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A COMPUTER PROGRAM FOR
FITTING SMOOTH SURFACES
TO AN AIRCRAFT CONFIGURATION
AND OTHER THREE-DIMENSIONAL GEOMETRIES

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16. Abstract <p>A computer program that uses a three-dimensional geometric technique for fitting a smooth surface to the component parts of an aircraft configuration is presented. The resulting surface equations are useful in performing various kinds of calculations in which a three-dimensional mathematical description is necessary. Program options may be used to compute information for three-view and orthographic projections of the configuration as well as cross-section plots at any orientation through the configuration.</p> <p>The aircraft (Harris) geometry input section of the program may be easily replaced with a surface point description in a different form so that the program could be of use for any three-dimensional surface equations.</p>					
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A COMPUTER PROGRAM FOR FITTING SMOOTH SURFACES
TO AN AIRCRAFT CONFIGURATION AND OTHER
THREE-DIMENSIONAL GEOMETRIES

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SUMMARY

A digital computer program (D3400) that uses a three-dimensional geometric technique for fitting a smooth surface to the component parts of an aircraft configuration is presented. The resulting surface equations are useful in performing various kinds of calculations in which a three-dimensional mathematical description is necessary.

Program options may be used to compute information for three-view and orthographic projections of the configuration as well as cross-section plots at any orientation through the configuration. These operations were implemented to validate the usefulness and versatility of the surface equations. Output from this program has been used to drive Calcomp, Gerber, and Varian plotters and for on-line display on a cathode-ray-tube device.

The aircraft (Harris) geometry input section of the program may be easily replaced with a surface point description in a different form. Therefore, the program could be of use for any three-dimensional surface equations.

At the present time, the program can only be applied to relatively smooth surfaces; that is, there must be no abrupt changes in curvature. This deficiency is overcome to some degree by using the airplane component parts or, stated another way, by using a collection of surfaces.

INTRODUCTION

Aerospace vehicles, automobiles, and ships are examples of objects which require smooth curved surfaces to establish their exterior shapes. An integral part of the design, development, and manufacture of these objects is the construction of surface models which can be analyzed for their interaction with the environment in which they are to operate. The most useful models from the point of view of versatility and exactness of definition are mathematical models.

The simplest mathematical model of a three-dimensional surface is a set of planes which are defined by points and approximate the curved surface. In order to obtain an

accurate definition using a discrete set of planes, a large number of points on the surface must be defined. Preparing and manipulating the data which yield a planar approximation of a surface is laborious if an accurate definition is desired. Another difficulty with planar approximation occurs when cross sections or contours of curved surfaces are necessary. Planar approximation yields a very rough cross section or contour unless an extremely large number of points are used to define the surface.

In recent years a high-order accurate method for mathematical modeling of smooth three-dimensional surfaces has been developed. (See ref. 1.) This method is based on approximating an arbitrary surface by piecing together surface "patches." Each patch is defined by four boundary curves and is bicubic with respect to two parametric variables in the interior. A patch is therefore defined by four corner points, the first derivative of the corner points with respect to two parametric variables, and the cross derivatives of the corner points with respect to the parametric variables. The patch-equation definition yields a smooth representation of an arbitrary surface with relatively few points of definition. It also yields smooth approximations to cross sections and contour plots.

The purpose of this report is to describe a computer program which is based on the use of sets of bicubic patches to define a relatively smooth surface. (See ref. 2.) In particular the data description for the program is oriented toward aircraft configurations. This allows the organization of data for the various components to be identical with the data used for several standardized aerodynamic analysis computer programs. (See ref. 3.) The aircraft data description has become known as the Harris Wave Drag geometry.

The program can also be used to model arbitrary three-dimensional objects by using an alternate data input format. The data-point input to the program is not required to be equally spaced in any coordinate variable. However, there are some restrictions on the number of points in the descriptive lines for the same surface.

A three-dimensional parametric cubic spline technique is used to curve fit the input data points roughly describing the surface. From the curve fit, the derivatives of the surface patches with respect to the parametric variable at the corner points are established. The cross derivatives of the patch representations with respect to the parametric variables are not used in this program. The values of the corner points and the derivatives at the corner points constitute the information necessary to solve the patch equation. In this way 36 pieces of information are required to define a patch; however, only 12 pieces of information must be supplied as input. The remainder is determined from the spline fit. Appendix A describes the cubic spline fit technique and appendix B, the patch equations.

The entire aircraft geometry or other three-dimensional object is converted into surface patch form. Each patch definition is identical in matrix structure which simplifies the organization of the computer program and data base. (See appendix C.) All

computations, such as rotations, are performed directly on patch equations rather than on interpolated x-, y-, and z-coordinates.

The computer program has the ability to display the orthographic projections of the input description of the surface and the enriched description of the surface based on the patch definition. (See appendix D.) The desired angles of orientation for viewing the surface are inputs to the computer program and the transformation based on these angles is applied to the patch definition. An option of the program tests the derivatives normal to the surface and deletes those points from the orthographic projection which are facing away from the observer. This option gives the program a partial hidden-line capability which works very well for convex closed surfaces. Figures 1 to 3 are examples of orthographic projections.

The program is also capable of producing plots of the surface coordinates of a cross section at any desired orientation. (See appendix E.) Figures 4 to 6 are examples of cross-section plots. The cross-section calculations consist of the simultaneous solution of the patch equations and the equation of a plane. The plane is defined by three points which are input to the program.

SYMBOLS

A,B,C,D	parametric cubic spline coefficients
a,b,c,d	plane equation coefficients
\bar{B}	boundary matrix
L	chord length
M	blending function matrix
\bar{M}	Mach number
N	surface normal vector
P	a vector whose components are functions of t
P_1, P_2, P_3	points used to define a plane
S	component of surface patch equation

T	diagonal vectors
t	independent variable in cubic equation
u,w	independent variables in patch equation
V	a vector whose components are functions of u and w
v	unit vector
x,y,z	coordinates of a point
θ	pitch angle
$\bar{\theta}$	roll angle for Mach plane orientation
ϕ	roll angle
ψ	yaw angle

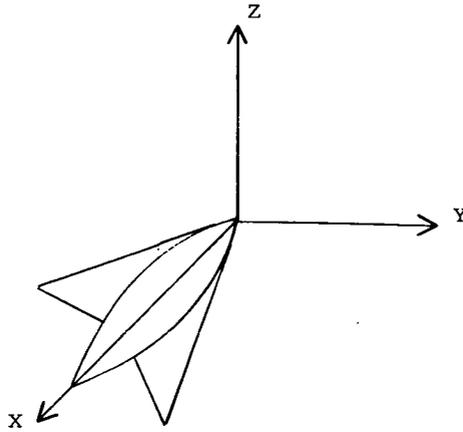
PROBLEM DESCRIPTION AND METHOD OF SOLUTION

The numerical model of the input airplane configuration is assumed to be symmetrical about the XZ-plane (positive Y-side) and may include any combination of components: wing, body, pods, fins, and canards. The wing is made up of airfoil sections, the fuselage is defined by either circular or arbitrary sections, the pods are defined similar to the fuselage, and fins and canards are defined similar to the wings.

The configuration is usually positioned with its nose at the origin and with the length of the body stretching in the positive X-direction.

The coordinate system used for this program is a right-handed Cartesian coordinate system as illustrated in sketch (a).

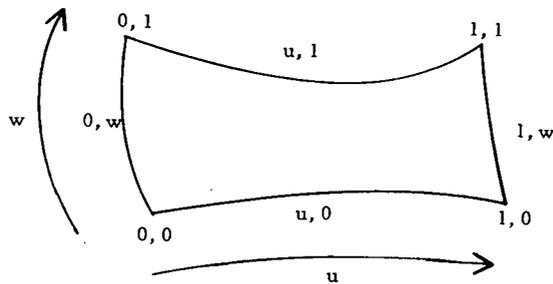
Since the modeling technique expects to approximate a smooth surface, sufficient input data points with no abrupt changes in curvature should be supplied. A three-dimensional parametric cubic spline technique is used for the patch boundary-curve definitions in which the coordinates are expressed as cubic functions of one variable. A series of adjacent polynomial segments between each given point is used to represent the curve. The length of each segment is used as the parameter and later normalized to 1. Linear segments are used when a line consists of less than three points.



Sketch (a)

The cubic spline curve fitting subroutine uses a technique from a paper by Timothy Johnson of Massachusetts Institute of Technology and is summarized in appendix A.

The x-, y-, and z-coordinates of a surface patch are each single-valued cubic functions of two parameters, u and w. The coefficients of these cubics are expressed in terms of end points and partial and cross derivatives with respect to the u and w parameters. The result is a parametric bicubic representation of three-dimensional surfaces. Sketch (b) shows a typical patch.



Sketch (b)

Each patch equation requires 48 pieces of information.

A summary of the bicubic surface patch equation form is given in appendix B and the storage file description of the surface patches is given in appendix C.

The orthographic projections illustrated in this report are created by applying the three-dimensional rotation equations directly to the patch equations describing the body surface for plotting the aircraft at any desired viewing angle. The rotated patch equations are projected into the two-dimensional patch form of the paper plane. An enriched

surface may be obtained from the rotated and projected patch equations by holding u constant and varying w from 0.0 to 1.0, then by holding w constant and varying u from 0.0 to 1.0.

The orthographic plotting routine also includes a hidden-line option where the normal vectors are computed from the rotated and projected form of the patches. A positive normal vector indicates that the point is visible and a negative normal vector indicates that the vector points away from the viewer and thus is not visible. The method used for the orthographic projections is given in appendix D.

Another routine has been written to compute and plot the surface coordinates of a cross section through the body at any desired orientation. The calculations consist of the simultaneous solution of the patch equations and the equation of a plane. The method is described in appendix E.

PROGRAM DESCRIPTION

LABELED COMMON

The following list contains the FORTRAN variables appearing in labeled COMMON.

<u>COMMON label</u>	<u>FORTRAN variable</u>	<u>Description</u>
PATPLT		
	XMIN	Minimum x-value for plotting
	XMAX	Maximum x-value for plotting
	YMIN	Minimum y-value for plotting
	YMAX	Maximum y-value for plotting
	ZMIN	Minimum z-value for plotting
	ZMAX	Maximum z-value for plotting
	NOBJ	Total number of objects (or components) which could form an aircraft configuration
THREED		
	ABCDE(8)	Identification
	HORZ	X-axis of the paper plane
	VERT	Y-axis of the paper plane
	TEST1	Hidden-line option flag

COMMON
label

FORTTRAN
variable

Description

PHI	Roll angle
THETA	Pitch angle
PSI	Yaw angle
PLOTSZ	Plot frame size
TYPE	Type of plot desired
NOU	Number of internal points for each patch in u-direction
NOW	Number of internal points for each patch in w-direction
ISIDE	Flag for plotting object or object and its mirror image
KODE	Flag for plot-option branch

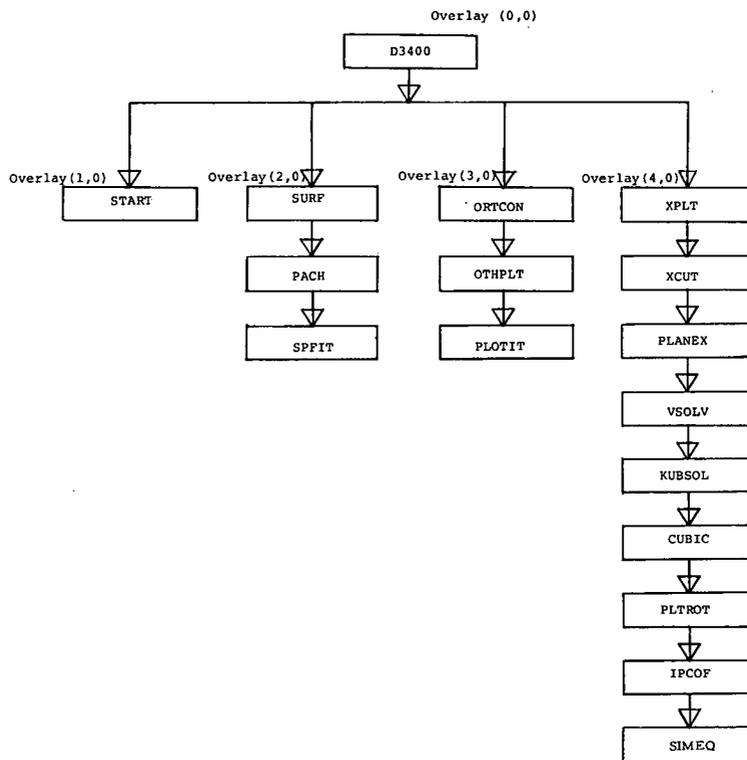
XSECT

ABCDE(8)	Identification
PPL1(3)	Origin of cross-section plot and one point in three-point-plane definition
PPL2(3)	Second point in three-point-plane definition; or X-intercept, roll angle, and Mach number in plane-angle definition
PPL3(3)	Third point in three-point-plane definition
PLOTSZ	Scale factor
HPAGE	Horizontal paper origin
VPAGE	Twice the vertical paper origin
INP	Specifies kind of plane input
NOU	Number of points to interpolate for each patch in u-direction
NOW	Number of points to interpolate for each patch in w-direction
ISIDE	Flag for examining object or object and its mirror image

<u>COMMON label</u>	<u>FORTTRAN variable</u>	<u>Description</u>
	IPRIN	Print code
	KODE	Flag for plot-option branch
	XSTAT	X-intercept for Mach plane
	THETR	Roll angle for Mach plane orientation
	XMACH	Mach number

OVERLAY ARRANGEMENT

Program D3400 is set up in the overlay mode and sketch (c) illustrates the overlay arrangement.



Sketch (c)

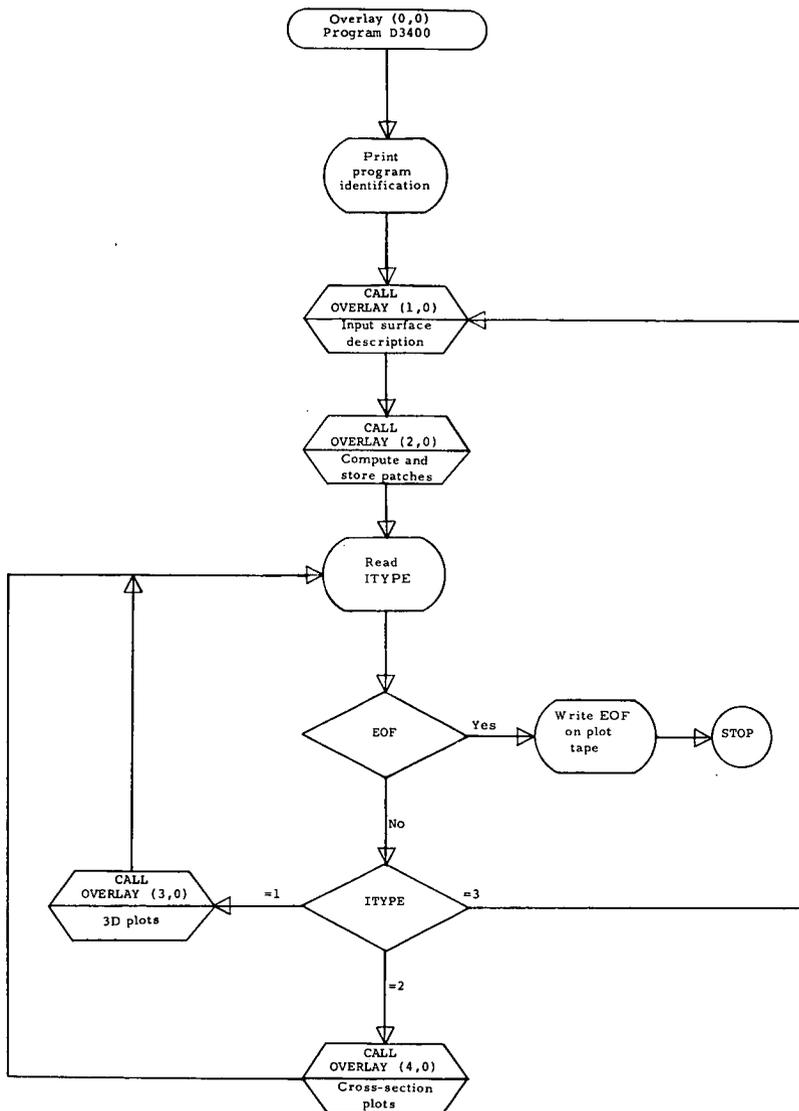
The control program (0,0) calls in the other parts of the program as they are needed. The initialization overlay (1,0) reads cards defining the body surface, converts the input to actual units, and temporarily stores the surface description as a series of lines. Cubic

spline fairing is performed on curved lines defining the body surface in overlay (2,0) and surface patch equations are constructed and temporarily stored. Overlay (3,0) generates orthographic plot information using the patch equations, and overlay (4,0) generates cross-sectional plot information using the patch equations.

PROGRAMS AND SUBPROGRAMS

Program D3400

Program D3400 (overlay (0,0)) is the control program. This program initiates loading and execution of other parts of the program as required. The flow chart and the FORTRAN statements for this overlay are as follows:



```
OVERLAY(CBC,0,0)
PROGRAM D3400(INPUT=201,OUTPUT=201,TAPE10=201,
1TAPE5=INPUT,TAPE6=OUTPUT,TAPE7)
```

```
C
C      D3400 (SPADE) - SURFACE PATCH DEFINITION EQUATIONS
C      (CONVERTS A SURFACE POINT DESCRIPTION
C      TO THREE DIMENSIONAL SURFACE PATCH EQUATIONS)
C      PROGRAMER - CHARLOTTE B. CRAIDON
C
```

```
COMMON/PATPLT/
LXMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX,NOBJ
```

```
C
C
C      CBC=3LCBC
C      RECALL=6HRECALL
C      CALL PSEUDO
C      WRITE (6,20)
```

```
20  FORMAT (1H11OX,24HPROGRAM D3400 (SPADE) - ,34HSURFACE PATCH DEFINI
TION EQUATIONS///)
```

```
C
C      INPUT SURFACE POINT DESCRIPTION AND PROCESS
C      FOR TAPE 10 AND FOR LABELED COMMON PATPLT
C
```

```
30  CONTINUE
CALL OVERLAY (CBC,1,0,0)
```

```
C
C      COMPUTE AND STORE PATCH EQUATIONS
C
```

```
CALL OVERLAY (CBC,2,0,0)
```

```
C
40  READ (5,50) ITYPE
50  FORMAT (14)
IF (ENDFILE 5) 90,60
60  GO TO (70,80,30), ITYPE
C
```

```
C      THREE DIMENSIONAL PLOTS
C
```

```
70  CONTINUE
CALL OVERLAY (CBC,3,0,0)
GO TO 40
```

```
C
C      CROSS SECTION PLOTS
C
```

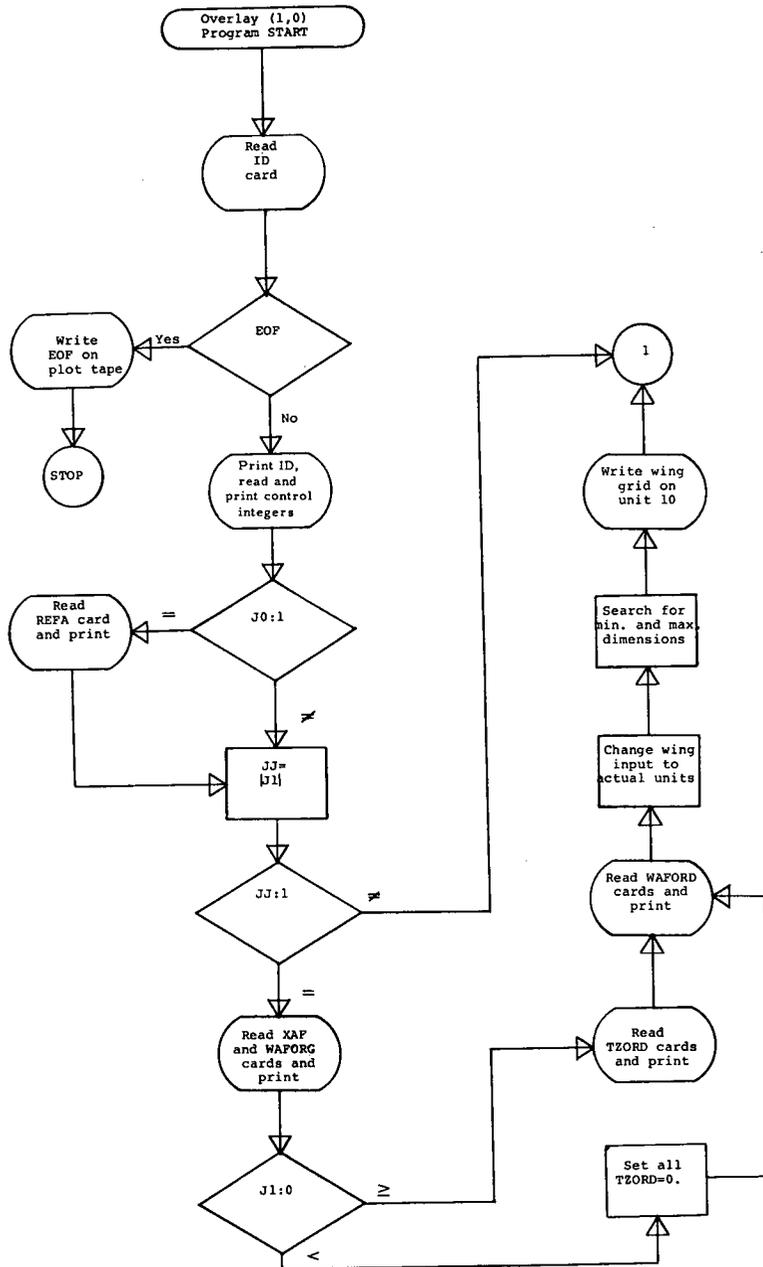
```
80  CALL OVERLAY (CBC,4,0,0)
GO TO 40
90  CALL NFRAME $ CALL CALPLT(0.,0.,999) $ STOP
C
```

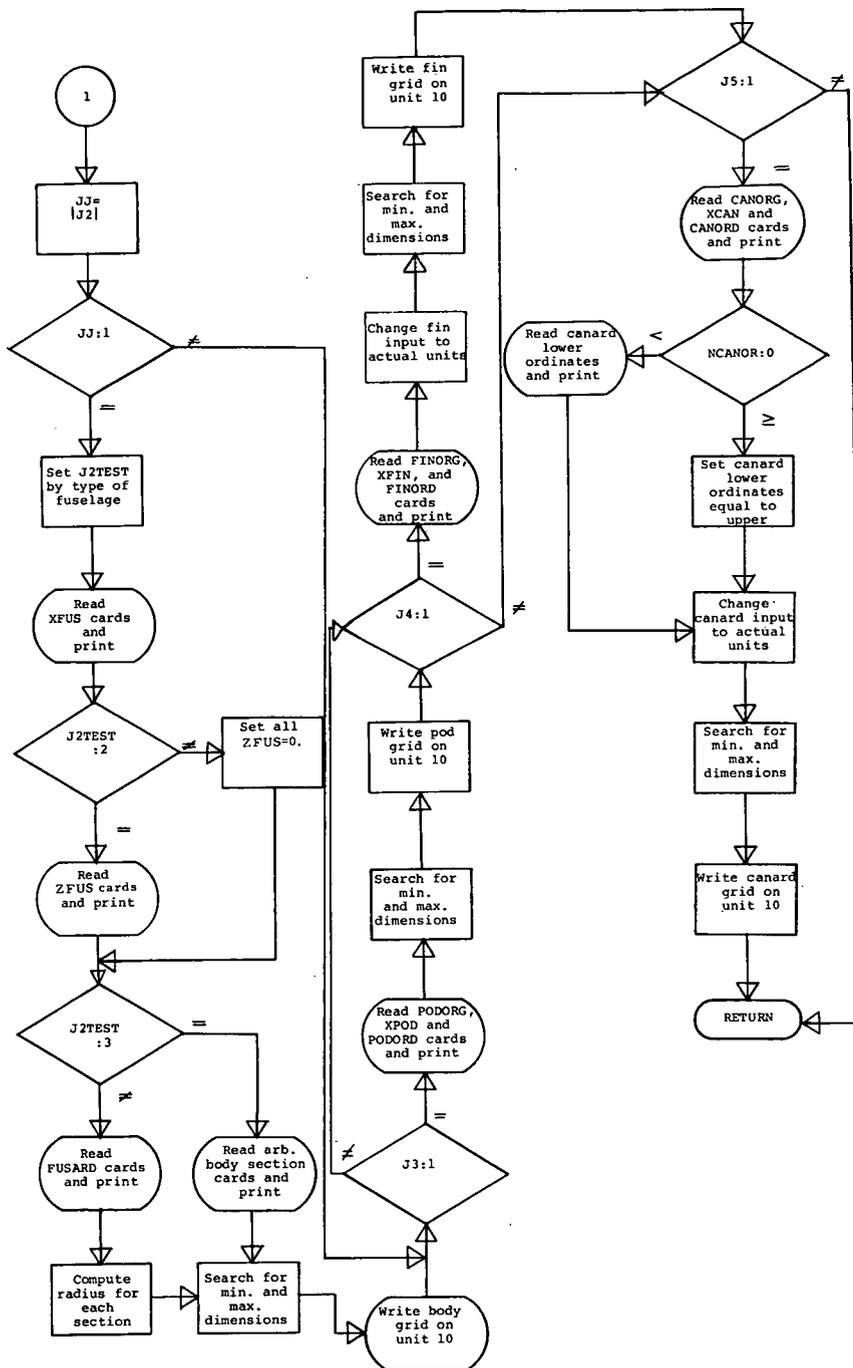
```
C      END OF D3400
C
```

```
END
```

Program START

Program START (overlay (1,0)) reads the configuration description cards and prints them, changes the input values to actual units where necessary, computes the minimum and maximum dimensions of the given configuration, and temporarily stores the airplane description as a series of lines. The flow chart and the FORTRAN statements for this overlay are as follows:





OVERLAY(CBC,1,0)
PROGRAM START

C
C
C
C

INPUTS AIRCRAFT SURFACE DESCRIPTION,
FORMS INTO DESCRIPTIVE LINES WRITTEN ON TAPE 10,
AND COMPUTES MINIMUMS AND MAXIMUMS

COMMON/PATPLT/
LXMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX,NGBJ

C
C

DIMENSION BLOCK (7500)

DIMENSION XAF(30),WAFORG(20,4),WAFORD(20,3,30),TZORD(20,30)
EQUIVALENCE (BLOCK,XAF),(BLOCK(31),WAFORG),
1(BLOCK(111),WAFORD),(BLOCK(1911),TZORD)

C

DIMENSION XFUS(30,4),ZFUS(30,4),FUSARD(30,4),FUSRAD(30,4),
LSFUS(30,30,8)
EQUIVALENCE (BLOCK,XFUS),(BLOCK(121),ZFUS),(BLOCK(241),FUSARD),
1(BLOCK(361),FUSRAD),(BLOCK(241),SFUS)

C

DIMENSION PODURG(9,3),XPOD(9,30),PODORD(9,30),XPOD1(9,30)
EQUIVALENCE (BLOCK,PODURG),(BLOCK(28),XPOD),(BLOCK(298),PODORD),
1(BLOCK(568),XPOD1)

C

DIMENSION FINORG(6,2,4),XFIN(6,10),FINORD(6,2,10),
1FINX2(6,2,10),FINX3(6,2,10)
EQUIVALENCE (BLOCK,FINORG),(BLOCK(49),XFIN),(BLOCK(109),FINORD),
1(BLOCK(229),FINX2),(BLOCK(349),FINX3)

C

DIMENSION CANORG(2,2,4),XCAN(2,10),CANORD(2,2,10),
1CANOR1(2,2,10),CANORX(2,2,10)
EQUIVALENCE (BLOCK,CANORG),(BLOCK(17),XCAN),(BLOCK(37),CANORD),
1(BLOCK(77),CANOR1),(BLOCK(117),CANORX)

C

DIMENSION ABC(8),ABCD(8),ANSIN(30),ANCOS(30),NAME(2)
DIMENSION NRADX(4),NFORX(4)
DIMENSION ALERT (31,3)
DATA PI/3.14159265/

C

REWIND 10
10 FORMAT (8A10)
20 FORMAT (1X8A10)
30 FORMAT (10F7.0)

C
C
C

READ 10 CARD AND CARD OF CONTROL INTEGERS

READ (5,10) ABC
IF (ENDFILE 5) 35,40
35 CALL NFRAME \$ CALL CALPLT(0.,0.,999) \$ STOP
40 CONTINUE
WRITE (6,50) ABC
50 FORMAT (23X,34HAIRCRAFT CONFIGURATION DESCRIPTION//1X8A10/)
READ (5,10) ABCD
WRITE (6,60) ABCD
60 FORMAT (1X8A10/)
DECODE (72,70,ABCD) J0,J1,J2,J3,J4,J5,J6,NWAF,NWAFOR,NFUS,(NRADX(I
1),NFORX(I),I=1,4),NP,NPODOR,NF,NFINOK,NCAN,NCANOR

```

70  FORMAT (24I3)
C
WRITE (10) ABC
NOBJ=0

C
C      REFERENCE AREA
C

IF (JO.NE.1) GO TO 80
READ (5,10) ABCD
WRITE (6,20) ABCD

C
C      WING
C

80  JJ=IABS(J1)
IF (JJ.NE.1) GO TO 290
N=IABS(NWAFOR)
NREC=(N+9)/10
I1=-9
I2=0
DO 90 NN=1,NREC
READ (5,10) ABCD
WRITE (6,20) ABCD
I1=I1+10
I2=I2+10
DECODE (70,30,ABCD) (XAF(I),I=I1,I2)
90  CONTINUE
DO 100 I=1,NWAF
READ (5,10) ABCD
WRITE (6,20) ABCD
DECODE (28,30,ABCD) (WAFGRG(I,J),J=1,4)
100 CONTINUE
IF (J1.LT.0) GO TO 130
DO 120 NN=1,NWAF
I1=-9
I2=0
DO 110 N1=1,NREC
READ (5,10) ABCD
WRITE (6,20) ABCD
I1=I1+10
I2=I2+10
DECODE (70,30,ABCD) (TZORD(NN,I),I=I1,I2)
110 CONTINUE
120 CONTINUE
GO TO 150
130 DO 140 I=1,NWAF
DO 140 K=1,N
TZORD(I,K)=0.
140 L=1
150 IF (NWAFDR.LT.0) L=2
DO 170 NN=1,NWAF
DO 170 K=1,L
I1=-9
I2=0
DO 160 N1=1,NREC
READ (5,10) ABCD
WRITE (6,20) ABCD
I1=I1+10
I2=I2+10

```

```

        DECODE (70,30,ABCD) (WAFORD(NN,K,I),I=11,12)
160    CONTINUE
170    CONTINUE
        IF (NWAFOR.LT.0) GO TO 190
        DO 180 NN=1,NWAF
        DO 180 K=1,N
180    WAFORD(NN,2,K)=WAFORD(NN,1,K)
190    CONTINUE
        NWAFOR=IABS(NWAFOR)
        NW=NWAFOR
        J1=IABS(J1)
C
C      CHANGE TO ACTUAL UNITS, COMPUTE MINIMUMS AND MAXIMUMS
C
        DO 210 I=1,NWAF
        E=.01*WAFORG(I,4)
        E3=WAFORG(I,3)
        DO 200 J=1,NWAFOR
        WAFORD(I,1,J)=E*WAFORD(I,1,J)+E3+TZORD(I,J)
        WAFORD(I,2,J)=-E*WAFORD(I,2,J)+E3+TZORD(I,J)
200    WAFORD(I,3,J)=WAFORG(I,1)+E*XAF(J)
210    CONTINUE
        XMIN=XMAX=WAFORG(1,1)
        YMAX=WAFORG(1,2)
        YMIN=WAFORG(1,2)
        ZMIN=ZMAX=WAFORD(1,1,1)
        DO 230 N=1,NWAF
        XMAX=AMAX1(XMAX,WAFORD(N,3,NW))
        XMIN=AMIN1(XMIN,WAFORD(N,3,1))
        YMAX=AMAX1(YMAX,WAFORG(N,2))
        YMIN=AMIN1(YMIN,WAFORG(N,2))
        DO 220 NN=1,NW
        ZMAX=AMAX1(ZMAX,WAFORD(N,1,NN))
        ZMIN=AMIN1(ZMIN,WAFORD(N,2,NN))
220    CONTINUE
230    CONTINUE
C
C      WRITE LINE TAPE
C
        NN=2
        NCOMP=1$NAME(1)=10HWING      $NAME(2)=10H
        WRITE (10) NN,NCOMP,NAME,NN,NN
        NUBJ=NUBJ+1
        DO 280 I=1,2
        WRITE (10) NWAFA,NWAFOR,NN,NN,NN
        KKK=(I-1)*(NWAFOR+1)
        KK=(-1)**(I+1)
C
C      SETUP SPANWISE LINES
C
        DO 250 K=1,NWAFOR
        NN=KKK+KK*K
        DO 240 N=1,NWAF
        ALRT(N,1)=WAFORD(N,3,NN)
        ALRT(N,2)=WAFORG(N,2)
        ALRT(N,3)=WAFORD(N,1,NN)
240    CONTINUE
        WRITE (10) ((ALRT(N,N3),N=1,NWAF),N3=1,3)
250    CONTINUE

```

```

C
C      SETUP STREAMWISE LINES
C
DO 270 NN=1,NWAF
DO 260 K=1,NWAFUR
N=KKK+KK*K
ALRT(K,1)=WAFORD(NN,3,N)
ALRT(K,2)=WAFORG(NN,2)
ALRT(K,3)=WAFORD(NN,1,N)
260 CONTINUE
WRITE (10) ((ALRT(N,N3),N=1,NW),N3=1,3)
270 CONTINUE
280 CONTINUE
C
C      FUSELAGE
C
290 JJ=IABS(J2)
IF (JJ.NE.1) GO TO 590
J2TEST=3
IF (J2.EQ.-1.AND.J6.EQ.-1) J2TEST=1
IF (J2.EQ.-1.AND.J6.EQ.0) J2TEST=2
IF (J6.EQ.1) J2TEST=1
J2=1
DO 410 NFU=1,NFUS
NRAD=NRADX(NFU)
NFUSOR=NFURX(NFU)
N=NFUSUR
NREC=(N+9)/10
I1=-9
I2=0
DO 300 N1=1,NREC
READ (5,10) ABCD
WRITE (6,20) ABCD
I1=I1+10
I2=I2+10
DECODE (70,30,ABCD) (XFUS(I,NFU),I=I1,I2)
300 CONTINUE
IF (J2TEST.NE.2) GO TO 320
I1=-9
I2=0
DO 310 N1=1,NREC
READ (5,10) ABCD
WRITE (6,20) ABCD
I1=I1+10
I2=I2+10
DECODE (70,30,ABCD) (ZFUS(I,NFU),I=I1,I2)
310 CONTINUE
GO TO 340
320 DO 330 I=1,N
330 ZFUS(I,NFU)=0.
340 IF (J2TEST.NE.3) GO TO 380
NCARD=(NRAD+9)/10
DO 370 LN=1,N
DO 360 K=1,2
KK=K+(NFU-1)*2
II=10
I1=-9
I2=0

```

```

DO 350 NN=1,NCARD
IF (NN.EQ.NCARD) II=MOD(NRAD,10)
IF (II.EQ.0) II=10
I1=I1+10
I2=I2+II
READ (5,10) ABCD
WRITE (6,20) ABCD
DECODE (70,30,ABCD) (SFUS(I,LN,KK),I=I1,I2)
350 CONTINUE
360 CONTINUE
370 CONTINUE
GO TO 410
380 I1=-9
I2=0
DO 390 N1=1,NREC
READ (5,10) ABCD
WRITE (6,20) ABCD
I1=I1+10
I2=I2+10
DECODE (70,30,ABCD) (FUSARD(I,NFU),I=I1,I2)
390 CONTINUE
DO 400 I=1,N
FUSRAD(I,NFU)=SQRT(FUSARD(I,NFU)/PI)
C
410 CONTINUE
C
C FUSELAGE MIN AND MAX
C
IF (J1.NE.0) GO TO 430
XMIN=XFUS(1,1)
XMAX=XFUS(1,1)
IF (J2TEST.EQ.3) GO TO 420
YMIN=FUSRAD(1,1)
YMAX=FUSRAD(1,1)
ZMIN=-FUSRAD(1,1)+ZFUS(1,1)
ZMAX=FUSRAD(1,1)+ZFUS(1,1)
GO TO 430
420 YMAX=SFUS(1,1,1)
YMIN=SFUS(1,1,1)
ZMIN=SFUS(1,1,2)
ZMAX=SFUS(1,1,2)
430 DO 470 N=1,NFUS
NRAD=NRADX(N)
NFUSOR=NFORX(N)
XMIN=AMINI(XMIN,XFUS(1,N))
XMAX=AMAX1(XMAX,XFUS(NFUSOR,N))
DO 460 NN=1,NFUSOR
IF (J2TEST.EQ.3) GO TO 440
YMAX=AMAX1(YMAX,FUSRAD(NN,N))
YMIN=AMINI(YMIN,FUSRAD(NN,N))
ZMAX=AMAX1(ZMAX,FUSRAD(NN,N)+ZFUS(NN,N))
ZMIN=AMINI(ZMIN,-FUSRAD(NN,N)+ZFUS(NN,N))
GO TO 460
440 KK=1+(N-1)*2
DO 450 NR=1,NRAD
YMIN=AMINI(YMIN,SFUS(NR,NN,KK))
YMAX=AMAX1(YMAX,SFUS(NR,NN,KK))
ZMIN=AMINI(ZMIN,SFUS(NR,NN,KK+1))
450 ZMAX=AMAX1(ZMAX,SFUS(NR,NN,KK+1))

```

```

460 CONTINUE
470 CONTINUE
C
C WRITE LINE TAPE
C
JJN=2$N1=1$NAME(1)=10HFUSELAGE $NAME(2)=1.0H
NOBJ=NOBJ+NFUS
DO 580 NFU=1,NFUS
NRAD=NRADX(NFU)
NFUSOR=NFORX(NFU)
WRITE (10) N1,JJN,NAME,N1,N1
WRITE (10) NFUSOR,NRAD,N1,N1,N1
NAN=NRAD
IF (J2TEST.EQ.3) GO TO 490
FANG=(NRAD-1)*2
DELE=6.2831853/FANG
DO 480 N=1,NAN
E=N-1
ANSIN(N)=SIN(E*DELE+4.712389)
480 ANCOS(N)=COS(E*DELE+4.712389)
490 CONTINUE
KK=1+(NFU-1)*2
C
C SETUP STREAMWISE LINES
C
DO 530 N=1,NAN
DO 520 NN=1,NFUSOR
ALRT(NN,1)=XFUS(NN,NFU)
IF (J2TEST.EQ.3) GO TO 500
ALRT(NN,2)=FUSRAD(NN,NFU)*ANCOS(N)
ALRT(NN,3)=FUSRAD(NN,NFU)*ANSIN(N)+ZFUS(NN,NFU)
GO TO 510
500 ALRT(NN,2)=SFUS(N,NN,KK)
ALRT(NN,3)=SFUS(N,NN,KK+1)
510 CONTINUE
520 CONTINUE
WRITE (10) ((ALRT(N,N3),N=1,NFUSOR),N3=1,3)
530 CONTINUE
C
C SETUP LINES AROUND BODY
C
DO 570 N=1,NFUSOR
DO 560 NN=1,NAN
ALRT(NN,1)=XFUS(N,NFU)
IF (J2TEST.EQ.3) GO TO 540
ALRT(NN,2)=FUSRAD(N,NFU)*ANCOS(NN)
ALRT(NN,3)=FUSRAD(N,NFU)*ANSIN(NN)+ZFUS(N,NFU)
GO TO 550
540 ALRT(NN,2)=SFUS(NN,N,KK)
ALRT(NN,3)=SFUS(NN,N,KK+1)
550 CONTINUE
560 CONTINUE
WRITE (10) ((ALRT(N,N3),N=1,NAN),N3=1,3)
570 CONTINUE
580 CONTINUE
C
C NACELLES
C

```

```

590 CONTINUE
  IF (J3.NE.1) GO TO 730
  N=NPODOR
  NREC=(N+9)/10
  DO 620 NN=1, NP
  READ (5,10) ABCD
  WRITE (6,20) ABCD
  DECODE (21,30,ABCD) (PODORG(NN,I),I=1,3)
  I1=-9
  I2=0
  DO 600 N1=1,NREC
  READ (5,10) ABCD
  WRITE (6,20) ABCD
  I1=I1+10
  I2=I2+10
  DECODE (70,30,ABCD) (XPOD(NN,I),I=I1,I2)
600 CONTINUE
  I1=-9
  I2=0
  DO 610 N1=1,NREC
  READ (5,10) ABCD
  WRITE (6,20) ABCD
  I1=I1+10
  I2=I2+10
  DECODE (70,30,ABCD) (PODORD(NN,I),I=I1,I2)
610 CONTINUE
620 CONTINUE
C
C      COMPUTE ACTUAL X, MINIMUM, MAXIMUM
C
  DO 630 N=1, NP
  DO 630 NN=1, NPODOR
630 XPOD1(N,NN)=XPOD(N,NN)+PODORG(N,1)
  IF (J1.NE.0.OR.J2.NE.0) GO TO 640
  XMIN=XPOD1(1,1)
  XMAX=XPOD1(1,NPODOR)
  YMIN=PODORG(1,2)+PODORD(1,1)
  YMAX=PODORG(1,2)+PODORD(1,1)
  ZMIN=PODORG(1,3)-PODORD(1,1)
  ZMAX=PODORG(1,3)+PODORD(1,1)
640 DO 660 N=1, NP
  XMIN=AMIN1(XMIN,XPOD1(N,1))
  XMAX=AMAX1(XMAX,XPOD1(N,NPODOR))
  DO 650 NN=1, NPODOR
  YMIN=AMIN1(YMIN,PODORD(N,NN)+PODORG(N,2))
  YMAX=AMAX1(YMAX,PODORD(N,NN)+PODORG(N,2))
  ZMIN=AMIN1(ZMIN,PODORG(N,3)-PODORD(N,NN))
650 ZMAX=AMAX1(ZMAX,PODORG(N,3)+PODORD(N,NN))
660 CONTINUE
  DATA NAN2/4/,PIPL/4.712389/
  NANG1=NAN2+1
  NANG2=2*NAN2+1
  FANG=NAN2*2
  DELE=6.2831853/FANG
  DO 670 N=1,NANG2
  E=N-1
  EE=E*DELE
  ANSIN(N)=SIN(EE+PIPL)
670 ANCOS(N)=COS(EE+PIPL)

```

```

C
C      WRITE LINE TAPE
C
JUN=3;NAME(1)=10HPODS      $NAME(2)=10H
NOBJ=NOBJ+NP
DO 720 NP1=1,NP
I=2
IF (PODORG(NP1,2).EQ.0.) I=1
WRITE (10) 1,JUN,NAME,1,I
DO 720 I=1,2
IF (I.EQ.2.AND.PODORG(NP1,2).EQ.0.) GO TO 720
WRITE (10) NPODR,NANG1,I,I,I

C
C      SETUP STREAMWISE LINES
C
DO 690 K=1,NANG1
NN=(I-1)*NAN2+K
DO 680 N=1,NPODR
ALRT(N,1)=XPOD(NP1,N)+PODORG(NP1,1)
ALRT(N,2)=PODORD(NP1,N)*ANCOS(NN)+PODORG(NP1,2)
ALRT(N,3)=PODORD(NP1,N)*ANSIN(NN)+PODORG(NP1,3)
680 CONTINUE
WRITE (10) ((ALRT(N,N3),N=1,NPODR),N3=1,3)
690 CONTINUE

C
C      SETUP LINES AROUND PODS
C
DO 710 N=1,NPODR
DO 700 K=1,NANG1
NN=(I-1)*NAN2+K
ALRT(K,1)=XPOD(NP1,N)+PODORG(NP1,1)
ALRT(K,2)=PODORD(NP1,N)*ANCOS(NN)+PODORG(NP1,2)
ALRT(K,3)=PODORD(NP1,N)*ANSIN(NN)+PODORG(NP1,3)
700 CONTINUE
WRITE (10) ((ALRT(K,N3),K=1,NANG1),N3=1,3)
710 CONTINUE
720 CONTINUE

C
C      FINS
C
730 CONTINUE
IF (J4.NE.1) GO TO 890
N=NF INOR
DO 740 NN=1,NF
READ (5,10) ABCD
WRITE (6,20) ABCD
DECODE (56,30,ABCD) ((FINORG(NN,I,J),J=1,4),I=1,2)
READ (5,10) ABCD
WRITE (6,20) ABCD
DECODE (70,30,ABCD) (XF IN(NN,I),I=1,N)
READ (5,10) ABCD
WRITE (6,20) ABCD
DECODE (70,30,ABCD) (FINORD(NN,1,J),J=1,N)
740 CONTINUE

C
C      CHANGE TO ACTUAL UNITS, COMPUTE MINIMUMS AND MAXIMUMS
C

```

```

DO 760 LQ=1,NF
DO 760 I=1,2
J=3-I
E=.01*FINORG(LQ,J,4)
E2=FINORG(LQ,J,2)
DO 750 K=1,NFINOR
EE=FINORD(LQ,1,K)*E
FINORD(LQ,J,K)=E2+EE
FINX2(LQ,J,K)=E2-EE
750 FINX3(LQ,J,K)=FINORG(LQ,J,1)+E*XF(LQ,K)
760 CONTINUE
C
IF (J1.NE.0.OR.J2.NE.0.OR.J3.NE.0) GO TO 770
XMIN=FINORG(1,1,1)
XMAX=FINORG(1,1,1)
YMIN=FINORG(1,1,2)
YMAX=FINORG(1,1,2)
ZMIN=FINORG(1,1,3)
ZMAX=FINORG(1,1,3)
770 DO 780 N=1,NF
ZMIN=AMIN1(ZMIN,FINORG(N,1,3))
ZMAX=AMAX1(ZMAX,FINORG(N,2,3))
DO 780 N2=1,2
XMIN=AMIN1(XMIN,FINORG(N,N2,1))
XMAX=AMAX1(XMAX,FINX3(N,N2,NFINOR))
DO 780 NN=1,NFINOR
YMIN=AMIN1(YMIN,FINX2(N,N2,NN))
YMAX=AMAX1(YMAX,FINORD(N,N2,NN))
780 CONTINUE
C
C WRITE LINE TAPE
C
JJN=4$NAME(1)=10HFINS $NAME(2)=10H
NOBJ=NOBJ+NF
NK2=2
DO 880 NF1=1,NF
I=2
IF (FINORG(NF1,1,2).EQ.0.) I=1
WRITE (10) I,JJN,NAME,I,1
DO 870 NN2=1,2
IF (NN2.EQ.2.AND.FINORG(NF1,1,2).EQ.0.) GO TO 870
WRITE (10) NFINOR,NK2,I,1,1
I1=1
I2=2
IF (NN2.EQ.1) GO TO 790
I1=2$I2=1
790 CONTINUE
C
C SETUP HORIZONTAL LINES
C
DO 810 N=1,NFINOR
ALRT(N,1)=FINX3(NF1,I1,N)
ALRT(N,3)=FINORG(NF1,I1,3)
IF (NN2.EQ.2) GO TO 800
ALRT(N,2)=FINORD(NF1,I1,N)
GO TO 810
800 ALRT(N,2)=FINX2(NF1,I1,N)
810 CONTINUE

```

```

WRITE (10) ((ALRT(N,N3),N=1,NFINOR),N3=1,2)
DO 830 N=1,NFINOR
ALRT(N,1)=FINX3(NF1,I2,N)
ALRT(N,3)=FINORG(NF1,I2,3)
IF (NN2.EQ.2) GO TO 820
ALRT(N,2)=FINORD(NF1,I2,N)
GO TO 830
820 ALRT(N,2)=FINX2(NF1,I2,N)
830 CONTINUE
WRITE (10) ((ALRT(N,N3),N=1,NFINOR),N3=1,3)
C
C     SETUP VERTICAL LINES
C
DO 860 NN=1,NFINOR
ALRT(1,1)=FINX3(NF1,I1,NN)
ALRT(2,1)=FINX3(NF1,I2,NN)
ALRT(1,3)=FINORG(NF1,I1,3)
ALRT(2,3)=FINORG(NF1,I2,3)
IF (NN2.EQ.2) GO TO 840
ALRT(1,2)=FINORD(NF1,I1,NN)
ALRT(2,2)=FINORD(NF1,I2,NN)
GO TO 850
840 ALRT(1,2)=FINX2(NF1,I1,NN)
ALRT(2,2)=FINX2(NF1,I2,NN)
850 WRITE (10) ((ALRT(N,N3),N=1,2),N3=1,3)
860 CONTINUE
870 CONTINUE
880 CONTINUE
C
C     CANARDS
C
890 CONTINUE
IF (J5.NE.1) GO TO 1080
N=IABS(NCANOR)
DO 920 NN=1,NCAN
READ (5,10) ABCD
WRITE (6,20) ABCD
DECODE (56,30,ABCD) ((CANORG(NN,I,J),J=1,4),I=1,2)
READ (5,10) ABCD
WRITE (6,20) ABCD
DECODE (70,30,ABCD) (XCAN(NN,I),I=1,N)
READ (5,10) ABCD
WRITE (6,20) ABCD
DECODE (70,30,ABCD) (CANORD(NN,I,J),J=1,N)
IF (NCANOR.LT.0) GO TO 910
DO 900 J=1,N
900 CANOR1(NN,I,J)=CANORD(NN,I,J)
GO TO 920
910 READ (5,10) ABCD
WRITE (6,20) ABCD
DECODE (70,30,ABCD) (CANOR1(NN,I,J),J=1,N)
920 CONTINUE
NCANOR=IABS(NCANOR)
NC=NCANOR
C
C     CHANGE TO ACTUAL UNITS, COMPUTE MINIMUMS AND MAXIMUMS
C

```

```

DO 950 NN=1,NCAN
DO 940 K=1,2
I=3-K
E=.01*CANORG(NN,1,4)
E3=CANORG(NN,I,3)
DO 930 J=1,NCANDR
CANORD(NN,I,J)=E*CANORD(NN,1,J)+E3
CANOR1(NN,I,J)=-E*CANOR1(NN,1,J)+E3
930 CANORX(NN,I,J)=CANORG(NN,I,1)+E*XCAN(NN,J)
940 CONTINUE
950 CONTINUE
IF (J1.NE.0.OR.J2.NE.0.OR.J3.NE.0.OR.J4.NE.0) GO TO 960
XMIN=CANORX(1,1,1)
XMAX=CANORX(1,1,NCANDR)
YMIN=CANORG(1,2,2)
YMAX=CANORG(1,2,2)
ZMIN=CANOR1(1,1,1)
ZMAX=CANORD(1,1,1)
960 DO 990 NCA=1,NCAN
YMIN=AMINI(YMIN,CANORG(NCA,1,2))
YMAX=AMAXI(YMAX,CANORG(NCA,2,2))
DO 980 N2=1,2
XMIN=AMINI(XMIN,CANORX(NCA,N2,1))
XMAX=AMAXI(XMAX,CANORX(NCA,N2,NCANDR))
DO 970 NN=1,NCANDR
ZMIN=AMINI(ZMIN,CANOR1(NCA,N2,NN))
ZMAX=AMAXI(ZMAX,CANORD(NCA,N2,NN))
970 CONTINUE
980 CONTINUE
990 CONTINUE
C
C WRITE LINE TAPE
C
JJN=5$NAME(1)=10HCANARDS $NAME(2)=10H
NOBJ=NOBJ+NCAN
NK2=2
DO 1070 NCA=1,NCAN
WRITE (10) NK2,JJN,NAME,NK2,NK2
DO 1060 I=1,2
WRITE (10) NK2,NC,NK2,NK2,NK2
KKK=(I-1)*(NC+1)
KK=(-1)**(I+1)
C
C SETUP SPANWISE LINES
C
DO 1020 K=1,NC
NN=KKK+KK*K
DO 1010 N2=1,2
ALRT(N2,1)=CANORX(NCA,N2,NN)
ALRT(N2,2)=CANORG(NCA,N2,2)
IF (I.EQ.2) GO TO 1000
ALRT(N2,3)=CANORD(NCA,N2,NN)
GO TO 1010
1000 ALRT(N2,3)=CANOR1(NCA,N2,NN)
1010 CONTINUE
WRITE (10) ((ALRT(N2,N3),N2=1,2),N3=1,3)
1020 CONTINUE

```

C
C
C

SETUP TWO STREAMWISE LINES

```
DO 1050 N2=1,2
DO 1040 N=1,NC
J=KKK+KK*N
ALRT(N,1)=CANORX(NCA,N2,J)
ALRT(N,2)=CANORG(NCA,N2,2)
IF (I.EQ.2) GO TO 1030
ALRT(N,3)=CANORD(NCA,N2,J)
GO TO 1040
1030 ALRT(N,3)=CANORL(NCA,N2,J)
1040 CONTINUE
WRITE (10) ((ALRT(N,N3),N=1,NC),N3=1,3)
1050 CONTINUE
1060 CONTINUE
1070 CONTINUE
1080 CONTINUE
RETURN
```

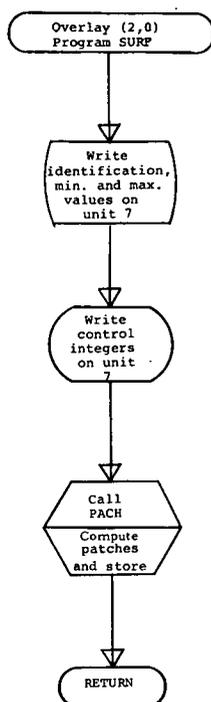
C
C
C

END OF START

END

Program SURF

Program SURF (overlay (2,0)) is the control program for constructing surface patch equations. The flow chart and the FORTRAN statements for this overlay are as follows:



```

OVERLAY(CBC,2,0)
PROGRAM SURF

```

```

C
C      CALLS A SUBROUTINE TO COMPUTE PATCHES
C      AND CONTROLS WRITING OF PATCH TAPE
C

```

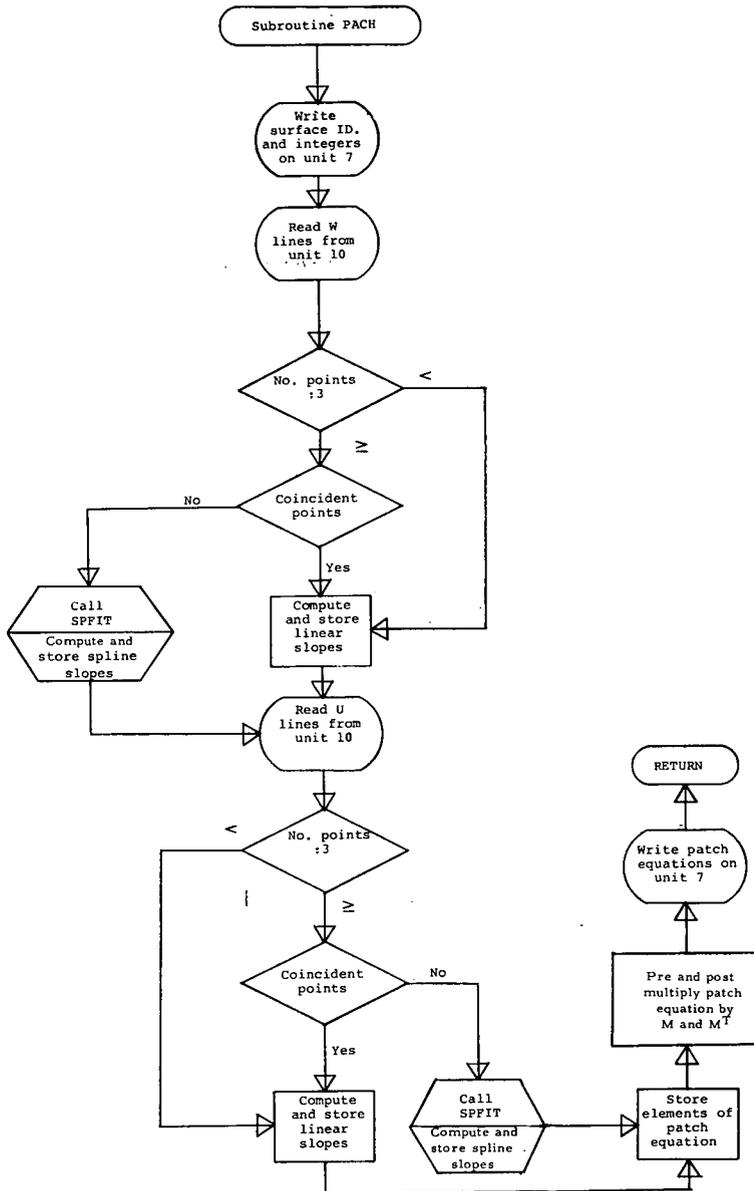
```

COMMON/PATPLT/
IXMIN, XMAX, YMIN, YMAX, ZMIN, ZMAX, NOBJ
DIMENSION ABC(8)
REWIND 7
REWIND 10
READ (10) ABC
CALL RECOU (7,2,0,ABC,1,8,1)
CALL RECOU (7,1,0,XMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX,NOBJ)
DO 20 I=1,NOBJ
READ (10) NSURF, J2, J3, J4, J5, J6
CALL RECOU (7,1,0,NSURF, J2, J3, J4, J5, J6)
DO 10 N=1,NSURF
READ (10) NCOL, NROW, N3, N4, N5
CALL PACH (NCOL, NROW, N3, N4, N5)
10 CONTINUE
20 CONTINUE
END FILE 7
RETURN
END

```

Subroutine PACH

Subroutine PACH computes surface patch equations from the given grid information describing a surface. The patch equations are stored for further use. The flow chart and the FORTRAN statements for this subroutine are as follows:



```

SUBROUTINE PACH (NLD,NLS,L1,L2,L3)
C
C   CONSTRUCTS SURFACE PATCHES WITH THE COMPONENTS
C   EXPRESSED AS CUBIC FUNCTIONS OF TWO PARAMETERS (U AND W)
C   AND WRITES ON TAPE
C
DIMENSION PATCH(4,4,3),COEF1(31,4,3),COEF2(31,4,3)
DIMENSION SLOPE(31,31,3),XMAT(4,4),ALINE(31,3),ELEN(31),PAT(4,4)
DATA (XMAT(I),I=1,16)/2.,-3.,0.,1.,-2.,3.,0.,0.,
11.,-2.,1.,0.,1.,-1.,0.,0./
DATA MAXN/31/,EPS/.00001/
NL=NLD-1
N2=NLS-1
CALL RECOU (7,1,0,N1,N2,L1,L2,L3)
C
C   COMPUTE PARAMETRIC SLOPES IN W DIRECTION
C
DO 70 N=1,NLS
READ (10) ((ALINE(NN,N3),NN=1,NLD),N3=1,3)
C
C   CHECK IF CUBIC FAIRING POSSIBLE
C
IF (NLD.LT.3) GO TO 20
C
C   CHECK FOR A POINT
C
NL=NLD-1
DO 10 NN=1,NL
E1=ABS(ALINE(NN,1)-ALINE(NN+1,1))
E2=ABS(ALINE(NN,2)-ALINE(NN+1,2))
E3=ABS(ALINE(NN,3)-ALINE(NN+1,3))
IF (E1+E2+E3.LE.EPS) GO TO 20
10 CONTINUE
GO TO 40
C
C   COMPUTE LINEAR SLOPES
C
20 DO 30 NN=1,NLD
DO 30 N3=1,3
SLOPE(NN,N,N3)=ALINE(2,N3)-ALINE(1,N3)
30 CONTINUE
GO TO 70
C
C   COMPUTE CUBIC SPLINE SLOPES
C
40 CALL SPFIT (MAXN,NLD,ALINE,ELEN,COEF1,11,0,12,EK,CP,13,14)
NL=NLD-1
DO 50 NN=1,NL
DO 50 N3=1,3
SLOPE(NN,N,N3)=COEF1(NN,3,N3)
50 CONTINUE
DO 60 N3=1,3
SLOPE(NLD,N,N3)=3.*COEF1(NLD-1,1,N3)+2.*COEF1(NLD-1,2,N3)+COEF1(NL
10-1,3,N3)
60 CONTINUE
70 CONTINUE
C

```

```

C      COMPUTE PARAMETRIC SLOPES IN U DIRECTION
C      FORM PATCHES AND WRITE TAPE
C
C      READ (10) ((ALINE(NN,N3),NN=1,NLS),N3=1,3)
C
C      CHECK IF CUBIC FAIRING POSSIBLE
C
C      IF (NLS.LT.3) GO TO 90
C
C      CHECK FOR A POINT
C
C      NL=NLS-1
C      DO 80 NN=1,NL
C      E1=ABS(ALINE(NN,1)-ALINE(NN+1,1))
C      E2=ABS(ALINE(NN,2)-ALINE(NN+1,2))
C      E3=ABS(ALINE(NN,3)-ALINE(NN+1,3))
C      IF (E1+E2+E3.LE.EPS) GO TO 90
80     CONTINUE
C      GO TO 110
C
C      COMPUTE LINEAR SLOPES
C
C      DO 100 NN=1,NLS
C      DO 100 N3=1,3
C      COEF1(NN,3,N3)=ALINE(2,N3)-ALINE(1,N3)
C      COEF1(NN,4,N3)=ALINE(NN,N3)
100    CONTINUE
C      GO TO 130
110    CONTINUE
C
C      COMPUTE CUBIC SPLINE SLOPES
C
C      CALL SPFIT (MAXN,NLS,ALINE,ELEN,COEF1,K1,0,K2,EP,CP,K3,K4)
C      DO 120 N3=1,3
C      COEF1(NLS,3,N3)=3.*COEF1(NLS-1,1,N3)+2.*COEF1(NLS-1,2,N3)+COEF1(NL
1S-1,3,N3)
C      COEF1(NLS,4,N3)=COEF1(NLS-1,1,N3)+COEF1(NLS-1,2,N3)+COEF1(NLS-1,3,
1N3)+COEF1(NLS-1,4,N3)
120    CONTINUE
130    CONTINUE
C      DO 290 N=2,NLD
C      READ (10) ((ALINE(NN,N3),NN=1,NLS),N3=1,3)
C      IF (NLS.LT.3) GO TO 150
C      NL=NLS-1
C      DO 140 NN=1,NL
C      E1=ABS(ALINE(NN,1)-ALINE(NN+1,1))
C      E2=ABS(ALINE(NN,2)-ALINE(NN+1,2))
C      E3=ABS(ALINE(NN,3)-ALINE(NN+1,3))
C      IF (E1+E2+E3.LE.EPS) GO TO 150
140    CONTINUE
C      GO TO 170
150    DO 160 NN=1,NLS
C      DO 160 N3=1,3
C      COEF2(NN,3,N3)=ALINE(2,N3)-ALINE(1,N3)
C      COEF2(NN,4,N3)=ALINE(NN,N3)
160    CONTINUE
C      GO TO 190

```

```

170 CALL SPFIT (MAXN,NLS,ALINE,ELEN,COEF2,K1,0,K2,EP,CP,K3,K4)
DO 180 N3=1,3
COEF2(NLS,3,N3)=3.*COEF2(NLS-1,1,N3)+2.*COEF2(NLS-1,2,N3)+COEF2(NL
1S-1,3,N3)
COEF2(NLS,4,N3)=COEF2(NLS-1,1,N3)+COEF2(NLS-1,2,N3)+COEF2(NLS-1,3,
1N3)+COEF2(NLS-1,4,N3)
180 CONTINUE
C
C STORE PATCHES
C
190 DO 270 L=2,NLS
DO 210 N3=1,3
DO 200 M=1,2
MM=MOD(M,2)
LL=L-MM
PATCH(M,1,N3)=COEF1(LL,4,N3)
PATCH(M,2,N3)=COEF2(LL,4,N3)
PATCH(M,3,N3)=SLOPE(N-1,LL,N3)
PATCH(M,4,N3)=SLOPE(N,LL,N3)
PATCH(M+2,1,N3)=COEF1(LL,3,N3)
PATCH(M+2,2,N3)=COEF2(LL,3,N3)
PATCH(M+2,3,N3)=0.
PATCH(M+2,4,N3)=0.
200 CONTINUE
210 CONTINUE
C
C COMPUTE PATCH IN FORM OF S=MBM(TRANPOSE) AND WRITE ON TAPE
C
DO 260 N3=1,3
DO 230 I4=1,4
DO 230 J4=1,4
SUM=0.
DO 220 K4=1,4
220 SUM=SUM+XMAT(I4,K4)*PATCH(K4,J4,N3)
230 PAT(I4,J4)=SUM
C
DO 250 I4=1,4
DO 250 J4=1,4
SUM=0.
DO 240 K4=1,4
240 SUM=SUM+PAT(I4,K4)*XMAT(J4,K4)
250 PATCH(I4,J4,N3)=SUM
260 CONTINUE
CALL RECOOT (7,2,0,PATCH,1,48,1)
270 CONTINUE
C
C MOVE COEFFICIENTS
C
DO 280 N3=1,3
DO 280 N4=1,4
DO 280 NN=1,NLS
COEF1(NN,N4,N3)=COEF2(NN,N4,N3)
280 CONTINUE
290 CONTINUE
RETURN
END

```

Subroutine SPFIT

Subroutine SPFIT uses a parametric cubic spline curve fit technique with optional enrichment of the given input curve. The method is explained in appendix A. The description, flow chart, and the FORTRAN statements for this subroutine are as follows:

Language: FORTRAN

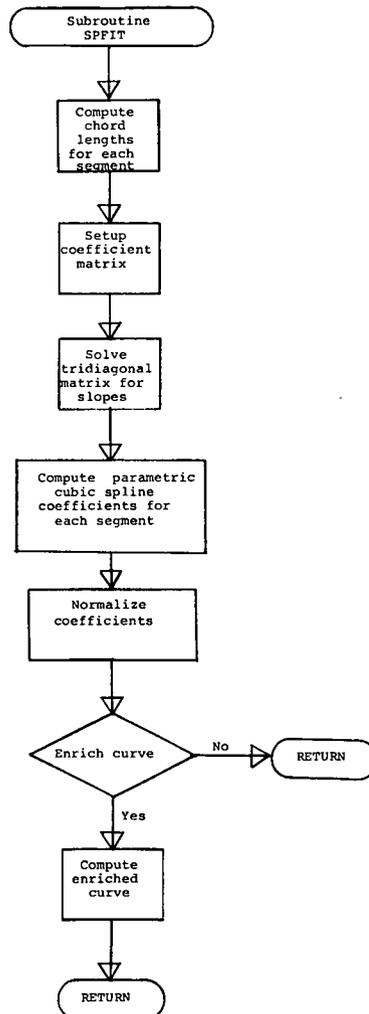
Purpose: SPFIT is a parametric cubic spline curve fit subroutine. Parametric coefficients are computed to approximate a cubic spline curve through a three-dimensional set of input points describing a curve, and, optionally an enriched curve is computed.

Use: CALL SPFIT (MAXN, N, PNT, ELEN, COEF, NFIT, MAXSP, II, EPS, CPT, K1, K2)

MAXN	The maximum number of input points allowed as stated in the dimension statement of the calling program.
N	The number of input points; $4 \leq N \leq \text{MAXN}$.
PNT	A two-dimensional array of the consecutive points describing the three-dimensional (X,Y,Z) input curve.
ELEN	A one-dimensional array used by the subroutine for the chord lengths between each consecutive pair of input points.
COEF	A three-dimensional array used by the subroutine for the parametric cubic spline coefficients.
NFIT	A number of interpolated points to be computed between each pair of given points as specified by the user.
MAXSP	The maximum number of points allowed in the enriched curve as stated in the dimension statement of the calling program. If MAXSP is 0, only the cubic spline coefficients are computed and the calculation of the enriched curve is omitted.
II	The total number of points in the enriched curve calculated by the subroutine.
EPS	A small number supplied by the user which is used to check the second derivative at each point of the faired curve. The point will be omitted if the absolute value of the second derivative is less than EPS. An EPS of 0.0 will cause all the interpolated points to be retained.
CPT	A two-dimensional array used by the program for storage of the enriched curve.

- K1** An integer supplied by the user. If $K1=1$, retain all the input points. If $K1=2$, include input points in second derivative test.
- K2** An integer supplied by SPFIT as an error code. If $K2=1$, normal return. If $K2=2$, error return when the number of interpolated points exceeds the allowable storage (MAXSP).

Restrictions: SPFIT has been written with a variable dimension statement, and the following must be dimensioned in the calling program: PNT(MAXN,3), ELEN(MAXN), COEF(MAXN,4,3), CPT(MAXSP,3). If the coefficient-only option is used (MAXSP=0), dummy entries for NFIT, II, EPS, CPT, K1, and K2 must be included in the calling sequence. The input curve must not include any consecutive duplicate points.



```

SUBROUTINE SPFIT (MAXN,N,PNT,ELEN,COEF,NFIT,MAXSP,II,EPS,CPT,K1,K2
1)

```

```

C
C   COMPUTES PARAMETRIC CUBIC SPLINE COEFFICIENTS TO
C   APPROXIMATE A SMOOTH CURVE THROUGH A 3D SET OF INPUT
C   POINTS AND OPTIONALLY COMPUTES AN ENRICHED CURVE
C   MAXN IS THE MAXIMUM NUMBER OF INPUT POINTS ALLOWED
C   N IS THE ACTUAL NO. OF INPUT POINTS
C   NFIT IS THE NUMBER OF DESIRED SPLINED POINTS BETWEEN GIVEN
C   POINTS
C   MAXSP IS THE MAXIMUM NUMBER OF SPLINED POINTS ALLOWED,
C   MAXSP=(MAXN-1)*(MAX,NFIT+1)+1 FOR EPS OF 0.
C   MAXSP=0 OUMITS COMPUTATION OF ENRICHED CURVE
C   II IS THE NO. OF POINTS IN THE ENRICHED CURVE
C   K1 IS AN INTEGER SUPPLIED BY THE USER
C   K1=1,RETAIN ALL INPUT POINTS
C   K1=2,INCLUDE INPUT POINTS IN SECOND DERIVATIVE TEST
C   K2 IS AN INTEGER SUPPLIED BY SPFIT AS AN ERROR CODE
C   K2=1,NORMAL RETURN
C   K2=2,INCOMPLETE FAIRED CURVE WHEN MAXSP IS EXCEEDED

```

```

PROGRAMER - CHARLOTTE CRAIDON    2-1-71

```

```

DIMENSION PNT(MAXN,3),ELEN(MAXN),COEF(MAXN,4,3),CPT(MAXSP,3)
DIST(X1,Y1,Z1,X2,Y2,Z2)=SQRT((X2-X1)**2+(Y2-Y1)**2+(Z2-Z1)**2)
N1=N-1

```

```

C
C   COMPUTE CHORD LENGTHS

```

```

C
C   DO 10 NN=2,N
C   ELEN(NN-1)=DIST(PNT(NN-1,1),PNT(NN-1,2),PNT(NN-1,3),PNT(NN,1),PNT(
10 1NN,2),PNT(NN,3))
C   CONTINUE

```

```

C
C   SETUP COEFFICIENT MATRIX WITH UNCLAMPED END POINTS
C   (2ND DER=0. AT P1 AND PN)

```

```

C
C   COEF(1,1,1)=0.
C   COEF(1,1,2)=2.
C   COEF(1,1,3)=1.
C   COEF(N,1,1)=1.
C   COEF(N,1,2)=2.
C   COEF(N,1,3)=0.
C   DO 20 NN=2,N1
C   COEF(NN,1,1)=ELEN(NN)
C   COEF(NN,1,2)=2.*(ELEN(NN-1)+ELEN(NN))
C   COEF(NN,1,3)=ELEN(NN-1)
20 CONTINUE

```

```

C
C   SOLVE FOR SLOPES

```

```

C
C   DO 60 I=1,3
C   COEF(1,4,I)=(3./ELEN(1))*(PNT(2,I)-PNT(1,I))
C   COEF(N,4,I)=(3./ELEN(N-1))*(PNT(N,I)-PNT(N-1,I))
C   DO 30 NN=2,N1
C   COEF(NN,4,I)=(3./(ELEN(NN-1)*ELEN(NN)))*(ELEN(NN-1)**2*(PNT(NN+1,I
30 1)-PNT(NN,I))+ELEN(NN)**2*(PNT(NN,I)-PNT(NN-1,I)))
C   CONTINUE

```

```

C
C      SOLVE TRIDIAGONAL MATRIX
C
COEF(1,2,1)=COEF(1,1,3)/COEF(1,1,2)
COEF(1,3,1)=COEF(1,4,1)/COEF(1,1,2)
DO 40 K=2,N
  KM1=K-1
  TEMP=COEF(K,1,2)-COEF(K,1,1)*COEF(KM1,2,1)
  COEF(K,2,1)=COEF(K,1,3)/TEMP
  COEF(K,3,1)=(COEF(K,4,1)-COEF(K,1,1)*COEF(KM1,3,1))/TEMP
40 CONTINUE
DO 50 K=1,N1
  KK=N-K
  COEF(KK,3,1)=COEF(KK,3,1)-COEF(KK,2,1)*COEF(KK+1,3,1)
50 CONTINUE
60 CONTINUE
C
C      COMPUTE CUBIC COEFFICIENTS FOR EACH SEGMENT
C
DO 70 NN=1,N1
  EL=1./ELEN(NN)
  EL2=EL*EL
  EL3=EL*EL2
  DO 70 I=1,3
    COEF(NN,4,I)=PNT(NN,I)
    E=PNT(NN+1,I)-PNT(NN,I)
    COEF(NN,2,1)=E*EL2*3.-EL*(2.*COEF(NN,3,1)+COEF(NN+1,3,1))
    COEF(NN,1,1)=-E*EL3*2.+EL2*(COEF(NN,3,1)+COEF(NN+1,3,1))
C
C      REFERENCE LENGTH TO 1.
C
COEF(NN,1,1)=COEF(NN,1,1)/EL3
COEF(NN,2,1)=COEF(NN,2,1)/EL2
COEF(NN,3,1)=COEF(NN,3,1)/EL
70 CONTINUE
IF (MAXSP.EQ.0) RETURN
IF (K1.EQ.0) K1=1
I1=0
C
C      COMPUTE ENRICHED POINTS
C
IFIT=NFIT+1
XFIT=IFIT
DELT=1./XFIT
DO 110 NN=1,N1
  DO 100 NF=1,IFIT
    E=NF-1
    T=DELT*E
    IF (NN.EQ.1.AND.NF.EQ.1) GO TO 80
    IF (NF.EQ.1.AND.K1.EQ.1) GO TO 80
    T6=6.*T
    EX=ABS(T6*COEF(NN,1,1)+2.*COEF(NN,2,1))
    EY=ABS(T6*COEF(NN,1,2)+2.*COEF(NN,2,2))
    EZ=ABS(T6*COEF(NN,1,3)+2.*COEF(NN,2,3))
    EE=(EX+EY+EZ)/(ELEN(NN)*ELEN(NN))
    IF (EE.LT.EPS) GO TO 100

```

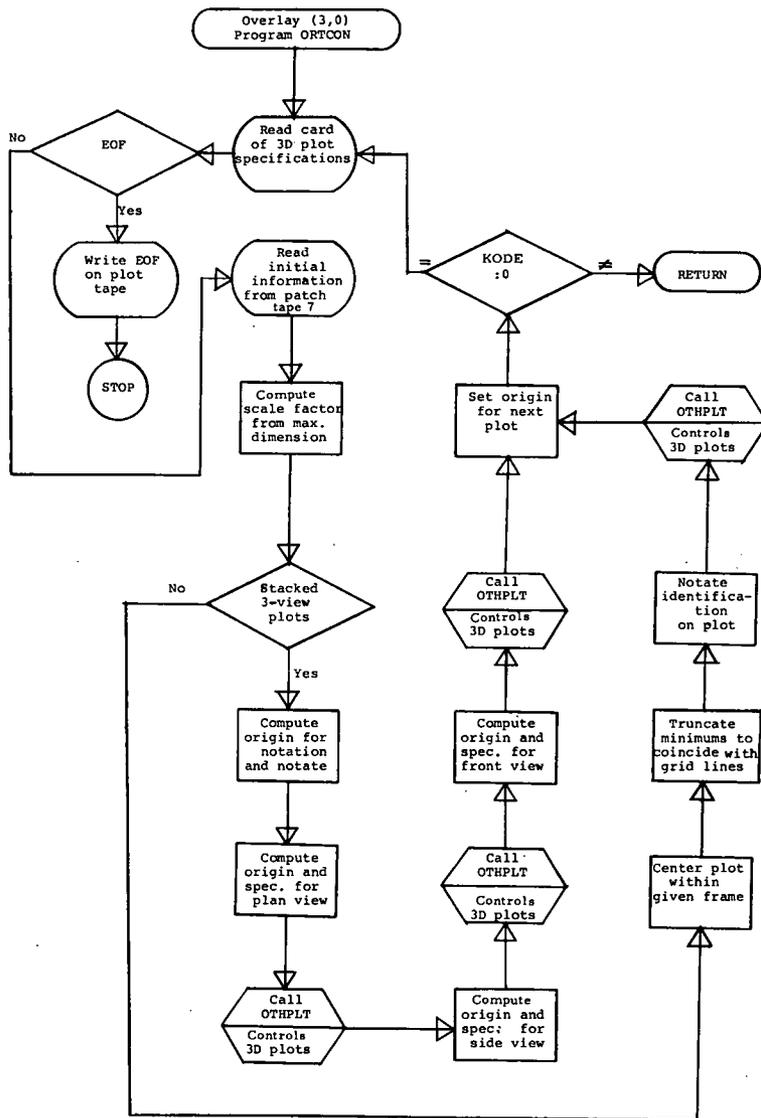
```

80  II=II+1
    IF (II.GT.MAXSP) GO TO 130
    T2=T*I
    T3=T*T2
    DO 90 I=1,3
90  CPT(II,I)=T3*COEF(NN,1,I)+T2*COEF(NN,2,I)+T*COEF(NN,3,I)+COEF(NN,4
1,I)
100 CONTINUE
110 CONTINUE
    II=II+1
    IF (II.GT.MAXSP) GO TO 130
    DO 120 I=1,3
120 CPT(II,I)=PNT(N,I)
    K2=1
    RETURN
130 K2=2
    RETURN
    END

```

Program ORTCOON

Program ORTCOON (overlay (3,0)) is the control routine for the orthographic projections of the input body. This program reads the plot information card and prints it, computes scale factors, computes vertical offsets for three-view plots, and notates on the plot. The flow chart and the FORTRAN statements for this overlay are as follows:



```

OVERLAY(CBC,3,0)
PROGRAM ORTCUN

C
C     CONTROL ROUTINE FOR ORTHOGRAPHIC PLOTS
C     OF A SURFACE OR OF A COLLECTION OF SURFACES
C
COMMON /THREED/ABCDE(8),HORZ,VERT,TEST1,PHI,THETA,PSI,
1 PLOTSZ,TYPE,NOU,NOW,ISIDE,KODE
C
DIMENSION ORG(3),ABC(8)
DATA TYPE0/3HURT/,TYPEV/3EVU3/
C
C     READ PLOT CARD
C
WRITE (6,10)
10 FORMAT (1H126X,27HTHREE DIMENSIONAL PLOT DATA//)
20 CONTINUE
READ (5,30) ABCDE
30 FORMAT (8A10)
IF (ENDFILE 5) 35,40
35 CALL NFRAME $ CALL CALPLT(0.,0.,999) $ STOP
40 WRITE (6,50) ABCDE
50 FORMAT (1X,8A10/)
DECODE (72,60,ABCDE) HORZ,VERT,TEST1,PHI,THETA,PSI,PLOTSZ,TYPE,NOU
1,NOW,ISIDE,KODE
60 FORMAT (2A2,A3,3F5.0,25X,F5.0,A3,3I3,7X,I1)
IF (ISIDE.EQ.0) ISIDE=1
C
C     READ PATCH TAPE
C
REWIND 7
CALL RECIN (7,2,IC,ABC,1,8,1)
IF (ENDFILE 7) 70,90
70 WRITE (6,80)
80 FORMAT (1H1/38H END OF FILE ENCOUNTERED ON PATCH TAPE)
STOP
90 CONTINUE
CALL RECIN (7,1,IC,XMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX,NOBJ)
IF (ISIDE.EQ.2) YMIN=-YMAX
C
C     FIND SCALE FACTOR FROM MAXIMUM DIMENSION
C
XDIS=XMAX-XMIN
YDIS=YMAX-YMIN
ZDIS=ZMAX-ZMIN
DMAX=AMAX1(XDIS,YDIS,ZDIS)
SCALE=DMAX/PLOTSZ
IF (TYPE.NE.TYPEV) GO TO 140
C
C     3VU WHERE VIEWS ARE STACKED VERTICALLY
C
ORG(1)=PHI
ORG(2)=THETA
ORG(3)=PSI
PHI=THETA=PSI=0.

```

```

YBIG=ORG(1)
YORG=FLOAT(IFIX(YMAX/SCALE))+ORG(1)
IF (YBIG.GT.ORG(2)) GO TO 100
YBIG=ORG(2)
YORG=FLOAT(IFIX(ZMAX/SCALE))+ORG(2)
100 IF (YBIG.GT.ORG(3)) GO TO 110
YBIG=ORG(3)
YORG=FLOAT(IFIX(ZMAX/SCALE))+ORG(3)
110 CALL CALPLT (0.,YORG,-3)
C
C     NOTATE ON 3VIEW PLOTS
C
NCHAR=IFIX(6.*PLOTSZ)
IF (NCHAR.GT.80) GO TO 120
X=0.
GO TO 130
120 CONTINUE
NDIF=(NCHAR-80)/2
X=FLOAT(NDIF)/6.
NCHAR=80
130 CALL NOTATE (X,0.,.2,ABC,0.,NCHAR)
YSAV=YMIN
XMIN=YMIN=ZMIN=0.
HORZ=1HX$VERT=1HY
YORG=ORG(1)-YORG-1
CALL CALPLT (0.,YORG,-3)
CALL DTHPLT (XMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX,NOBJ,XMID,YMID,ZMID,SCALE)
VERT=1HZ
YORG=ORG(2)-ORG(1)
CALL CALPLT (0.,YORG,-3)
CALL DTHPLT (XMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX,NOBJ,XMID,YMID,ZMID,SCALE)
HORZ=1HY
YORG=ORG(3)-ORG(2)
YMIN=(FLOAT(IFIX(YSAV/SCALE)-1))*SCALE
CALL CALPLT (0.,YORG,-3)
CALL DTHPLT (XMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX,NOBJ,XMID,YMID,ZMID,SCALE)
X=FLOAT(IFIX(PLOTSZ+6.))
Y=1.-ORG(3)
GO TO 160
140 CONTINUE
C
C     CENTER PLOT
C
XMID=.5*(XMAX+XMIN)
YMID=.5*(YMAX+YMIN)
ZMID=.5*(ZMAX+ZMIN)
XFIX=.5*(DMAX-XDIS)
XMIN=XMIN-XFIX
XMAX=XMAX+XFIX
YFIX=.5*(DMAX-YDIS)
YMIN=YMIN-YFIX
YMAX=YMAX+YFIX
ZFIX=.5*(DMAX-ZDIS)
ZMIN=ZMIN-ZFIX
ZMAX=ZMAX+ZFIX

```

```

C
C      ADJUST MINIMUMS FOR GRID LINES
C
XMIN=FLOAT(IFIX(XMIN/SCALE))*SCALE
YMIN=FLOAT(IFIX(YMIN/SCALE))*SCALE
ZMIN=FLOAT(IFIX(ZMIN/SCALE))*SCALE

C
C      NOTATE ID ON PLOT
C
X=0.
NCHAR=IFIX(11.*PLOTSZ)+3
IF (NCHAR.LE.80) GO TO 150
NDIF=(NCHAR-80)/2
X=FLOAT(NDIF)/11.
NCHAR=80
150 CALL NOTATE (X,.8,.1,ABC,0.,NCHAR)
    CALL NOTATE (X,.5,.1,ABCDE,0.,NCHAR)

C
C      ORTHOGRAPHIC
C
CALL UTHPLT (XMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX,NOBJ,XMID,YMID,ZMID,SCALE)
X=FLOAT(IFIX(PLOTSZ+2.))
Y=0.

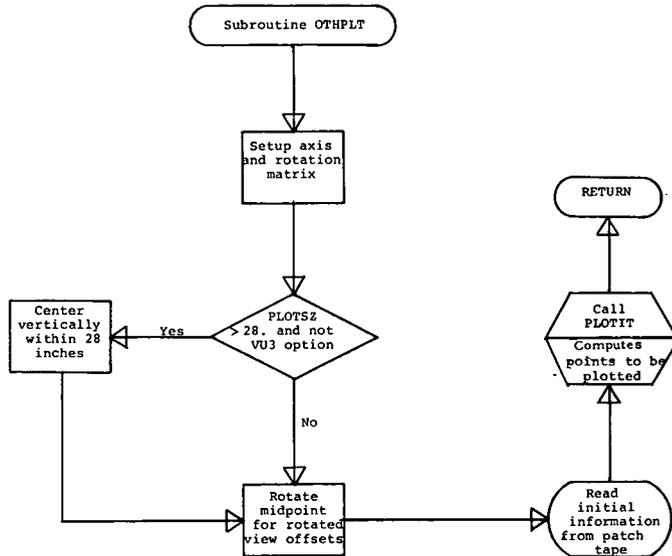
C
C      END OF COMPLETE PLOT
C
160 CONTINUE
    CALL CALPLT(X,Y,-3) $CALL NFRAME
    IF (KODE.EQ.0) GO TO 20
    RETURN

C
C      END OF ORTCUN
C
END

```

Subroutine OTHPLT

Subroutine OTHPLT determines the specified axis system and paper plane, sets up the rotation matrix, and establishes the necessary offsets for proper plot placement. The flow chart and the FORTRAN statements for this subroutine are as follows:



```

SUBROUTINE OTHPLT (XMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX,NOBJ,XMID,YMID,ZMID,SCALE)

```

C
C
C
C

ORTHOGRAPHIC PROJECTIONS

C
C
C

```

COMMON/THREED/ABCDE(8),HORZ,VERT,TEST1,PHI,THETA,PSI,
1PLOTSZ,TYPE,NOU,NOW,ISIDE,KODE

```

C
C
C

```

DIMENSION A(2,3),NAME(2),ABC(8)

```

C
C
C

```

DATA XSEE/2HX /,YSEE/2HY /,ZSEE/2HZ /,
1XINTST/3HOUT/,CONV/.017453293/,NUM2/2/,NAN2/24/

```

C
C

INITIALIZE

```

ITEST1=1
ITEST2=1
IF (XINTST.NE.TEST1) ITEST1=0
IF (PSI.EQ.0..AND.THETA.EQ.0..AND.PHI.EQ.0.) ITEST2=0
PHI=CONV*PHI
THETA=CONV*THETA
PSI=CONV*PSI

```

C
C

SETUP AXIS

```

C
SINPSI=SIN(PHI)
SINTHE=SIN(THETA)
SINPHI=SIN(PHI)
COSPSI=COS(PHI)
COSTHE=COS(THETA)
COSPFI=COS(PHI)
IF (XSEE.NE.HORZ) GO TO 20

C
C   USE X FOR HORIZONTAL VARIABLE
C
IF (ITEST2.EQ.0) GO TO 10
A(1,1)=COSTHE*COSPSI
A(1,2)=-SINPSI*COSPFI+SINTHE*COSPSI*SINPHI
A(1,3)=SINPSI*SINPHI+SINTHE*COSPSI*COSPFI
10  HMIN=XMIN
    HMAX=XMAX
    HMID=XMID
    IHORZ=1
    GO TO 60
20  IF (YSEE.NE.HORZ) GO TO 40

C
C   USE Y FOR HORIZONTAL VARIABLE
C
IF (ITEST2.EQ.0) GO TO 30
A(1,1)=COSTHE*SINPSI
A(1,2)=COSPSI*COSPFI+SINTHE*SINPSI*SINPHI
A(1,3)=-COSPSI*SINPHI+SINTHE*SINPSI*COSPFI
30  HMIN=YMIN
    HMAX=YMAX
    HMID=YMID
    IHORZ=2
    GO TO 60

C
C   USE Z FOR HORIZONTAL VARIABLE
C
40  CONTINUE
    IF (ITEST2.EQ.0) GO TO 50
    A(1,1)=-SINTHE
    A(1,2)=COSTHE*SINPHI
    A(1,3)=COSTHE*COSPFI
50  HMIN=ZMIN
    HMAX=ZMAX
    HMID=ZMID
    IHORZ=3
60  IF (XSEE.NE.VERT) GO TO 80

C
C   USE X FOR VERTICAL VARIABLE
C
IF (ITEST2.EQ.0) GO TO 70
A(2,1)=COSTHE*COSPSI
A(2,2)=-SINPSI*COSPFI+SINTHE*COSPSI*SINPHI
A(2,3)=SINPSI*SINPHI+SINTHE*COSPSI*COSPFI
70  VMIN=XMIN
    VMAX=XMAX
    VMID=XMID
    IVERT=1
    GO TO 120
80  IF (YSEE.NE.VERT) GO TO 100

```

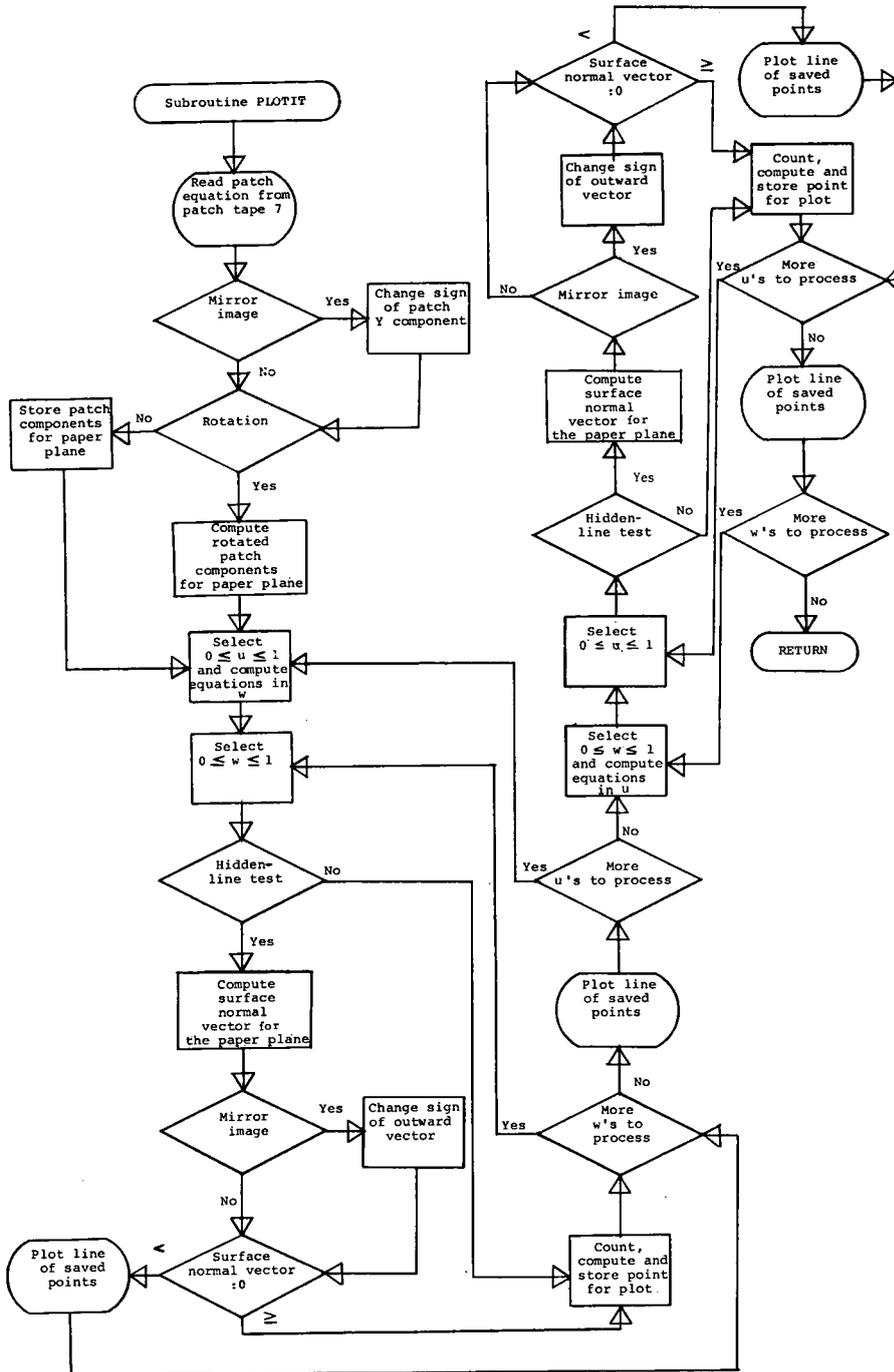
```

C
C      USE Y FOR VERTICAL VARIABLE
C
IF (ITEST2.EQ.0) GO TO 90
A(2,1)=COSTHE*SINPSI
A(2,2)=CUSPSI*COSPHI+SINHE*SINPSI*SINPHI
A(2,3)=-COSPSI*SINPHI+SINHE*SINPSI*COSPHI
90  VMIN=YMIN
    VMAX=YMAX
    VMID=YMID
    IVERT=2
    GO TO 120
C
C      USE Z FOR VERTICAL VARIABLE
C
100 CONTINUE
    IF (ITEST2.EQ.0) GO TO 110
    A(2,1)=-SINHE
    A(2,2)=COSTHE*SINPHI
    A(2,3)=COSTHE*COSPHI
110  VMIN=ZMIN
    VMAX=ZMAX
    VMID=ZMID
    IVERT=3
120  CONTINUE
C
C      CENTER WITHIN PAGE SIZE IF SIZE GREATER THAN 28 INCHES
C
    IF (PLOTSZ.GT.28..AND.TYPE.NE.3HVU3) VMIN=-13.*SCALE+FLOAT(IFIX(VM
1ID/SCALE))*SCALE
C
C      ROTATE MIDPOINT TO PLACE ROTATED VIEW CORRECTLY
C
    IF (ITEST2.EQ.0) GO TO 130
    AMID1=A(1,1)*XMID+A(1,2)*YMID+A(1,3)*ZMID
    AMID2=A(2,1)*XMID+A(2,2)*YMID+A(2,3)*ZMID
    HMIN=HMIN-HMID+AMID1
    VMIN=VMIN-VMID+AMID2
130  CONTINUE
C
C      BEGIN PLOTTING
C
DO 160 ISI=1,ISIDE
REWIND 7
CALL RECIN (7,2,IC,ABC,1,8,1)
CALL RECIN (7,1,IC,H1,H2,H3,H4,H5,H6,I7)
DO 150 J=1,NOBJ
CALL RECIN (7,1,IC,NSURF,J3,NAME(1),NAME(2),J4,J5)
DO 140 N=1,NSURF
CALL RECIN (7,1,IC,ND1,NS1,J3,J4,J5)
CALL PLOTIT (ND1,NS1,ISI,ITEST,ITEST1,ITEST2,IHORZ,IVERT,HMIN,VMIN
1,SCALE,A)
140  CONTINUE
150  CONTINUE
160  CONTINUE
    RETURN
C
C      END OF OTHPLT
C
    END

```

Subroutine PLOTIT

Subroutine PLOTIT reads patch equations from tape and rotates them, computes enriched surfaces, and does a visibility test if desired. The flow chart and the FORTRAN statements for this subroutine are as follows:



```
      SUBROUTINE PLOTIT (ND1,NS1,ISI,ITEST,ITEST1,ITEST2,IHORZ,IVERT,HMI  
      IN,VMIN,SCALE,A)
```

```
C  
C  
C  
C
```

```
      READS PATCHES FROM TAPE,  
      MANIPULATES IN SPECIFIED MANNER AND PLOTS
```

```
      DIMENSION PATCH(4,4,3),PAT(4,4,2),A(2,3),PLPAT(4,2),  
      IPLINE(54,2)  
      DIMENSION VEC(4,2),VPAT(4)  
      COMMON/THREED/ABCDE(8),HORZ,VERT,TEST1,PHI,THETA,PSI,  
      IPLOTSZ,TYPE,NOU,NUW,ISIDE,KUDE
```

```
C
```

```
      NNU=NOU+2  
      NNW=NUW+2  
      FU=NOU+1  
      FW=NUW+1  
      DU=1./FU  
      DW=1./FW  
      NPAT=ND1*NS1  
      DO 230 N=1,NPAT  
      CALL RECIN (7,2,IC,PATCH,1,48,1)  
      IF (ISI.EQ.1) GO TO 20
```

```
C  
C  
C
```

```
      CHANGE Y SIGN
```

```
      DO 10 I4=1,4  
      DO 10 J4=1,4  
      PATCH(I4,J4,2)=-PATCH(I4,J4,2)  
10      CONTINUE  
20      CONTINUE
```

```
C  
C  
C  
C  
C
```

```
      ROTATE PATCHES
```

```
      IF (ITEST2.EQ.1) GO TO 40  
      DO 30 I4=1,4  
      DO 30 J4=1,4  
      PAT(I4,J4,1)=PATCH(I4,J4,IHORZ)  
      PAT(I4,J4,2)=PATCH(I4,J4,IVERT)  
30      CONTINUE  
      GO TO 80  
40      CONTINUE  
      DO 70 I4=1,4  
      DO 70 J4=1,4  
      DO 60 K2=1,2  
      PAT(I4,J4,K2)=0.  
      DO 50 N3=1,3  
      PAT(I4,J4,K2)=PAT(I4,J4,K2)+A(K2,N3)*PATCH(I4,J4,N3)  
50      CONTINUE  
60      CONTINUE  
70      CONTINUE  
80      CONTINUE
```

```
C  
C  
C
```

```
      PLOT IN W DIRECTION
```

```
      DO 150 NU=1,NNU  
      EU=NU-1  
      U=EU*DU
```

```

DO 90 J4=1,4
DO 90 K2=1,2
PLPAT(J4,K2)=((U*PAT(1,J4,K2)+PAT(2,J4,K2))*U+PAT(3,J4,K2))*U+PAT(
14,J4,K2)
VEC(J4,K2)=(3.*U*PAT(1,J4,K2)+2.*PAT(2,J4,K2))*U+PAT(3,J4,K2)
90 CONTINUE
NIT=0
DO 140 NW=1,NNW
EW=NW-1
W=EW*DW
IF (ITEST1.EQ.0) GO TO 120
C
C COMPUTE DV/DU AND DV/DW
C
DO 100 J=1,2
VPAT(J)=((W*VEC(1,J)+VEC(2,J))*W+VEC(3,J))*W+VEC(4,J)
VPAT(J+2)=(3.*PLPAT(1,J)*W+2.*PLPAT(2,J))*W+PLPAT(3,J)
100 CONTINUE
VNORM=VPAT(1)*VPAT(4)-VPAT(2)*VPAT(3)
IF (-ISI.EQ.1) VNORM=-VNORM
IF (VNORM.GE.0.) GO TO 120
IF (NIT.GT.1) GO TO 110
NIT=0
GO TO 140
110 PLINE(NIT+1,1)=HMIN$PLINE(NIT+1,2)=VMIN
PLINE(NIT+2,1)=PLINE(NIT+2,2)=SCALE
CALL LINE (PLINE(1,1),PLINE(1,2),NIT,1,0,0,0)
NIT=0
GO TO 140
120 NIT=NIT+1
DO 130 K2=1,2
PLINE(NIT,K2)=((W*PLPAT(1,K2)+PLPAT(2,K2))*W+PLPAT(3,K2))*W+PLPAT(
14,K2)
130 CONTINUE
140 CONTINUE
IF (NIT.LE.1) GO TO 150
PLINE(NIT+1,1)=HMIN$PLINE(NIT+1,2)=VMIN
PLINE(NIT+2,1)=PLINE(NIT+2,2)=SCALE
CALL LINE (PLINE(1,1),PLINE(1,2),NIT,1,0,0,0)
150 CONTINUE
C
C PLOT IN U DIRECTION
C
DO 220 NW=1,NNW
EW=NW-1
W=EW*DW
DO 160 J4=1,4
DO 160 K2=1,2
PLPAT(J4,K2)=((W*PAT(J4,1,K2)+PAT(J4,2,K2))*W+PAT(J4,3,K2))*W+PAT(
1J4,4,K2)
VEC(J4,K2)=(3.*W*PAT(J4,1,K2)+2.*PAT(J4,2,K2))*W+PAT(J4,3,K2)
160 CONTINUE
NIT=0
DO 210 NU=1,NNU
EU=NU-1
U=EU*DU
IF (ITEST1.EQ.0) GO TO 190

```

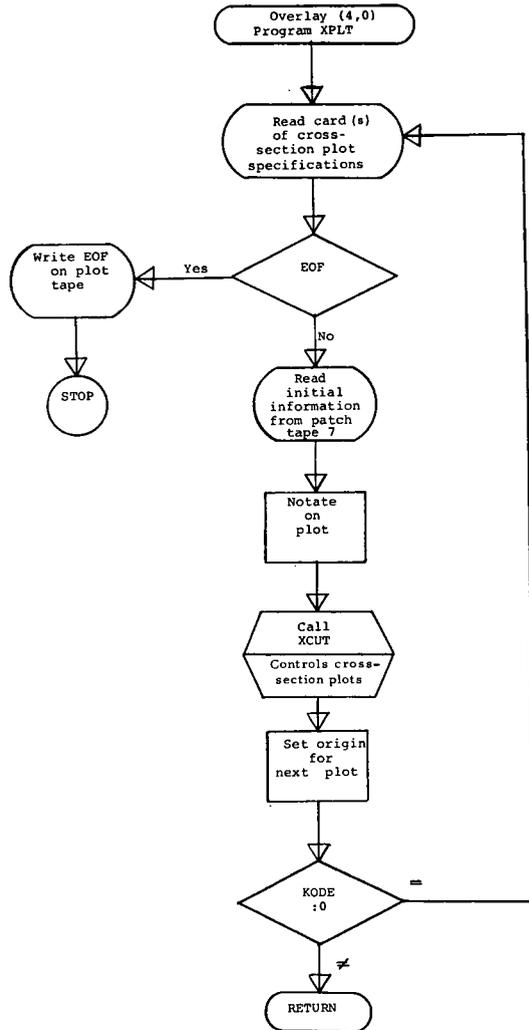
```

C
C      COMPUTE DV/DU AND DV/DW
C
DO 170 J=1,2
VPAT(J)=(3.*PLPAT(1,J)*U+2.*PLPAT(2,J))*U+PLPAT(3,J)
VPAT(J+2)=((U*VEC(1,J)+VEC(2,J))*U+VEC(3,J))*U+VEC(4,J)
170 CONTINUE
VNORM=VPAT(1)*VPAT(4)-VPAT(2)*VPAT(3)
IF (ISI.EQ.1) VNORM=-VNGRM
IF (VNORM.GE.0.) GO TO 190
IF (NIT.GT.1) GO TO 180
NIT=0
GO TO 210
180 PLINE(NIT+1,1)=HMIN$PLINE(NIT+1,2)=VMIN
PLINE(NIT+2,1)=PLINE(NIT+2,2)=SCALE
CALL LINE (PLINE(1,1),PLINE(1,2),NIT,1,0,0,0)
NIT=0
GO TO 210
190 NIT=NIT+1
DO 200 K2=1,2
PLINE(NIT,K2)=((U*PLPAT(1,K2)+PLPAT(2,K2))*U+PLPAT(3,K2))*U+PLPAT(
14,K2)
200 CONTINUE
210 CONTINUE
IF (NIT.LE.1) GO TO 220
PLINE(NIT+1,1)=HMIN$PLINE(NIT+1,2)=VMIN
PLINE(NIT+2,1)=PLINE(NIT+2,2)=SCALE
CALL LINE (PLINE(1,1),PLINE(1,2),NIT,1,0,0,0)
220 CONTINUE
230 CONTINUE
RETURN
END

```

Program XPLT

Program XPLT (overlay (4,0)) is the control routine for cross-section plots through the input body. The program reads the plot information card and prints it and notates on the plot. The flow chart and the FORTRAN statements for this overlay are as follows:



OVERLAY(CBC,4,0)
PROGRAM XPLT

C
C
C
C

CONTROL PROGRAM FOR CRGSS
SECTIONAL OR CONTOUR PLOTS

COMMON/XSECT/ABCDE(8),PPL1(3),PPL2(3),PPL3(3),
1PLOTSZ,HPAGE,VPAGE,INP,NGU,NOW,ISIDE,IPRIN,
2KODE,XSTAT,THETR,XMACH
DIMENSION ABC(8),ABCD(8)

C
C
C

READ PLOT CARD(S) AND PRINT

WRITE (6,10)
10
20
30
35
40
50
60
70
80
90
100
110
120
130
140
150
160
170

FORMAT (1H127X,25HCROSS SECTIONAL PLOT DATA//)
CONTINUE
READ (5,30) ABCDE
FORMAT (8A10)
IF (ENDFILE 5) 35,40
CALL NFRAME \$ CALL CALPLT(0.,0.,999) \$ STOP
CONTINUE
WRITE (6,50)
FORMAT (/26X,30H***** PLOT CARD(S) *****//)
WRITE (6,60) ABCDE
FORMAT (1X8A10)
DECODE (80,70,ABCDE) X1,Y1,Z1,X2,Y2,Z2,X3,Y3,Z3,PLOTSZ,HPAGE,VPAGE
1,INP,NGU,NOW,ICUT,ISIDE,IPRIN,KODE
FORMAT (10F6.0,2F3.0,A3,2I3,I2,3I1)
IF (ICUT.EQ.0) GO TO 90
READ (5,30) ABCD
WRITE (6,60) ABCD
DECODE (21,80,ABCD) DX,DY,DZ,IH
FORMAT (3F6.0,I3)
CONTINUE
IF (INP.EQ.3HANG) GO TO 110
WRITE (6,100) X1,Y1,Z1,X2,Y2,Z2,X3,Y3,Z3,PLOTSZ,HPAGE,VPAGE
FORMAT (/13X,13HCUTTING PLANE/6X,1HX11X,1HY11X,1HZ/3F12.5/3F12.5/
13F12.5//6X,5HSCALE7X,5HHPAGE7X,5HVHPAGE/F12.5,2F12.2)
GO TO 130
WRITE (6,120) X1,Y1,Z1,X2,Y2,Z2,PLOTSZ,HPAGE,VPAGE
FORMAT (/13X,13HCUTTING PLANE/6X,2HX010X,2HY010X,2HZ0/3F12.5/6X,1
1HX11X,5HTHETA7X,4HMACH/3F12.5//6X,5HSCALE7X,5HHPAGE7X,5HVHPAGE/F12.
25,2F12.2)
CONTINUE
WRITE (6,140) NGU,NOW,ICUT,ISIDE,IPRIN
FORMAT (6X,28HNGU NOW ICUT ISIDE IPRIN/19,15,16,217)
IF (ISIDE.EQ.0) ISIDE=1
IF (IPRIN.EQ.0) IPRIN=1
HSAV=HPAGE\$IF(IH.EQ.0)HPAGE=0.
NCUT=ICUT+1
IF (ICUT.NE.0) GO TO 150
DX=0.\$DY=0.\$DZ=0.
GO TO 200
WRITE (6,160) DX,DY,DZ
FORMAT (6X,2HDX10X,2HDY10X,2HDZ/3F12.5)
IF (IH.NE.0) GO TO 180
WRITE (6,170)
FORMAT (27H OVERLAID PLOTS WITH IH = 0)
GO TO 200

```

180 WRITE (6,190) IH
190 FORMAT (24H SPACED PLOTS WITH IH = ,I3)
C
C      LOOP FOR INCREMENTED CUTS
C
200 DO 350 N=1,NCUT
    IF (N.EQ.1) GO TO 290
    IF (INP.EQ.3HPNT) GO TO 250
    X2=X2+DX$Y2=Y2+DY$Z2=Z2+DZ
    DECODE (10,210,ABCDE(2) )TEMP1
210  FORMAT (A8)
    DECODE (10,220,ABCDE(4) )TEMP2
220  FORMAT (6XA4)
    ENCODE (40,230,ABCDE(2) )TEMP1,X2,Y2,Z2,TEMP2
230  FORMAT (A8,3F6.2,A4)
    WRITE (6,240) X2,Y2,Z2
240  FORMAT (//7X,25HINCREMENTED CUTTING PLANE/6X,1HX11X,5HTHETA7X,4HMA
1CH/3F12.5)
    GO TO 290
250  X1=X1+DX$Y1=Y1+DY$Z1=Z1+DZ
    X2=X2+DX$Y2=Y2+DY$Z2=Z2+DZ
    X3=X3+DX$Y3=Y3+DY$Z3=Z3+DZ
    DECODE (10,260,ABCDE(6) )TEMP1
260  FORMAT (4XA6)
    ENCODE (60,270,ABCDE(1) )X1,Y1,Z1,X2,Y2,Z2,X3,Y3,Z3,TEMP1
270  FORMAT (9F6.2,A6)
    WRITE (6,280) X1,Y1,Z1,X2,Y2,Z2,X3,Y3,Z3
280  FORMAT (//26H INCREMENTED CUTTING PLANE/6X,1HX11X,1HY11X,1HZ/3F12.
15/3F12.5/3F12.5)
290  CONTINUE
    PPL1(1)=X1$PPL1(2)=Y1$PPL1(3)=Z1
    PPL2(1)=X2$PPL2(2)=Y2$PPL2(3)=Z2
    PPL3(1)=X3$PPL3(2)=Y3$PPL3(3)=Z3
    IF (N.EQ.NCUT) HPAGE=HSAV
C
C      READ PATCH TAPE
C
    REWIND 7
    CALL RECIN (7,2,IC,ABC,1,8,1)
    IF (ENDFILE 7) 300,320
300  WRITE (6,310)
310  FORMAT (1H1/38H END OF FILE ENCOUNTERED ON PATCH TAPE)
    STOP
320  CONTINUE
C
C      NOTATE
C
    X=0.
    IF (HPAGE.EQ.0.) GO TO 330
    NCHAR=IFIX(11.*HPAGE)+2
    IF (NCHAR.GT.80) NCHAR=80
    CALL NOTATE (X,.8,.1,ABC,0.,NCHAR)
    IF (ICUT.NE.0) CALL NOTATE (X,.6,.1,ABCD,0.,NCHAR)
    CALL NOTATE (X,.4,.1,ABCDE,0.,NCHAR)
330  CONTINUE
    Y=FLOAT(IFIX(.5*VPAGE))+1.
    CALL CALPLT (X,Y,-3)
    IF (HPAGE.NE.0.) CALL NOTATE (0.,0.,2.,3,0.,-1)

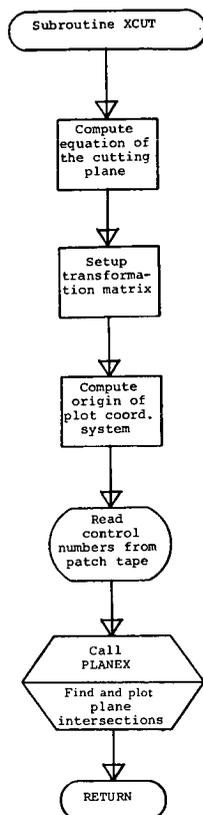
```

```
CALL XCUT
X=0.
Y=-Y
CALL CALPLT (0.,0.,3)
CALL CALPLT (X,Y,-3)
IF (HPAGE.EQ.0.) GO TO 340
X=HPAGE+2.
Y=0.
CALL CALPLT (X,Y,-3)
CALL NFRAME
340 CONTINUE
350 CONTINUE
IF (KODE.EQ.0) GO TO 20
RETURN

C
C     END OF XPLT
C
END
```

Subroutine XCUT

Subroutine XCUT sets up the transformation matrix and the origin of the plot coordinate system for the cross-section plots. The flow chart and the FORTRAN statements for this subroutine are as follows:



SUBROUTINE XCUT

C
C
C

CROSS SECTIONAL OR CONTOUR PLOTS

```

COMMON/XSECT/ABCDE(8),PPL1(3),PPL2(3),PPL3(3),
1PLOTSZ,HPAGE,VPAGE,INP,NGU,NOW,ISIDE,IPRIN,
2KODE,XSTAT,THETR,XMACH
DIMENSION A(3,3),NAME(2),ABC(8)
DIMENSION XPRM(3),PNT1(3),PNT2(3),PNT3(3),PNT4(3)
EQUIVALENCE (PNT1,PPL1),(PNT2,PPL2),(PNT3,PPL3)
  
```

C
C
C

INITIALIZE

```

SCALE=1./PLOTSZ
XB=PPL1(1)$YB=PPL1(2)$ZB=PPL1(3)
IF (INP.EQ.3HANG) GO TO 20
M=IPCDF(ACDEF,B,C,D,PPL1,PPL2,PPL3)
IF (M.EQ.1) GO TO 30
  
```

```

WRITE (6,10)
10  FORMAT (/19H NO PLANE DESCRIBED//)
    RETURN
20  XSTAT=PPL2(1)
    THETR=PPL2(2)*.01745329252
    XMACH=PPL2(3)
    Y=-Y

    THETR=PPL2(2)*.01745329252
    XMACH=PPL2(3)
    BETA=SQRT(XMACH**2-1.)
    ACOEF=1.
    B=-BETA*COS(THETR)
    C=-BETA*SIN(THETR)
    D=XSTAT
    PNT1(1)=XSTAT
    PNT1(2)=0.
    PNT1(3)=0.
    PNT2(2)=PNT3(3)=0.
    PNT2(3)=PNT3(2)=1.
    PNT2(1)=PNT1(1)-C
    PNT3(1)=PNT1(1)-B
30  CONTINUE
    PNT4(1)=PNT3(1)$PNT4(2)=PNT3(2)$PNT4(3)=PNT3(3)
C
C      COMPUTE VECTORS
C
    T1X=PNT3(1)-PNT1(1)$T1Y=PNT3(2)-PNT1(2)$T1Z=PNT3(3)-PNT1(3)
    T2X=PNT4(1)-PNT2(1)$T2Y=PNT4(2)-PNT2(2)$T2Z=PNT4(3)-PNT2(3)
    FNX=T2Y*T1Z-T1Y*T2Z
    FNY=T1X*T2Z-T2X*T1Z
    FNZ=T2X*T1Y-T1X*T2Y
    UN=SQRT(FNX*FNX+FNY*FNY+FNZ*FNZ)
    UNX=FNX/UN
    UNY=FNY/UN
    UNZ=FNZ/UN
    UT1=SQRT(T1X*T1X+T1Y*T1Y+T1Z*T1Z)
    UT1X=T1X/UT1
    UT1Y=T1Y/UT1
    UT1Z=T1Z/UT1
    UT2X=UNY*UT1Z-UNZ*UT1Y
    UT2Y=UNZ*UT1X-UNX*UT1Z
    UT2Z=UNX*UT1Y-UNY*UT1X
C
C      SETUP TRANSFORMATION MATRIX
C
    A(1,1)=UNX$A(1,2)=UNY$A(1,3)=UNZ
    A(2,1)=UT1X$A(2,2)=UT1Y$A(2,3)=UT1Z
    A(3,1)=UT2X$A(3,2)=UT2Y$A(3,3)=UT2Z
C
C      SET ORIGIN OF NEW COORD. SYSTEM
C
    XPRM(1)=A(1,1)*XB+A(1,2)*YB+A(1,3)*ZB
    XPRM(2)=A(2,1)*XB+A(2,2)*YB+A(2,3)*ZB
    XPRM(3)=A(3,1)*XB+A(3,2)*YB+A(3,3)*ZB
    HMIN=0.
    VMIN=0.
    WRITE (6,40) ACOEF,B,C,D

```

```

40  FORMAT (33H EQUATION OF THE PLANE AX+BY+CZ=D/3H A=E15.8,4X,2HB=,E1
    15.8,4X,2HC=,E15.8,4X,2HD=,E15.8)
C
C      BEGIN COMPUTING AND PLOTTING LINES OF INTERSECTION
C
    DO 80 ISI=1,ISIDE
    REWIND 7
    CALL RECIN (7,2,IC,ABC,1,8,1)
    CALL RECIN (7,1,IC,H1,H2,F3,H4,H5,H6,NOBJ)
    DO 70 J=1,NOBJ
    CALL RECIN (7,1,IC,NSURF,JJ,NAME(1),NAME(2),JJ,JJ)
    WRITE (6,50) NAME
50  FORMAT (1X2A10)
    DO 60 N=1,NSURF
    CALL RECIN (7,1,IC,ND1,NS1,J3,J4,J5)
    CALL PLANEX (ND1,NS1,ISI,ACDEF,B,C,D,HMIN,VMIN,A,SCALE,XPRM,NAME)
60  CONTINUE
70  CONTINUE
80  CONTINUE
    RETURN
C
C      END OF XCUT
C
    END

```



```

C
C      SOLVE FOR CUBIC IN W
C
DO 60 J4=1,4
GVEC(J4)=((U*GMAT(1,J4)+GMAT(2,J4))*U+GMAT(3,J4))*U+GMAT(4,J4)
60  CONTINUE
GVEC(4)=GVEC(4)-D
GUESS=W
IKODE=KUBSOL(GUESS,W,GVEC)
GO TO (130,70,70), IKODE

C
C      TRY U FOR w=1. ON OUTER BOUNDARY
C
70  W=1.
DO 90 I=1,4
GVEC(I)=0.
DO 80 J=1,4
80  GVEC(I)=GVEC(I)+GMAT(I,J)
90  CONTINUE
GVEC(4)=GVEC(4)-D
GUESS=1.
IKODE=KUBSOL(GUESS,U,GVEC)
GO TO (120,100,100), IKODE

C
C      TRY U FOR w=0. ON OUTER BOUNDARY
C
100 W=0.
DO 110 I=1,4
110 GVEC(I)=GMAT(I,4)
GVEC(4)=GVEC(4)-D
GUESS=1.
IKODE=KUBSOL(GUESS,U,GVEC)
GO TO (120,360,360), IKODE
120 CALL VSOLV (X,Y,Z,U,W,PATCH)
NPT=NPT+1
ALINE(NPT,1)=X$ALINE(NPT,2)=Y$ALINE(NPT,3)=Z
GO TO 360
130 CALL VSOLV (X,Y,Z,U,W,PATCH)
NPT=NPT+1
ALINE(NPT,1)=X$ALINE(NPT,2)=Y$ALINE(NPT,3)=Z
140 CONTINUE
GO TO 360

C
C      SOLVE FOR U WITH w=0.
C
150 W=0.
DO 160 I=1,4
160 GVEC(I)=GMAT(I,4)
GVEC(4)=GVEC(4)-D
GUESS=0.
IKODE=KUBSOL(GUESS,U,GVEC)
GO TO (170,250,250), IKODE
170 NPT=1
CALL VSOLV (X,Y,Z,U,W,PATCH)
ALINE(NPT,1)=X$ALINE(NPT,2)=Y$ALINE(NPT,3)=Z
DO 240 N=2,NNW
E=N-1
W=E*DW

```

```

C
C      SOLVE FOR CUBIC IN U
C
DO 180 J4=1,4
GVEC(J4)={(W*GMAT(J4,1)+GMAT(J4,2))*W+GMAT(J4,3))*W+GMAT(J4,4)
180 CONTINUE
GVEC(4)=GVEC(4)-D
GUESS=U
IKODE=KUBSOL(GUESS,U,GVEC)
GO TO (230,190,190), IKODE

C
C      TRY W FOR U=1. ON OUTER BOUNDARY
C
190 U=1.
DO 210 I=1,4
GVEC(I)=0.
DO 200 J=1,4
200 GVEC(I)=GVEC(I)+GMAT(J,I)
210 CONTINUE
GVEC(4)=GVEC(4)-D
GUESS=1.
IKODE=KUBSOL(GUESS,W,GVEC)
GO TO (220,360,360), IKODE
220 CALL VSOLV (X,Y,Z,U,W,PATCH)
NPT=NPT+1
ALINE(NPT,1)=X$ALINE(NPT,2)=Y$ALINE(NPT,3)=Z
GO TO 360
230 CALL VSOLV (X,Y,Z,U,W,PATCH)
NPT=NPT+1
ALINE(NPT,1)=X$ALINE(NPT,2)=Y$ALINE(NPT,3)=Z
240 CONTINUE
GO TO 360

C
C      SOLVE FOR U WITH W=1.
C
250 W=1.
DO 270 I=1,4
GVEC(I)=0.
DO 260 J=1,4
260 GVEC(I)=GVEC(I)+GMAT(I,J)
270 CONTINUE
GVEC(4)=GVEC(4)-D
GUESS=0.
IKODE=KUBSOL(GUESS,U,GVEC)
GO TO (280,370,370), IKODE
280 NPT=1
CALL VSOLV (X,Y,Z,U,W,PATCH)
ALINE(NPT,1)=X$ALINE(NPT,2)=Y$ALINE(NPT,3)=Z
DO 350 N=2,NNW
E=N-1
W=1.-E*DW

C
C      SOLVE FOR CUBIC IN U
C
DO 290 J4=1,4
GVEC(J4)={(W*GMAT(J4,1)+GMAT(J4,2))*W+GMAT(J4,3))*W+GMAT(J4,4)

```

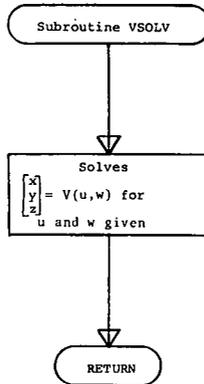
```

290  CONTINUE
      GVEC(4)=GVEC(4)-D
      GUESS=U
      IKODE=KUBSOL(GUESS,U,GVEC)
      GO TO (340,300,300), IKODE
C
C      TRY W FOR U=1. ON OUTER BOUNDARY
C
300  U=1.
      DO 320 I=1,4
      GVEC(I)=0.
      DO 310 J=1,4
310  GVEC(I)=GVEC(I)+GMAT(J,I)
320  CONTINUE
      GVEC(4)=GVEC(4)-D
      GUESS=1.
      IKODE=KUBSOL(GUESS,W,GVEC)
      GO TO (330,360,360), IKODE
330  CALL VSOLV (X,Y,Z,U,W,PATCH)
      NPT=NPT+1
      ALINE(NPT,1)=X$ALINE(NPT,2)=Y$ALINE(NPT,3)=Z
      GO TO 360
340  CALL VSOLV (X,Y,Z,U,W,PATCH)
      NPT=NPT+1
      ALINE(NPT,1)=X$ALINE(NPT,2)=Y$ALINE(NPT,3)=Z
350  CONTINUE
C
C      SCALE,PRINT AND PLOT
C
360  CONTINUE
      IF (NPT.LE.1) GO TO 370
      CALL PLTROT (NPT,A,ALINE,HMIN,VMIN,SCALE,IPRIN,XPRM,NAME)
370  CONTINUE
      RETURN
C
C      END OF PLANEX
C
      END

```

Subroutine VSOLV

Subroutine VSOLV evaluates a patch equation for x-, y-, and z-coordinates with u and w given. The flow chart and the FORTRAN statements for this subroutine are as follows:

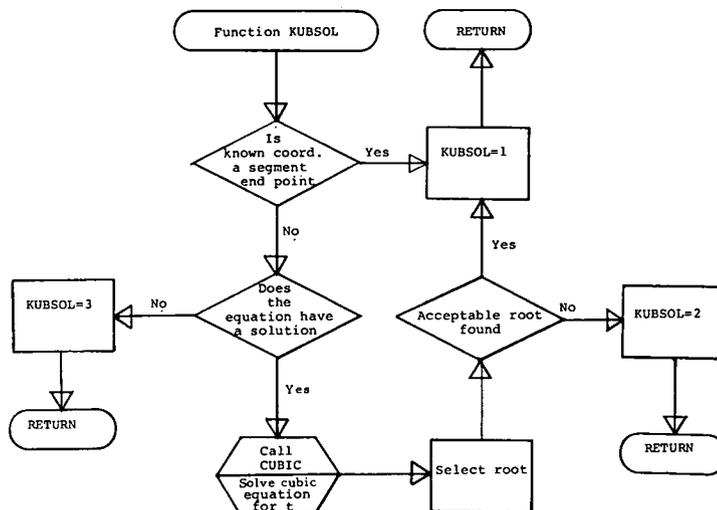


```

SUBROUTINE VSOLV (X,Y,Z,U,W,PATCH)
C
C     SOLVES FOR V(U,W) FROM PATCH EQUATION
C
C     DIMENSION VEC(4,3),PATCH(4,4,3),V(3)
C
    DO 10 J4=1,4
    DO 10 K3=1,3
    VEC(J4,K3)=((U*PATCH(1,J4,K3)+PATCH(2,J4,K3))*U+PATCH(3,J4,K3))*U+
1PATCH(4,J4,K3)
    10 CONTINUE
    DO 20 K3=1,3
    V(K3)=((W*VEC(1,K3)+VEC(2,K3))*W+VEC(3,K3))*W+VEC(4,K3)
    20 CONTINUE
    X=V(1) $ Y=V(2) $ Z=V(3)
    RETURN
    END
  
```

Function KUBSOL

Function KUBSOL selects the required real root from the roots of a cubic equation. The flow chart and the FORTRAN statements for this function are as follows:



FUNCTION KUBSOL(TL,T,COEFFS)

```

C
C   FINDS THE ROOTS OF A CUBIC AND SELECTS THE REQUIRED REAL
C   ROOT BETWEEN 0. AND 1. CLOSEST TO A GIVEN ESTIMATE
C
C   THE ROUTINE SETS
C   KUBSOL=1  SUCCESS
C   KUBSOL=2  NO ACCEPTABLE ROOT
C   KUBSOL=3  ERROR
C   TL IS ESTIMATE FOR SELECTION OF REQUIRED ROOT IF ALL ARE REAL
C   AND BETWEEN 0. AND 1.
C   T IS REQUIRED ROOT WITH KUBSOL=1
C   COEFFS(1) ARE THE COEFFICIENTS AT**3+BT**2+CT+D=0.
C
C   DIMENSION COEFFS(4)
C   COMPLEX ROOTS(3),FTEM(8)
C   DATA EPS/1.E-6/,EPI/1.E-5/
C
C   CHECK FOR GIVEN VARIABLE ON SEGMENT END POINTS
C
C   T=0.
C   IF (ABS(COEFFS(4)).LE.EPS) GO TO 90
C   T=1.
C   CCC=COEFFS(1)+COEFFS(2)+COEFFS(3)+COEFFS(4)
C   IF (ABS(CCC).LE.EPS) GO TO 90
  
```

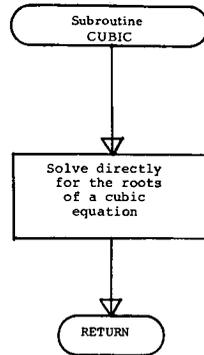
```

C
C      SOLVE CUBIC EQUATION FOR T
C
IF (ABS(COEFFS(1)).GT.EP1) GO TO 40
IF (ABS(COEFFS(2)).GT.EP1) GO TO 30
IF (ABS(COEFFS(3)).GT.EP1) GO TO 20
10  KUBSOL=3
    RETURN
20  T=-COEFFS(4)/COEFFS(3)
    ROOTS(1)=ROOTS(2)=ROOTS(3)=T
    IF (T.LT.0..OR.T.GT.1.) GO TO 100
    GO TO 90
30  TEMP=COEFFS(3)**2-4.*COEFFS(2)*COEFFS(4)
    IF (TEMP.LT.0.) GO TO 10
    TMP=SQRT(TEMP)
    ROOTS(1)=ROOTS(2)=(-COEFFS(3)+TMP)/(2.*COEFFS(2))
    ROOTS(3)=(-COEFFS(3)-TMP)/(2.*COEFFS(2))
    GO TO 50
40  CONTINUE
    CALL CUBIC (COEFFS,ROOTS)
C
C      SELECT DESIRED ROOT
C
TT=REAL(ROOTS(1))
T=TT
IF (AIMAG(ROOTS(1)).EQ.0..AND.TT.GE.0..AND.TT.LE.1.) GO TO 60
50  CONTINUE
    TT=REAL(ROOTS(2))
    T=TT
    IF (AIMAG(ROOTS(2)).EQ.0..AND.TT.GE.0..AND.TT.LE.1.) GO TO 80
    TT=REAL(ROOTS(3))
    T=TT
    IF (AIMAG(ROOTS(3)).EQ.0..AND.TT.GE.0..AND.TT.LE.1.) GO TO 90
60  GO TO 100
    IF (AIMAG(ROOTS(2)).NE.0.) GO TO 90
    TT=REAL(ROOTS(2))
    IF (TT.LT.0..OR.TT.GT.1.) GO TO 80
    PRINT 70, T,TT,TL,COEFFS,ROOTS
70  FORMAT (/ /40H TWO ACCEPTABLE ROOTS FOUND, ROOTS ARE ,2E17.8/34H E
1STIMATE FOR SELECTION OF ROOTS ,E17.8/15H COEFFICIENTS =,4E17.8/8
2H ROOTS =,6E17.8//)
    IF (ABS(TL-TT).LT.ABS(TL-T)) T=TT
    IF (AIMAG(ROOTS(3)).NE.0.) GO TO 90
    TT=REAL(ROOTS(3))
    IF (TT.LT.0..OR.TT.GT.1.) GO TO 90
    PRINT 70, T,TT,TL,COEFFS,ROOTS
    IF (ABS(TL-TT).LT.ABS(TL-T)) T=TT
90  CONTINUE
    KUBSOL=1
    RETURN
100 CONTINUE
    KUBSOL=2
    RETURN
    END

```

Subroutine CUBIC

Subroutine CUBIC uses the direct solution for the roots of the cubic equation:
 $AX^3 + BX^2 + CX + D = 0$. The flow chart and the FORTRAN statements for this subroutine are as follows:



```

SUBROUTINE CUBIC (A,X)
C
C
C      PROGRAMMER  HSING-SHIH, CHANG
C
C      COMPLEX X
C      DIMENSION X(3)
C      DIMENSION A(4),XR(3), XI(3),AQ(3)
C
C      SOLVE THE CUBIC EQUATION F(X)=0
C
C      F(X)=A(1)*X**3+A(2)*X**2+A(3)*X+A(4)
C
C      QUADRATODN F(X)=0
C
C      F(X)=AQ(1)*X**2+AQ(2)*X+AQ(3)
C
C      F(X)=X**2+B2*X+B3
C      IPATH=2
C      EX=1./3.
C      IF (A(4)) 20,10,20
10     XR(1)=0.
C      GO TO 150
20     A2=A(1)*A(1)
C      Q=(27.*A2*A(4)-9.*A(1)*A(2)*A(3)+2.*A(2)**3)/(54.*A2*A(1))
C      IF (Q) 40,30,50
30     Z=0.
C      GO TO 140
40     Q=-Q
C      IPATH=1
50     P=(3.*A(1)*A(3)-A(2)*A(2))/(9.*A2)
C      ARG=P*P*P+Q*Q
  
```

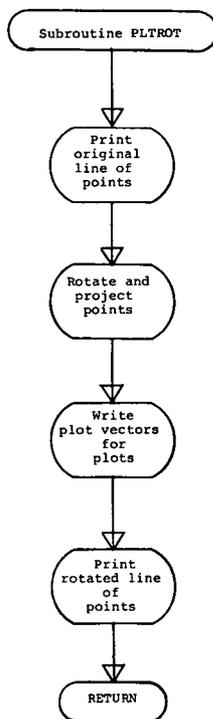
```

        IF (ARG) 60,70,80
60      Z=-2.*SQRT(-P)*CUS(ATAN(SQRT(-ARG)/Q)/3.)
        GO TO 120
70      Z=-2.*Q**EX
        GO TO 120
80      SARG=SQRT(ARG)
        IF (P) 90,100,110
90      Z=-(Q+SARG)**EX-(Q-SARG)**EX
        GO TO 120
100     Z=-(2.*Q)**EX
        GO TO 120
110     Z=(SARG-Q)**EX-(SARG+Q)**EX
120     GO TO (130,140), IPATH
130     Z=-Z
140     XR(1)=(3.*A(1)*Z-A(2))/(3.*A(1))
150     AQ(1)=A(1)
        AQ(2)=A(2)+XR(1)*A(1)
        AQ(3)=A(3)+XR(1)*AQ(2)
C
        B2=AQ(2)/AQ(1)
        B3=AQ(3)/AQ(1)
        X1=-B2/2.
        DISC=X1*X1-B3
160     IF (DISC.LT.0.0) 160,170
        X2=SQRT(-DISC)
        XR(2)=X1
        XR(3)=X1
        XI(2)=X2
        GO TO 200
170     IF (DISC.EQ.0.0) 180,190
180     X2=0.
        XR(2)=X1+X2
        XR(3)=X1-X2
        XI(2)=0.
        GO TO 200
190     X2=SQRT(DISC)
        XR(2)=X1+X2
        XR(3)=X1-X2
        XI(2)=0.
200     XI(1)=0.
        XI(3)=-XI(2)
        X(1)=CMPLX(XR(1),XI(1))
        X(2)=CMPLX(XR(2),XI(2))
        X(3)=CMPLX(XR(3),XI(3))
        RETURN
        END

```

Subroutine PLTROT

Subroutine PLTROT rotates and translates points defining a cross section, generates plot instructions, and prints the points. The flow chart and the FORTRAN statements for this subroutine are as follows:



```

SUBROUTINE PLTROT (NPT,A,ALINE,HMIN,VMIN,SCALE,IPRIN,XP,NAME)
C
C     ROTATES A SET OF 3D POINTS INTO A SPECIFIED PLANE
C     AND GENERATES A CALCGMP PLOT TAPE
C
DIMENSION A(3,3),ALINE(52,3),RLINE(54,3)
DIMENSION XP(3),NAME(2)
DATA EPS/.00000001/
C
N=1
10  N=N+1
    T1=ABS(ALINE(N-1,1)-ALINE(N,1))
    T2=ABS(ALINE(N-1,2)-ALINE(N,2))
    T3=ABS(ALINE(N-1,3)-ALINE(N,3))
    IF (.NOT.(T1.LE.EPS.AND.T2.LE.EPS.AND.T3.LE.EPS)) GO TO 30
    DO 20 NK=N,NPT
    DO 20 N3=1,3
20  ALINE(NK-1,N3)=ALINE(NK,N3)
    NPT=NPT-1
    N=N-1
  
```

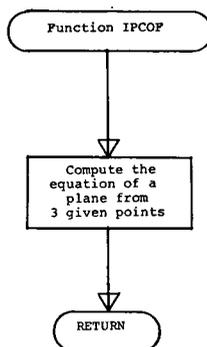
```

30  IF (N.NE.NPT) GO TO 10
    IF (NPT.LE.1) RETURN
    GO TO (70,40,70,40), IPRIN
40  CONTINUE
    DO 50 N=1,NPT
    DO 50 N3=1,3
50  RLINE(N,N3)=ALINE(N,N3)/SCALE
    WRITE (6,60) ((ALINE(I,J),J=1,3),(RLINE(I,J),J=1,3),I=1,NPT)
60  FORMAT (//44X,37HCOORDINATES OF POINTS OF INTERSECTION/27X,8HORIGI
    1NAL52X,6HSCALED//7X,1HX19X,1HY19X,1HZ19X,1HX19X,1HY19X,1HZ/(6E20.8
    2))
70  CONTINUE
    DO 100 N=1,NPT
    RLINE(N,1)=0.
    RLINE(N,2)=0.
    RLINE(N,3)=0.
    DO 90 I=1,3
    DO 80 J=1,3
80  RLINE(N,I)=RLINE(N,I)+A(I,J)*ALINE(N,J)
90  RLINE(N,I)=RLINE(N,I)-XP(I)
100 CONTINUE
    RLINE(NPT+1,2)=HMIN
    RLINE(NPT+1,3)=VMIN
    RLINE(NPT+2,2)=SCALE
    RLINE(NPT+2,3)=SCALE
    CALL LINE (RLINE(1,2),RLINE(1,3),NPT,1,0,0,0)
    GO TO (150,150,110,110), IPRIN
110 CONTINUE
    DO 130 N=1,NPT
    DO 120 N3=1,3
120 ALINE(N,N3)=RLINE(N,N3)/SCALE
130 CONTINUE
    WRITE (6,140) ((RLINE(I,J),J=1,3),(ALINE(I,J),J=1,3),I=1,NPT)
140 FORMAT (//33X,59HCOORDINATES OF POINTS OF INTERSECTION ROTATED INT
    10 YZ PLANE/27X,8HORIGINAL52X,6HSCALED//7X,1HX19X,1HY19X,1HZ19X,1HX
    219X,1HY19X,1HZ/(6E20.8))
150 CONTINUE
    RETURN
C
C      END OF PLTRUT
C
    END

```

Function IPCOF

Function IPCOF finds the coefficients of a plane from three given points. The flow chart and the FORTRAN statements for this function are as follows:



```

FUNCTION IPCOF (A,B,C,D,R1,P2,P3)
DIMENSION P1(3),P2(3),P3(3),AMAT(3,3),BMAT(3),IPIVOT(3)
C
C     FINDS THE COEFFICIENTS OF A PLANE IN THE
C     FORM AX+BY+CZ=D
C
DATA EPS/1.E-8/
C
D=1.
DO 50 I=1,4
DO 10 N3=1,3
AMAT(1,N3)=P1(N3)
AMAT(2,N3)=P2(N3)
AMAT(3,N3)=P3(N3)
10 BMAT(N3)=1.
II=I-1
IF (II.EQ.0) GO TO 30
DO 20 N3=1,3
BMAT(N3)=-AMAT(N3,II)
AMAT(N3,II)=-1.
20 CONTINUE
30 CONTINUE
CALL SIMEQ (AMAT,3,BMAT,1,DET,IPIVOT,3,ISCALE)
IF (ABS(DET).LE.EPS) GO TO 50
IF (I.EQ.1) GO TO 40
D=BMAT(II)
BMAT(II)=1.
40 A=BMAT(1)
B=BMAT(2)
C=BMAT(3)
IPCOF=1
RETURN
50 CONTINUE
IPCOF=2
RETURN
C
C     END OF IPCOF
C
END
  
```

Langley Library Subroutine SIMEQ

Language: FORTRAN

Purpose: SIMEQ solves the matrix equation $AX = B$ where A is a square coefficient matrix and B is a matrix of constant vectors. The solution to a set of simultaneous equations and the determinant may be obtained. If the user wants the determinant only, use DETEV for savings in time and storage.

Use: CALL SIMEQ (A, N, B, M, DETERM, IPIVOT, NMAX, ISCALE)

- A A two-dimensional array of the coefficients.
- N The order of A; $1 \leq N \leq NMAX$.
- B A two-dimensional array of the constant vectors B. On return to calling program, X is stored in B.
- M The number of column vectors in B.
- DETERM Gives the value of the determinant by the following formula:
$$DET(A) = (10^{100})^{ISCALE} (DETERM)$$
- IPIVOT A one-dimensional array of temporary storage used by the routine.
- NMAX The maximum order of A as stated in dimension statement of calling program.
- ISCALE A scale factor computed by subroutine to keep results of computation within the floating-point word size of the computer.

Restrictions: Arrays A, B, and IPIVOT are dimensioned with variable dimensions in the subroutine. The maximum size of these arrays must be specified in a DIMENSION statement of the calling program as: A (NMAX, NMAX), B (NMAX, M), IPIVOT (NMAX). The original matrices, A and B, are destroyed. They must be saved by the user if there is further need for them. The determinant is set to zero for a singular matrix.

Method: Jordan's method is used through a succession of elementary transformations: l_n, l_{n-1}, \dots, l_1 . If these transformations are applied to a matrix B of constant vectors, the result is X where $AX = B$. Each transformation is selected so that the largest element is used in the pivotal position.

Accuracy: Total pivotal strategy is used to minimize the rounding errors; however, the accuracy of the final results depends upon how well-conditioned the original matrix is.

Reference: (a) Fox, L.: An Introduction to Numerical Linear Algebra. Oxford Univ. Press, c.1965.

Storage: 4328 locations.

Subroutine date: August 1, 1968.

The FORTRAN statements for this subroutine are as follows:

```

SUBROUTINE SIMEQ (A,N,B,M,DETERM,IPIVOT,NMAX,ISCALE)
C SOLUTION OF SIMULTANEOUS LINEAR EQUATIONS
C *** DOCUMENT DATE 08-01-68 SUBROUTINE REVISED 08-01-68 *****
C
C DIMENSION IPIVOT(N),A(NMAX,N),B(NMAX,M)
C EQUIVALENCE (IROW,JROW),(ICOLUM,JCOLUM),(AMAX,T,SWAP)
C
C INITIALIZATION
C
10 ISCALE=0
R1=10.0**100
R2=1.0/R1
DETERM=1.0
DO 20 J=1,N
20 IPIVOT(J)=0
DO 380 I=1,N
C
C SEARCH FOR PIVOT ELEMENT
C
C AMAX=0.0
DO 70 J=1,N
IF (IPIVOT(J)-1) 30,70,30
30 DO 60 K=1,N
IF (IPIVOT(K)-1) 40,60,390
40 IF (ABS(AMAX)-ABS(A(J,K))) 50,60,60
50 IROW=J
ICOLUM=K
AMAX=A(J,K)
60 CONTINUE
70 CONTINUE
IF (AMAX) 90,80,90
80 DETERM=0.0
ISCALE=0
GO TO 390
90 IPIVOT(ICOLUM)=IPIVOT(ICOLUM)+1
C
C INTERCHANGE ROWS TO PUT PIVOT ELEMENT ON DIAGONAL
C
IF (IROW-ICOLUM) 100,140,100
100 DETERM=-DETERM
DO 110 L=1,N
SWAP=A(IROW,L)
A(IROW,L)=A(ICOLUM,L)
110 A(ICOLUM,L)=SWAP
IF (M) 140,140,120
120 DO 130 L=1,M
SWAP=B(IROW,L)
B(IROW,L)=B(ICOLUM,L)
130 B(ICOLUM,L)=SWAP
140 PIVOT=A(ICOLUM,ICOLUM)
IF (PIVOT) 150,80,150
C
C SCALE THE DETERMINANT
C
150 PIVOTI=PIVOT
IF (ABS(DETERM)-R1) 180,160,160
```

```

160 DETERM=DETERM/R1
    ISCALE=ISCALE+1
    IF (ABS(DETERM)-R1) 210,170,170
170 DETERM=DETERM/R1
    ISCALE=ISCALE+1
    GO TO 210
180 IF (ABS(DETERM)-R2) 190,190,210
190 DETERM=DETERM*R1
    ISCALE=ISCALE-1
    IF (ABS(DETERM)-R2) 200,200,210
200 DETERM=DETERM*R1
    ISCALE=ISCALE-1
210 IF (ABS(PIVOTI)-R1) 240,220,220
220 PIVOTI=PIVOTI/R1
    ISCALE=ISCALE+1
    IF (ABS(PIVOTI)-R1) 270,230,230
230 PIVOTI=PIVOTI/R1
    ISCALE=ISCALE+1
    GO TO 270
240 IF (ABS(PIVOTI)-R2) 250,250,270
250 PIVOTI=PIVOTI*K1
    ISCALE=ISCALE-1
    IF (ABS(PIVOTI)-R2) 260,260,270
260 PIVOTI=PIVOTI*R1
    ISCALE=ISCALE-1
270 DETERM=DETERM*PIVOTI
C
C   DIVIDE PIVOT ROW BY PIVOT ELEMENT
C
    DO 290 L=1,N
    IF (IPIVOT(L)-1) 280,290,390
280 A(ICOLUM,L)=A(ICOLUM,L)/PIVOT
290 CONTINUE
    IF (M) 320,320,300
300 DO 310 L=1,M
310 B(ICOLUM,L)=B(ICOLUM,L)/PIVOT
C
C   REDUCE NON-PIVOT ROWS
C
320 DO 380 LI=1,N
    IF (LI-ICOLUM) 330,380,330
330 T=A(LI,ICOLUM)
    DO 350 L=1,N
    IF (IPIVOT(L)-1) 340,350,390
340 A(LI,L)=A(LI,L)-A(ICOLUM,L)*T
350 CONTINUE
    IF (M) 380,380,360
360 DO 370 L=1,M
370 B(LI,L)=B(LI,L)-B(ICOLUM,L)*T
380 CONTINUE
390 RETURN
    END

```

PROGRAM USE

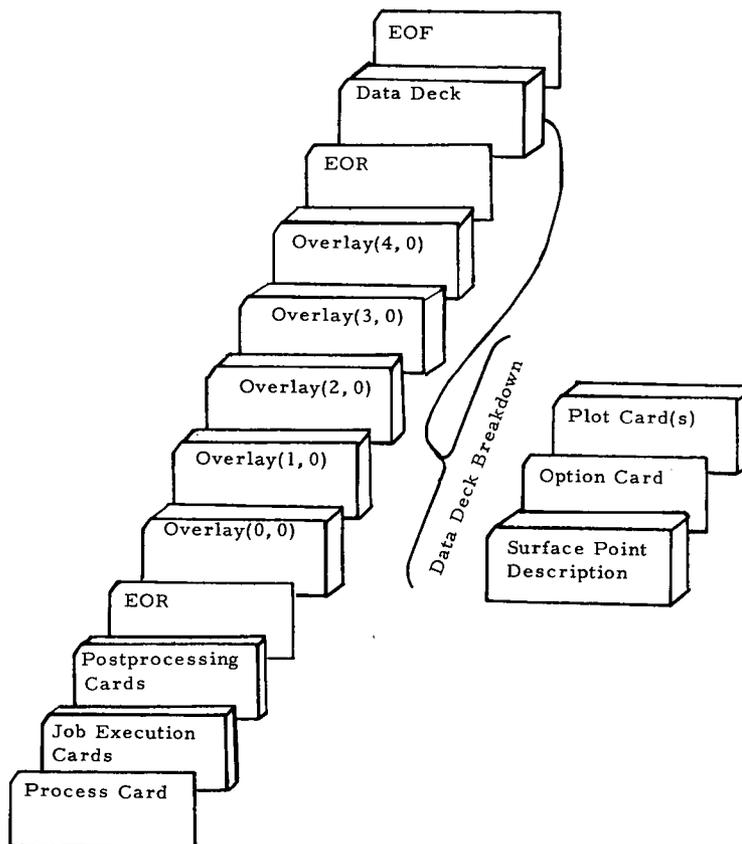
PROGRAM IDENTIFICATION

This program is for fitting smooth surfaces to the component parts of an aircraft configuration using a three-dimensional modeling technique called Coon's patches (ref. 1). It is identified as program D3400.

PROGRAM SETUP FOR A COMPILE AND EXECUTE

This section describes the input data requirements, limitations, and the punched card formats. The program will end normally if there are no input cards at the beginning of a READ sequence.

The input data cards are assembled with the program decks in the order illustrated in sketch (d).



Sketch (d)

DESCRIPTION OF INPUT DATA CARDS

Configuration

The form for the airplane configuration input has become known throughout the aircraft industry as the Harris Wave Drag geometry input and is identical to that described in reference 3.

Since the airplane has to be symmetrical about the XZ-plane, only half of the airplane need be described to the computer. The convention used in presenting the input data is that the half of the airplane on the positive Y-side of the XZ-plane is presented. The program then uses this information to construct the complete airplane if required. The number of input cards depends on the number of components used to describe the configuration and the amount of detail used to describe each component. It is not possible to change only part of a configuration in a succeeding case. The complete configuration must be input each time. The method of input is by FORTRAN "READ" statements.

Card 1 – Identification. - Card 1 contains any desired identifying information in columns 1 to 80.

Card 2 – Control integers. - Card 2 contains 24 integers, each punched right-justified in a 3-column field. Columns 73 to 80 may be used in any desired manner. An identification of the card columns, the name used by the source program, and a description of each integer are given in the following table:

<u>Columns</u>	<u>FORTTRAN name</u>	<u>Description</u>
01 to 03	J0	If J0 = 0, no reference area If J0 = 1, reference area to be read
04 to 06	J1	If J1 = 0, no wing data If J1 = 1, cambered wing data to be read If J1 = -1, uncambered wing data to be read
07 to 09	J2	If J2 = 0, no fuselage data If J2 = 1, data for arbitrarily shaped fuselage to be read If J2 = -1, data for circular fuselage to be read (with J6 = 0, fuselage will be cambered; with J6 = -1, fuselage will be symmetrical with XY-plane; with J6 = 1, entire configuration will be symmetrical with XY-plane)

<u>Columns</u>	<u>FORTTRAN name</u>	<u>Description</u>
10 to 12	J3	If J3 = 0, no pod data If J3 = 1, pod data to be read
13 to 15	J4	If J4 = 0, no fin data If J4 = 1, fin data to be read
16 to 18	J5	If J5 = 0, no canard data If J5 = 1, canard data to be read
19 to 21	J6	Simplification code: If J6 = 0, indicates a cambered circular or arbitrary fuselage if $J2 \neq 0$ If J6 = 1, complete configuration is symmetrical with respect to XY-plane, which implies uncambered circular fuselage if there is a fuselage If J6 = -1, indicates uncambered circular fuselage with $J2 \neq 0$
22 to 24	NWAF	Number of airfoil sections used to describe the wing; $4 \leq NWAF \leq 20$
25 to 27	NWAFOR	Number of ordinates used to define each wing airfoil section; $4 \leq NWAFOR \leq 30$
28 to 30	NFUS	Number of fuselage segments; $1 \leq NFUS \leq 4$
31 to 33	NRADX(1)	Number of points used to represent half-section of first fuselage segment; if fuselage is circular, the program computes indicated number of y- and z-ordinates; $4 \leq NRADX(1) \leq 30$
34 to 36	NFORX(1)	Number of stations for first fuselage segment; $4 \leq NFORX(1) \leq 30$
37 to 39	NRADX(2)	Same as NRADX(1) and NFORX(1), but for second fuselage segment
40 to 42	NFORX(2)	
43 to 45	NRADX(3)	Same as NRADX(1) and NFORX(1), but for third fuselage segment
46 to 48	NFORX(3)	
49 to 51	NRADX(4)	Same as NRADX(1) and NFORX(1), but for fourth fuselage segment
52 to 54	NFORX(4)	

<u>Columns</u>	<u>FORTTRAN name</u>	<u>Description</u>
55 to 57	NP	Number of pods described; $NP \leq 9$
58 to 60	NPODOR	Number of stations at which pod radii are to be specified; $4 \leq NPODOR \leq 30$
61 to 63	NF	Number of fins (vertical tails) described; $NF \leq 6$
64 to 66	NFINOR	Number of ordinates used to define each fin airfoil section; $4 \leq NFINOR \leq 10$
67 to 69	NCAN	Number of canards (horizontal tails) described; $NCAN \leq 2$
70 to 72	NCANOR	Number of ordinates used to define each canard airfoil section; $4 \leq NCANOR \leq 10$; if NCANOR is given a negative sign, the program will expect to read lower ordinates also; otherwise, airfoil is assumed to be symmetrical

Cards 3, 4, . . . - remaining data input cards. - The remaining data input cards contain a detailed description of each component of the airplane. Each card contains up to 10 values, each value punched in a 7-column field with a decimal and may be identified in columns 73 to 80. The cards are arranged in the following order: reference area, wing data cards, fuselage data cards, pod (or nacelle) data cards, fin (vertical tail) data cards, and canard (or horizontal tail) data cards.

Reference area card: The reference area value is punched in columns 1 to 7 and may be identified as REFA in columns 73 to 80. This value is not used by the program but may be present in an already existing input deck.

Wing data cards: The first wing data card (or cards) contains the locations in percent chord at which the ordinates of all the wing airfoils are to be specified. There will be exactly NWAFFOR locations in percent chord given. Each card may be identified in columns 73 to 80 by the symbol XAFj where j denotes the number of the last location in percent chord given on that card. For example, if NWAFFOR = 16, there are 16 ordinates to be specified for every airfoil, and two data cards will be required. The first XAF card is identified as XAF 10 and the second as XAF 16.

The next wing data cards (there will be NWAFF cards) each contain four numbers which give the origin and chord length of each of the wing airfoils that is to be specified. The cards representing the most inboard airfoil are given first, followed by the cards for successive airfoils. The information is arranged on each card as follows:

<u>Columns</u>	<u>Description</u>
1 to 7	x-ordinate of airfoil leading edge
8 to 14	y-ordinate of airfoil leading edge
15 to 21	z-ordinate of airfoil leading edge
22 to 28	Airfoil streamwise chord length
73 to 80	Card identification, WAFORGj where j denotes the particular airfoil; for example, WAFORG1 denotes first (most inboard) airfoil

If a cambered wing has been specified, the next set of wing data cards is the mean camber line (TZORD) cards. The first card contains up to 10 Δz values, referenced to the z-ordinate of the airfoil leading edge, at each of the specified percents of chord for the first airfoil. If more than 10 values are to be specified for each airfoil (there will be NWAFOR values), the remaining values are continued on successive cards. The remaining airfoils are described in the same manner, data for each airfoil starting on a new card, and the cards arranged in the order which begins with the most inboard airfoil and proceeds to the outboard. Each card may be identified in columns 73 to 80 as TZORDj, where j denotes the particular airfoil.

Next are the wing airfoil ordinate (WAFORD) cards. The first card contains up to 10 half-thickness ordinates of the first airfoil expressed as percent chord. If more than 10 ordinates are to be specified for each airfoil (there will be NWAFOR values), the remaining ordinates are continued on successive cards. The remaining airfoils are each described in the same manner, and the cards are arranged in the order which begins with the most inboard airfoil and proceeds to the outboard. Each card may be identified in columns 73 to 80 as WAFORDj, where j denotes the particular airfoil.

Fuselage data cards: The first card (or cards) specifies the x-values of the fuselage stations of the first segment. There will be NFORX(1) values and the cards may be identified in columns 73 to 80 by the symbol XFUSj where j denotes the number of the last fuselage station given on that card.

If the fuselage is circular and cambered, the next set of cards specifies the z-locations of the center of the circular sections. There will be NFORX(1) values and the cards may be identified in columns 73 to 80 by the symbol ZFUSj where j denotes the number of the last fuselage station given on that card.

If the fuselage is circular, the next card (or cards) gives the fuselage cross-sectional areas, and may be identified in columns 73 to 80 by the symbol FUSARDj where j denotes the number of the last fuselage station given on that card. If the fuselage is of

arbitrary shape, the y-ordinates for a half-section are given (NRADX(1) values) and identified in columns 73 to 80 as Y_i where i is the station number. Following these are the corresponding z-ordinates (NRADX(1) values) for the half-section identified in columns 73 to 80 as Z_i where i is the station number. Each station will have a set of Y and Z cards, and the convention of ordering the ordinates from bottom to top is observed.

For each fuselage segment a new set of cards as described must be provided. The segment descriptions should be given in order of increasing values of x .

Pod data cards: The first pod or nacelle data card specifies the location of the origin of the first pod. The information is arranged on the card as follows:

<u>Columns</u>	<u>Description</u>
1 to 7	x-ordinate of origin of first pod
8 to 14	y-ordinate of origin of first pod
15 to 21	z-ordinate of origin of first pod
73 to 80	Card identification, PODORG j where j denotes pod number

The next pod input data card (or cards) contains the x-ordinates, referenced to the pod origin, at which the pod radii (there will be NPODOR of them) are to be specified. The first x-value must be zero, and the last x-value is the length of the pod. These cards may be identified in columns 73 to 80 by the symbol XPOD j where j denotes the pod number. For example, XPOD1 represents the first pod.

The next pod input data cards give the pod radii corresponding to the pod stations that have been specified. These cards may be identified in columns 73 to 80 as PODR j where j denotes the pod number.

For each additional pod, new PODORG, XPOD, and PODR cards must be provided. Only single pods are described but the program assumes that if the y-ordinate is not zero an exact duplicate is located symmetrically with respect to the XZ-plane; a y-ordinate of zero implies a single pod.

Fin data cards: Exactly three data input cards are used to describe a fin. The information presented on the first fin data input card is as follows:

<u>Columns</u>	<u>Description</u>
1 to 7	x-ordinate of lower airfoil leading edge
8 to 14	y-ordinate of lower airfoil leading edge
15 to 21	z-ordinate of lower airfoil leading edge

<u>Columns</u>	<u>Description</u>
22 to 28	Chord length of lower airfoil
29 to 35	x-ordinate of upper airfoil leading edge
36 to 42	y-ordinate of upper airfoil leading edge
43 to 49	z-ordinate of upper airfoil leading edge
50 to 56	Chord length of upper airfoil
73 to 80	Card identification, FINORGj where j denotes fin number

The second fin data input card contains up to 10 locations in percent chord (exactly NFINOR of them) at which the fin airfoil ordinates are to be specified. The card may be identified in columns 73 to 80 as XFINj where j denotes the fin number.

The third fin data input card contains the fin airfoil half-thickness ordinates expressed in percent chord. Since the fin airfoil must be symmetrical, only the ordinates on the positive y-side of the fin chord plane are specified. The card identification, FINORDj, may be given in columns 73 to 80, where j denotes the fin number.

For each fin, new FINORG, XFIN, and FINORD cards must be provided.

Only single fins are described but the program assumes that if the y-ordinate is not zero an exact duplicate is located symmetrically with respect to the XZ-plane; a y-ordinate of zero implies a single fin.

Canard data cards: If the canard (or horizontal tail) airfoil is symmetrical, exactly three cards are used to describe a canard, and the input is given in the same manner as for the fin. If, however, the canard airfoil is not symmetrical (indicated by a negative value of NCANOR), a fourth canard data input card will be required to give the lower ordinates. The information presented on the first canard data input card is as follows:

<u>Columns</u>	<u>Description</u>
1 to 7	x-ordinate of inboard airfoil leading edge
8 to 14	y-ordinate of inboard airfoil leading edge
15 to 21	z-ordinate of inboard airfoil leading edge
22 to 28	Chord length of inboard airfoil
29 to 35	x-ordinate of outboard airfoil leading edge
36 to 42	y-ordinate of outboard airfoil leading edge
43 to 49	z-ordinate of outboard airfoil leading edge

<u>Columns</u>	<u>Description</u>
50 to 56	Chord length of outboard airfoil
73 to 80	Card identification, CANORGj where j denotes the canard number

The second canard data input card contains up to 10 locations in percent chord (exactly NCANOR of them) at which the canard airfoil ordinates are to be specified. The card may be identified in columns 73 to 80 as XCANj where j denotes the canard number.

The third canard data input card contains the upper half-thickness ordinates, expressed in percent chord, of the canard airfoil. This card may be identified in columns 73 to 80 as CANORDj where j denotes the canard number. If the canard airfoil is not symmetrical, the lower ordinates are presented on a second CANORD card. The program expects both upper and lower ordinates to be punched as positive values in percent chord.

For another canard, new CANORG, XCAN, and CANORD cards must be provided.

Alternate Surface-Description Input

The surface-description method used in this report is not restricted to any particular shape. An airplane configuration was chosen for the current application because of its complexity and an anticipated need. The program input is best thought of as a set of points describing a surface or surfaces.

To use the program for a different input form, the user may substitute another overlay (1,0) for preprocessing input data in the proper form to be used by the program. If desired to print this input data, provisions to do so should be provided for in overlay (1,0).

Overlay (1,0) must:

1. Store in labeled COMMON

COMMON/PATPLT/XMIN, XMAX, YMIN, YMAX, ZMIN, ZMAX, NOBJ

The minimums and maximums define a box in which the shape to be plotted orthographically will fit. These values are not used for the cross-section plots, but space must be allowed so that NOBJ will occupy the correct position.

NOBJ is the number of objects (or components) each made up of a number of surfaces, all of which could form a body.

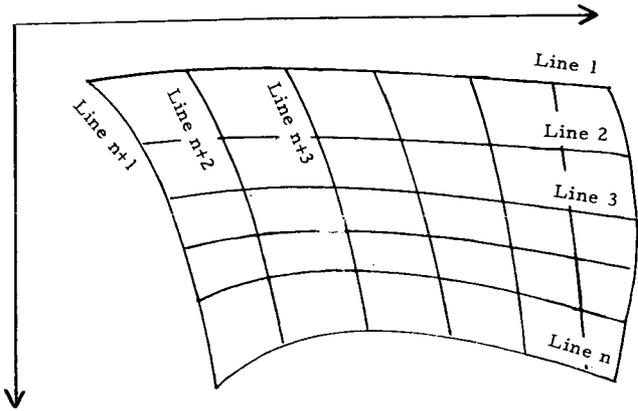
2. Write binary tape 10 in the following format. FORTRAN names from the given program are used for illustration.

<u>Record</u>	<u>Name</u>	<u>Purpose</u>
1	ABC(8)	Identification
2	(For NOBJ ₁)	
	NSURF	Number of surfaces in object
	M1	Not used
	M2(2)	Name of object (for printing only)
	M3	Not used
	M4	Not used
	3	(For NSURF ₁)
NCOL		Number of columns of grid points, ≤ 31
NROW		Number of rows of grid points, ≤ 31
N3		Not used
N4		Not used
N5		Not used
4	((ALINE(N,N3), N=1, NCOL), N3=1,3)	NROW lines of NCOL points (x,y,z)
5	((ALINE(N,N3), N=1, NROW), N3=1,3)	NCOL lines of NROW points (x,y,z)
6	(Repeat records 3, 4, and 5 for the number of surfaces given in record 2)	
.		
.		
.		
	(Repeat record 2 for each NOBJ as given in labeled COMMON PATPLT and repeat records 3, 4, and 5 as required.)	

(Although the dummy variables are not used at the present time, they must be written on tape.)

Great care must be taken to describe the grid of input points in exactly the manner specified so that in a collection of surfaces the outward normal vectors will be consistent. For the current application, the rectangular grid of values (not necessarily rectangular in shape) does not require any specific corner as the starting place. However, points must

be given as lines in a rowwise direction then as lines in a columnwise direction as illustrated in sketch (e)



Sketch (e)

3. If it is desired to increase the number of points in the rows and/or columns and it is not feasible to break a surface down into more than one surface, increase all dimensions of 31 to the maximum of NCOL or NROW in:

- (a) Overlay (1,0), program START
- (b) Overlay (2,0), subroutine PACH. Also in subroutine PACH, change the dimensions of the SLOPE array to $SLOPE(NCOL_{max}, NROW_{max}, 3)$ and change MAXN in the data statement to the largest of $NCOL_{max}$ or $NROW_{max}$.

Option Card

The option card indicates to the program the next kind of input to be read.

<u>Column</u>	<u>FORTTRAN name</u>	<u>Description</u>
4	ITYPE	<p>If ITYPE = 1, Read orthographic-projection plot card</p> <p>If ITYPE = 2, Read cross-section plot card</p> <p>If ITYPE = 3, Read another set of geometry cards</p>

Plot Cards

A single card contains all the necessary information for one plot. The available options and the necessary input for each are described in the following sections.

Orthographic projections (ITYPE = 1). - For one orthographic projection, the card should be set up as follows:

<u>Columns</u>	<u>FORTTRAN name</u>	<u>Description</u>
1	HORZ	"X", "Y", or "Z" for horizontal axis
3	VERT	"X", "Y", or "Z" for vertical axis
5 to 7	TEST1	Word "OUT" for deletion of hidden lines; otherwise, leave blank
8 to 12	PHI	Roll angle, degrees
13 to 17	THETA	Pitch angle, degrees
18 to 22	PSI	Yaw angle, degrees
48 to 52	PLOTSZ	Plot frame size (scale factor is computed by using PLOTSZ and maximum dimension of configuration, i.e., the maximum dimension, usually the body length, will be scaled to exactly PLOTSZ)
53 to 55	TYPE	Word "ORT"
56 to 58	NOU	Number of lines, originating on the $w = 0.0$ boundary, computed within each patch for enriching the surface grid in the w-direction, $NOU \leq 50$
59 to 61	NOW	Number of lines, originating on the $u = 0.0$ boundary, computed within each patch for enriching the surface grid in the u-direction, $NOW \leq 50$
64	ISIDE	If ISIDE = 0 or 1, plot described body If ISIDE = 2, plot described body and mirror image
72	KODE	If KODE = 0, continue to read plot cards If KODE \neq 0, return and read option card after this plot

Plan, front, and side views (stacked) (ITYPE = 1). - For plan, front, and side views stacked one above the other in a pleasing-to-the-eye arrangement, the card should be set up as follows:

<u>Columns</u>	<u>FORTTRAN name</u>	<u>Description</u>
5 to 7	TEST1	Word "OUT" for deletion of hidden lines; otherwise leave blank

<u>Columns</u>	<u>FORTTRAN name</u>	<u>Description</u>
8 to 12	PHI	y-origin on paper of plan view, inches
13 to 17	THETA	y-origin on paper of side view, inches
18 to 22	PSI	y-origin on paper of front view, inches
48 to 52	PLOTSZ	Plot frame size (scale factor is computed using PLOTSZ and maximum dimension of configuration, i.e., the maximum dimension, usually the body length, will be scaled to exactly PLOTSZ)
53 to 55	TYPE	Word "VU3"
56 to 58	NOU	Number of lines, originating on the $w = 0.0$ boundary, computed within each patch for enriching the surface grid in the w-direction, $NOU \leq 50$
59 to 61	NOW	Number of lines, originating on the $u = 0.0$ boundary, computed within each patch for enriching the surface grid in the u-direction, $NOW \leq 50$
64	ISIDE	If ISIDE = 0 or 1, plot described body If ISIDE = 2, plot described body and mirror image
72	KODE	If KODE = 0, continue to read plot cards If KODE \neq 0, return and read option card after this plot

Cross-section plots where the method of input for defining the plane is by three input points (ITYPE = 2). - For cross-section plots where the method of input for defining the plane is by three input points (ITYPE = 2), the input card should be set up as follows:

<u>Columns</u>	<u>FORTTRAN name</u>	<u>Description</u>
1 to 6	PPL1(1)	x_1 , also used as x_0
7 to 12	PPL1(2)	y_1 , also used as y_0
13 to 18	PPL1(3)	z_1 , also used as z_0

<u>Columns</u>	<u>FORTRAN name</u>	<u>Description</u>
19 to 24	PPL2(1)	x_2
25 to 30	PPL2(2)	y_2
31 to 36	PPL2(3)	z_2
37 to 42	PPL3(1)	x_3
43 to 48	PPL3(2)	y_3
49 to 54	PPL3(3)	z_3
55 to 60	PLOTSZ	Scale factor, inches/unit
61 to 63	HPAGE	Horizontal paper origin, inches (a value of 0.0 will overlay the plots)
64 to 66	VPAGE	Vertical paper origin will be half of VPAGE, inches
67 to 69	INP	Word "PNT"
70 to 72	NOU	Number of u-values between 0.0 and 1.0, together with the $u = 0.0$ and $u = 1.0$ values, where interpolated values of w are to be computed, $NOU \leq 50$
73 to 75	NOW	Number of w-values between 0.0 and 1.0, together with the $w = 0.0$ and $w = 1.0$ values, where interpolated values of u are to be computed, $NOW \leq 50$
76 to 77	*ICUT	Number of additional cross-section plots desired

*For ICUT $\neq 0$, a second input card is required:

<u>Columns</u>	<u>FORTRAN name</u>	<u>Description</u>
1 to 6	DX	ΔX for x_1 , x_2 , and x_3
7 to 12	DY	ΔY for y_1 , y_2 , and y_3
13 to 18	DZ	ΔZ for z_1 , z_2 , and z_3
21	IH	If $IH = 0$, plots will be overlaid with HPAGE applied only after last plot If $IH \neq 0$, normal HPAGE spacing between each plot

<u>Columns</u>	<u>FORTRAN name</u>	<u>Description</u>
78	ISIDE	If ISIDE = 0 or 1, examine given body If ISIDE = 2, examine given body and its mirror image
79	IPRIN	If IPRIN = 0 or 1, do not print intersection points If IPRIN = 2, print original and original rotated points of intersection If IPRIN = 3, print scaled and scaled rotated points of intersection If IPRIN = 4, print points of intersection original and original rotated, scaled and scaled rotated
80	KODE	If KODE = 0, continue to read plot cards If KODE \neq 0, return and read option card after this plot

Cross-section plots where the method of input for defining the plane is by specifying a Mach number to define a Mach angle, an angle to define the orientation of the Mach angle, and the plane intercept on the X-axis (ITYPE = 2).- For cross-section plots where the method of input for defining the plane is by specifying a Mach number to define a Mach angle, an angle to define the orientation of the Mach angle, and the plane intercept on the X-axis (ITYPE = 2), the input card should be set up as follows:

<u>Columns</u>	<u>FORTRAN name</u>	<u>Description</u>
1 to 6	PPL1(1)	X_0
7 to 12	PPL1(2)	Y_0
13 to 18	PPL1(3)	Z_0
19 to 24	PPL2(1)	X-intercept
25 to 30	PPL2(2)	Roll angle of plane, degrees
31 to 36	PPL2(3)	Mach number, >1.0
55 to 60	PLOTSZ	Scale factor, inches/unit
61 to 63	HPAGE	Horizontal paper origin, inches (a value of 0.0 will overlay the plots)
64 to 66	VPAGE	Vertical paper origin will be half of VPAGE, inches

<u>Columns</u>	<u>FORTRAN name</u>	<u>Description</u>
67 to 69	INP	Word "ANG"
70 to 72	NOU	Number of u-values between 0.0 and 1.0, together with the u = 0.0 and u = 1.0 values, where interpolated values of w are to be computed, NOU \leq 50
73 to 75	NOW	Number of w-values between 0.0 and 1.0, together with the w = 0.0 and w = 1.0 values, where interpolated values of u are to be computed, NOW \leq 50
76 to 77	*ICUT	Number of additional cross-section plots desired
78	ISIDE	If ISIDE = 0 or 1, examine given body If ISIDE = 2, examine given body and its mirror image
79	IPRIN	If IPRIN = 0 or 1, do not print intersection points If IPRIN = 2, print original and original rotated points of intersection If IPRIN = 3, print scaled and scaled rotated points of intersection If IPRIN = 4, print points of intersection: original and original rotated, scaled and scaled rotated
80	KODE	If KODE = 0, continue to read plot cards If KODE \neq 0, return and read option card after this plot

*For ICUT \neq 0, a second input card is required:

<u>Columns</u>	<u>FORTRAN name</u>	<u>Description</u>
1 to 6	DX	Δ for X-intercept
7 to 12	DY	Δ for roll angle
13 to 18	DZ	Δ for Mach number
21	IH	If IH = 0, plots will be overlaid with HPAGE applied only after last plot If IH \neq 0, normal HPAGE spacing between each plot

DESCRIPTION OF PROGRAM OUTPUT

The program output includes the input data printout, the printout of points of intersection for cross-section plots, and a plot vector file to be postprocessed for off-line machine plots.

Input Data Printout

The card images of all the input data – configuration description and plot cards – are printed. Cards for a sample case input deck are listed in table I.

Cross-Section Plot Printout

The points of intersection of the cutting plane and the given body may be printed as specified on the cross-section plot card. The actual points in the original coordinate system, the actual points in the scaled coordinate system, the rotated and projected points in the original coordinate system, and the rotated and projected points in the scaled coordinate system may be chosen for printing or printing of the intersection points may be omitted entirely. Since the plane of intersection is always transformed into the YZ-plane, the rotated x-coordinates should be all zeros. The equation of the plane is also printed.

Plot Vector File

A plot vector file is generated during execution of both plot options – three-dimensional orthographic or cross sectional. The plot vector file can be postprocessed on the same computer run or at a later time for the desired plotting device.

MACHINE SETUP

This program was written in FORTRAN Version IV for Control Data series 6000 computer systems with the Scope 3 operating system and library tape as modified for the Langley computer facility. Tape unit 5 is used for input, unit 6 for output, and units 7 and 10 for intermediate storage. Approximately 60000 octal locations of core storage are required and the processing of information for one plot is less than 1 minute of computer time.

OPERATIONAL DETAILS

The graphic output system at Langley Research Center is in two parts: (1) a device independent graphic language which produces a plot vector file containing only plotting

commands, and (2) a set of postprocessors which format the output of the graphic language to a particular graphic device or devices.

Subroutines PSEUDO, NFRAME, NOTATE, and LINE are the basic subroutines used from the graphic software package. Subroutine PSEUDO causes the necessary parameters and linkage to be set up to output a device independent plot vector file for postprocessing for a particular plotting device. Subroutine NFRAME provides a means of executing a frame advance movement. Alphanumeric information for annotation and labeling is drawn by subroutine NOTATE. Subroutine LINE draws a continuous line through a set of successive data points where the minimum values and scale factors are stored at the end of the data arrays.

CONCLUDING REMARKS

A computer program has been written to define mathematically an arbitrary curved surface in surface-patch-equation form. Although the program is oriented toward aircraft configurations, it can be used to model mathematically any three-dimensional object by using an alternate data input format. Parametric cubic spline curves are fitted to the input data points to define the boundary-curve slopes. These slopes and the corner points are the necessary components of the surface patch equations. Program options include the application of three-dimensional rotation equations directly to the patch equations for plotting the surface at any desired viewing angle and the solution of a number of patches and a plane for generating cross-section or contour plots of an object or surface. Output from this program has been used to drive Calcomp, Gerber, and Varian plotters. The program has also been used for on-line display on a cathode-ray-tube device.

Langley Research Center,
National Aeronautics and Space Administration,
Hampton, Va., February 28, 1975.

APPENDIX A

PARAMETRIC CUBIC SPLINE SPACE CURVES

The derivatives in u and w at the corners of the surface patches are required for the surface equation. The grid points which determine the boundary curves are fitted in the w -direction and then in the u -direction for computation of the derivatives. A parametric cubic spline curve fit technique by Timothy E. Johnson of Massachusetts Institute of Technology is used.

Parametric cubics are the lowest order polynomial with the property of being able to twist through space. The spline curve exhibits the usual meaning of smoothness by minimizing curvature. Parametric curves are not sensitive to infinite slopes.

For purposes of completeness a brief description of the method follows as well as an explanation of the calling sequence for Subroutine SPFIT which utilizes this method.

A series of adjacent polynomial segments between each pair of given points is used to represent the curve.

The component cubic parametric equations are

$$X(t) = A_x t^3 + B_x t^2 + C_x t + D_x$$

$$Y(t) = A_y t^3 + B_y t^2 + C_y t + D_y$$

$$Z(t) = A_z t^3 + B_z t^2 + C_z t + D_z$$

where all operations are performed once on each component equation.

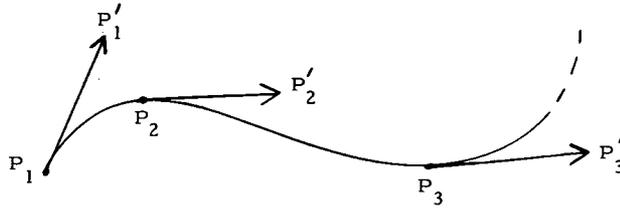
The component equations will be represented by

$$P(t) = At^3 + Bt^2 + Ct + D \quad (1)$$

The tangent parametric slopes at each point define the coefficients of the cubic segments and must be determined so that the tangent slopes give a smooth curve.

The given points P_1, P_2, \dots, P_n have the corresponding tangent slopes P'_1, P'_2, \dots, P'_n and the independent variable t varies so that $0 \leq t \leq L$ where L is the chord length between the given points. (See sketch (f).)

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Sketch (f)

The boundary conditions for one cubic segment $P(t)$ can be written as

$$P(0) = P_1$$

$$P(L_1) = P_2$$

$$\frac{dP(t)}{dt}_{t=0} = P'_1$$

$$\frac{dP(t)}{dt}_{t=L_1} = P'_2$$

The coefficients of equation (1) can be written in terms of the end points and parametric slopes for a given segment

$$P(0) = D_1 = P_1$$

$$\frac{dP(t)}{dt}_{t=0} = C_1 = P'_1$$

and

$$P(L_1) = AL_1^3 + BL_1^2 + P'_1L_1 + P_1 = P_2$$

$$\frac{dP(t)}{dt}_{t=L_1} = 3AL_1^2 + 2BL_1 + P'_1 = P'_2$$

Solving the last two equations yields

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$$A_1 = \frac{2(P_1 - P_2)}{L_1^3} + \frac{P_1'}{L_1^2} + \frac{P_2'}{L_1^2}$$

$$B_1 = \frac{3(P_2 - P_1)}{L_1^2} - \frac{2P_1'}{L_1} - \frac{P_2'}{L_1}$$

The coefficients for each adjoining segment are found in the same manner.

The adjacent cubic segments can be related by setting the second derivatives equal at the common points.

For equal second derivatives at P_2

$$\frac{d^2P(t)}{dt^2}_{t=L_1} = \frac{d^2P(t)}{dt^2}_{t=0}$$

$$6A_1L_1 + 2B_1 = 2B_2 \tag{2}$$

Substituting the expressions for A and B into equation (2) and collecting terms give in terms of the unknown slopes:

$$L_2P_1' + 2(L_2 + L_1)P_2' + L_1P_3' = \frac{3}{L_1L_2} \left[L_1^2(P_3 - P_2) + L_2^2(P_2 - P_1) \right]$$

This equation may be written over all segments in matrix notation:

$$\begin{bmatrix} L_2 & 2(L_1 + L_2) & L_1 & \bigcirc \\ & L_3 & 2(L_2 + L_3) & L_2 \\ & & L_4 & 2(L_3 + L_4) \\ \bigcirc & & & \end{bmatrix} \times \begin{bmatrix} P_1' \\ P_2' \\ P_3' \\ \vdots \\ P_n' \end{bmatrix} = \begin{bmatrix} 3/L_1L_2 \left[L_1^2(P_3 - P_2) + L_2^2(P_2 - P_1) \right] \\ 3/L_2L_3 \left[L_2^2(P_4 - P_3) + L_3^2(P_3 - P_2) \right] \\ \vdots \\ 3/L_{n-2}L_{n-1} \left[L_{n-2}^2(P_n - P_{n-1}) + L_{n-1}^2(P_{n-1} - P_{n-2}) \right] \end{bmatrix}$$

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Since there are two more unknowns than there are equations, the second derivatives at P_1 and P_N are made equal to zero. The Thomas Algorithm, which is equivalent to Gaussian Elimination without pivoting, is used for solving the tridiagonal matrix. The cubic coefficients are normalized so that the parametric space for each curve segment varies from 0 to 1:

$$A' = AL^3$$

$$B' = BL^2$$

$$C' = CL$$

APPENDIX B

BICUBIC SURFACE PATCHES

This appendix is a brief description of the surface patch method used in program D3400.

The x-, y-, and z-coordinates of surface points are functions of two variables u and w:

$$X = f(u,w)$$

$$Y = g(u,w)$$

$$Z = h(u,w)$$

$$V = (X \ Y \ Z)$$

The vector $V(u,w)$ is a function of the two variables, u and w, which take on only the values between 0.0 and 1.0.

The method builds a surface by joining surface "patches." A surface patch can be thought of as a portion of a surface bounded by four space curves: $(0,w)$, $(1,w)$, $(u,0)$, and $(u,1)$.

The surface patch equation used is

$$V(u,w) = U\bar{B}M^tW^t$$

where

$$U = \begin{bmatrix} u^3 & u^2 & u & 1 \end{bmatrix}$$

$$W = \begin{bmatrix} w^3 & w^2 & w & 1 \end{bmatrix}$$

$$\bar{B} = \begin{bmatrix} V(0,0) & V(0,1) & V_w(0,0) & V_w(0,1) \\ V(1,0) & V(1,1) & V_w(1,0) & V_w(1,1) \\ V_u(0,0) & V_u(0,1) & V_{uw}(0,0) & V_{uw}(0,1) \\ V_u(1,0) & V_u(1,1) & V_{uw}(1,0) & V_{uw}(1,1) \end{bmatrix}$$

APPENDIX B

This 4×4 matrix is called a boundary matrix as it contains only geometric properties from the boundary curves: corner coordinates, corner slopes, and corner twists. (The corner twists are all made equal to zero in the present application.) These quantities are constants and grouped systematically in the matrix.

The blending function matrix M provides a blending effect from one surface patch into an adjoining patch

$$M = \begin{bmatrix} 2 & -2 & 1 & 1 \\ -3 & 3 & -2 & -1 \\ 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & 0 \end{bmatrix}$$

Since the matrix product MBM^t is constant, the pre- and post-multiplications are performed and the equation stored as $S = MBM^t$ for further computer processing. It is a simple matter, then, for writing an expression for u with w held fixed or u held fixed and w varying.

For a detailed development of the surface patch equation, see reference 1. Reference 2 presents the bicubic form of the surface patch equation as used in this report.

APPENDIX C

DESCRIPTION OF FILE AND METHOD OF STORAGE FOR SURFACE PATCH EQUATIONS

Program D3400 computes and stores by columns of the surface grid the patch matrix equations using the previously stored lines of grid points. A disk file is used for temporary storage of the elements of all the patch matrix equations.

The elements and certain other information are written in binary on disk unit 7 in the following format. FORTRAN names from the given program are used for illustration.

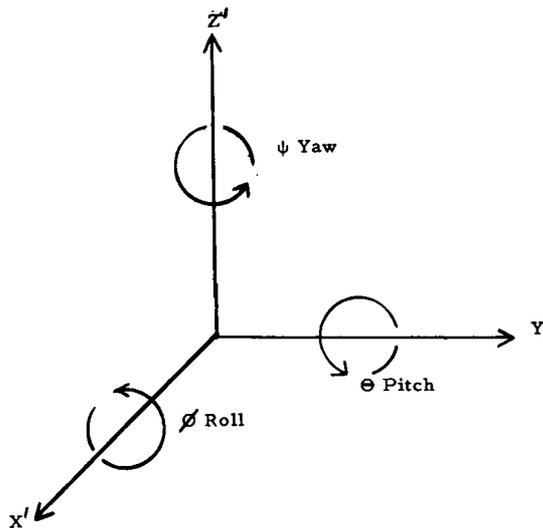
<u>Record</u>	<u>Name</u>	<u>Purpose</u>
1	ABC(8)	Identification
2	XMIN	Minimum X of the entire body
	XMAX	Maximum X of the entire body
	YMIN	Minimum Y of the entire body
	YMAX	Maximum Y of the entire body
	ZMIN	Minimum Z of the entire body
	ZMAX	Maximum Z of the entire body
	NOBJ	Total number of objects (or components) to form the complete body
3	(for NOBJ ₁)	
	NSURF	Number of surfaces in object
	M1	Not used
	M2(2)	Name of object (for printing only)
	M3	Not used
	M4	Not used
4	(for NSURF ₁)	
	N1	Number of rowwise patches (NCOL - 1)
	N2	Number of columnwise patches (NROW - 1)
	N3	Not used
	N4	Not used
5	PATCH (4,4,3)	48 elements of a patch equation are written by columns as one record
		(Record 5 is repeated for N1 × N2 patches taken by columns over the surface grid)
		(Records 4, 5, and so forth are repeated for each NSURF from record 3)
		(Repeat record 3 for each NOBJ as given in record 2 and repeat records 4, 5, and so forth as required)

APPENDIX D

ORTHOGRAPHIC PROJECTIONS USING SURFACE PATCH EQUATIONS

The orthographic projections illustrated in this report are created by rotating each patch element to the desired viewing angle, transforming the rotated patch into a coordinate system in the plane of the paper, and computing actual coordinates from the patch equation. The body coordinate system is coincident with the fixed system in the plane of the paper when all the rotation angles are zero; for example, the configuration X-axis and Y-axis would coincide with the paper for plots in the X'Y' paper plane.

The rotations of the body and its coordinate system to give a desired viewing angle are specified by angles of yaw, pitch, and roll (ψ , θ , and ϕ), shown in sketch (g).



Sketch (g)

The equations used to transform the patch equations defining the body with a set of rotation equations (ψ , θ , and ϕ) into the desired paper plane are

$$S'_x = S_x(\cos \theta \cos \psi) + S_y(-\sin \psi \cos \phi + \sin \theta \cos \psi \sin \phi) \\ + S_z(\sin \psi \sin \phi + \sin \theta \cos \psi \cos \phi)$$

$$S'_y = S_x(\cos \theta \sin \psi) + S_y(\cos \psi \cos \phi + \sin \theta \sin \psi \sin \phi) \\ + S_z(-\cos \psi \sin \phi + \sin \theta \sin \psi \cos \phi)$$

APPENDIX D

$$S'_Z = S_X(-\sin \theta) + S_Y(\cos \theta \sin \phi) + S_Z(\cos \theta \cos \phi)$$

Each element of the patch equation is rotated to the desired viewing angle and then transformed into a coordinate system in the plane of the paper. Only two of the preceding equations, determined by the desired paper plane, are used and result in a two-component patch equation.

The body surface plots may be enriched to any desired degree. By assigning u a value between 0.0 and 1.0, we have two cubic equations in w which may be easily solved by varying w from 0.0 to 1.0 for the rotated and projected coordinate values of a line across the patch. In a similar manner, w may be assigned a value from 0.0 to 1.0 resulting in cubic equations in u . By varying u from 0.0 to 1.0, coordinate values are generated across the patch in the u -direction.

An optional hidden-line test is incorporated into the program which may be used to provide the capability of deleting most elements on the surface of the configuration which would not be seen by a viewer. No provision is made for deleting portions of an element or components hidden by other components.

The surface vector normal to the paper plane is computed at each interpolated point. (See ref. 1.) If the surface vector is positive, the computed point faces the viewer and is visible; if the surface vector is negative the computed point is not visible and is not plotted. With

$$U = \begin{bmatrix} X_u & Y_u & Z_u \end{bmatrix} = \begin{bmatrix} \frac{\partial X}{\partial u} & \frac{\partial Y}{\partial u} & \frac{\partial Z}{\partial u} \end{bmatrix}$$

$$W = \begin{bmatrix} X_w & Y_w & Z_w \end{bmatrix} = \begin{bmatrix} \frac{\partial X}{\partial w} & \frac{\partial Y}{\partial w} & \frac{\partial Z}{\partial w} \end{bmatrix}$$

For one surface, the surface normal vector is

$$N = U \times W = \begin{bmatrix} J_x & J_y & J_z \end{bmatrix}$$

where

$$J_x = \begin{vmatrix} Y_u & Z_u \\ Y_w & Z_w \end{vmatrix}$$

APPENDIX D

$$J_y = \begin{vmatrix} Z_u & X_u \\ Z_w & X_w \end{vmatrix}$$

$$J_z = \begin{vmatrix} X_u & Y_u \\ X_w & Y_w \end{vmatrix}$$

The visibility of the point under consideration is determined by evaluating only the Jacobian outwardly normal to the paper plane at the point.

APPENDIX E

CROSS-SECTION OR CONTOUR PLOTS USING SURFACE PATCH EQUATIONS

By using both the surface patch equation in the form

$$V(u,w) = USW^T$$

where the components of the 4×4 matrix S are $[S_x \quad S_y \quad S_z]$ (see appendix B) and the equation of a plane

$$ax + by + cz - d = 0.0$$

and equation of the intersection of the plane and the patch surface may be written. Substitute $x = US_x W^T$, $y = US_y W^T$, and $z = US_z W^T$ in the preceding equation so that

$$U[aS_x + bS_y + cS_z]W^T - d = 0.0$$

The matrix $[G] = [aS_x + bS_y + cS_z]$ is composed of constant elements and may be evaluated for an equation in the two variables u and w

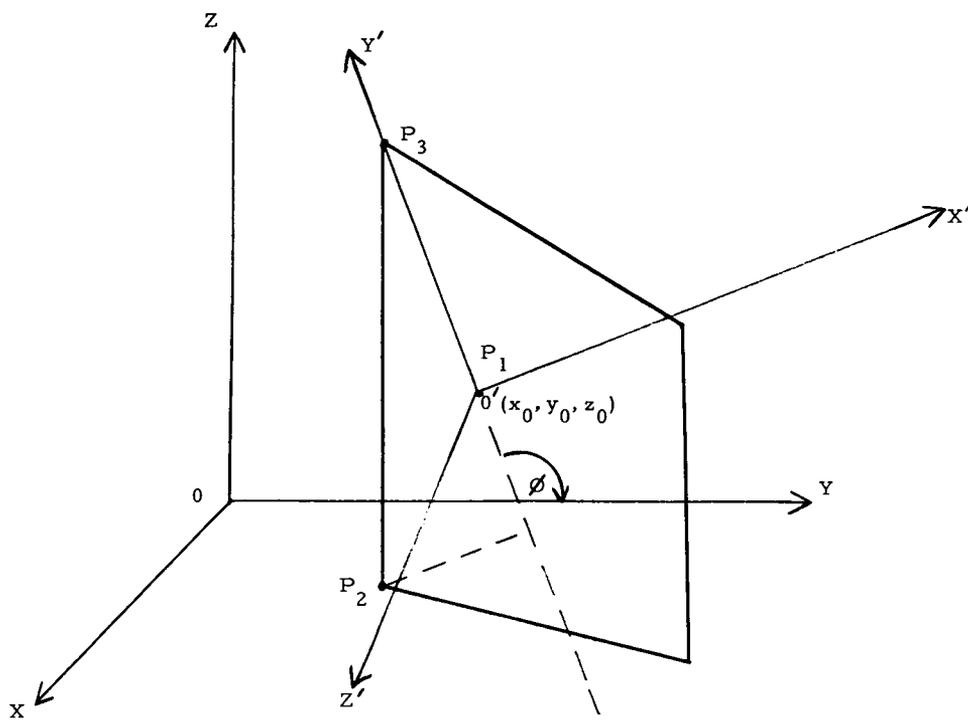
$$UGW^T = d$$

By assigning values to w , a series of cubic equations in u are solved for points on the intersection curve of the surface with the plane or values may be assigned to u for cubic equations in w to solve for the intersection curve. (See ref. 1.) Only one solution for a curve of intersection is allowed.

The points of the curve of intersection are then rotated and translated so that the plane of intersection coincides with the YZ-plane of the paper. The method for rotation and translation follows.

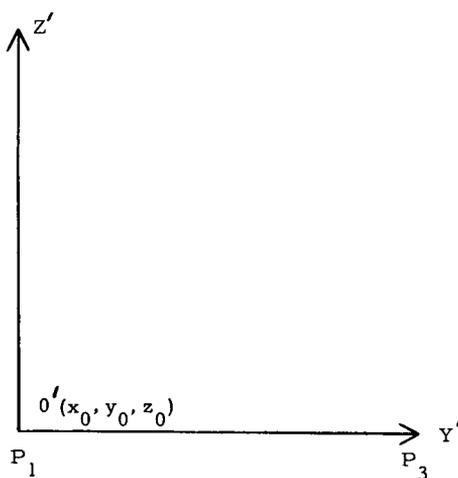
Sketch (h) illustrates the transformation system established by the 3 input points used to define the cutting plane.

APPENDIX E



Sketch (h)

The translated and rotated coordinate system used for plotting is shown in sketch (i).



Sketch (i)

Sketch (j) illustrates the choosing of three points on a cutting plane when the method of defining the plane is by the input of an X -intercept, a roll angle $\bar{\theta}$, and a Mach number.

- XGF One-quarter of Mach cone
- EFGHIJ Lies in plane parallel to YZ -plane

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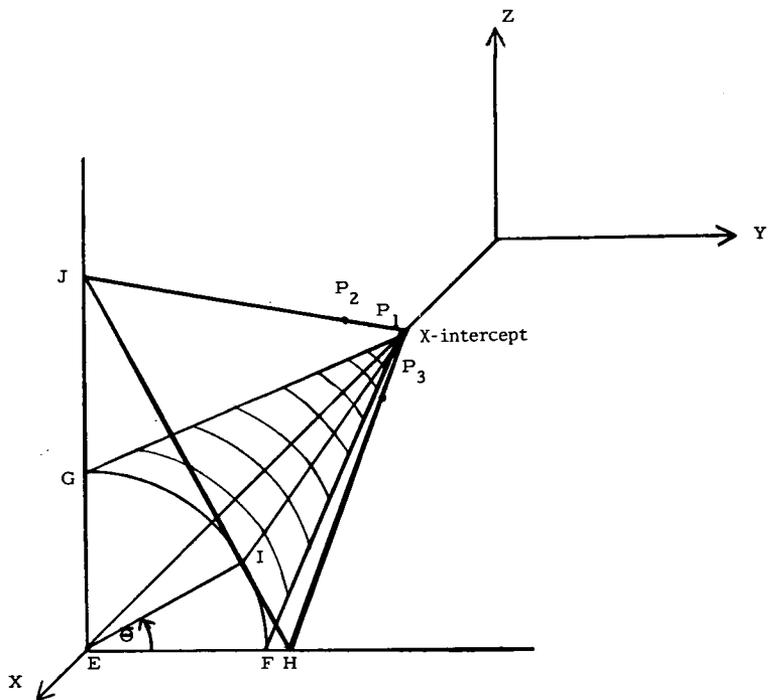
- JXH Mach plane, tangent to cone along IX
 IE Projection onto plane JHE of normal to Mach plane at I

To locate three points on the plane:

<u>Point</u>	<u>X</u>	<u>Y</u>	<u>Z</u>
P ₁	X	0.0	0.0
P ₂	X - C	0.0	1.0
P ₃	X - B	1.0	0.0

where the equation of the plane is expressed as $AX + BY + CZ = D$ with

$$\beta = \sqrt{M^2 - 1}, \quad A = 1.0, \quad B = -\beta \cos \bar{\theta}, \quad C = -\beta \sin \bar{\theta}, \quad \text{and} \quad D = X$$



Sketch (j)

By using the three input coordinates that define the cutting plane, two diagonal vectors may be formed with the components:

APPENDIX E

$$T_{1X} = x_3 - x_1$$

$$T_{1Y} = y_3 - y_1$$

$$T_{1Z} = z_3 - z_1$$

$$T_{2X} = x_3 - x_2$$

$$T_{2Y} = y_3 - y_2$$

$$T_{2Z} = z_3 - z_2$$

The cross products of the diagonal vectors give

$$N_X = T_{2Y}T_{1Z} - T_{1Y}T_{2Z}$$

$$N_Y = T_{1X}T_{2Z} - T_{2X}T_{1Z}$$

$$N_Z = T_{2X}T_{1Y} - T_{1X}T_{2Y}$$

which when divided by $N = \sqrt{N_X^2 + N_Y^2 + N_Z^2}$ yield the unit normal vector n of the cutting plane

$$n_X = \frac{N_X}{N}$$

$$n_Y = \frac{N_Y}{N}$$

$$n_Z = \frac{N_Z}{N}$$

To determine the coordinate system for plotting, two unit vectors lying in the cutting plane are needed

$$v_{1X} = \frac{T_{1X}}{T}$$

$$v_{1Y} = \frac{T_{1Y}}{T}$$

$$v_{1Z} = \frac{T_{1Z}}{T}$$

where

$$T = \sqrt{T_{1X}^2 + T_{1Y}^2 + T_{1Z}^2}$$

and

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$$v_{2X} = n_Y v_{1Z} - n_Z v_{1Y}$$

$$v_{2Y} = n_Z v_{1X} - n_X v_{1Z}$$

$$v_{2Z} = n_X v_{1Y} - n_Y v_{1X}$$

The transformation matrix becomes

$$[A] = \begin{bmatrix} a_{11} & a_{12} & a_{13} \\ a_{21} & a_{22} & a_{23} \\ a_{31} & a_{32} & a_{33} \end{bmatrix}$$

where

$$a_{11} = n_X \quad a_{12} = n_Y \quad a_{13} = n_Z$$

$$a_{21} = v_{1X} \quad a_{22} = v_{1Y} \quad a_{23} = v_{1Z}$$

$$a_{31} = v_{2X} \quad a_{32} = v_{2Y} \quad a_{33} = v_{2Z}$$

The origin of the reference coordinate system is transferred to the first point given in defining the cutting plane

$$\begin{bmatrix} x_0 \\ y_0 \\ z_0 \end{bmatrix} = [A] \begin{bmatrix} x_1 \\ y_1 \\ z_1 \end{bmatrix}$$

The transformation from the reference to the paper coordinate system is accomplished by:

REFERENCES

1. Coons, Steven A.: Surfaces for Computer-Aided Design of Space Forms. MAC-TR-41 (Contract No. AF-33(600)-42859), Massachusetts Inst. Technol., June 1967. (Available from DDC as AD 663 504.)
2. Eshleman, A. L.; and Meriwether, H. D.: Graphic Applications to Aerospace Structural Design Problems. Douglas Paper 4650, McDonnell Douglas Corp., Sept. 1967.
3. Craidon, Charlotte B.: Description of a Digital Computer Program for Airplane Configuration Plots. NASA TM X-2074, 1970.

TABLE I.- SAMPLE CASE INPUT CARDS

SIMPLE CAMBERED CIRCULAR BODY														
1	1	-1	1	1	6	5	1	5	6	1	4	1	5	
9494.														REFA
0.	20.	50.	70.	100.										XAF 5
82.30	5.05	0.	180.	100										WAFORG 1
114.1999.90		-.45	142.351											WAFORG 3
157.98	19.80	-1.85	98.570											WAFORG 5
239.18	46.20	-2.80	36.719											WAFORG 9
269.23	59.40	-4.30	15.670											WAFORG11
282.00	66.00	-4.40	7.400											WAFORG12
3.6	2.75	-3.45	-6.8	-9.4										TZORD 1
0.	1.35	-1.2	-3.45	-6.8										TZORD 3
0.	.72	.0875	-.7825	-2.173										TZORD 5
0.	.248	.311	.2995	.2385										TZORD 9
0.	-.043	-.090	-.110	-.1224										TZORD 11
0.	-.0325	-.075	-.100	-.1324										TZORD 12
0.	1.069	1.518	1.451	0.										WAFORD 1
0.	.889	1.272	1.136	0.										WAFORD 3
0.	.886	1.294	1.087	0.										WAFORD 5
0.	.880	1.375	1.155	0.										WAFORD 9
0.	.880	1.375	1.155	0.										WAFORD11
0.	.880	1.375	1.155	0.										WAFORD12
0.	70.	130.	200.	260.	312.									XFUS 6
7.4	7.4	1.25	-7.45	-10.2	-10.2									ZFUS 6
0.	96.	98.	79.	62.	0.									AFUS 6
241.0	31.75	-3.60												PODORG 2
0.	12.	24.	34.5											XPOD
2.292	2.79	3.08	3.1											PODR
252.0	47.0	-2.95	35.3	285.36	47.0	6.31	4.77							FINORG 2
0.	30.	50.	70.	100.										XFIN
0.	.76	.977	.927	0.										FINORD
	1													
		10.	4.	8.										
X Z		-45.	10.	-30.				15.	VU3				2	
X Z		-45.	10.	-30.				15.	ORT				2	
X Z OUT		-45.	10.	-30.				15.	ORT	5	6	2		
	2							15.	ORT	5	6	2		1
200.	0.	0.	200.	0.	1.	200.	1.	0.	.30	0.	16.PNT			
200.	0.	0.	200.	0.	1.	200.	1.	0.	.30	20.	16.PNT	8	8	
-10.	0.	0.	0.	45.	1.2				.1	0.	16.ANG	8	8202	
2.5														
-10.	0.	0.	55.	45.	1.2				.1	20.	16.ANG	8	8482	
5.														

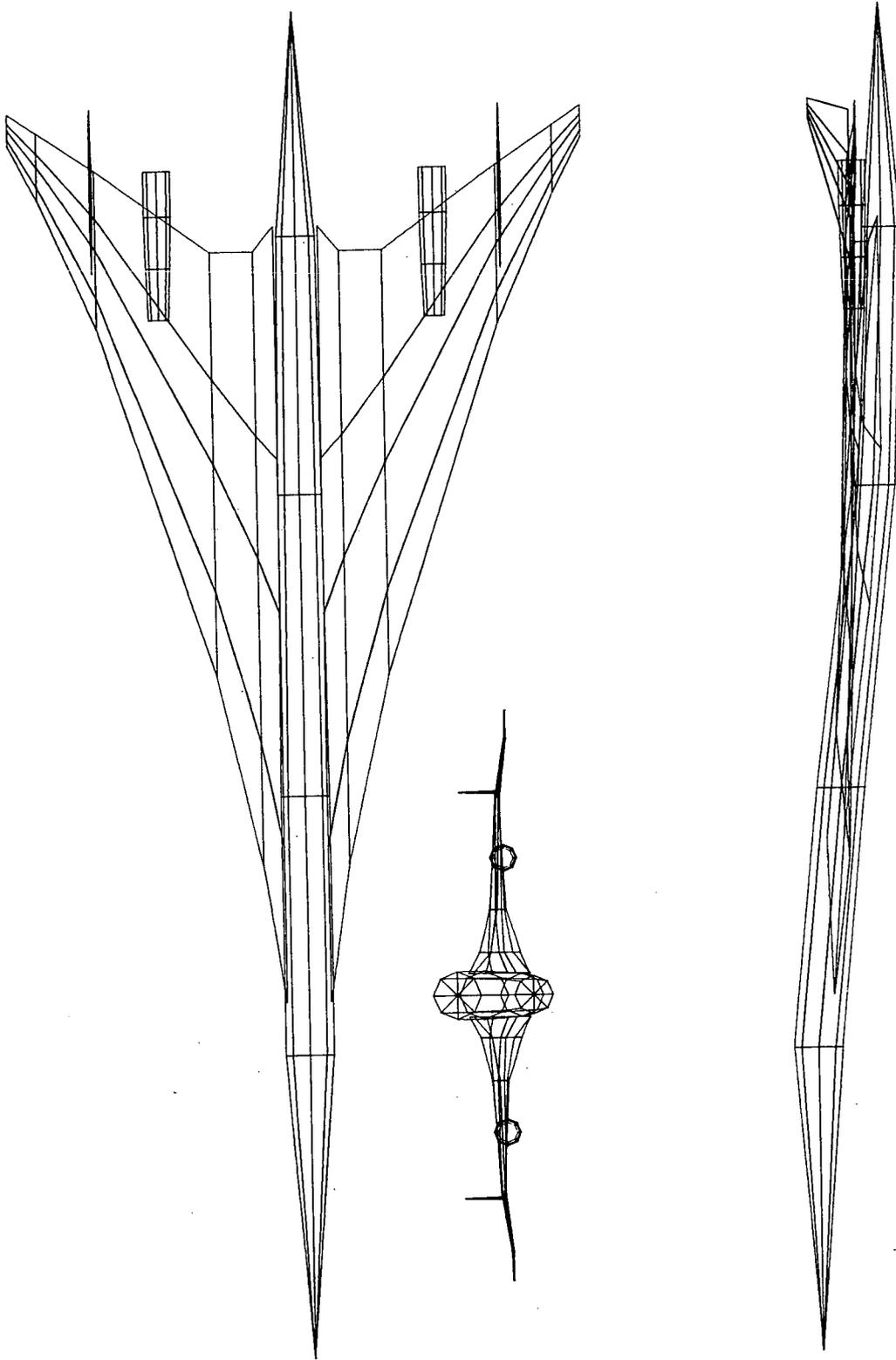
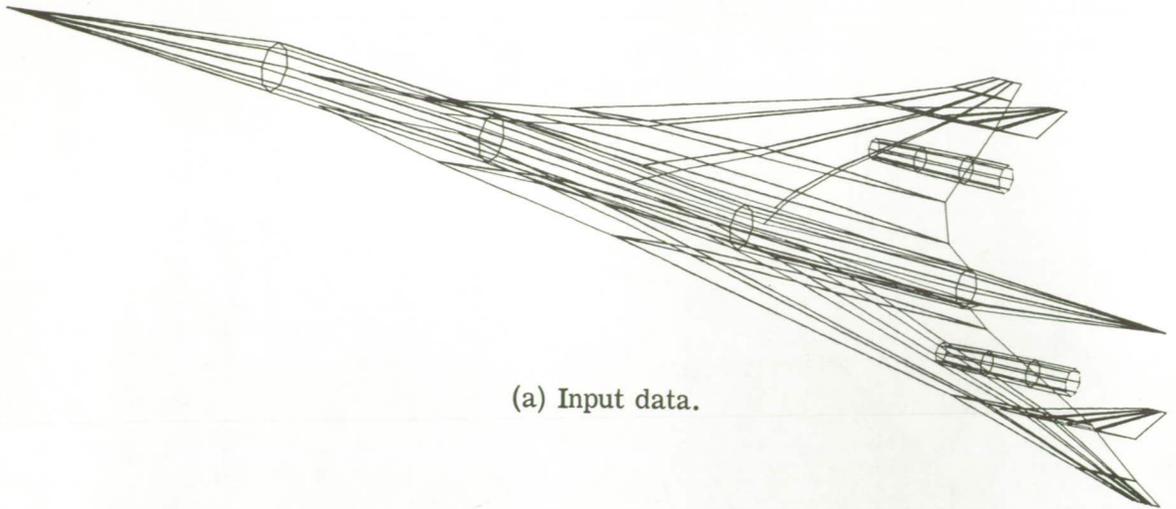
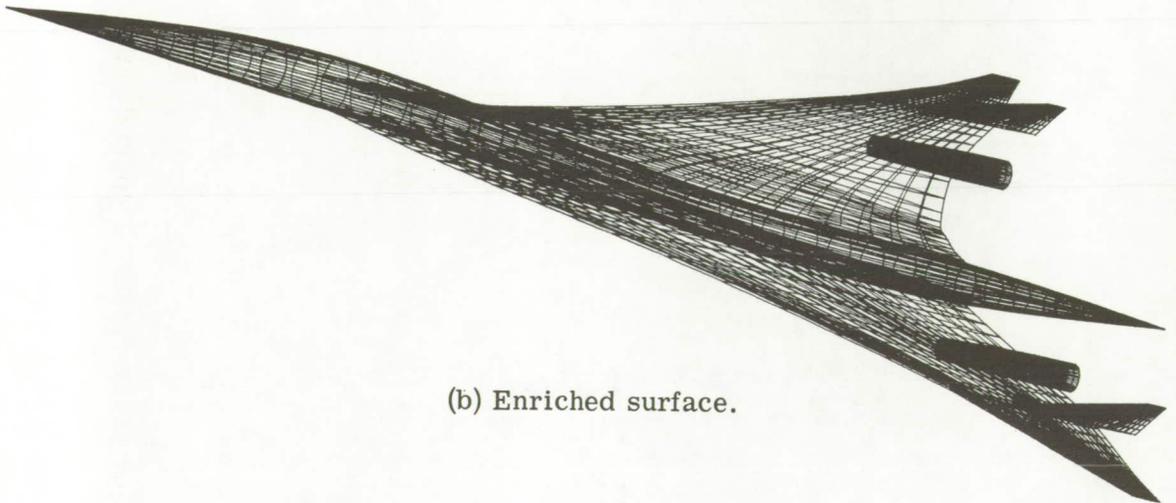


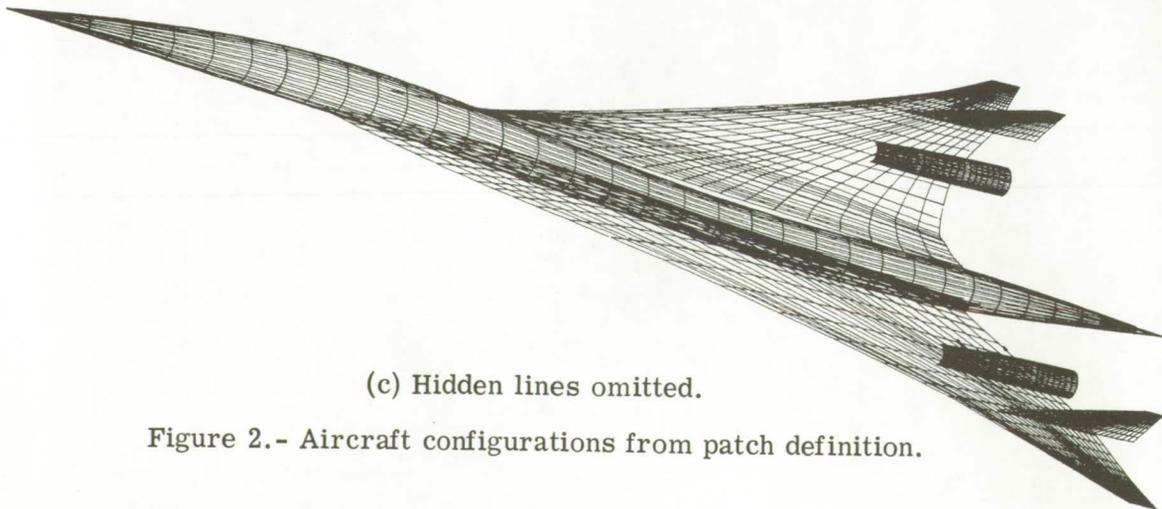
Figure 1.- A sample input configuration - simple cambered circular body.



(a) Input data.

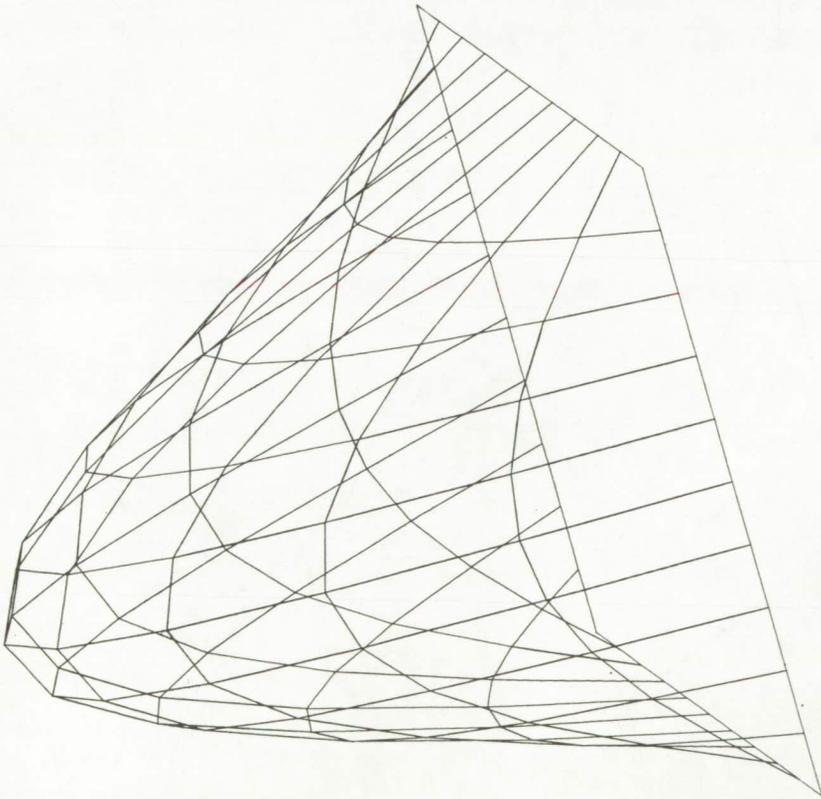


(b) Enriched surface.

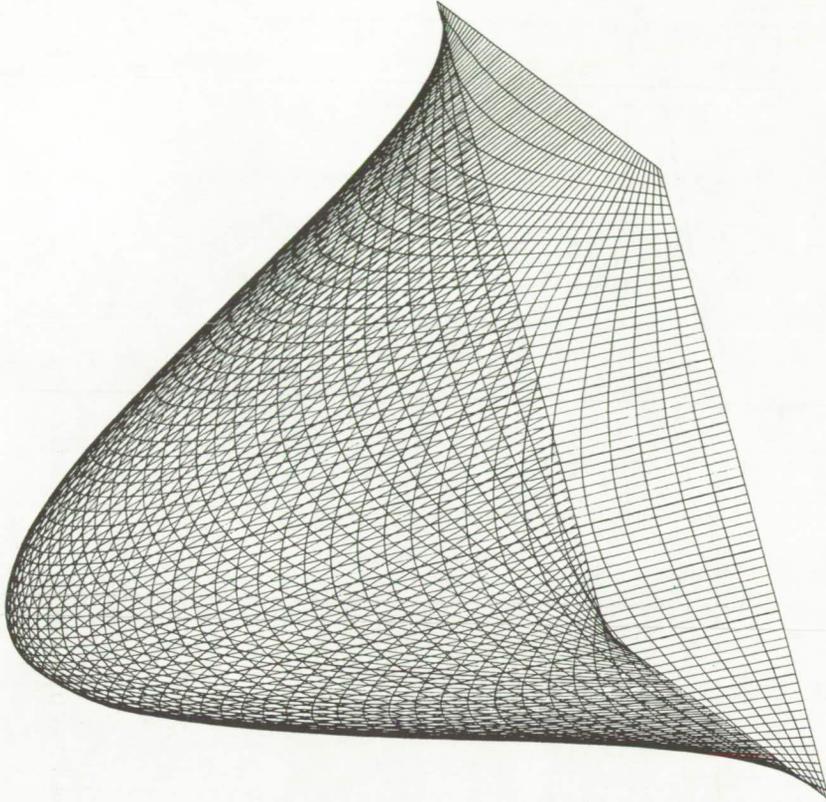


(c) Hidden lines omitted.

Figure 2.- Aircraft configurations from patch definition.



(a) Input data.



(b) Enriched surface.

Figure 3.- Alternate input from patch definition.

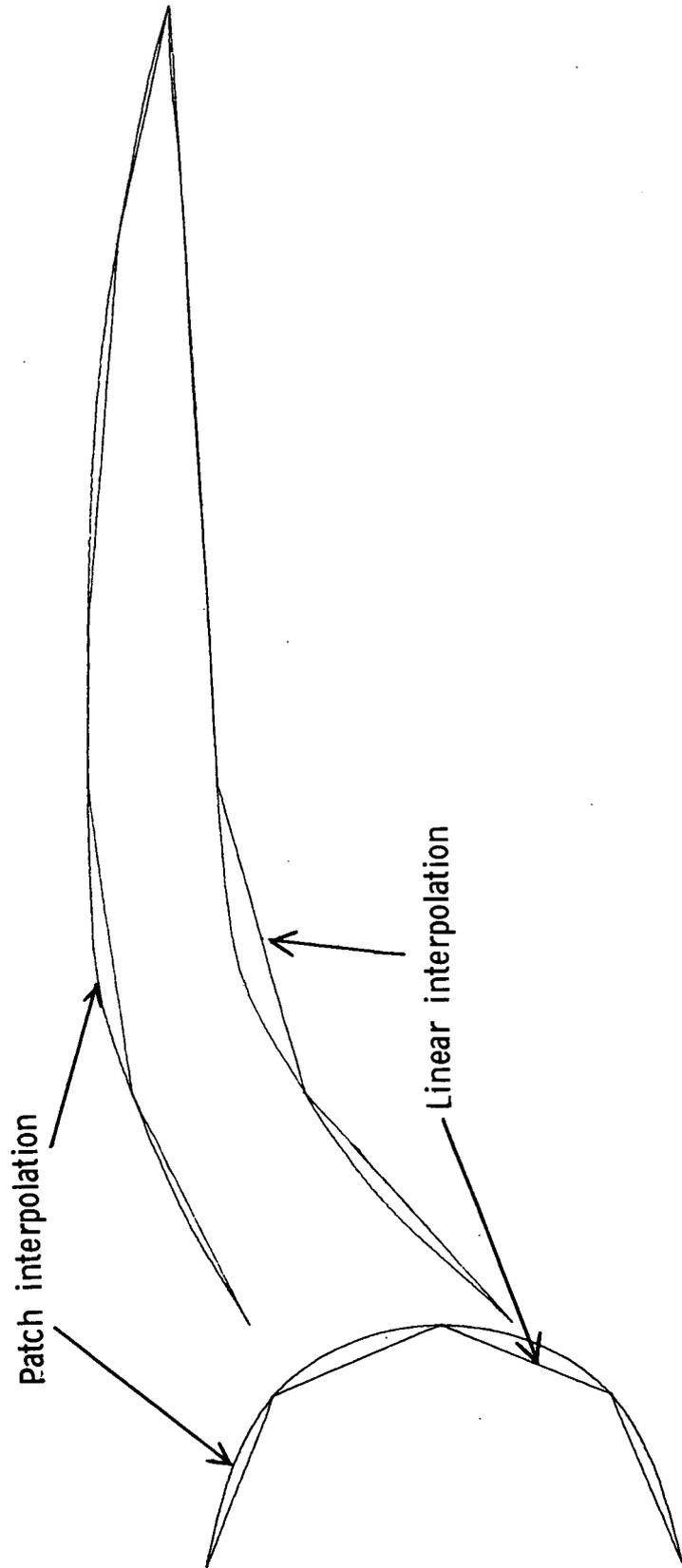


Figure 4.- Aircraft configuration cross section from patch definition.

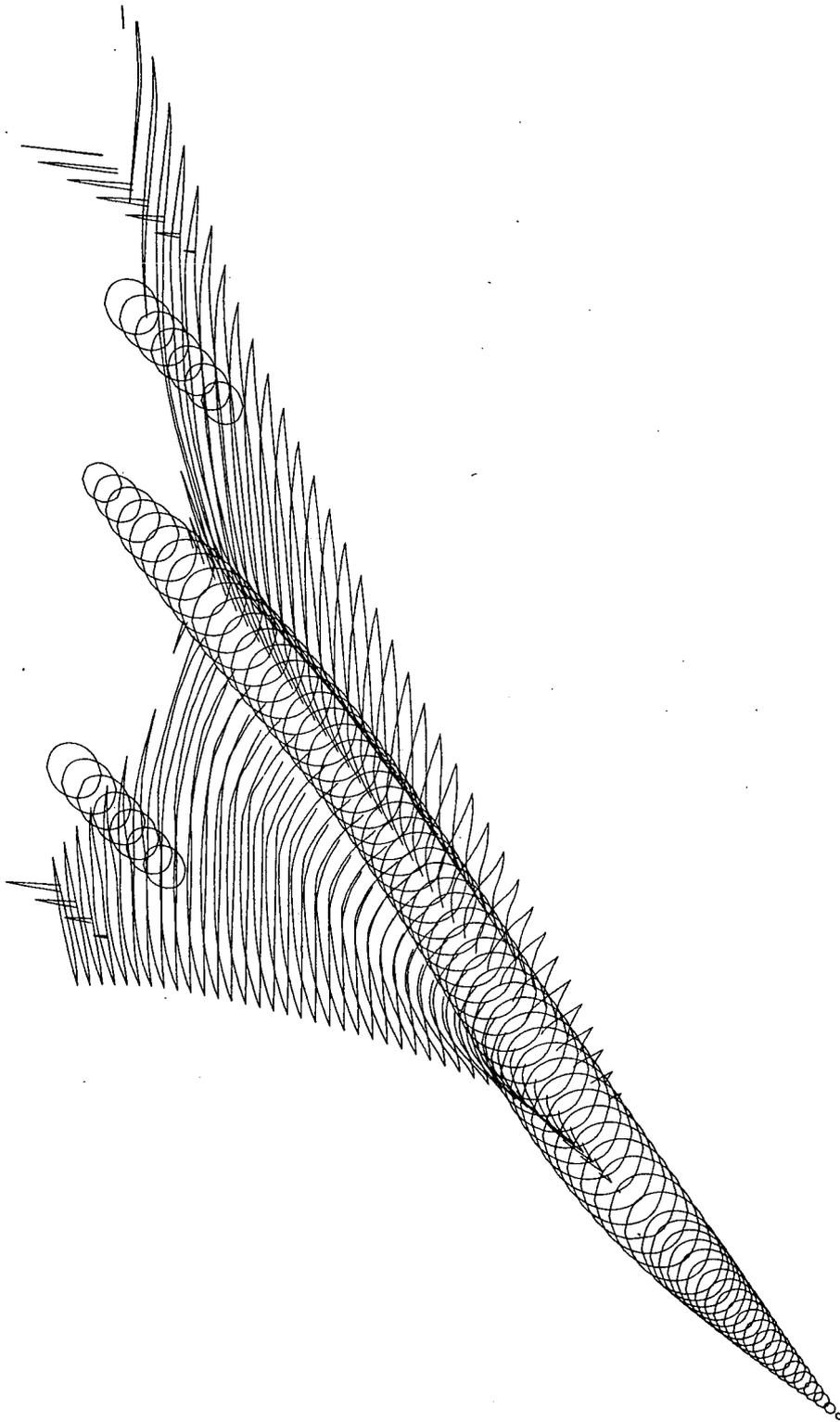
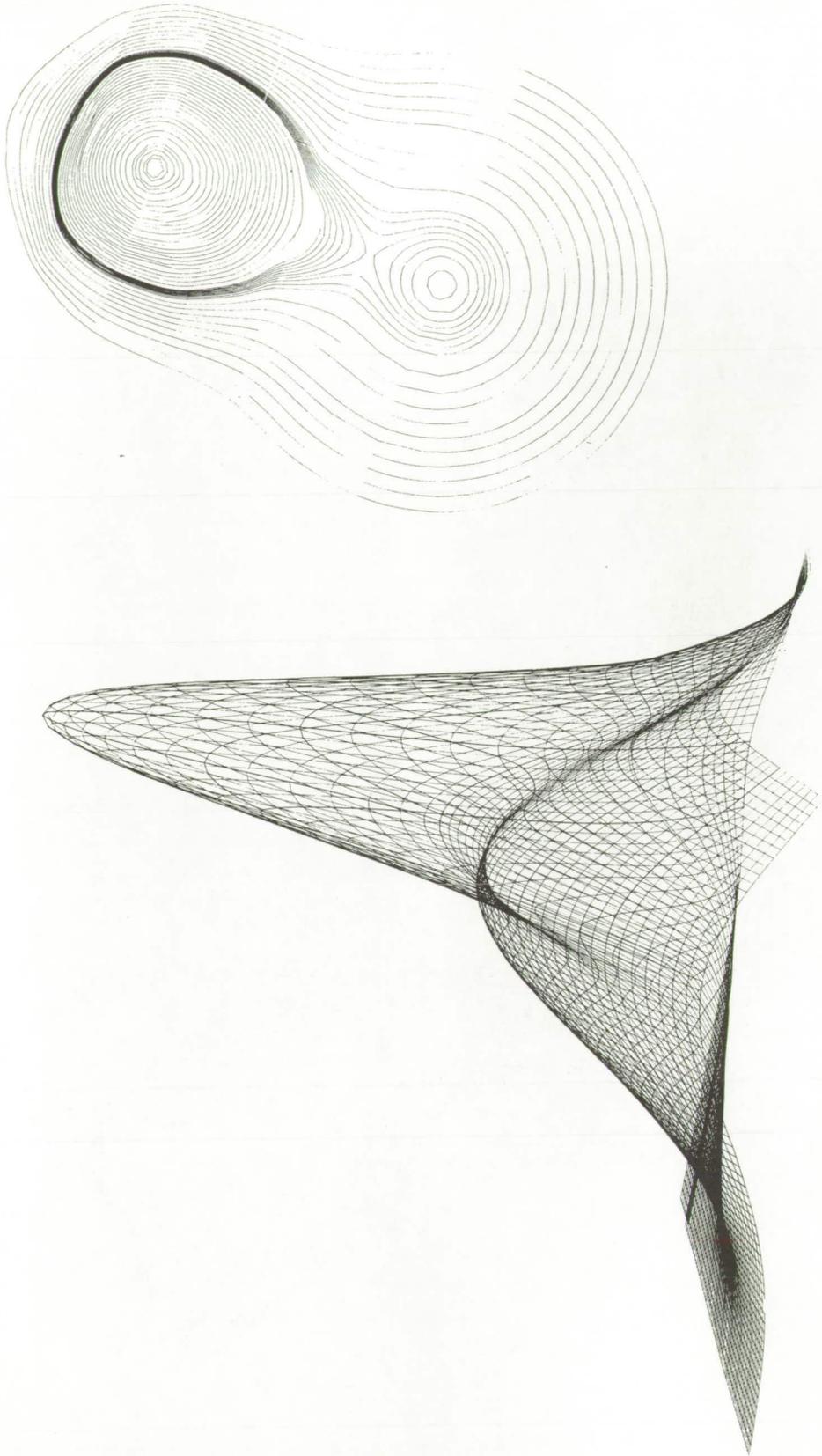


Figure 5.- Aircraft configuration cross sections with constant reference.



(a) Input data.

(b) Contour data.

Figure 6. - Optional input cross sections with constant reference.



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—NATIONAL AERONAUTICS AND SPACE ACT OF 1958

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