TO: KSI/Scientific & Technical Information Division  
Attention: Miss Winnie M. Morgan

FROM: GP/Office of Assistant General Counsel for Patent Matters

SUBJECT: Announcement of NASA-Owned U.S. Patents in STAR

In accordance with the procedures agreed upon by Code GP and Code KSI, the attached NASA-owned U.S. Patent is being forwarded for abstracting and announcement in NASA STAR.

The following information is provided:

U.S. Patent No. : 3,395,565

Government or Corporate Employee :
National Research Corporation
Cambridge, MA

Supplementary Corporate Source (if applicable) :

NASA Patent Case No. : XGS-07752

NOTE - If this patent covers an invention made by a corporate employee of a NASA Contractor, the following is applicable:  
Yes [X]  No 

Pursuant to Section 305(a) of the National Aeronautics and Space Act, the name of the Administrator of NASA appears on the first page of the patent; however, the name of the actual inventor (author) appears at the heading of column No. 1 of the Specification, following the words "... with respect to an invention of ... ."

Elizabeth A. Carter
Enclosure
Copy of Patent cited above
Aug. 6, 1968

F. J. BROCK ET AL

3,395,565

GAUGE CALIBRATION BY DIFFUSION

Filed March 11, 1966

3 Sheets-Sheet 1

TO VACUUM SYSTEM
(<10^-10 mm. Hg.)

FIG. 1

3,395,565

FIG. 2

FIG. 4

VACUUM CHAMBER

PUMP

THERMAL VALVE

HYDROGEN SUPPLY

HYDROGEN SUPPLY
CERAMIC INSULATORS

GOLD-NICKEL BRAZE

TUBULAR CERAMIC FEED-THROUGHS

THERMOCOUPLE LEADS

CALIBRATION GAS

FIG. 5

FIG. 5a
Vacuum Society standards as pressure on the order of
where \( C \) is the conductance of the con-
Q = \( \frac{C}{P_0} (P_0 - P_0) \)

lignment or auxiliary equipment, such as power supplies,
to malfunctioning of the gauge itself and/or malfunc-
both relative and absolute senses. An unknown gauge may
be compared with a previously calibrated gauge and the
from the gauge volume. Equation 1 may be transposed to
estab-
of ambient gas density. A gauge which was calibrated
less than this figure. As another instance, a space vehicle
material under vacuum are under study, the experimenter
controls, cables, or read-out apparatus. In addition, sur-
face effects within the gauge may cause serious depu-
tures from correct pressure sensitivity. If this calibration
is largely dependent in the development of a method of
producibility and not jeopardize the pressure measurements
during periods when calibration is not required.
procedure outlined above
be reliably and accurately.
objective to reduce the size and amount of apparatus required for gauge calibra-
consistent with the foregoing objects.
object of the invention to provide a large number of calibration cycles (as opposed to a
 calibration consistent with the foregoing objects.
it is another object of the invention to provide a calibration unit in which the effects of calibration are quickly
dissipated so that the gauge can resume pressure measurements quickly, consistent with the foregoing objects.
these objects are met by diffusing a stored calibration gas through a permeable barrier in a “thermal
which is activated by heating. When inactive, the valve essentially prevents loss of gas to the
gauge. We have found that this approach results in reproducible and accurate measurements and that it is
suitable to use with ultrahigh vacuum systems on the
or in space vehicles.
method and apparatus for calibration of ultrahigh vacuum
gauges and an improved gauge with a built-in calibrator.
for a fuller understanding of the invention, reference
should be had to the following detailed description of a preferred embodiment in which the effects of calibration are quickly
conjunction with the accompanying drawings wherein:
FIG. 1 is a diagrammatic view of a calibration appara-
tus and a gauge to be calibrated;
FIG. 2 shows a second embodiment of the apparatus;
FIG. 3 shows an operating curve for the calibration of
FIG. 2;
FIG. 4 shows a modified calibrator-gauge arrangement;
FIG. 5 shows another embodiment of the thermal valve
used in the calibrator; and FIG. 5A is a detail from
FIG. 5.
The invention accordingly comprises an improved
method and apparatus for calibration of ultrahigh vacuum
gauges and an improved gauge with a built-in calibrator.
pressure within the gauge envelope by
controlling the rate of flow of a gas into and out of the
gauge volume. For instance, when the gauge is being used
for pressure measurement, calibration gas would not be
added to the system and the system pressure will be some
base pressure \( P_0 \). For calibration, gas is added to the
gauge volume at a flow rate \( Q \). The pressure \( P_0 \)
established in the gauge is then related to \( Q \) by the Equation 1:
where \( C \) is the conductance of the con-
duct which controls the rate at which the gas is removed
from the gauge volume. Equation 1 may be transposed to
give:

\[
P_0 = \frac{Q}{C} \left( P_0 - P_0 \right)
\]

Consequently, by regulating the ratio \( Q/C \), the gas
downstream may be brought to any desired value for
the required \( P_0 \) may be increased such that \( P_0 \)
is negligible compared to \( P_0 \).

In principle the method of calibration may be used in
both relative and absolute senses. An unknown gauge
may be compared with a previously calibrated gauge and the
above procedure used to establish the value of \( Q/C \).
the tube diameter and/or length. The function of the exit orifice is to allow a pressure rise at the gauge due to the admission of calibration gas through the thermal valve.

The design of the system is determined by the limits imposed through pumping action inherent in all ultrahigh vacuum systems and outgassing of the gauge and calibrating system. It has been shown in the art that the outgassing rate of a small glass system baked to 400°C for 8 hours can be reduced to below \(10^{-12}\) torr \(1\) cm.\(^2\) sec. The pumping speed of gauges is on the order of 0.1 to 1.0 liters per second.

In FIG. 1 of the drawings, the gauge to be calibrated is shown at 10. The gauge is connected through a tube 12 to a vacuum system whose pressure is to be measured by the gauge. With the gauge properly calibrated, the pressure measured at the gauge will be directly proportional to the true pressure in the vacuum system or equal to it if gas flow rates from leaks, outgassing, gauge pumping, and other extraneous sources are negligible. Within the tube is an exit orifice 14. A source 16 of calibration gas is connected to the tube to feed calibration gas to the gauge volume. The source comprises a branch tube 18 within which is disposed a permeable metal tube 20. The tube 20 is connected to a supply of calibration gas which may be as simple as a gas bottle and a valve.

The tube 20 constitutes a "thermal valve" since it only has a substantial permeability when heated. A preferred material for this purpose is stainless steel when hydrogen is the calibration gas. However, other materials such as nickel or palladium —25 silver alloy may be used for this purpose.

A heater 22 is provided within the thermal valve and connected to a 5 watt power supply 24. The leads of the heater are 26 and 28. A thermo-couple 30 is connected to the lead 28. The tube 20 is brazed to the lead 28 to form a vacuum tight enclosure for the calibration gas. An alumina insulator tube surrounds the heater. R.F. coils 34 are wound around the gauge and branch tube 18 for degassing heating.

**Example 1**

A calibrator was built as described above and attached to a Notthingham gauge. The vacuum system comprised a cold trap and diffusion pump which were capable of producing pressures below \(10^{-20}\) m.m. Hg. The tube 20 of the thermal valve was constructed of a stainless steel tube .077 inch outer diameter and .005 inch wall thickness.

The internal diameter of the tube 12 was 1.0 in. and its length was 5 in. The exit tubulation and the orifice 14 and a conductance of 131./sec, for nitrogen at 300° K.

The gauge was pumped to an initial pressure of \(4\times10^{-10}\) torr. Then the heater was operated at .37 watts for 60 seconds. The pressure in the gauge volume rose to 8.5 \(\times 10^{-10}\) torr and then recovered to the initial pressure after termination of heating. The heating was again conducted for 60 seconds at a lower level of .96 watts and the gauge pressure reading went up to an apparent pressure of \(3.5 \times 10^{-10}\) torr. The gauge recovered to the initial low pressure when heating was stopped.

The above recoveries of low pressures are attainable in watts and the gauge pressure reading went up to an approximate pressure of \(3.5 \times 10^{-10}\) torr. The gauge recovered to the initial low pressure when heating was stopped.

**Example 2**

The thermal valve of the above gauge was heated at 400°C for 24 hours. There was no change in permeation rate. The permeation rate appears to be reproducible and a function of temperature only (for a constant hydrogen pressure in the diffuser).

**Example 3**

The thermal valve was heated several times to 450°C in pulses of 3 to 5 minute periods to find if the maximum pressure in the gauge could be increased by several orders of magnitude. The pressure attained was \(10^{-8}\) torr.

The choice of calibration gas and thermal barrier will depend on the calibration pressure selected and the system under investigation. Some of the feasible calibration couples are:

<table>
<thead>
<tr>
<th>Gas</th>
<th>Barrier</th>
</tr>
</thead>
<tbody>
<tr>
<td>Hydrogen</td>
<td>Stainless steel</td>
</tr>
<tr>
<td>Oxygen</td>
<td>Silver</td>
</tr>
<tr>
<td>Nitrogen</td>
<td>Molybdenum</td>
</tr>
<tr>
<td>Carbon monoxide</td>
<td>Iron</td>
</tr>
<tr>
<td>Helium</td>
<td>Quartz or glass</td>
</tr>
</tbody>
</table>

If large throughputs are desired, suitable couples are:

<table>
<thead>
<tr>
<th>Gas</th>
<th>Barrier</th>
</tr>
</thead>
<tbody>
<tr>
<td>Hydrogen</td>
<td>Nickel</td>
</tr>
<tr>
<td>Hydrogen</td>
<td>25% silver — 75% palladium alloy</td>
</tr>
</tbody>
</table>

In using (6) care should be observed because of the possibility of embrittlement of the nickel. Couple (7) is relatively free of the problem.

The danger of contamination can be minimized in (6) or (7), or any of the other combinations, by using a high purity calibration gas supply or by inserting a purifier upstream of the thermal valve. For instance, if the gas is hydrogen, a palladium wall is a very effective purifier. If the gas is argon, it can be passed over active uranium chips upstream of the thermal valve.

In some instances, a calibration point less than an order of magnitude below the low point is satisfactory and even desirable. A typical calibration couple for this purpose would be any of (1)–(7) above or:

<table>
<thead>
<tr>
<th>Gas</th>
<th>Barrier</th>
</tr>
</thead>
<tbody>
<tr>
<td>Hydrogen</td>
<td>Copper</td>
</tr>
</tbody>
</table>

The volume of the barrier material and selection of barrier material should not provide such a high outgassing rate as to impose significant errors on the pressure reading in either the active or inactive conditions of operation of the thermal valve. Typical dimensions are given in the above examples.

It is a common characteristic of all the suitable calibration couples that the gas moves through the thermal valve in a sub-molecular form (e.g. hydrogen ions through the stainless steel or copper, helium atoms through the quartz). It is also a common characteristic of the preferred calibration couples that they have high activation energy and show a rapid rise in permeation rate with temperature. Consequently, the pressure in the calibration volume becomes a strong function of temperature. Relatively large increases in pressure may be obtained with small temperature increases and hence small power inputs. In general, a high activation energy for a couple is associated with a low diffusion coefficient. Hence, thinner walled tubing with small mass may be used to obtain the same gas throughput. The thinner walled tubing then requires less heat to raise to a required temperature. The preferred range of free energy of activation is greater than 10 kilocalories per gram-atoms as a lower limit and about 30 kilocalories per gram-atoms as an upper limit.

A couple of hydrogen-palladium is undesirable partly because of its high permeation rate, as indicated by a free energy of activation of 10, but mostly because of its slow temperature response and vulnerability to poisoning of the palladium. Couples within the above-stated range are suitable in terms of temperature response and structural stability.
through a high carbon stainless steel diffuser. A plate 319 is made of OFHC copper (typical dimensions 1/4" x 1/4" x 0.016") and is brazed onto the high temperature region of the diffuser to insure that the diffuser tube portion where permeation occurs is isothermal. The exterior of the diffuser was vacuum coated with gold (thickness in excess of 1000 A.), except for the portion 121 where permeation is desired. The gold coating prevents significant permeation in other regions.

The thermal valve of the second embodiment was degassed by heating to about 650° C. by radio frequency and resistance methods. After degassing, permeation experiments were run. A typical trace is shown in FIG. 3. As shown in the drawing, the behavior of the diffuser is repeatable from one run to the next. The diffusion rate is not altered by many runs. Pulsing from the range between 10⁻¹⁰ to 10⁻¹⁴ torr; up to 1 x 10⁻¹³ or 1 x 10⁻⁴ is readily attained. The operator can control the desired final pressure to within 1% by control of diffuser heating.

Typically, pulsing to 1 x 10⁻¹³ torr has been done from initial conditions of 2.2 to 10⁻¹⁰ torr, with the diffuser at 50° C. by running the diffuser heater at 15 volts and 0.3 ± 0.22 amperes for 40-50 seconds, causing the resistance into the series with the heater and continuing the heating for 10 seconds. Cooling to 50° C. resulted in a pressure of 2.3 x 10⁻¹⁰ torr pressure. This was accomplished in 13.75 minutes after heating was stopped.

Another embodiment is shown in FIG. 4. This shows the calibration technique of the invention adapted for use with a gage mouth. A gage mouth indicated at 310 and comprises the usual electrodes (e.g., cathode 210F, anode 210A and collector 210C) mounted from a flange 211. Also mounted from the flange is a baffle plate 213. By passing through the flange is a tubular passage 215. The hydrogen supply and thermal valve are connected to the passage 215 so that it serves as a tubular outlet for the calibration gas. The baffle 213 is arranged in line of sight relation to the outlet 215 and normal to the path provided by the tubular passage 215 to reflect gases back with a specific distribution, preferably a cosine distribution, aimed primarily at the gauge 210. With this geometry, calibration gas introduced via valve 16 and outlet 215 can be accurately measured by the gauge 210. This arrangement does away with the need for an existent calibration port found in the embodiments of FIGS. 3 and 5.

The baffle 213 should be adjacent the gauge 210 and it is preferably flat, but curved shapes may be employed. Another embodiment of the thermal valve is shown in FIGS. 5 and 5A. As in the previous embodiments, the vacuum manifold 315 is made of OFHC copper (typical dimensions 1/4" x 1/4" x 0.016") and is brazed onto the high temperature region of the manifold. A Kovar tube 317 surrounds the leads and tube and may be mated to a branch tube 318 of an ultra-high vacuum gauge by a conventional glass-Kovar seal.

The manifold 315 is isolated from the ultra-high vacuum conditions prevailing within the encapsulated tube 317/318. The elongated annular passage between tube 317 and skirt 319 provides an effective way of removing those gasses which do permeate through the lower portion of tube 318. The net result is a high sensitivity thermal valve.

It will be apparent that other embodiments can be made within the scope of our invention. It is therefore intended that the above description and accompanying drawing shall be read as illustrative and not in a limiting sense.

What is claimed is:

1. An improved method of calibrating a vacuum gauge, or the like, which is connected to a vacuum pumping means, the method comprising the steps of storing a calibration gas upstream of a diffusion barrier at a pressure above the vacuum region, placing the downstream side of the barrier in communication with the gauge to be calibrated, the calibration gas and barrier materials having an effective free energy of activation greater than 10 kilocalories per gram per atom and less than about 30 kilocalories per gram per atom, and intermittently heating the barrier to a known temperature to increase the rate of permeation to raise the pressure in the gauge by a known amount for brief calibration periods for comparison with the gauge's pressure reading.

2. The method of claim 1 wherein the gas is hydrogen and the barrier is stainless steel.

3. The method of claim 1 wherein the gas is helium and the barrier is selected from the group consisting of quartz, silica and glass.

4. The method of claim 1 wherein the gas is nitrogen and the barrier is molybdenum.

5. The method of claim 1 wherein the gas is oxygen and the barrier is silver.

6. The method of claim 1 wherein the gas is carbon monoxide and the barrier is iron.

7. The method of claim 1 wherein the gas is hydrogen and the barrier is copper.

8. The method of claim 1 wherein the calibration gas is selected to diffuse through the gas in sub-molecular form and wherein the barrier is selected to sufficiently block flow of gas molecules when cool to provide a permeation rate Q in torr liters per second, which is less than the product PC where P is said lower limit of the gauge and wherein C is the conductance from the gauge to the said pumped region.

9. A predictable gas source apparatus for use in vacuum gauge calibration and the like comprising in combination: means defining a closed volume; means for connecting a device such as a gauge or the like which is to utilize a supply gas admitted to the closed volume at a known pressure to said closed volume; means defining an exit orifice from said closed volume; means defining a thermal valve connected to said closed volume; means for storing a gas supply on the side of said valve away from the closed volume and means for heating the thermal valve to a known temperature to provide a predetermined flow rate of said gas into the volume with said flow rate and known flow and pressure characteristics of said volume and exit means providing said predetermined pressure in the volume.

10. The apparatus of claim 9 further comprising a vacuum pump wherein the exit orifice means places the apparatus in communication with said vacuum pump.

11. The apparatus of claim 9 wherein the thermal valve comprises a stainless steel tube.

12. The apparatus of claim 9 in an improved ultra-high vacuum enclosed gauge-gauge calibrator combination wherein the said device comprises an enclosed gauge;
the gauge being connected to said volume through a passage which bypasses said closed volume exit; the said thermal valve means being in said passage.

13. The apparatus of claim 12 wherein the thermal valve is a metal tube with an internal electric heater, the tube forming a portion of one of the leads for the electric heater.

14. The apparatus of claim 12 wherein a portion of the thermal valve structure is coated with a material having a lower constant of diffusion than the barrier material.

15. The improved ultra-high vacuum gauge-gauge calibrating combination of claim 14 wherein the gauge comprises a nude gauge mounted on a flange.

16. The apparatus of claim 15 wherein the said passage means comprises a tubular outlet into the gauge region, the apparatus further comprising a baffle mounted adjacent the gauge, the baffle being constructed and arranged as a line of sight target with respect to said tubular outlet and the baffle also being constructed and arranged to reflect incident molecules with a specific distribution aimed at the gauge.

17. The apparatus of claim 16 wherein the specific distribution is a cosine distribution.

18. A thermal valve assembly for ultra-high vacuum gauge calibration apparatus and the like comprising a source of gas, a closed permeation tube leading from said gas source into an ultra-high vacuum region, a heater located within said tube at the end of the tube away from the gas source to define a thermal valve element at said end, passage forming means surrounding the tube between the heater and gas source, the passage forming means having an exit at a point thereof remote from the heater, a vacuum pump connected to said exit, means on said tube in proximity to the heater for maintaining constant temperature along the region of the tube surrounding the heater, a thermocouple junction for measuring the temperature of the tube in proximity to the heater and thermocouple leads leading from said junction to feed-throughs in the thermal valve assembly, and means for removing gas from all exterior portions of the thermal valve assembly remote from the desired diffusion area near the heater.

References Cited

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DAVID SCHOENBERG, Primary Examiner.
N. B. SIEGEL, Assistant Examiner.