is "safed" by dumping the remaining propellants and gas from gas bottles through the latch-open, nonpropulsive vents. This velocity change in the S-IVB will perturb the S-IVB trajectory so that the vehicle will be influenced by the moon's gravitational field. This influence will increase velocity sufficiently so as to place the S-IVB/IU/SLA in solar orbit.

Lunar Orbit Insertion. Prior to lunar orbit insertion, the crew will check the LM for operational readiness and return to the CSM. If all conditions are "go", the Service Module (SM) propulsion system will be used to deboost the CSM/LM into a moon orbit ranging from 60 to 170 NMI above the moon's surface. Two orbits later, approximately four hours, the astronauts will circularize the orbit at 60 NMI.
Lunar Module Descent. Approximately fourteen hours later, two members of the three man crew, (Armstrong and Aldrin), will enter the LM through the connecting tunnel. Upon completion of a LM checkout, they will undock the LM and begin maneuvers which will take them to the moon's surface. Landing, via the lunar module descent propulsion system, will occur approximately 2-1/2 hours later. (The LM can hover like a helicopter for approximately 60 seconds to select the smoothest landing spot.) While separated, the astronauts will use the radio for communication using Code names "Snowcone" for the Command Module and "Haystack" for the Lunar Module. Present planning calls for lunar touchdown to occur at 3:21 p.m. CDT on July 20, 1969. The third crewman (Collins) will continue to orbit the moon in the CM.

Lunar Surface Activities. Following touchdown, Armstrong and Aldrin are to rest for approximately eight hours, then don their portable life support backpacks and make other necessary preparation to walk the moon's surface. At 1:09 a.m. CDT on July 21, 1969, Armstrong is to climb down a nine-step ladder and become the first man to plant his footstep on the moon's surface. This activity is to be relayed live to television viewers on earth with Aldrin handling the TV camera. Armstrong will stroll alone for about half an hour, gathering a quick sample of lunar soil so that they won't come home empty-handed if they should have to make an early takeoff. Then Aldrin is to join Armstrong on the surface for approximately 2 hours during which they are to gather about 80 pounds of lunar rocks and soil and to set up a scientific experiments package which will transmit lunar data after the astronauts leave.

Lunar Module Ascent. After returning to the LM, the astronauts are to rest for nearly six hours. They will have been on the moon for approximately 21 hours and 30 minutes. The LM ascent stage is used to liftoff from the moon's surface and to fly a 3-hour and 30 minute rendezvous course to catch-up and link-up with the CM. Orbital plane changes, trim burns, or maneuvers required to achieve CSM/LM rendezvous are made with the LM reaction control system. As soon as CSM/LM docking has been accomplished, the two crew members, the lunar soil samples and the exposed film are transferred to the CSM and the LM is secured. Service module RCS is used to separate the CSM from the LM.

Transearth injection and Coast. The SM propulsion system is used to boost the CSM out of lunar orbit. During transearth coast (approximately 64 hours) midcourse corrections are made if required.

Reentry, Splashdown and Recovery. The Command Module is separated from the Service Module prior to atmospheric reentry. The nominal range from reentry (400,000 feet) to splashdown is approximately 2000 miles. Splashdown will take place in the Pacific Ocean approximately 12:00 p.m. CDT July 24, 1969. Immediate recovery of the crew after splashdown has been arranged.

Quarantine Period. Upon recovery, the astronauts will be transferred to a special sealed van on the deck of the carrier for the sea-air-truck trip to the Manned Spacecraft Center in Houston, Texas. There they are to be quarantined with the lunar soil samples in a lunar receiving laboratory for 18 days. Doctors want to be certain they do not bring back any lunar germs.
LUNAR TAKEOFF PHASE

Lunar Orbit
Moon's Orbit
LM rendezvous and docking with CSM
Midcourse Corrections (Multiple restarts as required)
Transit time to Earth ~ 64 hours

LUNAR LANDING PHASE

Lunar Orbit ~ 60 n. mi.
S/C brakes into lunar orbit
Lunar descent
Moon/Earth gravity overcomes each others at ~26000 N M from the moon
S/C translunar trajectory
Transit time to moon ~ 75 hours

Mean Distance to Moon ~ 207,700 N M

JULY PRIMARY LUNAR LANDING SITES

L.O. Date Site Lat. Long.
7-16 2 30°44N 23°59'E
7-18 3 30°22N 1° 21'W
7-21 4 1°46N 41°56'W

*TD & E - Transposition, Docking and (CSM/LM) Ejection

MISSION PROFILE
REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR.

LAUNCH DATA
- Launch Complex 39 Pad A
- Launch Azimuth: 90° E of N
- Flight Azimuth: 72° E of N

ABOVE INFORMATION BASED UPON 72° FLIGHT AZIMUTH AND 3-IVB 2nd IGNITION OCCURRING ON FIRST OPPORTUNITY
Align along local horizontal

**LV CUTOFF INITIATION**

- **S-IC**
  - CECO -- Timer Commanded
  - OECO -- Propellant-depletion sensors backed up by thrust "OK" switches

- **S-II**
  - CECO -- Timer Commanded
  - OECO -- Propellant-depletion sensors backed up by thrust "OK" switches

- **S-IVB**
  - 1st Burn C.D. -- Velocity Cutoff backed-up by crew C.D. on overspeed
  - 2nd Burn C.D. -- Velocity Cutoff backed-up by depletion Sensors

Trajectory Information
Lunar Module

- Crew transfer (2 men)
  from CM to LM
- Pre-descent LM checkout &
  landing site reconnaissance
- Separate LM from CSM &
  turn LM around to descent
  attitude.

Command/Service
Module

CSM continues in Lunar
Parking Orbit (1 man)

LM landing stage ignition & burning
to descent ellipse.

Landing stage propulsion cutoff and coast
via elliptical orbit to near lunar surface.
LM landing stage re-ignition &
breaking out of elliptical orbit

LM hover, translation,
descent maneuvers, &
lunar landing

Lunar Surface Activities
- Assess crew capabilities in
  lunar environment
- Collect lunar soil samples
- LEM inspection
- Photography

Lunar Stay
- Scientific exploration
- Experiments
- Sample gathering

LUNAR LANDING PHASE
Prior to L.M. liftoff, CSM makes plane change to permit nominally coplanar rendezvous.

Main engine firing into circular orbit, engine cutoff and prepare for rendezvous and docking with CSM.

Midcourse correction

Lunar launch stage propulsion cutoff and coast to Lunar orbit

LM Lunar Launch stage ignition & launch

Landing stage is used as a launch platform for the L.M. lunar launch stage. Landing stage remains on the moon.

Experiments Package:
- Laser Reflector
- Seismic Instruments

Rendezvous & Docking
Transfer of crew (2 men) & scientific material from L.M. Lunar Launch stage to CSM.

Jettison L.M. Launch stage & prepare CSM for lunar orbit escape.

LUNAR TAKEOFF PHASE

Lunar Descent And Ascent Phases
Spacecraft is being guided to enter the earth's atmosphere in a corridor 400 mi by 26 mi. If the re-entry angle is too steep, the SC will burn up. If too shallow, the SC will bounce back into space.

CM begins to establish re-entry attitude

CM Earth atmosphere re-entry and aerodynamic maneuver to slow descent. Deceleration force ≈ 4g's.

Jettison fuel compartment heat shield (≈ 90,000 ft.) and then deploy drogue chutes at 20,000 ft. attitude after CM slowed to 200 mph

Main chute deployment (reefed condition)

NOTE: The desired flotation mode after splashdown is with CM Apex Up.

To achieve this mode, the flotation bags are released from the forward hatch causing the module to float upright.

At 10,000 ft. attitude, the main chutes are fully deployed for final descent after CM is slowed to ~140 mph

Each chute 85 ft. dia.

At splashdown, the Apex Up. Main chutes released at splashdown

Water Landing (Splashdown)

Landing site in the Pacific ~ 1000 mi NW of Hawaii

Figure 5
LAUNCH COMPLEX 39

Launch Complex 39 (LC-39), Kennedy Space Center, Florida, provides all the facilities necessary for the assembly, checkout, and launch of the Apollo/Saturn space vehicle. The vehicle assembly building (VAB) provides a controlled environment in which the vehicle is assembled and checked out on a mobile launcher (ML). The space vehicle and the launch structure are then moved as a unit by the crawler-transporter (C-T) to the launch site, where vehicle launch is accomplished after propellant loading and final checkout. The major elements of the launch complex shown in Figure 7, are the vehicle assembly building (VAB), the launch control center (LCC), the mobile launcher (ML), the crawler-transporter (C-T), the crawlerway, the mobile service structure (MSS), and the launch pad.
The Vehicle Assembly Building (VAB) and the Launch Control Center (LCC) are 3 miles from the Launch Pads.

The VAB
- First Floor: Service and Support Area
- Complex Control Center
- Second Floor: Telemetry, RF, and Tracking Equipment
- Third Floor: Firing and Mission Control Rooms
- Mezzanine: Direct Viewing of the Firing Rooms
- Fourth Floor: Launch Information Exchange Facility (LIEF), Display Area

The LCC is 180ft

Each Pad ~ 3000 ft across and 40 ft above sea level

Figure 7

Launch Complex 39
MOBILE LAUNCHER

The Mobile Launcher, figure 8, is a transportable steel structure which provides the capability of moving the erected vehicle to the launch pad via the crawler-transporter. The umbilical tower, permanently erected on the mobile launcher base, is a means of ready access to all important levels of the vehicle during assembly, checkout and servicing prior to launch. The intricate vehicle-co-ground interfaces are established and checked out within the protected environment of the Vertical Assembly Building (VAB) and then moved undisturbed aboard the mobile launcher to the launch pad.

1. S-IC Intertank (preflight). Provides LOX fill and drain. Arm may be reconnected to vehicle from LCC. Retract time 8 seconds. Reconnect time 5 minutes.


3. S-II Aft (preflight). Provides access to vehicle. Retracted prior to liftoff as required.


8. Service Module (inflight). Provides air-conditioning, vent line, coolant, electrical, and pneumatic interfaces. Retract time 5.0 seconds.


Note: Preflight arms are retracted and locked against umbilical tower prior to launch.

Inflight arms retract at vehicle liftoff on command from service arm control switches (located in hold-down arms).
Umbilical Tower
- Open Steel Structure
- Height: 380 ft
- Two high-speed elevators service 18 landings, from level "A" of the base to the 340 ft tower level
- Provides support for eight umbilical service arms, one access arm, 18 work and access platforms, distribution equipment for the propellant, pneumatic, electrical and instrumentation subsystems, and other ground support equipment.

Hammerhead Crane
- Launch position 90° CW from that shown below
- Load capacity 10 to 25 tons depending on extension of boom
- Can rotate 360° at 1 rpm

Attached at 320 ft level (443 ft above ground)

Slide Wire Escape System (Capacity: 11 persons)

Ground Terminal Point 2500 ft west of pad

Engine Holddown Arm Tail Service Mast Orientation
- 45A & 45B opening
- Tower Service Mast
- Engine #1, #2
- Holding Arm (4)
- Tail Service Mast

Launcher Base
- Two-story steel structure
- Height: 255 ft
- Length: 160 ft
- Width: 135 ft
- Level "A" has 21 rooms
- Level "B" has 22 rooms

Launcher-in-ground mount mechanisms (6)

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Figure 8

Mobile Lai Chor
GROUND SUPPORT EQUIPMENT

A computer controlled automatic checkout system is used to accomplish checkout or testing of the launch vehicle when in the Vertical Assembly Building (VAB) highbay and on the launch pad.

An RCA 110A Computer and other equipment necessary for service and checkout are installed with the vehicle on the mobile launcher. Similar equipment, joined by an integration system (relay network), a facilities cable tunnel and video cables for visual display are located in the Launch Control Center (LCC).

A Digital Data Acquisition System (DDAS) collects vehicle and support equipment responses to test commands and formulates test data for transmission, decommutation, and display to the LCC or ML.

Digital Events Evaluators (DEE) monitor the status of input lines and generate a time labeled printout for each detected change in input status. High speed printers in the LCC are connected to each DEE to provide a means for real time or post-test evaluation of discrete data.

The propellant tanking computer system (PTCS) determines and controls the quantities of fuel and oxidizer on board each stage. Optimum propellant levels are maintained and LOX and LH₂ are replenished as boiloff occurs during the countdown. The propellant tanking operation is monitored on the PTCS control panel.

Final countdown begins at T-102 hours. A countdown clock, located in the LCC, officially records this countdown.
Liftoff

△ Disconnect IC Umbilical

△ Multiple Engine Cutoff Enable ~ 0min 14 sec

△ EDS Engine Cutoff Enable ~ 0min 30 sec

△ Automatic Abort Capability Disable ~ 2min 14 sec

△ 5-1C Inboard Engine Cutoff ~ 2min 15 sec

△ 5-1C Outboard Engines Cutoff ~ 2min 41 sec

△ 5-11 Ullage Ignition ~ 2min 41 sec

△ 5-1C/5-11 Separation ~ 2min 41 sec

△ 5-11 Engine Start ~ 2min 41 sec

△ Water Coolant Valve Opens ~ 3min 00 sec

△ 5-11 Second Plane Separation ~ 3min 11 sec

△ 5-11 LOX Step Pressurization ~ 3min 21 sec

NOTE:
Approximate times shown are measured from liftoff

Start of Time Base 1

Start of Time Base 2

Start of Time Base 3

Figure 10

3-1C/5-11 Stage Flight Sequencing
△ S-11 Inboard Engine Cutoff ~ 7min 40sec

△ S-11 LH₂ Step Pressurization ~ 7min 41sec

△ S-11 LOX & LH₂ Depletion Sensors Enable ~ 8min 17sec

△ S-11 Outboard Engines Cutoff ~ 9min 11sec

△ S-1V6 Ullage Engine On ~ 9min 12sec

△ S-11/S-1V6 Stage Separation ~ 9min 12sec

△ S-1V6 Engine Ignition ~ 9min 15sec

△ S-1V6 Engine Velocity Cutoff ~ 11min 30sec

△ S-1V6 Ullage Engine On ~ 11min 39sec

△ S-1V6 Insertion Into Earth Parking Orbit ~ 11min 35sec

△ SIC Control Enable ~ 11min 36sec

△ S-1V6 Ullage Engine Off ~ 13min 07sec

NOTE:
Approximate times shown are measured from liftoff.
**Begin S-IVB Stage Restart Preparations ~ 2 hr 34 min**

△ SIC Control Disable ~ 2 hr 35 min

△ O₂/H₂ Burner On ~ 2 hr 35 min

△ LOX & LH₂ Chilldown Pump On ~ 2 hr 38 min

△ S-IVB Ullage On ~ 2 hr 42 min

△ O₂/H₂ Burner Off ~ 2 hr 42 min

△ LOX & LH₂ Chilldown Pump Off ~ 2 hr 44 min

△ S-IVB Ullage Off ~ 2 hr 44 min

**S-IV Stage Engine Restart ~ 2 hr 44 min**

**NOTE:**

Approximate times shown are measured from lift-off.

* If restart is delayed until the second injection opportunity this and major subsequent events will occur approximately one hour and twelve minutes later than shown.

**Inhibited for first opportunity restart**

**S-IVB LOX & LH₂ Point Level Sensor Enable ~ 2 hr 49 min**

**S-IVB Stage Engine 2nd Cutoff ~ 2 hr 50 min**

**S-IVB LOX & LH₂ Point Level Sensor Disarm ~ 2 hr 50 min**

△ LH₂ Vent Valve Open ~ 2 hr 50 min

△ SIC Control Enable ~ 2 hr 50 min

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**Figure 12**

FIVB Stage Flight Sequencing
\[ \Delta \text{LH}_2 \text{ Vent Valve Close} \sim 3 \text{ hr 05 min} \]

\[ \Delta \text{ IU Command System Enable} \sim 3 \text{ hr 10 min} \]

\[ \Delta \text{5-1VB/CSM Separation} \sim 3 \text{ hr 10 min} \]

\[ \Delta \text{LH}_2 \text{ Tank Latching Relief Valve Open On} \sim 3 \text{ hr 50 min} \]

\[ \Delta \text{LH}_2 \text{ Tank Latching Relief Valve Open Off} \sim 4 \text{ hr 05 min} \]

\[ \Delta \text{Commence 5-1VB Trans: Liner Safing} \sim 4 \text{ hr 50 min} \]

\[ \Delta \text{Passivation Enable} \sim 5 \text{ hr 02 min} \]

\[ \Delta \text{Engine He Control Valve Open On} \sim 5 \text{ hr 02 min} \]

\[ \Delta \text{Engine He Control Valve Open Off} \sim 5 \text{ hr 04 min} \]

\[ \Delta \text{Passivation Disable} \sim 5 \text{ hr 29 min} \]

\[ \Delta \text{5-1VB Ullage Engines No.1 & No.2 On} \sim 5 \text{ hr 30 min} \]

\[ \Delta \text{5-1VB Ullage Engines No.1 & No.2 Off} \sim 5 \text{ hr 41 min} \]

**NOTE:**

Approximate times shown are measured from start.
1. Time Base 6 Inhibit
2. Translunar Injection Inhibit (S/C switch)
   Prior to Time Base 6
3. Translunar Injection Inhibit (S/C switch)
   During Time Base 6
4. Inhibit Removed by Ground Command
   After Time Base 7 + 2 Hours

**Nominal Mission**

NOTE: In order to provide for D/E in Earth Orbit, a Ground Command will inhibit the initiation of time Base 6 and Time Base 5 will continue to the EOM

Figure 14

Alternate Time Base Sequencing
GUIDANCE AND CONTROL SYSTEM (G&C)

Function and Description

The G&C system provides the following basic functions during flight:

1. Stable positioning of the vehicle to the commanded position with a minimum amount of sloshing and bending.

2. A first stage tilt attitude program which gives a near zero lift trajectory through the atmosphere.

3. Steering commands during S-II and S-IVB burns which guide the vehicle to a predetermined set of end conditions while maintaining a minimum propellant trajectory for earth orbit insertion.

4. The proper vehicle position during earth orbit.

5. Guidance during the second S-IVB burn, placing the vehicle in the proper waiting orbit.

G&C Hardware

The Stabilized Platform (ST-124H) is a three gimbal configuration with gas bearing gyros and accelerometers mounted on the stable element. Gimbal angles are measured by redundant resolvers and inertial velocity is obtained from integrating accelerometers.

The Launch Vehicle Data Adapter (LVDA) is an input-output device for the Launch Vehicle Digital Computer (LVDC). The LVDA/LVDC components are digital devices which operate in conjunction to carry out the flight program. The flight program performs the following functions: (1) processes the inputs from the ST-124H, (2) performs navigation calculations, (3) provides the first stage tilt program, (4) calculates IGM steering commands, (5) calculates attitude errors, (6) issues launch vehicle sequencing signals.

The Control/Eds Rate Gyro Package contains nine rate gyros (triple redundant in three axes). Their outputs go the Control Signal Processor (CSP) where they are voted and sent to the Flight Control Computer (FCC) for damping vehicle angular motion.

The FCC is an analog device which receives attitude error signals from the LVDA/LVDC and vehicle angular rate signals from the CSP. These signals are filtered and scaled, then sent as commands to the S-1C, S-II, and S-IVB engine actuators and to the Auxiliary Propulsion System (APS) Control Relay Packages. The Control Relay Packages accept FCC commands and relay these commands to operate propellant valves in the APS. During spacecraft control of the launch vehicle, the FCC receives attitude error signals from the Command Module Computer or the Astronaut hand controller.

The Switch Selectors in each stage are used to control the inflight sequencing as commanded from the LVDA/LVDC.
The Launch Vehicle Flight Control Computer will accept attitude commands from the spacecraft instead of the LVDC during (1) boost to Earth Parking Orbit (EPO); (2) orbital coast mode; (3) Translunar Injection (TLI) burn; and (4) the post TLI coast mode, with the following constraints:

**During Burn Modes**

The Spacecraft attitude commands will be accepted by the flight control computer only in the event that the LVDA signals that the LV ST-124M Platform has failed followed by the Astronaut enabling the LV Guidance Switch. If the ST-124M Platform should fail before Time Base 5 (TB6) initiation, a navigation update by ground command will be required to start TB6 (S-IVB preps. and second burn). There are two modes to the backup system operations and they are:

1. **Automatic Backup Guidance and Control**

   In the automatic guidance mode both the control and guidance functions will be provided by the Spacecraft. This backup mode is used during S-IC stage flight and S-II flight up to LET jettison. The sequence of events are as follows:
   
   a. Failure of ST-124M is verified by LVDA.
   b. LVDA illuminates warning light in S/C.
   c. Astronaut enables LV Guidance switch.
   d. S/C transmits error signals to LV flight control computer.

2. **Manual Backup Guidance and Control**

   In the manual guidance mode both guidance and control loops will be closed through the Astronauts. An Astronaut continuously adjusts vehicle attitude via the Rotation hand Controller to maintain the desired trajectory. Sequence of events following a Platform failure after LET jettison are:
   
   a. Failure of ST-124M verified by LVDA.
   b. LVDA illuminates warning light in S/C.
   c. Astronaut enables LV Guidance Switch.
   d. Manual guidance and control is initiated by the Astronaut entering a word into the S/C computer to switch AUTO/ MANUAL switches to MANUAL.
   e. If automatic backup guidance is in operation at LET jettison, switching to manual backup is accomplished by performing step (d).

**During Orbital and Post TLI Coast Modes**

In earth orbit and post TLI coast modes the Astronauts have a manual attitude control capability. The takeover follows somewhat the procedure for Manual Backup Guidance and Control takeover.
EMERGENCY DETECTION SYSTEM

The Emergency Detection System (EDS) is designed to sense and react to emergency situations resulting from launch vehicle malfunctions which may arise during the mission. Crew safety and protection is the primary function of the EDS. Triple redundant sensors and majority voting logic are used in the automatic abort system. Dual redundancy is used for most of the manual abort sensors. The redundancy in the sensing systems is designed to protect against inadvertent aborts.

Automatic Aborts - During most of the S-IC flight, the EDS provides the capability of automatically aborting the mission. The automatic abort system is enabled at liftoff and disabled by the crew at approximately 2 minutes or by the IU switch selector prior to S-IC inboard engine cutoff. The system responds to failure modes that lead to rapid vehicle breakup. The parameters and the associated limits monitored for an automatic abort are:

1. Simultaneous loss of thrust on two or more S-IC engines
2. Vehicle rates in excess of ±4°/sec in pitch or yaw; or ±20°/sec in roll
3. S/C to IU breakup.

Manual Aborts - After the automatic abort mode is disabled, aborts may be initiated manually by the astronauts. Manual aborts are initiated based on at least two separate and distinct indications. The indications may be a combination of EDS sensor displays, physiological indications, and ground information to the astronauts. EDS displays for the crew consist of light and meters which indicate loss of thrust of each engine, staging sequences, launch vehicle attitude reference failure, angle of attack, tank ullage pressures, spacecraft attitude error and angular rates. The manual abort overrate limits are:

1. Pitch and Yaw - L.O. to S-IC/S-II Staging - ± 10°/sec
   - S-IC/S-II Staging to S-IVB C.O. - ±9°/sec
2. Roll - L.O. to S-IVB C.O. - ±20°/sec

Aborts occurring during the launch phase will be performed by using either the Launch Escape System (LES) or the Service Propulsion System (SPS). The LES is used to propel the CM a safe distance from the launch vehicle and to ensure a water landing. Aborts prior to 30 seconds of flight do not terminate S-IC thrust in order to protect the launch area. The SPS aborts utilize the Service Module SPS engine to propel the CSM away from the launch vehicle, and to maneuver to a planned landing area or boost into a contingency orbit.
During the first 30 seconds of flight, if an AUTO or MANUAL abort is initiated, C.O. of the S-IC engines will not occur until 7-30 seconds, except if the Range Safety Officer gives emergency C.O.
LAUNCH VEHICLE SECURE RANGE SAFETY SYSTEMS

The Secure Range Safety Systems, located on the S-IC, S-II and S-IVB stages, provide a means to terminate the flight of an erratic vehicle by the transmission of coded commands from ground stations to the vehicle during launch phase. The Range Safety Officer (RSO) terminates the flight of an erratic vehicle (trajectory deviations) by initiating the emergency engine cutoff command and, if necessary, the propellant dispersion command.

The command destruct system in each stage is completely separate and independent of those in the other stages with the exception of a 2 for 3 voting arrangement between the S-IC and S-II Range Safety System Controllers. This arrangement eliminates a single point failure in the S-IC range safety system controller, which, if it failed would cause an unnecessary S-IC engine cutoff.

The system in each powered stage consists of a range safety antenna subsystem, two secure command receivers, two Range Safety Controllers, two Secure Range Safety Decoders, two Exploding Bridge Wire (EBW) firing units, two EBW detonators and a common safe and arm device which connects the subsystem to the tank cutting charge. Electrical power for all elements appearing in duplicate is supplied from separate stage batteries.

Prior to launch, the safe and arm device is set to the "ARM" position by ground support equipment and the system remains active until orbital insertion. After orbital insertion, the S-IVB stage range safety receiver is deactivated (Safed) by ground command from the Range Safety Officer.
MEASUREMENT SYSTEM

The vehicle measurement systems sense performance parameters and feeds signals to the stage and spacecraft telemetry systems. It includes transducers, signal conditioning, and distribution equipment necessary to provide the required measurement ranges and suitably scaled voltage signals to the inputs of the telemetry systems. The vehicle measuring systems performs three main functions:

1. Detection of the physical phenomena to be measured and transformation of these phenomena into electrical signals.

2. Process and condition the measured signals into the proper form for telemetering.

3. Distribution of the data to the proper channel of the vehicle's telemetry systems.

The table on the opposite page contains a measurement breakdown for the launch vehicle and spacecraft, and a measurement summary of past Saturn V flights.
AS-506
Launch Vehicle
Measurement Summary

** Included in Launch Vehicle Totals

<table>
<thead>
<tr>
<th>Measurement Designation</th>
<th>S-IC</th>
<th>S-II</th>
<th>S-IVB</th>
<th>IU</th>
<th>L/V Totals</th>
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<td>12</td>
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<tr>
<td>AS-504</td>
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<td>AS-505</td>
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</table>

* LM measurements added to AS-504 & 505

Note: All measurement numbers approximate
COMMAND AND COMMUNICATION INTERFACES FOR MISSION CONTROL

Mission Control Center (MCC) Manned Spacecraft Center, Houston, Texas. Contains communication, computers, display and command systems to monitor and control the space vehicle.

Kennedy Space Center, Florida (KSC). The space vehicle is assembled, checked-out, and launched from KSC. Central Instrumentation Facility (CIF) collects powered flight data and data received from Merritt Island Launch Area (MILA) and Air Force Eastern Test Range (AFETR).

Goddard Space Flight Center (GSFC). Greenbelt, Maryland operates the Manned Space Flight Network (MSFC) and NASA communications network. The MSFC is under control of MCC during flight.

George C. Marshall Space Flight Center (MSFC) Huntsville, Alabama. Using The Huntsville Operations Support Center (HOSC) and the Launch I Formation Exchange Facility (LIEF), real-time support is provided to KSC and MCC for preflight, launch and flight operations.

The Manned Space Flight Network is a global network of ground stations, ships, and aircraft designed to support manned and unmanned space flight.

While selected ground stations throughout the world monitors all phases of flight activity from liftoff to recovery, pre-destined ships and aircraft are strategically situated to monitor "Insertion to Earth Parking Orbit", "Translunar Injection", "Reentry and Recovery".
**VEHICLE TRACKING SYSTEMS**

In the Saturn V space vehicle there is a continuous requirement to transmit information to ground stations in order to determine the vehicle’s trajectory. This requirement is satisfied by the RF tracking systems. The tracking data is used by mission control, range safety, and for post-flight evaluation of the vehicle’s performance. The tracking systems used are:

**C-Band (IU and S/C)**

C-Band is a pulse radar system which is used for precise tracking during powered flight into earth orbit, orbital flight, injection into trans-lunar trajectory, and coast flight after injection.

**S-Band (IU and S/C)**

The Unified Side Band (USB) System provides tracking capability to the USB ground stations and these stations track the spacecraft to the moon.
Mainstage propellant consumption during S-IC powered flight (approximately 161 seconds) is approximately 4,670,300 pounds. Propellant consumption during S-II powered flight (approximately 389 seconds) is approximately 971,450 pounds. During S-IVB powered flight, including first and second burns, (approximately 461 seconds) the propellant consumption is approximately 223,900 pounds.

<table>
<thead>
<tr>
<th>Vehicle Weight Data (Approximate)</th>
<th>Pounds</th>
</tr>
</thead>
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<tr>
<td>Total at S-IC ignition</td>
<td>6,484,300</td>
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<tr>
<td>Total at liftoff</td>
<td>6,398,500</td>
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<tr>
<td>Total at S-IC OECO</td>
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<tr>
<td>Total at S-II ignition</td>
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<tr>
<td>Total at S-II OECO</td>
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<tr>
<td>Total at S-IVB 1st ignition</td>
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<tr>
<td>Total at S-IVB 1st ECO</td>
<td>297,500</td>
</tr>
<tr>
<td>Total at S-IVB engine restart</td>
<td>294,600</td>
</tr>
<tr>
<td>Total at S-IVB 2nd ECO</td>
<td>133,600</td>
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<tr>
<td>Total at S-IVB/CSM separation</td>
<td>120,900</td>
</tr>
<tr>
<td>Total at SC translunar injection</td>
<td>100,800</td>
</tr>
</tbody>
</table>
The 343,600 gallon capacity LOX tank is the structural link between the forward and intertank sections. Stiffened by machined "T" stiffeners the tank is internally equipped with ring baffles for additional stability as well as to reduce LOX sloshing and to provide support for four helium bottles.

The Intertank Section

The intertank section provides structural continuity between the S-IC and RP-1 tanks.

The RP-1 (Fuel) Tank

The RP-1 fuel tank, located between the thrust structure and the intertank section, is a cylindrical aluminum structure with a capacity of 218,900 gallons. Antislosh ring baffles are located on the inner wall while cruciform baffles are located on the lower bulkhead. A lightweight foam material, bonded to the lower bulkhead, serves as an exclusive riser to minimize unusable residual fuel.

The Thrust Structure

The thrust structure provides support for the five engines, the base heat shield, engine fairings and fins, propellant lines, retro rockets and environmental control ducts. The lower thrust ring also has four-holddown points to restrain the vehicle, as necessary, from lifting off at full F-1 engine thrust.

Pogo Suppression

The longitudinal oscillation in the LV, or "Pogo" effect as it has been called, has been suppressed by utilizing the LOX prevalve cavities in the four outboard engines as surge chambers. Each of the four cavities is pressurized with gaseous helium (GH) at T -1 minutes from ground supply. Initial fill is closely monitored using liquid level resistance thermometers. Ground fill maintains cavity pressure until umbilical disconnect after which pressure is maintained by the cold helium spheres in the LOX tank. Pressure readings are transmitted via telemetry to ground monitors during flight.
Stage Weight
- Dry: ~ 268,700 lbs
- At Ignition: ~ 5,028,000 lbs
- At Separation: ~ 363,430 lbs

Figure 22

'5-1C Stage Configuration
F-1 Engine Operation

The F-1 engine is started by ground support equipment. Ground fluid pressure ports in the main LOX valves. Opening of the main LOX valves admits oxidizer tank pressure to the thrust chamber and allows control fluid to enter the gas generator. Opening of the gas generator valve permits LOX and RP-1 to enter the gas generator combustion chamber where they are ignited by the turbine exhaust igniters. While the RP-1 reaches approximately 375 psig a valve in the hypergol cartridge opens allowing LOX and RP-1 to build up pressure against the hypergol burst diaphragm. At approximately 500 psig the diaphragm ruptures allowing hypergol and RP-1 to enter the thrust chamber causing spontaneous combustion upon contact with the LOX, thereby establishing primary ignition. As thrust pressure builds up the RP-1 valves open admitting RP-1 to the thrust chamber and the transition to mainstage operation is achieved.

The inboard engine engine is cutoff by a signal from the IU. Outboard engines are cutoff by optical type LOX depletion sensors with fuel depletion sensors as back-up. A command from the IU supplies a command to the switch selector to enable the outboard engine cutoff circuitry. When two or more of the four LOX level sensors are energized, a timer is activated. Expiration of the timer energizes a stop solenoid for each engine which energizes the main LOX and main RP-1 valves. The sequence closing of the main LOX valve followed by sequence closing of the main RP-1 valve interrupts propellant flow and terminates engine operation.

Engine Control Valve "Open" Signal
Oxidizer Valves Open
Gas Generator Valve Open
Gas Generator Propellant Ignition
Igniter Fuel Valve Open
Hypergol Cartridge Rupture
Thrust Chamber Ignition
Fuel Valves Open
Start of Thrust Increase
"Thrust OK" Signal
90 Percent Engine Thrust
Start Sequence Complete

Engine Start Sequence in Seconds from Control Valve "Open" Signal
The turbopump is a combined LOX and fuel pump driven through a common shaft by a single gas turbine.

A four-way control valve directs hydraulic fluid to open and close the fuel, LOX, and gas generator valves.

A mixture ratio of LOX:RP-1 2.27:1.

The engine is started by ground support equipment (GSE) and is capable of only one start before repurvising.

The main fuel and LOX valves are fast-acting, pressure balanced, poppet type, hydraulically operated valves.

The main fuel and LOX valves are fast-acting, pressure balanced, poppet type, hydraulically operated valves.

Thrust Chamber (Pressure Inlet and Exit)
The S-IC stage propellant system is composed of one LOX tank, one RP-1 tank, propellant lines, control valves, vents, and pressurization subsystems. Loading of LOX and RP-1 tanks is controlled by ground computers. RP-1 loading is completed approximately nine days prior to liftoff. LOX bubbling is started at the beginning of LOX chilldown operation and is continued throughout LOX loading and again before liftoff to prevent possible pyrolyzing. Prior to liftoff the RP-1 tank and the LOX tank is pressurized by helium from a good source. At liftoff the RP-1 tank is pressurized with helium stored in bottles located in the LOX tank and heated by passing the helium through the heat exchanger. LOX tank pressurization is maintained by LOX bled from the engine and converted to GOX in the heat exchanger.
LOX Tiltage Pressure Sensor Line

Pressurization Valves (5)
Open - 26.5 psia
Close - 242 psia

LOX Fill & Drain Valve (2)
with Heaters

Vent & Relief Valve
Vent 30.5 psia
Relief 35.0 psia

Pressure Vent & Relief Switch
Activate 21.6 psia
Deactivate 29.1 psia

G-1 Engine (5)

Total Propellant at Ignition
- 4,738,900 lbs
Total Propellant consumed after Ignition
- 4,670,300 lbs

Figure 24

3-IC Propellant System
S-IC STAGE THRUST VECTOR CONTROL SYSTEM

The four outboard F-1 engines are gimbal mounted on the stage thrust structure to provide attitude control during S-IC stage powered flight. Each independent gimbal system employs two hydraulic servo actuators. These servo actuators convert electrical command signals (from IU Flight Control Computer) and hydraulic pressure into mechanical outputs which gimbal the outboard engines on the S-IC stage. An integral mechanical feedback, varied by piston position, modifies the effect of the control signal from the FCC. Built-in servo actuator potentiometers sense servo actuator positions for telemetry as well as providing an interlock to preclude liftoff with an engine hardover.

Hydraulic pressure is supplied to the Thrust Vector Control System from a GSE pressure source during prelaunch checkout and engine start. The GSE pressure source utilizes RP-1 ramjet fuel as the hydraulic fluid. During engine operation, hydraulic pressure is supplied from the fuel discharge of the engine turbo pump to the servo actuators. The fuel returns through a check valve to the fuel inlet of the turbo pump. RP-1, the fuel used by the S-IC stage, is used as the hydraulic fluid during engine operation.
NOTE:
Check valves in the Filter Manifold block the flow of fluid from the Filter Manifold to the engine, when operating on ground supply and to the ground supply inlet when on flight supply.

Actuators (2 per engine)

Vehicle Yaw Axis

Eng#2
Eng#3

Outboard Engines (4) Gimballed

Eng#4

Eng#1

Vehicle Pitch Axis

Gimballed Point

IV

Square Gimbal Pattern ± 5.1° Engine Gimbal rate under load 5° per sec.

Inboard Engine (1) Fixed Position, Canted 0°

S-1C Thrust Vector Control System

Figure 25

47
Figure 26
- **PCM/DDAS**: Provides data acquisition link for analog and digital data plus a redundant means for monitoring the PAM link.

- **FM-RF Assembly**
  - Link AF-1 (256.2 MHz)
  - Link AP-1 (244.3 MHz)

- **PAM/FM/FM Assembly (telemetry oscillator)**
  - Mod. 270
  - MUX.

- **Calibration Command (from Switch Selector)**

- **PCM/DDAS Assembly (model 301)**

- **RF Power Divider**

- **Coax Switch**
  - To GSE

- **Antennae**

- **Transmitter**

- **TM Calibrator**

- **Mod. 270 Multiplexer**

- **Measuring Distributors**

- **Low level Analog data**

- **Thrust Frame Area**

- **Forward Shift Area**

- **PAM/FM/FM**: Pulse Amplitude Modulation/Frequency Modulation/Freq. Mod.

- **PCM/DDAS**: Pulse Code Modulation/Digital Data Acquisition System

---

**Figure 27**

**S-IC Telemetry System**
S-II Stage Structure

The S-II stage is a large cylindrical booster approximately 81 feet in length and 33 feet in diameter. The stage is powered by five liquid-propelled J-2 rocket engines which combine to develop a total thrust of 1,150,000 pounds.

Forward Skirt

The forward skirt, a part of the S-II body shell structure, is a cylindrical aluminum alloy material, strengthened and supported internally and externally by stringers and circumferential ring frames. The forward skirt also houses the telemetry and command (range safety) antenna.

The Fuel (LH₂) Tank

The LH₂ tank is a long cylinder with a concave bulkhead forward and a convex bulkhead aft. The tank structure is made up of six cylindrical sections which incorporate stiffening members in both the longitudinal and circumferential directions.

The Common Bulkhead

This is an adhesive-bonded assembly of aluminum alloy and fiberglass/phenolic honeycomb core to prevent heat transfer and retain the cryogenic properties of the fluids to which it is exposed (LOX and LH₂). Fiberglass core material varies in thickness between .080 inches to 5 inches. No connections or lines pass through the common bulkhead.

The LOX Tank

The LOX tank consists of ellipsoidal fore and aft halves with reinforced gore segments. Three ring type slosh baffles control propellant sloshing and minimize surface disturbances. A six part sump assembly at the lowest point provides fill and drain openings for the five engine feed lines.

Aft Interstage

The aft interstage, also part of the body shell structure, is made up of aluminum alloy material and is supported internally by hat stringers and circumferential ring frames. The aft interstage has four ullage rockets mounted in its outer surface.

System Tunnel

The systems tunnel houses electrical cables, pressurization lines and the propellant dispersion ordnance. The tunnel is attached externally from the S-II stage aft skirt to the forward skirt.
Figure 28

S-11 Stage Weights
* Dry: 75,800 lbs.
* At S-11 ignition: 103,900 lbs
* At S-11 cutoff: 94,500 lbs
* At S-11 separation: 94,100 lbs
J-2 ENGINE OPERATION S-II STAGE

The operating cycle of the J-2 Engine consists of prestart, start, steady-state operation and cutoff sequences. During prestart, LOX and LH₂ flow through the engine to temperature-condition the engine components, and to assure the presence of propellant in the turbopumps for starting. Following a timed cooldown period, the start signal is received by the sequence controller which energizes various control solenoid valves to open the propellant valves in the proper sequence. The sequence controller also energizes spark plugs in the gas generator and thrust chamber to ignite the propellant. In addition, the sequence controller releases GH₂ from the start tank. The GH₂ provides the initial drive for the turbopumps that deliver propellant to the gas generator and the engine. The propellant ignites, gas generator output accelerates the turbopumps, and engine thrust increases to main stage operation. At this time, the spark plugs are de-energized and the engine is in steady-state operation.

Steady-state operation is maintained until a cutoff signal is received by the sequence controller. The sequence controller de-energizes the solenoid valves which in turn close the engine propellant valves in the proper sequence. As a result, engine thrust decays and the cutoff sequence is complete.

Engine Start
Main Fuel Valve Open
Main Fuel Propellant Flow
Start Tank Discharge Valve Open
Pump Buildup
Bypass Flow Through Oxidizer Turbine Bypass Valve
Main Oxidizer Flow
Gas Generator Propellant Flow
Main Oxidizer Valve Open
Mainstage OK Signal
90 Percent Thrust

IGNITION COMMAND
TIME FROM IGNITION

SEC SEC SEC SEC SEC SEC
Each turbine is independently driven through direct drive. Both turbines are powered in series by a single gas generator.

Mixture Ratio
LOX: LH₂ 5.5-4.5:1

All components shown above are located on the engine.

Figure 29

LOX Pump

LOX Valve

Main LOX Valve

Gas Gen

LH₂ Pump

LH₂ Valve

Heat Exchanger

Throat Chamber (Pressure 7770 psia at 50°F)

Expansion Ratio 27.5:1

~ 200,000 lbs thrust

LOX Turbine

LH₂ Turbine

Injector

LH₂ Tank Pressurization

Vent LH₂ turbine exhaust gas through engine bell during J-2 Engine Start

Propellant Utilization (PU) Valve varies engine mixture ratio by bypassing LOX from the pump.

Each of the 5 S-II J-2 engines is a high performance, high altitude engine utilizing liquid oxygen and liquid hydrogen as propellants and is capable of a single start.
S-II STAGE PROPELLANT SYSTEM

The S-II Stage propellant system is composed of integral LOX/LH₂ tanks, propellant lines, control valves, vents, and prepressurization subsystems. Loading of propellant tanks and flow of propellants is controlled by the propellant utilization systems. The LOX/LH₂ tanks are prepressurized by ground source gaseous helium. During powered flight of S-II Stage, the LOX tank is pressurized by GOX bled from the LOX heat exchanger. The LH₂ tank is pressurized by GH₂ bled from the thrust chamber hydrogen injector manifold: pressurization is maintained by the LH₂ Pressure Regulator.

S-II PROPELLANT LOAD AND OPERATIONAL SEQUENCE
Above LOX and LH₂ lines typical for each engine.

Total propellant at ignition
~979,250 lbs.
Total propellant consumed after ignition ~97,050 lbs.

Figure 30

5-11 Propellant System
S-II STAGE THRUST VECTOR CONTROL SYSTEM

The four outboard J-2 engines are gimbal mounted to provide thrust vector control during powered flight. Attitude control is maintained by gimballing the outboard engines in response to electrical control signals from the IUI flight control computer.

The system consists of four independent closed-loop hydraulic control subsystems which provide power for engine gimballing. The primary components of the subsystem are an auxiliary pump, a main pump, an accumulator/reservoir manifold assembly and two servo actuators. The auxiliary pump is electrically driven from the GSE to provide hydraulic fluid circulation prior to launch. The main pump is mounted to and driven by the engine LOX turbopump. The accumulator/reservoir manifold assembly consists of a high pressure accumulator which receives high pressure fluid from the pump and a low pressure reservoir which receives return fluid from the servo actuators. The servo actuator is a power control unit that converts electrical signals and hydraulic power into mechanical outputs that gimbal the engine.

During the pre-launch period, the auxiliary hydraulic pump circulates the hydraulic fluid to preclude fluid freezing during propellant loading. Circulation is not required during the S-IC burn due to the short duration burn. After S-IC/S-II separation, an S-II switch selector command unlocks the accumulator lock up valves, releasing high pressure fluid to each of the servo actuators. The accumulators provide gimballing power prior to the main hydraulic pump operation. During S-II mainstage operation, the main hydraulic pump supplies high pressure fluid to the servo actuators. The return fluid from the actuators is routed to the reservoir which stores hydraulic fluid at sufficient pressure to supply a positive pressure at the main pump inlet.
Inflight use - Driven by Engine Turbo Pump at 8000RPM output 8.0gpm at 3000psig

Main Pump

Reservoir ~80psig

Accumulator ~3500psig

Hydraulic Servo Actuators (2)

Servo Valve

I/U

Electrical Commands

Engine Actuator Attachment

Gimbal Point

 Typical for each engine

 Accumulator pressurized from ground with CAFE at 2350±50 psig at 10°F

Motor

Electric Motor driven at 13,000 rpm
Output 1.5gpm at 3500psig

Auxiliary Pump

NOTE: Auxiliary pump used only during prelaunch checkout

Actuators (2 per engine)

Vehicle Yaw Axis

Vehicle Roll Axis

Vehicle Pitch Axis

Eng#1

Eng#2

Eng#3

Eng#4

Eng#5

Vehicle, Yaw Axis

Outboard Engines (4)

Gimballed

Canted 0° at Nominal Thrust

Square Gimbal Pattern ±1°

Engine Gimbal Rate

Under Load 9.6° per sec.

Inboard Engine (1)

Fixed Position

Gimbal Point

+Pitch

CC

+Yaw

+Roll

S-11 Thrust Vector Control System

Figure 31
S-II STAGE PROPELLANT MANAGEMENT SYSTEM

The propellant management system provides a means for controlling and monitoring propellants during ground loading, powered flight and engine shutdown.

Continuous capacitance probes and point level sensors in the LH₂ and LOX tanks monitor propellant mass. During the propellant loading sequence, a signal from each capacitance probe is transmitted from the on board propellant electronics to GSE to indicate the level of propellants in the tanks. Overfill point level sensors are provided for both the LH₂ and LOX systems. When the propellant mass in the tanks reach a predetermined amount, the GSE loading computer automatically stop the loading sequence.

The propellant utilization (PU) subsystem controls the mixture ratio (MR) of the LOX/LH₂. The PU subsystem consists of a rotary valve, to control the amount of LOX flowing to the engine, and electrical controls for the valve. At engine start, the PU valve is in a neutral position and supplies a MR of 5:0:1. Approximately 5 seconds after engine start, electrical signals from the LVDC in the IU commands the PU valve to supply a nominal MR of 5:3:1. Five minutes and 20 seconds after engine start the LVDC commands the PU valve to a MR of 4:5:1 for the remainder of the S-II Stage burn. Capacitance probes in the propellant tanks provide telemetered data to ground stations so that propellant consumption can be monitored.

Center engine shutdown is initiated by a programmed command (timed) from the IU through the S-II switch selector. Outboard engine shutdown is initiated when any two of the five liquid level sensors in either propellant tank indicate propellant depletion.
Each power system is isolated from each other.

**Figure 98**
S-IVB STAGE STRUCTURE

The S-IVB, the third booster stage, is approximately 59 feet in length with a stage weight at ground lift-off of approximately 262,150 pounds. The S-IVB stage is powered by a single J-2 engine capable of providing 232,000 pounds of thrust at first burn and 211,000 pounds during second burn.

The Forward Skirt Assembly

The forward skirt is the load supporting member between the LH₂ tank and the Instrument Unit. The forward umbilical plate, antennas, the LH₂ flight vents and tunnel fairings are attached externally to this skirt.

Propellant Tank Assembly

The propellant tank assembly is a cylindrical aluminum structure with a hemispherical shaped dome at each end. LOX and LH₂ are separated by a common bulkhead of sandwich type construction which is bonded to and separated by a fiberglass-phenolic honeycomb core.

LH₂ Tank

The internal surface of the LH₂ tank is a machined, waffle-like pattern to provide structural rigidity. Polyurethane insulation blocks, covered with fiberglass and a sealant coating, are bonded to the intertank waffle-like pattern to minimize LH₂ boiloff. The LH₂ tank is equipped internally with a slosh baffle, propellant utilization probe, temperature and level sensors and fill, pressurization and vent pipes.

LOX Tank

The LOX tank is located in the aft end of the propellant structure and is surrounded by the aft skirt assembly. The LOX tank is equipped internally with a slosh baffle, a chilldown pump, a 13.5 foot propellant utilization probe, temperature and level sensors, and fill, pressurization and vent pipes.

Aft Skirt Assembly

The aft skirt assembly is the load bearing structure between the LOX tank and the aft interstage.

Thrust Structure

The thrust structure is an inverted, truncated cone attached at its larger end to the aft dome of the LOX tank and at the smaller end to the J-2 engine mount.

Aft Interstage

The aft interstage is a truncated cone that provides a load support structure between the S-II and the S-IVB stages. S-II retro rocket mounts are attached to this stage. The aft interstage remains with the S-II at interstage separation.
Figure 39

S-IVB Configuration
J-2 ENGINE OPERATION S-IVB STAGE

The operating cycle of the J-2 Engine consists of prestart, start, steady-state operation and cutoff sequences. During prestart, LOX and LH₂ flow through the engine to temperature-condition the engine components, and to assure the presence of propellant in the turbopumps for starting. Following a timed cool-down period, the start signal is received by the sequence controller which energizes various control solenoid valves to open the propellant valves in the proper sequence. The sequence controller also energizes spark plugs in the gas generator and thrust chamber to ignite the propellant. In addition, the sequence controller releases GH₂ from the start tank. The GH₂ provides the initial drive for the turbopumps that deliver propellant to the gas generator and the engine. The propellant ignites, gas generator output accelerates the turbopumps, and engine thrust increases to main stage operation. At this time, the spark plugs are de-energized and the engine is in steady-state operation.

Steady-state operation is maintained until a cutoff signal is received by the sequence controller. The sequence controller de-energizes the solenoid valves which in turn close the engine propellant valves in the proper sequence. As a result, engine thrust decays and the cutoff sequence is complete.

Engine Start
Main Fuel Valve Open
Main Fuel Propellant Flow
Start Tank Discharge Valve Open
Pump Buildup
Bypass Flow Through Oxidizer
Turbine By-pass Valve
Main Oxidizer Flow
Gas Generator Propellant Flow
Main Oxidizer Valve Open
Mainstage OK Signal
90 Percent Thrust
The J-2 engine is a high performance, high altitude engine utilizing liquid oxygen and liquid hydrogen as propellants and is capable of multiple restarts.
S-IVB STAGE PROPELLANT SYSTEM

The S-IVB stage propellant system is composed of integral LOX/LH₂ tanks, propellant lines, control valves, vents and pressurization subsystems. Loading of the propellant tanks and flow of propellants is controlled by the propellant utilization system. Both propellant tanks are initially pressurized by ground source cold helium.

LOX tank pressurization during S-IVB stage burn is maintained by helium supplied from spheres in the LH₂ tank, which is expanded by passing through the heat exchanger, to maintain positive pressure across the common tank bulkhead and to satisfy engine net positive suction head. LH₂ tank pressurization during S-IVB stage burn is maintained by GIH₂ from the J-2 engine injector. Pressurization of the LH₂ tank strengthens the stage in addition to satisfying engine net positive suction head.

Repressurization of the propellant tanks, prior to J-2 engine restarts, is attained by passing cold helium, from the helium spheres in the LH₂ tank, through the O₂/H₂ burner. The heated helium is then routed to the propellant tanks. Should the O₂/H₂ burner fail, ambient repressurization will ensure propellant tank pressure for engine restarts.

S-IVB PROPELLANT LOAD AND OPERATIONAL SEQUENCE
Figure 37

5-IVB Propellant System

GH2 from J-2 Engine injector for LH2 tank pressurization during first and second S-IVB Stage burn.

LH2 Tank
~ 43,500 lbs at ignition

GH2/LH2
28-31 psia

LH2 Vent Valve

35 cu ft 3100 psia GH2 spheres (4). Inflight LOX Tank pressurization.

LOX/GHE
39-41 psia

LOX Fill and Drain

LOX Tank
~192,000 lbs. at ignition

LOX Vent Valve

LOX Fill & Drain

4.4 cu ft 3100 psia GH2 spheres (5) LH2 Tank depressurization (Backup System)
Prior to J-2 engine restart

O2/H2 Burner

J-2 Engine

35 cu ft 3100 psia GH2 spheres (2) for J-2 engine pneumatic system

Total propellant at ignition
~ 235,500 lbs.
Total propellant consumed after ignition ~ 223,900 lbs.
S-IVB THRUST VECTOR CONTROL SYSTEM

The single J-2 Engine is gimbal mounted on the longitudinal axis of the S-IVB Stage to provide pitch and yaw control during S-IVB powered flight. Engine firing is accomplished by an independent closed loop hydraulic system which supplies power to the two servo-actuators. The two servo-actuators may extend or retract individually or simultaneously. Gimbal position is proportional to the magnitude of an electrical input to the electro-hydraulic servomechanism located on each actuator. Mechanical feedback from the actuator to the servomechanism completes the closed engine position loop.

During S-I and S-II stage burns, the actuators hold the engine position to null. This is accomplished by utilizing the electrically driven auxiliary hydraulic pump. The auxiliary hydraulic pump is also used during orbit to periodically circulate the hydraulic fluid to prevent freezing. During the S-IVB burn, the main hydraulic pump, driven by the engine, provides the necessary pressure and circulation for actuator operation (pitch and yaw control). Real control is provided by the Auxiliary Propulsion System (see page 71).
Inflight use:

- Driven by Engine LOX Turbopump at 8000 RPM
- Output 8.0 gpm at 3500 psig

Low Pressure ~170 psig

Vehicle Thrust Structure Attachment Point

Hydraulic ServoActuators (2)

Servo Valve

III Electrical Commands

Accumulator pressurized from ground CH₃ at 2550 ± 50 psig at 70°F

NOTE: Auxiliary pump used during preflight checkout and during flight

Motor

Reservoir ~88 psig

Accumulator ~3500 psig

Auxiliary Pump

Electric Motor driven at 18,000 RPM
- Output 1.6 gpm at 3500 psig

Gimbal Point

Vehicle Yaw Axis

Vehicle Roll Axis

Vehicle Pitch Axis

Actuators (2)

Square Gimbal pattern
±7° Engine gimbal rate
under load ~ 8° per sec.

Gimbal Pattern
(looking forward)

Figure 38

5-DEB Thrust Vector Control System
AUXILIARY PROPULSION SYSTEM

The S-IVB Auxiliary Propulsion System (APS) provides vehicle attitude control during powered flight in the roll axis only and during S-IVB coast provides control in the pitch, yaw, and roll axes. Attitude corrections are made by firing the control engines, individually or in combination, in short bursts of approximately 65 ms minimum duration. Commands from the Flight Control Computer actuate fuel and oxidizer solenoid valve clusters that admit hypergolic propellants to the control engine combustion chambers.

The attitude control engines are located in two aerodynamically shaped modules, 180 degrees apart, on the aft end of the S-IVB stage (positions I and III). Each module contains four hypergolic engines, three 150 pound thrust attitude control engines and one 70 pound thrust ullage engine. The 70 pound thrust (ullage) engine in each module is used to settle the main stage propellants after S-IVB cutoff and again prior to restart. One control engine of each module is used to control the vehicles' attitude in pitch, while the other two are used for yaw and roll control.

Each APS module contains its own propellant supply and pressurization system. The hypergolic propellants used by the engines are monomethyl hydrazine (MMH) for the fuel and nitrogen tetroxide (N₂O₄) for the oxidizer. Helium is the pressurant used in the system.
Figure 39

Auxiliary Propulsion System
S-IVB STAGE PROPELLANT MANAGEMENT SYSTEM

The propellant management system provides a means for controlling and monitoring propellants during ground loading, powered flight and engine shutdown.

Continuous capacitance probes and point level sensors in the LOX and LH₂ tanks monitor propellant mass. During the propellant loading sequence, a signal from each capacitance probe is transmitted from the on board propellant electronics to GSE to indicate the level of propellants in the tanks. Overfill point level sensors are provided for LOX and LH₂ systems. When the propellant mass in the tanks reach a predetermined amount, the GSE loading computer automatically stops the loading sequence.

The propellant utilization (PU) subsystem controls the mixture ratio (MR) of the LOX/LH₂. The PU subsystem consists of a rotary valve, to control the amount of LOX flowing to the engine, and electrical controls for the valve. The MR is controlled by the switch selector outputs which are used to operate the PU valve.

Prior to engine start the PU valve is commanded to the neutral position to obtain a MR of 5.0:1. The PU valve remains at the 5.0:1 position during the first burn. Prior to engine restart (first opportunity) the PU valve is commanded by the switch selector to a MR of 4.5:1 and remains at this position for approximately one minute and 55 seconds of the S-IVB burn. The PU valve is then commanded to the neutral position (5.0:1). If the S-IVB restart is delayed to the second opportunity, the MR is shifted from 4.5:1 to 5.0:1 when the engine reaches 90 percent thrust.

Engine shutdown, during first burn, is initiated by a programmed command (velocity) from the IU through the switch selector. Engine shutdown after second burn is initiated by a programmed command (velocity) from the IU through the S-IVB switch selector. Backup shutdown is provided by any two of the five liquid level sensors in either propellant tank indicating propellant depletion.
S-IVB Propellant Utilization (PU) Timeline
For S-IVB Second Burn

- 230 K 5.5
- 200 K 5.0
- 180 K 4.5

250 Sec. Low EMR "ON"
Engine start Command
Tb6 + 570 Sec.
Low EMR "OFF"
Tb6 + 696.2 Sec.

Engine Thrust (pounds)  Engine Mixture Ratio

Note: PU valve remains at 5.0 throughout 1st burn

Figure 40
Each Battery Unit Weight: 201 lbs

Battery Weight: 201 lbs

Forward Bus 1 (28 vdc)

Forward Bus 2 (28 vdc)

Each Battery Unit Weight: 85 lbs

Each Battery Unit Weight: 85 lbs

Forward Skirt Area

Size Skirt Area

Figure 41

5-IVB Electrical Power & Distribution System
Analog data

Model 270 Multiplexer

IU PCM/DDAS Assembly

Antennae (~20 watts)

Power Divider

To GSE

Coaxial Switch

Digital data to ground facility via coaxial cable (DDAS)

Directional Coupler

Link CPI 258.5 MHz

Transmitter

PCM/RF Assembly

Calibration Command (from Switch Selector)

PCM/DDAS Assembly (Model 301)

TM Calibrator

Model 270 Multiplexer

Analog data

Model 270 Multiplexer

Analog data

Remote digital Submultiplexer

Digital Data

Figure 42

S-IVB Telemetry System
INSTRUMENT UNIT

The Instrument Unit is a cylindrical structure approximately 260 inches in diameter and 36 inches high which is attached to the forward end of the S-IVB stage. IU structure is composed of an aluminum alloy honeycomb sandwich material which was selected for its high strength-to-weight ratio, acoustical insulation, and thermal conductivity properties.

The cylinder is composed of three 120 degree segments—the access door segment, the flight control computer segment, and the ST-124-M segment.

The IU Stage contains:

- Guidance, Navigation and Control Equipment
- Telemetry Systems
- Tracking Systems
- Crew Safety Systems
- Environmental Control System

The guidance, navigation and control equipment contained in the IU includes that which is necessary for vehicle guidance and control during boost through orbital coast and subsequently for translunar injection.

Telemetry along with measuring systems is used to monitor certain conditions and events which take place in the IU and to transmit these monitored signals to ground receiving stations.

Tracking systems assist in the determination of the vehicle's trajectory. Tracking data is used for mission control, range safety and post flight evaluation of vehicle performance.

Crew Safety is provided by the Emergency Detection System, a portion of which is located in the IU stage. EDS senses conditions in the vehicle during boost phase which could cause vehicle failure.

Environmental Control maintains an acceptable operating environment during preflight and flight operations.
**Instrument Unit Configuration**

**Figure 4.5**

- **Weight:**
  - Dry = 4,000 lbs.
  - Service = 4,300 lbs.
PCMV/CCS Assembly (Model 301)

Digital data to ground facility via coaxial cable (DDAS)

Analog data

Model 270 Multiplexer

Remote Digital Multiplexer

Remote Digital Multiplexer

Computer Interface Unit

Model 270 Multiplexer

Data Adapter

IU Telemetry System

CCS Command Communication System

Figure 45
ENVIRONMENTAL CONTROL SYSTEM (ECS)

The Environmental Control System (ECS) has been developed to maintain an acceptable operating environment for the IU/S-IVB equipment during preflight and inflight operations.

The ECS is made up of the following:

**Thermal Conditioning System** - maintains a circulating Methanol Water coolant temperature of approximately 59° ± 1°F.

**Preflight Purging System** - maintains a supply of temperature and pressure regulated air/GN₂ in the IU/S-IVB equipment.

**Gas Bearing Supply System** - furnishes GN₂ to the ST-124-M3 inertial platform gas bearings.

**Hazardous Gas Detection System** - monitors the IU/S-IVB forward interstage area for the presence of hazardous vapors.
SPACECRAFT DESCRIPTION

The Spacecraft for the AS-506 mission is composed of:

Launch Escape System (LES)
Command Module (CM)
Service Module (SM)
Lunar Module (LM)
Spacecraft Lunar Module Adapter (SLA)

Launch Escape System

The Launch Escape System, which is jettisoned approximately 35 seconds after S-II Ignition, is made up of a Launch Escape Tower (LET), and a three-motor propulsion system (Tower Jettison, Launch Escape and Pitch Control Motors).

Command Module

The Command Module is a Block II Configuration. The module's inner structure, or pressure vessel, is separated from the outer structure by a layer of insulation. A heat shield structure is made up in three segments consisting of a forward heat shield, a crew compartment heat shield, and an aft shield. The CM is slightly over 11 feet in length and is about 12 feet in diameter. A propulsion system consists of Reaction Control Engines which may operate pulsed or continuous.

Service Module

The Service Module may be described as a cylindrical, aluminum shell which is made up of honeycomb-sandwich panels and a forward and aft bulkhead. 0ke gimbaled propulsion engine (capable of up to 30 restarts) and a reaction control system (4 clusters, 4 chambers each) make up the SM Propulsion System. The Command and Service Module are joined by three tension ties each of which is equipped with explosive charges for SM/CM separation.

Lunar Module

The Lunar Module consists primarily of an Ascent and Descent Stage. The Ascent Stage, which contains the crew compartment, is equipped with a Reaction Control System which provides thrust capability, an ingress and egress hatch to the crew's instrumentation and controls. The Descent Stage, consists primarily of a descent engine and four retractable landing gear assemblies. Over all weight of the Lunar Module is approximately 30,000 pounds.

Spacecraft Lunar Module Adapter

The Spacecraft Lunar Module Adapter (SLA) joins the Service Module (SM) to the S-IVB/ID. The SLA encloses the Lunar Module. Adapter panels which enclose the Lunar Module are jettisoned prior to docking and Lunar Module extraction.
Figure 49

Spacecraft Electrical Power & Distribution System
Type: Block II (manned)

Weights:
at CM/SM Sep. ~18,000 lbs
at entry ~12,000 lbs
at splashdown ~11,000 lbs

Dimensions:
~ 11 ft in length
~ 12 ft in diameter

Propulsion System:
12 Reaction Control Motors
~100 lbs Thrust each

Figure 50
- **Weight**: ~ 33,300 lbs.
- **Envelope dimensions**:
  - Height ~ 230 in
  - Width ~ 350 in (legs extended)
- **Diameter**: ~177 in (Ascent Stage Main Body)
- **Propulsion System**:
  - 1 **Descent Engine**
    - Throttle controlled thrust from 1000 to 10,500 lbs.
  - 1 **Ascent Engine**
    - 3500 lbs. thrust
  - Reaction controlled motors (4 clusters/4 chambers each) 100 lbs thrust each motor.
EVA (Extra Vehicular Activity) will consist of:
- Lunar Walk
  (First one then both crew members)
- All soil and rock samples
- Set up experiments for use after departure

**Figure 54**

**LUNAR SURFACE COMMUNICATIONS**