TO: KSI/Scientific & Technical Information Division  
Attention: Miss Winnie M. Morgan  
FROM: GP/Office of Assistant General Counsel for Patent Matters  
SUBJECT: Announcement of NASA-Owned U.S. Patents in STAR

In accordance with the procedures agreed upon by Code GP and Code KSI, the attached NASA-owned U.S. Patent is being forwarded for abstracting and announcement in NASA STAR. The following information is provided:

U.S. Patent No. : 3,310,699
Government or Corporate Employee : National Research Operation, Cambridge, MA
Supplementary Corporate Source (if applicable) :
NASA Patent Case No. : LAR-02743

NOTE - If this patent covers an invention made by a corporate employee of a NASA Contractor, the following is applicable:

Pursuant to Section 305(a) of the National Aeronautics and Space Act, the name of the Administrator of NASA appears on the first page of the patent; however, the name of the actual inventor (author) appears at the heading of column No. 1 of the Specification, following the words "... with respect to an invention of ..."

Elizabeth A. Carter
Enclosure
Copy of Patent cited above
ULTRAHIGH VACUUM GAUGE HAVING TWO COLLECTOR ELECTRODES

Filed Oct. 16, 1964

Fig. 1

Fig. 2

Fig. 3

Fig. 4

Fig. 5
The present invention relates to vacuum gauges and particularly to the measurement of ultra high vacuum. The invention described herein was made in the performance of work under a NASA contract and is subject to the provisions of the National Aeronautics and Space Act of 1958, Public Law 85-568 (72 Stat. 426; 42 U.S.C. 2451) as amended. A license has been granted to the United States Government for practice of the invention and title to the invention and this patent have been reversed to the assignee, subject to voidability by NASA.

It is known that the calibration of vacuum gauges, particularly hot filament ionization gauges without magnets, departs from linear in the ultra high vacuum range. The collection current is much higher than the current corresponding to the pressure to be measured. It is therefore the object of this invention to provide a technique of pressure measurement which allows the nonlinear gauge readings in the ultra high vacuum range to be corrected to true pressure with greater accuracy.

A preferred embodiment of the invention is shown in FIG. 5. The gauge elements are essentially the same as in FIG. 1, except that a modulator ring 124 is added, as shown in FIG. 5. The modulator ring 124 is added to the suppressor gauge to provide more accurate readings of ultra high vacuum pressures than would be obtainable from the use of a suppressor gauge, a modulation gauge, or both operated simultaneously.

The invention accordingly comprises an improved gauge and an improved technique of measuring ultra high vacuum pressures.

The experiments were conducted by comparing the measured collector current \( I_m \) of the suppressor gauge with the collector current \( I_{ref} \) of a modulated Bayard-Alpert type gauge after Redhead (Review of Scientific Instruments, vol. 31: pp. 343–344, 1960). It was expected that the calibration curve would be as shown in FIG. 2. That is, operating without the secondary emission suppression (suppressor voltage zero; curve A), the collector current would depart from linear in the range of \( 10^{-10} \) amperes reference current as X-ray effects became significant compared to ion current. Operating with the suppressor ring at minus 300 volts the departure from linear would be attenuated (curve B).

Instead, the anomalous results of FIG. 3 were encountered. The curve AA produced without suppression was similar to the expected curve A of FIG. 2. The curve BB, produced with suppression, was lower than AA in the range where X-ray effects are not significant. The difference in collector currents between curves AA and BB was essentially constant down to the middle of the \( 10^{-10} \) reference current range. Then both curves departed from linear at different rates.

Later the gauge was disassembled and it was observed that the suppressor ring was tilted away from its intended position as shown in FIG. 4.

It is concluded that, due to the inadvertent tilting, and its negative potential, the suppressor ring \( 16 \) intercepted a portion of the ions destined for the collector \( 14 \), in a manner analogous to the operation of a modulated Bayard-Alpert gauge, thus producing the lower calibration curve BB. It must be that a uniform percentage of ions are collected since the difference (about 10%) between curves AA and BB is constant in the high vacuum range. A modulator can be provided in a suppressor gauge, either as part of the suppressor or as a separate element. The discovery that the modulation fraction is constant allows one to use suppression and modulation functions together to provide more accurate readings of ultra high vacuum pressures than would be obtainable from the use of a suppressor gauge, a modulation gauge, or both operated simultaneously.
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The total collector current in a gauge (no modulation, no suppression), may then be described as follows:

\[ I_{m} = (I_{s} + I_{c}) + (I_{N} + I_{H}) \]  

(1)

If the gauge is modulated, without suppression, Equation 1 must be revised as follows:

\[ I_{m} = a(I_{s} + I_{c}) + (I_{N} + I_{H}) \]  

(2)

where \( a \) is the constant of modulation which can be determined. The collector current of a suppressor gauge (no modulation) is:

\[ I_{m} = I_{s} + I_{c} + I_{H}, I_{N} = 0 \]  

(3)

The operation of the suppressor grid reduces secondary emission to zero.

Subtracting Equation 3 from Equation 1:

\[ I_{m} - I_{m} = I_{N} \]  

(4)

That is, the difference between the gauge readings with and without suppression gives the true secondary emission current of the gauge.

Further information can be developed from the readings \( I_{m} \), \( I_{m2} \), \( I_{m3} \), and follows:

Equation 1 is multiplied by \( a \):

\[ aI_{m} = a(I_{s} + I_{c}) + a(I_{N} + I_{H}) \]  

(1')

Subtracting Equation 2 from Equation 1':

\[ I_{N} = \frac{aI_{m} - I_{m2}}{a - 1} = I_{N} \]  

(5)

Since \( I_{N} \) and \( a \) can be determined for a gauge, one can solve for \( I_{N} \).

It has been proposed by Redhead (see e.g., Vacuum Magazine, vol. 13, p. 253, 1963) that the ratio \( I_{c}:I_{H} \) is about 100. Experimental data indicates that this figure is correct. Therefore, once the reading, \( I_{m} \), \( I_{m2} \), and \( I_{m3} \) have been made and \( a \) is determined for a gauge, one can compute \( I_{c} \), \( I_{N} \), \( I_{H} \) as noted above. Then, returning to Equation 1 above, \( I_{s} \), which is the measure of gas density, can be computed.

The above finding that the deviation in collector current due to inadvertent modulation is constant leads to the conclusion that the factors \( I_{N} \) and \( I_{c} \) are independent of pressure. This allows the present invention to be used in the following manner. Operating at known pressures in the range of \( 10^{-9} \) torr based on a reference current of a gauge having a sensitivity of 0.1 amp./torr, the gauge of FIG. 5 is operated with modulation and without modulation. The uniform difference between curves

\[ I_{m} - I_{m3} \]

gives the current \( I_{N} \). Then, at lower pressures, the gauge is operated with suppression to eliminate \( I_{N} \). The measured collector current at lower pressures \( (I_{m3}) \) will be utilized in Equations 2 and 5 with a known value of \( I_{N} \), to find \( I_{c} \). \( I_{c} \) is then determined as \( 100I_{c} \). Equation 1 can then be utilized to find the ionization current \( (I_{s}) \) related to the gas under study. Thus, a pressure gauge with suppressor and modulator, constructed as described above, affords advantages beyond those attainable by measuring gas density with a suppressor gauge and a modulator gauge together.

Many variations can be made from the preferred embodiment of the above description. It is therefore intended that the above description shall be regarded as illustrative and not in a limiting sense.

What is claimed is:

An improved ultra high vacuum gauge comprising in combination means for ionizing molecules of the gas whose pressure is to be measured, a first collector electrode for collecting ions, means for suppressing secondary emission from the first collector electrode, means for shielding the suppressing means from radiation from the ionizing means, and a second collector means interposed between said first collector and said suppressor and biassed negatively with respect to said first collector, said second collector arranged to selectively collect ions and reduce ion flow to said first collector.

References Cited by the Examiner

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