THERMOCHEMISTRY OF TANTALUM-WALL COOLING SYSTEM WITH LITHIUM AND SODIUM WORKING FLUIDS

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Plots are presented which show the distribution of oxygen between liquid lithium and tantalum or niobium, and between liquid sodium and tantalum at elevated temperatures. Additional plots showing the composition of the gas phase above the solutions of oxygen and alkali metal are presented. The use of the plots is illustrated by an example tantalum heat pipe filled with lithium.
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SUMMARY

Plots are presented which show the distribution of oxygen between liquid lithium and tantalum or niobium, and between liquid sodium and tantalum at elevated temperatures. Additional plots showing the composition of the gas phase above the solutions of oxygen and alkali metal are presented. The use of the plots is illustrated by an example tantalum heat pipe filled with lithium.

INTRODUCTION

Liquid metals as heat-transfer media have been advocated for many applications. Some of the alkali liquid metals, in particular, have vapor-pressure and heat-transfer properties favorable for use in nuclear-reactor cooling systems (ref. 1).

Because of the elevated service temperatures and the high chemical reactivity of the alkali metals, difficult materials problems in the liquid-metal cooling systems will be encountered. A continuing review of such materials problems is being conducted here at the Lewis Research Center in support of an experimental study of heat pipes for removing nuclear-reactor thermal energy. In reference 2, published solubility data for oxygen in lithium and in sodium were used to construct chemical potential diagrams. The use of the diagrams in assessing the chemical stability of systems containing refractory metal, lithium, and oxygen is illustrated by an example involving hafnium, a possible constituent of the containment structure.

Both niobium and tantalum can hold large amounts of oxygen in solution (ref. 3). Oxygen exceeding about 200 to 500 parts per million in these metals is known to result in corrosive attack by the lithium through a little-understood mechanism (ref. 4). For this reason, caution must be exercised in removing oxygen from refractory metal by the method of leaching or soaking in alkali metals.

In this report, the chemical potential data for oxygen in lithium or in sodium (ref. 2) and data for oxygen in tantalum or in niobium (refs. 3 and 5) were used to estimate the
distribution of oxygen between lithium and niobium or tantalum. The information should be of use in estimating the effectiveness of methods proposed for leaching oxygen from tantalum or niobium and in setting limits on lithium purity for heat pipes.

The chemical potential diagrams from reference 2 are very tentative because of the uncertainties in the solubility-limit data and arbitrary assumptions used in their construction. The possible formation of a ternary oxide of refractory metal, alkali metal, and oxygen was not considered. Such oxides are suspected as important corrosion factors in refractory-metal–alkali-metal systems (refs. 6 and 7). Because of the importance of liquid-metal cooling systems to nuclear-reactor technology, thermochemical analyses such as the ones contained herein are required until more definitive experimental data are available.

**ANALYSIS AND DISCUSSION**

Reference 2 contains plots of the free-energy function

\[
\left( \frac{\Delta F_T}{RT} \right)_{O_2} = \frac{\left( F_T \right)_{O_2(g)} - \left( F_T^0 \right)_{O_2(g)}}{RT} = \ln p_{O_2}
\]

for gaseous diatomic oxygen \((O_2(g))\) in equilibrium with solutions containing varying mole fractions of dilithium oxide \((Li_2O)\) in lithium or disodium oxide \((Na_2O)\) in sodium at several temperatures \(T\). Here, \(F_T\) is the free energy at the equilibrium condition, \(F_T^0\) is the free energy at 1 atmosphere pressure, \(R\) is the gas constant, and \(p\) is the partial pressure in atmospheres (1 atmosphere = 1.013\times10^5 N/m^2).

For each liquid metal, two plots were presented in reference 2. In one plot, existing oxygen solubility data were used to determine the coefficient of a first-order term for departure from ideal solution behavior. The form of the expression for this nonideal behavior was essentially that of the regular solution (ref. 8). For the other plot, ideal solution behavior was assumed so that the sensitivity of the plots to the assumptions made in the analysis might be assessed. In the present report, only the plots for nonideal behavior derived from the oxygen solubility data will be used.

**Distribution of Oxygen Between Lithium and Tantalum or Niobium**

Reference 3 presents equations relating the concentration of oxygen dissolved in niobium \((Nb)\) and tantalum \((Ta)\) to temperature and \((\Delta F_T/RT)_{O_2}\) (eq. (1)) at equilibrium. For oxygen in niobium,
\[
\left( \frac{\Delta F_T}{RT} \right)_{O_2} = 21.2 + \ln x_{O(Nb)}^2 - \frac{90300}{T}
\]  
(2)

and for oxygen in tantalum,

\[
\left( \frac{\Delta F_T}{RT} \right)_{O_2} = 21.2 + \ln x_{O(Ta)}^2 - \frac{89800}{T}
\]  
(3)

where \( x_{O(Ta, Nb)} \) is the atomic fraction of oxygen in the refractory metal indicated.

Lines of \( (\Delta F_T/RT)_{O_2} \) for tantalum at fixed \( x_{O(Ta)} \) are superimposed in figure 1 upon a plot from reference 2 \( (\Delta F_T/RT)_{O_2} \) against \( x \) and \( T \) for \( Li_2O \) in lithium. Here, \( x \) is the mole fraction of \( Li_2O \) in lithium. Lines of \( (\Delta F_T/RT)_{O_2} \) for niobium (eq. (3)) lie very close to those for tantalum and are not shown. For any temperature and concentration \( x_{O(Ta)} \) of oxygen in tantalum, the mole fraction \( x \) of \( Li_2O \) in solution with Li is read on the abscissa. The ordinate then gives values of the equilibrium diatomic oxygen partial pressure \( p_{O_2} \) through equation (1).

In figure 2, the data of figure 1 are replotted as lines of constant temperature, with \( x_{O(Ta)} \) as the ordinate. Also shown in figure 2 are lines for niobium, rather than tantalum, in contact with the alkali metal, in which case the ordinate is interpreted as \( x_{O(Nb)} \).

Figure 2 illustrates the gettering capability of lithium for oxygen. For equilibrium at 1800 K, the ratio of oxygen in tantalum to that in lithium is about \( 10^{-3} \). At 1300 K, the ratio of oxygen in tantalum to that in lithium is about \( 10^{-5} \).

In reference 9, some isolated theoretical and experimental values of the ratio of oxygen in refractory metals to oxygen in alkali metals (distribution coefficient) are presented. For the system Ta - O - Li at 800° C (1073 K), a value of \( 3 \times 10^{-8} \) is calculated, which is essentially in agreement with figure 2, while the experimental value estimated from corrosion studies is listed as 0.1. If the theoretical value were actually encountered in practice, its observation would require the measurement of less than \( 3 \times 10^{-5} \) parts per million of oxygen by weight in tantalum. Such a task would, no doubt, prove impossible. In fact, the theoretical and experimental values for the refractory-metal - alkali-metal combinations in reference 9 are only in reasonable agreement when the distribution coefficient differs from unity by less than about 2 orders of magnitude and is thus amenable to experimental determination.
Distribution of Oxygen Between Sodium and Tantalum

Figure 3, from reference 2, is a plot of \((\Delta F_T/RT)_{O_2}\) against \(x\) at various temperatures for \(\text{Na}_2\text{O}\) in sodium. Lines of constant \(\chi_{O(Ta)}\) (eq. (2)) are also plotted in figure 3. The lines of constant \(\chi_{O(Ta)}\) for \(\text{Ta} - \text{O} - \text{Na}\) in figure 3 have an entirely different trend than those for \(\text{Ta} - \text{O} - \text{Li}\) in figure 1. Also, for given \(\chi_{O(Ta)}\) they are located at far lower concentrations \(x\) of alkali metal oxide in alkali metal. The data are replotted in figure 4 as lines of constant \(T\) with \(\chi_{O(Ta)}\) as the ordinate and \(\chi_{O(Na)}\) as the abscissa. For equilibrium from 800 to 1600 K, the ratio of oxygen in tantalum to that in sodium is about \(10^{-2}\). The gettering capability of sodium for the oxygen in tantalum is thus poorer than that of lithium by a factor of \(10^2\) to \(10^3\). This result is consistent in direction with the measured heats of formation of the compounds \(\text{Na}_2\text{O}\) and \(\text{Li}_2\text{O}\) (ref. 8).

Vapor Composition

The foregoing analysis has been concerned only with the liquid lithium or sodium phase and the solid tantalum or niobium phase. In many real situations, a gas phase of appreciable volume may also be present. The elemental composition for the vapor will generally differ from that for the solid phases. In the operation of systems such as heat pipes, a fractional distillation of the components of the condensed phase will have to be considered. In addition, if the vapor volume is very large relative to the volume of condensed phases, an accurate inventory of material in the system should include the species in the gas phase.

Any species \(j\) in the vapor phase can be expressed in terms of oxygen, refractory metal, and alkali metal atoms by a general formula typified for the \(\text{Ta} - \text{O} - \text{Li}\) system by \(\chi_{O(j)}\) \(\chi_{\text{Li}(j)}\) \(\chi_{\text{Ta}(j)}\). Thus in \(\text{Li}_2\text{O}\), \(\chi_{O(\text{Li}_2\text{O})} = 1\), \(\chi_{\text{Li}(\text{Li}_2\text{O})} = 2\), and \(\chi_{\text{Ta}(\text{Li}_2\text{O})} = 0\). The density of any species \(j\) in the gas phase, by the ideal gas law, is

\[
\rho_j = \frac{p_j M_j}{RT}
\]

where \(R\) is the universal gas constant in suitable units, and \(M\) is the molecular weight of species \(j\). The contribution of species \(j\) to the total oxygen density is

\[
\rho_{O(j)} = \chi_{O(j)} \rho_j \frac{M_O}{M_j}
\]

the contribution to the lithium density is
and the contribution to the tantalum density is

\[ \rho_{Ta(j)} = n_{Ta(j)} \rho(j) \frac{M_{Ta}}{M_j} \] (7)

The total oxygen density is then

\[ D_O = \sum_j \rho_{O(j)} \] (8)

the total lithium density is

\[ D_{Li} = \sum_j \rho_{Li(j)} \] (9)

and the total tantalum density is

\[ D_{Ta} = \sum_j \rho_{Ta(j)} \] (10)

The sums are over all species \( j \) in the gas phase.

Combination of equations (5) to (10) yields

\[ D_O = \frac{M_O}{RT} \sum_j n_{O(j)} p_j = \frac{M_O P_O}{RT} \] (11)

\[ D_{Li} = \frac{M_{Li}}{RT} \sum_j n_{Li(j)} p_j = \frac{M_{Li} P_{Li}}{RT} \] (12)

and

\[ D_{Ta} = \frac{M_{Ta}}{RT} \sum_j n_{Ta(j)} p_j = \frac{M_{Ta} P_{Ta}}{RT} \] (13)

where the effective partial pressures of oxygen, lithium, and tantalum are
\[ P_O = \sum_j n_{O(j)} p_j, \quad P_{Li} = \sum_j n_{Li(j)} p_j, \quad \text{and} \quad P_{Ta} = \sum_j n_{Ta(j)} p_j, \]
respectively. For \( P \) in torr (1 torr = 1.333 \times 10^2 \text{ N/m}^2), D in grams per cubic centimeter, M in gram atomic weights, and T in degrees Kelvin, \( R = 62.363 \text{ (torr)(cm}^3)/(\text{mole})(\text{K}) \).

The evaluation of the set of equations (4) and (5) involves first the specification of \( x \) and \( T \). Figures 1 and 3 or the computations leading thereto furnish \( p_{O_2} \). From reference 2, the following expression for the partial pressure of the alkali metal \( M(M=\text{Li, Na}) \) above a liquid solution of the metal and its oxide \( M_2O \) can be obtained:

\[ \ln p_M = \ln p_{M(\ell)} + \ln(1 - x) + Bx^2 \quad (14) \]

where \( p_{M(\ell)} \) is the vapor pressure of pure liquid. Values of \( p_{M(\ell)} \) for Li and Na are available from reference 8.

With \( p_M \) and \( p_{O_2} \) known, the remaining pressures required are given by

\[ p_O = K_O \sqrt{p_{O_2}} \quad (15) \]

\[ p_{MO} = K_{MO} p_M \sqrt{p_{O_2}} \quad (16) \]

\[ p_{M_2} = K_{M_2} p_M^2 \quad (17) \]

\[ p_{M_2O} = K_{M_2O} p_M^2 \sqrt{p_{O_2}} \quad (18) \]

where the equilibrium constants \( K \), with the exception of \( K_{Li_2O} \), are from reference 8. In computing \( K_{Li_2O} \), the free-energy data for \( \text{Li(g)} \) and \( \text{Li}_2\text{O(g)} \) were from reference 10, while those for \( \text{O}_2 \) were from reference 11. For gaseous tantalum-bearing species, the partial pressures in atmospheres are (from ref. 3)

\[ p_{TaO} = 1.74 \times 10^6 \sqrt{p_{O_2}} \exp \frac{-21414}{T} \quad (19) \]

and

\[ p_{TaO_2} = 1.35 \times 10^6 \sqrt{p_{O_2}} \exp \frac{-11513}{T} \quad (20) \]
where \( p_{TaO} \) and \( p_{TaO_2} \) are in torr (1 torr = 1.333 N/m\(^2\)) and \( p_{O_2} \) is in atmospheres (1 atm = 1.013\( \times \)10\(^5\) N/m\(^2\)).

With the use of equations (4) to (20), \( p_{O_2} \) from figure 1, and \( B = 1.835 \) (from ref. 2), computations of \( P_{Li} \), \( P_{O} \), and \( P_{Ta} \) were made for the system Ta - O - Li. Figure 5 shows \( \log_{10} P_O \) and \( \log_{10} P_{Li} \) against \( x \) for several temperatures. For all conditions of \( T \) and \( x \) shown in figure 5, \( P_O \) was greater than \( P_{Ta} \) by a factor of \( 10^8 \) and, therefore, \( P_{Ta} \) is not shown.

Figure 6 shows \( \log_{10} P_O \) and \( \log_{10} P_{Na} \) against \( x \) at several temperatures for the system Ta - O - Na, computed with the use of \( B = 2.0 \) (from ref. 2) and \( p_{O_2} \) from figure 2. For the conditions of \( T \) and \( x \) shown in figure 6, \( P_O \) was greater than \( P_{Ta} \) by a factor of \( 10^3 \) or more. No data for the molecule \( Na_2O(g) \) appear in reference 10, and computations have suggested that this molecule does not exist (ref. 12). The species \( Na_2O(g) \) was, therefore, not included in the sums \( P_O \) and \( P_{Na} \).

Figures 2 and 5, or 4 and 6, suffice for determination of the distribution of total alkali metal and oxygen between the condensed and gaseous phases. The total inventory of tantalum, alkali metal, and oxygen must be specified, together with the gas volume \( V_g \). For instance, suppose a system contains \( N_{Li} \) moles of lithium and \( N_O \) moles of oxygen in all phases,

\[
N_{Li} = \left[ 1 - x_{O(Li)} \right] N_s + \frac{V_g P_{Li}}{RT} \tag{21}
\]

\[
N_O = x_{O(Li)} N_s + \frac{V_g P_O}{RT} + N_{Ta} x_{O(Ta)} \tag{22}
\]

where \( x_{O(Li)} \) is the atomic fraction of oxygen in solution, and \( N_s \) is the moles of solution containing oxygen and lithium. Elimination of \( N_s \) between equations (21) and (22) gives

\[
N_O = \left( N_{Li} - \frac{V_g P_{Li}}{RT} \right) \frac{x}{1 + x} + \frac{V_g P_O}{RT} + N_{Ta} x_{O(Ta)} \tag{23}
\]

where the atom fraction \( x_{O(Li)} \) of oxygen in solution has been replaced by \( x \), the equivalent mole fraction of \( Li_2O \) in solution. For any specified \( N_O \), \( N_{Li} \), \( N_{Ta} \), \( V_g \), and \( T \), an iteration involving figures 2 and 5, with the constraint of equation (23) imposed, yields \( x \), \( x_{O(Ta)} \), \( P_{Li} \), and \( P_O \). In most practical cases, the following initial assumptions can be made, which greatly simplify the solution and render an iteration unnecessary:
\[ N_{Li} \gg \frac{V_g P_{Li}}{RT} \]
\[ N_{O} \gg \frac{V_g P_{O}}{RT} \]
\[ N_{O} \gg N_{R} x_{O(Ta)} \]

For example, consider a tantalum-walled heat pipe operating at 1600 K, with 1.02-centimeter (0.4-in.) outer diameter and 0.102-centimeter (0.04-in.) wall. A tantalum screen of 0.71-centimeter (0.280-in.) outer diameter and 0.018-centimeter (0.007-in.) thickness with 50-percent open volume is inside. The entire passage between screen and tube, as well as the pores of the screen, is filled with lithium. The length of the pipe is sufficient to permit the tantalum in the end caps to be neglected. Assume 1000 parts per million of oxygen by weight in the system. Then, per centimeter of length, \( N_{O} = 3.28 \times 10^{-4} \) gram atomic weight of O, \( N_{Li} = 1.09 \times 10^{-2} \) gram atomic weight of Li, \( N_{Ta} = 2.85 \times 10^{-2} \) gram atomic weight of Ta, and \( V_g = 0.81 \) cubic centimeters.

If the conditions specified in the inequalities (24) are assumed, equation (23) yields \( x \approx 3.01 \times 10^{-2} \). From figure 2, \( x_{O(Ta)} \approx 4.5 \times 10^{-6} \), and from figure 5, \( P_{Li} \approx 740 \) torr, and \( P_{O} \approx 3.4 \times 10^{-3} \) torr. Conditions (24) are therefore satisfied. From equations (11) and (12), \( D_{Li} = 5.5 \times 10^{-5} \) gram per cubic centimeter, and \( D_{O} = 5.5 \times 10^{-10} \) grams per cubic centimeter.

**CONCLUDING REMARKS**

The distribution of oxygen between liquid lithium and tantalum or niobium, and between liquid sodium and tantalum at high temperature was shown. The composition of the gas phase above solutions of oxygen and alkali metal were presented. The plots were used in an example concerning a tantalum heat pipe filled with lithium. The plots are tentative because of uncertainties in the experimental data used in their construction. The importance of liquid-metal cooling systems to nuclear-reactor technology requires the use of such analyses as the one herein until better experimental data are obtained.

Lewis Research Center,
National Aeronautics and Space Administration,
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503-05.
REFERENCES


Figure 1. Chemical potential diagram for Li-Li₂O solution in equilibrium with tantalum containing dissolved oxygen.

Figure 2. Equilibrium distribution of oxygen between liquid lithium and solid tantalum or niobium at several temperatures.
Figure 4. - Equilibrium distribution of oxygen between liquid sodium and tantalum at several temperatures.

Figure 3. - Chemical potential diagram for Na-Na₂O solution in equilibrium with tantalum containing dissolved oxygen.
Figure 5. - Effective partial pressures of the oxygen and lithium in the vapor above solutions of oxygen and lithium.
Figure 6. - Effective partial pressures of the oxygen and sodium in the vapor above solutions of oxygen and sodium.
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