FINAL REPORT on
ANALYSIS OF FATIGUE, FATIGUE-CRACK PROPAGATION, AND FRACTURE DATA

by
Carl E. Jaske, Charles E. Feddersen, Kent B. Davies, and Richard C. Rice

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Prepared under Contract No. NAS1-11344 for NATIONAL AERONAUTICS AND SPACE ADMINISTRATION LANGLEY RESEARCH CENTER

BATTELLE
Columbus Laboratories
505 King Ave.
Columbus, Ohio 43201
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Prepared under Contract No. NAS1-11344 by BATTELLE'S COLUMBUS LABORATORIES Columbus, Ohio

for

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
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ANALYSIS OF FATIGUE, FATIGUE-Crack PROPAGATION, AND FRACTURE DATA

By Carl E. Jaske, Charles E. Feddersen, Kent B. Davies, and Richard C. Rice
Battelle's Columbus Laboratories

SUMMARY

Analytical methods have been developed for consolidation of fatigue, fatigue-crack propagation, and fracture data for use in design of metallic aerospace structural components. To evaluate these methods, a comprehensive file of data on 2024 and 7075 aluminums, Ti-6Al-4V, and 300M and D6AC steels was established. Data were obtained from both published literature and unpublished reports furnished by aerospace companies. Fatigue and fatigue-crack-propagation analyses were restricted to information obtained from constant-amplitude load or strain cycling of specimens in air at room temperature. Fracture toughness data were from tests of center-cracked tension panels, part-through crack specimens, and compact-tension specimens.

Both fatigue and fatigue-crack-propagation data were analyzed on a statistical basis using a least-squares regression approach. An arc-hyperbolic tangent function was used to relate the independent variable to the dependent variable. For fatigue, an equivalent strain parameter was used to account for stress ratio effects and was treated as the independent variable, and cyclic fatigue life was considered to be the dependent variable. An effective stress-intensity factor was used to account for the effect of load ratio on fatigue-crack propagation and was treated as the independent variable. In this latter case, crack-growth rate was considered to be the dependent variable.

Smooth-specimen and notched-specimen fatigue data were treated separately. Notched-specimen results were analyzed using a local stress-strain approach to account for fatigue damage at the notch root. Data for various types of notches and theoretical stress-concentration factors were consolidated by using a computed fatigue-strength reduction factor. Both the cyclic and monotonic stress-strain curves were employed in calculating the local stress-strain response from nominal loading information.

After computing mean fatigue and crack-growth curves by least-squares regression, tolerance-level curves were determined. Lower-level tolerance curves for 90 and 99 percent probability of survival with 95 percent level of confidence were determined for each fatigue curve. Two-sided tolerance bands for 90 and 99
percent probability with 95 percent confidence were determined for each mean crack-growth curve.

Fracture toughness data were tabulated for a particular material and specimen thickness in terms of average values at various temperatures and panel widths. Apparent, critical, and onset fracture toughness indexes were used in this tabulation.

INTRODUCTION

Recent experience with modern aerospace structures has emphasized the importance of considering both fatigue and fracture in the design and service performance of aircraft. A structural member may fracture at loads well below the nominal yield strength of the material if it contains a critical-size flaw. In some instances, such flaws may be introduced into the structural material by manufacturing processes. However, in most cases, flaws will become critical by growing from smaller flaws or from unflawed areas of stress concentration. This type of growth occurs by fatigue processes during cyclic loading of the structure.

Reaching total fracture under cyclic loading involves both fatigue-crack initiation and propagation. As shown in figure 1, crack-initiation life can vary considerably, depending upon the definition of a crack. The wide range of sizes ($10^{-5}$ to $10^{-1}$ inch) considered to be cracks by various investigators causes an ill-defined area of overlap between initiation and propagation. In most fatigue tests of small specimens of virgin material, the initiation phase is generally considered to be a more significant portion of cyclic life than the propagation phase. Fatigue-crack-propagation data are usually obtained from precracked or flawed specimens.

In this program, fatigue data from uncracked smooth or notched specimens were treated separately from fatigue-crack-propagation data from precracked specimens. It was assumed that the total number of cycles to failure normally reported in fatigue tests of simple specimens was a reasonable approximation of the number of cycles required to initiate an engineering size flaw. Crack-propagation information was obtained from studies where cyclic crack growth was measured using a precracked sample. Fracture at a critical load level or flaw size also was treated separately.
Figure 1. — Effect of definition of crack initiation on relation between fatigue-crack initiation and fatigue-crack propagation.
For conventional static properties of metals and alloys, extensive design allowables information is available in documents such as MIL-HDBK-5B (ref. 1). For fatigue, fatigue-crack propagation, and fracture data, however, design allowable values are usually not available and the data are presented in terms of typical or average values.

Part of the problem for fatigue and fatigue-crack propagation is that these behaviors are influenced by a wide range of parameters that include cyclic stress, mean stress, cyclic frequency, temperature, environment, product form and orientation with respect to loading, structural geometry (size, shape, and notch configuration), metallurgical and surface effects associated with heat treatment, microstructure, and machining practices. Most aerospace companies tend to generate data for a limited number of these many variables to fulfill specific local design needs. Much of this information is retained within each company, and that which becomes available in open literature is often digested in accordance with particular theoretical considerations and analytical procedures endemic to a given organization. Since these considerations and procedures vary among companies, it is difficult to affect a systematic consolidation of such data. Assessment of fatigue and fatigue-crack-propagation data is further complicated by the fact that there have been no standard methods for these types of testing. Recommended procedures for fatigue testing have been published recently (ref. 2).

Many of the aforementioned problems also influence fracture results. Standards for obtaining plane-strain fracture-toughness information have been developed recently (ref. 3). However, major differences in testing and analysis procedures still exist for plane-stress and transition-thickness conditions.

As a result of extensive visits and discussions with all major aerospace companies, it became evident to personnel at Battelle's Columbus Laboratories (BCL) who are responsible for maintaining MIL-HDBK-5B (ref. 1) that the major deficiencies in the Handbook were in the important areas of fatigue, fatigue-crack propagation, and fracture. This realization led to the initiation of a research program at BCL under the sponsorship of Langley Research Center. Work was directed toward systematizing and consolidating available fatigue, fatigue-crack propagation, and fracture information on 2024 and 7075 aluminum alloys, Ti-6Al-4V alloy, and 300M and D6AC steels. It was considered imperative that the analytical procedures be compatible with statistical methods of data presentation.
Similar approaches were used for both fatigue and fatigue-crack propagation, as illustrated in figure 2. The logarithm of fatigue life was the dependent variable in both cases. An equivalent strain parameter similar to that suggested by Walker (ref. 4) and Smith, et al. (ref. 5) was used to account for stress ratio effects and was treated as an independent variable in the fatigue analysis. A similar effective stress-intensity factor (ref. 4) was used to account for stress ratio effects and was treated as the independent variable in the fatigue-crack-propagation analysis.

Fatigue-crack propagation is more complicated than fatigue because different life curves (fig. 2) are obtained for each different state of initial damage. Thus, fatigue-crack-propagation results are usually presented in terms of crack-growth rate as shown schematically in figure 3. The layering of rate data as a function of stress ratio can be accounted for using the effective stress-intensity concept mentioned above.

Treatment of fracture data was limited to tabulation and graphical summary of information in terms of three indexes of fracture toughness.

Primary emphasis of the fatigue work was on data for 2024 and 7075 aluminum alloys, with a secondary effort directed toward annealed Ti-6Al-4V alloy and a high-strength steel. The fatigue-crack propagation and fracture work was limited to data for the 2024 and 7075 alloys and 300M and D6AC steels.
FATIGUE ANALYSIS, $\epsilon_{eq}$

$\log N_f = f [\Delta \epsilon, R]$

or specifically,

$\log N_f = f [\Delta \epsilon^m (S_{max}/E)^{1-m}]$

FATIGUE CRACK PROPAGATION ANALYSIS, $K_{eff}$

$\log N_f = f [\Delta K, R]$

or specifically,

$\log N_f = f [\Delta K^m K_{max}^{1-m}]$

$m$ may be treated as a material parameter

Figure 2. — Similarity between fatigue and fatigue-crack-propagation analysis.
Figure 3. - Schematic illustration of layering in fatigue-crack-propagation rate data.
SYMBOLS

A mean stress coefficient
A_i ith regression coefficient
a crack length, mm (in.)
da/dN fatigue crack growth rate
Δa/ΔN approximate crack growth rate
a_i ith value of crack length, mm (in.)
B stress amplitude coefficient
C Paris' coefficient
C_1, C_2 regression coefficient in arc-hyperbolic tangent relation
c crack half length, mm (in.)
c_c crack half length at unstable fracture, mm (in.)
c_0 initial crack half length, mm (in.)
D multiplicative regression coefficient
DD_j(i) the jth order divided difference at point i
E elastic modulus, MN/m^2 (ksi)
e nominal strain
Δe nominal strain range
e_a nominal strain amplitude
e_a(1), e_a(2) specific values of e_a used to define stress-strain curve
e_max maximum nominal strain
Δe_p plastic nominal strain range
K stress intensity factor, MN/m^3/2 (ksi/In.)
ΔK range of stress intensity factor, MN/m^3/2 (ksi/In.)
K_app apparent fracture toughness, MN/m^3/2 (ksi/In.)
K_c critical fracture toughness, MN/m^3/2 (ksi/In.)
K eff effective stress intensity factor, MN/m^3/2 (ksi/In.)
Fatigue strength reduction factor

Mode I critical fracture toughness, MN/m² (ksi/in.)

Ith value of stress-intensity factor, MN/m² (ksi/in.)

Maximum stress-intensity factor, MN/m² (ksi/in.)

Threshold stress-intensity factor, MN/m² (ksi/in.)

Toughness at onset of crack extension, MN/m² (ksi/in.)

Theoretical stress concentration factor

Strain concentration factor

Stress concentration factor

Strength coefficients, MN/m² (ksi)

Stulen coefficient

Regression coefficient

Elber optimization coefficient

Value of slope of function $\phi$

Walker exponent

Number of cycles

Number of cycles to failure

Ith value of number of cycles

Sample population

Paris' exponent

Strain hardening exponents

Maximum load, KN (kip)

5 percent secant offset load, KN (kip)

Plasticity corrected shape factor

Degree of polynomial

Stress ratio

Proportion of variation explained by regression equation

Modification of $R^2$ to account for degrees of freedom
r  notch root radius, mm (in.)
S  nominal stress, MN/m² (ksi)
ΔS  nominal stress range, MN/m² (ksi)
SSD  residual sum of squares
Sₐ  nominal stress amplitude, MN/m² (ksi)
Sₐ(1), Sₐ(2)  specific values of Sₐ used to define stress-strain curve
Sₐ  maximum nominal fracture stress, MN/m² (ksi)
Sₐ  equivalent nominal stress, MN/m² (ksi)
Sₐ  mean nominal stress, MN/m² (ksi)
Sₐ  maximum nominal stress, MN/m² (ksi)
Sₐ  minimum nominal stress, MN/m² (ksi)
Sₐ  net stress or uncracked section
Sₒ  nominal stress at onset of crack extension, MN/m² (ksi)
Sₒ  crack closure nominal stress, MN/m² (ksi), Sₒ > 0
s  standard error of estimate
T  thickness, mm (in.)
TSS  regression (or total) sum of squares
TUS  tensile ultimate strength, MN/m² (ksi)
TYS  tensile yield strength, MN/m² (ksi)
t  Students' t multiplier
u  confidence level
V  variance
w  panel width, mm (in.)
X  independent variable - tanh⁻¹ [Φ(σₑq)] or tanh⁻¹ [Φ(Kₑff)]
Xᵢ  ith value of independent variable
X̄  mean value of X
Y  dependent variable - log Nᵢ or log da/dN
Yᵢ  ith value of dependent variable
<table>
<thead>
<tr>
<th>Symbol</th>
<th>Description</th>
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<tr>
<td>$\bar{Y}$</td>
<td>mean value of $Y$</td>
</tr>
<tr>
<td>$Y_{u',\nu}$</td>
<td>tolerance limit at a level of confidence ($u$) for a given number of degrees of freedom ($\nu$)</td>
</tr>
<tr>
<td>$\alpha$</td>
<td>mean stress exponent</td>
</tr>
<tr>
<td>$\beta$</td>
<td>stress amplitude exponent</td>
</tr>
<tr>
<td>$\varepsilon$</td>
<td>local strain</td>
</tr>
<tr>
<td>$\Delta\varepsilon$</td>
<td>local strain range</td>
</tr>
<tr>
<td>$\varepsilon'$</td>
<td>translated local strain</td>
</tr>
<tr>
<td>$\varepsilon_a$</td>
<td>local strain amplitude</td>
</tr>
<tr>
<td>$\varepsilon_e$</td>
<td>lower limit of inverse hyperbolic tangent function</td>
</tr>
<tr>
<td>$\varepsilon_{eq}$</td>
<td>equivalent local strain</td>
</tr>
<tr>
<td>$\varepsilon_{max}$</td>
<td>maximum local strain</td>
</tr>
<tr>
<td>$\Delta\varepsilon_p$</td>
<td>plastic local strain range</td>
</tr>
<tr>
<td>$\varepsilon_u$</td>
<td>upper limit of inverse hyperbolic tangent function</td>
</tr>
<tr>
<td>$\nu$</td>
<td>degrees of freedom</td>
</tr>
<tr>
<td>$\rho$</td>
<td>notch analysis material constant</td>
</tr>
<tr>
<td>$\sigma$</td>
<td>local stress, MN/m² (ksi)</td>
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<tr>
<td>$\Delta\sigma$</td>
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<td>$\sigma_m$</td>
<td>mean local stress, MN/m² (ksi)</td>
</tr>
<tr>
<td>$\sigma_{max}$</td>
<td>maximum local stress, MN/m² (ksi)</td>
</tr>
<tr>
<td>$\sigma_{min}$</td>
<td>minimum local stress, MN/m² (ksi)</td>
</tr>
<tr>
<td>$\delta_1$</td>
<td>value of intercept of function $\delta$</td>
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To implement the evaluation of existing fatigue, fatigue-crack-propagation, and fracture data, it was necessary to make an extensive survey of the literature and of aerospace companies that might have unpublished internal reports. A computerized system was developed to compile and store data obtained from this survey. Data from more than 120 reports and documents were acquired, compiled, and stored.

Data Acquisition

Information was taken both from the open literature and from company reports. Applicable reports were obtained from the technical files of the Metals and Ceramics Information Center (MCIC) located at BCL. Throughout the program, new reports, acquired by MCIC, were screened and added to the data base when applicable. In order to obtain as much recent information as possible, additional literature searches were obtained from the National Aeronautics and Space Administration (NASA) (refs. 6 and 7) and the Defense Documentation Center (DDC) (refs. 8 and 9). In addition, pertinent reports obtained through the MIL-HDBK-5 (ref. 1) program were used.

Internal reports from aerospace companies and unpublished data were obtained from various laboratories that conduct fatigue, fatigue-crack-propagation, and fracture research. A letter was prepared and sent out to 89 selected members of the American Society for Testing and Materials (ASTM) Committee E09 on Fatigue. A similar letter was also sent to 18 members of the ASTM Committee E24 on Fracture Testing of Metals and to 46 members of the MIL-HDBK-5 Coordination Group. Positive responses were received from about 40 percent of those surveyed. Pertinent data from the responses were entered into the data storage files. The type of information that was requested in these letters is summarized in the following three sections.

**Basic Fatigue Information.**—For the alloys of interest (2024 and 7075 aluminum, Ti-6Al-4V, and high-strength steels), fatigue data were desired from axial-load tests of simple specimens that reflect basic material behavior. This requirement excluded joints or components but included both notched and unnotched data, where notch configuration and severity were variables. Data for cyclic...
lives ranging from $>10^6$ to $<10^7$ cycles, both strain and load-controlled test data, and variable stress ratio (or mean stress) data were of interest.

Basic test data were desired; i.e., tables of stress or strain versus lifetime. In cases where crack initiation was determined, this information (and the initiation criterion employed) was desired. For tests involving cyclic plasticity, cyclic stress-strain information in the form of stress and strain as a function of loading history were needed.

In addition to the fatigue data, correlative information concerning specimen geometry and fabrication, material product form, dimensions and processing, test techniques and controls, laboratory environment and mechanical properties were also desired. The latter information was required to aid in making decisions about pooling various samples of data.

**Fatigue-Crack-Propagation Information.**—Fatigue-crack-propagation data were desired for center-cracked panels (in a variety of widths), part-through-cracked or surface-flawed specimens, compact-tension specimens, and double-cantilever-beam specimens. It was useful to have data that delineated crack initiation cycles from a geometrically known starter flaw as well as initial propagation data from it, if such information was available. Delineation of the stress cycle employed for each test, as well as test frequency, was necessary. In some cases, multiple tests were conducted on a single specimen such that propagation occurred on successive crack-growth segments under different cyclic-stress conditions. Each of these conditions was considered as a single test in the analysis, and the conditions needed to be described.

Basic test data again were desired; i.e., tabular displays of crack size versus cycles. For each specimen, the associated test stress cycle description was given.

In addition to the basic crack-propagation data, correlative information as described for fatigue data were necessary.

**Fracture Information.**—The fracture data collection was more complex in that there was a thickness dependence on fracture toughness that was of greater significance than for fatigue and fatigue-crack propagation. This thickness dependence influenced the mode of fracture (such designations as slant, transition, and flat fracture descriptions were used) corresponding to plane stress, transitional stress, and plane-strain fracture toughness. A variety of tests have been
employed, only a few of which are standardized (ref. 3). Thus, test specimen
test specimen
description and test techniques had to be delineated carefully and completely.
Specific tests for which data were desired included the center-cracked panel,
part-through or surface-flawed specimens, compact-tension specimens, double-
cantilever-beam specimens, and notched-bend specimens.

Basic test data were needed rather than fracture toughness values. These
included original crack length, critical crack length, ultimate load or stress,
and load or stress at which slow stable crack growth initiated (presented in
tabular form). Load-compliance records were obtained when possible.

As stated before, correlative information was desired with particular
emphasis on test methods and techniques.

Data Recording and Storage

Information used in this program was stored in a format for computerized
analysis. Detailed data has been recorded on punched cards for use at BCL.
These data were transferred to magnetic tapes and forwarded to NASA Langley Re-
search Center. To help document the encoded data, a short abstract was prepared
for each report from which information was taken. This abstract summarized
briefly the type of data encoded along with correlative information not recorded
in the data file. The check list shown in figure 4 was used in preparing these
abstracts. Sample abstracts are presented in figures 5 and 6. A complete set
of abstracts was sent to NASA Langley along with the magnetic tapes. Each source
from which data were taken and an abstract prepared are listed in Appendix A.
Each source was assigned a unique reference number when it was added to the data
base.

The basic medium for recording the fatigue, fatigue-crack-propagation, and
fracture data collected and compiled on this program is the standard 80 column
computer punch card. Data card file sequences and formats which have been se-
lected to provide a consistent procedure for encoding these data are described
in the following subsections.

Each data file may contain up to four basic types of cards depending on the
type of information being recorded. These card forms are

Card 1: Title or lead card, identifying test and material
Card 2: Subtitle card, containing supplementary testing, composi-
tional, or processing information where desirable
Card 3: Data card describing specific test parameters and results
Card 4: Crack growth card listing cycle count and crack size.
DATA SOURCE ABSTRACT CHECKLIST

For Each Report From Which Data is Obtained
Check for, and Record, the Following Items.

General Report Information

(1) Reference Number.
(2) Materials.
(3) Authors, Title, Publisher/Source, Publication Date.

Test Information

(1) Type of Test (Fatigue, Fatigue-Crack Propagation, Fracture), Summary of Report Abstract.
(2) Type of Test Machines, Load or Strain Control?
(3) Number of Specimens.
(4) Stress Ratios.
(5) Test Temperature and Environment.
(6) Test Frequencies.
(7) If Fatigue-Crack Propagation —
   (a) Plane Strain or Plane Stress?
   (b) Basic Data or "Digested" Data?

Specimen Data

(1) Melting Practice/Heat Treatment of Specimens.
(2) Ductility.
(3) Fabrication Methods.
(4) Surface Finish.
(5) Specimen Dimensions.
(6) Chemical Composition.
(7) Tensile Properties (TYS, TUS, Reduction of Area, Elongation, Elastic Modulus).
(8) Are There Stress-Strain Curves or Data? Are They Monotonic or Cyclic?

Figure 4. — Checklist used for preparation of report abstracts.
Materials: 2024-T3, 7075-T6, 4130 Steel


Test Information

(1) Fatigue Tests: Axial-load fatigue tests were conducted on notched specimens of three sheet materials with one stress concentration factor and four mean stress levels.

(2) Type of Test Machine: Krouse direct repeated-stress test machine.

(3) Number of Specimens: 49/2024-T3, 47/7075-T6, and 42/4130.

(4) Stress Ratio: R = -1.0 to 0.70.

(5) Test Temperature and Environment: Tests were conducted at room temperature in air.

(6) Test Frequency: 1100 - 1500 cpm.

Specimen Data

(1) Melting Practice/Heat Treatment: Not specified.

(2) Ductility: Not specified.

(3) Fabrication Methods: Specimens were machined from 0.09 inch thick 2024-T3 and 7075-T6 aluminum and from 0.075 inch thick 4130 steel. Notches were cut in a series of machining cuts.

(4) Surface Finish: Specimens were electropolished.

(5) Specimen Dimensions: Gross length = 15.5 inches, gross width = 2.25 inches, net width = 1.5 inches, root radius = 0.03125 inch (K_t = 5).

(6) Chemical Composition: Not specified.

(7) Tensile Properties:

<table>
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<tr>
<th>Material</th>
<th>TYS, ksi</th>
<th>TUS, ksi</th>
<th>Elong., %</th>
</tr>
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<tbody>
<tr>
<td>2024-T3</td>
<td>54.0</td>
<td>73.0</td>
<td>18.2</td>
</tr>
<tr>
<td>7075-T6</td>
<td>76.0</td>
<td>82.5</td>
<td>11.4</td>
</tr>
<tr>
<td>4130</td>
<td>98.5</td>
<td>117.0</td>
<td>14.3</td>
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(8) Stress-Strain Curves: Not given.

Figure 5. - Sample abstract for report containing fatigue data.
REFERENCE NUMBER 15 (MCIC 73988)

Materials: 300 M


Test Information

(1) Fracture and Crack Propagation Tests: Tests were conducted on one material in three product forms to study the effects of material thickness and strength level.

(2) Type of Test Machine: Lockheed-designed closed-hoop servohydraulic fatigue machine (150,000 lb. capacity), Lockheed-designed axial load resonant fatigue machine (250,000 lb. capacity), and a universal hydraulic testing machine (60,000-400,000 lb. capacity).

(3) Number of Specimens: 132 specimens were used to obtain both crack propagation and fracture data.

(4) Stress Ratio: $R = 0.1$ or $0.5$.

(5) Test Temperature and Environment: Tests were conducted at room temperature in a moist air or salt spray environment.

(6) Test Frequency: 20 cps to precrack specimens.

(7) FCP Data: Presented in basic form.

Specimen Data

(1) Melting Practice/Heat Treatment: Specimens were normalized at 1700°F/1-1/2 hours, air cooled, austinitized at 1600°F/1-1/2 hours, oil quenched, and double-tempered at 500°F to 1050°F depending upon strength level desired.

(2) Ductility: Not given.

(3) Fabrication Methods: Specimens were machined from 0.125 inch sheet, 0.5 or 0.75 inch plate or forgings. Precracking was done by axial tension-tension fatigue generated from an EDM slot.

(4) Surface Finish: Specimens were left as machined.

(5) Specimen Dimensions:

<table>
<thead>
<tr>
<th>Specimen Type</th>
<th>Thickness, inch</th>
<th>Gross Length, inch</th>
<th>Gross Width, inch</th>
<th>Net Length, inch</th>
<th>Net Width, inch</th>
<th>Slot Length, inch</th>
<th>Slot Width, inch</th>
</tr>
</thead>
<tbody>
<tr>
<td>Surface Crack</td>
<td>.125</td>
<td>14</td>
<td>3.5</td>
<td>4</td>
<td>2.25</td>
<td>.08</td>
<td>.006</td>
</tr>
<tr>
<td>Surface Crack</td>
<td>.375</td>
<td>16</td>
<td>3.5</td>
<td>5</td>
<td>2.25</td>
<td>.08</td>
<td>.006</td>
</tr>
<tr>
<td>Surface Crack</td>
<td>.75</td>
<td>28</td>
<td>9.0</td>
<td>12</td>
<td>4.5</td>
<td>.08</td>
<td>.010</td>
</tr>
<tr>
<td>Through Crack</td>
<td>.125</td>
<td>15</td>
<td>---</td>
<td>5</td>
<td>---</td>
<td>.5</td>
<td>---</td>
</tr>
<tr>
<td>Through Crack</td>
<td>.375</td>
<td>28</td>
<td>9.0</td>
<td>12</td>
<td>5.0</td>
<td>.5</td>
<td>.010</td>
</tr>
</tbody>
</table>

(6) Chemical Composition: See report for analysis of each heat of material.

(7) Tensile Properties: See report for original materials' properties, results of heat treatment study and properties of control specimens after heat treatment.

(8) Stress-Strain Curves: Not given.

Figure 6. - Sample abstract for report containing fatigue-crack propagation and fracture data.
Each data file always contains at least Cards 1 and 3. Card 2 is an optional card which may be necessary to supplement, clarify or expand Card 1 information in particular situations. Card 4 is a particular addenda of crack-growth information (i.e., cycle count and crack size) necessary only for fatigue-crack-propagation analysis.

**Title or Lead Card (Card 1) Format.** The format of Card 1 is illustrated in figure 7. Eleven fields of general descriptive information are presented. Their contents are as follows:

<table>
<thead>
<tr>
<th>Field</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Reference Number</td>
</tr>
<tr>
<td>2</td>
<td>Material</td>
</tr>
<tr>
<td>3</td>
<td>Alloy Designation</td>
</tr>
<tr>
<td>4</td>
<td>Product Form</td>
</tr>
<tr>
<td>5</td>
<td>Heat Treatment</td>
</tr>
<tr>
<td>6</td>
<td>TYS, MN/m² (ksi)</td>
</tr>
<tr>
<td>7</td>
<td>TUS, MN/m² (ksi)</td>
</tr>
<tr>
<td>8</td>
<td>Thickness of Diameter, mm (or in.)</td>
</tr>
<tr>
<td>9</td>
<td>Width, mm (in.)</td>
</tr>
</tbody>
</table>

![Figure 7. Format for encoding of title or lead card (card 1).](image)

(1) The **type of data** contained in the associated data file is indicated in columns 1 through 3 by using an alphanumeric format with three coding abbreviations:

- **FAT** - data from constant-amplitude-fatigue tests where the controlled variable is stress or strain and the dependent variable is the total number of cycles to complete failure of the specimen (i.e., the fatigue life).
- **FCP** - fatigue-crack-propagation data from a constant-amplitude stress or strain-cycling test where the size of a fatigue crack is monitored as a function of the number of loading cycles.
FT — data from a monotonic loading (load or displacement controlled) test to fracture of a specimen with an initial fatigue precrack.

(2) The dimensional units of the recorded data in the file are identified in column 4. A blank denotes International System (SI) of Units; a value of 1 indicates English units; and a value of 2 indicates CGS units.

(3) The source reference number is listed in columns 5 through 11 in an alphanumeric code of the following format:

"NNNNNNNL",

where N is a numeric character (0 to 9) and L is an alphabet character (A to Z). The numeric code corresponds to the references numbers in Appendix A. The suffix letter refers to a specific batch of data from the referenced document. This reference number is the same as that listed on the succeeding data cards.

(4) The type of material (e.g., aluminum, steel, and titanium) is described in columns 11 through 19 using an alphanumeric format.

(5) The alloy designation (e.g., SAE 4340, 7075-T651, Ti-6Al-4V) is given in columns 20 through 29 in an alphanumeric format.

(6) The product form (e.g., plate, sheet, bar, forging, and casting) is listed in columns 30 through 39 in an alphanumeric format.

(7) The heat treatment (e.g., Q and T, STA, annealed, normalized) is described in columns 40 through 58 in an alphanumeric format.

(8) The TYS, MN/m² (or ksi), is given in columns 59 through 63 in a fixed point numeric format.

(9) The TUS MN/m² (or ksi), is given in columns 64 through 68 in a fixed point numeric format.

(10) Thickness or diameter, mm (or in.), of the specimen is listed in columns 69 through 74 in a fixed point numeric format. For a round specimen where this value represents the diameter, columns 75 through 80 (item 11 below) will be blank.

(11) Width, mm (or in.), of the specimen is given in columns 75 through 80 in a fixed point numeric format. For a round specimen these columns are blank and the diameter is given in item 10 above.
Subtitle Card (Card 2) Format. — The subtitle card is an optional card provided for particular instances where supplementary information is necessary or desirable. This is an open-field card whose format is coded alphanumerically and read directly as a subtitle to Card 1 in data listings or tabulations.

Data Card (Card 3) Format. — This card contains the principal test parameters and results of each test on which data are collected and compiled. Since the types of data may represent either fatigue, fatigue-crack propagation, or fracture tests, three formats are necessary for this card as detailed in the following subsections. Where similar test parameters are encountered among the types of data, common fields have been assigned to the formats.

Fatigue (FAT) Data Card Format. — The fatigue data card contains 13 fields of information listed in the following formats (see fig. 8):

<table>
<thead>
<tr>
<th>Field</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Specimen identification</td>
</tr>
<tr>
<td>2</td>
<td>Maximum Stress, MN/m^2 (or ksi), or Maximum Strain</td>
</tr>
<tr>
<td>3</td>
<td>Stress Ratio or Strain Ratio</td>
</tr>
<tr>
<td>4</td>
<td>Cyclic Frequency</td>
</tr>
<tr>
<td>5</td>
<td>Theoretical Stress Concentration Factor</td>
</tr>
<tr>
<td>6</td>
<td>Notch Root Radius, mm (or in.)</td>
</tr>
<tr>
<td>7</td>
<td>Fatigue Life, Cycles</td>
</tr>
<tr>
<td>8</td>
<td>Temperature, C</td>
</tr>
<tr>
<td>9</td>
<td>Reference Number</td>
</tr>
</tbody>
</table>

Figure 8. — Format for encoding fatigue data card (card 3).

1. **Specimen identification** is listed in columns 1 through 8 using an alphanumeric format.
2. **Maximum stress**, MN/m^2 (or ksi), or **maximum strain** is listed in columns 9 through 14 in a fixed point numeric format. The stress or strain option is designated by the Field 5 indicator.
3. **Stress ratio** or **strain ratio** (ratio of minimum to maximum value) is listed in columns 15 through 19 in a fixed point numeric format. The stress or strain option is designated by the Field 5 indicator.
4. **Cyclic frequency**, Hz, is listed in columns 20 through 24 in a fixed point numeric format.
(5) An indicator is given in column 25 to show whether items 2 or 3 above are in terms of stress or strain. If this column is blank, stress is indicated; and if this column contains an "E", strain is indicated.

(6) The type of notch configuration is listed in columns 26 and 27 by the following abbreviations:
   CN - center-notched sheet or plate
   EN - edge-notched sheet or plate
   FN - fillet-notched sheet or plate
   CR - circumferentially notched round bar.
   These columns are blank for an unnotched specimen.

(7) The theoretical stress-concentration factor of the notch geometry is given in columns 28 through 32 in a fixed point numeric format. These columns are blank for an unnotched specimen.

(8) The notch root radius, mm (or in.), is given in columns 33 through 37 in a fixed point numeric format. These columns are blank for an unnotched specimen.

(9) The fatigue life, cycles, is given in columns 38 through 47 in a fixed point numeric format.

(10) An indicator is given in column 48 to show whether or not the specimen was a runout. A "1" in column 48 indicates that the specimen did not fail (DNF).

(11) This is an open field and columns 48 through 69 are left blank.

(12) Test temperature, °C (or °F), is listed in columns 70 through 73 in a fixed point numeric format.

(13) The source reference number is given in columns 74 through 80 in an alphanumeric format of the following type:

   "NNNNNNNL",

   where N is a numeric character (0 to 9) and L is an alphabet character (A to Z). The numeric code corresponds to the source reference numbers in Appendix A. The suffix letter refers to a specific batch of data from the referenced document. This source reference number is the same as that listed on the corresponding Number 1 Lead Data Card.

Fatigue-Crack Propagation (FCP) Data Card Format.—The complete recording of fatigue-crack-propagation data requires two different card formats. Card 3,
described herein, contains the basic test information; Card 4, described later, contains the cycle counts and crack size measurements as determined from the test. Thus, the data file from a single fatigue-crack-propagation test is made up of one Card 3 and one or more Card 4's.

The layout of Card 3 for the fatigue-crack-propagation test parameters is shown in figure 9.

<table>
<thead>
<tr>
<th>Field</th>
<th>Specimen Identification</th>
<th>Max. Cyclic Stress, MN/m² (or ksi) or Load, kN (or kips)</th>
<th>Stress Ratio or Load Ratio (Min. to Max.)</th>
<th>Cyclic Frequency, Hz</th>
<th>Thickness, mm (or in)</th>
<th>Width, mm (or in)</th>
<th>TYS, MN/m² (or ksi)</th>
<th>TUS, MN/m² (or ksi)</th>
<th>Reference Dimension, mm (or in)</th>
<th>Open</th>
<th>Elastic Modulus, 10¹¹ MN/m³ (or 10¹⁰ kips⁻¹)</th>
<th>Compliances, 10⁻¹² MN/m² (or 10⁻¹⁰ kips⁻¹)</th>
<th>Poisson Ratio</th>
<th>Test Temperature</th>
<th>Reference Number</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>A8</td>
<td>10.0</td>
<td>2.0</td>
<td>3.0</td>
<td>4.0</td>
<td>5.0</td>
<td>6.0</td>
<td>7.0</td>
<td>8.0</td>
<td>9.0</td>
<td>10.0</td>
<td>11.0</td>
<td>12.0</td>
<td>13.0</td>
<td>14.0</td>
</tr>
</tbody>
</table>

Figure 9. — Format for encoding fatigue-crack-propagation data card (card 3).

A total of 16 fields are indicated. The field contents are as follows:

1. **Specimen identification** is listed in columns 1 through 8 using an alphanumeric format.

2. **Maximum cyclic stress**, MN/m² (or ksi), or maximum cyclic load, kN (or kips) is listed in columns 9 through 14 in a fixed point numeric format. The stress or load option is designated by the Field 5 indicator.

3. **Stress ratio** or **load ratio** (ratio of minimum to maximum values) is listed in columns 15 through 19 in a fixed point numeric format. The stress or load option is designated by the Field 5 indicator.

4. **Cyclic frequency**, Hz, is listed in columns 20 through 24 in a fixed point numeric format.

5. The **specimen type** is indicated in column 25 as a numeric code and supplemented in columns 26 and 27 by an acronymonic code for easier identification. Since the **specimen type** also determines the usual convention for selecting either stress or load in the analysis, it is
this field that designates the stress or load option for Fields 2 and 3. The following convention is used in fatigue-crack propagation:

<table>
<thead>
<tr>
<th>Code</th>
<th>Specimen Type</th>
<th>Option</th>
</tr>
</thead>
<tbody>
<tr>
<td>ICT</td>
<td>Compact Tension</td>
<td>Load</td>
</tr>
<tr>
<td>2CC</td>
<td>Center Crack</td>
<td>Stress</td>
</tr>
<tr>
<td>3SF</td>
<td>Surface Flaw or Part-through Crack</td>
<td>Stress</td>
</tr>
<tr>
<td>5DC</td>
<td>Double Cantilever Beam</td>
<td>Load</td>
</tr>
<tr>
<td>6NB</td>
<td>Notch Bend</td>
<td>Load</td>
</tr>
</tbody>
</table>

(6) Specimen thickness, mm (or in.), is listed in columns 28 through 32 in a fixed point numeric format.

(7) Specimen width, mm (or in.), is listed in columns 33 through 37 in a fixed point numeric format.

(8) *Tensile yield strength*, MN/m² (or ksi), representative of that specimen material is listed in columns 38 through 42 in a fixed point numeric format.

(9) *Tensile ultimate strength*, MN/m² (or ksi), representative of that specimen material is listed in columns 43 through 47 in a fixed point numeric format.

(10) A reference dimension, mm (or in.), is listed in columns 48 through 52 in a fixed point numeric format. This dimension is utilized when experimental measurements are recorded relative to a point other than the crack origin prescribed by the analysis.

(11) This is an open field and columns 53 through 57 are left blank.

(12) *Elastic modulus*, 10⁵ MN/m² (or 10⁸ ksi), is listed in columns 58 through 61 in a fixed point numeric format.

(13) Specimen compliance, 10⁻⁶N⁻¹ (or 10⁻⁶lb⁻¹), used specifically for the double cantilever specimen is listed in columns 62 through 66 in a fixed point numeric format.

(14) *Poisson's ratio* for elastic deformation is listed in columns 67 through 69 in a fixed point numeric format.
(15) **Test temperature**, °C (or °F), is listed in columns 70 through 73 in a fixed point numeric format.

(16) The source **reference number** is given in columns 74 through 80 in an alphanumeric format of the following type:

"NNNNNNNL",

where N is a numeric character (0 to 9) and L is an alphabet character (A to Z). The numeric code corresponds to the source reference numbers in Appendix A. The suffix letter refers to a specific batch of data from the referenced document. This source **reference number** is the same as that listed on the corresponding Number 1 Lead Data Card.

**Fracture (FT) Data Card Format.**—Fracture data for a variety of test specimen configurations is accommodated on the card format shown in figure 10. The detail presented is dictated to a large degree by the number of important crack lengths and stresses which are associated with and reported for thin sheet (plane stress) fracture studies.

<table>
<thead>
<tr>
<th>Field</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Specimen Identification</td>
</tr>
<tr>
<td>2</td>
<td>Thickness, mm (or in.)</td>
</tr>
<tr>
<td>3</td>
<td>Width, mm (or in.)</td>
</tr>
<tr>
<td>4</td>
<td>Initial Crack Length, mm (or in.)</td>
</tr>
<tr>
<td>5</td>
<td>Pop-in Stress, MN/m² (or ksi) or Load, kN (or kips)</td>
</tr>
<tr>
<td>6</td>
<td>Offset Stress, MN/m² (or ksi) or Load, kN (or kips)</td>
</tr>
<tr>
<td>7</td>
<td>Visually Determined Critical Crack Length, mm (or in.)</td>
</tr>
<tr>
<td>8</td>
<td>Photo-Recorded Critical Crack Length, mm (or in.)</td>
</tr>
<tr>
<td>9</td>
<td>Maximum Stress, MN/m² (or ksi) or Load, kN (or kips)</td>
</tr>
<tr>
<td>10</td>
<td>TYS, MN/m² (or ksi) or Load, kN (or kips)</td>
</tr>
<tr>
<td>11</td>
<td>TUS, MN/m² (or ksi) or Load, kN (or kips)</td>
</tr>
<tr>
<td>12</td>
<td>Special Dimension, mm (or in.)</td>
</tr>
<tr>
<td>13</td>
<td>Specimen Type</td>
</tr>
<tr>
<td>14</td>
<td>Test Temperature, °C (or °F)</td>
</tr>
<tr>
<td>15</td>
<td>Reference Number</td>
</tr>
<tr>
<td>16</td>
<td>Open</td>
</tr>
</tbody>
</table>

**Figure 10.** — Format for encoding fracture data card (card 3).

A total of 16 fields of data are contained on the card. Their contents are as follows:

1. **Specimen identification** is listed in columns 1 through 8 using an alphanumeric format.

2. **Specimen thickness**, mm (or in.), is listed in columns 11 through 13 using a fixed point numeric format.

3. **Specimen width**, mm (or in.), is listed in columns 14 through 18 using a fixed point numeric format.
(4) **Initial crack length**, mm (or in.), as measured for the fatigue precrack is listed in columns 19 through 23 using a fixed point numeric format.

(5) "**Pop-in** stress, MN/m² (or ksi), or "**pop-in** load, kN (or kips), is listed in columns 24 through 28 using a fixed point numeric format. The stress or load option is designated by the Field 13 indicator.

(6) **Offset stress**, MN/m² (or ksi), or **offset load**, kN (or kips), is listed in columns 29 through 33 using a fixed point numeric format. The stress or load option is designated by the Field 13 indicator.

(7) **Visually determined critical crack length**, mm (or in.), is listed in columns 34 through 38 using a fixed point numeric format.

(8) **Photo-recorded critical crack length**, mm (or in.), is listed in columns 39 through 43 in a fixed point numeric format.

(9) **Maximum stress**, MN/m² (or ksi), or **maximum load**, kN (or kips), is listed in columns 44 through 48 in fixed point numeric format. The stress or load option is designated by the Field 13 indicator.

(10) **Tensile yield strength**, MN/m² (or ksi), representative of that specimen material is listed in columns 49 through 53 in a fixed point numeric format.

(11) **Tensile ultimate strength**, MN/m² (or ksi), representative of that specimen material is listed in columns 54 through 58 in a fixed point numeric format.

(12) A **special dimension**, mm (or in.), characteristic of that specimen type is listed in columns 59 through 63 in a fixed point numeric format.

(13) The **specimen type** is indicated in column 64 as a numeric code and supplemented in columns 65 and 66 by an acronymonic code for easier identification. Since the **specimen type** also determines the usual convention for selecting either stress or load in the analysis, it is this field that designates the option for Fields 5, 6, and 9.

The following conventions that were used in fatigue-crack propagation are also used for fracture:
<table>
<thead>
<tr>
<th>Code</th>
<th>Specimen Type</th>
<th>Option</th>
</tr>
</thead>
<tbody>
<tr>
<td>1CT</td>
<td>Compact Tension</td>
<td>Load</td>
</tr>
<tr>
<td>2CC</td>
<td>Center Crack</td>
<td>Stress</td>
</tr>
<tr>
<td>3SF</td>
<td>Surface Flaw or Part-through Crack</td>
<td>Stress</td>
</tr>
<tr>
<td>5DC</td>
<td>Double Cantilever Beam</td>
<td>Load</td>
</tr>
<tr>
<td>6NB</td>
<td>Notch Bend</td>
<td>Load</td>
</tr>
</tbody>
</table>

(14) An open field is in columns 67 through 69.

(15) Test temperature, °C (or °F), is listed in columns 70 through 73 in an integer format.

(16) The source reference number is given in columns 74 through 80 in an alphanumeric format of the following type:

"NNNNNNNL",

where N is a numeric character (0 to 9) and L is an alphabet character (A to Z). The numeric code corresponds to the source reference numbers in Appendix A. The suffix letter will refer to a specific batch of data from the referenced document. This source reference number is the same as that listed on the corresponding Number 1 Lead Data Card.

Crack-Growth Card (Card 4) Format.—The crack-growth card is used for recording the crack-size measurements and cycle counts associated with a given fatigue-crack-propagation test or test specimen. Each card contains one set of data points. The format of Card 4 for crack-growth measurements is illustrated in figure 11.

Figure 11. — Format for encoding crack-growth data card (card 4).
A total of 4 fields are indicated. Their contents are as follows:

1. **Specimen identification** is listed in columns 1 through 8 using an alphanumeric format.
2. **Number of cycles** associated with the first data point on the card is listed in columns 11 through 20 in an integer format.
3. **Crack length**, mm (or in.), associated with the first data point on the card as measured in the width dimension of the specimen is listed in columns 21 through 30 in a fixed point numeric format.
4. **Crack depth**, mm (or in.), as measured into the thickness of the specimen is listed in columns 31 through 40 in a fixed point numeric format.

**Data Retrieval and Sorting**

The data handling system consists of two sets of programs. The first set implements the storage of fatigue, fatigue-crack propagation, and fracture data on magnetic tape. The second set implements the retrieval of data on the basis of certain specified parameters.

The storage program writes the data in card-image format on seven-track magnetic tape at a density of 800 bits per inch. Materials are separated from each other by end-of-file cards. There is a different tape for each type of data.

Data retrieval is implemented through a set of programs that sorts the data by a number of parameters including stress ratio, stress, frequency, environment, and test temperature. These parameters must be specified on a separate control card. Specified data then may be transferred from the magnetic tape to any of a number of output devices. Information may be obtained in the form of magnetic tape, punched cards, or printed output. Either SI or English units may be used.

Additional analytical subprograms are added to the sorting program to obtain graphical output and to perform curve fitting and statistical analysis. Figure 12 presents a flow chart outlining the data storage and retrieval system.
Figure 12. — Data storage, retrieval, and sorting system flow chart.
The phenomenological approach to the study of fatigue and fatigue-crack propagation is usually concerned with formulating a model of material behavior. In the present program, this model took the form of a regression equation that was fitted to empirical data. Statistical analysis provided a method by which the performance of the various empirical models could be compared and evaluated.

The method which was developed for the analysis of fatigue data is outlined in Appendix C. The formulations which were used in the analysis are discussed in the following section.

In the fatigue analysis, a third-order polynomial proved to be useful for many of the initial comparative studies. The equation was written in the following form:

$$\log N_f = A_0 + A_1 \varepsilon_{eq} + A_2 \varepsilon_{eq}^2 + A_3 \varepsilon_{eq}^3 \quad (1)$$

Further investigations revealed that equation (1) could be simplified to a linear regression equation involving a single independent variable,

$$Y = A_0 + A_1 X \quad (2)$$

where X represented a mapping function linearly related to the dependent variable Y. This same simple functional form was also found to be useful in the fatigue-crack-propagation analyses.* A least-squares regression procedure was used to establish optimum coefficients for equations (1) and (2). The optimization procedure was based on a minimization of the standard error of estimate,

$$s = \sqrt{\frac{\sum(Y-Y_{\text{mean}})^2}{n-2}} \quad (3)$$

Different formulations for the independent variables were compared through calculation of the statistical parameter, $R^2$. This factor, which provided a quantitative estimate of goodness of fit, was used to describe the fraction of the sum of squares of deviations of the dependent variable from its mean associated with the regression. It was defined by the relationship

$$R^2 = 1 - \frac{\text{SSD}}{\text{TSS}} = 1 - \frac{\sum(Y_i - Y)^2}{\sum(Y - \bar{Y})^2} \quad (4)$$

* The exact definition of this mapping function was omitted here for simplicity, it is detailed in the later sections on fatigue and fatigue-crack propagation. Briefly, however, for the fatigue analysis $X = f(\varepsilon_{eq})$ and $Y = \log N_f$, and for the fatigue-crack-propagation analysis, $X = f(K_{eff})$ and $Y = \log da/dN.$
Values of $R^2$ approaching 100 percent were considered most desirable, since that tendency indicated a large percentage of the variance of the dependent variable was attributable to the regression. In the case of fatigue, such values of $R^2$ indicated a good correlation between equivalent strain and fatigue life. In the case of fatigue-crack propagation, they indicated a well-defined relationship between the effective stress-intensity factor and crack-growth rate. The $R^2$ parameter was used extensively in the two sections of this report on fatigue and fatigue-crack propagation.

In parts of the fatigue analysis where the degree of fit for one material was compared with that for another material, a modified value of $R^2$, designated as $R_m^2$, was used. Such a statistic was necessary when the sample population was fairly small in comparison with the number of degrees of freedom. For example, $R_m^2$ was used to compare a small sample of fatigue data on Ti-6Al-4V alloy with a large sample of data on 300M steel. (See Table 2 on page 38.) This term provided a more realistic estimate of fit than $R^2$, since it accounted for the number of degrees of freedom and the sample population. It provided a sample estimate of the fraction of the variance of the dependent variable attributable to regression (ref. 10) and was expressed as follows:

$$R_m^2 = 1 - \frac{(1-R^2)(n-1)}{(n-v-1)}$$  \hspace{1cm} (5)

In cases where $n$ was only slightly larger than $v$, the $R_m^2$ statistic was appreciably smaller than the $R^2$ statistic. However, when $n \gg v$, the value of $R_m^2$ approached that of $R^2$. Thus, only values of $R^2$ were computed for comparison of results from large data sample populations.

After screening the formulations of interest, it was considered desirable to establish tolerance limits on the best empirical models. These tolerance limits are calculated to define an interval which can be claimed to contain a specified proportion of the data population with a specific degree of confidence. Before tolerance limits could be calculated, it was necessary to determine whether the data satisfied the appropriate statistical conditions. Primarily, the data had to be independent and be normally distributed about the regression line and had to have zero mean deviations from that line and have a constant variance (ref. 11). When the residuals (or deviations from the mean curve) were plotted as a function of actual values of the dependent variable, it was possible to determine, by inspection, whether the data were independent and had an essentially uniform variance throughout their range. Actual values for the dependent variable were used since it was then possible to compare different fitting functions without
changing the fatigue life values of individual data points on the residual plot.
If only one fitting function had been studied, it would have been reasonable to use
predicted values of the dependent variable as is customary in most statistical
analyses. The additional criterion of log-normality was tested in several cases
through construction and examination of frequency distribution plots of the
residuals. Although log-normality of the data was not proved, the frequency
distribution plots indicated that the data were not skewed appreciably and were
reasonably approximated by a log-normal distribution.

After statistical conditions were satisfied, it was possible to calculate the
estimated variance of a specific value of Y about the regression line. For a first
order equation [eq. (2)], the point estimate of variance was defined according to
the following expression:

\[ \sigma^2 = \frac{s^2}{n} \left( \frac{1}{\sum (X_i - X)^2} \right) \]

To solve equation (6), it was necessary to determine values of \( X_i \) for each
data value based on values of \( \varepsilon_{eq} \). Then \( X \) was calculated as a simple average of
the \( X_i \)'s. The same process was used in order to calculate \( s^2 \), based on values of
\( Y_i \). After these calculations were completed, the variance was calculated for a
selected value of \( X \). Knowing the estimates of variance at \( X \), it was then possible
to determine tolerance limits of level (u) at a desired confidence (v), according
to the following formulation (ref. 12)

\[ Y_{u,v} = Y \pm t \sqrt{s^2 + v} \]

Equation (7) was only valid, however, for data sets which were essentially of
uniform variance throughout the range of \( Y \).

In cases where the variance was nonuniform, it was necessary to modify the
residuals through the use of a weighting function, \( W(X) \), so that the transformed
residuals were approximately uniform. A discussion of this process is included in
the Fatigue Analysis section of this report.

In defining all of the above equations, it was assumed that the data under
analysis were constituents of a single population, presumably from a single source,
where factors such as between laboratory and between test machine variability were
of no importance. In a practical situation, however, a large data accumulation for
a given material is often the result of work at numerous laboratories. In such a
case, it is inevitable that some portion of the observed data variance is really
caused by between-system variations. It is desirable to isolate these two factors
so that the material scatter can be considered apart from the laboratory-introduced
scatter. If, for example, it is found that the between-laboratory variance of two combined data sets is much larger than the within-laboratory variance of either subpopulation, it is reasonable to analyze the data separately since the ratio of variances indicates that there is a strong possibility the two materials are different or the procedure used to test them was not the same. The following paragraphs discuss this problem as it pertains to populations of fatigue data. Basic aspects of the discussion are also applicable to fatigue-crack-propagation data.

A method proposed by Mandel and Paule (ref. 13), involving the interlaboratory evaluation of a material with an uneven number of specimens from different sources, was considered as a means of properly accounting for within-laboratory and between-laboratory variance factors. This method was found to be useful in certain cases where fatigue data for a given material, although generated at different laboratories, were obtained from tests run at consistent values of stress ratio and notch concentration. It was questionable whether the approach had application for most of the accumulated data file, however, since the majority of data from different sources were nonuniform in values of stress ratio and notch concentration. To use the method for data such as these, it would necessarily have followed that the means of consolidation on R and Kt was sufficiently good that individual sets of data could not be statistically isolated. This then implied that data from different sources, even though possibly of nonequal stress ratio or notch concentration, could have been compared, after consolidation, as identical data.

Investigations did not provide sufficient evidence to support this conclusion. Most sources contained data at only a few values of R. In some cases, a particular stress ratio was represented by only a few nonreplicate tests. The same was true for much of the data generated with Kt as a variable. This lack of uniform and consistent data made it difficult to conclude with confidence that consolidated data run at different R and Kt values were completely homogeneous.

Despite this problem, it was considered appropriate to calculate tolerance limits on the combined data sets according to equation (7), since all requirements involving randomness, normality, and uniformity of variance appeared to be met satisfactorily. Since it was concluded that subpopulations could not be accepted or rejected on the basis of an examination of variances, particular data sets were included or excluded on the basis of their overall effect on the quality of fit \( R^2 \) which was obtainable. In some instances, a visual examination of the plotted data was sufficient to exclude a particular data subset.
Designers of aircraft structural components usually base their fatigue analysis on data from stress versus number of cycles to failure (S-N) curves. Data for these S-N curves are obtained from constant-amplitude fatigue tests of simple notched or unnotched specimens. The stress value in the S-N curve is usually either $S_{max}$ or $S_a$ and the S-N relationship is defined for a constant value of $S_m$ or $R$. Curves are generated at several values of $S_m$ or $R$ to determine the effect of mean stress or stress ratio. To obtain estimates of fatigue life for other values of mean stress, interpolations between existing data must be made. Average S-N curves are often used to construct modified Goodman diagrams to aid in making these interpolations. A set of S-N curves is normally required for both smooth specimens and several sets of notched specimens with different notch concentrations.

Determination of a meaningful set of average S-N curves for a material may require 100 or more specimens. If a statistically based S-N curve is required for each condition, this number could easily increase to 500 or more specimens. Since such large amounts of fatigue data are not available, even for well-characterized materials, it is desirable to have an analytical method for combining data from different S-N curves to obtain a single curve containing sufficient data to allow the development of a statistically based S-N type relationship for each material.

The following sections describe the analytical formulations and approximations which were used in the development of the final analytical model. The problem of consolidation of data generated at different mean stresses is considered first. Three different formulations of equivalent strain are reviewed and compared. Next, the consolidation of notched data is considered. Various methods of estimating local alternating, mean and maximum stress levels are described and critically analyzed. The final step relates to the establishment of a functional relationship between equivalent strain and fatigue life. The overall results conclude the section.

Equivalent Strain Concept in Unnotched Specimens

It has been found in work done at BCL that the effect of mean stress on fatigue life can be reasonably accounted for through the use of an equivalent stress (or strain). Equivalent stress is defined by an equation relating two
terms that uniquely define constant-amplitude loading conditions. One term represents the cyclic stress amplitude in terms of either $\Delta S$ or $S_a$, while the other term defines the mean stress, either directly as $S_m$ or indirectly as $S_{\text{max}}$ in conjunction with $S_a$. If equivalent strain rather than stress is used, $\Delta S$ and $S_a$ are replaced by $\Delta e$ and $e_a$.

The following section includes a derivation of the equivalent strain equations which were evaluated as a part of this program. The determination of strain amplitudes through usage of the cyclic stress-strain curve is also described. Factors influencing the final choice of an equivalent strain formulation are discussed at the close of the section.

**Formulations of Interest.** - Two general formulations of equivalent stress have been reviewed. The first involves an additive combination of two stress parameters,

$$S_{eq} = A S_m^\alpha + B S_a^\beta .$$

Equation (8) reduces to a form suggested by Stulen (ref. 14) when $B$, $\alpha$, and $\beta$ are set equal to unity,

$$S_{eq} = k S_m + S_a .$$

When both coefficients, $A$ and $B$, and the exponent $\beta$ are assumed equal to one, equation (8) simplifies to another form originally proposed by Topper and Sandor (ref. 15),

$$S_{eq} = S_m^\alpha + S_a .$$

Since equations (8a) and (8b) are applicable only in cases where stress levels are nominally elastic, it was necessary to consider a more general formulation. To account for inelastic stress-strain behavior, equations (8a) and (8b) were modified to define an equivalent strain so that equation (8a) was transformed to

$$\varepsilon_{eq} = e_a + k S_m / E ,$$

and equation (8b) was rewritten as

$$\varepsilon_{eq} = e_a + S_m^\alpha / E .$$

* For unnotched specimens, local equivalent strain was considered to be the same as nominal equivalent strain. For notched specimens, the determination of a local equivalent strain was of prime interest.
The second general formulation of equivalent stress involves a multiplicative combination of stress factors,

\[ S_{eq} = D \Delta S^\alpha S_{max}^\beta \quad . \quad (9) \]

When the parameters \( D = 1 \), \( \alpha + \beta = 1 \), and \( m = \alpha \), equation (9) describes a form proposed by Walker (ref. 4)

\[ S_{eq} = (\Delta S)^m (S_{max})^{1-m} \quad . \quad (9a) \]

For inelastic stress-strain response, equation (9a) was modified to the following form:

\[ \varepsilon_{eq} = (2\varepsilon_a)^m (S_{max}/E)^{1-m} \quad . \quad (9b) \]

Since \( \varepsilon_a \) was required to define each equivalent strain, it became necessary to calculate the strain amplitude in cases where it was not measured during the test. The following section briefly outlines this calculation procedure.

**Strain-Amplitude Determination by Use of the Cyclic Stress-Strain Curve.**

In tests performed under strain control, values for \( \varepsilon_a \) and \( S_m \) (or \( S_{max} \)) were known. However, in load control tests, only values of \( S_m \) (or \( S_{max} \)) and \( S_a \) were known and \( \varepsilon_a \) had to be calculated. Use of the cyclically stable stress-strain curve provided a good estimate of \( \varepsilon_a \) from known values of \( S_a \). A logarithmic trilinear approximation of the cyclic stress-strain curve was defined as follows:

\[ S_a = E\varepsilon_a, \quad 0 \leq S_a(1) \] ,

\[ S_a = K_1\varepsilon_a^{n_1}, \quad S_a(1) < S_a \leq S_a(2) \] ,

\[ S_a = K_2\varepsilon_a^{n_2}, \quad S_a(2) < S_a \] .

(10)

Appropriate values of the equation parameters for the investigated materials are presented in table 1. Experimental cyclic stress-strain data from the present study are detailed in Appendix B.

A number of different parameter values are indicated for Ti-6Al-4V because cyclic as well as monotonic properties for the material vary greatly, depending on processing and product form. When the titanium data were analyzed, the set of cyclic and monotonic values which appeared to most reasonably represent the cyclic and monotonic stress-strain behavior of the material were used.

**Selection of a Method.** Initial investigations showed that all three equivalent strain formulations [eqs. (8c), (8d), and (9b)] provided good mean
<table>
<thead>
<tr>
<th>Material</th>
<th>E, MN/m² (ksi)</th>
<th>K₁, MN/m² (ksi)</th>
<th>K₂, MN/m² (ksi)</th>
<th>S_a1, MN/m² (ksi)</th>
<th>S_a2, MN/m² (ksi)</th>
<th>e_a1</th>
<th>e_a2</th>
<th>n₁</th>
<th>n₂</th>
</tr>
</thead>
<tbody>
<tr>
<td>2024-T4 Bar⁴</td>
<td>70 300 (10 200)</td>
<td>1 165 (169)</td>
<td>676 (98)</td>
<td>414 (60)</td>
<td>572 (83)</td>
<td>0.0059</td>
<td>0.0275</td>
<td>0.200</td>
<td>0.048</td>
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<tr>
<td>2024-T3 Sheet⁵</td>
<td>73 100 (10 600)</td>
<td>5 135 (745)</td>
<td>917 (133)</td>
<td>358 (52)</td>
<td>435 (63)</td>
<td>0.0049</td>
<td>0.0071</td>
<td>0.499</td>
<td>0.150</td>
</tr>
<tr>
<td>7075-T6 Bar⁴</td>
<td>71 000 (10 300)</td>
<td>1 406 (204)</td>
<td>896 (130)</td>
<td>483 (70)</td>
<td>662 (96)</td>
<td>0.0068</td>
<td>0.0285</td>
<td>0.213</td>
<td>0.087</td>
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<tr>
<td>7075-T6 Sheet⁵</td>
<td>72 400 (10 500)</td>
<td>22 260 (3 230)</td>
<td>2 550 (370)</td>
<td>326 (47)</td>
<td>465 (67)</td>
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<td>0.0071</td>
<td>0.782</td>
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<tr>
<td>300M Billet⁵</td>
<td>199 900 (29 000)</td>
<td>17 370 (2 520)</td>
<td>7 240 (1 050)</td>
<td>1 140 (165)</td>
<td>1 520 (220)</td>
<td>0.0057</td>
<td>0.0098</td>
<td>0.529</td>
<td>0.339</td>
</tr>
<tr>
<td>Ti-6Al-4V Plate⁵</td>
<td>110 300 (16 000)</td>
<td>6 650 (965)</td>
<td>2 400 (348)</td>
<td>618 (90)</td>
<td>7 55 (111)</td>
<td>0.0056</td>
<td>0.0089</td>
<td>0.458</td>
<td>0.240</td>
</tr>
<tr>
<td>Ti-6Al-4V Cylindrical Forging⁵</td>
<td>115 100 (16 700)</td>
<td>8 890 (1 290)</td>
<td>2 140 (310)</td>
<td>702 (102)</td>
<td>828 (120)</td>
<td>0.0061</td>
<td>0.0081</td>
<td>0.493</td>
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<tr>
<td>Ti-6Al-4V Hot Rolled Bar⁶</td>
<td>108 900 (15 800)</td>
<td>3 915 (568)</td>
<td>1 340 (194)</td>
<td>741 (107)</td>
<td>828 (120)</td>
<td>0.0068</td>
<td>0.0105</td>
<td>0.341</td>
<td>0.104</td>
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<tr>
<td>Ti-6Al-4V Bar⁷</td>
<td>110 300 (16 000)</td>
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<td>1 870 (272)</td>
<td>794 (115)</td>
<td>978 (142)</td>
<td>0.0072</td>
<td>0.0110</td>
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<td>0.144</td>
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</table>

⁴Values based on data of Endo and Morrow (ref. 16) and Landgraf, et al. (ref. 17).
⁵Values based on data generated at BCL.
⁶Annealed condition, based on unpublished BCL data.
⁷Annealed condition, coarse microstructure, from Gamble (data source ref. 90).
⁸Annealed condition, fine microstructure, from Gamble (data source ref. 90).
⁹STA condition, from Smith, et al. (ref. 18).
stress data consolidations. Subsequently, the three methods were analyzed in
detail to determine which method gave the best overall results.

As stated previously, the major objective in selecting an equivalent strain
formulation was to consolidate fatigue test data generated at different stress
ratios so that all data for a particular material might be treated as one set
and be represented by a single curve. Examination of the Stulen and Topper-
Sandor equivalent strain relations [eqs. (8c) and (8d)] reveals that data gener-
ated at nonzero mean stress values are adjusted by a factor related to the mag-
nitude of the equation parameters $k$ or $\alpha$, so that the data more closely repre-
sent zero mean stress data trends. The best value of $k$ or $\alpha$ is determined by
the relative influence on fatigue life of mean stress as compared to alternating
stress. A high value of $k$ or $\alpha$ indicates a large mean stress effect.

An analogous situation exists for the Walker formulation [eq. (9b)]. Mean
stress is not present directly in the formulation but it can be easily intro-
duced because $S_m = S_{\text{max}} - S_a$. In this case, lower values of $m$ imply greater
effect of mean stress, since lowering the $m$ value increases the exponent on $S_{\text{max}}'$,
making a change in $S_{\text{max}}$ (and therefore $S_m$) more important relative to $e_{a_{\text{max}}}$.

To determine the best values of $k$, $\alpha$, and $m$, a third order polynomial equa-
tion [eq. (1)] was fit to selected data sets for each definition of equivalent
strain. Which of these three constants was optimized, depended upon which
definition of equivalent strain was used. The constant $k$ was used for the Stulen
method [eq. (8c)], $\alpha$ was used for the Topper-Sandor method [eq. (8d)], and $m$ was
used for the Walker method [eq. (9b)]. The polynomial was used because it fit the
results quite well in the region of available data and because it provided a
convenient tool for comparison of the degree of data collapse obtainable for each
equivalent strain equation. It was found, however, that the polynomial behaved
unrealistically outside the range of data. This did not inhibit its use as a
comparative tool, but did create some doubt as to the polynomial's usefulness in
providing a functional relationship between equivalent strain and fatigue life.
This problem will be discussed further in a later section.

In using equation (1), equivalent strain was treated as the dependent vari-
able (i.e., $Y = \epsilon_{eq}$), and the logarithm of fatigue life was treated as the inde-
dependent variable (i.e., $X = \log N_f$). The equation coefficients ($A_0$, $A_1$, $A_2$, and
$A_3$) were determined by least squares regression. Depending upon which of the
three methods was used, an optimum value of the material constant ($k$, $\alpha$, or $m$)
was determined by iteratively conducting the regression analysis until a minimum
value of the standard error of estimate was obtained. Results for five differ-
etent sets of smooth-specimen data are summarized in table 2. All data points
<table>
<thead>
<tr>
<th>Method</th>
<th>Number of Data Points</th>
<th>( R^2 ), percent</th>
<th>( R_m^2 ), Percent</th>
<th>Material(^a)</th>
<th>Regression Coefficients for 3rd Degree Polynomial</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td>Constant</td>
<td>( B_1 )</td>
</tr>
<tr>
<td><strong>2024-T4 Bar(^b)</strong></td>
<td></td>
<td></td>
<td></td>
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<td></td>
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<tr>
<td>Stulen</td>
<td>18</td>
<td>97</td>
<td>96</td>
<td>0.444</td>
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<tr>
<td>Walker</td>
<td>18</td>
<td>96</td>
<td>95</td>
<td>0.324</td>
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<td>18</td>
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<td>96</td>
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<tr>
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<td></td>
<td></td>
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<tr>
<td>Stulen</td>
<td>64</td>
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<td>91</td>
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<td>Topper-Sandor</td>
<td>64</td>
<td>92</td>
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<tr>
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<td></td>
<td></td>
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<tr>
<td>Stulen</td>
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<td>91</td>
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<td>6.28 x 10^{-5}</td>
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<td>Walker</td>
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<td>92</td>
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<td>Topper-Sandor</td>
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<td>90</td>
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<td><strong>Ti-6Al-4V Bar(^d)</strong></td>
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<tr>
<td>Stulen</td>
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<td>84</td>
<td>0.564</td>
<td>1.11 x 10^{-1}</td>
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<tr>
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<td>93</td>
<td>0.354</td>
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<tr>
<td>Topper-Sandor</td>
<td>18</td>
<td>88</td>
<td>85</td>
<td>0.870</td>
<td>1.13 x 10^{-1}</td>
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<tr>
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<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Stulen</td>
<td>69</td>
<td>85</td>
<td>84</td>
<td>0.480</td>
<td>2.67 x 10^{-5}</td>
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<tr>
<td>Walker</td>
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<td>85</td>
<td>84</td>
<td>0.366</td>
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<td>Topper-Sandor</td>
<td>69</td>
<td>85</td>
<td>84</td>
<td>0.852</td>
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</table>

\(^a\) Value of \( k \) for Stulen method; value of \( m \) for Walker method; and value of \( \sigma \) for Topper-Sandor method.

\(^b\) Data reported by Topper and Morrow (data source ref. 13), negative mean stresses excluded.

\(^c\) Data reported by Grover, et al. (data source ref. 1).

\(^d\) Data reported by Titanium Metals Corporation of America (data source ref. 70), bar stock was in the annealed condition.

\(^e\) Data reported by Dateh, et al. (data source ref. 14).
were equally weighted in the analysis, and results for specimens that did not fail (i.e., runouts) were excluded.

After performing the regression analysis for each material with each formulation, a review of the results did not provide sufficient evidence for the selection of one method of defining equivalent strain in preference to the other two. In four out of five data sets, the Walker method was as good or better in terms of $R^2$ than the Stulen and Topper-Sandor equations. In the one instance, where the regression fit was poorer, the $R^2$ value was still a very high 96 percent.

The Walker method was attractive for one other major reason - the formulation used for stress-ratio compensation in the consolidation of fatigue data was exactly analogous to the equation found useful in the consolidation of fatigue-crack-propagation data obtained from tests at different stress ratios. In a real structure, where flaw initiation and propagation both may represent a significant percentage of the useful service life, it is expedient to treat both phases as two interrelated parts of a single damage process rather than as separate phenomena. Therefore, an equation such as the Walker equivalent-strain equation, which compensates for stress-ratio effects in the same manner for both initiation and propagation, appeared to be the most useful method of the three investigated.

Further investigations were then conducted using the Walker formulation to determine the importance of specifying an exact value for $m$. Since the $m$ value provided a compensation on stress ratio, it seemed likely that the optimum value of $m$ determined by regression for a given data set was related to the stress-ratio values for which it was optimized. This was found to be true in a regression analysis performed on 2024-T3 sheet data, in which $R = -1.0$ data were excluded. This screening of the data reduced the $m$ value from 0.41 to 0.39. Although the difference was only slight, it did indicate that an exact specification of $m$ for a particular material was somewhat unrealistic. To choose a reasonable approximate value, however, it was necessary to determine how much deviation from optimum was allowable in the specification of $m$ before drastic reductions in $R^2$ would occur. Figure 13 illustrates the results of a study performed on unnotched 2024-T3 sheet data. The percentage reduction in $R^2$ is plotted as a function of the deviation from the optimum value of $m$. The $R^2$ value was reduced less than one percent for all values of $m$ within 0.07 of the optimum value. Deviations in $m$ greater than 0.07 from the optimum caused substantial $R^2$ reductions, with large deviations in $m$ (> 0.20) causing reductions in $R^2$ of over 10 percent.
Figure 13. - Sensitivity of data consolidation to variation in m value.
After reviewing the data for all the investigated materials, it appeared reasonable to attempt usage of a single optimum $m$ value for all the data. Table 3 indicates the resultant decrease in $R^2$ for each material when an $R^2$ value of 0.40 was chosen. The greatest $R^2$ reduction occurred with a titanium data sample in which an approximately 0.60 percent reduction was observed. Since even this reduction was comparatively small, an $m$ value of 0.40 was used in all later analyses.

TABLE 3
REDUCTION IN $R^2$ RESULTING FROM SPECIFICATION OF $m$

<table>
<thead>
<tr>
<th>Material</th>
<th>Optimum $m$ Value</th>
<th>Optimum $R^2$, percent</th>
<th>TSS</th>
<th>SSD for $m = 0.40$, percent</th>
<th>Reduction in $R^2$, percent</th>
</tr>
</thead>
<tbody>
<tr>
<td>2024-T3 Sheet</td>
<td>0.414</td>
<td>91.55</td>
<td>167.9</td>
<td>14.24</td>
<td>0.03</td>
</tr>
<tr>
<td>7075-T6 Sheet</td>
<td>0.403</td>
<td>86.29</td>
<td>28.43</td>
<td>3.894</td>
<td>0.00</td>
</tr>
<tr>
<td>300M Billet</td>
<td>0.366</td>
<td>77.02</td>
<td>33.02</td>
<td>7.725</td>
<td>0.41</td>
</tr>
<tr>
<td>Ti-6Al-4V Bar</td>
<td>0.426</td>
<td>86.09</td>
<td>13.87</td>
<td>2.012</td>
<td>0.59</td>
</tr>
</tbody>
</table>

aData reported by Grover, et al (data source ref. 1).

bData reported by Bateh, et al (data source ref. 14).

cData reported by Titanium Metals Corporation of America (data source ref. 70), bar stock was in the annealed condition.

Local Stress and Strain Approximations in Notched Specimens

Beyond the consolidation of smooth-specimen data through mean-stress compensation, it was also of interest to combine notched-specimen data in a similar fashion by appropriately accounting for notch effects. Since values of $e_a$ and $S_{\text{max}}$ were used to calculate equivalent strain values for unnotched specimens, it
also seemed reasonable to calculate equivalent strain values for notched specimens in exactly the same way by using adjusted values of $e_a$ and $S_{\text{max}}$, which would be representative of local strain amplitudes and maximum-stress levels.

**Estimation of Local Alternating Stresses and Strains.** — Smooth-specimen simulations of local stress-strain behavior in notched specimens (ref. 19) indicate that combined strain hardening and stress relaxation often occur at the notch tip during constant-amplitude nominal-stress cycling. To estimate stable local values of alternating stress and strain from nominal values, it is necessary to compensate for this combined hardening and relaxation. Research (ref. 20) has shown that the effects of strain hardening or softening can be accounted for by using a cyclic stress-strain curve in combination with nominal alternating strain values modified by an appropriate notch-concentration factor, such as $K_t$, $K_f$, or $K_e$.

All three modifying factors were investigated to determine which one gave the most reasonable indication of the local strain concentration. Consolidation of notched-specimen fatigue data was considered to be a measure of how well local strain was estimated.

**$K_t$ as a Strain-Concentration Factor.** — The theoretical stress-concentration factor was used extensively in initial investigations as an estimate of the effective strain magnification at the notch root. In this way, local strain amplitude was estimated as follows:

$$
e_a = \frac{K_t S_a}{E}$$

which is equivalent to the more general form

$$
e_a = K_t e_a$$

when nominal strains are elastic. This method was found undesirable in further investigations because estimated strains were unrealistically high and conservative in cases where conditions of high nominal stress amplitude and high $K_t$ existed.

The Neuber Rule and $K_e$. — As an alternative, the strain-concentration factor was next investigated. This factor can be calculated by several different methods, but the most commonly used method employs a relationship developed by Neuber (ref. 21) which states that

$$K_t = (K_0 K_e)^{\frac{1}{3}}$$
The value of $K_\sigma$ can be written as

$$K_\sigma = \frac{\sigma_a}{S_a},$$

(13)

and $K_\varepsilon$ can be written similarly as

$$K_\varepsilon = \frac{\varepsilon_a}{e_a}.$$  

(14)

Thus, equation (12) can be rewritten as

$$K_t = \left(\frac{\sigma_a}{S_a} \frac{\varepsilon_a}{e_a}\right)^{1/2}.$$  

(15)

If equation (11) is used to define $\varepsilon_a$ and the stress-strain function of equation (10) is used to define $\sigma_a$, it is possible to rewrite equation (15) so that $\varepsilon_a$ is given in terms of known values of $K_t$, $S_a$, and $e_a$, and appropriate values of $K_1$, $K_2$, $n_1$, and $n_2$. Three different equation forms may result, depending on whether the nominal and local strains are elastic or plastic.

Case 1.- If both local and nominal stress and strain are elastic, equation (15) reduces to equation (11a).

Case 2.- If local stress and strain are plastic and nominal stress and strain are elastic, the insertion of the elastic modulus and the stress-strain function of equation (10) into equation (15) gives

$$K_1 (or \ K_2) \ v_a \ n_1 (or \ n_2) = (S_a K_t)^{3/2}.$$  

(16)

Solving equation (16) in terms of local strain yields

$$\varepsilon_a = \exp\left[\ln(S_a K_t) / (E K_1 (or \ K_2)) / (n_1 (or \ n_2) + 1)\right].$$  

(17)

Case 3.- If both local and nominal stresses are plastic, equation (10) must be used for both nominal and local stress-strain behavior, so that equation (15), in general form, is rewritten as

$$K_1 (or \ K_2) \ v_a \ n_1 (or \ n_2) = K_1 (or \ K_2) \ v_a \ n_1 (or \ n_2) + 1 / K_t ^{2/3}.$$  

(18)

* When equation (10) is used to compute local stress-strain response, $S_a$ and $e_a$ are replaced by $\sigma_a$ and $\varepsilon_a$, respectively.
Simplification of equation (18) reveals that local strain amplitude for the fully plastic condition is given by

$$
e_a = \exp[\ln(K_1 \text{or } K_2)e_a^{n_1 \text{or } n_2}(K_t \text{or } K_e)/K_1(\text{or } K_2))/(n_1 \text{or } n_2 + 1)] . \tag{19}$$

In general, the constant terms, $K_1$, $K_2$, $n_1$, and $n_2$, on the left and right sides of equation (19) may have different values and must be treated separately.

A computerized solution of these equations then yields a means of local strain (or stress) determination through application of the Neuber Rule. It should be pointed out that Case 3 is rarely encountered in most practical applications. It is included in the discussion for the sake of completeness.

To determine the degree of data consolidation possible using the Neuber method of local strain determination, local stresses and strains for notched fatigue data were calculated from equations (11a), (17), and (19). Comparison of calculated equivalent strains for test data at different $K_t$ values and zero mean stress revealed that unrealistically high strain amplitude estimates were calculated in cases involving high levels of nominal strain and $K_t$. Since no method was found to reasonably account for data at these extreme conditions, this method was also considered undesirable, at least when used in the manner outlined herein.

$K_f$ as a Stress and Strain Concentration Factor. — As a third possibility, use of $K_f$ was subsequently tested as a means of local strain estimation. This factor can also be written in several different forms; values of $K_f$ calculated in this investigation were based on a method proposed by Peterson (ref. 22),

$$K_f = 1 + \frac{K_t - 1}{1 + \rho/r} . \tag{20}$$

This expression was selected for use because it is simple and has been shown (ref. 23) to work reasonably well in comparison to a number of other methods of calculating $K_f$. Also, it offered a possible solution to the problems observed when using $K_t$ or $K_e$ as a strain multiplier, where data fell further above the unnotched equivalent strain curve as the value of $K_t$ increased.

Analysis of various notched-specimen data sets helped support this idea. Using a computer procedure to optimize the value of $\rho$ for a given material, it was possible to account for even the highest values of $K_t$. Results were good enough to warrant the use of this method for determination of local cyclic strain amplitudes in all further notched-specimen analyses.

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Table 4 indicates optimum values of \( \rho \) for the four investigated materials. Optimum values for the two aluminum alloys were very similar and it was possible to approximate these values at \( \rho = 0.18 \text{mm (0.007 in.)} \) with a reduction in the optimum value of \( R^2 \) of less than 0.10 percent. The value of 0.18 mm (0.007 in.) is considerably below that recommended by Peterson (ref. 22). His value of 0.63 mm (0.025 in.) gave \( R^2 \) values almost 2 percent lower than the optimized value. This difference was explained in part by the fact that the notched data were analyzed independently from the unnotched data. If the unnotched data had been included, a higher optimum \( \rho \) value would have resulted, because an increase in \( \rho \) would have lowered the overall notched curve, bringing it closer to the unnotched curve. It was considered desirable, however, to separate notched and unnotched data, since higher \( \rho \) values caused layering of the notched data for different \( K_t \).

**TABLE 4**

<table>
<thead>
<tr>
<th>Material</th>
<th>SSD</th>
<th>TSS</th>
<th>( R^2 ), percent</th>
<th>Optimum ( \rho ), mm (in.)</th>
</tr>
</thead>
<tbody>
<tr>
<td>2024-T3 Sheet(^b)</td>
<td>5.37</td>
<td>110.10</td>
<td>95.13</td>
<td>0.21 (0.0083)</td>
</tr>
<tr>
<td>7075-T6 Sheet(^b)</td>
<td>4.73</td>
<td>146.30</td>
<td>96.77</td>
<td>0.17 (0.0067)</td>
</tr>
<tr>
<td>300M Forging(^c)</td>
<td>16.81</td>
<td>153.40</td>
<td>89.04</td>
<td>0.046 (0.0018)</td>
</tr>
<tr>
<td>Ti-6Al-4V Bar(^d)</td>
<td>5.10</td>
<td>21.94</td>
<td>76.76</td>
<td>0.020 (0.0008)</td>
</tr>
</tbody>
</table>

\(^a\)Data were adjusted according to the weighting function \( W(X) \), defined in the next part of the Fatigue Analysis section.

\(^b\)Data reported by Grover et al (data source refs. 2 through 4).

\(^c\)Data reported by Bateh et al (data source ref. 14).

\(^d\)Data reported by Titanium Metals Corp. of America (data source ref. 70).

The optimum \( \rho \) value for the 300M forging data was 0.046 mm (0.0018 in.). This compares with a \( \rho \) value of 0.028 mm (0.0011 in.) which was developed from
Peterson's empirical formula (ref. 22) based upon an ultimate tensile strength of 2000 MN/m² (290 ksi). Although Peterson's value resulted in only a 0.5 percent reduction in $R_e$, the optimized value of 0.046 mm (0.0018 in.) was used in all 300M data consolidation. Since there was substantial scatter in most of the titanium data, a reasonable $\rho$ value was difficult to define. The optimized value of 0.02 mm (0.0008 in.) obtained from a sample of Ti-6Al-4V bar data did appear to provide reasonable consolidation on $K_t$ for most data sets, so this value was used in all subsequent analyses.

**Estimation of Mean and Maximum Stress Levels.** — Even after appropriately determining a local cyclic strain amplitude, it was necessary to develop a method for prediction of the effects of stress relaxation on stable local mean-stress values. Smooth specimen, strain-controlled tests performed at BCL (see Appendix B) indicated that the stable local mean stress under constant-amplitude cycling could be approximated by considering a hypothetical mean stress which would develop after an initial loading cycle, if no hardening or softening occurred during that cycle. The development of this method and experimental results to determine its validity are presented in the following discussion.

Two simple methods of predicting local mean stresses were evaluated using results from strain-controlled tests in which positive mean strains were maintained. As table 5 indicates, especially for the 7075-T6 sheet, the cyclically stable mean stresses were low when $\Delta \varepsilon$ was large, but they were higher when $\Delta \varepsilon$ was small. This reduction of mean stress is related to the amount of plastic deformation that occurs in each cycle.

An understanding of this phenomenon can be found through an examination of the material stress-strain behavior under these conditions. Upon initial loading in tension, deformation will follow the monotonic stress-strain curve (Curve A in fig. 14) and $\sigma$ is related to $\varepsilon$ by some function

$$\sigma = f_m(\varepsilon),$$

Deformation upon reversal of the loading direction (Curve B in fig. 14) will be influenced by the prior loading. If the influence of previous loading is small, Curve B can probably be related to the monotonic stress-strain response. However, if this influence is large, Curve B would be more closely approximated by the stable cyclic stress-strain curve. For intermediate cases, use of a transient cyclic stress-strain curve would be more appropriate.
TABLE 5
COMPARISON OF ACTUAL WITH PREDICTED VALUES OF STABLE MEAN STRESS

<table>
<thead>
<tr>
<th>Specimen</th>
<th>Strain Ratio</th>
<th>Total Strain Range</th>
<th>Actual Mean Stress, MN/m² (ksi)</th>
<th>Predicted Mean Stress By equation (27a) MN/m² (ksi)</th>
<th>Predicted Mean Stress By equation (27b) MN/m² (ksi)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
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<td></td>
</tr>
</tbody>
</table>

**2024-T3 Aluminum Sheet**

<p>| | | | | | |</p>
<table>
<thead>
<tr>
<th></th>
<th></th>
<th></th>
<th></th>
<th></th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>7</td>
<td>0</td>
<td>0.0206</td>
<td>25 (3.6)</td>
<td>8.3 (1.2)</td>
<td>-81.3 (-11.8)</td>
</tr>
<tr>
<td>8</td>
<td>0</td>
<td>0.0153</td>
<td>7.6 (1.1)</td>
<td>8.3 (1.2)</td>
<td>-65 (-9.4)</td>
</tr>
<tr>
<td>6</td>
<td>0</td>
<td>0.0101</td>
<td>15 (2.2)</td>
<td>20 (2.9)</td>
<td>5.0 (0.73)</td>
</tr>
<tr>
<td>10</td>
<td>0.5</td>
<td>0.0100</td>
<td>36 (5.2)</td>
<td>29 (4.2)</td>
<td>15 (2.2)</td>
</tr>
</tbody>
</table>

**7075-T6 Aluminum Sheet**

<p>| | | | | | |</p>
<table>
<thead>
<tr>
<th></th>
<th></th>
<th></th>
<th></th>
<th></th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>8</td>
<td>0</td>
<td>0.0204</td>
<td>49 (7.1)</td>
<td>41 (5.9)</td>
<td>73.8 (10.7)</td>
</tr>
<tr>
<td>9</td>
<td>0</td>
<td>0.0152</td>
<td>43 (6.3)</td>
<td>58 (8.4)</td>
<td>106 (15.4)</td>
</tr>
<tr>
<td>7</td>
<td>0</td>
<td>0.0101</td>
<td>160 (23.2)</td>
<td>188 (27.3)</td>
<td>198 (28.7)</td>
</tr>
<tr>
<td>11</td>
<td>0.5</td>
<td>0.0096</td>
<td>198 (28.8)</td>
<td>247 (35.9)</td>
<td>253 (36.7)</td>
</tr>
</tbody>
</table>
Morrow (ref. 24) has pointed out that stable stress-strain behavior after a reversal in loading can be approximated by multiplying the cyclic stress-strain curve by a factor of 2. Using this observation, the translated stress-strain values of Curve B, could be approximated by the monotonic or cyclic stress-strain function,

\[
\sigma'/2 = f_m (\varepsilon'/2) \quad (22a)
\]

or

\[
\sigma'/2 = f_c (\varepsilon'/2) \quad (22b)
\]

It follows from equation (21) that

\[
\sigma_{\text{max}} = f_m (\varepsilon_{\text{max}}) \quad (23)
\]

From equation (23), it can be shown that

\[
\sigma'_{\text{max}} = 2f_m (\varepsilon'_{\text{max}}/2) \quad (24a)
\]

or

\[
\sigma'_{\text{max}} = 2f_c (\varepsilon'_{\text{max}}/2) \quad (24b)
\]
Then, it follows that

$$\sigma_{\text{min}} = \sigma_{\text{max}} - \sigma'_{\text{max}}$$  \hspace{1cm} (25)

and

$$\sigma_{\text{m}} = \frac{\sigma_{\text{max}} + \sigma_{\text{min}}}{2}$$  \hspace{1cm} (26)

By combining equations (24), (25), and (26) one finds that

$$\sigma_{\text{m}} = \sigma_{\text{max}} - \frac{f_m}{2} (e'_{\text{max}}/2)$$  \hspace{1cm} (27a)

or

$$\sigma_{\text{m}} = \sigma_{\text{max}} - \frac{f_c}{2} (e'_{\text{max}}/2)$$  \hspace{1cm} (27b)

Using equation (10) as the cyclic function ($f_c$) and equation (10) again with monotonic parameters as listed in table 6 as the monotonic function ($f_m$), two predicted values [eqs. (27a) and (27b)] of mean stress were computed for each of the tests with a mean strain. Results of these calculations are compared with the actual stable mean stresses in table 5. Examination of the data shows that use of equation (27a) gave the most reasonable predictions for both alloys. Equation (27b) gave lower predicted values for 2024-T3 aluminum than did equation (27a) because this alloy cyclically hardened. This trend was opposite for 7075-T6 aluminum because it cyclically softened. It is interesting to note that compressive-mean stresses would be obtained with initial loading in compression. Also, it is important to realize that this procedure will not apply to variable-amplitude loading because each loading cycle is influenced by the prior cyclic history. Thus, a more detailed and complete stress-strain analysis as a function of loading history would be required for variable-amplitude conditions.

Establishment of a Relationship Between Equivalent Strain and Fatigue Life

One of the major goals at the outset of this program was to develop the capability to estimate, within a desired confidence, the expected fatigue life of a particular alloy, given information on maximum stress, stress ratio, and (if notched) notch condition. Toward this end, initial work was centered on maximum consolidation of notched and unnotched fatigue data for various combinations of stress concentration and/or mean stress. The Walker equivalent-strain formulation, discussed in earlier sections of this report, was found to be useful in the consolidation process, and good correlations were established between $\varepsilon_{eq}$ and $\log N_f$ through the use of a polynomial expression,

$$\varepsilon_{eq} = A_0 + A_1 \log N_f + A_2(\log N_f)^2 + A_3(\log N_f)^3$$  \hspace{1cm} (28)
## Table 6

### Constants Used to Define Tri-Linear Monotonic Stress-Strain Curves

<table>
<thead>
<tr>
<th>Material</th>
<th>$E_r$ (MN/m²)</th>
<th>$K_1$ (ksi)</th>
<th>$K_2$ (ksi)</th>
<th>$S_a(1)$, (MN/m²)</th>
<th>$S_a(2)$, (MN/m²)</th>
<th>$e_a(1)$</th>
<th>$e_a(2)$</th>
<th>$n_1$</th>
<th>$n_2$</th>
</tr>
</thead>
<tbody>
<tr>
<td>2024-T4 Bar</td>
<td>70 300 (10 200)</td>
<td>841 (122)</td>
<td>462 (67)</td>
<td>274 (40)</td>
<td>379 (55)</td>
<td>0.0039</td>
<td>0.0185</td>
<td>0.200</td>
<td>0.048</td>
</tr>
<tr>
<td>2024-T3 Sheet</td>
<td>73 100 (10 600)</td>
<td>1 013 (147)</td>
<td>431 (62.5)</td>
<td>344 (50)</td>
<td>364 (53)</td>
<td>0.0047</td>
<td>0.0060</td>
<td>0.200</td>
<td>0.032</td>
</tr>
<tr>
<td>7075-T6 Bar</td>
<td>74 000 (10 300)</td>
<td>1 303 (189)</td>
<td>827 (120)</td>
<td>444 (62)</td>
<td>601 (87)</td>
<td>0.0060</td>
<td>0.0265</td>
<td>0.213</td>
<td>0.087</td>
</tr>
<tr>
<td>7075-T6 Sheet</td>
<td>72 400 (10 500)</td>
<td>3 240 (470)</td>
<td>889 (129)</td>
<td>493 (72)</td>
<td>544 (79)</td>
<td>0.0069</td>
<td>0.0086</td>
<td>0.375</td>
<td>0.103</td>
</tr>
<tr>
<td>300M Billet</td>
<td>199 900 (29 000)</td>
<td>24 950 (3 620)</td>
<td>7 860 (1 140)</td>
<td>1 280 (186)</td>
<td>1 590 (231)</td>
<td>0.0064</td>
<td>0.0093</td>
<td>0.588</td>
<td>0.342</td>
</tr>
<tr>
<td>Ti-6Al-4V Plate</td>
<td>110 300 (16 000)</td>
<td>4 450 (645)</td>
<td>1 050 (153)</td>
<td>750 (109)</td>
<td>875 (127)</td>
<td>0.0068</td>
<td>0.0101</td>
<td>0.354</td>
<td>0.032</td>
</tr>
<tr>
<td>Ti-6Al-4V Cylindrical Forging</td>
<td>115 100 (16 700)</td>
<td>5 100 (740)</td>
<td>1 075 (156)</td>
<td>760 (110)</td>
<td>886 (129)</td>
<td>0.0066</td>
<td>0.0100</td>
<td>0.380</td>
<td>0.047</td>
</tr>
<tr>
<td>Ti-6Al-4V Hot Rolled Bar</td>
<td>108 900 (15 800)</td>
<td>4 110 (598)</td>
<td>1 330 (193)</td>
<td>937 (136)</td>
<td>1 010 (147)</td>
<td>0.0086</td>
<td>0.0120</td>
<td>0.318</td>
<td>0.056</td>
</tr>
<tr>
<td>Ti-6Al-4V Bar</td>
<td>110 300 (16 000)</td>
<td>2 860 (415)</td>
<td>1 340 (194)</td>
<td>1 100 (160)</td>
<td>1 170 (170)</td>
<td>0.0100</td>
<td>0.0119</td>
<td>0.202</td>
<td>0.030</td>
</tr>
</tbody>
</table>

*All data are from references as cited in Table 1.*
A major difficulty arose, however, when an attempt was made to establish a measure of confidence in the calculated fatigue lives. Since log $N_f$ was the independent variable in this equation, it was appropriate to establish limits on $e_{eq}$, given log $N_f$, rather than the desired result which would have established confidence limits on log $N_f$, given $e_{eq}$.

**Fatigue Life as a Dependent Variable.**—In order to eliminate the problem discussed above, a variety of new formulations were studied employing log $N_f$ as a dependent variable. The desirability of a given formulation was based on essentially three factors: (1) predictive capability, (2) simplicity, and (3) physical significance.

The first important aspect, predictive capability, was defined solely on the basis of the $R^2$ statistic, which was discussed in the earlier section on statistical analysis. Simplicity in a formulation was also an important factor since the addition of extra terms in an expression often reduces the significance of the coefficients of original terms. Lastly, the physical significance of a particular equation was considered important since a physically meaningful equation, in contrast to an empirically derived one, was more likely to be useful in a general application. This, of course, was true only as long as the initial insight was correct and was properly applied.

The following sections outline a variety of attempted formulations involving log $N_f$ as a dependent variable. They briefly summarize the relative merit of the various equations as applied to notched and unnotched data used in previous evaluations.

**Polynomial Data Fitting.**—The first method investigated for establishing fatigue life as a dependent variable simply involved an interchange of variables in equation (28), making $e_{eq}$ an independent variable so that

$$\log N_f = A_0 + A_1e_{eq} + A_2e_{eq}^2 + A_3e_{eq}^3,$$  \hspace{1cm} (29)

where $e_{eq}$ represented the Walker formulation as expressed in equation (9b). Using equation (29), a regression analysis of selected data sets showed that $R^2$ values were almost equal to those obtained with equation (28). The problem of polynomial uncontrollability outside the range of data still existed, however. To partially eliminate this problem, it was thought useful to define
an intercept value for the polynomial at \( \frac{1}{2} \) cycle of fatigue life in terms of the true fracture ductility, in a manner comparable to that suggested by Morrow (ref. 24).

This operation eliminated one degree of freedom in the polynomial and resulted in slightly better curve definition, but it did not sufficiently improve the overall usefulness of the polynomial as a functional relationship between \( \epsilon_{eq} \) and \( \log N_f \) to warrant its implementation.

**Multivariable Stepwise Regression Analysis.** Much of the analytical work performed in the early phases of this program was centered on usage of the three formulations for equivalent strain, but there was also some interest in and some effort devoted towards the development of alternate functional forms which could give comparable or superior data consolidations. Multivariable stepwise regression was used to test and compare a variety of factors in regard to their usefulness as components of a fatigue life prediction equation.

Two basic equation forms were reviewed, the first of which involved combinations of \( \epsilon_a \) and \( S_m \), as follows:

\[
\log N_f = f(\epsilon_a, S_m) \quad .
\]  

Stepwise multiple regression of equation (30) provided an optimum solution of the form

\[
\log N_f = A_0 + A_1 \epsilon_a S_m/E + A_2 \epsilon_a + A_3 \epsilon_a S_m/E \quad .
\]  

The independent variables are listed in order of significance, with the combination \( \epsilon_a S_m/E \) providing the most significant increase in \( R^2 \) and the terms \( \epsilon_a \) and \( \epsilon_a S_m/E \) providing lesser, yet significant, improvements in \( R^2 \). Including all three variables, the accumulated \( R^2 \) for the equation using unnotched 7075-T6 data was 82.0 percent. This was a much poorer consolidation than that obtained using equation (29).

The second general equation was defined so that combinations of maximum stress and stress ratio or total strain range could be examined,

\[
\log N_f = f(S_{max}, R \text{ or } \Delta e) \quad .
\]  

The optimum solution for this combination of variables was found to be an inverse relationship, written as follows:

\[
\log N_f = \frac{1}{A_0 + A_1 \log S_{max} + A_2(1+R)} \quad .
\]
The $R^2$ value for this functional form using unnotched 7075-T6 data was 90.9 percent which was only slightly less than the value obtained for the third order polynomial using the Walker equivalent strain term. However, this formulation did not appear to be entirely satisfactory either, since it was observed that the regression fit for certain stress ratios was much better than that at others. Also, the data could not be displayed as well graphically since it was necessary to consider two variables ($S_{\text{max}}$ and $R$) in each plot, as compared to a single variable ($\varepsilon_{eq}$) in the polynomial equation. So, investigations were continued in an attempt to discover a simpler formulation which would accurately model the consolidated fatigue data trends.

The Inverse Hyperbolic Tangent Function. — A variety of functions were reviewed in the search for a functional relationship which would provide a useful empirical model for consolidated fatigue data. Hyperbolic, exponential, and power functions were all investigated and found to be unsatisfactory for fitting the complete range of available data. However, the inverse hyperbolic tangent function provided a reasonable model of fatigue data trends throughout the life range of interest, 10 to $10^5$ cycles to failure.

This function, which was chosen and modified specifically to model the sigmoidal shape of the fatigue-crack-propagation ($da/dN$ versus $K_{\text{eff}}$) curve, was also found to provide a useful model of consolidated fatigue data trends. Since this relation is derived in detail in the Fatigue-Crack-Propagation Analysis Section, it is outlined only briefly here in terms of its application to fatigue data.

To implement its usage, the following functional form was established:

$$\log N_f = A_0 + A_1 \text{tanh}^{-1}[\Phi(\varepsilon_{eq})] \quad (34)$$

The scaling function, $\Phi(\varepsilon_{eq})$, was appropriately defined as

$$\Phi(\varepsilon_{eq}) = \frac{\log(\varepsilon_u \varepsilon_e/\varepsilon_{eq}^2)}{\log(\varepsilon_u/\varepsilon_e)} \quad (35)$$

where values of $\varepsilon_u$ and $\varepsilon_e$ were selected to appropriately bound the complete range of data, as illustrated in figure 15. The upper limit, $\varepsilon_u$, was found to be reasonably represented in most cases by the following approximation:

$$\varepsilon_u = \varepsilon_{eq} \left| \frac{N_f}{10} \right| + 0.0025 \quad (36)$$

53
In cases where representative data did not exist at a fatigue life of 10 cycles, it was necessary to estimate a value of $\epsilon_u$. Attempts to define a value for $\epsilon_u$ in terms of true fracture ductility and true fracture strengths resulted in values of $\epsilon_u$ which were unacceptably high. Values for the lower limit, $\epsilon_e$, were well represented by an equivalent strain value approximately corresponding to a fatigue limit. It was determined accordingly as

$$\epsilon_e = \epsilon_{eq} \mid N_f = 10^8 - 0.0005$$

Once again, in cases where representative data did not exist, a reasonable value of $\epsilon_e$ was chosen.

To avoid error in calculation of the inverse hyperbolic tangent function, it was necessary to specify values of $\epsilon_u$ and $\epsilon_e$ which were higher and lower, respectively, than any calculated value of equivalent strain.

**The Weighting Function, W(X).** - To calculate point estimates of variance for establishing tolerance limits on the inverse hyperbolic tangent function, it was necessary (in the case of fatigue) to apply a weighting function to the data in order to satisfy the statistical requirement of uniform variance.
Before this step could be taken, it was important to identify the pattern of changing variance. Examination of plotted residuals revealed that the data scatter often increased substantially at either extreme of the fatigue life range. The increased variance was most evident in long-life fatigue data. It was also in this life range that the slope of the fitted curve was greatest (i.e., a small change in the independent variable, $\varepsilon_{eq}$, corresponded to a large change in the dependent variable, $\log N_f$). Since the variance seemed to be related in some fashion to the slope of the curve, it appeared desirable to establish a weighting function which would modify the residuals (and, therefore, the observed data variance) according to the "steepness" of the fitting function.

Several functions of this type were reviewed. One suggested formulation, involving a weight factor proportional to the square of the slope of the fitted curve, proved to be useful with some modifications. The weighting function was expressable as

$$\frac{1}{W(X)} \propto \left( \frac{d(Y)}{d(X)} \right)^2 = \left( \frac{d(\log N_f)}{d(\varepsilon_{eq})} \right)^2,$$

where the derivative for the inverse hyperbolic tangent expression [eq. (34)] was found to be

$$\frac{d(\log N_f)}{d(\varepsilon_{eq})} = \frac{-2.0 A_1 [\log(\varepsilon_u/\varepsilon_e)(\log \varepsilon)]}{\varepsilon_{eq} \left[ [\log(\varepsilon_u/\varepsilon_e)]^2 - [\log(\varepsilon_u\varepsilon_e/\varepsilon_{eq}^2)]^2 \right]}.$$

To make the weighting function [eq. (38)] independent of the absolute slope of the curve and dependent only on a ratio of slopes at two points along the curve, the derivative [eq. (39)] was normalized through division by a minimum value of that derivative. For the inverse hyperbolic tangent function, the minimum derivative always occurred at the inflection point of the curve which was located midway between the function limits. Therefore, at an equivalent strain given by

$$\varepsilon_{eq} = \frac{\varepsilon_u + \varepsilon_e}{2},$$

* With $\log N_f$ plotted in the customary fashion, along the abscissa, it appears that the slope is actually least in the long-life region. It is useful to consider, however, that $\log N_f = f(\varepsilon_{eq})$, rather than the visually implied relationship, $\varepsilon_{eq} = f(\log N_f)$.

** Based on communication with Lars Sjodahl, General Electric Company, Cincinnati, Ohio, May 8, 1973.
the minimum derivative was defined as*

\[ \left( \frac{d \log N_f}{d \epsilon_{eq}} \right) \bigg|_{\epsilon_u + \epsilon_e} = \frac{-4.0 A_1 [\log(\epsilon_u/\epsilon_e)](\log \epsilon)}{(\epsilon_u + \epsilon_e)[\log(\epsilon_u/\epsilon_e)]^2 - [\log(\epsilon_u\epsilon_e/\epsilon_{eq})]^2} \]  

(41)

Then a combination of equations (38), (39), and (41) resulted in a normalized weighting function, expressable as

\[ W(\epsilon_{eq}) = \left[ \frac{\left( \frac{d \log N_f}{d \epsilon_{eq}} \right)}{\epsilon_u + \epsilon_e} \right]^2 \]  

(42)

The value of \( W(\epsilon_{eq}) \) was then bounded between 0.0 and 1.0 with values near 1.0 at midrange of the fitted curve and values decreasing (according to the square of the ratio of slopes) toward 0.0 at the limits of the curve.

This function was then applied directly to the residuals in the manner shown in Appendix H. Characteristically, the function had almost no effect on data falling in the midrange portion of the curve. It did, however, substantially reduce the relative magnitudes of the residuals near the extremes of the function. The overall effect of this weighting operation was an approximately uniform data variance.

Results of Fatigue Analysis

Up to this point, the discussion has dealt with the various considerations which were involved in the development of the overall fatigue data consolidation and modelling process. The following paragraphs describe the results of those considerations.

A fatigue data consolidation and modelling process was developed through which a conglomerate set of fatigue test data at various mean stresses and notch concentrations could be consolidated into a single curve and be reasonably described by a simple analytical expression. Also, statistical considerations were applied, incorporating weight factors, so that probability of survival curves

* In equations (41) and (42) the vertical slash adjacent to the derivative designates an evaluation of the derivative at the indicated point.
could be constructed about this consolidated data band from which an estimate of simple specimen fatigue life for a given material could be obtained from a single plot, once the controlling parameters \(S_{\text{max}}, \Delta e, K_t, \text{ and } r\) were specified. An outline in Appendix C provides a step-by-step illustration of this procedure.

This process was successfully applied to 2024 and 7075 aluminum alloys in several different product forms and tempers and to 300M steel in the forged condition. It was also used with marginal success on a Ti-6Al-4V alloy, consisting of numerous product forms and heat-treatment conditions.

In these analyses, notched and unnotched specimen data were treated separately because there was a sufficient amount of each type of data to consider them on a statistical basis. When the two types were combined, the \(R^2\) values were decreased by amounts up to about 10 percent. Thus, it would be acceptable to combine notched and unnotched results when there are not enough data to analyze them separately on a statistical basis. A better correlation of notched and unnotched data would have been obtained if a more realistic analysis of notch root stress-strain behavior had been available.

Table 7 summarizes the results of the analyses that were made for each material using the final model incorporating the hyperbolic tangent function. Weighted \(R^2\) values are presented for each combined data set. Also, optimum equation coefficients are listed, along with the function limits which were employed in each consolidation process. The data source references for each material are included in the final column. Graphical displays of the consolidated fatigue data are presented in Appendix D. The best-fit regression curve is drawn through the data and 90 and 99 percent tolerance curves (95 percent confidence) are drawn below that line. Comments concerning individual plots are presented in the introductory comments of Appendix D.

**FATIGUE-Crack-Propagation Analysis**

The determination of the safe life of an aerospace structure must be based on a detailed knowledge of the entire continuum of damage mechanisms. This begins with an understanding of the process of fatigue and its role in leading to the initiation of macrocracks, and continues as these macrocracks grow to a size which may be critical for the complete fracture of a structure or structural component. Once a macrocrack has been initiated, crack growth from the initiation site, due to continuing fatigue damage, must be predicted in a rational
TABLE 7.
RESULTS OF NOTCHED AND UNNOTCHED FATIGUE DATA CONSOLIDATION USING THE INVERSE HYPERBOLIC TANGENT FUNCTION WITH WEIGHTED EQUIVALENT STRAIN DATA

<table>
<thead>
<tr>
<th>Material</th>
<th>Type of Data</th>
<th>Number of Data Points</th>
<th>Weighted R², percent</th>
<th>Regression Coefficients</th>
<th>Limits Employed</th>
<th>Data Source Reference Numbers</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td>A₀, A₂</td>
<td>εₙ, εₑ</td>
<td></td>
</tr>
<tr>
<td>2024-T3 Sheet</td>
<td>Unnotched</td>
<td>121</td>
<td>98.9</td>
<td>4.644, 2.914</td>
<td>0.0152, 0.0018</td>
<td>1, 7, 2 through 9</td>
</tr>
<tr>
<td></td>
<td>Notched</td>
<td>687</td>
<td>96.8</td>
<td>4.867, 3.417</td>
<td>0.0150, 0.0021</td>
<td></td>
</tr>
<tr>
<td>2024-T6 Bar and Rod</td>
<td>Unnotched</td>
<td>62</td>
<td>97.8</td>
<td>4.170, 2.705</td>
<td>0.0150, 0.0020</td>
<td>13, 82</td>
</tr>
<tr>
<td></td>
<td>Notched</td>
<td>114</td>
<td>94.9</td>
<td>4.635, 2.892</td>
<td>0.0150, 0.0020</td>
<td>82</td>
</tr>
<tr>
<td>7075-76 Sheet</td>
<td>Unnotched</td>
<td>220</td>
<td>97.3</td>
<td>4.899, 3.509</td>
<td>0.0150, 0.0016</td>
<td>1, 7, 10</td>
</tr>
<tr>
<td></td>
<td>Notched</td>
<td>695</td>
<td>96.3</td>
<td>4.969, 3.313</td>
<td>0.0170, 0.0020</td>
<td>2 through 10</td>
</tr>
<tr>
<td>7075-76 Clad Sheet</td>
<td>Unnotched</td>
<td>369</td>
<td>99.6</td>
<td>4.408, 1.760</td>
<td>0.0160, 0.0015</td>
<td>91</td>
</tr>
<tr>
<td></td>
<td>Notched</td>
<td>137</td>
<td>87.3</td>
<td>4.587, 2.658</td>
<td>0.0160, 0.0015</td>
<td>82, 87</td>
</tr>
<tr>
<td>7075-76, -T651 Bar</td>
<td>Unnotched</td>
<td>471</td>
<td>93.4</td>
<td>4.818, 2.618</td>
<td>0.0160, 0.0015</td>
<td>82, 87</td>
</tr>
<tr>
<td></td>
<td>Notched</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>300M Billet and Forging</td>
<td>Unnotched</td>
<td>289</td>
<td>90.4</td>
<td>4.796, 2.565</td>
<td>0.0154, 0.0026</td>
<td>11,12,14,88,89</td>
</tr>
<tr>
<td></td>
<td>Notched</td>
<td>218</td>
<td>89.2</td>
<td>5.239, 3.073</td>
<td>0.0161, 0.0023</td>
<td>11, 12, 14</td>
</tr>
<tr>
<td>Annealed Ti-6Al-4V Sheet</td>
<td>Unnotched</td>
<td>76</td>
<td>81.9</td>
<td>6.033, 6.402</td>
<td>0.0160, 0.0020</td>
<td>75, 81</td>
</tr>
<tr>
<td>Bar and Extrusion (125 ksi TYS)</td>
<td>Notched</td>
<td>60</td>
<td>68.1</td>
<td>5.756, 3.218</td>
<td>0.0160, 0.0020</td>
<td>69, 70, 86</td>
</tr>
<tr>
<td>Bar, Extrusion, and Forging (140 ksi TYS)</td>
<td>Notched</td>
<td>367</td>
<td>73.3</td>
<td>5.415, 3.577</td>
<td>0.0160, 0.0020</td>
<td>12,73,76,79,86</td>
</tr>
<tr>
<td>Casting</td>
<td></td>
<td>50</td>
<td>76.6</td>
<td>5.033, 1.044</td>
<td>0.0160, 0.0020</td>
<td>71</td>
</tr>
<tr>
<td>Annealed Ti-6Al-4V Sheet</td>
<td>Notched</td>
<td>28</td>
<td>43.3</td>
<td>6.625, 2.789</td>
<td>0.0160, 0.0020</td>
<td>75</td>
</tr>
<tr>
<td>Bar and Extrusion (125 ksi TYS)</td>
<td>Notched</td>
<td>53</td>
<td>80.8</td>
<td>7.149, 4.140</td>
<td>0.0160, 0.0020</td>
<td>69, 70</td>
</tr>
<tr>
<td>Bar, Extrusion, and Forging (140 ksi TYS)</td>
<td>Notched</td>
<td>171</td>
<td>73.2</td>
<td>6.164, 3.591</td>
<td>0.0160, 0.0020</td>
<td>12, 73, 76, 79</td>
</tr>
<tr>
<td>Casting</td>
<td></td>
<td>78</td>
<td>86.1</td>
<td>5.862, 3.354</td>
<td>0.0160, 0.0020</td>
<td>71, 72, 80</td>
</tr>
<tr>
<td>STA Ti-6Al-4V Sheet</td>
<td>Unnotched</td>
<td>98</td>
<td>95.1</td>
<td>4.565, 1.967</td>
<td>0.0160, 0.0020</td>
<td>84</td>
</tr>
<tr>
<td>Forging, Casting, and Plate</td>
<td>Notched</td>
<td>50</td>
<td>79.0</td>
<td>5.897, 4.100</td>
<td>0.0160, 0.0020</td>
<td>78, 79</td>
</tr>
<tr>
<td>STA Ti-6Al-4V Sheet</td>
<td>Notched</td>
<td>96</td>
<td>85.0</td>
<td>6.905, 3.909</td>
<td>0.0170, 0.0020</td>
<td>84</td>
</tr>
<tr>
<td>Casting and Plate</td>
<td>Notched</td>
<td>28</td>
<td>88.6</td>
<td>5.848, 2.177</td>
<td>0.0160, 0.0020</td>
<td>78, 80</td>
</tr>
</tbody>
</table>

*Monotonic and cyclic stress-strain calculations were based on data from Ti-6Al-4V Hot Rolled Bar (see tables 1 and 6).*

*Monotonic and cyclic stress-strain calculations were based on data from Ti-6Al-4V Plate (see tables 1 and 6).*

*Monotonic and cyclic stress-strain calculations were based on data from Ti-6Al-4V Cylindrical Forging (see tables 1 and 6).*

*Monotonic and cyclic stress-strain calculations were based on data from Ti-6Al-4V Bar (see tables 1 and 6).*
manner. Since an accurate physical model of crack-tip damage accumulation does not exist, a fatigue-crack-propagation model that accurately characterizes the mechanical behavior of the material is generally used. Then the model, which summarizes or characterizes experimental results, must be inverted to yield predictions of structure life under given loading conditions.

This section of the report describes the formulation of a phenomenological, fatigue-crack-propagation model. The initial subsection on mechanical behavior, which describes the basic characteristics of the crack-growth process, is followed by a discussion of the problem of modelling this process. This latter subsection is broken down into descriptions of formulating the dependent variable, independent variable, and analytical model. Methods of evaluating crack-growth rate as the dependent variable are discussed in detail. The independent variable portion explains various functions used to account for the effects of stress ratio. Based on the results of the above work, various analytical models, including a nonlinear analytical expression, are examined in Formulation of an Analytical Model. The final subsection details the application of the analytical model to five sets of data.

Observed Mechanical Behavior

Studies have been conducted in numerous laboratories to obtain fatigue-crack-propagation data for various materials. Extensive tests have been performed by various investigators utilizing center-cracked, compact-tension, and surface-flaw specimens. Data have been generated on high-strength steel, aluminum, and titanium alloys under both constant- and variable-amplitude loading conditions. The present investigation, however, is concerned only with constant-amplitude results. Fatigue-crack-propagation data, recorded in the form of crack-length measurements and cycle counts \((a_i, N_i)\) are not directly useful for design purposes since a variety of stress levels, stress ratios, initial crack conditions, and environmental conditions are encountered. To make use of these data, a fatigue-crack-propagation model must account for the effects of these parameters on crack growth and, hence, on specimen life.

In general, the relationship between crack size and number of applied cycles can be represented as a crack-growth curve drawn through the raw data points as shown in figure 16. The resulting monotonic curve is described in terms of two intervals connected by a transition region.
(1) A region (Region 1) of slow growth over a wide range of cycles where the slope is relatively small.

(2) A region (Region 2) of exceedingly rapid growth until failure or test termination.

Families of curves for a given material are generated when the maximum stress, stress ratio, or environmental conditions are varied.

Historically, it has been found convenient to model this crack-damage behavior as a rate process and to formulate a dependent variable based on the slope of the growth curve. The instantaneous rate of change of crack length, or an approximation to it,

\[ \frac{da}{dN} \sim \frac{\Delta a}{\Delta N} \]

was chosen as the dependent variable for the formulation of a fatigue-crack-propagation model. The independent variable for the process was selected to account for the more basic mechanical variables of cyclic stress, stress ratio, and crack size.

An appeal to the theory of linear elasticity has suggested that the damage severity at the crack tip might be represented by a stress-intensity factor which, in general form, may be written as

\[ K = \frac{S}{\sqrt{a}} g(a,w) \]

where \( g(a,w) \) is a geometric scaling function dependent on crack and specimen geometry. As a result, the independent variable is usually considered as some function of \( K \) and stress ratio, or as originally suggested by Paris et al (ref. 25), some function of

\[ \Delta K = (1-R)K \]

If the slope of the crack-growth curve is calculated at the various data points, and if the stress-intensity factor is calculated at these same points, then the locus of points \( \left( \frac{da}{dN}, K \right) \) can be plotted. These variables are generally plotted on log-log scales to obtain a crack-growth-rate curve such as that shown in figure 17. Examination of this curve suggests several factors of importance that will have to be accounted for in the formulation of a crack-growth model.

In most materials, there is an upper limit to the crack severity and associated critical stress-intensity factor which a material can sustain. At this critical value, the crack will propagate unstably. For the rate diagram of \( \frac{da}{dN} \) versus \( \Delta K \) or \( K_{\text{max}} \), the \( K_{\text{c}} \) value is the terminal (or upper) limit on the abscissa as illustrated schematically in figure 17. On a \( K_{\text{max}} \) basis, the rate of crack growth becomes very large as \( K_{\text{max}} \) approaches \( K_{\text{c}} \), such that the growth-rate curve...
Figure 17. - Typical crack-growth-rate behavior.
becomes asymptotic to this limit. On a $\Delta K$ basis, this limit is $(1-R)K_c$. At the other extreme, a minimum crack-growth rate of zero is anticipated at a zero value of $\Delta K$ or $K_{\text{max}}$ value. However, this assumption appears to be conservative because of evidence that there actually exists a threshold below which there is no fatigue-crack propagation. (See fig. 17.)

The doubly logarithmic plot of $\frac{da}{dN}$ versus $K$ reveals a curve having sigmoidal shape. As an approximation, the curve might be represented by three linear segments. The first segment, beginning with crack initiation at $K_0$, is steeply sloped and indicates rapid rate of change of crack-growth rate. The second segment represents a longer interval of slower rate of change of crack-growth rate. The third segment also has a high slope and represents rapid, terminal crack growth near $K_c$. Most of the available test data lies in the second interval.

Within the general curve shape, described above, systematic variations in the data point locations are observed. When data from tests conducted at several different stress ratios are present, the plot of crack-growth rate versus stress-intensity factor will be layered into distinct bands about the locus of points having zero stress ratio. (Refer to fig. 3 on page 7.) Layering of data points also occurs as a result of variation in such parameters as test frequency, environment, and specimen grain direction. It is desirable to predict the characteristic effects of each parameter; thus, many researchers have formulated mathematical models accounting for these parametric effects. Assuming the variables $K$, $R$, and $\frac{da}{dN}$, the general form for the fatigue-crack-propagation model was established as

$$\frac{da}{dN} = f(K, R) \quad (46)$$

The following discussion describes efforts to obtain a useful functional form for $f(K, R)$.

Structure of the Modelling Problem

The basic concepts discussed in the previous section suggest that the modelling procedure can be thought of as consisting of three distinct steps.

1) Formulation of a dependent variable. - How can the crack-growth rates be best calculated from the discrete $(a_i, N_i)$ data points?
(2) **Formulation of an independent variable.** — What combination of R and K can best be used to formulate an independent variable that will consolidate the crack-growth-rate data?

(3) **Formulation of an analytical model.** — What functional form containing the dependent and independent variables should be chosen to best approximate the sigmoidal character of the crack-growth-rate curve?

An approach to the solution of these three modelling problems is described in the following subsections.

Particular effort was devoted to obtaining an expression in which compensations for the effects of stress ratio were uncoupled from the factors influencing general curve shape. Such a feature permits a greater flexibility in the analysis of fatigue-crack-propagation data. Although several parameters affect the distribution of data points, stress ratio is the most significant of these. Accounting for other important parameters, such as frequency, was beyond the scope of the present work.

**Formulation of a Dependent Variable.** — It is necessary to obtain values for the dependent variable, the crack-growth rate, from the \((a_i, N_i)\) data. Two basic methods of deriving the crack-growth rate have been used in the past; curve fitting and incremental-slope approximation. Curve fitting implies that an analytical expression is fitted to all of the crack-growth data by least-squares regression. Incremental-slope calculation implies the use of a divided differences scheme to find the slope at any given point along the crack-growth curve.

From the analyses conducted, it is apparent that the determination of such a derivative by means of some analytical expressions is far less desirable than the use of a local or segmental fit to the data. Since this observation has been made in all of the data sets analyzed, a formalized illustration of the inadequacies of the fitting of a single analytical expression is presented.

Of the general analytical expressions which are available for curve fitting, the most popular choice of functions with respect to numerical considerations are polynomials. To explore the application of polynomials in fitting the crack-growth curve, one must consider the characteristics of the crack-growth curve. Typically, two regions of the curve from crack initiation to specimen failure may be described as done earlier and shown in figure 16. These curve segments are connected by a transition region having a considerably smaller radius of curvature. It is observed that over the entire range of cyclic values, the curve is monotonically increasing.
Some general observations can be made about polynomials that are relevant to this situation. Consider a polynomial of degree q,

\[ a(N) = A_0 + A_1N + A_2N^2 \ldots + A_qN^q \quad (47) \]

The first derivative of equation (47) is expressed by the following relation:

\[ \frac{da}{dN} = A_1 + 2A_2N + \ldots + (q-1)A_qN^{q-1} \quad (48) \]

Equation (48) possesses q roots implying a finite number, q - 1, of extrema over the range of the function. Since the polynomial is not a strictly monotone function over its range, it is necessary to utilize the function on regions where it does display monotone behavior. The existence of extrema in a candidate curve-fitting function presents very real difficulties. Sections of the curve having negative slope due to extrema would represent the physically impossible situation of negative crack growth. Such a result is unacceptable. Furthermore, since it is generally desirable to obtain the logarithms of the crack-growth rates, \( \log(\frac{da}{dN}) \), also will be undefined at points having negative slope.

Figure 18 represents attempts to fit second through seventh degree polynomials to a typical crack-growth curve. These particular data were obtained from a 9.6-inch-wide, centrally cracked panel of 0.29-inch-thick, mill-annealed Ti-6Al-4V plate tested at a maximum cyclic stress of 5 ksi and a stress ratio of 0.1. No terms greater than degree seven were added because of computational difficulties encountered in dealing with the coefficients. Successive addition of higher order terms improved the fit of the polynomial to the data as indicated by the sum of squares of deviation listed in table 8. Although the higher order terms improved the fit, they introduced extrema with their resulting negative slopes. Because of these extrema, the fitted functions obtained are unsatisfactory models of crack growth.

**TABLE 8.**

**COMPARISON OF CURVE FITTING RESULTS FOR POLYNOMIALS OF DEGREE q = 2 TO q = 7**

<table>
<thead>
<tr>
<th>Degree of Polynomial</th>
<th>SSD</th>
</tr>
</thead>
<tbody>
<tr>
<td>2</td>
<td>7.4038</td>
</tr>
<tr>
<td>3</td>
<td>3.8250</td>
</tr>
<tr>
<td>4</td>
<td>2.1020</td>
</tr>
<tr>
<td>5</td>
<td>1.2387</td>
</tr>
<tr>
<td>6</td>
<td>0.7809</td>
</tr>
<tr>
<td>7</td>
<td>0.5254</td>
</tr>
</tbody>
</table>

Examination of figure 18 reveals a very close fit of data in the region of high crack-growth rate for q = 6 and q = 7. In this situation, where only
Figure 18. - Crack-growth data with best fit polynomial for Ti-6Al-4V plate.
isolated segments of the crack-growth curve are to be dealt with, the polynomials
gave good results. However, this type of function seems to be unsuited to appli-
cation to the whole cyclic range. Thus, either the selection of another class of
candidate functions for curve fitting or an appeal to point-to-point methods of
slope evaluation was necessary.

Several other curve-fitting functions were examined. Among these was an
exponential series,
\[ a(N) = \sum_{i=0}^{q} A_i e^{iN} \]  
(49)

Cases of \( q = 1 \) and \( q = 3 \) were tried, but no improvement was found.

The point-to-point method of slope evaluation involved use of the various
divided difference schemes. The first divided difference was merely the slope
between two adjacent points; thus
\[ \text{DD} 1(i) = \frac{\Delta a}{\Delta N} = \frac{a_{i+1} - a_i}{N_{i+1} - N_i} \]  
(50)

Since the crack growth achieved between two data points was usually small,
observational errors, measurement errors, and subtle material variations influ-
enced the rate evaluation. With this technique, each rate or slope determination
was defined entirely by the local conditions. An averaging of these variations
was achieved by using higher order divided-difference schemes. In the next
level of refinement, the three-point divided-difference technique, a selection
of successive subsets of three data points was used to specify the derivative
at the central point. By using Newton's interpolation formula to define a
second-degree polynomial through the three data points, we may express the
derivatives at the intermediate point \( i \) as
\[ \frac{da}{dN}\big|_i = f[N_{i-1}, N_i] + (N_i - N_{i-1}) \left( \frac{f[N_{i-1}, N_i+1] - f[N_{i-1}, N_i]}{N_{i+1} - N_{i-1}} \right) \]  
(51)

where
\[ f[N_{i-1}, N_i] = \frac{a_i - a_{i-1}}{N_i - N_{i-1}} \]
and
\[ f[N_i, N_i+1] = \frac{a_{i+1} - a_i}{N_{i+1} - N_i} \]
are the first divided differences. From a physical perspective, this can also
be viewed as a slope-averaging technique since the first divided differences are
merely the slopes between data points. The mechanics of selecting subsets of data are shown in figure 19a. Figure 19b presents an array of divided differences in which the progression to higher order approximation can be seen.

A comparison of regression results for 2-, 3-, and 5-point subsets showed the superiority of the five-point divided-difference method in evaluating fatigue-crack-growth rates. Some researchers have utilized a seven-point divided-difference technique. Even though this method may result in a slightly better evaluation of crack-growth rates, it is questionable as to whether the magnitude of improvement would justify the added computational complexity. Use of a divided-difference technique implied that a certain number of data points had to both proceed and follow the data point at which the slope was being evaluated. Consequently, q - 1 data points had to be discarded when a qth order divided difference was used. In data sets where a small number of readings was taken, this feature often caused rejection of the entire set.

Most of the analyses performed in this study, involved use of the five-point divided-difference method.

**Formulation of the Independent Variable.** — It was previously suggested that the independent variable be some function of K and R. As a general form for the independent variable, assume

\[ K_{\text{eff}} (K, R) = U(R)K_{\text{max}}, \]  

(52)

where \( U(R) \) is a functional relation that accounts for the effect of stress ratio.

A number of different forms for \( U(R) \) have been proposed. The simplest of these is \( U(R) = 1.0 \). In this way, it is asserted that no stress ratio effects are present; then,

\[ K_{\text{eff}} = K_{\text{max}} \]  

(53)

This relation is appropriate if no variation in stress ratio is contained in the data, or if the material is insensitive to changes in stress ratio.

The stress-intensity range also may be used as an independent variable. Letting \( U(R) = (1-R) \), the expression

\[ K_{\text{eff}} = (1-R)K_{\text{max}} = \Delta K \]  

(54)

results. This relation has been widely used in the past.
a. Sequential grouping of data subsets.

b. Divided difference array of basic crack growth data.

Figure 19. - Schematic illustration of point-to-point method of determining the slope of crack-growth curves.
Walker (ref. 4) proposed that the independent variable should represent a combination of maximum stress intensity and stress-intensity range. Letting \( U(R) = (1-R)^m \), \( K_{\text{eff}} \) has the form

\[
K_{\text{eff}} = (1-R)^m K_{\text{max}}.
\] (55)

Mukherjee and Burns (ref. 26), and Roberts and Erdogan (ref. 27) have proposed similar relations in their respective studies.

More recently, Elber (ref. 28) proposed a fatigue-crack-propagation model that is based on crack-closure concepts. Elber observed that a crack in a center-cracked panel tended to close before the tensile load was removed. As a result, he defined a crack-closure stress below which the crack would be totally closed. A general form for the crack-propagation independent variable, based on these considerations, may be obtained. Elber proposed that \( U(R) = (1-R)(1+MR) \), so that

\[
K_{\text{eff}} = K_{\text{max}} (1-R)(1+MR),
\] (56)

where \( M \) is determined by optimization or by an experimental procedure.

The four candidates for \( U(R) \) may be compared graphically. Since \( U(R) \) represents a shifting factor accounting for the effect of stress ratio, it is reasonable to plot \( U(R) \) versus \( R \) for the four candidate functions (fig. 20).

Nominal coefficient values have been chosen in both the Walker and Elber relations to represent application to 7075-T6 aluminum alloy data. When \( U(R) = 1.0 \), no shifting for stress ratio occurs. If \( U(R) = (1-R) \), then a linearly varying shifting factor from \( U(R) = 2.0 \) to \( U(R) = 0 \) is generated. Setting \( U(R) = (1-R)^m \) produces much greater variation in \( U(R) \) for positive stress ratio than for negative stress ratios. A similar observation is made when \( U(R) = (1+MR)(1-R) \).

The selection of a form for the independent variable should be based on physical insights as well as on statistical performance. Although physical arguments are not completely formulated at this time, some general considerations are possible. Since it has been observed that most materials exhibit stress-ratio dependent behavior, it is reasonable to assume that the choice of \( U(R) = 1.0 \) would seldom be satisfactory. It is also not reasonable to assume that \( U(R) = (1-R) \), i.e., that the behavior is governed only by the stress-intensity range. The Walker formulation, which is a combination of these two effects, is a more physically justifiable selection. Taking a rather different approach, Elber based his expression directly on the observed physical behavior.
Figure 20. – Comparison of four candidate effective stress-intensity functions.
of crack closure. Table 9 contains a statistical comparison of the formulations. A three-point divided-difference scheme was used to evaluate the crack-growth rates. The four independent variable forms were used in a linear fatigue-crack-growth model. It was found on the basis of \( R^2 \), that the Walker expression, followed by the Elber expression, provided the best consolidation of data. The Walker formulation was chosen for use as an independent variable in the fatigue-crack-propagation model.

**TABLE 9**

**COMPARISON OF INDEPENDENT VARIABLE FORMULATIONS FOR REGRESSION ANALYSIS OF DATA ON 2024-T3 ALUMINUM ALLOY**

<table>
<thead>
<tr>
<th>Formulation</th>
<th>SSD</th>
<th>( R^2 )</th>
</tr>
</thead>
<tbody>
<tr>
<td>( K_{\text{eff}} = K_{\text{max}} )</td>
<td>257.40</td>
<td>0.793</td>
</tr>
<tr>
<td>( = (1-R) K_{\text{max}} )</td>
<td>205.99</td>
<td>0.769</td>
</tr>
<tr>
<td>( = (1-R)^m K_{\text{max}} )</td>
<td>104.29</td>
<td>0.915</td>
</tr>
<tr>
<td>( = (1-R)(1+MR) K_{\text{max}} )</td>
<td>186.80</td>
<td>0.890</td>
</tr>
</tbody>
</table>

Since the Walker formulation of the independent variable was chosen for use in the following analyses, it is of interest to examine the nature of the coefficient \( m \). Investigation of crack-growth-rate curves indicate the formation of bands of data with respect to stress ratio as indicated in figure 3 on page 7. From a graphical point of view, the coefficient \( m \), which affects the coupling between \( K_{\text{max}} \) and \( \Delta K \), caused a shift of the data bands, i.e., a collapse of data towards the mean curve. In the case of a set of data having both positive and negative stress ratios, the points collapsed toward the \( R = 0 \) data since these data are not affected by coupling through \( m \). When the subset consisted of two positive stress ratios, the coefficient \( m \) was selected to produce the best collapse of the two stress ratios towards a central line between them.

The value of the parameter \( m \) was obtained for various sets of data by minimizing the SSD value. A series of investigations was undertaken to determine the variations of \( m \) with respect to stress ratio within a set of data for a particular material. The data sets used previously (7075-T6 and 2024-T3 aluminum) were partitioned in various ways for analysis. The results are presented in table 10.

These correlations indicated that the coefficient \( m \) was highly dependent on the stress ratio distribution and the number of data points. In other words,
different m values were obtained when different subsets of data of a given material were regressed. Generally,

- The formulations \( \frac{da}{dN} = C(K_{\text{max}})^n \) and \( \frac{da}{dN} = C(\Delta K)^n \) were equally satisfactory when \( R = \text{constant} \).
- When the subset of data consisted of specimens for which \( R > 0 \), m tended to be greater than 0.50.
- When the subset of data consisted of specimens for which \( R < 0 \), m tended to be less than 0.50.

A dependence of m on the material properties probably also exists. To uncover this relation, it would be necessary to compare test results for different materials. The comparison sets would have to consist of an identical number of data points run at the same stress ratio. Unfortunately, data meeting these requirements were not available.

**TABLE 10**

**VARIATION OF COEFFICIENT m WITH RESPECT TO DISTRIBUTION OF STRESS RATIOS**

<table>
<thead>
<tr>
<th>Material</th>
<th>Stress Ratio</th>
<th>m</th>
<th>SSD</th>
<th>( R^2 )</th>
</tr>
</thead>
<tbody>
<tr>
<td>7075-T6</td>
<td>-1.0 to 0.80</td>
<td>0.37</td>
<td>38.90</td>
<td>0.908</td>
</tr>
<tr>
<td>7075-T6</td>
<td>0.0 to 0.80</td>
<td>0.53</td>
<td>23.70</td>
<td>0.914</td>
</tr>
<tr>
<td>7075-T6</td>
<td>-1.0 to 0.0</td>
<td>0.04</td>
<td>4.10</td>
<td>0.972</td>
</tr>
<tr>
<td>7075-T6</td>
<td>0.0 to 0.33</td>
<td>0.50</td>
<td>7.30</td>
<td>0.922</td>
</tr>
<tr>
<td>7075-T6</td>
<td>0.50 to 0.80</td>
<td>0.70</td>
<td>12.20</td>
<td>0.912</td>
</tr>
<tr>
<td>7075-T6</td>
<td>-1.0 to -0.80</td>
<td>0.32</td>
<td>1.77</td>
<td>0.974</td>
</tr>
<tr>
<td>2024-T3</td>
<td>-1.0 to 0.70</td>
<td>0.42</td>
<td>97.00</td>
<td>0.920</td>
</tr>
<tr>
<td>2024-T3</td>
<td>0.0 to 0.70</td>
<td>0.44</td>
<td>104.00</td>
<td>0.915</td>
</tr>
</tbody>
</table>

*Data from Hudson (data source ref. 48), and Dubensky (data source ref. 32).*

**Formulation of an Analytical Model.** — Numerous models of the type illustrated by equation (46) have been formulated by researchers during the last decade. Excellent reviews of the literature have been presented in papers by Erdogan (ref. 29), Hoskin (ref. 30), and Coffin (ref. 31). Several fatigue-crack-propagation laws that have been widely used are described below. All of these are empirical equations relying upon regression analysis to calculate empirical coefficients. These relations can be quite logically divided into classes of linear and nonlinear functions.
Linear models, of necessity, neglect initial and terminal behavior. The general form for the linear model is

\[ \frac{da}{dN} = C(K_{eff})^{n'} \]  

Best known of these models is the linear law of Paris (ref. 32),

\[ \frac{da}{dN} = C[(1-R)K]^n' = C(\Delta K)^n' \]  

This equation is commonly fitted to the data in log-log form to yield the Paris regression coefficients C and n'. The Paris model is a linear approximation to the rate curve that incorporates a term to account for the effect of stress ratio. Although the law generally fits only the central segment of the data accurately, it has been used extensively in the literature.

Other linear models are possible, and several have been proposed. These relations, which must be considered elaborations on the Paris model, are due to Elber (ref. 28), Walker (ref. 4), and Roberts and Erdogan (ref. 27). The primary differences in these expressions lie in the choice of the independent variable as discussed in the previous section.

Modifications of the linear Paris model have been made to create a non-linearity at the terminal end of the curve. To approximate the sigmoidal character of the rate curve, and to better account for the effects of stress ratio, Forman (ref. 33) proposed the relation,

\[ \frac{da}{dN} = \frac{C[(1-R)K]^n'}{(1-R)(K_c-K)} \]

Forman's equation contains a singular term in the denominator to model the terminal region of crack growth. As K approaches the critical stress intensity, the denominator goes to zero. Manipulation of the Forman equation leads to

\[ \frac{da}{dN} = \frac{(1-R)^{n'} \left[ C K^{n'} \right]}{(1-R) (K_c-K)} = \frac{(C(1-R)^{n'-1}) K^{n'}}{K_c-K} \]

The term, \((1-R)^{n'-1}\), is clearly similar to the Walker formulation for the independent variable and as such helps to account for the effect of stress ratio. Forman's equation has no provision for modelling the interval of crack initiation and, hence, generates only half of the sigmoidal curve. Variations on the form of the singularity are possible.

A computer program was written to evaluate various fatigue-crack-propagation laws. This program computed K values and calculated crack-growth rates by three-point divided differences. The models were fitted to these results by
linear regression. Sets of data for 7075-T6 and 2024-T3 aluminum alloys and Ti-6Al-4V titanium alloy were used for comparison purposes. Results of these regression analyses, in terms of $R^2$ values, are compared in table II.

Variations on the form of the singularity in the Forman equation proved to be ineffective. The linear model with the Walker formulation for the independent variable and the Forman model showed the most promising results.

The other approach to the modeling of the crack-propagation process is to assume a nonlinear function. Recently, Collipriest (ref. 34) suggested a fatigue-crack-propagation law to model the entire rate curve. This nonlinear equation is based on the inverse hyperbolic-tangent function. The model may be written as

$$\frac{da}{dN} = \exp\left[ n \cdot \frac{\ln K_c - \ln \Delta K_o}{2} \cdot \text{arc tanh} \left( \frac{1}{2} \ln \Delta K - \ln K_c(1-R) + \ln \Delta K \right) \right] + \ln \left\{ C \cdot \exp \left( \frac{\ln K_c - \ln \Delta K_o \cdot n}{2} \right) \right\} . \quad (61)$$

In Collipriest's equation, the independent variable takes the form of $K_{\text{eff}} = \Delta K$. This nonlinear approach was investigated further because it seemed to provide a realistic method for analysis of fatigue-crack-propagation data. Rather than utilizing Collipriest's equation, it was decided to derive a fatigue-crack-propagation model that would allow the implementation of the most effective of the independent variable formulations described earlier. The goal of this derivation was also to obtain a more compact analytical form for the fatigue-crack-propagation model.

The model was based on the inverse hyperbolic tangent suggested by Collipriest. The shape of the inverse hyperbolic-tangent function is shown in figure 21. The functional form assumed was

$$\log \frac{da}{dN} = C_1 + C_2 \tanh^{-1} \left[ \frac{\Phi(K_{\text{eff}})}{\Delta K} \right] . \quad (62)$$

The coefficients, $C_1$ and $C_2$, were to be determined by least squares regression. Examination of the $\tanh^{-1}$ curve suggested the proper form for $\Phi(K_{\text{eff}})$. The function, $\Phi(K_{\text{eff}})$, was chosen to scale values of the effective stress-intensity factor into values of the argument, thus positioning the $\tanh^{-1}$ curve relative to the rate curve. Figure 21 shows that the $\tanh^{-1}$ function goes to infinity at the values of $\Phi = -1$ and $\Phi = +1$. The initial and final conditions of the
<table>
<thead>
<tr>
<th></th>
<th>Material</th>
<th>m</th>
<th>log C</th>
<th>n'</th>
<th>L</th>
<th>SSD</th>
<th>R²</th>
</tr>
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<td></td>
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<td></td>
<td></td>
<td></td>
<td></td>
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<td>da/dN = C(ΔK)^n'</td>
<td>Ti-6Al-4V</td>
<td>-8.830</td>
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<tr>
<td></td>
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<td>2.214</td>
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<td></td>
</tr>
<tr>
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<td>3.600</td>
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<td>0.983</td>
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<td>2024-T3</td>
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<td>4.470</td>
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<td>0.915</td>
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<tr>
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<td>-9.310</td>
<td>3.890</td>
<td></td>
<td></td>
<td>0.908</td>
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<td></td>
</tr>
<tr>
<td>da/dN = \frac{C(ΔK)^n'}{[(1-R)(K_{c}-K_{max})]}</td>
<td>Ti-6Al-4V</td>
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<td>Ti-6Al-4V</td>
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<td>3.600</td>
<td>-0.012</td>
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<td>2024-T3</td>
<td>0.68</td>
<td>-7.621</td>
<td>3.870</td>
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<td>94.50</td>
<td>0.924</td>
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<td>7075-T6</td>
<td>0.61</td>
<td>-7.090</td>
<td>3.290</td>
<td>-0.869</td>
<td>36.30</td>
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<td>Ti-6Al-4V</td>
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<td>--</td>
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<td>0.918</td>
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<td>2024-T3</td>
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<td>41.10</td>
<td>0.903</td>
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<td>7075-T3</td>
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<tr>
<td>da/dN = \frac{C[(1-R)^m][K_{max}]^n'}{\frac{K_{max}}{(1-R)K_{c}}}</td>
<td>Ti-6Al-4V</td>
<td>0.72</td>
<td>-9.330</td>
<td>3.370</td>
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<td></td>
<td>2024-T3</td>
<td>0.54</td>
<td>-9.560</td>
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<tr>
<td>da/dN = C[(0.5+0.4R)(1-R)K_{max}]^n'</td>
<td>2024-T3</td>
<td>-8.500</td>
<td>4.150</td>
<td></td>
<td></td>
<td></td>
<td>0.890</td>
</tr>
</tbody>
</table>
physical problem implied that the rate of change of $\frac{da}{dN}$ should go to infinity at both the terminal and threshold values of $K$. Clearly, the regions of rapid rate of change of $\frac{da}{dN}$ should correspond to arguments in the neighborhood of $\pm 1$. To establish this correspondence, a function was assumed to scale the $K_{\text{eff}}$ values into the interval $\hat{\phi} = -1$ to $\hat{\phi} = +1$.

![Figure 21. - Inverse hyperbolic tangent function.](image)

The physical initial and final conditions were assigned to the points $(\log K_0, -1)$ and $(\log K_c, +1)$ on the $\hat{\phi} - \log K$ plane as illustrated in figure 22.

Assuming a linear scaling function,

$$\hat{\phi} = M' \log K + \hat{\phi}_I$$

(63)

the slope and the intercept were determined by applying the conditions

$$\hat{\phi} = 1 \text{ when } K = \log K_c$$

$$\hat{\phi} = -1 \text{ when } K = \log K_0$$

(64)

These conditions yielded a system of simultaneous, linear, algebraic equations,

$$1 = M'(\log K_c) + \hat{\phi}_I$$

$$-1 = M'(\log K_0) + \hat{\phi}_I$$

(65)
The slope and intercept were found by substitution to be

$$\dot{\gamma}_1 = \frac{\log K_c K_\infty}{\log K_0 / K_c} \quad \text{and} \quad M' = \frac{-2}{\log K_0 / K_c}.$$  

Thus, it followed that

$$\dot{\gamma}(K_{\text{eff}}) = -2 \frac{\log K_{\text{eff}}}{\log K_0 / K_c} + \frac{\log K_c K_\infty}{\log K_0 / K_c} = \frac{\log(K_c K_\infty / K_{\text{eff}}^2)}{\log (K_0 / K_c)},$$  

(66)

and the basic form of the fatigue-crack-propagation model became

$$\log \frac{da}{dN} = C_1 + C_2 \tanh^{-1} \left( \frac{\log(K_c K_\infty / K_{\text{eff}}^2)}{\log(K_0 / K_c)} \right).$$  

(67)

Completion of the fatigue-crack-propagation model required that a form for $K_{\text{eff}}$ be chosen. Based on the previous comparison of the four possible candidates, the Walker formulation for $K_{\text{eff}}$ was chosen. Thus, the complete fatigue-crack-propagation model was

$$\log \frac{da}{dN} = C_1 + C_2 \tanh^{-1} \left[ \frac{\log \left( K_c K_\infty / \left(K_{\text{max}}(1-R)^m\right)^2 \right)}{\log (K_0 / K_c)} \right].$$  

(68)
It should be noted that when data containing only one stress ratio are regressed, the $K_{\text{max}}$ formulation provided equally satisfactory results. In this case, the model was

$$\log \frac{da}{dN} = C_1 + C_2 \tanh^{-1} \left[ \frac{1}{\log \left( \frac{K_{C_0}}{K_{\text{max}}^2} \right)} \right]. \quad (69)$$

**Analyses of Data: Application of the Inverse Hyperbolic Tangent Model**

A fatigue-crack-propagation model that successfully accounted for the effects of stress ratio made possible the combination of sets of data from different sources. This was particularly desirable since the ultimate goal of the modelling effort was the characterization of the crack-propagation behavior of specific materials. Accordingly, it was necessary to obtain data over as wide a range of stress-intensity factors as was available. This collection effort included not only data from different specimen types but also from different heats of material. Data from various sources were combined on the basis of visual inspection although statistical techniques for combining data sets were available. Statistical methods (standard deviation and tolerance limits) were applied to regression equations for the combined data sets to complete the material characterization.

A computer program was developed to apply equation (68) to large sets of fatigue-crack-propagation data. Starting with encoded $(a_i, N_i)$ data, this program fitted the inverse hyperbolic-tangent model to $K_i, \frac{da}{dN_i}$ values in the following steps:

1. Crack-propagation rates were evaluated by a five-point divided-difference scheme.
2. Maximum stress-intensity-factor values were calculated using the appropriate formula for the given specimen type.
3. Values of the argument $\phi(K_{\text{eff}})$ were calculated from the $K_{\text{max}}$ results.
4. Equation (67) was fitted to the $(\phi(K_{\text{eff}}), \frac{da}{dN_i})$ values by least squares regression. The coefficient $m$ was optimized by minimizing the SSD value through iterative regression.
5. Statistical parameters, including SSD, $R^2$, and $S$, were generated. Tolerance limits were computed from equation (7).
6. The data, regression mean curve, and 90 and 99 percent tolerance-limit curves were plotted.
Analysis of the data necessitated that a selection be made for the values of \( K^o \) and \( K_c \). An excellent summary of threshold values is presented in the paper by Donahue et al (ref. 35). Data are included in this source on a large number of materials. Values of \( K_c \) can be found in such publications as the Damage Tolerant Design Handbook (ref. 36). These two sources yielded average values for the \( K^o \) and \( K_c \) limits on the crack-growth rate curve. The data sets analyzed also contained upper and lower bounds on \( K_{max} \).

Nominal values for \( K^o \) were selected from the paper by Donahue et al (ref. 35). Nominal values for \( K_c \) were established by inspection of the \( K_{max} \) values for the data sets. Data on five materials were analyzed: 7075-T6, 7075-T7351, and 2024-T3 aluminum; 300M steel; and Ti-6Al-4V alloy. The composition of these five data sets are listed below.

7075-T6 Aluminum Alloy. — Data on center-cracked bare and clad specimens were compiled from reports authored by Hudson (data source ref. 48), Hudson and Hardrath (data source ref. 92), McEvily and Illig (data source ref. 93), Broek (data source ref. 118), and Dubensky (data source ref. 32).

7075-T7351 Aluminum Alloy. — Data for center-cracked bare specimens including wide panels were obtained from unpublished BCL work and from Feddersen (data source ref. 41).

2024-T3 Aluminum Alloy. — A large amount of data on center-cracked bare and clad specimens was taken from reports published by Broek (data source refs. 118 and 119), Hudson and Hardrath (data source ref. 92), McEvily and Illig (data source ref. 93), Schijve et al (data source refs. 68, 120, and 121), Dubensky (data source ref. 32), and Carter (data source ref. 128).

Ti-6Al-4V Alloy. — Data on both center-cracked and compact-tension specimens were extracted from reports by Feddersen (data source ref. 125) and Bucci et al (data source ref. 115).

300M Steel Alloy. — Data on center-cracked specimens tested in humid air and saltwater spray environments, which covered a limited range of stress-intensity factors, comes from a report by Pendleberry et al (data source ref. 15).

Detailed results of the regression analysis performed on the five materials are presented in Appendix F and summarized in table 12. Number of data points, regression and optimization coefficients, \( K^o \) and \( K_c \) values, and statistical parameters are presented. Appendix figures F1 through F10 show the consolidated fatigue-crack-propagation data, the fitted curve and tolerance limits, and the plotted residuals.
TABLE 12
RESULTS OF REGRESSION ANALYSIS, COEFFICIENTS FOR EQUATIONS (68) AND (7)

<table>
<thead>
<tr>
<th>Material</th>
<th>n, Number of Data Points</th>
<th>C₁</th>
<th>C₂</th>
<th>m</th>
<th>$K_{O}^{2/3}/a$ (ksi-in.$^{3/2}$)</th>
<th>$K_{C}^{2/3}/a$ (ksi-in.$^{3/2}$)</th>
<th>R²</th>
<th>SSD</th>
<th>σ</th>
<th>X̄</th>
<th>Σ(X-X̄)$^{2}$</th>
</tr>
</thead>
<tbody>
<tr>
<td>2024-T3</td>
<td>3,407</td>
<td>-4.490</td>
<td>3.465</td>
<td>0.420</td>
<td>2.20 (2.00)</td>
<td>142.74 (130.00)</td>
<td>0.923</td>
<td>221.6</td>
<td>0.255</td>
<td>0.105</td>
<td>182.07</td>
</tr>
<tr>
<td>7075-T6</td>
<td>746</td>
<td>-4.207</td>
<td>2.241</td>
<td>0.320</td>
<td>3.29 (3.00)</td>
<td>85.64 (78.00)</td>
<td>0.912</td>
<td>57.28</td>
<td>0.252</td>
<td>0.178</td>
<td>79.34</td>
</tr>
<tr>
<td>7075-T7351</td>
<td>1,082</td>
<td>-4.043</td>
<td>2.574</td>
<td>0.350</td>
<td>4.36 (4.00)</td>
<td>109.90 (100.00)</td>
<td>0.952</td>
<td>33.81</td>
<td>0.177</td>
<td>0.221</td>
<td>79.38</td>
</tr>
<tr>
<td>300M</td>
<td>513</td>
<td>-5.186</td>
<td>1.296</td>
<td>0.335</td>
<td>8.78 (8.00)</td>
<td>65.88 (60.00)</td>
<td>0.661</td>
<td>28.56</td>
<td>0.236</td>
<td>0.00024</td>
<td>27.21</td>
</tr>
<tr>
<td>Ti-6Al-4V</td>
<td>782</td>
<td>-4.046</td>
<td>2.825</td>
<td>0.580</td>
<td>4.39 (4.00)</td>
<td>274.50 (250.00)</td>
<td>0.982</td>
<td>36.14</td>
<td>0.215</td>
<td>-0.161</td>
<td>161.20</td>
</tr>
</tbody>
</table>
Good characterizations of the data were obtained in most cases. Particularly satisfactory results were achieved for the titanium alloy (fig. F9). The sigmoidal character of this crack-growth-rate curve is clearly displayed. Rather poor results were obtained for the 300M steel (fig. F7). These data included only a limited range of stress-intensity factors and contained a large amount of scatter. This scatter probably represents the inherent behavior of the material because similar observations were made earlier for fatigue data on 300M steel.

A final comparison between three methods of fatigue-crack-propagation analysis was made. The five data sets were regressed in three different ways; with the inverse hyperbolic-tangent model, with the Paris model [eq. (58)], and with the Forman model [eq. (59)]. The results of the comparison are presented in table 13. From this table it is observed that the inverse hyperbolic-tangent model provided significant improvement in representation of the data, compared with the other two methods.

<table>
<thead>
<tr>
<th>TABLE 13</th>
</tr>
</thead>
<tbody>
<tr>
<td>COMPARISON OF FATIGUE-CRACK-PROPAGATION MODELS WITH COMPLETE DATA SETS</td>
</tr>
<tr>
<td>Values of $R^2$</td>
</tr>
<tr>
<td>Material</td>
</tr>
<tr>
<td>7075-T6</td>
</tr>
<tr>
<td>2024-T3</td>
</tr>
<tr>
<td>Ti-6Al-4V</td>
</tr>
<tr>
<td>300M</td>
</tr>
<tr>
<td>7075-T7351</td>
</tr>
</tbody>
</table>

FRACTURE ANALYSIS

The accumulation of damage in a structural material terminates at fracture instability. In a chronological sense, this event concludes a chain of crack-damage processes such as have been portrayed in the previous sections. Fracture toughness and residual strength provide the quantitative characterizations of
Fracture instability which are necessary to determine both the load carrying capacity of the material at a given stage of crack damage and the life remaining for subcritical damage processes.

Fracture Toughness and Residual Strength

Although fracture toughness and residual strength are related descriptors of fracture instability, they do imply different subtleties in the fracture event as well as different perspectives on the occurrence of crack extension prior to fracture. Generally, fracture toughness refers to a distinct material characteristic associated with abrupt fracture instability, under a rising load, after only minimal amounts of crack extension. In contrast, residual strength refers to fracture behavior which is accompanied by much larger amounts of crack extension prior to the critical instability. The former term is usually associated with relatively brittle fracture under quasi-plane-strain conditions of stress state in the material, while the latter is associated with quasi-plane-stress or transitional-stress-state behavior.

In name, the term residual strength infers that useful strength remains in the structural material even after some stable extension of the crack. As will be seen later in the discussion, residual strength is also quantified in dimensions of toughness and is frequently identified as "apparent" fracture toughness.

Factors Influencing Fracture Behavior

There are a large number of material, metallurgical, and mechanical variables which influence fracture behavior. These include alloy composition, process details (i.e., mechanical reduction and/or heat treatment) associated with a product form, the stress-state effects related to product size, and temperature.

While such an itemization of primary factors may suggest that a characterization of fracture behavior can be achieved through a simple categorization of these details, such is not the case generally. These factors are highly interdependent, and a discrete segregation of effects is frequently impossible or, at least, not economically feasible.

For example, for a given alloy composition and product form, a specific section size (and, hence, stress-state characteristic) may be associated with a particular degree of mechanical reduction, such that another section size may
have a distinctly different level of mechanical reduction. In other words, two different size product forms of common alloy composition may, in reality, be two different materials from the perspective of fracture behavior due to differing degrees of contained mechanical work. Similarly, in quench-rate sensitive materials, the degree and uniformity of heat treatment can vary dramatically with the geometric size of the product.

As a result of these considerations, it is reasonable to expect a close quantitative correlation of fracture behavior where details of alloy, process, size, and temperature are closely aligned. Where any one of these factors is allowed to vary, anomalous fracture behavior can be expected. Although the differences may be rationalized in a qualitative manner, they cannot be assessed with much quantitative satisfaction.

It appears that further insight to fracture behavior is still dependent on a continuing compilation of fracture data, until a broad enough reservoir of data is available to enlarge the analysis.

Characterization of Fracture Behavior by Stress-Intensity-Factor Concepts

The severity of the crack-tip elastic-stress field can be defined by the stress-intensity-factor concepts of linear elastic fracture mechanics. The general analytical formulation of the stress-intensity factor is

\[ K = \frac{S}{\sqrt{a}} f(a,c,w) \quad , \quad (70) \]

where \( f(a,c,w) \) is a geometric scaling function dependent on crack and specimen geometry. For the specimen configurations considered in this program, the specific formulations are, for the compact-type (CT) specimen,

\[ K = \frac{(P/T_w)}{\sqrt{a}} \left[ 29.6-185.5(a/w) + 655.7(a/w)^2 -1017.0(a/w)^3 + 638.9(a/w)^4 \right] ; \quad (71) \]

for the center-cracked (CC) tension panel,

\[ K = \frac{S}{\sqrt{c}} \left[ \pi \sec(\pi c/w) \right]^{\frac{1}{2}} \quad ; \quad (72) \]

and for the part-through crack (PTC) or surface-flaw specimen,

\[ K = \frac{S}{\sqrt{a}} \left[ 1.21 \frac{\pi}{Q} \right]^{\frac{1}{2}}, \quad (73) \]

where

\[ Q = \left[ E(a/c) \right]^2 - 0.212 \left( \frac{S}{TYS} \right)^2 \quad , \quad (74) \]

and \( E(a/c) \) is the complete elliptic integral of the second kind. These are the basic formulations which were used for evaluating fracture data in this program.
As will be seen in the ensuing discussion, fracture instability is not a discrete event for most structural materials. Thus, the characterization of different stages of the fracture process will be identified by different subscripts on the stress and crack dimensions contained in the above expressions.

Crack Behavior Associated With Fracture

As a basis for comparing of the fracture behavior of various specimen and crack configurations, a brief description of the crack extension associated with the fracture process is presented in the following discussion. As will be seen, there are a number of important bench marks associated with crack extension prior to fracture. Any or all of these may be noted in a particular specimen and crack configuration. In order to make a rational correlation of the characteristic fracture parameters which are derived, it is necessary to relate the important bench marks in a comparable and equivalent manner.

Crack Extension and Specimen Response. — Under a rising load, a fatigue-precracked fracture specimen deforms initially in the linear and elastic manner shown in figure 23. During this initial stage of loading, the crack extension and plasticity associated with specimen deformation are nonexistent or, at least, negligible. At some point of loading, a nonlinearity in the specimen load-deflection curve is noted and may be attributed to a combination of crack extension and plasticity. The degree to which each process prevails could be characterized by unloading and marking these specimens; however, this is usually not done in the general characterization of fracture. It is only important to note that the two processes can and do interact to develop the nonlinearity. Finally, after sufficient loading and crack extension, a strain or energy instability will develop to fracture the specimen.

Parameters of Fracture Characterization. — From the previous descriptions, there are at least three bench marks to which fracture characterization parameters can be referenced. These are

- The onset of crack extension
- Apparent fracture instability
- Critical fracture instability.

These points are indicated on figure 23 as the points Q, A, and C, respectively.
Figure 23. Relation of crack extension and specimen response during fracture test.
At this point, it is appropriate to point out and repeat the distinction between the general concepts of fracture toughness and residual strength. If fracture occurs in an abrupt fashion after only minimal amounts of crack extension, Point C will occur very close to Points Q and A, such that the fracture event is essentially a discrete and unique point. The resultant characterization parameter would be a "fracture toughness" value for the material. However, if Point C is removed from Points Q and A, all points, as well as the intervening curve, are important descriptors of the fracture behavior. This latter behavior is generally referred to as residual strength for which one partial, but incomplete measure is the "apparent" fracture toughness at Point A.

The fracture parameters which are associated with these points for various specimens are indicated in table 14.

TABLE 14.
FRACTURE PARAMETERS ASSOCIATED WITH BENCHMARKS OF STRESS AND CRACK EXTENSION

<table>
<thead>
<tr>
<th>Stress State</th>
<th>Plane-Strain</th>
<th>Plane-Stress and Transitional</th>
</tr>
</thead>
<tbody>
<tr>
<td>Specimen Type</td>
<td>CT</td>
<td>CC</td>
</tr>
<tr>
<td>Onset of Crack Extension</td>
<td>$K_{IC}$</td>
<td>$K_q, K_{IC}$</td>
</tr>
<tr>
<td>Apparent Fracture Instability</td>
<td>$K_{app}$</td>
<td>$K_{app}$</td>
</tr>
<tr>
<td>Critical Fracture Instability $^b$</td>
<td>--</td>
<td>$K_c$</td>
</tr>
</tbody>
</table>

$^a$Provided that plane-strain criteria are satisfied.
$^b$Generally not monitored in compact specimen and part-through crack specimen tests.

Data Evaluation

As a characterization of terminal crack behavior, the compilation of fracture toughness and residual strength data on the subject materials has been limited to those stress state and specimen configurations which are most relevant to the fatigue-crack-propagation studies. These are the quasi-plane-strain fracture toughness as determined by compact specimens in accordance with ASTM Designation: E-399-72 (ref. 3), quasi-plane stress and transitional fracture
toughness, as determined by center-cracked tension panels, and part-through crack (or surface flaw) fracture toughness, which simulates natural crack conditions. While each of these has a distinct role in the analysis of damage tolerant structures, their interfaces are not completely clear because of the interdependent complexities of geometric configuration, stress state and basic material properties.

The evaluation of experimental data of any nature involves two basic steps, namely screening and analysis. The data are screened in order to assure satisfaction of the basic criteria on the characteristics being evaluated. The analysis, of course, is concerned with computation of the characteristic parameters.

Screening Criteria. — Within the concepts of linear elastic fracture mechanics, there are two basic constraints imposed on fracture data to assure the characterization of elastic fracture instability. These are frequently referred to as the net section stress criterion and the size requirement. The former assures that the stress on the gross structural section is dominantly elastic at failure; the latter reflects the degree of local plasticity which may be manifested adjacent to the crack tip. Together, these constraints determine the validity* of the test as a representation of elastic fracture.

Net Section Stress Criterion. — The criterion which is imposed on fracture toughness and residual strength data to assure elastic fracture conditions has evolved from experience and, to a large degree, is approximate for each specimen type.

The net section stress is the nominal stress on the uncracked section determined in accordance with elementary concepts of strength of materials. It does not include the stress concentrating effect of the notch or crack and is used only as a simple measure of the nominal stress conditions on the load bearing area of the specimen. The net section stress formulations and ratios are defined in table 15. For the compact fracture specimen, the net section stress includes both a bending and tension stress component due to the load eccentricity. For the center-cracked and part-through crack specimen, the net section stress is simply a tension stress on the uncracked area due to axial loading.

* It is important to recognize that in this context the terms "valid" and "invalid" refer to the adequacy of the elastic-stress condition and do not question the authenticity of the test per se.
TABLE 15.
NET SECTION STRESS CRITERIA FOR VARIOUS SPECIMEN-CRACK CONFIGURATIONS

<table>
<thead>
<tr>
<th>Specimen Type</th>
<th>Net Section Stress, $S_n$</th>
<th>Net Section Stress Criterion, $S_n/TYS$</th>
</tr>
</thead>
<tbody>
<tr>
<td>Compact</td>
<td>[ \frac{P}{T \cdot w} \left( \frac{2(2+\sqrt{3})}{(1-\frac{a}{w})} \right) ]</td>
<td>0.8</td>
</tr>
<tr>
<td>Center-Cracked</td>
<td>[ \frac{S}{(1-\frac{2c}{w})} ]</td>
<td>0.8</td>
</tr>
<tr>
<td>Part-Through Crack</td>
<td>[ \frac{S}{(1-\frac{\pi a}{4 T \cdot w} \frac{2c}{w})} ]</td>
<td>0.9</td>
</tr>
</tbody>
</table>

Size Requirement. — Although the size requirement is not totally independent of the net section stress criterion, its consideration arises from slightly different concepts. In this context, it is used primarily as a thickness requirement on the compact specimen to assure plane-strain constraint of the plastic zone. In accordance with ASTM Designation: E-399-72 (ref. 3), this requirement is stated as

\[ T \leq 2.5 \left( \frac{K_{Ic}}{TYS} \right)^2 \]  \hspace{1cm} (75)

It should be noted that while this criterion is also imposed on the crack length within the above standard, the previous net section stress criterion is even more restrictive on crack length, such that it need not be included here.

Data Analysis. — The basic fracture data in the form of specimen and crack dimensions, loads and stress levels have been analyzed in accordance with equations (71), (72), and (73) subject to the above screening criteria. Specifically, the combinations of load or stress levels, and crack size dimensions used with these equations for the parameters listed in table 14 are, for the compact specimen,

\[ K_{Ic} = g(P, a_c) \]  \hspace{1cm} (76)

\[ K_{app} = g(P_{max}, a_c) \]  \hspace{1cm} (77)
for the center-cracked specimen,
\[ K_q = g(S_q, c_o) \]  
\[ K_{app} = g(S_c, c_o) \]  
\[ K_c = g(S_c, c_c) \]  
\[ (78) \]
\[ (79) \]
\[ (80) \]
and for the part-through crack specimen,
\[ K_q = g(S_q, a_o) \]  
\[ K_{app} = g(S_c, a_o) \]  
\[ (81) \]
\[ (82) \]

The analyses have been performed by digital computer using the program listed in Appendix G. The output of such analyses are available as a tabular format of basic fracture data and associated fracture parameters. For each specimen type, the data are categorized by material alloy, product form, thickness, grain direction, and buckling restraint of the crack edge (if appropriate to the thickness). Within this grouping, tabulations are presented by subcategories of test temperature and specimen size or width.

Results

The tabulations of data which have been compiled and evaluated in accordance with the previous procedures are described in the following subsections. Although the formats have been developed to consolidate the data on a common basis, there are variations which reflect the different quantities and measurements involved in each type of test.

Compact Specimen. - The compact specimen is used primarily to determine the plane-strain fracture toughness of relatively thick materials. A sample tabular format for the output of this type of fracture data is presented in figure 24. Since, at the present time, the initial fatigue precrack length, the 5 percent secant offset load and the maximum load are the principal quantities derived from such a test, these quantities are presented along with the specimen dimensions as basic data. The analysis results are presented as toughness values associated with the offset and maximum load calculated in accordance with equation (71), using the combination of equations (76) and (77), respectively. The effective net section stress ratio and size requirements are presented as validity checks. Finally, the data source reference is listed.
### Table 1: Fracture Toughness Values for Compact Type Specimens of 13.72 Millimeter Thick Aluminum

<table>
<thead>
<tr>
<th>SPECIMEN</th>
<th>TENSILE</th>
<th>NOTCH</th>
<th>CRACK</th>
<th>LENGTH</th>
<th>MATERIAL</th>
<th>TOUGHNESS</th>
<th>SIZE</th>
<th>REF.</th>
<th>STRESS</th>
<th>LOAD</th>
<th>STRESS</th>
<th>RATIO</th>
<th>LOAD</th>
<th>STRESS</th>
</tr>
</thead>
<tbody>
<tr>
<td>L045</td>
<td>19.37</td>
<td>21.15</td>
<td>21.60</td>
<td>22.60</td>
<td>19.90</td>
<td>19.95</td>
<td>20.00</td>
<td>20.10</td>
<td>20.95</td>
<td>20.95</td>
<td>20.85</td>
<td>20.80</td>
<td>20.75</td>
<td>20.70</td>
</tr>
<tr>
<td>L055</td>
<td>18.37</td>
<td>20.15</td>
<td>20.60</td>
<td>21.60</td>
<td>18.90</td>
<td>18.95</td>
<td>19.00</td>
<td>19.10</td>
<td>18.95</td>
<td>18.95</td>
<td>18.85</td>
<td>18.80</td>
<td>18.75</td>
<td>18.70</td>
</tr>
<tr>
<td>L065</td>
<td>17.37</td>
<td>19.15</td>
<td>19.60</td>
<td>18.60</td>
<td>17.90</td>
<td>17.95</td>
<td>17.00</td>
<td>17.10</td>
<td>17.95</td>
<td>17.95</td>
<td>17.85</td>
<td>17.80</td>
<td>17.75</td>
<td>17.70</td>
</tr>
</tbody>
</table>

**Notes:** Fracture toughness values are in mega-pascal-millimeters. 

![Basic Fracture Data](Basic%20Fracture%20Data.png)

![Toughness Evaluation](Toughness%20Evaluation.png)

**Figure 24.** Sample of tabular output for compact specimen fracture analysis results.
Center-Crack Specimen. — In that the center-crack specimen is used primarily to determine plane stress and transitional fracture toughness of relatively thin materials, more experimental quantities are usually recorded. A more expansive tabular format for this specimen type is shown in figure 25. The initial fatigue precrack length, the critical crack length as reported by the investigator, the 5 percent secant offset load, and maximum load are tabulated along with the specimen dimensions as basic fracture data. From these items, the offset, apparent and critical toughness are computed in accordance with equation (72) and the dimensional combinations of equations (78), (79), and (80), respectively. The associated net section stress ratios are also presented as validity checks. Finally, the data source reference is noted.

Within the field of each table, the data are categorized and grouped by test temperature and specimen width. Following each grouping, where more then one valid value exists, an average value and standard deviation are presented.

Part-Through Crack Specimen. — The part-through crack or surface flaw specimen is used primarily as a direct representative of naturally occurring cracks in structural materials in a wide range of thicknesses. As a result, these specimens and their data can reflect a full range of stress states. A sample illustration of the tabular format for these data is presented in figure 26. Because this crack shape is generally semielliptical in shape, two dimensions, length and depth, are required for its description. The initial precrack size, 5 percent secant offset stress, and maximum stress are presented along with specimen dimensions as basic data. The toughness values are computed in accordance with equation (73) and the dimensional combinations of equations (81) and (82). The net section stress ratio is presented as a validity check. The shape ratio is included as an indication of the ellipticity of the shape. Finally, the data source reference is noted.

CONCLUSIONS

As a result of this study, it was found that large amounts of fatigue, fatigue-crack propagation, and fracture data can be consolidated for use in design applications. Each of these three areas of material behavior were treated separately, using large files of pertinent data that were gathered on 2024 and 7075
Table 25: Effects of Transverse Fracture Toughness on Yield Strength, Young's Modulus, and Overall Panel Strength and Deflection

<table>
<thead>
<tr>
<th>SPECIMEN</th>
<th>YIELD STRESS (ksi)</th>
<th>ELONGATION (%)</th>
<th>TUGHNESS (ksi)</th>
<th>OFFSET WAVE</th>
<th>OFFSET LENGTH (in)</th>
<th>NET STRESS RATIO</th>
<th>REF</th>
</tr>
</thead>
<tbody>
<tr>
<td>21</td>
<td>35.0</td>
<td>0.25</td>
<td>30.0</td>
<td>0.25</td>
<td>0.25</td>
<td>0.75</td>
<td>0.75</td>
</tr>
<tr>
<td>22</td>
<td>35.5</td>
<td>0.30</td>
<td>30.5</td>
<td>0.30</td>
<td>0.30</td>
<td>0.70</td>
<td>0.70</td>
</tr>
</tbody>
</table>

**Figure 25.** Sample of tabular output for center-cracked specimen fracture analysis results.
TABLE - SURFACE-FRAC FRACTURE TOUGHNESS OF .320 MILLIMETER THICK TITANIUM 73-5AL-5VALLOY PLATE

<table>
<thead>
<tr>
<th>SPECIMEN</th>
<th>TEST</th>
<th>MATERIAL</th>
<th>DIMENSIONS</th>
<th>APPLIED STRES</th>
<th>NET TOUGHNESS</th>
<th>AVERAGE REF.</th>
<th>OFFSET</th>
<th>AVERAGE</th>
<th>OFFSET</th>
<th>RATIO</th>
</tr>
</thead>
<tbody>
<tr>
<td>SMT1 - 0.25</td>
<td>145</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
</tr>
<tr>
<td>SMT2 - 0.25</td>
<td>145</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
</tr>
<tr>
<td>SMT3 - 0.25</td>
<td>145</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
</tr>
<tr>
<td>SMT4 - 0.25</td>
<td>145</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
<td>0.25</td>
</tr>
</tbody>
</table>

NOTE: NET SECTION STRENGTH AS PERCENT OF YIELD STRENGTH. VALUE NOT INCLUDED IN AVG. VALUE OR STD. DEV.

Figure 26. - Sample of tabular output for part-through crack or surface flaw fracture analysis results.
aluminum alloys, Ti-6Al-4V alloy, and 300M steel. Fatigue and fatigue-crack-propagation analyses were limited to constant-amplitude cycling conditions.

From studies of fatigue data, it was concluded that

1. The Walker equivalent strain parameter can be used to account for effects of stress ratio.
2. A local stress-strain analysis, which uses a computed $K_f$ value and a technique to approximately account for relaxation of mean stress, can be used to account for notch effects.
3. The inverse hyperbolic tangent function can be employed to model fatigue curves in terms of $\varepsilon_{eq}$ versus log $N_f$ for both unnotched and notched specimens.
4. Using the $\tanh^{-1}$ function, it is possible to compute mean fatigue curves and tolerance limit curves for 90 and 99 percent probability of survival with 95 percent level of confidence.

From studies of fatigue-crack-propagation data, it was concluded that

1. Crack growth curves can be simply and effectively approximated using a five-point, divided-difference scheme.
2. The Walker effective stress-intensity formulation can be used to account for stress ratio effects.
3. The inverse hyperbolic-tangent function can be used to model crack-growth rate curves.
4. Using the $\tanh^{-1}$ function, mean growth rate curves and 90 and 99 percent probability two-sided tolerance bands with 95 percent confidence level can be developed.

From studies of fracture toughness and residual strength data, it was concluded that

1. Consistent fracture characterization can be achieved with stress-intensity-factor concepts within a common categorization of the details of alloy, process, size, and temperature.
2. Correlation of fracture behavior for various specimen types and stress-state conditions must be based on equivalent degrees of crack extension.
3. A broader characterization of fracture data reflecting the influence of thickness effects, processing variable grain direction, and specimen configuration requires a continued expansion of the data reservoir.
APPENDIX A

DATA SOURCE REFERENCES


APPENDIX A


APPENDIX A


APPENDIX A


APPENDIX A


APPENDIX A


70. Anon.: Room and Elevated Temperature Fatigue Characteristics of Ti-6Al-4V. Titanium Metals Corp. of America, 1957.


APPENDIX A


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86. Anon.: Unpublished fatigue data on Ti-6Al-4V bar stock from Sikorsky Aircraft, SE-1521.


APPENDIX A


APPENDIX A


APPENDIX A


APPENDIX B

CYCLIC STRESS-STRAIN DATA

The method of fatigue analysis developed in this program required the use of both cyclic and monotonic stress-strain curves. Using the data source references of Appendix A and information from MIL-HDBK-5B (ref. 1), it was possible to characterize the monotonic stress-strain response for the materials of interest. However, outside of the data reported by Endo and Morrow (ref. 16), Landgraf et al (ref. 17), Smith et al (ref. 18), and Gamble (data source ref. 90), there was no appropriate information available on the cyclic stress-strain response of these same materials. To fill this void of information, a limited amount of complementary tests were conducted on 2.29 mm (0.09 in.) thick 2024-T3 and 7075-T6 aluminum sheet. Specimens were from the same lot of material used in a number of previous experimental programs (data source refs. 1 through 9).

All tests were performed using an electrohydraulic test system operated in closed-loop strain control at a constant strain rate of $4 \times 10^{-3}$ sec$^{-1}$. Experimental procedures were similar to those reported by Jaske et al (ref. 37). Loading was axial and special lateral guides were used to prevent buckling. These guides were clamped about the specimen with a force light enough to avoid significantly influencing loading of the specimen. Strain was measured over a 1.27 mm (0.500 in.) gage length using a special extensometer with a linear variable displacement transformer (LVDT) as the transducer. Load was measured by a standard load cell in series with the specimen and continuously recorded on a time-based chart. Load-strain records were made periodically using an X-Y recorder.

Results of these experiments are summarized in table B1. For each alloy, three incremental step tests (ref. 17) were used to develop continuous monotonic and cyclic stress-strain curves up to 0.01 maximum strain (see figs. B1 and B2). To see if the cyclic stress-strain curves from the step tests could be used to predict cyclic stress-strain response under constant-amplitude strain cycling, seven specimens of each alloy were tested under constant-amplitude loading. For three tests the strain ratio (algebraic ratio of minimum to maximum strain) was equal to -1.0 (i.e., the mean strain was zero). A positive value of mean strain
APPENDIX B

was used in the other four tests - three were with a strain ratio of 0.0 and one was at a strain ratio of 0.5.

In all cases, results from the constant-amplitude tests were close to those predicted by the cyclic stress-strain curve from the step tests (figs. B1 and B2). Thus, it was concluded that these cyclic stress-strain curves could be used to describe the stable stress-strain response of these two materials.

Unpublished cyclic stress-strain data have been generated on 300M steel and annealed Ti-6Al-4V alloy during in-house studies conducted at BCL. Experimental procedures were the same as those described earlier, except that a 0.635 mm (0.250 in.) diameter, 1.27 mm (0.500 in.) gage length specimen was used. Cyclic stress-strain curves for these two alloys are presented in figures B3 and B4. Samples of the titanium alloy from the transverse (T) direction and from electron-beam (EB) welded plate cyclically hardened. Whereas, samples from the longitudinal (L) direction cyclically softened. The cyclic curve shown in figure B4 is for the L direction and the monotonic curve was estimated from published data (data source ref. 70). To show the wide variation in cyclic stress-strain behavior of this alloy, data from Smith et al (ref. 18) are presented in figure B5 and data from Gamble (data source ref. 90) are presented in figures B6 and B7.
TABLE B1.
RESULTS OF CYCLIC STRESS-STRAIN TESTS AT A STRAIN RATE OF $4 \times 10^{-3}$ SEC$^{-1}$

<table>
<thead>
<tr>
<th>Specimen</th>
<th>Type of Test$^a$</th>
<th>Strain Ratio$^b$</th>
<th>Stable Strain Range</th>
<th>Stable Stress Range$^c$, MN/m$^2$ (ksi)</th>
<th>Stable Mean Stress, MN/m$^2$ (ksi)</th>
<th>Fatigue Life $N_f$, cycles$^c$ (or blocks)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td>Total</td>
<td>Plastic</td>
<td></td>
<td></td>
</tr>
<tr>
<td>2</td>
<td>STEP</td>
<td>-1.0</td>
<td>0.0204 max</td>
<td></td>
<td>--</td>
<td>--</td>
</tr>
<tr>
<td>3</td>
<td>STEP</td>
<td>-1.0</td>
<td>0.0204 max</td>
<td></td>
<td>--</td>
<td>--</td>
</tr>
<tr>
<td>4</td>
<td>STEP</td>
<td>-1.0</td>
<td>0.0200 max</td>
<td></td>
<td>--</td>
<td>--</td>
</tr>
<tr>
<td>1</td>
<td>CA</td>
<td>-1.0</td>
<td>0.0233</td>
<td>0.0105</td>
<td>938</td>
<td>--</td>
</tr>
<tr>
<td>9</td>
<td>CA</td>
<td>-1.0</td>
<td>0.0152</td>
<td>0.0029</td>
<td>917</td>
<td>--</td>
</tr>
<tr>
<td>5</td>
<td>CA</td>
<td>-1.0</td>
<td>0.0098</td>
<td>0.0005</td>
<td>745</td>
<td>--</td>
</tr>
<tr>
<td>7</td>
<td>CA</td>
<td>0</td>
<td>0.0206</td>
<td>0.0075</td>
<td>917</td>
<td>23</td>
</tr>
<tr>
<td>8</td>
<td>CA</td>
<td>0</td>
<td>0.0153</td>
<td>0.0029</td>
<td>917</td>
<td>7.6</td>
</tr>
<tr>
<td>6</td>
<td>CA</td>
<td>0</td>
<td>0.0101</td>
<td>0.0001</td>
<td>710</td>
<td>15</td>
</tr>
<tr>
<td>10</td>
<td>CA</td>
<td>0.5</td>
<td>0.0100</td>
<td>0.0002</td>
<td>717</td>
<td>36</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>Total</td>
<td>Plastic</td>
<td></td>
<td></td>
</tr>
<tr>
<td>2</td>
<td>STEP</td>
<td>-1.0</td>
<td>0.0208 max</td>
<td></td>
<td>--</td>
<td>--</td>
</tr>
<tr>
<td>3</td>
<td>STEP</td>
<td>-1.0</td>
<td>0.0204 max</td>
<td></td>
<td>--</td>
<td>--</td>
</tr>
<tr>
<td>6</td>
<td>CA</td>
<td>-1.0</td>
<td>0.0201</td>
<td>0.0056</td>
<td>1 050</td>
<td>--</td>
</tr>
<tr>
<td>10</td>
<td>CA</td>
<td>-1.0</td>
<td>0.0150</td>
<td>0.0011</td>
<td>944</td>
<td>--</td>
</tr>
<tr>
<td>Specimen</td>
<td>Type of Test&lt;sup&gt;a&lt;/sup&gt;</td>
<td>Strain Ratio&lt;sup&gt;b&lt;/sup&gt;</td>
<td>Stable Strain Range</td>
<td>Stable Stress Range, MN/m&lt;sup&gt;2&lt;/sup&gt; (ksi)</td>
<td>Stable Mean Stress, MN/m&lt;sup&gt;2&lt;/sup&gt; (ksi)</td>
<td>Fatigue Life N&lt;sub&gt;f&lt;/sub&gt;, cycles&lt;sup&gt;c&lt;/sup&gt; (or blocks)</td>
</tr>
<tr>
<td>----------</td>
<td>------------------------</td>
<td>------------------</td>
<td>------------------</td>
<td>---------------------------------</td>
<td>---------------------------------</td>
<td>-------------------------</td>
</tr>
<tr>
<td>4</td>
<td>CA</td>
<td>-1.0</td>
<td>0.0097</td>
<td>0.0001</td>
<td>710 (103)</td>
<td>6 173</td>
</tr>
<tr>
<td>8</td>
<td>CA</td>
<td>0</td>
<td>0.0204</td>
<td>0.0050</td>
<td>1 000 (145)</td>
<td>49 270</td>
</tr>
<tr>
<td>9</td>
<td>CA</td>
<td>0</td>
<td>0.0152</td>
<td>0.0007</td>
<td>979 (142)</td>
<td>43 511</td>
</tr>
<tr>
<td>7</td>
<td>CA</td>
<td>0</td>
<td>0.0101</td>
<td>--</td>
<td>703 (142)</td>
<td>160 4 611</td>
</tr>
<tr>
<td>11</td>
<td>CA</td>
<td>0.5</td>
<td>0.0096</td>
<td>--</td>
<td>684 (102)</td>
<td>198 (23.2)</td>
</tr>
</tbody>
</table>

<sup>a</sup>STEP indicates an incremental step test and CA indicates a constant amplitude test.

<sup>b</sup>Ratio of minimum to maximum strain.

<sup>c</sup>Cycles for constant-amplitude tests and blocks for incremental-step tests.
Figure Bl. - Cyclic stress-strain behavior of 2024-T3 aluminum sheet.
Figure B2. — Cyclic stress-strain behavior of 7075-T6 aluminum sheet.
Figure B3. - Cyclic stress-strain behavior of 300M steel forging.
Figure B4. - Cyclic stress-strain behavior of annealed Ti-6Al-4V plate.
Figure B5. — Cyclic stress-strain behavior of solution-treated and aged (STA) Ti-6Al-4V bar, data from Smith et al (ref. 18).
Figure B6. - Cyclic stress-strain behavior of annealed Ti-6Al-4V forging, data from Gamble (data source ref. 90).
Figure B7. — Cyclic stress-strain behavior of annealed Ti-6Al-4V bar, data from Gamble (data source ref. 90).
APPENDIX C

STEP-BY-STEP APPROACH TO ANALYSIS OF FATIGUE DATA

The following outline provides an illustration of the procedure which was developed for the consolidation and analysis of fatigue data. Each part of the analysis is broken down in a step-by-step fashion so that the details of the process might be more clearly defined. Possible simplifying assumptions are also noted.

A. Material Data Acquisition

(1) Constant-amplitude smooth-specimen fatigue data (preferably obtained over a range of stress ratios or mean stress values) are required to optimize the equivalent strain $m$ factor. If only notched data are to be analyzed, an optimum $m$ value must be estimated.

(2) Constant-amplitude notched-specimen fatigue data make up the second part of the data file for a given material. Again, data generated at various $K_t$ values are desirable if a reasonable value for $\rho$ is to be determined.

(3) Monotonic and cyclic stress-strain information for the investigated material, heat treatment and product form are required for both the smooth and notched fatigue specimen analyses. In order to perform the analyses, it may be necessary, in some cases, to develop reasonable estimates of the cyclic and monotonic curves on the basis of available information. This should be done with considerable caution, however, since effectiveness of the entire analysis is based on appropriate material property definition.

B. Smooth Specimen Fatigue Data Analysis

(1) Calculate maximum nominal stress and alternating strain values for the complete data set.

(a) If the input is in terms of maximum strain and strain ratio, calculate alternating strain values

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for each specimen according to the following expression:

\[ e_a = \frac{e_{\text{max}}(1-R)}{2}, \quad (C1) \]

and determine maximum stress values through usage of the cyclic stress-strain curve [eq. (10)].

(b) If input is in terms of maximum stress and stress ratio, calculate values of alternating stress in the same manner as shown in equation (C1), substituting values of \( S_a \) and \( S_{\text{max}} \) for values of \( e_a \) and \( e_{\text{max}} \). Then determine alternating strain values according to the cyclic stress-strain curve [eq. (10)].

(2) Convert cycles to failure to \( \log N_f \).

(3) Set limits within which the optimum \( m \) value is likely to occur. In most cases, limits of 0.30 and 0.50 would bound the optimum \( m \) value.

(4) For a particular \( m \) value, calculate values of equivalent strain for the entire smooth data set according to equation (9b).

(5) Fit a third order polynomial [eq. (29)] to the set of calculated equivalent strain values through a least-squares regression process. (The polynomial, rather than the \( \tanh^{-1} \) function, was used in computations involving an optimization on \( m \) because the quality of fit for the polynomial was related solely to the degree of data consolidation. Quality of fit for the \( \tanh^{-1} \) function, however, was somewhat dependent on the specific function limits which were used, and these limits could not be appropriately determined until a specific \( m \) value was chosen.)

(6) Calculate and record the total sum of squares and the sum of squares of deviations for the regressed equation. Then calculate an \( R^2 \) value according to equation (4).

(7) Repeat steps B4 through B6 for complete range of \( m \) values and select the best \( m \) value in terms of maximum \( R^2 \). (This procedure is almost necessarily handled by a computer using an iterative process.)
(8) Using the optimum m value (or a satisfactory approximation), perform a least-squares regression to determine the best fit inverse hyperbolic tangent equation for the investigated data set. If the data cover the entire fatigue life range from 10 to $10^6$ cycles, establish the range of the function according to equations (36) and (37). Otherwise reasonable values must be specified for these limits.

(9) Apply the weighting function $W(eq)$, [eq. (42)], to the residuals and determine whether the modified residuals are sufficiently uniform throughout the range of data. It may be desirable to examine normality through construction of a frequency distribution plot of the residuals. This is done by plotting the frequency of occurrence versus the magnitude of deviations from the mean curve.

(10) If step B9 is completed satisfactorily, probability of survival lines can be constructed according to equation (7), and the resultant curves may then be displayed graphically along with the individual equivalent strain data values.

C. Notched Specimen Fatigue Data Analysis

(1) As in the smooth specimen fatigue analysis, nominal values of maximum stress and alternating strain must be calculated in the analysis of notched specimen data. Steps Bla and Blb are applicable. The cyclic stress-strain function [eq. (10)] is used in both cases.

(2) To calculate local mean stress values according to equations (23) and (27a), it is also necessary to calculate monotonically based values of nominal maximum and alternating stress and strain. The same stress-strain equation [eq. (10)] is used for these calculations as was used in step Cl, but monotonic parameters (as in table 6) are required.

(3) Convert cycles to failure to log $N_f$.

(4) Set limits within which the optimum $\rho$ value is likely to occur. (In most cases, limits of 0.00 and 0.03 would bound the optimum $\rho$ value.)
(5) For a particular \( p \) value, calculate values for the fatigue concentration factor according to equation (20). Knowledge of the notch root radius is required for this calculation.

(6) Calculate an estimate of local alternating strain values according to the following expression:

\[
e_a = K_f e_a
\]

(7) Then calculate approximate values for local maximum stress using the following relationship:

\[
\sigma_{\text{max}} = \sigma_a + \sigma_m
\]

It is not possible to calculate \( \sigma_{\text{max}} \) directly because cyclic plasticity allows mean stress relaxation that decreases stable local mean stress values. Equation (C3) is an approximate means of accounting for that relaxation for constant-amplitude loading.

(a) In this equation, \( \sigma_a \) is calculated from equation (10) using values of local alternating strain determined in equation (C2).

(b) Values for \( \sigma_m \) in equation (C3) are found according to equations (23) and (27a).

(i) In equation (27a), the value, \( e'_{\text{max}}/2 \), is equivalent to a monotonic value of local alternating strain. This quantity can be determined by multiplying the monotonic nominal value of alternating strain, found in step C2, by the fatigue concentration factor which was found in step C5.

(ii) Similarly, the magnitude of the monotonic local maximum strain used in equation (23) can be determined by multiplying the monotonic maximum nominal strain found in step C2, by the fatigue concentration factor \( K_f \).

(8) For a particular \( p \) value and for an optimum \( m \) value found in part B, calculate values of equivalent strain for the entire notched data set according to equation (9b). Values of \( \sigma_{\text{max}} \) and \( e_a \) calculated in steps C6 and C7 are used, however, in place of \( S_{\text{max}} \) and \( e_a \).
(9) Fit a third order polynomial [eq. (29)] to the set of equivalent strain values in the same manner as in step B5.

(10) As in step B6, determine TSS, SSD, and $R^2$ values for the regressed equation.

(11) Repeat steps C5 through C10 for the complete range of $\rho$ values and select an optimum $\rho$ on the basis of a maximum $R^2$ value. (Again, the computer is almost essential for this operation.)

(12) Using optimum values for $m$ and $\rho$, determine a best-fit inverse hyperbolic tangent equation in the same manner as in step B8.

(13) As in step B9, apply the weighting function, examine the residuals; and if necessary, construct a frequency distribution plot of the residuals.

(14) If step C13 is completed satisfactorily, construct probability of survival lines as in step B10.
APPENDIX D

RESULTS OF CONSTANT-AMPLITUDE FATIGUE DATA CONSOLIDATION

The collection of figures in this appendix displays results of the constant-amplitude fatigue data consolidation effort. One figure is presented on each page, and each figure consists of two related plots. The upper plot shows the consolidated data along with the regressed mean curve. Below the mean curve, are the calculated 90 and 99 percent statistical tolerance curves, respectively, which were established at a 95 percent confidence level. The lower plot illustrates the pattern of weighted residuals for the consolidated data shown in the upper plot. As explained earlier (see page 30), the abscissa is in terms of actual fatigue life. The residual plots were included to provide a visual indication of whether the statistical requirements of randomness, zero mean deviations, and uniformity of variance were satisfied for the consolidated data.

Figures D1 through D4 represent consolidated data for 2024-T3 and 2024-T4 aluminum. Figures D5 through D9 consist of consolidated data on 7075-T6 and 7075-T651 aluminum. For both series of aluminum, the data consolidation was substantial. The best collapse of data ($R^2 = 99.6$ percent) was obtained for the unnotched 7075-T6 clad sheet material, where all data came from a single source. In all but one case (fig. D8), consisting of both notched and unnotched aluminum data, the $R^2$ value was 94 percent or greater. Other than the noted exception, unnotched data were consolidated better than notched data. Nonuniformity of variance was of some concern in several cases (figs. D2 and D6), but this problem was not due to inadequacy of the weighting function; it was due to layering of data from different sources in the high cycle fatigue range. This layering made it impossible to account for data in this region as effectively as data in the lower cycle regions where no such layering was evident. The nonuniformity of variance was not considered to be severe enough, however, to make the construction of tolerance limits inappropriate.

Results for the 300M steel fatigue analysis are presented in figures D10 and D11. The $R^2$ values for both curves were not as high as the values determined for the aluminum alloys, but the overall data collapse was considered good since the inherent data scatter for the two data sets was quite large.

The Ti-6Al-4V alloy data, displayed in figures D12 through D23, were the most difficult to analyze and provided the poorest results. The difficulties were due
to two major factors. First, the titanium data file consisted of a large number of different product forms and heat treatments, and although an attempt was made to develop accurate monotonic and cyclic stress-strain data for each variation, only a rough approximation of these curves was possible in some cases. Secondly, the inherent scatter in most of the titanium data was very great, making a consolidation effort difficult. Despite these problems, $R^2$ values exceeding 80 percent were obtained in figures D12, D17, D19, D20, D22, and D23. The best results were found for the Ti-6Al-4V data in the solution-treated and aged condition. For cases where the data consolidations were not acceptable as shown in figures D13, D14, D15, D16, D18, and D21, the values of $R^2$ were below 80 percent. Such curves cannot be used for design applications and are included in this report only to show how poorly the analytical procedures worked in some instances. Until more experimental information is obtained upon the cyclic stress-strain and fatigue behavior of Ti-6Al-4V alloy, it will not be possible to refine the analytical procedures to account for such anomalies.
a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D1. - 2024-T3 Sheet (unnotched).
a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D2. – 2024-T3 Sheet (notched).
APPENDIX D

a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D3. — 2024-T4 Bar and rod (unnotched).
a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D4. - 2024-T4 Bar and rod (notched).
APPENDIX D

a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D5. - 7075-T6 Sheet (unnotched).
a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D6. 7075-T6 Sheet (notched).
a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D7. - 7075-T6 Clad sheet (unnotched).
APPENDIX D

a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D8. - 7075-T6 and 7075-T651 Bar (unnotched).
APPENDIX D

a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D9. - 7075-T6 and 7075-T651 Bar (notched).
a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D10. - 300M Billet and forging (unnotched).
a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D11. - 300M Billet and forging (notched).
a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D12. — Annealed Ti-6Al-4V sheet (unnotched).
a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D13. - Annealed Ti-6Al-4V bar and extrusion [125 ksi TYS (unnotched)].
a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D14. - Annealed Ti-6Al-4V bar, extrusion, and forging [140 ksi TYS (unnotched)].
APPENDIX D

a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D15. - Annealed Ti-6Al-4V casting (unnotched).
a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D16. - Annealed Ti-6Al-4V sheet (notched).
a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

Figure D17. - Annealed Ti-6Al-4V bar and extrusion [125 ksi TYS (notched)].
APPENDIX D

a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D18. — Annealed Ti-6Al-4V bar, extrusion, and forging [140 ksi TYS (notched)].

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APPENDIX D

a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D19. - Annealed Ti-6Al-4V casting (notched).
APPENDIX D

a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D20. — STA Ti-6Al-4V sheet (unnotched).
APPENDIX D

a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D21. — STA Ti-6Al-4V forging, casting, and plate (unnotched).
a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D22. - STA Ti-6Al-4V sheet (notched).
APPENDIX D

a. Consolidated fatigue data with mean curve and 90 and 99 percent survival lines.

b. Distribution of weighted residuals.

Figure D23. - STA Ti-6Al-4V casting and plate (notched).
APPENDIX E

APPLICATION OF FATIGUE-CRACK-PROPAGATION RATE ANALYSIS

An actual structural element functioning in a real world environment is usually subjected to an extremely diverse loading spectrum. Large fluctuations in maximum stress, stress ratio, and frequency, not to mention temperature and environment, are likely to occur.

A crack extending in a structural element in such a loading environment will propagate in a complex manner. It is this highly complex situation that the designer must consider when structural life predictions are made. Clearly, some simplifications of the actual loading situation must be made for the purposes of analysis. Crack-growth-rate analysis is often used to predict life. Such an approach provides a model of the damage process by which cracks grow under constant-amplitude cyclic loading. Once the characteristic model for a material is obtained, it can be integrated to yield life predictions. Application of the rate analysis approach developed in the program is discussed briefly in this appendix.

Fatigue-Crack-Growth Rate Model

Previous discussions in the main body of this report have examined how crack-growth data can be converted to a crack-growth-rate format and subsequently represented by an analytical model of fatigue-crack propagation. Using this approach, data from a large number of sources, covering a wide range of parameters, can be combined to characterize a material quite thoroughly. As a result of this investigation, the inverse hyperbolic tangent model has been proposed as a suitable tool for data analyses.

Rate Integration

Once a satisfactory composition for the governing differential equation has been developed, the second part of the fatigue-crack-propagation problem, integration, becomes important. Some of the possible integration procedures are presented here in schematic form. However, implementation of these procedures was outside the scope of the present work. The general expression,

$$\frac{da}{dN} = f[K(a)]$$

(E1)
APPENDIX E

is a first order, linear differential equation. Although the fatigue-crack-propagation law is in the form of a rate equation, it is essential that the designer be able to calculate crack length for the case where a given number of cycles have been applied under specified loading conditions. This calculation can be accomplished by using the result of integrating equation (E1),

\[
\int_{a_1}^{a_2} \frac{da}{f(K(a))} = \int_{N_1}^{N_2} dN.
\] (E2)

Mathematically speaking, this integration is representative of a class of solutions of differential equations known as "initial value problems". In other words, it is desired to find the final crack length after a certain number of cycles have elapsed, starting from initial values for crack length and cycle number.

Two general methods of solution of the initial value problem are available. The first, and most straightforward method consists of carrying out the integration indicated in equation (E2) to yield a closed-form solution. The closed-form solution has the advantage of being a concise equation from which the number of cycles required for a crack to grow to a given length is easily computed. Unfortunately, it is not always easy, or even possible, to perform the integration of the differential equation. The second method of solution involves the use of a numerical integration scheme such as the Runge-Kutta method.

Hoskin (ref. 30) gives some closed-form solutions to the most common fatigue-crack-propagation models where the variables can be readily separated and integrated. Consider, for example, Paris' Law,

\[
\frac{da}{dN} = C(\Delta K)^n.
\] (E3)

Assuming \( K_{\max} = S_{\max}^{1/n} a \) for the case of center-cracks where width effects are negligible, the integration for \( n' > 2 \) is given as

\[
N = \frac{\left[ \frac{n'}{2} - 1 \right]}{1 - \left( \frac{a_1}{a} \right)^n}.
\] (E4)
A similar procedure may be carried out for the Forman-model differential equation,

$$\frac{da}{dN} = \frac{C(\Delta K)^{n'}}{(1-R)(K_c - K_{max})}, \quad (E5)$$

yields for $n' > 3$

$$N = \frac{2}{C_{\text{max}}^n (1-R)} \left[ \frac{(n'-3)/2}{a_1} \right] \left[ \begin{array}{c} \frac{a_c/a_1}{(n'-2)} \left\{ \frac{n'-1}{1-(a_1/a)} \right\} \\ 1 \end{array} \right]$$

$$+ \frac{1}{(n'-3)} \left\{ 1 - \frac{a_1 (n' - 3/2)}{a} \right\}.$$ \quad (E6)

When the $K$ expression involves more complex algebraic or transcendental functions for which a closed form solution often cannot be achieved. Such is the case when width effects are not negligible. For example, when a width correction factor term is used, the expression for $K_{\text{max}}$ becomes

$$K_{max} = \frac{S_{\text{max}}}{\pi a \sec \left( \frac{\pi a}{w} \right)} \quad , \quad (E7)$$

and the integration is much more complex.

The alternative to closed-form solution of equation (E2) is numerical integration, which necessitates the use of a digital computer. Engle (ref. 38) for example, utilized the Runge-Kutta numerical integration scheme in Program CRACKS (which, incidentally, accommodates variable-amplitude loads as well as the more elementary constant-amplitude cases). This is typical of the type of numerical solutions used today. Since the inverse hyperbolic tangent model has been based on the above form for $K_{max'}$, equation (E7), the integration process becomes exceedingly complex. A closed-form integration of the model does not seem to be practical. However, the model may be integrated numerically. The expression may be put in the form,

$$N_2 - N_1 = 10^{-C_1} = \int_{a_1}^{a_2} \left[ \log \left( \frac{K_0 K}{K_c} \right) + \log \left( \frac{\Delta K}{(1-R)2m S^2 \pi a \sec \left( \frac{\pi a}{w} \right)} \right) \right] \, da$$

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APPENDIX E

which is suitable for numerical integration. Several integration schemes are
directly applicable to this expression. These include iterated Gaussian quad-
ratures as well as the Runge-Kutta method mentioned earlier.

Summary of the Life Prediction Procedure

The procedure for predicting the life of a structure, neglecting variable-
amplitude loading effects is outlined below,

(1) Crack growth data on the material of interest is collected and
combined.

(2) Crack growth data are converted to crack-growth-rate values by
means of the five-point divided difference scheme. Values of
$K_{max}$ are calculated.

(3) The inverse hyperbolic tangent function is fitted to the data
to yield regression and optimization coefficients, as well as
statistical parameters.

(4) Initial and final crack lengths, the stress levels, and mean
stresses for the structures to be investigated are specified.
This information may be presented in the form of load spectrum.

(5) Finally, the values specified in item (4) are used to integrate
the characteristic fatigue-crack-propagation model for the
number of cycles required to extend the crack to the specified
final crack length.
APPENDIX F

RESULTS OF FATIGUE-CRACK-PROPAGATION ANALYSIS FOR FIVE MATERIALS

Figures F1 through F10 present the results of analyses performed on 2024-T3, 7075-T6, and 7075-T7351 aluminum alloys, 300M steel, and Ti-6Al-4V alloy. The composition of these data sets was previously described in the report. (See pages 79 and 80.) Each material is characterized by a crack-growth-rate curve and an accompanying plot of the distribution of residuals as a function of actual crack propagation rate.

The crack-growth-rate curves consist of the experimental data plotted on a $K_{\text{eff}} = (1-R)^n K_{\text{max}}$ basis. The best-fit regression curve is represented by the solid central line through the data points. On either side of the mean curve are the 90 and 99 percent tolerance limits, with 95 percent level of confidence. Coefficients of the inverse hyperbolic tangent model and the tolerance limit formula were presented previously in Table 12.
Figure F1. — Fatigue-crack-propagation-rate curve for 2024-T3 aluminum alloy
Figure F2. - Distribution of residuals for regression equation representing 2024-T3 aluminum alloy.
Figure F3.—Fatigue-crack-propagation-rate curve for 7075-T6 aluminum alloy.
Figure F4. – Distribution of residuals for regression equation representing 7075-T6 aluminum alloy.
Figure F5. – Fatigue-crack-propagation-rate curve for 7075-T7351 aluminum alloy.
Figure F6. - Distribution of residuals for regression equation representing 7075-T7351 aluminum alloy.
Figure F7.—Fatigue-crack-propagation-rate curve for 300M steel alloy.
Figure F8. - Distribution of residuals for regression equation representing 300M steel alloy.
Figure F9. — Fatigue-crack-propagation-rate curve for Ti-6Al-4V alloy.
Figure F10. — Distribution of residuals for regression equation representing Ti-6Al-4V alloy.
APPENDIX G

COMPUTER PROGRAM FOR FRACTURE ANALYSIS TABULATION

A listing of the computer program, FRACTAB, for the analysis of fracture data is presented in this appendix. The data input formats for this computer routine have been presented in the subsection on Data Recording and Storage. The typical printout formats have been illustrated in figures 24, 25, and 26.
 FOR ENGLISH INPUT PLACE 8+11 CARDS IN SOURCE DECK FOR ENGLISH OUTPUT OMIT SWITCH 2 CARD FOR METRIC OUTPUT FOR METRIC INPUT PLACE SWITCH 2 CARD IN SOURCE DECK FOR METRIC OUTPUT OMIT SWITCH 2 CARD FOR ENGLISH OUTPUT

PROGRAM FRACTA3(INPUT,OUTPUT,TAPES=INPUT,TAPE6=OUTPUT)

DIMENSION KODE1(5), KODE2(50), KOMET(8), SUM(3), SS(3), XN(3),
AVG(3), DEVI(3), XXYVAR(3), XLAG(3), RATIO(3), AI(2)

READ AND STORE REPLACEMENT CODE NUMBERS

READ (5, 555) KODE1(N), KODE2(N)
IF (ENF, 5) 105, 107
CONTINUE
STOP
CALL SSWITCH (1) IM1
CALL SSWITCH (2) IM2
PRIVATE IM0
LIM=N
THICK=0
READ AND STORE NEW TITLE FOR WRITE STOP RUN
READ (5, 565) 1UNIT1, 1UNIT2, THICK
IF (ENF, 5) 295, 305
READ (5, 530) KOMET
READ (5, 540) THICK, ITYPE
IF (THICK.EQ.0.) THICK=THICK
READ INPUT RECORD BACK ONE CARD
WIDTH=N
READ Sums FOR NEXT DATA SUBSET
READ (5, 519) SUM(N)=,
READ (5, 520) SSV(N)=
READ (5, 521) XH(N)=
READ NEXT DATA CARD
READ (5, 549) IDENT,THICK,WIDTH,CSUB0,SSUB2,SSUB3,DOCCL,PRCCL,STMAX
1+Y5+Y5+SPECL+ITYPE+ISPEC+ITEM+IREF
IF (ENF, 5) 275, 140
TEST FOR BLANK CARD (WIDTH=0)
IF (1040) 50 TO 275
IF SWITCH IS ON REPLACE REF CODE
IF (1050) 50 TO 155
READ (5, 502) GO TO 155
PRIVATE LNT, LTR
IF (IREF.EQ.KODE1(N)) GO TO 150
CONTINUE
GO TO 155
IREF=KODE2(N)
APPENDIX G

C CHECK FOR MISSING INPUT DATA
C IF (TYS.LT.1) GO TO 390
C
dLK=OUT FLAG* K + RATiN
C
GO TO 155
C
XXVAR(N)=I
RATIO(N)=I
KFLAG(N)=I
C CHECK INPUT AND TYPE OF OUTPUT DESIRED AND MAKE ANY CHANGES
C IF (UNIT.EQ.1) GO TO 165
C IF (IMET.EQ.2) GO TO 170
GO TO 174
C IF (IMET.EQ.2) GO TO 175
GO TO 180
C SWITCH MCMLN UNITS TO ENGLISH UNITS
THICK=THICK/R.0254/1000
WIDTH=WIDTH/R.0254/1000
CS3=CS3/R.0254/1000
CS4=CS4/R.0254/1000
CSU3=CSU3/R.0254/1000
CSU4=CSU4/R.0254/1000
VOCCL=VOCCL/R.0254/1000
PMCC=PMCC/R.0254/1000
TY5=TY5/R.635
ITEM=ITEM/9./5.32
SPECL=SPECL/R.0254/1000
GO TO 190
C SWITCH ENGLISH UNITS TO METRIC UNITS
THICK=THICK*R.0254/1000
WIDTH=WIDTH*R.0254/1000
CS3=CS3*R.0254/1000
CS4=CS4*R.0254/1000
CSU3=CSU3*R.0254/1000
CSU4=CSU4*R.0254/1000
VOCCL=VOCCL*R.0254/1000
PMCC=PMCC/R.0254/1000
TY5=TY5/R.635
ITEM=ITEM/9./5.32
SPECL=SPECL/R.0254/1000
GO TO 200
C BRANCH TO APPROPRIATE EQUATION
C 1 *COMPACT TENSION*
C 2 *CENTER CRACK*
C 3 *SURFACE F.A.*
C 4 *SURFACE F.A.*
C 5 *DOUBLE CANTILEVER BEAM*
C 6 *NOTCH BEAD*
APPENDIX G

C SELECT CRITICAL STRESS AT CRACK
000327 180 SCHIT=SSUM3
000328 180 SCHIT=PHCCL
000329 IF (SCHIT.EQ.0) SCHIT=SSUM3
000330 IF (SCHIT.EQ.0) SCHIT=VUCC1
000331 IF (ITYPE.EQ.0) GO TO 390
000332 IF ((ITYPE=5) .AND. NE.EQ.0) STO+41190
000333 GO TO (185*220*245*390*390)*ITYPE

C COMPACT TENSION
000334 185 IF (CSIH.EQ.0) 30 TO 395
000335 185 IF (THICK.EQ.0) 30 TO 395
000336 X=CSUH/WIDTH
000337 XXVAR(1)=SSUH*13TH/THICK*SQRT(CSUBU)*129.6-185.5*X+655.7*X*X-101
000338 X=MAX/13TH/THICK*SQRT(CSUBU)*129.6-185.5*X+655.7*X*X-101
000341 X=(2.5*X(XXVAR(1)/TS)**2)
000342 X=(2.5*X(XXVAR(2)/TS)**2)
000343 IF (11+E.EQ.0) GO TO 195
000344 IF (11+E.EQ.0) GO TO 195
000345 IF (11+E.EQ.0) GO TO 195
000346 X=XXVAR(N)*10**6/X(XXVAR(N)/TS)**2*1000
000347 190 N=1+2
000348 IF (XXVAR(N).GT.0) N=NET/SSJ3
000349 IF (N.FG.2) GO TO 200
000350 SN=NET/1000
000351 200 XX=SN/TS

C COMPARE MAX LOAD WITH 5 PERCENT OFFSET LOAD SHOULD NOT EXCEED 1.1
000352 IF (SSUH3*GT.0) HAT103*SMAX/SSUH3
000353 IF (X(N).GT.THICK) GO TO 205
000354 HAT104*GT.CSJD3*GO TO 205
000355 IF (N.FG.2) SNET/SN=NET/CSjd3
000356 IF (SNET.GT.TYS*3) GO TO 205
000357 IF (HAT103*GT.1.1) GO TO 205
000358 GO TO 210

C INVALIUD
000359 210 KFLAG(N)=1
000360 NVAL=2
000361 GO TO 215
000362 215 IF (KFLAG(N).EQ.1) CONTINUE
000363 SUM(N)=SUM(N)+XXVAR(N)
000364 SSUM(N)=SSUM(N)+XXVAR(N)**2
000365 CONTINUE
000366 11=1
000367 11=1
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APPENDIX G

```
C PRIVILEGE LINE OF INPUT/OUTPUT DATA
DO 1050 IDENT=ITEMS=INPUT=WSH=0
C
C LENRQ_CHK
DO 10613 X=1.57*N*CSURG
C
C COMPUTE STRESS RATIOS
C 1 #APPARENT
DO 10623 IF (CSURG.GT.3) RAT10(1)=STMAX/TYS/(1-CSURG/WIDTH) A1800
C 2 #CRITICAL
DO 10624 IF (CSURG.GT.0) RAT10(3)=STMAX/TYS/(1-CRIT/WIDTH) A1820
C 3 #PEAK STRES
DO 10622 IF (CSURG.GT.0) RAT10(1)=STVAR1(2)=STMAX*SQRT(X/COS(A)/WIDM) A1840
DO 10621 IF (CSURG.GT.0) XXVAR(2)=STVAR1(2)=STMAX*SQRT(X/COS(A)/WIDM) A1860
DO 10624 IF (X.GT.0) XXVAR(1)=STVAR1(1)=STMAX*SQRT(X/COS(A)/WIDM) A1880
DO 10664 IF (XXVAR(3).GT.XCRY) XXVAR(3)=STMAX*SQRT(X/COS(A)/WIDM) A1900
C
C 210700 IF (INET.NE.2) GO TO 230
C 210701 DD 225 N=1,3
DO 10700 XVAR(N)=XXVAR(N)*SORT(L+01)
C CHECK M STRESS RAT10 LF 8
DO 10711 230 IF (XXVAR(N).LE.1.) GO TO 240
C 210716 IF (RATIO(N).GT.8) GO TO 235
C
C 210720 IF (XVAR(N).EQ.1) XVAR(N)=1
C 210722 NOAS=1
C 210723 GO TO 240
C
C 210725 VALID
DO 10733 XN(N)=XN(N)+1
C 210726 SUM1=SUM1+N*XVAR(N)
C 210730 SSQ(N)=SSQ(N)+XXVAR(N)**2
C 210732 240 CONTINUE
C
C PRINT ONE LINE OF INPUT/OUTPUT DATA
C 21074 IF=2
DO 10755 WHITE (6+16) IDENT=ITEMS=INPUT=WSH=0
C
C SURFACE FLAW
C 21075 IF (SPEC1.EQ.6) GO TO 390
C 21076 IF (CSURG.EQ.6) GO TO 390
C 21077 IF (STMAX.EQ.0) GO TO 390
C
C COMPUTE ASPECT AND STRESS RATIOS
C 21079 ASPECT=SPEC1/CSURG
C
100000 END
100500 CONTINUE
```

APPENDIX G

C

011016 A=YST(1)*1-745*SPEC+CSU2/(THICK/LENGTH)
011022 RATIO(1)=SCRIT/X
011024 RATIO(2)=S MAX/X

C PRELIMINARY COMPUTATIONS

011026 PHISU=1.*4.6*ASPECT*1.05
011034 XFlAGUE(ST MAX/ETY)*2/S*EPS

011037 PHIXX=SUM(PHISU)

011041 XKVAR(1)=1.1*SCRIT*SORT(3.1416*SPEC+CSU2)/(SORT(PHISU,1.2*XXXSQ))
011055 XKVAR(2)=1.1*ST MAX*SORT(3.1416*SPEC+CSU)/(SORT(PHISU,1.2*XXXSQ))
011072 XKVAR(3)=1.1*ST MAX*SORT(3.1416*SPEC+CSU2)/(SORT(PHISU,1.2*XXXSQ))

011107 IF (RAT(1)<.9) GO TO 255

011112 255 WW=5+5
011113 XKVAR(N)=XKVAR(N)*SORT(0,1)

C CHECK 4-S STRESS RATIO LE .9

011121 255 WW=5+5 N=1,2
011123 IF (XKVAR(N)<.1) GO TO 255
011126 IF (RATIO(N)<.9) GO TO 260

C

011131 VALIV

011132 XN(N)=XN(N)+1
011135 SSU(N)=SUM(N)*XKVAR

011137 GO TO 265

C

011140 260 WW=5+5
011142 MAX=1
011143 CONTINUE

9

011145 1=3

C PRINT ONE LINE OF INPUT/OPTUT DATA

011146 WRITE (6,425) IUEVI+ITEMP+TYSH+THICK+WIDTH+CSU2+SPEC+SCRIT+ST

011148 MAX=1

011151 MAX=1

011152 GO TO 136

C

011160 IF(I1=1) GO TO 260

C IF LAST CARD WAS BLANK SET MORE=21 IF EOF, SET MORE=1

011172 270 MORE=1
011172 275 MORE=1

C COMPUTE AND PRINT STATISTICS IF AN GT 1

011183 280 WW=5+5 N=1,3
011185 AVG(N)=1
011186 DEVI(N)=1
011186 IF (XN(N)<.2) GO TO 255

011187 AVG(N)=SUM(N)/XN(N)

011190 DEVI(N)=SORT(SSU(N)-SUM(N)*SUM(N)/XN(N))/XN(N)-1.)

011194 CONTINUE

011196 285 WRITE (6,455)

011198 IF ((XN(N)<.1) AND AND (XN(N)<.1) AND (XN(N)<.1)) GO TO 310

C BRANCH TO APPROPRIATE OUTPUT FORMAT

011203 300 IF (X=5+5) GO TO 300
```plaintext
C CHECK INPUT AND OUTPUT TYPE AND BRANCH TO APPROPRIATE FORMAT

01351 29u WRITE (6,415) AVG
01353 WHITE (6,416) DEV
01355       GO TO 365
01357 36u WRITE (6,410) AVG(1),AVG(2)
01359 37u WRITE (6,417) DEV(1),DEV(2)
01361 36u WRITE (6,410) AVG(1),AVG(2)
01363 30u WRITE (6,417) DEV(1),DEV(2)
01365 39u WRITE (6,410) AVG(1),AVG(2)
01367 32u WRITE (6,417) DEV(1),DEV(2)
01369 30u WRITE (6,410) AVG(1),AVG(2)
01371 32u WRITE (6,417) DEV(1),DEV(2)
01373 36u WRITE (6,410) AVG(1),AVG(2)
01375 32u WRITE (6,417) DEV(1),DEV(2)
01377 36u WRITE (6,410) AVG(1),AVG(2)
01379 30u WRITE (6,417) DEV(1),DEV(2)
01381 34u WRITE (6,410) AVG(1),AVG(2)
01383 32u WRITE (6,417) DEV(1),DEV(2)
01385 36u WRITE (6,410) AVG(1),AVG(2)
01387 32u WRITE (6,417) DEV(1),DEV(2)
01389 36u WRITE (6,410) AVG(1),AVG(2)
01391 32u WRITE (6,417) DEV(1),DEV(2)
01393 36u WRITE (6,410) AVG(1),AVG(2)
01395 32u WRITE (6,417) DEV(1),DEV(2)
01397 36u WRITE (6,410) AVG(1),AVG(2)
01399 32u WRITE (6,417) DEV(1),DEV(2)
01401 36u WRITE (6,410) AVG(1),AVG(2)
01403 32u WRITE (6,417) DEV(1),DEV(2)
01405 36u WRITE (6,410) AVG(1),AVG(2)
01407 32u WRITE (6,417) DEV(1),DEV(2)
01409 36u WRITE (6,410) AVG(1),AVG(2)
01411 32u WRITE (6,417) DEV(1),DEV(2)
01413 36u WRITE (6,410) AVG(1),AVG(2)
01415 32u WRITE (6,417) DEV(1),DEV(2)
01417 36u WRITE (6,410) AVG(1),AVG(2)
01419 32u WRITE (6,417) DEV(1),DEV(2)
01421 36u WRITE (6,410) AVG(1),AVG(2)
01423 32u WRITE (6,417) DEV(1),DEV(2)
01425 36u WRITE (6,410) AVG(1),AVG(2)
01427 32u WRITE (6,417) DEV(1),DEV(2)
01429 36u WRITE (6,410) AVG(1),AVG(2)
01431 32u WRITE (6,417) DEV(1),DEV(2)
01433 36u WRITE (6,410) AVG(1),AVG(2)
01435 32u WRITE (6,417) DEV(1),DEV(2)
01437 36u WRITE (6,410) AVG(1),AVG(2)
01439 32u WRITE (6,417) DEV(1),DEV(2)
01441 36u WRITE (6,410) AVG(1),AVG(2)
01443 32u WRITE (6,417) DEV(1),DEV(2)
01445 36u WRITE (6,410) AVG(1),AVG(2)
01447 32u WRITE (6,417) DEV(1),DEV(2)
```

APPENDIX G

051723 60.10.12C A3360
C A3370
C ERROR MESSAGE - MISSING ENTRY DATA A3380
C
051724 39U PHIVI 55U A3390
051730 GO TO 139 A3394
051731 395 CONTINUE A3410
C A3420
C
051731 40U FORMAT (1X,A8,14,4X,F5.1,13X,F5.1,...,8X,F5.3,3X,F6.3,2) A3450
051731 405 FORMAT (1X,A8,14,4X,F5.1,13X,F5.1,...,8X,F5.3,3X,F6.3,2) A3480
051731 41U FORMAT (64X,AVERAGE VALUE 59,2,5X,F7.2) A3500
051731 413 FORMAT (64X,AVERAGE VALUE 59,2,5X,F7.2) A3510
051731 42U FORMAT (59X,AVERAGE VALUE 59,2,5X,F7.2) A3520
051731 425 FORMAT (59X,AVERAGE VALUE 59,2,5X,F7.2) A3530
051731 43U FORMAT (61X,STANDARD DEVIATION 59,2,5X,F7.2) A3540
051731 435 FORMAT (61X,STANDARD DEVIATION 59,2,5X,F7.2) A3550
051731 44U FORMAT (62X,NOTE: NET SECTION STRENGTH EXCEEDS 1.13 PERCENT OF Y A3560
051731 445 FORMAT (62X,NOTE: NET SECTION STRENGTH EXCEEDS 1.13 PERCENT OF Y A3570
051731 44U FORMAT (62X,NOTE: NET SECTION STRENGTH EXCEEDS 1.13 PERCENT OF Y A3580
051731 45U FORMAT (62X,NOTE: NET SECTION STRENGTH EXCEEDS 1.13 PERCENT OF Y A3590
051731 455 FORMAT (62X,NOTE: NET SECTION STRENGTH EXCEEDS 1.13 PERCENT OF Y A3600
051731 45U FORMAT (62X,NOTE: NET SECTION STRENGTH EXCEEDS 1.13 PERCENT OF Y A3610
051731 455 FORMAT (62X,NOTE: NET SECTION STRENGTH EXCEEDS 1.13 PERCENT OF Y A3620
051731 46U FORMAT (63X,NOTE: NET SECTION STRENGTH EXCEEDS 1.13 PERCENT OF Y A3630
051731 466 FORMAT (63X,NOTE: NET SECTION STRENGTH EXCEEDS 1.13 PERCENT OF Y A3640
051731 46U FORMAT (63X,NOTE: NET SECTION STRENGTH EXCEEDS 1.13 PERCENT OF Y A3650
051731 465 FORMAT (63X,NOTE: NET SECTION STRENGTH EXCEEDS 1.13 PERCENT OF Y A3660
051731 46U FORMAT (63X,NOTE: NET SECTION STRENGTH EXCEEDS 1.13 PERCENT OF Y A3670
051731 465 FORMAT (63X,NOTE: NET SECTION STRENGTH EXCEEDS 1.13 PERCENT OF Y A3680
051731 46U FORMAT (63X,NOTE: NET SECTION STRENGTH EXCEEDS 1.13 PERCENT OF Y A3690
051731 465 FORMAT (63X,NOTE: NET SECTION STRENGTH EXCEEDS 1.13 PERCENT OF Y A3700
051731 47U FORMAT (*TARE <C AND KIC FRACTURE TOUGHNESS VALUES FOR A3650
1COMPACT TYPE SPECIMENS IF 59,2,5X,F7.2) A3660
051731 475 FORMAT (*TARE <C AND KIC FRACTURE TOUGHNESS VALUES FOR A3670
20U) A3680
051731 47U FORMAT (*TARE FRACTURE TOUGHNESS VALUES FOR COMPACT TYPE A3690
10U) A3700
051731 475 FORMAT (*TARE FRACTURE TOUGHNESS VALUES FOR COMPACT TYPE A3710
10U) A3720
051731 48U FORMAT (*TARE FRACTURE TOUGHNESS VALUES FOR COMPACT TYPE A3730
10U) A3740
051731 485 FORMAT (*TARE FRACTURE TOUGHNESS VALUES FOR COMPACT TYPE A3750
10U) A3760
051731 48U FORMAT (*TARE FRACTURE TOUGHNESS VALUES FOR F5,3 INCH THICK A3770
10U) A3780
051731 485 FORMAT (*TARE FRACTURE TOUGHNESS VALUES FOR F5,3 INCH THICK A3790
10U) A3800
051731 49U FORMAT (*TARE FRACTURE TOUGHNESS VALUES FOR F5,3 INCH THICK A3810
10U) A3820
051731 495 FORMAT (*TARE FRACTURE TOUGHNESS VALUES FOR F5,3 INCH THICK A3830
10U) A3840
051731 50U FORMAT (*TARE FRACTURE TOUGHNESS VALUES FOR F5,3 INCH THICK A3850
10U) A3860
051731 505 FORMAT (*TARE FRACTURE TOUGHNESS VALUES FOR F5,3 INCH THICK A3870
10U) A3880
THE WEIGHTING FUNCTION, W(X)

In order to obtain uniformity of variance in combined sets of fatigue data, a weighting function, W(X), was applied to each data population. The following comments are included to clarify the method employed in this weighting process.

Initially, the data were analyzed without weights, and the quality of fit was based on the $R^2$ parameter. The process used in maximizing $R^2$ involved a minimization of the sum of squares of deviations or SSD. Using equations (2) and (4), the unweighted SSD can be described as

$$SSD = \sum_{i=1}^{n} (Y_i - \bar{Y})^2 = \sum_{i=1}^{n} (Y_i - A_0 - A_1 \bar{X})^2$$  \hspace{1cm} (H1)

where $\bar{X}$ represents the mean, or predicted value of $X$ for a particular value of $Y_i$.

When the weighting function was used, the minimization was based on a modified SSD, written as follows,

$$SSD = \sum_{i=1}^{n} W_i (Y_i - A_0 - A_1 \bar{X})^2$$  \hspace{1cm} (H2)

In this way, each deviation from the mean is modified according to the magnitude of $W_i$. When $W_i$ is small, the square of the residual is reduced correspondingly. If $W_i$ is near unity, almost no modification of the residual results.
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