COMPARISON OF NUMERICAL TECHNIQUES FOR THE EVALUATION OF THE DOPPLER BROADENING FUNCTIONS $\psi(x,\theta)$ AND $\chi(x,\theta)$

by R. Bruce Canright, Jr., and Thor T. Semler

Lewis Research Center
Cleveland, Ohio 44135
Several approximations to the Doppler broadening functions $\psi(x, \theta)$ and $\chi(x, \theta)$ are compared with respect to accuracy and speed of evaluation. A technique due to A. M. Turing (1943) is shown to be at least as accurate as direct numerical quadrature and somewhat faster than Gaussian quadrature. FORTRAN IV listings are included.
COMPARISON OF NUMERICAL TECHNIQUES FOR THE EVALUATION OF
THE DOPPLER BROADENING FUNCTIONS $\psi(x, \theta)$ AND $\chi(x, \theta)$
by R. Bruce Canright, Jr., and Thor T. Semler
Lewis Research Center

SUMMARY

The two Doppler broadening functions, $\psi(x, \theta)$ and $\chi(x, \theta)$, are necessary for the computation of accurate temperature dependent resonance neutron cross sections. With the present use of many resonances and ever increasing resonance energies for reactor physics calculations in support of fast reactor development, the direct numerical quadrature evaluation of these functions has become prohibitively expensive in terms of computer time.

In this report direct numerical quadrature is compared with the techniques of Gaussian quadrature, contour integrations, and cubic spline interpolation in terms of both accuracy and ease of computation. A form of contour integration due to A. M. Turing (1943) is found to be much faster than (approximately six times) and as accurate as direct numerical quadrature.

Execution times for the evaluation of these functions on the IBM 7094-II computer and FORTRAN IV listings are included.

INTRODUCTION

It was noted early in the study of neutron physics that the neutron cross section, or interaction probability, of materials is dependent on the temperature of the material. Thus, a rapid variation of cross section with respect to neutron energy could be inferred (refs. 1 and 2). It was then pointed out by Breit and Wigner (ref. 3) that the nuclear cross sections for the formation of the compound nucleus, or target nucleus plus neutron, should exhibit a resonance structure. For the reaction, neutron in and gamma out, the cross section $\sigma_{n\gamma}$ should vary as a function of neutron energy $E$ as shown in the following equation (ref. 4):
\[ \sigma_{n\gamma}(E) = \frac{\pi}{k^2} g_J \frac{\Gamma_n \Gamma_\gamma}{(E - E_0)^2 + \left(\frac{\Gamma}{2}\right)^2} \quad (1) \]

where \( k \) is the wave number of the neutron in the center of the mass system, \( g_J \) is the spin factor \((2J + 1)/2(2I + 1)\), \( J \) is the spin quantum number of the compound system and \( I \) that of the nucleus, \( \Gamma_n \) is the scattering width, \( \Gamma_\gamma \) is the radiative width, \( E_0 \) is the energy of resonance, and \( \Gamma \) is the total width. Equation (1) is correct for stationary nuclei. However, since the nuclei of all materials are in thermal agitation, equation (1) must be modified to account for the effect of thermal motion. Briefly, the nuclei are assumed to have a Maxwellian velocity distribution and the cross section is folded into this velocity distribution. The resulting cross section is then a function of temperature as well as neutron energy; this cross section is the Doppler broadened cross section. Two functions arise from the derivation of the Doppler broadening of the cross section; they are \( \psi(x, \theta) \) and \( \chi(x, \theta) \). The derivation of the function \( \psi(x, \theta) \) is shown in detail in appendix A. The respective definitions are as follows:

\[ \psi(x, \theta) = \frac{\theta}{2\sqrt{\pi}} \int_{-\infty}^{\infty} \frac{\exp\left[-\frac{1}{4} \frac{\theta^2 (x - y)^2}{1 + y^2}\right]}{1 + y^2} \, dy \quad (2) \]

\[ \chi(x, \theta) = \frac{\theta}{2\sqrt{\pi}} \int_{-\infty}^{\infty} \frac{\exp\left[-\frac{1}{4} \frac{\theta^2 (x - y)^2}{1 + y^2}\right]}{2y} \, dy \quad (3) \]

Here \( x = (2/\Gamma)(E - E_0) \), \( \theta = \Gamma(4mTE_0/M)^{-1/2} \), \( m \) is the neutron mass, \( M \) is the nuclear mass, and \( T \) is the effective temperature in eV's.

Plots of \( \psi(x, \theta) \) and \( \chi(x, \theta) \) are shown for selected values of \( \theta \) and a range of \( x \) from 0 to 10 in figures 1 and 2. Detailed plots of the regions of interest are shown in figures 3 and 4.

In the past various forms of "brute force" direct numerical quadrature have been used to evaluate \( \psi \) and \( \chi \) (ref. 5). However, with the present use of many resonances and ever increasing resonance energies for reactor physics calculations in support of fast reactor development direct numerical quadrature has become prohibitively expensive in terms of computer time. The following report evaluates various techniques which might avoid the excessively long computer runs needed to calculate the Doppler
Figure 1. - Values of $\psi$ for selected values of $\theta$.

Figure 2. - Values of $\chi$ for selected values of $\theta$. 

Symbol $\theta$

A 0.01
B 0.05
C 0.1
D 0.5
E 1.0
F 5.0
G 50.0
broadened cross sections by direct numerical quadrature. Such an evaluation is valuable because of present widespread interest in such fast reactors, and because "lengthy and involved routines giving wrong values for the (Doppler broadening) functions are prevalent" (ref. 6).

It should be noted that, although these integrals have been extensively studied (refs. 6 to 12), there is virtually no standard notation for either the Doppler broadening functions or the independent variables. We follow the notation of Dresner (ref. 4). Here $\theta$ is proportional to $T^{-1/2}$ and $x$ is proportional to the energy distance from the resonance peak. Typical transformations for comparing our notation to others include

Dresner \quad Bhat and Lee-Whiting \quad Matta and Reichel

\begin{align}
\psi(x, \theta) &= \frac{\theta \sqrt{\pi}}{2} u \left(\frac{x \theta}{2}, \frac{\theta}{2}\right) = U_0 \left(x, \frac{1}{\theta^2}\right) \quad (4) \\
\chi(x, \theta) &= \theta \sqrt{\pi} v \left(\frac{x \theta}{2}, \frac{\theta}{2}\right) = 2V_0 \left(x, \frac{1}{\theta^2}\right) \quad (5)
\end{align}

**NUMERICAL TECHNIQUES**

In order to evaluate temperature dependent continuous neutron cross sections, one must evaluate $\psi$ and $\chi$ many times; therefore, both accuracy and as much speed in computation as possible are required. Special series methods, numerical quadrature, contour integration techniques, and interpolation have been considered for their evaluation; these studies indicate that a specialized quadrature and contour integration yield the accuracy required.
Asymptotic Series and Limiting Cases

Several special forms for \( \psi \) and \( \chi \) are known which are simple to evaluate, but taken all together, do not cover much of the physically meaningful range of \( x \) and \( \theta \). For most work \( |x| < 1000, \ 0.001 < \theta < 100 \). For this reason such special forms are used only as boundary check values for the other more general methods.

For example, for \( x\theta \gg 1 \)

\[
\psi(x, \theta) = \frac{1}{1 + x^2} \left( 1 + \frac{2}{\theta^2} \frac{3x^2 - 1}{(1 + x^2)^2} + \ldots \right) \quad \text{(ref. 4)}
\]

Also,

\[
\psi(x, \infty) = \frac{1}{1 + x^2} \quad \chi(x, \infty) = \frac{2x}{1 + x^2} \quad \text{(ref. 4)}
\]

\[
\psi(0, \theta) = \frac{1}{2} \sqrt{\pi \theta} \exp \left( \frac{\theta^2}{4} \right) \text{erfc} \left( \frac{\theta}{2} \right) \quad \chi(0, \theta) = 0 \quad \text{(ref. 4)}
\]

Direct Numerical Quadrature

For large-scale problems, several hundred resonances and several thousand energy points, the standard quadrature techniques in use at Lewis Research Center are too slow by at least two orders of magnitude. Because of the form of the integrand, programs using a Gaussian quadrature and also a Simpson's rule quadrature containing step modification logic were tried. This adaptive Simpson's rule quadrature, called method A, is coded in FORTRAN in appendix B as function SIMPS1. Both programs produced large errors for some values of \( x \) and \( \theta \); the critical parameter is the product \( x\theta \). Both the shape of the integrands and the choice of limits of integration depend on this product. Let us transform the integrands and examine their behavior. Let

\[
t = \frac{\theta}{2} (y - x) \quad \text{(6)}
\]

Then
\[ \psi(x, \theta) = \frac{1}{\sqrt{\pi}} \int_{-\infty}^{\infty} \frac{e^{-t^2}}{1 + \left(\frac{2t}{\theta} + x\right)^2} dt \]  

(7)

\[ \chi(x, \theta) = \frac{2}{\sqrt{\pi}} \int_{-\infty}^{\infty} \frac{e^{-t^2} \left(\frac{2t}{\theta} + x\right)}{1 + \left(\frac{2t}{\theta} + x\right)^2} dt \]  

(8)

The damping factor \( e^{-t^2} \) in these integrands is now independent of \( x \) and \( \theta \) both (with a maximum at \( t = 0 \)) and the remaining terms are

\[ f \equiv \frac{1}{1 + \left(\frac{2t}{\theta} + x\right)^2} \]  

(9)

\[ g \equiv \frac{\left(\frac{2t}{\theta} + x\right)}{1 + \left(\frac{2t}{\theta} + x\right)^2}. \]  

(10)

These terms are sketched in figures 5 and 6. Note that both \( f \) and \( g \) have critical points which depend on \(-x\theta/2\).

Figure 6. - Integrand \( g \).

Figure 5. - Integrand \( f \).
The integrals for $\psi$ and $\chi$ are now in convenient form for application of Gauss-Hermite quadrature (ref. 13). That is,

$$\psi = \int_{-\infty}^{\infty} e^{-t^2} f(t) \, dt = \sum_{i=1}^{N} A_i f(t_i)$$  \hspace{1cm} (11)

$$\chi = \int_{-\infty}^{\infty} e^{-t^2} g(t) \, dt = \sum_{i=1}^{N} A_i g(t_i)$$  \hspace{1cm} (12)

where the $t_i$ and $A_i$ are tabulated for many $N$; for example, we chose $N = 16$ and $N = 32$.

However, it can be seen from figures 5 and 6 that, for Gauss-Hermite quadrature, no matter what $t_i$ are picked, there will be both $x$ and $\theta$ such that much of the area under $f$ and $g$ is far from any of the $t_i$. For example, for $N = 16$, the maximum $t_i = \pm 4.689$ - meaning $f$ and $g$ are sampled only in this range; typical values of $x = 20$, $\theta = 2$ place the critical points at $t = -20$. This inability to sample from significant values of $f(t)$ and $g(t)$ explains why Gauss-Hermite quadrature fails to give accurate results.

On examining figure 6 from the point of view of using a Simpson's rule quadrature, it can be seen that, for some values of $x$ and $\theta$, the $\chi$ integrand has a positive portion and a negative portion. To achieve and maintain accuracy, $\chi$ must be broken into positive and negative portions and evaluated separately. With these modifications, the adaptive Simpson's rule was successfully applied to $\psi$ and $\chi$; this shall be referred to as method A. One should note that the two parts $-\infty < t < -x\theta/2$ and $-x\theta/2 < t < +\infty$ of $\chi$ sometimes agree in magnitude to 12 significant figures. For comparison, another quadrature method in use at this center called method D was also studied.

**Contour Integration**

Integrals of the form $\int_{-\infty}^{\infty} f(t) e^{-t^2} \, dt$, as we see in equations (7) and (8) can sometimes be evaluated by contour integration in the complex plane (ref. 14). A. M. Turing first suggested this method for evaluating $\psi$ and $\chi$ in 1943 (ref. 15). The Turing method is attractive because it should require much less arithmetic than numerical quadrature. This method has been formulated independently by Bhat and Lee-
Whiting, and by Matta and Reichel. We have applied the method of Bhat and Lee-Whiting (ref. 6), called method B and the similar method of Matta and Reichel (ref. 12), which we call method C. These methods are very useful for many related integrals as well (ref. 12). Methods B and C use series with a parameter $h$ (and corresponding error estimate $E(h)$) which can be varied to achieve desired accuracy. In addition to the series contribution, both methods have a contribution from the poles (places where the denominator of the integrands is zero) which depends on whether $\theta$ is inside, on, or outside the contour chosen for integration. The formulas are the following: For method B let $a = x\theta/2$, $b = \theta/2$, and recall transformations (4) and (5). Then

$$
\psi(a, b) = \frac{\text{hb}}{\sqrt{\pi}} \sum_{-\infty}^{\infty} \frac{e^{-n^2h^2}}{(a - nh)^2 + b^2} + 2P(h)e^{(b^2-a^2)} \frac{\cos(2ab) - e^{2\pi b/h} \cos\left(\frac{2\pi a}{h} - 2ab\right)}{D}
$$

+ real part of $E(h)$ \hfill (13)

$$
\chi(a, b) = \frac{2h}{\sqrt{\pi}} \sum_{-\infty}^{\infty} \frac{e^{-n^2h^2}(a - nh)}{(a - nh)^2 + b^2} - 4P(h)e^{(b^2-a^2)} \frac{\sin(2ab) + e^{2\pi b/h} \sin\left(\frac{2\pi a}{h} - 2ab\right)}{D}
$$

+ imaginary part of $E(h)$ \hfill (14)

where

$$
D = 1 - 2e^{2\pi b/h} \cos\frac{2\pi a}{h} + e^{4\pi b/h}
$$

and

$$
P = 0 \quad \text{for} \quad 2\pi/h < \theta
$$

$$
P = 1/2 \quad \text{for} \quad 2\pi/h = \theta \quad \text{(ref. 6)}
$$

$$
P = 1 \quad \text{for} \quad 2\pi/h > \theta
$$

Finally,
This method is coded in FORTRAN in appendix C, as subroutine PSCH.

Similarly, for method C, let \( t = 1/\theta^2 \). Then

\[
|E(h)| \sim \frac{\sqrt{a^2 + b^2} e^{-\pi 2/h}}{|\frac{\pi^2}{h^2} - b^2|} \tag{15}
\]

\[
\psi(x, t) = \frac{h}{\sqrt{\pi (1 + x^2)}} + \frac{2h}{\sqrt{\pi}} \sum_{n=1}^{\infty} e^{-n^2h^2(1 + x^2 + 4t^2h^2)} + \frac{pP_1 - E(h)}{t} \tag{16}
\]

\[
\chi(x, t) = \frac{2hx}{\sqrt{\pi (1 + x^2)}} + \frac{4hx}{\sqrt{\pi}} \sum_{n=1}^{\infty} e^{-n^2h^2(1 + x^2 - 4t^2h^2)} - 2 \left[ PQ_1 + \frac{x}{t} E(h) \right] \tag{17}
\]

where

\[
P = 0 \quad \text{for} \quad 2\pi/h < \theta \quad \text{or} \quad t < h^2/4\pi^2
\]

\[
P = 1/2 \quad \text{for} \quad 2\pi/h = \theta \quad \text{or} \quad t = h^2/4\pi^2
\]

\[
P = 1 \quad \text{for} \quad 2\pi/h > \theta \quad \text{or} \quad t > h^2/4\pi^2
\]

Also,

\[
P_1 = \alpha \left( \frac{AC - BD}{C^2 + D^2} \right), \quad Q_1 = \alpha \left( \frac{BC + AD}{C^2 + D^2} \right)
\]

and

\[
\alpha = \sqrt{\frac{\pi}{t}} e^{-\left(x^2/4t + \pi/h \sqrt{t - 1/4t}\right)}
\]
A = \cos \frac{x}{2t}

B = \sin \frac{x}{2t}

C = e^{-\frac{\pi}{h\sqrt{t}}} - \cos \frac{\pi x}{h\sqrt{t}}

D = \sin \frac{\pi x}{h\sqrt{t}}

Finally,

\[ |E(h)| \leq \frac{e^{-\frac{\pi^2}{h^2}}}{2\left(1 - e^{-\frac{\pi^2}{h^2}}\right)} \]  \hspace{1cm} (18)

This method is coded in FORTRAN in appendix C, as subroutine PSIPHI.

Using these estimates for the error, and knowing the accuracy desired, one can choose the largest possible \( h \) which will achieve this accuracy. For method B, \( h = 1.0 \) was used; for method C, \( h = 0.75 \). The series of each method was truncated at nine terms. The same number of terms is used in order to make comparisons of execution times.

**Interpolation**

Using methods A, B, and C tables were built of \( \psi \) and \( \chi \) for various \( x \) and \( \theta \) in hopes that interpolation would be possible. These tables were fit with cubic splines (refs. 16 and 17). Briefly, cubic splines are cubic polynomials passed piecewise through each pair of adjacent data points. The coefficients of these cubics are chosen so as to match first and second derivatives at the data points; this is usually called the spline property. These points were used to generate contour plots as shown in figures 7 and 8. This method of interpolation has not yet achieved the accuracy of methods A, B, or C. Interpolation remains attractive and is a subject for future work.
Contour label | Contour value
---|---
A | 0.050
B | 0.100
C | 0.200
D | 0.300
E | 0.400
F | 0.500
G | 0.600
H | 0.800

Figure 7. - Contour plot of $\psi$. 
Figure 8. - Contour plot of $x$. 

<table>
<thead>
<tr>
<th>Contour label</th>
<th>Contour value</th>
</tr>
</thead>
<tbody>
<tr>
<td>A</td>
<td>0.050</td>
</tr>
<tr>
<td>B</td>
<td>0.100</td>
</tr>
<tr>
<td>C</td>
<td>0.200</td>
</tr>
<tr>
<td>D</td>
<td>0.300</td>
</tr>
<tr>
<td>E</td>
<td>0.400</td>
</tr>
<tr>
<td>F</td>
<td>0.500</td>
</tr>
<tr>
<td>G</td>
<td>0.600</td>
</tr>
<tr>
<td>H</td>
<td>0.800</td>
</tr>
</tbody>
</table>
RESULTS

Accuracy Comparisons

The Gaussian quadrature techniques as used herein do not give satisfactory relative accuracy in computing $\psi$ and $\chi$. This is true whether or not the weighting function $e^{-t^2}$ is removed from the integrand. For most values of $x$ and $\theta$ this method is satisfactory, but wrong results occur in an unpredictable fashion. Since the error estimate associated with Gaussian quadrature assumes the use of functionals not readily obtainable, it has not been used. The results are in error because this quadrature uses fixed abscissas, while, as discussed in the section Direct Numerical Quadrature, the peaks of the integrands for $\psi$ and $\chi$ vary as the product $x\theta$.

The adaptive Simpson's rule method (method A), with numerical results given in table I, yields satisfactory accuracy for our work, four significant figures. This method was the first one found to be sufficiently accurate; it was used as a check against published values and against other methods discussed in this report.

The contour integration methods, methods B and C, have accuracies controllable by choice of a parameter $h$. See tables II and III. They both have corresponding error estimates $E(h)$. For a given fixed $h$, methods B and C give much the same results, and speed becomes the deciding factor. However, there is one region where method B

|TABLE I. - TYPICAL VALUES OBTAINED BY METHOD A |

(a) Values of $\psi$

<table>
<thead>
<tr>
<th>$x$</th>
<th>0.01</th>
<th>0.5</th>
<th>1</th>
<th>2</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.001</td>
<td>0.00881246</td>
<td>0.341353</td>
<td>0.545648</td>
<td>0.757895</td>
</tr>
<tr>
<td>0.1</td>
<td>0.00881246</td>
<td>0.341191</td>
<td>0.544852</td>
<td>0.755166</td>
</tr>
<tr>
<td>1</td>
<td>0.00881224</td>
<td>0.325577</td>
<td>0.472498</td>
<td>0.540149</td>
</tr>
<tr>
<td>4</td>
<td>0.00880896</td>
<td>0.164687</td>
<td>0.0915975</td>
<td>0.0643058</td>
</tr>
</tbody>
</table>

(b) Values of $\chi$

<table>
<thead>
<tr>
<th>$x$</th>
<th>0.001</th>
<th>0.5</th>
<th>1</th>
<th>2</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.0001</td>
<td>9.991191×10^{-7}</td>
<td>0.164663×10^{-3}</td>
<td>0.454362×10^{-3}</td>
<td>0.968510×10^{-3}</td>
</tr>
<tr>
<td>0.1</td>
<td>9.991191×10^{-7}</td>
<td>0.016461</td>
<td>0.0453743</td>
<td>0.0965705</td>
</tr>
<tr>
<td>1</td>
<td>9.99175×10^{-4}</td>
<td>0.159261</td>
<td>0.408498</td>
<td>0.738117</td>
</tr>
<tr>
<td>4</td>
<td>3.96371×10^{-3}</td>
<td>0.400753</td>
<td>0.504762</td>
<td>0.481550</td>
</tr>
</tbody>
</table>
TABLE II. - TYPICAL VALUES OBTAINED BY METHOD B

(a) Values of $\psi$

<table>
<thead>
<tr>
<th>$x$</th>
<th>0.01</th>
<th>0.5</th>
<th>1</th>
<th>2</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.001</td>
<td>0.00881269</td>
<td>0.341350</td>
<td>0.545639</td>
<td>0.757862</td>
</tr>
<tr>
<td>1</td>
<td>0.00881239</td>
<td>0.341189</td>
<td>0.544844</td>
<td>0.755133</td>
</tr>
<tr>
<td>4</td>
<td>0.00880900</td>
<td>0.164686</td>
<td>0.091598</td>
<td>0.064308</td>
</tr>
</tbody>
</table>

(b) Values of $\chi$

<table>
<thead>
<tr>
<th>$x$</th>
<th>0.001</th>
<th>0.5</th>
<th>1</th>
<th>2</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.001</td>
<td>$9.995718 \times 10^{-7}$</td>
<td>$1.64663 \times 10^{-3}$</td>
<td>$4.54363 \times 10^{-3}$</td>
<td>$9.66573 \times 10^{-3}$</td>
</tr>
<tr>
<td>.1</td>
<td>$9.88693 \times 10^{-5}$</td>
<td>0.0164608</td>
<td>0.0458372</td>
<td>0.0965732</td>
</tr>
<tr>
<td>1</td>
<td>$9.92042 \times 10^{-4}$</td>
<td>0.159267</td>
<td>0.408535</td>
<td>0.738138</td>
</tr>
<tr>
<td>4</td>
<td>$3.96523 \times 10^{-3}$</td>
<td>0.400761</td>
<td>0.504784</td>
<td>0.481569</td>
</tr>
</tbody>
</table>

TABLE III. - TYPICAL VALUES OBTAINED BY METHOD C

(a) Values of $\psi$

<table>
<thead>
<tr>
<th>$x$</th>
<th>0.01</th>
<th>0.5</th>
<th>1</th>
<th>2</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.001</td>
<td>0.00881246</td>
<td>0.341351</td>
<td>0.545641</td>
<td>0.757872</td>
</tr>
<tr>
<td>1</td>
<td>0.00881249</td>
<td>0.341189</td>
<td>0.544846</td>
<td>0.755143</td>
</tr>
<tr>
<td>4</td>
<td>0.00880698</td>
<td>0.164687</td>
<td>0.091599</td>
<td>0.064307</td>
</tr>
</tbody>
</table>

(b) Values of $\chi$

<table>
<thead>
<tr>
<th>$x$</th>
<th>0.001</th>
<th>0.5</th>
<th>1</th>
<th>2</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.001</td>
<td>$9.90694 \times 10^{-7}$</td>
<td>$1.64662 \times 10^{-3}$</td>
<td>$4.54359 \times 10^{-3}$</td>
<td>$9.66511 \times 10^{-3}$</td>
</tr>
<tr>
<td>.1</td>
<td>$9.91765 \times 10^{-5}$</td>
<td>0.0164607</td>
<td>0.0453867</td>
<td>0.0965709</td>
</tr>
<tr>
<td>1</td>
<td>$9.90592 \times 10^{-4}$</td>
<td>0.159265</td>
<td>0.408530</td>
<td>0.738117</td>
</tr>
<tr>
<td>4</td>
<td>$3.96352 \times 10^{-3}$</td>
<td>0.400756</td>
<td>0.504770</td>
<td>0.481536</td>
</tr>
</tbody>
</table>
loses all accuracy, while method C remains stable. For $\theta \sim 0.001$ (high energies $>1$ eV) method B failed, even with $h = 0.5$ and 20 terms in the series. In this region method C, with $h = 0.75$ and nine terms as before, gives four significant figures for $\psi$ and one for $\chi$. We conclude that, for small $\theta$, method B should be used with caution.

Some sample results obtained by methods A, B, C, and D are given in tables I to IV.

### TABLE IV. - TYPICAL VALUES OBTAINED BY METHOD D

**(a) Values of $\psi$**

<table>
<thead>
<tr>
<th>$x$</th>
<th>$\theta$</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>0.01</td>
</tr>
<tr>
<td>0.001</td>
<td>0.00881212</td>
</tr>
<tr>
<td>0.1</td>
<td>0.00881228</td>
</tr>
<tr>
<td>1</td>
<td>0.00881233</td>
</tr>
<tr>
<td>4</td>
<td>0.00880896</td>
</tr>
</tbody>
</table>

**(b) Values of $\chi$**

<table>
<thead>
<tr>
<th>$x$</th>
<th>$\theta$</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>0.01</td>
</tr>
<tr>
<td>0.001</td>
<td>9.51862x10^{-7}</td>
</tr>
<tr>
<td>0.1</td>
<td>9.41018x10^{-5}</td>
</tr>
<tr>
<td>1</td>
<td>9.94859x10^{-4}</td>
</tr>
<tr>
<td>4</td>
<td>3.95791x10^{-3}</td>
</tr>
</tbody>
</table>

**Speed Comparisons**

Because the numerical quadrature of method A requires far more arithmetic operations than methods B and C, method A has been modified to split the argument ranges into two regions and to use an asymptotic expansion when possible. Values for $x$ were chosen uniformly in the range $0 < x < 1000$. (Note that $\psi(-x) = \psi(x)$ and $\chi(-x) = -\chi(x)$.) Two sets of $\theta$ ranges were used: in the range $0 < \theta < 1$, the pole contributions are always present; while in the range $0 \sim \theta < 100$, these contributions are usually zero. Execution times on an IBM 7094 for 2000 evaluations are given in table V. An example of a Doppler broadening resonance cross section code which may be used with the subroutines herein is shown in appendix D.
TABLE V. - COMPARISON OF EXECUTION TIMES

<table>
<thead>
<tr>
<th>θ range</th>
<th>Method</th>
<th>Time, sec</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>A (integrals only)</td>
<td>0.77</td>
</tr>
<tr>
<td></td>
<td>A (integrals + series)</td>
<td>2.05</td>
</tr>
<tr>
<td></td>
<td>B</td>
<td>1.87</td>
</tr>
<tr>
<td></td>
<td>C</td>
<td>2.16</td>
</tr>
<tr>
<td>0 &lt; θ &lt; 100</td>
<td></td>
<td>a5.30</td>
</tr>
<tr>
<td>0 &lt; θ &lt; 1</td>
<td>----</td>
<td>11.5</td>
</tr>
</tbody>
</table>

aRun for comparison only--it was known that this method would not be fast enough to be practicable.

Discussion of Execution Times

Several conclusions can be drawn from table I. First, even the slow numerical quadrature method is accurate, and as mentioned earlier "lengthy and involved routines giving wrong values for the ψ and χ functions are prevalent" (ref. 6). Study of these integrals began because an existing routine was very slow, about six times slower than our quadrature. Note that adding a test and an asymptotic expansion to method A increases the speed nearly $2^{1/2}$ times. Most important for this study, method B is nearly $2^{1/2}$ times faster than method C for the distribution $0 < θ < 100$. This is because terms in the series of method B can be written more compactly than those of method C; and only for small θ is the pole contribution needed; that is, the series is the only calculation required. Fourth, for $0 < θ < 1$ most of this speed advantage is gone. Now the pole calculations are always needed. Method B, coded as subroutine PSCH listed in appendix C, is still to be preferred, for methods B and C are about equally accurate.

CONCLUDING REMARKS

Direct numerical quadrature using an adaptive Simpson's rule technique yields results accurate to four significant figures for both $ψ(x, θ)$ and $χ(x, θ)$. However, this method is quite slow and expensive in terms of computer time.

The method of Gaussian quadrature used herein was evaluated and found to be erratic in terms of error and somewhat slower than the techniques of contour integration. Error estimation for the Gaussian quadrature proved to be incapable of rapid calculation.

Both contour integration methods, method B using subroutine PSCH, and method C using subroutine PSIPHI gave very rapid and accurate results. The accuracy is comparable with that of direct numerical quadrature.
The method of cubic spline interpolation failed to achieve the accuracy of the other methods evaluated.

Of the numerical methods considered and evaluated contour integration, subroutines\textsc{psch} and \textsc{psphi}, achieved the greatest speed of computation combined with quite satisfactory accuracy.

\textbf{Lewis Research Center,}
\textbf{National Aeronautics and Space Administration,}
\textit{Cleveland, Ohio, April 10, 1972},
\textit{132-80}.
APPENDIX A

DERIVATION OF $\psi(x, \theta)$ - THE DOPPLER BROADENING FUNCTION

If a beam of neutrons with velocity $\vec{v}$ impinges upon a group of nuclei at rest, the reaction rate for process $x$ is proportional to $v\sigma_x(v)$, where $\sigma_x(v)$ is the nuclear cross section for process $x$ as a function of velocity. However, the nuclei are not stationary but are in thermal motion. We may assume the nuclei have a Maxwellian velocity distribution characterized by a temperature $T$; then the three-dimensional Maxwell velocity distribution may be written as

$$P(\vec{v}) \, d\vec{v} = \left(\frac{M}{2\pi kT}\right)^{3/2} e^{-MV^2/2kT} \, dV_x \, dV_y \, dV_z$$

where $T$ is the effective temperature, $M$ is the nuclear mass, and $\vec{V}$ is the nuclear velocity.

The value of the velocity of the neutron, of mass $m$, relative to the nucleus is then the magnitude of the difference of the velocity vectors. That is,

$$v_r = |\vec{V} - \vec{V}|$$

The corresponding energy is then $E_r = \frac{1}{2} mv_r^2$. Since $P(\vec{v}) \, d\vec{v}$ is the probability of a nucleus having a velocity within $d\vec{v}$ about $\vec{V}$, the probable number of reactions to type $x$ per second is

$$v_r \sigma_x(E_r)P(\vec{v}) \, d\vec{v}$$

The total probability is then

$$\sigma_x(E) = \frac{1}{v} \int v_r \sigma_x(E_r)P(\vec{v}) \, d\vec{v}$$

If a coordinate system is chosen such that the $z$-direction is parallel to the neutron velocity, then

$$E_r = \frac{1}{2} m(\vec{V} - \vec{V})^2 = \frac{1}{2} m \left[(v - V_z)^2 + V_x^2 + V_y^2\right]$$
Since the neutron velocity is quite high compared to the thermal motion of the nuclei, the $V_z^2$, $V_x^2$, and $V_y^2$ terms may be neglected. Hence,

$$E_r = \frac{1}{2} m (v^2 - 2vV_z)$$

Thus

$$v_r = \sqrt{\frac{2E_r}{m}}$$

Integrating out the $V_x$ and $V_y$ velocity components from the Maxwellian results on the following distribution for the $z$-component:

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} P(V) \, dV_x \, dV_y = \left(\frac{M}{2\pi kT}\right)^{1/2} e^{-M^2 V_z^2 / 2kT}$$

The Breit-Wigner expression for a single-level resonance cross section for absorption is

$$\sigma_{\gamma}(E) = \sigma_0 \frac{\Gamma \gamma}{\Gamma} \sqrt{\frac{E_0}{E}} \frac{\Gamma^2}{4(E - E_0)^2 + \Gamma^2}$$

where $\sigma_0 = 4\pi \bar{\kappa}^2 (\Gamma_n / \Gamma)$, $\bar{\kappa}$ is neutron wave length over $2\pi$, $g$ is the statistical weighting factor, $\Gamma_n$ is the scattering width, $\Gamma$ is the total width, $\Gamma_\gamma$ is the radiative width, and $E_0$ is the resonance energy. Substituting into the previous equation gives

$$\sigma_{\gamma}(E) = \sigma_0 \frac{\Gamma \gamma}{\Gamma} \sqrt{\frac{E_0}{E}} \frac{\Gamma^2}{4(E - E_0)^2 + \Gamma^2} \int_{-\infty}^{\infty} e^{-M^2 V_z^2 / 2kT} \frac{\Gamma^2 \, dV_z}{4(E_r - E_0)^2 + \Gamma^2}$$

If one defines

$$x = \frac{2}{\Gamma} (E - E_0)$$
\[
y = \frac{2}{\Gamma} \left( E_r - E_0 \right)
\]

\[
\Delta = \sqrt{\frac{4mkTE}{M}} = \sqrt{\frac{4kTE_0}{M}} \quad m \geq 1
\]

(a very good approximation for large \( E_0 \)) and

\[
\theta = \frac{\Gamma}{\Delta}
\]

then

\[
\sigma_\gamma(E) = \sigma_0 \frac{\Gamma \gamma}{\Gamma} \sqrt{\frac{E_0}{E}} \frac{\theta}{\theta} \int_{-\infty}^{\infty} \frac{\exp\left[-\frac{1}{4} \theta^2 (y - x)^2\right]}{1 + y^2} \psi(x, \theta)\]

or

\[
\sigma_\gamma(E) = \sigma_0 \frac{\Gamma \gamma}{\Gamma} \sqrt{\frac{E_0}{E}} \psi(x, \theta)
\]

where

\[
\psi(x, \theta) = \frac{\theta}{2\sqrt{\pi}} \int_{-\infty}^{\infty} \frac{\exp\left[-\frac{1}{4} \theta^2 (y - x)^2\right]}{1 + y^2} dy
\]

The function

\[
\chi(x, \theta) = \frac{\theta}{2\sqrt{\pi}} \int_{-\infty}^{\infty} \frac{2y \exp\left[-\frac{1}{4} \theta^2 (y - x)^2\right]}{1 + y^2} dy
\]

may be derived in the same manner using the same assumptions.
This function SIMPS1 is a Simpson's rule integrating routine, which integrates the external function FUNC1 from XMIN to XMAX. When sufficient accuracy is not attained, the flag KER is incremented by 1.

```
FUNCTION SIMPS1(XMIN, XMAX, FUNC1, KER)
DIMENSION V(200), H(200), A(200), P(200), E(200)
DATA T/3.CE-4/
IF(XMIN.EC.XMAX) GO TO 18
V(1)=XMIN
H(1)=C.5*(XMAX-XMIN)
A(1)=FUNC1(XMIN)
B(1)=FUNC1(XMIN+H(1))
C(1)=FUNC1(XMAX)
P(1)=H(1)*(A(1)+4*C*E(1)+C(1))
E(1)=F(1)
ANS=P(1)
N=1
FRAC=2.0*T
1 FRAC=C.5*FRAC
2 TEST=ABS(FPAC*ANS>
4 IF(ABS(E(I)).LE.TEST) GO TO 7
5 N = N+1
V(N)=V(I)+H(I)
H(N)=C.5*H(I)
A(N)=E(I)
B(N)=FUNC1(V(N)+H(N))
C(N)=C(I)
P(N)=H(N)*(A(N)+4*C*P(N)+C(N))
G=F(I)
H(I)=H(I)
B(I)=FUNC1(V(I)+H(I))
C(I)=A(I)
P(I)=H(I)*(A(I)+4*C*P(I)+C(I))
Q=P(I)+P(A)-Q
ANS=ANS+Q
E(I)=G
E(N)=G
6 IF(A-2.G) 7,13,13
7 CONTINUE
E IF(A-K) 9,9,2
9 G = C.0
10 DC 11 I=1,N
11 Q=G+E(I)
12 IF(ABS(E(I)-T*ABS(ANS)) 14,14,1
Ker=KER+1
14 ANS=C.0
15 DC 16 I=1,N
16 ANS=ANS+F(I)
```
APPENDIX C

FORTRAN IV LISTINGS OF METHODS B AND C

Subroutine PSCH uses the technique of Bhat and Lee-Whiting (ref. 6). The arguments are XX and TT where

XX  natural distance X
TT  temperature parameter

The values U and V are returned where

U  first Doppler broadening integral
V  second Doppler broadening integral

SUBF1C PSCH

C FROM E HAT AND LEE-WHITING, P. 278
C
I = 1.
SUBROUTINE PSCH(XX, TT, U, V)
DIMENSION EN(5), EN2(10)
DATA PI2/12.566371/
DATA RTPI/1.7724539/, PIH/1.5707963/
DATA PI, FI2, N /3.1415927, 6.2831854, 5/
DATA (EKM I ), 1 = 2, 5) / .11709966E0, .5830489E-2, .39282561E-4,
  1 .35821059E-7 /
DATA (EN2(I), 1=2,10) / .24785599, .1709966, .33549615E-1, .58300489E-
  *2, .61448264E-3, .39282561E-4, .15231502E-5, .35821059E-7, .51095996E-9
C
XC = ABS(XX)
THETA = ABS(TT)
Y = THETA/2.
X = XC*Y
C ARE WE IN DANGER
XTEST = X - INT(X)
IF((XTEST.LT.0.01) .OR. XTEST.GT.0.99) AND. ABS(Y).LT.0.01) GO TO 40
IF(XC.GT.75.*SQRT(1.-H./(Y*Y))) GO TO 30
IF(Y.LT.0.01) GO TO 40
C BEGIN SERIES SUMATION.
Y2 = Y*Y
C SET N = 0 TERM -- NOTE PI IS IN THIS ONE
D = PI*(X*Y+Y2)
SU = Y/C
SV = X/C
CC 10 I = 2, N
AW = I - 1
XNF = X - AM
XNM = X + AM
DP = XNM*XAP + Y2
DM = XNM*XAM + Y2
23
SU = SU + EMN(I)*Y*(1./DP+1./DM)
SV = SV + EMN(I)*(XNP/DP*XNM/DM)

1C CONTINUE
IF(Y.GT.FI) GO TO 20
P=2.
IF(Y.EQ.FI) P=1.
BEGIN POLAR CONTRIBUTION
XP2=X*PI**2
EYP2=EXP(Y*PI**2)

15 CONTINUE
XY2=X*Y**2
SXY2=SIN(XY2)
CXY2=COS(XY2)
SXP2=SIN(XP2)
CXP2=COS(XP2)
EYX=EXP(Y2-X*X)
D = 1. - EYP2*(2.*CXP2-EYP2)
SU = SU + P*EYX*(CXY2-EYP2*(CXP2*CXY2-SXP2*SXY2))/C
SV = SV - P*EYX*(SXY2+EYP2*(SXP2*CXY2-CXP2*SXY2))/C

2C U=SU*Y*RTPI
V=SV*THETA*RTPI
IF(XX.LT.O.) V=-V
GO TO 5C

3C F=RTPI*Y
SU=1./*((1.+XC*XC)*F)
SV=SL*XC
GO TO 2C

4C CONTINUE
IF(XC.LT.1.4*THETA.LE..C09) WRITE(6,1G1) XD,THETA
1C1 FCPMTUh BAD,2G14.6)
This is expansion with H=C.5
Y2=Y*Y
D=PI*(X*X)+Y2)
SL=Y/C
SV=X/C
DC 45 I=2,10
AM=0.5*FLOAT(I-1)
XNP=X-AM
XNM=X+AM
DP=XNP*XNP+Y2
DM=XNM*XNM+Y2
SU = SU + EN2(I)*Y*(1./DP+1./DM)
SV = SV + EN2(I)*(XNP/DP*XNM/DM)

45 CONTINUE
SU=SL*O.5
SV=SV*O.5
IF(Y.GT.FIH) GO TO 2C
P=2.
IF(Y.EQ.FIH) P=1.
XP2=X*PI**2
EYP2=EXP(Y*PI**2)
GO TO 15

5C RETURN
END
Subroutine PSIPHI uses the technique of Matta and Reichel (ref. 12). The arguments and values are the same as for routine PSCH.

```
$IBFTC MATTA
C
FRCM MATTA+REICHEL MATH. COMP. P.340 APRIL 1971
C
H=1. , 11 TERMS (FOR COMPARISON)
C
SUBROUTINE PSIPHI(XX,TT,U,V)
DATA H/C.75/
DATA PI/3.14159265/ , RTPI/1.7724539/
DIMENSION ENH(9),FNH(9)
DATA FNH/2.25,20.25,36.,56.25,81.,110.25,144.,182.25/
DATA ENH/,56978283.,10539922.,63297154E-2.,1234098E-3.
* .7814854E-6.,1605228E-8.,10709232E-11,.23155228E-15,
 16310129E-19 /
DATA BOUND/.14248292E-1/
X=APS(XX)
TH=APS(TT)
T=1.C/TH**2
X2=X*X
C
START SERIES -- SET N=0 TERM
C
XP=1.0+X2
XN=1.0-X2
SU=C.5/XF
SV=SU
X24=4.0*X2
C
DC 1C N=1,9
FNHT=FNH(N)*T
DENCM=X24+(XN+FNHT)**2
TERM=EH(N)/DENOM
SU = SU + TERM*(XP+FNHT)
SV = SV + TERM*(XP-FNHT)
1C CONTINUE
C
SU=SU*2.C*H/RTPI
SV=SV*2.C*H/RTPI*X
C
START PCLE TESTS
C
IF(T.LT.ECUND) GOTO 30
RTT=5CRT(T)
EXPON=XN*0.25/T - PI/H/RTT
IF(EXPON.LT. (-34.)) GO TO 3C
ARG1=X*X*0.5/T
ARG2=PI*H/(H*RTT)
A=COS(ARG1)
B=SIN(ARG1)
C=EXP(-PI/(H*RTT)) - COS(ARG2)
D=SIN(ARG2)
TERM=RTPI/RTT*EXP(EXPON)/(C*C+D*D)
```

P1 = TERM*(A*C - B*D)  
C1 = TERM*(B*C + A*D)  
IF(T.NE.ECUND) GOTO 20  
P1 = P1**0.5  
C1 = C1**0.5  
20 CONTINUE  
SU = SL + P1  
SV = SV - Q1  
30 CONTINUE  
U = SU  
V = SV**2.0  
RETURN  
END
APPENDIX D

A SAMPLE DOPPLER BROADENING CROSS SECTION CODE

WHICH REQUIRES VALUES OF $\psi$ AND $\chi$

$IBFIC RP3TAP$

C

LOGICAL START
DIMENSION CATUM(12003)
DIMENSION CATUMS(4001,3)
EQUIVALENCE (DATUM(1),DATUMS(1,1))
DIMENSION TITLE(24), UG(150), DU(150)
DIMENSION GG(20)
DIMENSION EC(300), GAMN(300), GAMG(300), GAM(300), GAME(300)
DIMENSION SIGCD(300), SIGCF(300), SIGSC(300), SIGTO(300), CON3(300)
DIMENSION A(300), SIG1(300), SIG2(300), SIG3(300)
DIMENSION X(300), THETA(300), PSI(300), PHI(300)

C

CCM MC NFES, X, THETA, PSI, PHI

C

C

C

C

START= .TRUE.
NLNIT=1
REWIND NLNIT
CALL SKFILE(NUNIT)
BACKSPACE NLNIT
CONTINUE
IF(START) GC TO 111
C

FIND END OF THIS TAPE
C

PLT ON IC RECORD
WRITE(NUNIT) ID
C

WRITE GCCC STUFF
JWCRCS=3*NWCRCS
WRITE(NUNIT) DATUM
75 FCMAT(AE,4X,110)
76 FCMAT(1H1,A6)
77 FCMAT(1C2,3F13.4)
CONTINUE
START=.FALSE.
READ (5,50) (TITLE(M),M=1,24)
READ(5,75) ID,NWCRCS
READ (5,51) T,ANL,UKT,SIGCT,SIGFT,USTART,NRES,NDU
READ (5,53) SIGMAT,SIGPOT,G
READ (5,52) (UG(K),DU(K),K=1,NDU)
READ (5,57) (A(I),EO(I),GAMN(I),GAMG(I),GAME(I),I=1,NRES)
READ (5,71) NUMBG
READ (5,53) (GG(I),I=1,NUMBG)
READ(5,72) I2,I4,I6,I8
WRITE (6,54)
WRITE (6,50) (TITLE(M),M=1,24)
WRITE (6,55)
WRITE (6,56) T, ANU, UKT, SIGCT, SIGFT, SIGMAT, SIGPOT
DC 2 K=1, NCU, 52
IHI=PINO(NEU, K+51)
C NEW PAGE
WRITE (6, 54)
WRITE (6, 57)
WRITE (6, 58) (J, UT(J), DU(J), J=K, IHI)
C CCONTINUE
DC 2 I=1, NRES
Gam(I)=GAM(I)+GAMG(I)+GAME(I)
CCN1=(2.607E06/(GAM(I)**2))E*GAMN(I)
CCN2 =(A(I)+1.0)/A(I)
CCN3(I)=1.0/CCN2
AEC =AES(EC(I))
SIGCC(I)=(CCN1*GAMG(I)*CON2 **1.5)/SQRT(AEO)
SIGFC(I)=(GAME(I)*SIGCO(I))/GAMG(I)
SIGSC(I)=(CCN1*GAMN(I)*CCN2 **2)/AEO
SIGTC(I)=2.607E06*G*CAMN(I)/(AEO*GAM(I))
C CCONTINUE
DC 4 I=1, NRES, 52
IHI=PINO(NRES, I+51)
C NEW PAGE
WRITE (6, 54)
WRITE (6, 59)
WRITE (6, 60) (J, A(J), EO(J), GAMN(J), GAMG(J), GAME(J), J=I, IHI)
C CCONTINUE
DC 5 I=1, NRES, 52
IHI=PINO(NRES, I+51)
C NEW PAGE
WRITE (6, 54)
WRITE (6, 61)
WRITE (6, 62) (J, EO(J), SIGCO(J), SIGFO(J), SIGSO(J), SIGTO(J), J=I, IHI)
C CCONTINUE
WRITE (6, 55)
C NCCUNT=0
NTALLY=1
KJK=0
JJJ=0
C ET=EXP(-LKT)*1.0E07
DC 12 I=1, NRES
IF (KKK) 7, 7, 10
7 X(I)=(2.0*(ET-EO(I))*CON3(I))/GAM(I)
IF (T) 8, 8, 9
8 TCCF=0.0
GC TC 11
9 TCCF=293.0
GC TC 11
10 TCCF=T
11 THETAI = GAM(I)/CON3(I)*SQRT(A(I)/(TDOP*ABS(EO(I))*3.446E-04))
C CCONTINUE
14 CALL PSIFHI
IF (KJK) 25, 15, 25
15 SIGCTF=0.0
SIGFTP=0.0
ZECl=SQRT(ET)
DC 16 I=1, NRES
28
SIGCTP = SIGCTP + SIGCO(I) * PSI(I)
SIGFTP = SIGFTP + SIGFO(I) * PSI(I)

16 CONTINUE
SCV = SIGCT - SIGCTP / ZE01
SFV = SIGFT - SIGFTP / ZED1
AKC = SCV * ZEC1
AKF = SFV * ZEC1
WRITE (6,64) SCV, SFV
ABN = 0.0
DC 17 I = 1, NRES
ABN = ABN + A(I)
17 CONTINUE
SIGP = 0.27154671 * (ABN / FLOAT(NRES))**0.66666667
IF (SCV < 0.0.ANC.SFV < 0.0.C) GO TO 1
IF(I2) 19,19,18
18 SIGP = SIGFCT
GC TC 20
19 CONTINUE
WRITE (6,65) SIGP
IF (SIGP) 1,20,20
20 WRITE( 6,54)
WRITE( 6,66)
LA = 1
IF(I6) 22,22,21
21 E = USTART
U = 16.118C96 - ALOG(E)
GC TC 23
22 U = USTART
E = 1.0E07*EXP(-U)
23 DC 24 I = 1, NRES
24 X(I) = (2.0*CON3(I)/GAM(I)) * (E - EO(I))
KKK = KKK + 1
GC TC 6
C
25 SIGCN = 0.0
SIGFN = 0.0
SIGSN = 0.0
ZEC1 = SQRT(E)
DC 26 I = 1, NRES
ZILCH1 = SQRT(SIGSC(I))
ZILCH2 = PSI(I) * SQRT(G * SIGP * SIGSO(I))
ZILCH3 = PSI(I)
SIG1(I) = FH1(I) * ZILCH1
SIG2(I) = ZILCH2
SIG3(I) = ZILCH3 * ZILCH1
WCRK = ZILCH2 / CON3(I)
TEMP = SIGSC(I) * PSI(I)
SIGCN = SIGCN + SIGCC(I) * ZILCH3
SIGFN = SIGFN + SIGFC(I) * ZILCH3
SIGSN = SIGSN + SIGP
26 CONTINUE
SIGCN = (SIGCN + AKC) / ZEC1
SIGFN = (SIGFN + AKF) / ZEC1
SIGSN = SIGSN + SIGP
IF(I8) 30,30,27
27 SIGSN = SIGP
DC 29 I=1,NUMBG
SIGY1=0.
SIGY2=0.
SIGY3=0.
CC 28 J=1,NRES
IF (ABS(C-CG(I)) .GT. C .00001) GO TO 28
SIGY1=SIGY1+SIG1(J)
SIGY2=SIGY2+SIG2(J)
SIGY3=SIGY3+SIG3(J)
28 CONTINUE
SIGSN=SIGSN+0.25*SIGY1**2+SIGY2+SIGY3**2
29 CONTINUE
30 IF (SIGSN) 31,32,32
31 JJJ=1
32 SIGA=SIGCN+SIGFN
ANUSIG=ANU*SIGFN
C
IF (ACOUNT-54) 34,34,33
33 WRITE( 6,54)
WRITE( 6,66)
NCCLNT=G
34 WRITE( 6,68) NTALLY,U,E,SIGA,SIGSN,ANUSIG
I&WRC = &WCRDS-NTALLY + 1
NTALLY=NTALLY+1
NCCLNT=NCCLNT+1
DATLMS(I&WRC,1) = E
DATLMS(I&WRC,2) = SIGA
DATLMS(I&WRC,3) = SIGSN
C
IF(I6) 44,44,37
37 IF ((LG(LA)-U)-0.00001) 38,40,40
38 E=E-ELU(LA)
U=16.11896-ALOG(E)
GC TC 43
40 E=UCL(LA)
LA=LA+1
IF ((LG(LA)-U)-0.00001) 38,41,41
41 CONTINUE
IF(JJJ) 1,1,42
42 WRITE (6,54)
WRITE (6,70)
WRITE (18,70)
GC TC 1
C
44 IF ((LG(LA)-U)-0.00001) 47,47,45
45 U=U+ELU(LF)
E=1.0E07*EXP(-U)
46 CC NTINUE
CC 46 I=1,NRES
46 X(I) = '(2.0*CGN3(I)/CGM(I))*(E-EO(I))'
GC TC 14
47 U=LG(LA)
LA=LA+1
IF ((LG(LCU)-U)-0.00001) 48,48,45
48 CONTINUE
IF (JJJ) 1,1,49
C
50  FCRMAT (12A6)
51  FCRMAT (6F10.5,2F15)
52  FCRMAT (2F10.6)
53  FCRMAT (7F10.7)
54  FCRMAT (1H1)
55  FCRMAT (1H1)
56  FCRMAT (3X, 6HTEMP =F12.2, 3X, 4HNU =F6.3, 3X, 6HU KT =F8.4, 3X, 12HSIG C: 1AP KT =F10.4, 3X, 10HSIG F KT =F10.4, 3X, 9HSIG TOT =F1C.4/3X, 9HSIG PO 2T =F5.3)
57  FCRMAT (10X, 2H K, 7X, 3H UG, 11X, 3H DU)
58  FCRMAT (112, 2F13.5)
59  FCRMAT (1HJ/3X, 1HI, 15H ATOMIC WEIGHT, 3X, 1CHRES ENERGY, 6X, 7H GAMMA 1N, 7X, 7H GAMMA G, 7X, 7H GAMMA F)
60  FCRMAT (14, F14.3, F18.4, 3F14.8)
61  FCRMAT (4X, 1HI, 3X, 10HRES ENERGY, 5X, 5H SIGCO, 9X, 5H SIGFO, 9X, 5H SIGSO, 9X, 5H SIGTC)
62  FCRMAT (15, F13.4, 4F14.4)
63  FCRMAT (10X, 10HSIG C/V =, F12.4, 5X, 10HSIG F/V =, F12.4)
64  FCRMAT (1H /10X, 10HSIG POT = F12.4)
65  FCRMAT (6X, 1HK, 6X, 1HU, 11X, 1HE, 11X, 5H SIG A, 8X, 6H SIG ES, 7X, 8H NU SIG 1F)
66  FCRMAT (10X, F10.7, 10X, 4F10.7)
67  FCRMAT (17, 2X, F8.5, F13.5, 6F13.4)
68  FCRMAT (10X, 22HSIG S IS NEG AT SOME E)
69  FCRMAT (15)
70  FCRMAT (1X, 1X, 1X, 1X, 1X, 1X, 1X, 1X, 1X)
REFERENCES


5. Seth, Kamal K.; and Tabony, R. H.: A Tabulation of the Doppler Integrals $\psi(x, t)$ and $\varphi(x, t)$. AEC Rep. TID-21304, 1965.


"The aeronautical and space activities of the United States shall be conducted so as to contribute . . . to the expansion of human knowledge of phenomena in the atmosphere and space. The Administration shall provide for the widest practicable and appropriate dissemination of information concerning its activities and the results thereof."

— NATIONAL AERONAUTICS AND SPACE ACT OF 1958

NASA SCIENTIFIC AND TECHNICAL PUBLICATIONS

TECHNICAL REPORTS: Scientific and technical information considered important, complete, and a lasting contribution to existing knowledge.

TECHNICAL NOTES: Information less broad in scope but nevertheless of importance as a contribution to existing knowledge.

TECHNICAL MEMORANDUMS: Information receiving limited distribution because of preliminary data, security classification, or other reasons.

CONTRACTOR REPORTS: Scientific and technical information generated under a NASA contract or grant and considered an important contribution to existing knowledge.

TECHNICAL TRANSLATIONS: Information published in a foreign language considered to merit NASA distribution in English.

SPECIAL PUBLICATIONS: Information derived from or of value to NASA activities. Publications include conference proceedings, monographs, data compilations, handbooks, sourcebooks, and special bibliographies.

TECHNOLOGY UTILIZATION PUBLICATIONS: Information on technology used by NASA that may be of particular interest in commercial and other non-aerospace applications. Publications include Tech Briefs, Technology Utilization Reports and Technology Surveys.

Details on the availability of these publications may be obtained from:

SCIENTIFIC AND TECHNICAL INFORMATION OFFICE

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

Washington, D.C. 20546