FLOW VISUALIZATION STUDY OF
CLOSE-COUPLED CANARD-WING AND STRAKE-WING CONFIGURATION

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An investigation has been conducted in the Langley 1/8-scale V/STOL model tunnel to qualitatively determine the flow fields associated with semi-span close-coupled canard-wing and strake-wing models. Small helium filled bubbles were injected upstream of the models to make the flow visible. Photographs were taken over the angle-of-attack ranges of $-10^\circ$ to $40^\circ$.
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SUMMARY

An investigation has been conducted in the Langley 1/8-scale V/STOL model tunnel to qualitatively determine the flow fields associated with semi-span close-coupled canard-wing and strake-wing models. Small helium filled bubbles were injected upstream of the models to make the flow visible. Photographs were taken over the angle of attack range of -10° to 40°.

The results of this study indicate that the presence of a canard above or in the wing chord plane enhances the wing's leading edge vortex and delays the stall of the wing. At positive angles of attack, the wake of the canard located above the wing chord plane passes above the wing; however, over the same angle of attack range, the wing is in or above the wake of the canard located below the wing chord plane. Also, for the strake-wing configuration at angles of attack greater than 18°, there are three vortex systems associated with this model.
INTRODUCTION

Currently, NASA is conducting studies on devices, such as the close-coupled canard-wing and strake-wing combinations, which improve the performance of highly maneuverable aircraft at high angles of attack (Refs. 1, 2, 3). The data from these studies has been limited primarily to force data, with some theoretical analysis. Although the fighter type wing planforms, because of their moderate sweep angles, generally do not develop appreciable vortex lift, the results of references 1 and 3 have indicated the presence of vortex lift on the wing in the presence of a canard. The wing-strake data of reference 2 has indicated that, in addition to the strong vortex lift generated on the strake, a favorable interference on the wing lift characteristics. As a result, this cursory flow visualization study was initiated to ascertain the general nature of the flow fields associated with the canard, strake, wing configurations.

This study used semi-span canard-wing and strake-wing models (scaled versions of those models used in Refs. 1, 2, and 3) mounted on a reflection plane. Helium filled soap bubbles were injected into the tunnel flow upstream of the model, and as these small bubbles passed through the flow field, photographs were taken. The tests were conducted in the Langley 1/8-scale V/STOL model tunnel at a dynamic pressure of approximately 1.5 lbf/ft². Angles of attack were from -10 to 40⁰.

MODEL DESCRIPTION

The canard-wing model investigated is shown in Figure 1 and the strake-wing model is shown in Figure 2. The same wing is used on both models. The model
planforms studied were scaled down versions of those used in References 1, 2, and 3. The canard and wing were constructed from 0.25 inch thick plexiglass and the strake was made of 0.125 inch thick brass. All models were uncambered with sharp beveled edges; the wing and canard had a 1/2" bevel and the strake had a slight bevel. All three components were painted glossy black to produce the best contrast between model and soap bubbles.

The model configurations studied were: (1) canard alone; (2) wing alone; (3) canard located above the wing chord plane in the presence of the wing (high canard); (4) canard located in the wing chord plane in the presence of the wing (mid canard); (5) canard located below the wing chord plane in the presence of the wing (low canard); (6) strake and wing. For a detailed definition of the vertical positions of the canard see Figure 3.

APPARATUS AND TEST PROCEDURES

The present investigation was conducted in the Langley 1/8-scale V/STOL model tunnel. Figure 4 shows two views of the tunnel test section. The flow field was visualized by injecting small, neutrally bouyant, helium filled, soap bubbles into the freestream forward of the model. The bubble head (that piece of equipment from which the bubbles eminated) was attached to a thin dowel rod so that the bubbles could be directed to the desired flow field region. The source of light was a high-intensity lamp mounted downstream of the model and directed upstream. The lamp has louvers to help "focus" the light beam. The camera used in this study was a Hasselblad, model 500 EL/M, 70 mm. The film used was Kodak Tri-X Pan, 70 mm., black and white, which had an ASA rating of 400. A development process was used which pushed the ASA rating to approximately
1000. This helped to heighten the contrast between the model and the bubbles. The best camera setting found for this test was a shutter speed of 1/8 second and a 5.6 f-stop. At this speed and setting, the bubbles produced streaks on the photographic film as they passed through the flow field. Since all models had sharp leading edges, the flow field about the models was probably not significantly affected by variations in tunnel velocity, i.e. Reynolds number; so the tunnel was operated at a dynamic pressure of approximately 1.5 lbf/ft$^2$ which was found to give the best photographic results. Photographs were taken of the models at angles of attack from -10 to 40 degrees.

DISCUSSION OF RESULTS

Figures 5-73 present photographs of the flow fields of the canard wing configurations and Figures 74-102 the strake-wing configuration. It should be noted that the helium bubbles injected into the flow field are generally neutrally buoyant whose average diameter was approximately 0.1 inch. Thus, if the flow field details were too small, for example the leading edge vortex at the planform apex, the bubbles would not show the detail because of their physical size.

There are photographs at low angles of attack that show no leading edge vortex, only a slight ripple of the flow near the leading edge. The conclusion that no vortex exists should not be drawn without further examination since the vortex might be too small or weak to trap a soap bubble.

Occasionally, the light reflected from the white picture identification numbers is reflected from the glossy wing leading edge. (See Figure 18 for an example). Although it is readily seen that it is not a bubble streak, the
reader should be alerted to this photographic phenomena. Also the camera angle relative to the models is not always the same for all configurations and angles of attack.

In the following, high canard, mid canard, and low canard refer to the canard position relative to the wing chord plane.

I) Canard-Wing Configuration

a) ALPHA = -10°: Figures 5-14 present the canard-wing configuration at -10° angle of attack. It should be noted that, since the canard and wing have no camber, twist, or dihedral the top view of the flow field at -10° angle of attack is also the bottom surface flow field for the model at a positive 10° angle of attack. The photographs for all the configurations at this angle of attack show no spanwise flow on the upper surface of the model. Figure 9 (high canard) shows that the wing is in the canard's wake at -10° angle of attack.

b) ALPHA = 0°: Figures 15 and 16 are photographs of the mid and low canard-wing configurations. These pictures are typical of all configurations at 0° angle of attack.

c) ALPHA = 10°: The configurations at an angle of attack of 10° are presented in Figures 17-27. The canard alone picture (Fig. 17) shows a fairly streamwise flow field. The bubble streaks show no indication of leading edge vortex formation. However, as mentioned earlier, a vortex may exist, but it may too small and weak to be detected by the soap bubbles. The bubble streaks in Figures 18 and 19 (wing alone) indicate that the flow has separated all along the leading edge. Note the rippling of the bubble
streaks near the leading edge. Comparing the photograph in Figure 17 (canard alone) with those in Figures 20, 23 and, 25 (high, mid, low canards respectively), it is clear that the wing up wash has enhanced the leading edge vortex of the canard. Again note the rippling of the bubble streaks near the leading edge. It is felt that the canard leading edge vortex (as depicted in Figures 20, 23, & 25) does not have enough strength to entrain the soap bubbles; thus there is no visualization of the vortex details. A comparison of Figures 18 and 19 (wing alone) with Figures 21, 24 and 26 (wing in the presence of the high, mid, and low canard, respectively) show two things: (1) no large flow changes on the wing due to the canard at this angle of attack, 10°; (2) bubbles have entered the leading edge vortex flow field of the wing for the high and low canard configurations which may indicate a stronger vortex system for these two configuration than for the wing alone configuration. Comparing Figures 22 and 27 it is clear that the canard wake flows above the wing for the high canard configuration and below the wing for the low canard configuration.

d) ALPHA = 12°: Figures 28 and 29 are presented to show that in general the vortex systems for the canard and wing become visible at this angle of attack. The leading edge vortex has not burst on the wing till approaching the wing trailing edge (Figure 29), however it appears that the canard vortex (Figure 28) has burst near mid-span at 1/4 chord. Leading edge vortex bursting is believed to have occurred when the vortex appears to grow in radial size rather abruptly.

e) ALPHA = 15°: Figures 30-39 present the photographs of the canard-wing configurations at 15° angle of attack. In comparing Figure 30 (canard alone) to the high, mid, and low canard pictures of figures 32, 35, and 37...
respectively, it appears that the canard vortex is strengthened when the canard is in the presence of the wing. The canard leading edge vortices shown in all these photographs seem to be bursting half way between the root and tip. The leading edge vortex on the wing alone (Figure 31) is quite strong but bursts soon after forming. The addition of the high or mid canard (Figs. 33 and 36 respectively) noticeably delays the vortex bursting on the wing. But for the low canard (Figure 38) the leading edge vortex appears to start forming near mid span but bursts very soon after. Figures 34 and 39 again show that the high canard wake passes over the wing and that the wing is in the wake of the low canard.

f) ALPHA = 180°: The photographs showing several canard-wing configurations at 180° angle of attack are presented in Figures 40-43. In general, these flow fields show very few differences from the flow fields of these configurations at an angle of attack of 15°.

g) ALPHA = 200°: Figures 44-54 show the flow fields of the canard-wing combinations at 200° angle of attack. Comparing the canard alone, high canard, mid canard, and low canard pictures (Figures 44, 46, 49 and 52, respectively), it is seen that the leading edge vortex on the canard in the low position (Figure 52) appears to burst noticeably closer to the canard apex than the other canard configurations. The leading edge vortex on the wing alone, Figure 45, bursts considerably closer to the wing apex than the vortex on the wing in the presence of the high canard (Figure 47) or of the mid canard (Figure 50). The wing in the presence of the low canard (Figure 53) still has a small vortex forming near mid span. Figures 48, 51, and 54 are side views of the high, mid, and low canards in the presence of the wing and show the same canard wake trends established at lower angles of attack.
h) \( \alpha = 25^\circ \): Figures 55 and 56 show the vortex flow field on the canard alone and on the wing with the mid canard.

i) \( \alpha = 30^\circ \): The canard-wing models at an angle of attack of \( 30^\circ \) are presented in Figures 57-65. Figure 57 shows the canard alone with the leading edge vortex bursting very close to the canard apex. The wing alone (Figure 58) appears to be completely stalled at this angle of attack. With the addition of a high or mid canard (Figs. 60 and 62, respectively) the positive influence of the canard on the wing is readily seen. In both cases the wing has a leading edge vortex, bursting close to the apex. The flow field of the wing in the presence of a high or mid canard is better organized than the flow field on the wing alone. However, both the canards, high and mid locations (Figures 59 and 61), are close to being stalled. For the low canard case (Figures 63 and 64), the canard is nearly stalled and the wing again has very disorganized flow with a short mid-span vortex. Figure 65 (wing with low canard) shows the flow being turned by the upwash of the wing. This appears to produce an increase in effective angle of attack and stalls the wing sooner.

j) \( \alpha = 40^\circ \): Figures 66-73 present the canard-wing models at \( 40^\circ \) angle of attack. At this angle all canards and wings are stalled.

II) **Strake-Wing Configuration**

a) \( \alpha = -10^\circ \): Figure 74 shows the strake-wing configuration at \( -10^\circ \) angle of attack. The flow is streamwise with no apparent sidewash disturbances.

b) \( \alpha = 0^\circ \): At \( 0^\circ \) angle of attack (Figure 75), the flow field is very smooth with no spanwise flow.
c) \( \alpha = 10^\circ \): As with the wing alone photographs (Figures 18 and 19) at \( 10^\circ \) angle of attack, the wing with the strake has a slight disturbance along the wing leading edge (Figure 76). Again, there probably is a small, weak leading edge vortex that cannot trap a helium bubble so the bubble streaks just flow over the vortex. However, Figure 77 shows that a strake vortex has been formed. A side view of the strake-wing is presented in Figure 78.

d) \( \alpha = 12^\circ \): At \( 12^\circ \) angle of attack (Figure 79) the strake vortex becomes stronger and a wing leading edge vortex develops just outbound of the kink (where the strake meets the leading edge of the wing). This vortex appears to be bursting near the trailing edge of the wing.

e) \( \alpha = 15^\circ \): Figures 80 and 81 present photographs of the strake-wing configuration at \( 15^\circ \) angle of attack. A wing leading edge vortex is formed but it appears to be bursting further upstream than this vortex did at \( 12^\circ \) angle of attack. Also a still tighter strake vortex is present than was present at \( 12^\circ \) angle of attack.

f) \( \alpha = 18^\circ \): At \( 18^\circ \) angle of attack, a secondary wing leading edge vortex has appeared along with the vortex that developed at lower angles of attack (Figure 82). This secondary vortex was not expected; however, it appears to be very weak. A tight primary vortex is displayed in Figure 83. Figure 84 is a photograph of the strengthening strake vortex. No bursting of this vortex system occurs until higher angles of attack are reached. Another side view is provided by Figure 85.

g) \( \alpha = 20^\circ \): Figures 86-90 present the strake-wing at \( 20^\circ \) angle of attack. Figures 86 and 87 show the main wing vortex and Figures 88-90 show both the primary and secondary wing leading edge vortex systems. The
secondary leading edge vortex is weaker than the main vortex and sometimes gets wrapped up in it (Figure 89).

h) ALPHA = 25°: Figures 91-94 present several views of the strake-wing vortices. Figure 91 shows the main wing vortex bursting earlier than when the model was at 20° angle of attack. Figure 94 shows the tight core of the strake vortex created at these higher angles of attack.

i) ALPHA = 30°: The angle of attack of 30° for the strake-wing is shown in Figures 95-99. The wing primary vortex is bursting soon after forming but the secondary wing leading edge vortex is still present (Figure 97). Figure 99 shows the strake vortex bursting near the wing mid-root chord.

j) ALPHA = 34°: A photograph of the strake vortex is presented in Figure 100. This picture shows a good example of vortex bursting.

k) ALPHA = 40°: At 40° angle of attack, Figure 101 shows the wing is now stalled. The strake vortex (Figure 102) is now bursting near the wing's leading edge.

CONCLUDING REMARKS

Semi-span, close-coupled canard-wing and strake-wing models were mounted in the Langley 1/8-scale V/STOL model tunnel to qualitatively determine the flow field about these models. Small helium filled soap bubbles were injected into the flow upstream of the models to make the flow field visible. Photographs were taken over the angle of attack range of -10° to 40° at 0° sideslip. Some of the major results are outlined below:

1. The presence of a canard above or in the wing chord plane enhances the wing's leading edge vortex and delays wing stall.
2. At positive angles of attack the wake of the canard location above the wing chord plane passes over the wing, however, over the same angle of attack range, the wing is in or above the wake of the canard located below the wing chord plane.

3. For angles of attack greater than 180°, there are three separate vortex systems attached to the strake-wing configuration: strake leading edge vortex, a primary wing leading edge vortex emitting from the kink, and a secondary wing leading edge vortex.

REFERENCES


FIGURE 1. WING AND CANARD PLANFORM
Figure 5. Canard alone at \(-10^\circ\) angle of attack.
Figure 6. Wing alone at $-10^\circ$ angle of attack.
Figure 7. High canard at $-10^\circ$ angle of attack.
Figure 8. Wing in the presence of the high canard at $-10^\circ$ angle of attack.
Figure 9. Side view of high canard configuration at $-10^\circ$ angle of attack.
Figure 10. Mid canard at $-10^0$ angle of attack.
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Figure 13. Low canard at $-10^\circ$ angle of attack.
Figure 14. Wing in the presence of the low canard at $-10^\circ$ angle of attack.
Figure 15. Wing in the presence of the mid canard at $0^\circ$ angle of attack.
Figure 16. Wing in the presence of the low canard at $0^\circ$ angle of attack.
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Figure 18. Wing alone at $10^0$ angle of attack.
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Figure 20. High canard at $10^0$ angle of attack.
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