EVALUATION OF UPWELLING INFRARED RADIANCE FROM
EARTH'S ATMOSPHERE

By
S.K. Gupta

and
S.N. Tiwari

Prepared for the
National Aeronautics and Space Administration
Langley Research Center
Hampton, Virginia

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Dr. Henry G. Reichle, Technical Monitor
Meteorology Section

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EVALUATION OF UPWELLING INFRARED RADIANCE FROM EARTH'S TROPOSPHERE

by

S. K. Gupta and S. N. Tiwari
School of Engineering
Old Dominion University
Norfolk, Virginia 23508

SUMMARY

Basic equations for calculating the upwelling atmospheric radiation are presented which account for various sources of radiation coming out at the top of the atmosphere. The theoretical formulation of the transmittance models (line-by-line and quasi-random band model) and the computational procedures used for the evaluation of the transmittance and radiance are discussed in detail. By employing the Lorentz line-by-line and quasi-random computer programs, model calculations were made to determine the upwelling radiance and signal change in the wave number interval of CO fundamental band. These results are useful in determining the effects of different interfering molecules, water vapor profiles, ground temperatures, and ground emittances on the upwelling radiance and signal change. This information is of vital importance in establishing the feasibility of measuring the concentrations of pollutants in the atmosphere from a gas filter correlation instrument flown on an aircraft or mounted on a satellite.
I. INTRODUCTION

The present status of knowledge about the fate of the relevant pollutants in the atmosphere is limited. Determination of the concentration of various atmospheric pollutants is important because of their considerable influence on the weather and environment.

The earth's surface with its temperature in the vicinity of 300°K emits like a black body from the near to the far infrared region of the spectrum. The emission in the near infrared (between 2 and 20 microns) is particularly important because most of the minor atmospheric constituents (i.e., CO₂, N₂O, H₂O, CO, CH₄, NH₃, etc.) absorb and emit in this spectral region. The upwelling infrared radiation from the earth's atmosphere, therefore, consists of the modulated surface radiation and the radiation from the atmosphere. This radiation carries the spectral signature of all the minor atmospheric constituents amongst which gases such as CO, CH₄ and NH₃ are called the atmospheric pollutants.

Detection of the atmospheric pollutants from infrared radiation measurements requires a detailed knowledge of the atmospheric constituents which absorb and emit significantly in the spectral range of interest. A systematic representation of the absorption and emission by a gas, in the infrared, requires the identification of the major infrared bands and evaluation of the line parameters of these bands. The line parameters depend upon the temperature, pressure, and concentration of the absorbing molecules and, in general, these quantities vary continuously along a nonhomogeneous path through the atmosphere. With the availability of high resolution spectrometers, it is now possible to determine the line positions, intensities, and half-widths of spectral lines quite accurately. As a result, the
line parameters of the strong infrared bands of most minor atmospheric constituents are now known quite well [1-3].

An accurate model for the spectral absorption coefficient is of vital importance in the calculations of the transmittance of an atmospheric constituent and in the correct formulation of the radiative flux equations which are employed in the reduction of data obtained from either direct or remote measurements. High spectral resolution measurements make it necessary to employ line-by-line models for data reduction. If, however, the integrated signals over a relatively wide spectral interval are measured, then one could employ an appropriate band model. The line models usually employed in the study of atmospheric radiation are Lorentz, Doppler, and combined Lorentz-Doppler (Voigt) line profiles. A complete formulation (and comparison) of the transmittance (and absorptance) by these lines, in an infinite and finite spectral interval, is given in [4-6]. The most appropriate band model for atmospheric application is the quasi-random model which is discussed in detail in this report.

Ludwig et al. [3] have explored the possibilities of measuring the amount of atmospheric pollutants through remote sensing. An important method of measuring the pollutant concentration by remote sensing is the passive mode (also called the nadir experiment) in which the earth-oriented detector receives the upwelling atmospheric radiation. The near infrared region is particularly suitable for passive mode measurements simply because the radiation in this region is practically free from the scattering effects. Radiation in the visible and ultra-violet regions is severely affected by the scattering processes which make meaningful passive mode measurements impossible.
The purpose of this study is to present a comprehensive analysis procedure for calculating the atmospheric transmittance and upwelling radiance in the wave number interval of CO fundamental band (between 2070 and 2220 cm\(^{-1}\)). For this purpose computer programs were developed by employing the Lorentz line-by-line model as well as the quasi-random narrow band model. The basic equations for calculating the upwelling atmospheric radiance are presented in Sec. II. The theoretical formulations of the transmittance by the two spectral models is given in Sec. III. Listings of the computer programs are provided in the Appendicies. By employing the line-by-line and quasi-random computer programs, model calculations were made to study the effects of different interfering molecules, water vapor profiles, ground temperatures, and ground emittances on the upwelling radiance. These are presented in Sec. IV.
II. UPWELLING ATMOSPHERIC RADIATION

As shown in Fig. 2.1, the radiation emergent from the atmosphere, \( E(\omega) \), may be given by the expression [3,5]

\[
E(\omega) = E_G(\omega) + E_R(\omega) + E_\phi(\omega) + E_{R\phi}(\omega)
\]  

(2.1)

where

- \( E_G(\omega) \) = thermal radiation emitted by underlying surface and atmosphere
- \( E_R(\omega) \) = incident solar radiation reflected by the surface
- \( E_\phi(\omega) \) = radiation scattered by single or multiple scattering processes in the atmosphere without having been reflected from the surface
- \( E_{R\phi}(\omega) \) = scattered energy which has undergone a reflection from the surface.

In general, these quantities are functions of surface temperature, atmospheric temperature, surface emittance, surface reflectance, sun zenith angle, scattering characteristics of particles, and transmittance of the atmosphere.

In the spectral region of infrared measurements, the effect of scattering is negligible. The incident solar radiation reflected by the surface, however, is important especially if the surface reflectance is assumed to be high (0.2 and higher).

Upon neglecting the scattering and solar radiation, the expression for thermal radiation emerging from a plane-parallel atmosphere can be written as
Fig. 2.1 Radiative energy received by an aircraft or satellite-mounted instrument
\[ E(\omega) = E_G(\omega) = \varepsilon(\omega) \, B(\omega, T_s) \, \tau(\omega, \theta) \]
\[ + \int_0^h B(\omega, T(z)) \left[ d\tau(\omega, z)/dz \right] dz \]  
\[ (2.2) \]

where \( \varepsilon(\omega) \) is the surface emittance, \( B(\omega, T) \) is the Planck's blackbody function, \( T_s \) is the surface temperature, \( T(z) \) is the temperature at altitude \( z \), and \( \tau(\omega, z) \) is the monochromatic transmittance of the atmosphere. The first term on the right hand side of this equation represents the radiation from the surface, while the second term is the radiation from the atmosphere.

The contribution from sunlight reflected from the surface becomes significant at shorter wavelengths. This contribution is given by the component \( E_R(\omega) \) as
\[ E_R(\omega) = (1/\pi)[1 - \varepsilon(\omega)] \cos \theta \, H_s(\omega) [\tau(\omega)] \zeta \]  
\[ (2.3) \]

where \( \theta \) is the sun zenith angle and \( \zeta = 1 + f(\theta) \). Function \( f(\theta) = \sec \theta \) for \( 0 < \theta \leq 60^\circ \) and equals to \( C\theta \) for \( \theta > 60^\circ \), with \( C\theta \) denoting the Chapman function. \( H_s(\omega) \) is the sun irradiance on top of the atmosphere, and \( \tau(\omega) \) is the transmission vertically through the atmosphere.

The expression for the transmittance \( \tau(\omega, z) \) is obtained by employing an appropriate molecular (band or line) model, and, in general, this can be written as
\[ \tau(\omega, z) = \prod_i [\tau_i(\omega, z)] = \exp\left[ - \int_0^z \sum_i \beta_i(\omega, z') \, n_i(z') \, dz' \right] \]
\[ = \exp\left[ - \int_0^z \sum_i \beta_i(\omega, z') \, C_i(z') \, P(z') \, dz' \right] \]  
\[ (2.4) \]
where \( \beta_i(w,z) \) is the extinction coefficient for species \( i \) (which is equal to the sum of absorption and scattering coefficients), \( n_i(z) \) is the number density of the contributing molecules of species \( i \) in the optical path, \( C_i(z) \) is the concentration of species \( i \), and \( P_t(z) \) is the total pressure. If scattering is neglected, then atmospheric transmittance can be expressed in a convenient form as

\[
\tau(w,z) = \prod_i [\tau_i(w,z)] = \exp\left[-\int_0^x \sum_i \kappa_i^m(w,x') \rho_i(x') \, dx'\right] \tag{2.5}
\]

where \( \kappa_i^m(w,x') \) is the mass absorption coefficient for the \( i \)th absorbing gas, \( \rho_i \) is the mass density, and \( x \) is the depth of the level measured from the top of the atmosphere.

Upon introducing new definitions for the absorption coefficient and path length as [7,8]

\[
\kappa(w) = \kappa^m(w) \left(\rho_z / \rho_g\right) \tag{2.6}
\]

\[
du = \rho_g \left(\rho_z / \rho_g\right) \, dx \tag{2.7}
\]

Eq. (2.5) can be transformed into an alternate form as

\[
\tau(w,z) = \exp\left[-\int_0^u \sum_i \kappa_i(w) \, du_i\right] \tag{2.8}
\]

where \( \rho_g \) is the partial pressure and \( \rho_z \) is the mass density of the absorber, \( u \) is the optical path length in cm atm, and \( \rho_z \) is the absorber density corresponding to reference conditions (usually chosen as STP).

A combination of Eqs. (2.2) and (2.8) yields a relation for thermal radiation emerging from a plane-parallel atmosphere. This equation, with appropriate spectroscopic information, is used to obtain the concentration of
atmospheric pollutants from radiation measurements provided other governing parameters are known.

In actual calculations of atmospheric transmittance, the nonhomogeneous atmosphere is divided into a number of layers and for each layer an average value of pressure and temperature is assumed. With reference to Eq. (2.7), the pressure path length for each layer can be written as

\[ du_{ij} = Q_{ij} \left( \frac{P_j}{P_{NTP}} \right) \left( \frac{T_{NTP}}{T_j} \right) dx_j \]  

(2.9)

where \( Q_{ij} \) is the volume mixing ratio of the \( i \)th constituent in the \( j \)th layer, \( dx_j \) is the thickness of the \( j \)th layer, and \( P_j \) and \( T_j \) are the average pressure and temperature of the \( j \)th layer. Since the line intensity depends upon temperature and the line-width on temperature and pressure both, the absorption coefficient will be slightly different for different layers. Equation (2.8) can, therefore, be written as

\[ \tau(\omega, z) = \exp \left[ - \int_0^h \sum_j \sum_i \kappa_{ij}(\omega) du_{ij} \right] \]  

(2.10)

where \( \sum_j \) indicates the summation over all the layers between the top and level \( z \).

In general, the absorption coefficient for a single line centered at the wave number \( \omega_n \) is given by

\[ \kappa_{\omega_n} = S_n f_n(\omega, \gamma_n) \]  

(2.11)

where \( S_n \) is the intensity of the \( n \)th spectral line and is given by

\[ S_n = \int_{\omega_\text{min}}^{\infty} \kappa_{\omega_n} d(\omega-\omega_n) \]  

(2.12)
The line intensity may be described in terms of the molecular number density and Einstein coefficients, i.e., it depends upon the transition probabilities between the initial and final states and upon the populations of these states. For a perfect gas it may be shown that $S_n$ is a function solely of temperature. The quantity $f_n(\omega, \gamma_n)$ is the line shape factor for the $n$th spectral line. It is a function of the wave number $\omega$ and the line half width $\gamma_n$ and is normalized on $(\omega-\omega_n)$ such that

$$\int_{-\infty}^{\infty} f_n(\omega-\omega_n) d(\omega-\omega_n) = 1 .$$

(2.13)

Several approximate line profiles have been described in the literature. Most commonly used profiles are rectangular, triangular, Lorentz, Doppler, or Voigt (combined Lorentz and Doppler) profiles. Lorentz, Doppler, and Voigt profiles are of special interest in the atmospheric studies and these are discussed in detail in [4,6].

As indicated in Refs. [4,5,9], use of the Lorentz line profile is justified for radiative transfer analyses in earth's lower atmosphere. The shape factor, $f_n$, for the $n$th rotational Lorentz line is such that the absorption coefficient for species $i$ can be written from Eq. (2.11) as

$$(\kappa_{ij})_n = S_n f_n(\omega, \gamma_n) = S_n \gamma_n / \{\pi[(\omega-\omega_n)^2 + \gamma_n^2]\} .$$

(2.14)

It should be emphasized here that the units for the absorption coefficient and the pressure path length, in Eqs. (2.6) and (2.7), are $cm^{-1} \cdot atm^{-1}$ and $cm \cdot atm$ respectively. In the case of water vapor, however, the path length is expressed in precipitable centimeters (pr - cm) and the corresponding absorption coefficient in (pr - cm)$^{-1}$.
The total atmospheric transmittance is obtained by combining Eqs. (2.10) and (2.11) and integrating the resulting expression over the spectral range of interest. The exact procedure for calculating this, by employing the line-by-line and quasi-random band models, is discussed in the next section.

The total energy emergent from the atmosphere is obtained by integrating either Eq. (2.1) or (2.2) over the specified spectral interval $\Delta \omega$ as

$$E_D = E_{\Delta \omega} = \int_{\Delta \omega} E(\omega) \, d\omega$$  \hspace{1cm} (2.15)

The procedure for calculating the upwelling radianace, by employing the line-by-line and quasi-random band model for the transmittance, is briefly discussed in Sec.IV.
III. EVALUATION OF ATMOSPHERIC TRANSMITTANCE

As pointed out earlier, an accurate model for the spectral absorption coefficient is essential in the calculation of atmospheric transmittance and in the correct formulation of the radiative flux equations which are used in the reduction of data obtained from either direct or remote measurements. While use of line-by-line models is essential in the data reduction of high spectral resolution measurements, an appropriate band model could be employed if integrated signals are measured over relatively wide spectral intervals. Several line-by-line and band models are available in the literature. In this section, the procedure for obtaining the atmospheric transmittance by employing the line-by-line model and the quasi-random band model is discussed.

3.1 Direct Integration (Line-By-Line Model)

A computer program has been developed to determine the atmospheric transmittance by employing the Lorentz line-by-line model. The procedure for computing the transmittance is presented here and a listing of the program is given in Appendix B. Explanation of the symbols used in the computer program is given in Appendix A. The procedure can easily be extended to incorporate other line profiles.

The direct integration method consists of calculating the absorption coefficient, and then the transmittance, at a large number of frequencies within the spectral range of interest. Since the absorption coefficient is a highly varying function of the frequency (varying by orders of magnitude over the width of a single line, which is often less than 1 cm$^{-1}$), it has to be evaluated at very closely spaced locations. The total absorption coefficient at any frequency location is made up of contributions from a large number of lines in the vicinity of that frequency. Some molecules
have thousands of lines in the spectral range of a particular band and the contribution from each one of these lines should be evaluated at each frequency location. It is, therefore, evident that the evaluation of the atmospheric transmittance with high accuracy is a time consuming task.

Since the absorption coefficient varies rapidly only in the vicinity of the line center, it should be evaluated at very close intervals near the line centers, while away from the line centers bigger intervals could be used without any serious loss of accuracy. Kunde and Maguire \[8\] and Drayson \[9\] have proposed a scheme for selecting the frequency locations for the calculation of absorption coefficients and transmittances. The scheme essentially consists of numerically evaluating the average transmittance over a narrow spectral interval by employing the Legendre-Gauss quadrature formula \[10\]. The scheme employed in the present study is a modified form of the formulation presented in \[8,9\] where a different set of parameters are used. The choice of the parameters and the basic features of the computational scheme is discussed in the following subsections.

3.1.1 Spectral Divisions into Intervals and Subintervals

The entire frequency range of interest (usually the spectral interval of a particular vibration-rotation band) is first divided into a large number of rather narrow intervals $\Delta \omega$. Each of these $\Delta \omega$ intervals is then divided into a variable number $k$ of subintervals depending upon the number of lines falling in that interval. The arrangements of spectral divisions are illustrated in Fig. 3.1. Two very narrow subintervals are created on each side of the line center and these are denoted in the computer program by ALX (see Appendix B). As shown in Fig. 3.1, an interval $\Delta \omega$ remains one subinterval if no line is present, but is divided into 6 or 11 subintervals in the presence of one or two lines respectively. For greater
Fig. 3.1 Variable number of subintervals in a narrow interval $\Delta \omega$. 

(a) NO LINE (4 mesh points)

(b) ONE LINE (24 mesh points)

(c) TWO LINES (44 mesh points)
number of lines in the interval $\Delta \omega$, the number of subintervals will also be greater. Four frequency locations are then obtained within each subinterval by using the relation

$$\omega_{k\ell} = \left[\frac{(\omega_{B_k} - \omega_{A_k})}{2}\right] x_{\ell} + \frac{(\omega_{B_k} + \omega_{A_k})}{2}, \quad (3.1)$$

where $k$ refers to the $k$th subinterval $\omega_{B_k}$ and $\omega_{A_k}$ are the upper and lower frequency limits of the subinterval respectively, and $x_{\ell}$ are the abscissa values for the four point Gauss-Legendre quadrature formula [10].

3.1.2 Evaluation of Absorption Coefficients

The resultant magnitude of the absorption coefficient at the wave number location $\omega_{k\ell}$ is due to two separate contributions; (a) direct contribution and (b) wing contribution and is given by the equation

$$\kappa(\omega_{k\ell}) = \kappa^D(\omega_{k\ell}) + \kappa^W(\omega_{k\ell}), \quad (3.2)$$

The contribution to the absorption coefficient from lines whose centers lie in close vicinity (on both sides) of the wave number under consideration is called the direct contribution and is obtained for Lorentz lines from Eq. (2.14) as

$$\kappa^D(\omega_{k\ell}) = \sum_n \kappa_n(\omega_{k\ell}) = \sum_n \left(\frac{S_n \gamma_n}{\pi(\omega-n)^2 + \gamma_n^2}\right) \quad (3.3)$$

where $\omega_n$ refers to the center of the $n$th contributing line. In the computer program, the range of direct contribution is denoted by DLIM. Thus, if $|\omega - \omega_n| \leq \text{DLIM}$, the contribution is called the direct contribution and is evaluated by using Eq. (3.3).

The wing contribution to $\kappa(\omega_{k\ell})$ arises from lines located at wave numbers farther than DLIM from $\omega_{k\ell}$ (on both sides). The wave number range of the
wing contribution is denoted by WLIM and the absorption coefficient for this range is calculated from the equation

\[ \kappa^W(\omega_{kl}) = \sum_n \kappa_n(\omega_{kl}) = \sum_n \left\{ S_n \gamma_n / \left[ \pi (\omega - \omega_n)^2 \right] \right\}, \quad (3.4) \]

only for the interval \( DLIM < |(\omega - \omega_n)| < WLIM \). The contribution from the lines for which \( |(\omega - \omega_n)| > WLIM \) is found to be negligible. The range of WLIM is established by several trial calculations.

Since the number of lines between DLIM and WLIM (on each side) is very large, the wing contribution is not evaluated at each \( \omega_{kl} \) individually. Instead, it is evaluated at the boundaries and the center of an interval. The values at all the \( \omega_{kl} \)'s within that interval is obtained by linear interpolation. As pointed out by Drayson [9], this procedure does not affect the accuracy of the results seriously.

Since \( S_n \) varies with temperature and \( \gamma_n \) varies with temperature as well as pressure, the nonhomogeneous atmosphere is divided into appropriate numbers of homogeneous slabs for the purpose of calculating the absorption coefficients and the atmospheric transmittances. For each slab (or layer) an average value of the temperature and pressure is assumed.

3.1.3 Optical Thickness and Transmittance

The path length of each homogeneous slab of a nonhomogeneous atmosphere is evaluated separately. For any constituent, the path length for the jth layer is found from either Eq. (2.7) or Eq. (2.9) to be

\[ u_j = Q_j (P_j / P_{NTP}) (T_{NTP} / T_j) x_j, \quad (3.5) \]

where \( x_j \) is the thickness of the jth layer.

The optical thickness of the jth layer at the wave number \( \omega_{kl} \) is given by
\[ \kappa(\omega_{k\ell})_{ij} u_{ij}, \]  
and the total optical thickness for the atmosphere by
\[ \sum_j \kappa(\omega_{k\ell})_{ij} u_{ij}. \]  
For several absorbing species in the spectral range of interest, the total optical thickness is given by
\[ \sum_j \sum_i \kappa(\omega_{k\ell})_{ij} u_{ij}, \]  
where the summation over \( i \) constitutes the contribution of all the absorbing constituents.

The atmospheric transmittance at \( \omega_{k\ell} \) can now be expressed by
\[ T(\lambda_k) = \exp\{-\sum_j \sum_i \kappa(\omega_{k\ell})_{ij} u_{ij}\} \]  
where \( \kappa(\omega_{k\ell}) \) is given by Eq. (3.2).

The average transmittance over the interval \( \Delta\omega \) is obtained from the equation
\[ \tau(\Delta\omega) = \{\sum_{k=1}^k [(\omega_{k-1} - \omega_{k-1})/2][\sum_{\ell=1}^\ell w_{\ell} \tau(\omega_{k\ell})]/\Delta\omega \]  
where the summation \( k \) extends over all the subintervals within the interval \( \Delta\omega \), and \( w_{\ell} \)'s are the weight factors for the four point Gauss-Legendre quadrature formula [10].

3.1.4 Optimization of Spectral Parameters

The spectral parameters (such as \( \Delta\omega \), ALX, DLIM, WLIM, etc.) entering in the numerical calculation of atmospheric transmittance are optimized for accuracy and for saving the computational time. Various
parameters are carefully chosen on the basis of considerable numerical experimentation. In a particular numerical scheme for calculation of the atmospheric transmittance, the choice of an optimized spectral parameter may slightly depend on the nature of the molecules under consideration (i.e. on the spectral distribution of the rotational lines). For the present study, spectral parameters were optimized by considering the CO spectral lines in the region 2070–2220 cm\(^{-1}\) and by assuming a uniform CO distribution of one part per million (1 ppm) by volume in the atmosphere from zero to ten kilometers.

As pointed out earlier, the entire spectral range of interest is first divided into a large number of narrow intervals \(\Delta \omega\)'s. In the computer program, this parameter is denoted by DEL (see Appendix B). By employing Eq. (3.10), the transmittance values were calculated for \(\Delta \omega = \text{DEL} = 2.0, 1.0, \text{and} 0.5 \text{ cm}^{-1}\). These are given in Table 3.1. It is seen that while the transmittance increases by about 0.1% when DEL decreases from 2.0 to 1.0 cm\(^{-1}\), it decreases by about 0.03% when DEL goes from 1.0 to 0.5 cm\(^{-1}\). This variation being significantly small, the intermediate value of \(\Delta \omega = \text{DEL} = 1.0 \text{ cm}^{-1}\) is chosen for the present study as opposed to the value of \(\Delta \omega = 0.1 \text{ cm}^{-1}\) used by Kunde and Maguire [8].

The effect of varying the width of the subintervals near the line centers (denoted by ALX in the computer program) was also studied by numerical experimentation. Average transmittance values were calculated for \(\text{ALX} = 0.04, 0.02, \text{and} 0.01 \text{ cm}^{-1}\) and these are listed in Table 3.1. Since there is no effect of changing the ALX values on the transmittance, a value of \(\text{ALX} = 0.03 \text{ cm}^{-1}\) was selected simply because the subintervals on each side of the line center will cover a relatively larger portion of the important part of the line profile.
The effect of changing the value of DLIM on the average transmittance was found to be insignificant (see Table 3.1) and a value of DLIM = 5.5 cm\(^{-1}\) was selected for the present study in order to save computational time. The effect of changing the WLIM values was, however, found to be significant and a value of WLIM = 45.5 cm\(^{-1}\) was adapted. This value of WLIM maintains the general accuracy of the program and provides savings of computational time. It was not necessary to consider a WLIM value beyond 45.5 cm\(^{-1}\) in view of the expected small gain in accuracy.

**TABLE 3.1**

Average Atmospheric Transmittance from CO Fundamental Band as a Function of Various Spectral Parameters.

<table>
<thead>
<tr>
<th>Spectral Parameter</th>
<th>Spectral Parameter Range (cm(^{-1}))</th>
<th>Average Transmittance (nondimensional)</th>
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<tbody>
<tr>
<td>DEL</td>
<td>2.0</td>
<td>0.79605</td>
</tr>
<tr>
<td></td>
<td>1.0</td>
<td>0.79678</td>
</tr>
<tr>
<td></td>
<td>0.5</td>
<td>0.79655</td>
</tr>
<tr>
<td>ALX</td>
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<td>0.79678</td>
</tr>
<tr>
<td></td>
<td>0.02</td>
<td>0.79678</td>
</tr>
<tr>
<td></td>
<td>0.01</td>
<td>0.79678</td>
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<td>DLIM</td>
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<tr>
<td></td>
<td>25.5</td>
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<tr>
<td>WLIM</td>
<td>35.5</td>
<td>0.79655</td>
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<td></td>
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</tbody>
</table>
In the literature [1-3], individual line widths are available for CO and H$_2$O lines while only the average values are available for CO$_2$, N$_2$O, and O$_3$ lines. For CO and H$_2$O, model calculations indicate that the mean transmittances obtained by using the average line widths are different than those obtained by using the individual line widths. For CO, a value of average transmittance of 0.83282 was obtained by using the average line widths while a value of 0.82834 was obtained when individual line widths were used. Similarly for H$_2$O, a value of $\bar{\tau}$ of 0.85563 was obtained for average line widths while a value of 0.86948 was obtained for individual line widths. In the results of model calculations (reported in the next section), individual line widths were used for CO and H$_2$O lines.

The computer program listed in Appendix B calculates the atmospheric transmittance in the spectral 2070-2220 cm$^{-1}$. This is the range of CO fundamental band. The program accounts for the contribution of the interfering molecules such as H$_2$O, CO$_2$, N$_2$O, and O$_3$. The program can easily be modified to calculate the atmospheric transmittance in any spectral range.
3.2 Quasi-Random Band Model

The use of narrow band models (such as Elsasser, statistical, random-Elsasser, and quasi-random) is justified if integrated signals are measured over relatively wide spectral intervals. The use of these models in transmittance calculations results in a considerable reduction in computational time. The results obtained from most of these models, however, usually lack the high accuracy needed in atmospheric transmittance calculations. The quasi-random model, introduced by Wyatt; Stull, and Plass [11], is probably the best model to represent the absorption of a vibration-rotation band quite accurately. Discussions on various band models are available in the literature [12-15]. The procedure for calculating the atmospheric transmittance by employing the quasi-random band model is discussed here in detail. A listing of the computer program is given in Appendix C and various symbols used in the program are explained in Appendix A.

The fundamental features of the quasi-random band model are discussed in references [7,11]. For this model, the entire band span, $\Delta$, is divided into a number of small subintervals of equal spectral width $\delta$. The average transmittance is first evaluated for each $\delta$ subinterval. The lines within each subinterval are assumed to be distributed randomly. The average transmittance over the entire spectral range (i.e., over the band pass) is obtained by arithmetically averaging of the transmittances of all subintervals.

The lines in a particular subinterval $\delta$ are divided into intensity subgroups. Reckoning from the intensity of the strongest line, five intensity groups (each spanning one decade) are created. Thus, lines whose intensities are within $10^{-5}$ times the intensity of the strongest line (in that group) are taken into consideration. It was suggested in [11] that the contribution from still weaker lines is negligible.
Since the line positions and intensities are assumed to vary within the narrow subintervals $\delta$ (rather than the entire band pass $\Lambda$), the results obtained from this model are expected to be better than other band models.

3.2.1 Evaluation of Average Transmittance

For a homogeneous path, the spectral transmittance at $\omega$ due to a line with center at $\omega_n$ is obtained by combining Eqs. (2.8) and (2.11) as

$$\tau(\omega) = \exp[-S_n \, u \, f_n(\omega, \gamma_n)] = \exp[-S_n \, u \, f(\omega, \omega_n)]$$

(3.11)

where the shape factor $f(\omega, \omega_n)$ for the Lorentz line profile is defined in Eq. (2.14).

For theoretical line shapes (i.e., for Lorentz, Doppler, and Voigt lines) the location of $\omega$ is symmetrical with respect to $\omega_n$. Thus, the average transmittance of a line over $\delta$ can be evaluated in two ways:

(a) keep $\omega_n$ at its fixed location and average $\tau(\omega)$ for location of $\omega$ varying over $\delta$, (b) keep $\omega$ fixed at the center of the subinterval and average $\tau(\omega)$ for location of $\omega_n$ varying over $\delta$. The second approach is adapted in the calculation of the average transmittance while using the quasi-random band model.

The average transmittance over $\delta$ due to a single spectral line may, therefore, be expressed by

$$\tau_n(\omega) = \frac{1}{\delta} \int_{\delta} \exp[-S_n \, u \, f(\omega, \omega_n)] \, d\omega_n$$

(3.12)

where it should be noted that $\omega_n$ is the variable of integration.

If $N$ is the number of lines in an intensity decade then the average transmittance due to all the lines in that decade, $\tau_d$, is given by
\[
\tau_d(\omega) = \frac{1}{6} \int_6 \exp\left[-\bar{S}_n u f(\omega, \omega_n)\right] d\omega_n^N,
\]

where \( \bar{S}_n \) is the average intensity of all the lines within the decade under consideration. It is assumed that the range of intensity in a decade is not large enough to cause any serious errors because of intensity averaging. A considerable saving in computational time is realized if the number of lines in each intensity decade is large.

The average transmittance due to all lines in the five intensity decades of the subinterval \( \delta \) is given by

\[
\tau_k(\omega) = \frac{5}{6} \int_6 \tau_d(\omega) = \frac{5}{6} \int_6 \exp\left[-\bar{S}_n u f(\omega, \omega_n)\right] d\omega_n^N, \quad (3.13)
\]

where subscript \( k \) represents the \( k \)th spectral subinterval (i.e., \( \delta_k \)) of the total spectral interval \( \Delta \).

Equation (3.13) represents the transmittance due to the lines within \( \delta_k \). The wings of the lines in the adjacent subintervals also make a significant contribution to the absorption in \( \delta_k \). The resultant transmittance over the subinterval \( \delta_k \), therefore, is given by

\[
\tau_k(\omega) = \tau_{k-k}(\omega) \prod_{j=1}^{k} \tau_{k-j}(\omega), \quad (3.14)
\]

where \( \tau_{k-j}(\omega) \) represents the transmittance in \( \delta_k \) due to lines in \( \delta_j \).

Large variations are observed between the transmittances of adjacent subintervals if the above procedure is employed directly. Wyatt, Stull and Plass [11] attributed this to the arbitrary locations of the subinterval boundaries and the resulting arbitrary distribution of lines between the subintervals. This spurious variation in transmittances is smoothed out by adapting the following procedure. (a) Divide the total spectral range \( \Delta \)
(starting at $A_0$) into $K$ subintervals with boundaries at $A_0, A_0 + \delta$, $A_0 + 2\delta$, $\ldots$, $A_0 + k\delta$ and centers at $A_0 + \frac{1}{2}\delta$, $A_0 + \frac{3}{2}\delta$, $\ldots$ etc. Evaluate transmittances at the centers, i.e. at $A_0 + \frac{1}{2}\delta$, $A_0 + \frac{3}{2}\delta$, $\ldots$ etc.

(b) Shift the spectral mesh of subintervals by $\delta/2$. The subinterval centers now lie at $A_0$, $A_0 + \delta$, $A_0 + 2\delta$, $\ldots$, etc. Evaluate transmittances at these shifted spectral locations. The resultant transmittances at the centers of original set of subintervals are obtained from these two sets by using the three point sliding average procedure. For subinterval between $A_0$ and $A_0 + \delta$, the resultant transmittance at the center $A_c = A_0 + \delta/2$ is given by

$$\overline{\tau}_k(A_c) = \frac{1}{3}\left[\tau_k(A_0) + \tau_k(A_c) + \tau_k(A_0 + \delta)\right].$$

(3.15)

The average transmittance for the entire range $\Delta$ is now expressed by

$$\overline{\tau}(\Delta) = \frac{1}{K} \sum_{k=1}^{K} \overline{\tau}_k(\omega) = \frac{1}{K} \sum_{k=1}^{K} \overline{\tau}_k(A_c).$$

(3.16)

From the above description, it is evident that the basic quantity to be evaluated is the average transmittance due to a single line over the subinterval $\delta$. This is given by Eq. (3.12). Upon introducing the following change of variables

$$y = \omega_n - \omega_0 - \delta/2,$$

$$z = \omega - \omega_0 - \delta/2,$$

$$\xi_n = \frac{\pi_n u}{\gamma_n},$$

$$\rho = 2\gamma_n/\delta,$$

$$\eta = 2y/\delta,$$

$$\varepsilon = 2z/\delta,$$

(3.17)
Eq. (3.12) can be expressed for the Lorentz line shape as
\[
\tau_n(\omega) = \frac{1}{2} \int_{-1}^{1} \exp\left[-\rho^2 \xi_n / \left( (\xi - \eta)^2 + \rho^2 \right) \right] \, d\eta .
\] (3.18)

For direct contribution (i.e., contribution to the transmittance due to lines in the same subinterval), \( \xi = 0 \) and the integrand in Eq. (3.18) is symmetrical about \( \eta = 0 \). For this case, Eq. (3.18) reduces to
\[
\tau_n(\omega) = \int_{0}^{1} \exp\left[-\rho^2 \xi_n / (\eta^2 + \rho^2) \right] \, d\eta .
\] (3.19)

For evaluating the wing contribution, it is assumed that \( \rho^2 \ll (\xi - \eta)^2 \), and Eq. (3.18) reduces to
\[
\tau_n(\omega) = \frac{1}{2} \int_{-1}^{1} \exp\left[-\rho^2 \xi_n / (\xi - \eta)^2 \right] \, d\eta .
\] (3.20)

The numerical procedures used for evaluating the integrals in Eqs. (3.19) and (3.20) are discussed in the next subsection.

3.2.2 Optimization of Integration Procedure and Parameters

The integrand in Eq. (3.19) is a strong function of \( \eta \) and, therefore, an accurate procedure for evaluating the integral is required. Wyatt, Stull and Plass [11] have obtained an analytical solution of Eq. (3.19). Following the procedure suggested by Young [16], Kunde [7] divided the range of integration (0-1) into seven subintervals as
\[
\eta = 0.0, 0.001, 0.005, 0.01, 0.05, 0.1, 0.5, 1.0 ,
\]
and used an eight point Gauss-Legendre quadrature formula for each subinterval.

In the present work, a much simpler scheme was used to evaluate Eq. (3.19). Twenty-six abscissa points were chosen in the interval (0-1) and suitable subintervals around them were created by a graphical experiment. Table 3.2 lists the abscissa values and the subintervals associated with them. The
The integrand is evaluated at the twenty-six abscissa points, multiplied by the corresponding subinterval width, and the results are then summed. A comparison of results of this procedure with the results of ten subinterval ten-point Gauss-Legendre quadrature formula (for the same interval) revealed excellent agreement. It is, therefore, concluded that this procedure yields results of high accuracy.

The integrand in Eq. (3.20) is a slow varying function of $\eta$. Thus, a simple twenty-one point Simpson's rule quadrature formula was used to evaluate the integral instead of a ten-point Gauss-Legendre quadrature formula suggested by Kunde [7]. Accuracy checks were made on this quadrature scheme, and no appreciable differences were observed.

It should be emphasized here that the use of these simple quadrature schemes results in considerable reduction in computational time.

**TABLE 3.2**

Abscissa Points and Subintervals Selected to Evaluate the Direct Contribution.

<table>
<thead>
<tr>
<th>Abscissa</th>
<th>Subinterval</th>
<th>Abscissa</th>
<th>Subinterval</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.0</td>
<td>0.0006</td>
<td>0.04</td>
<td>0.01</td>
</tr>
<tr>
<td>0.001</td>
<td>0.0006</td>
<td>0.05</td>
<td>0.01</td>
</tr>
<tr>
<td>0.0015</td>
<td>0.0006</td>
<td>0.06</td>
<td>0.015</td>
</tr>
<tr>
<td>0.002</td>
<td>0.0007</td>
<td>0.08</td>
<td>0.02</td>
</tr>
<tr>
<td>0.003</td>
<td>0.001</td>
<td>0.10</td>
<td>0.03</td>
</tr>
<tr>
<td>0.004</td>
<td>0.001</td>
<td>0.15</td>
<td>0.05</td>
</tr>
<tr>
<td>0.005</td>
<td>0.001</td>
<td>0.20</td>
<td>0.08</td>
</tr>
<tr>
<td>0.006</td>
<td>0.0015</td>
<td>0.30</td>
<td>0.10</td>
</tr>
<tr>
<td>0.008</td>
<td>0.002</td>
<td>0.40</td>
<td>0.10</td>
</tr>
<tr>
<td>0.01</td>
<td>0.003</td>
<td>0.50</td>
<td>0.10</td>
</tr>
<tr>
<td>0.015</td>
<td>0.005</td>
<td>0.60</td>
<td>0.15</td>
</tr>
<tr>
<td>0.02</td>
<td>0.008</td>
<td>0.80</td>
<td>0.20</td>
</tr>
<tr>
<td>0.03</td>
<td>0.01</td>
<td>1.00</td>
<td>0.10</td>
</tr>
</tbody>
</table>
The optimization of the computational parameters was carried out in a separate study by considering the CO spectral lines in the region 2070–2220 cm\(^{-1}\) and by assuming a uniform CO distribution of one part per million by volume.

Computations were made for four different values of the subinterval size, \(\delta\). This is denoted in the computer program by \(\text{DEL}\) (see Appendix C). Average transmittances obtained for the entire range of CO fundamental band (between 2070–2220 cm\(^{-1}\)) are shown in Table 3.3 for the four subinterval sizes. An attempt was also made to compute the transmittance for \(\text{DEL} = 3\) cm\(^{-1}\) but was eventually abandoned as the computational cost became too large. A value of \(\text{DEL} = 6\) cm\(^{-1}\) was adapted for the present study simply because of the cost considerations. It was not considered necessary to go to even lower values of \(\delta\) in order to gain slight accuracy at higher cost.

The number of adjacent subintervals (on each side of the main subinterval) contributing to the wing effects were also investigated. The results shown in Table 3.3 indicate that consideration of seven subintervals on each side yields sufficiently accurate results. It was not necessary to consider the influence of all neighboring subintervals in order to gain slight improvement (<0.02%) in the final result.

Since averaging of the line widths over each decade in every subinterval is unavoidable (because of the approximations in the basic formulation of the band model), no attempt was made to consider the individual line widths even for CO and H\(_2\)O lines. Average line widths for these molecules were found to have 10–15% standard deviation. The effect of using the average line widths on the overall transmittance is expected to be minimal.
**TABLE 3.3**

Average CO Fundamental Band Transmittance as a Function of Various Quasi-Random Band Model Computational Parameters

<table>
<thead>
<tr>
<th>Parameters</th>
<th>Range</th>
<th>Average Transmittance (nondimensional)</th>
</tr>
</thead>
<tbody>
<tr>
<td>DEL (cm⁻¹)</td>
<td>15</td>
<td>0.81664</td>
</tr>
<tr>
<td></td>
<td>10</td>
<td>0.81523</td>
</tr>
<tr>
<td></td>
<td>6</td>
<td>0.81183</td>
</tr>
<tr>
<td></td>
<td>5</td>
<td>0.81050</td>
</tr>
<tr>
<td>Number of Intervals</td>
<td>4</td>
<td>0.81225</td>
</tr>
<tr>
<td></td>
<td>7</td>
<td>0.81198</td>
</tr>
<tr>
<td></td>
<td>8</td>
<td>0.81194</td>
</tr>
<tr>
<td></td>
<td>10</td>
<td>0.81190</td>
</tr>
<tr>
<td></td>
<td>all</td>
<td>0.81183</td>
</tr>
</tbody>
</table>
IV. MODEL CALCULATIONS

In order to establish the feasibility of measuring the average concentration of pollutants in the atmosphere (either from an aircraft mounted instrument or from satellites), it is essential to perform model calculations to evaluate upwelling radiance and signal change under physically realistic conditions. By using the appropriate line parameters and employing the Lorentz line-by-line model and quasi-random band model, upwelling radiance (and signal change) calculations were made in the spectral range of CO fundamental band (2070-2220 cm\(^{-1}\)). Results were obtained to study the effects of different interfering molecules, water vapor profiles, ground temperatures, and ground emittances on the upwelling radiance and the signal change. In this section, the procedure for calculating the upwelling radiance and signal change is briefly discussed, information regarding data sources is provided, and finally, the discussions of various results are presented.

4.1 Procedure for Calculating the Upwelling Radiance and Signal Change

In radiation modeling for pollution measurement in a nonhomogeneous atmosphere, the upwelling radiation is calculated by dividing the atmosphere into an appropriate number of sublayers. Each sublayer is assumed to be homogeneous in species concentration, temperature and pressure.

In a specified spectral interval in which a particular pollutant absorbs, the total energy emergent from the atmosphere is obtained from Eq.(2.15). If in this interval, \( n \) independent measurements (corresponding to the number of homogeneous layers) could be made to find \( E_{D1}, E_{D2}, \ldots, E_{Dn} \), then the uniform concentration of the pollutant in each layer (and therefore the concentration profile in the actual atmosphere) could be determined from Eq.(2.15). Because of low concentrations of pollutants in the atmosphere, however, \( n \) such measurements are not feasible. Thus, only one independent
measurement is usually made and an average value of the particular pollutant concentration in the atmosphere is obtained. Even if only one value of the pollutant concentration can be obtained from an independent measurement, it is essential to divide the nonhomogeneous atmosphere into several homogeneous layers for the purpose of data reduction. This is because the pressure, temperature, and amount of interfering molecules vary in the atmosphere, and spectroscopic parameters and pressure path lengths are strong functions of these variables.

By employing the Lorentz line-by-line model for atmospheric transmittance, the upwelling radiance at the top of the atmosphere is obtained from Eq. (2.15) for each narrow spectral interval \( \Delta \omega \). The exact procedure for doing this is to evaluate the average value of the Planck function for this interval first, then by using the mean value of the transmittance for the interval, Eq. (3.10), evaluate the upwelling radiance at the top of the atmosphere. The total upwelling radiance \( (E = \sum E_{\Delta \omega}) \) at the top of the atmosphere for the entire spectral range \( \Delta \) is obtained by summing the radiances of individual intervals. As pointed out earlier, for the present study the spectral range of interest is the range of CO fundamental band. The computer program for calculating the upwelling radiance in this spectral range is given in Appendix B.

By employing the quasi-random band model, the total upwelling radiance at the top of the atmosphere can be evaluated from Eq. (2.15) in the following two ways.

(a) First calculate the integrated Planck function for the entire spectral range \( \Delta \). Then by using the value of average transmittance for the range \( \Delta \), obtain the net (integrated) radiance at the top of the atmosphere.

(b) Obtain the net (integrated) radiance at the top of the atmosphere for
each subinterval by calculating the Planck function and the average transmittance for that subinterval. Obtain the total radiance for the entire range $\Delta$ by summing the integrated radiances of each subinterval.

For the spectral range of CO fundamental band, total radiances at the top of the atmosphere were obtained by employing the above two procedures and these are $2.8102 \ \text{E-05}$ and $2.8423 \ \text{E-05}$ respectively. Procedure (b) was adapted for the present work because of its correctness in the formulation logic. Also, results obtained by this procedure were found to be in good agreement with the line-by-line results. A further simplification was introduced in procedure (b) in the final version of the computer program. Planck functions were calculated at the center frequency of each subinterval. This value was used as a mean for the subinterval rather than calculating it by integration over each $\delta$. No difference in the final results was observed. This is because Planck function is a slow varying function of the frequency (especially within the spectral range of subinterval $\delta$).

The signal change $SC = \Delta E$ (in watts/cm²-sr) can be calculated by employing Eq.(2.15) as

$$SC = \Delta E = \int_{\Delta \omega} [E(\omega, \tau_o) - E(\omega, \tau_p)] d\omega,$$

(4.1)

where $\tau_o$ represents the transmittance of a "clean" atmosphere in which the pollutant concentration is zero, and $\tau_p$ refers to the transmittance of the atmosphere in the presence of the pollutant. The numerical procedure for evaluating Eq.(4.1) is identical to that described for calculating the upwelling atmospheric radiance.

4.2 Data and Data Sources

Upwelling radiances and signal change values were calculated in the spectral range of CO fundamental band. Contributions from the thermal
radiation and reflected sunlight terms in Eqs. (2.15) and (4.1) were taken into consideration while that from scattering terms were neglected. For the present study, the top of the atmosphere was considered to be 10 km which is approximately the top of the troposphere. For numerical calculations, this nonhomogeneous atmosphere was divided in 10 layers of equal thickness. The sun zenith angle was taken to be zero (overhead sun, $\theta = 0$) for all calculations.

The data used in the present work were obtained from a number of well known sources and are considered to be highly reliable.

The atmospheric temperature and pressure profiles were adapted from the U. S. Standard Atmosphere, 1962 [17]. Distributions of infrared active species, such as H$_2$O, CO$_2$, N$_2$O, and O$_3$ were taken from McClatchey et al. [18]. Rotational and vibrational partition functions, needed to account for the temperature dependence of line strengths, were obtained from McClatchey et al. [2]. Table 4.1 shows the range of variation of some of these parameters. Values of the parameters listed in the table refer to the conditions at the boundaries of each layer. Mean values of the parameters in each layer (corresponding to the values at layer centers) were used in actual calculations. Carbon dioxide and nitrous oxide are assumed to be uniformly mixed in the atmosphere. For these gases, average values for the concentration used in the calculations are: CO$_2$ = 330 ppmV, and N$_2$O = 0.28 ppmV.
Science Applications Incorporated (NASA-Contractor, responsible for the development of the non-dispersive correlation instrument for pollution measurement [3,19]) has compiled spectral line parameters (position, strength, width, and lower energy level) for lines of CO fundamental band and for lines of other molecules which interfere with the CO band. In the calculation of transmittances, these line parameters are directly read from a tape provided by SAI [19] to NASA-Langley.

Solar irradiances at the top of the atmosphere, at a few selected wave numbers, are also available from the SAI tape [19]. Values obtained from the tape, for the spectral range of present interest, are listed in Table 4.2. In the evaluation of contribution of the reflected solar radiation to the upwelling radiance, the solar irradiance for each spectral subinterval is obtained from a linear interpolation of values given in Table 4.2.
4.3 Results of Model Calculations

By employing the Lorentz line-by-line and quasi-random band model for atmospheric transmittance, upwelling radiance and signal change were calculated for several illustrative cases. As indicated before, all calculations were made for the spectral range of CO fundamental band.

The results of integrated upwelling radiance at the top of the troposphere (i.e., at 10 km.) for different CO concentrations (uniformly distributed through the troposphere), in the presence of various interfering molecules, are illustrated in Fig. 4.1. The solid curves represent the results of the line-by-line model and broken curves for the quasi-random band model. As would be expected, the upwelling radiance \( E \) decreases with increasing CO concentration and with the inclusion of different interfering molecules. Inclusion of \( O_3 \) causes a slight decrease in radiance (not exceeding 0.5%) and it was difficult to illustrate this decrease in Fig. 4.1. The agreement between the line-by-line and the quasi-random band model results is seen to be excellent for the case of \( CO + H_2O \). The slightly lower radiances for the next two cases is attributed to the over-estimation of absorption by the band model. The reason for this lies in the assumption of random distribution of many lines.
(in the presence of interfering molecules) in the subintervals of the band model. In the actual spectra, however, the lines are more closely spaced in some regions than in others. The reason for slightly higher radiance values, with the band model for the case of pure CO atmosphere (where relatively small number of lines are present), is not clear at this time. The variation in the signal change, $\Delta \varepsilon$, with the CO concentration is illustrated in Fig. 4.2. These results follow the general trend of the results presented in Fig. 4.1.

The influence of different amounts of water vapor on the upwelling radiance and the signal change is shown in Figs. 4.3 and 4.4 respectively. Increased water vapor concentration results in increased absorption in the atmosphere. This, in turn, results in lower values for upwelling radiance and signal change. It should be noted that the effect of CO concentration on the signal change would be relatively small in the presence of larger quantity of water vapor.

Figures 4.5 and 4.6 show the upwelling radiances and signal changes for surface temperatures of 280, 290, and 300 °K and a surface emittance of 0.8. The strong dependence of the upwelling radiance and signal change on the surface temperature is obvious from these results. The relatively lower radiance values obtained with the band model are indicative of slight overestimation of absorption by this model.

Figure 4.7 shows the variation of upwelling radiance for three different values of surface emittance and for a surface temperature of 288 °K. As explained earlier, the radiances obtained from the band model are lower than the line-by-line model because of overestimation of absorption by the band model. The relative increase of the difference for the lower $\varepsilon$-values is due to lower total emission from the earth for the small values of surface.
Fig. 4.1 Upwelling radiance as a function of CO concentration in the presence of interfering molecules, $T_s = 288 \text{K}$, $\varepsilon = 0.8$. 

\[ \text{CO} \]
\[ \text{CO} + \text{H}_2\text{O} \]
\[ \text{CO} + \text{H}_2\text{O} + \text{CO}_2 \]
\[ \text{CO} + \text{H}_2\text{O} + \text{CO}_2 + \text{N}_2\text{O} \]
Fig. 4.2 Signal change as a function of CO concentration in the presence of different interfering molecules, $T_s = 288^\circ K$, $\varepsilon = 0.8$. 
Fig. 4.3 Upwelling radiance as a function of CO concentration for different water vapor profiles, $T_s = 288^\circ K$, $\varepsilon = 0.8$. 

- w/o $H_2O$, WITHOUT WATER VAPOR
- $\frac{1}{2} H_2O$, HALF GUTNICK PROFILE
- $1 H_2O$, STANDARD GUTNICK
- $2 H_2O$, TWICE GUTNICK

![Graph showing upwelling radiance as a function of CO concentration for different water vapor profiles.]

CO CONCENTRATION (ppm by volume)
Fig. 4.4 Effects of water vapor concentration on the signal change $T_s = 288^\circ \text{K}, \varepsilon = 0.8$. 

0.40  
0.30  
0.20  
0.10  
0.00  

SIGNAL CHANGE, $\Delta E$ (10^{-5} \text{ watts cm}^{-2} \text{ sr}^{-1})

w/o H$_2$O, WITHOUT WATER VAPOR
1/2 H$_2$O, HALF GUTNICK PROFILE
1 H$_2$O, STANDARD GUTNICK
2 H$_2$O, TWICE GUTNICK

CO CONCENTRATION (ppm by volume)
Fig. 4.5 Upwelling radiance as a function of CO concentration for three different surface temperatures (surface emittance $\varepsilon = 0.8$).
Fig. 4.6 Signal change as a function of CO concentration for three different surface temperatures (surface emittance = 0.8).
emittance. In these cases, therefore, the increased absorption by the band model has a greater relative effect on the radiance. Figure 4.8 shows the signal change for the cases considered in Fig. 4.7 and the results indicate the same general trend.

Figure 4.9 shows the variation of the upwelling radiance with the surface temperature for a fixed concentration of CO (1 ppm by volume) in the atmosphere and for \( e = 0.8 \). The strong dependence of radiance on the surface temperature may be easily explained on the basis of the Stefan's law. However, because of the interference from the infrared active atmospheric molecules, the results obtained here do not exhibit an exact fourth power relationship.

Figure 4.10 shows the variation of radiance with the surface emittance for a fixed CO concentration (1 ppm by volume) and \( T_s = 288 \, ^\circ\text{K} \). As would be expected, the results indicate the linear dependence of radiance on the surface emittance. Similar results were obtained in reference [3] for different values of the surface temperature and the sun zenith angle. In general, the ground emittance varies with the wave number. However, for the spectral range of CO fundamental band, it was shown in reference [20] that the radiance is not influenced by a significant amount when the wave number dependent ground emittance is replaced by an averaged value.

Figure 4.11 shows a comparison of the results obtained from the present line-by-line program (given the name LINBLIN) and another line-by-line program (called POLAYER) developed by the Science Applications Inc. [19]. In computing the total absorption coefficient at any wave number, the present program considers contributions from all the lines up to a fixed wave number location (on both sides) of 45.5 cm\(^{-1}\) from the wave number under consideration. This value of 45.5 cm\(^{-1}\) for the so-called wing effect was chosen after several numerical experimentations. The POLAYER, on the other hand, considers the effect of a fixed number of 20 lines on each side of the wave number under
consideration. This causes the range of wing effect to change depending upon the density of lines in the spectrum. Thus, in some cases, POLAYER will not consider the influence of lines which are only 1 cm\(^{-1}\) away from the wave number under consideration. This, of course, will result in underestimation of absorption. This, at least in part, is responsible for the higher integrated radiance obtained from the POLAYER program. The difference between the signal change curves, shown in Fig. 4.12, follows from the difference in the radiance values.
Fig. 4.7 Upwelling radiance as a function of CO concentration for three different surface emittances, $T_s = 288^\circ K$. 

- **LINE BY LINE**
- **QUASI-RANDOM BAND**

RADIANCE, $E$ (10^{-5} \text{ watts cm}^{-2} \text{ sr}^{-1})$

CO CONCENTRATION (ppm by volume)
Fig. 4.8 Signal change as a function of CO concentration for three different surface emittances, $T_s = 288^\circ K$. 
Fig. 4.9 Upwelling radiance as a function of surface temperature for a fixed CO concentration (1 ppm by volume), \( \varepsilon = 0.8 \).
Fig. 4.10 Upwelling radiance as a function of surface emittance for a fixed CO concentration (1 ppm by volume), $T_s = 288^\circ$K.
Fig. 4.11 Comparison of upwelling radiance obtained from POLAYER program and the present LINBLIN program, $T_s = 288^\circ K$, $\varepsilon = 0.8$. On the average, LINBLIN values are 2% lower than POLAYER values.
Fig. 4.12 Comparison of signal change results obtained from the program POLAYER and the present LINBLIN program, $T = 288^\circ K, \varepsilon = 0.8$. On the average, LINBLIN values are 2% lower than POLAYER values.
V. CONCLUSIONS

A computer program has been developed for calculating the atmospheric transmittance and upwelling radiance in the spectral interval 2070-2220 cm\(^{-1}\) which employs the Lorentz line-by-line model. The spectral region selected in the region of CO fundamental band. The program allows for variation in CO concentration and accounts for the radiative contributions from the interfering gases such as H\(_2\)O, CO\(_2\), N\(_2\)O, and O\(_3\). The program has been optimized for accuracy and running time by varying such computation parameters as the interval width, subinterval width and the width of the region from which lines make significant contribution to the absorption at a certain frequency. Furthermore, this program has been diversified so that radiances can be computed for several values of surface temperature or surface emittance in a single run, thereby drastically reducing the computational cost. This line-by-line computer program is given the name LINBLIN. Upwelling radiance results obtained by using the present LINBLIN program are compared with the results of SAI-POLAYER program [19]. The agreement between the two results is within 2\%. For homogeneous gas columns, the results obtained by LINBLIN program compare well with available experimental results. This LINBLIN program can easily be extended to any line model and for any spectral region.

A computer program similar to the line-by-line program has been developed which employs the quasi-random narrow band model. This program was given the name QRANDOM. Comparison of results obtained from LINBLIN and QRANDOM programs indicate small differences.

By employing the LINBLIN and QRANDOM programs, model calculations were made to study the effects of different interfering molecules, water vapor profiles, ground temperatures, and ground emittances on the upwelling radiance and signal change. Physically realistic values of various parameters were
used in the model calculations. This information is very useful in establishing the feasibility of measuring the concentration of pollutants in the atmosphere from a gas filter correlation instrument flown on an aircraft or mounted on a satellite.
REFERENCES


APPENDIX A

EXPLANATION OF SYMBOLS USED IN COMPUTER PROGRAMS

A-i. Symbols Used in Program LINBLIN

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>ALC</td>
<td>Individual line widths for CO and H$_2$O lines respectively, cm$^{-1}$.</td>
</tr>
<tr>
<td>ALV</td>
<td>Width of the narrow subinterval on each side of the line center, cm$^{-1}$.</td>
</tr>
<tr>
<td>ALX</td>
<td>2 x (ALX)</td>
</tr>
<tr>
<td>AL1, AL2, AL3, AL4, ALD</td>
<td>Average line width for the molecules H$_2$O, CO$_2$, N$_2$O, O$_2$ and CO respectively, cm$^{-1}$.</td>
</tr>
<tr>
<td>DEL</td>
<td>Width of an interval, cm$^{-1}$.</td>
</tr>
<tr>
<td>DLIM</td>
<td>Wave number region around an interval from which the contribution to the absorption coefficient is considered direct, cm$^{-1}$.</td>
</tr>
<tr>
<td>EMI</td>
<td>Surface emittance.</td>
</tr>
<tr>
<td>EL1, EL2, EL3, EL4, ELD</td>
<td>Energies of the lower states for the lines of the molecules, cm$^{-1}$.</td>
</tr>
<tr>
<td>FRL</td>
<td>Lower frequency limit of the range (2070 cm$^{-1}$).</td>
</tr>
<tr>
<td>FRU</td>
<td>Upper frequency limit of the range (2220 cm$^{-1}$).</td>
</tr>
<tr>
<td>FRB</td>
<td>Wave number at the interval boundaries, cm$^{-1}$.</td>
</tr>
<tr>
<td>FRC</td>
<td>Wave number at the interval centers, cm$^{-1}$.</td>
</tr>
<tr>
<td>FR1, FR2, FR3, FR4, FRD</td>
<td>Wave numbers of the lines of the molecules, cm$^{-1}$.</td>
</tr>
<tr>
<td>GAM</td>
<td>$1 + f(\theta)$ where $f(\theta) = \sec \theta$ for $\theta \leq 60^\circ$ and $f(\theta) = \text{Ch} (\theta)$ for $\theta &gt; 60^\circ$.</td>
</tr>
<tr>
<td>GR</td>
<td>Gradients used in calculation of HL</td>
</tr>
</tbody>
</table>

*The same order subscripts 1, 2, 3, 4, and D has been used for these molecules throughout the programs.*
Tabulated values of the solar irradiance at the top of the atmosphere, watts cm\(^{-2}\) sr\(^{-1}\) (cm\(^{-1}\))\(^{-1}\).

Computed solar irradiance at the top of the atmosphere in an interval, watts cm\(^{-2}\) sr\(^{-1}\).

An integer for the molecule which is 0 when average line width is used and 1 when individual line widths are used.

Number of different CO concentrations used in the computation (8).

Number of spectral intervals (150).

Number of layers into which the atmosphere is divided (10).

Number of lines in the spectra of the molecules.

Number of interfering gases.

Identifying integers for the interfering molecules H\(_2\)O, CO\(_2\), N\(_2\)O and O\(_3\) respectively.

Planck's function.

Pressure at NTP, mbar

Pressure at the center of the layers, mbar

Altitude distribution of the molecules H\(_2\)O, CO\(_2\), N\(_2\)O and O\(_3\) respectively.

Concentration of CO, ppm by volume

Radiance in each interval, watts cm\(^{-2}\) sr\(^{-1}\).

Integrated radiance, watts cm\(^{-2}\) sr\(^{-1}\).

Radiance component due to reflected solar radiation.

Exponent to account for the temperature dependence of the rotational partition function for the molecules.

Integrated intensities for the lines of the molecules, cm\(^{-2}\) atom\(^{-1}\).
<table>
<thead>
<tr>
<th>Abbreviation</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>TEMC</td>
<td>Temperatures at the layer centers, °K</td>
</tr>
<tr>
<td>TEMR</td>
<td>Reference temperature for line parameters, °K</td>
</tr>
<tr>
<td>TEMS</td>
<td>Surface temperature, °K</td>
</tr>
<tr>
<td>THC</td>
<td>Thickness of each layer (1 km)</td>
</tr>
<tr>
<td>TNTP</td>
<td>Temperature at NTP (273 °K)</td>
</tr>
<tr>
<td>TRA</td>
<td>Transmittances for different intervals and altitudes for one gas.</td>
</tr>
<tr>
<td>TRF</td>
<td>Combined transmittances of all the interfering gases.</td>
</tr>
<tr>
<td>TRM</td>
<td>Average transmittance over the entire frequency range for each CO distribution.</td>
</tr>
<tr>
<td>TRT</td>
<td>Transmittance for each interval and CO concentration, between the top of the atmosphere and surface.</td>
</tr>
<tr>
<td>TRX</td>
<td>Transmittance for an interval and altitude including the contribution from CO.</td>
</tr>
<tr>
<td>VPF</td>
<td>Vibrational partition functions for H₂O, CO₂, N₂O and O₃.</td>
</tr>
<tr>
<td>WLIM</td>
<td>Wave number range of the wing contribution, cm⁻¹.</td>
</tr>
<tr>
<td>WL1, WL2</td>
<td>Weight factors for the 4-point Gauss-Legendre quadrature formula.</td>
</tr>
<tr>
<td>WN</td>
<td>Wave numbers at which the solar irradiance at the top of the atmosphere is tabulated.</td>
</tr>
<tr>
<td>XL1, XL2</td>
<td>Abscissa values for the 4-point Gauss-Legendre quadrature formula.</td>
</tr>
</tbody>
</table>
A-2. Symbols Used in Subroutine TRANS

AC  Total absorption coefficient at the frequency specified by the subscripts.
ACD  Direct contribution to the total absorption coefficient.
ACW  Wing contribution to the total absorption coefficient.
ACB  Absorption coefficient at the lower boundary of the interval due to wing contributions.
ACE  Same as ACB, at the upper boundary of the interval.
ACM  Same as ACB, at the center of the interval.
AL  Average width for the lines of the molecule under consideration.
ALA  Altitude dependent average width of the lines of a molecule.
ALB  Altitude dependent individual widths of the lines of a molecule (for CO and H2O).
EL  Energies of lower states of lines of the molecule under consideration.
FACT  Factor used in the computation of altitude dependence of integrated intensity.
FR  Frequencies of the lines of the molecule under consideration.
FRE  Frequencies of the lines falling with an interval.
FRG  Frequencies of all the Gauss-Legendre quadrature points within an interval.
FRS  Frequencies at the subinterval boundaries within an interval.
IG  Number of Gauss-Legendre points within an interval.
IN  An integer for each molecule which is zero if average line widths are used and 1 if individual widths are used for that molecule.
LE  Number of lines for the molecule under consideration.
<table>
<thead>
<tr>
<th>Symbol</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>NQ</td>
<td>Number of subintervals within an interval.</td>
</tr>
<tr>
<td>PART</td>
<td>An altitude dependent factor which takes into account the vibrational and rotational partition functions.</td>
</tr>
<tr>
<td>PL</td>
<td>Optical path length at the frequency under consideration.</td>
</tr>
<tr>
<td>RP</td>
<td>Exponent which accounts for the temperature dependence of the rotational partition function.</td>
</tr>
<tr>
<td>SI</td>
<td>Integrated intensities of the lines of the molecule under consideration.</td>
</tr>
<tr>
<td>SIA</td>
<td>Altitude dependent integrated intensities of lines of the molecule under consideration.</td>
</tr>
<tr>
<td>SL1</td>
<td>Gradient used in the calculation of the wing contribution between AGB and ACM.</td>
</tr>
<tr>
<td>SL2</td>
<td>Same as SL1, between ACM and ACE.</td>
</tr>
<tr>
<td>TR</td>
<td>Transmittance at the frequency under consideration.</td>
</tr>
<tr>
<td>WIDF</td>
<td>Factor which takes into account the altitude dependence of the widths of the lines.</td>
</tr>
</tbody>
</table>
A-3. Symbols used in PROGRAM QRANDOM*

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>TRA</td>
<td>Combined transmittance of all the interfering gases.</td>
</tr>
<tr>
<td>TRF</td>
<td>Combined transmittance including CO contribution for all CO distributions.</td>
</tr>
<tr>
<td>TRFM</td>
<td>Average transmittances for the entire frequency range for different altitudes and CO contributions.</td>
</tr>
<tr>
<td>TRG</td>
<td>Transmittances for a single gas returned by the subroutine.</td>
</tr>
<tr>
<td>X1, T1</td>
<td>Convolution parameters for integration of direct contribution.</td>
</tr>
<tr>
<td>X2, T2</td>
<td>Convolution parameters for the integration of wing contribution.</td>
</tr>
</tbody>
</table>

*As far as possible, same symbols have been used in the programs LINBLIN and QRANDOM. Only the symbols which are defined differently for QRANDOM are explained here.
### Symbols Used in SUBROUTINE SMITH

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>AVSI</td>
<td>Average value of intensity for the lines in one decade in an interval.</td>
</tr>
<tr>
<td>BIGI</td>
<td>Intensity of the strongest line in an interval, ( \text{cm}^{-2} \text{atm}^{-1} ).</td>
</tr>
<tr>
<td>BIG</td>
<td>Intensity values separating the five decades in each interval.</td>
</tr>
<tr>
<td>ELE</td>
<td>Altitude dependent energies of the lower states for lines in an interval.</td>
</tr>
<tr>
<td>JB</td>
<td>Number of adjacent intervals from which the wing contribution is considered.</td>
</tr>
<tr>
<td>NSI</td>
<td>Number of lines in a decade within an interval.</td>
</tr>
<tr>
<td>SFE</td>
<td>Intensities of the lines within a decade in an interval.</td>
</tr>
<tr>
<td>SIE</td>
<td>Intensities of the lines within an interval.</td>
</tr>
<tr>
<td>SLE</td>
<td>Altitude dependent intensities of the lines within an interval.</td>
</tr>
<tr>
<td>SSI</td>
<td>Sum of the intensities of the lines in a decade within an interval.</td>
</tr>
<tr>
<td>SUMSI</td>
<td>Optical thickness between the top of the atmosphere and the altitude under consideration.</td>
</tr>
</tbody>
</table>
APPENDIX B

LINE-BY-LINE COMPUTER PROGRAM TO CALCULATE
ATMOSPHERIC TRANSMITTANCE AND UPWELLING RADIANCE

B-1. Computer Program LINBLIN

PROGRAM LINBLIN(INPUT,OUTPUT)
DIMENSION FR1(100),SI1(100),EL1(100)
DIMENSION FR2(400),SI2(400),EL2(400)
DIMENSION FR3(750),SI3(750),EL3(750)
DIMENSION FR4(1220),SI4(1220),EL4(1220)
DIMENSION FRD(100),SID(100),ELD(100)
DIMENSION QVD(10),QV(10,5),ALC(100),TRF(11,150),TRX(11,150),
/ TRT(150,8),PCK(11,150),GR(5),RADNC(150,8),TRH(10),RADNCE(10),
/ VPF(10,4),WN(5),HS(5),HL(150)
INTEGER G,X
COMMON FRC(150),FRB(151),PREC(10),TEMC(10),GG(10),TRA(11,150),
/ TEMR,XL1,XL2,WL1,WL2,ALX,LC,KR,PNTP,TNTP,DEL,DLIM,WMIM,THC,
/ ALV(100),VPF(10),ALY,DEL,PART(10),FACT(10),WIDF(10)
READ 10, FRL,FRU,DEL,THC,PNTPTNTPTEIRTEMS.EMI,ZEN
READ 11, LC,JQ,NG,LE1,LE2,LE3,LE4,LED
READ 10, DLIM,WMIM
READ 10, (QVD(J),J=1,JQ)
READ 15, ((QV(L,G),L=1,LC),G=1,NG)
READ 10, (PREC(L),L=1,LC)
READ 10, (TEMC(L),L=1,LC)
READ 12, XL1,XL2,WL1,WL2
READ 13, AL1,AL2,AL3,AL4,ALD,ALX
READ 10, RP1,RP2,RP3,RP4,RPD
READ 17, ((VPF(L,G),L=1,LC),G=1,NG)
READ 11, NG1,NG2,NG3,NG4
READ 11, IN1,IN2,IN3,IN4,IND
READ 18, (WN(N),N=1,5), (HS(N),N=1,5)
READ 16, (FR1(X),SI1(X),EL1(X),ALV(X),X=1,LE1)
READ 14, (FR2(X),SI2(X),EL2(X),X=1,LE2)
READ 14, (FR3(X),SI3(X),EL3(X),X=1,LE3)
READ 14, (FR4(X),SI4(X),EL4(X),X=1,LE4)
READ 16, (FRD(X),SID(X),ELD(X),ALC(X),X=1,LED)
10 FORMAT(10F8.2)
11 FORMAT(16I5)
12 FORMAT(8F10.6)
13 FORMAT(10F8.3)
14 FORMAT(2(F11.3,E13.4,F11.3,S5X))
15 FORMAT(8E10.3/2E10.3)
16 FORMAT(2(F11.3,E13.4,F11.3,F5.3))
17 FORMAT(10F8.4)
18 FORMAT(5F8.2,5E8.3)
C CALCULATES THE NUMBER OF INTERVALS—DEFINES FREQUENCIES AT THE INTERVAL
C BOUNDARIES AND CENTERS
LB=LC+1

ORIGINAL PAGE IS OF POOR QUALITY
DELA=0.5*DEL
RK=(FRU-FRL)/DEL+0.1
KR=RK
FRB(I)=FRL
DO 101 K=1,KR
FRB(K+1)=FRB(K)+DEL
101 FRC(K)=FRB(K)+DELA
ALY=2.*ALX
C INITIALIZES THE COMBINED TRANSMITTANCES OF ALL THE INTERFERING GASES
DO 102 K=1,KR
DO 102 L=1,LB
102 TRF(L,K)=1.
C DECIDE IF WATER VAPOR IS TO BE TAKEN INTO CONSIDERATION. IF SO, THE C WATER VAPOR TRANSMITTANCES RETURNED BY THE SUBROUTINE ARE COMBINED C WITH TRF
IF (NG1-2) 118,119,118
119 CONTINUE
DO 107 L=1,LB
VP(L)=VPF(L,1)
107 QG(L)=QV(L,1)/1245.
CALL TRANS(FR1,S1,E1,AL1,RP1,IN1)
DO 103 K=1,KR
DO 103 L=1,LB
103 TRF(L,K)=TRF(L,K)*TRA(L,K)
C DECIDES IF CARBON DIOXIDE IS TO BE TAKEN INTO CONSIDERATION
118 IF (NG2-12) 165,166,167
166 CONTINUE
DO 108 L=1,LB
VP(L)=VPF(L,2)
108 QG(L)=QV(L,2)
CALL TRANS(FR2,S2,E2,AL2,RP2,IN2)
DO 104 K=1,KR
DO 104 L=1,LB
104 TRF(L,K)=TRF(L,K)*TRA(L,K)
C DECIDES IF NITROUS OXIDE IS TO BE TAKEN INTO CONSIDERATION
165 IF (NG3-7) 167,168,169
168 CONTINUE.
DO 109 L=1,LB
VP(L)=VPF(L,3)
109 QG(L)=QV(L,3)
CALL TRANS(FR3,S3,E3,AL3,RP3,IN3)
DO 105 K=1,KR
DO 105 L=1,LB
105 TRF(L,K)=TRF(L,K)*TRA(L,K)

ORIGINAL PAGE IS
OF POOR QUALITY
C DECIDES IF OZONE IS TO BE TAKEN INTO CONSIDERATION
167 IF (NG4-19) 169,170,169
170 CONTINUE
   DO 110 L=1,LC
   VP(L)=VPF(L,4)
   110 QG(L)=QV(L,4)
   CALL TRANS(FR4,SI4,EL4,LE4,AL4,RP4,IN4)
   DO 106 K=1,KR
   DO 106 L=1,LB
   106 TRF(L,K)=TRF(L,K)*TRA(L,K)
   169 CONTINUE
C CALCULATES PLANCK FUNCTIONS FOR DIFFERENT ALTITUDES AND INTERVALS
   CONS=18.*6.625*1.E-07
   CNST=6.625*0.3/1.38
   DO 115 K=I,KR
   RNUM=DEL*CONS*FRC(K)**3
   EEX=CNST*FRC(K)
   PCK(1,K)=RNUM/(EXP(EEX/TEMS)-1.)
   DO 115 L=I,LC
   115 PCK(L+1,K)=RNUM/(EXP(EEX/TEMC(L))-1.)
C CALCULATES SOLAR IRRADIANCE AT THE TOP OF THE ATMOSPHERE IN EACH INTERVAL
   DO 173 N=I,4
   173 GR(N)=(HS(N+1)-HS(N))/(WN(N+1)-WN(N))
   DO 174 K=1,KR
   N=0
   177 N=N+1
   IF (FRC(K)-WN(N)) 174,175,175
   IF (FRC(K)-WN(N+1)) 176,177,177
   176 HL(K)=HS(N)+GR(N)*(FRC(K)-WN(N))
   HL(K)=HL(K)*DEL
   174 CONTINUE
   ZEN=ZEN/57.29578
   GAM=1.+1./COS(ZEN)
   DO 172 X=1,LED
   DO 178 L=1,LC
   178 VP(L)=VPF(L,4)
C CALCULATES TRANSMITTANCES FOR ALL CONCENTRATIONS OF CO ONE BY ONE-
C COMBINES THEM WITH TRF AND CALCULATES RADIANCE AT THE TOP TAKING
C REFLECTED SOLAR COMPONENT INTO ACCOUNT
   DO 112 J=1,JG
   DO 112 L=1,LC
   112 QG(L)=QVD(J)
   CALL TRANS(FRD,SID,ELD,LED,ALD,RPD,IND)
DO 113 K=1, KR
DO 114 L=1, LB
114 TRX(L,K)=TRF(L,K)*TRA(L,K)
113 TRT(K,J)=TRX(1,K)
DO 116 K=1, KR
   RCOM=(1.-EMI)*(COS(ZEN.))*HL(K)*(TRT(K,J))**GAM.
   RADNC(K,J)=EMI*PCK(I,K)*TRT(K,J)*1.E-07+RCOM
   DO 116 L=2, LB
      COMP=PCK(L,K)*((TRX(L,K)-TRX(L-1,K))*1.E-07
116 RADNC(K,J)=RADNC(K,J)+COMP
   TRM(J)=0.
   RADNCE(J)=0.
DO 117 K=1, KR
   TRM(J)=TRM(J)+TRT(K,J)/KR
117 RADNCE(J)=RADNCE(J)+RADNC(K,J)
111 CONTINUE
PRINT 60, ((TRT(K,J), J=1, JQ), K=1, KR)
PRINT 61, ((RADNC(K,J), J=1, JQ), K=1, KR)
PRINT 62, (TRM(J), J=1, JQ), (RADNCE(J), J=1, JQ)
60 FORMAT(IH1/(8E15.5))
61 FORMAT(IH1/(8E15.4))
62 FORMAT(IH1////(8F15.5///8E15.4))
STOP
END
B-2. Subroutine TRANS for Program LINBLIN

SUBROUTINE TRANS(FR, SI, EL, AL, RP, IN)
DIMENSION FR(1220), SI(1220), EL(1220), SIA(1220), FRE(40), FRS(50),
/FRG(200), ACD(200), ACW(200), AC(200, 10), TR(200, 11), ALB(100)
INTEGER X
COMMON FRC(150), FRB(151), PREC(10), TEMC(10), QG(10), IRA(11, 150),
/TEMR, XL1, XL2, WL1, WL2, ALX, LC, KR, PNTP, TNTP, DELA, DLIM, WLM, THC,
/ALV(100), VP(10), ALY, DEL, PART(10), FACT(10), WIDF(10)
CST = SQRT(TEMR)/PNTP
C DEFINES VARIABLES WHICH ACCOUNT FOR THE VIBRATIONAL AND ROTATIONAL
C PARTITION FUNCTIONS AND THE ALTITUDES VARIATION OF THE WIDTH OF LINES
DO 120 L=1, LC
PART(L) = VP(L) * (EMR/TEMC(L))**RP
FACT(L) = 1.439 * (TEMC(L) - TEMR) / (TEMC(L)*IEMR)
120 WIDF(L) = CST * PREC(L) / SQRT(TEMCL))
X=0
C ONE INTERVAL CONSIDERED AT A TIME - FINDS ALL THE LINES FALLING WITHIN
C IT - DETERMINES SUBINTERVAL BOUNDARIES WITHIN THE INTERVAL.
DO 126 K=1, KR
X=M
MP=M
126 IF (X-LE) 124, 125, 125
124 X=X+1
IF (FR(X) - FRB(K)) 126, 127, 127
127 IF (FR(X) - FRB(K+1)) 128, 125, 125
128 M=M+1
FRE(M) = FR(X)
MP=M
GO TO 126
125 X=M-1
N=1
FRS(N) = FRB(K)
IF (MP) 129, 129, 130
130 CONTINUE
DO 131 M=1 , MP
DIF = FRE(M) - FRS(N)
IF (DIF-ALX) 132, 132, 133
133 IF (DIF-ALY) 134, 134, 135
132 FRS(N+1) = FRE(M)
N=N+1
GO TO 136
134 FRS(N+1) = FRE(M) - ALX
FRS(N+2) = FRE(M)
N=N+2
GO TO 136
135 $\text{FRS}(N+1) = \text{FRE}(M) - \text{ALY}$
   $\text{FRS}(N+2) = \text{FRE}(M) - \text{ALX}$
   $\text{FRS}(N+3) = \text{FRE}(M)$
   $N = N + 3$

136 IF $(M - MP) 
eq 0$

137 DIF = FRE$(M+1) - \text{FRS}(N)$
   IF $(\text{DIF} - \text{ALX}) 
eq 0$

140 IF $(\text{DIF} - \text{ALY}) 
eq 0$

139 GO TO 131

141 $\text{FRS}(N+1) = \text{FRE}(M) + \text{ALX}$
   $N = N + 1$
   GO TO 131

142 $\text{FRS}(N+1) = \text{FRE}(M) + \text{ALX}$
   $\text{FRS}(N+2) = \text{FRE}(M) + \text{ALY}$
   $N = N + 2$

131 CONTINUE

138 DIF = FRE$(M+1) - \text{FRE}(M)$
   IF $(\text{DIF} - \text{ALX}) 
eq 0$

144 IF $(\text{DIF} - \text{ALY}) 
eq 0$

143 $\text{FRS}(N+1) = \text{FRB}(K+1)$
   $NP = N + 1$
   GO TO 147

145 $\text{FRS}(N+1) = \text{FRE}(M) + \text{ALX}$
   $\text{FRS}(N+2) = \text{FRB}(K+1)$
   $NP = N + 2$
   GO TO 147

146 $\text{FRS}(N+1) = \text{FRE}(M) + \text{ALX}$
   $\text{FRS}(N+2) = \text{FRE}(M) + \text{ALY}$
   $\text{FRS}(N+3) = \text{FRB}(K+1)$
   $NP = N + 3$
   GO TO 147

129 $\text{FRS}(N+1) = \text{FRB}(K+1)$
   $NP = N + 1$

147 $NQ = NP - 1$

C DETERMINES THE FREQUENCIES OF THE GAUSS-LEGENDRE QUADRATURE POINTS
C WITHIN A SUBINTERVAL

DO 148 N = 1, NQ
   VAR = 0.5 * (FRS$(N+1) - \text{FRS}(N))$
   CON = 0.5 * (FRS$(N+1) + \text{FRS}(N))$
   X = 4 * $(N-1) + 1$
   $\text{FRG}(1) = \text{CON} + \text{VAR} \times X$
   $\text{FRG}(1+1) = \text{CON} - \text{VAR} \times X$
   $\text{FRG}(1+2) = \text{CON} + \text{VAR} \times X$
   $\text{FRG}(1+3) = \text{CON} + \text{VAR} \times X$

148 $\text{FRG}(1+3) = \text{CON} + \text{VAR} \times X$
IG = 4*NQ
PI = 3.14159

C EACH ALTITUDE CONSIDERED SEPARATELY - DIRECT CONTRIBUTION EVALUATED
C AT EACH GRID POINT AND WING CONTRIBUTION AT THE BOUNDARIES AND
C CENTER OF THE INTEGRAL

DO 149 L = 1, LC
ALA = AL*WDF(L)
ACB = 0.
ACM = 0.
ACE = 0.
DO 179 I = 1, IG
ACD(I) = 0.
ACW(I) = 0.

179 ACW(I) = 0.

IF (IN) 167, 167, 168

167 DO 150 X = 1, LE
DIF = ABS(FR(X) - FRG(K))
IF (DIF - WLIM) 151, 151, 156
151 IF (DIF - DLIM) 152, 152, 153
152 SIA(X) = S1(X) * PAR(L) * EXP(E(L) * FAC(L))
DO 154 I = 1, IG
FD = FR(X) - FRG(I)
DEN = PI * (FD**2 + ALB**2)
ACD(I) = ACD(I) + SIA(X) * ALB / DEN
GO TO 150
153 SIA(X) = S1(X) * PAR(L) * EXP(E(L) * FAC(L))
FB = FR(X) - FRB(K)
FM = FR(X) - FRC(K)
FE = FR(X) - FRB(K+1)
PNUM = SIA(X) * ALB
ACB = ACB + PNUM / (PI*FD**2 + ALB**2)
ACM = ACM + PNUM / (PI*FM**2)
ACE = ACE + PNUM / (PI*FE**2)
150 CONTINUE
GO TO 174

168 DO 169 X = 1, LE
DIF = ABS(FR(X) - FRG(K))
IF (DIF - WLIM) 170, 170, 169
170 IF (DIF - DLIM) 171, 171, 172
171 SIA(X) = S1(X) * PAR(L) * EXP(E(L) * FAC(L))
ALB(X) = ALB(X) * WDF(L)
DO 173 I = 1, IG
FD = FR(X) - FRG(I)
DEN = PI * (FD**2 + ALB(X)**2)
ACD(I) = ACD(I) + SIA(X) * ALB(X) / DEN
173 CONTINUE
GO TO 169

172 SIA(X)=SI(X)*PART(L)*EXP(EL(X)*FACf(L))
   ALB(X)=ALV(X)*WI*DF(L)
   FB=FR(X)-FRB(K)
   FM=FR(X)-FRC(K)
   FE=FR(X)-FRB(K+1)
   PNUM=SIA(X)*ALB(X)
   ACB=ACB+PNUM/(PI*FB**2)
   ACM=ACM+PNUM/(PI*FM**2)
   ACE=ACE+PNUM/(PI*FE**2)
169 CONTINUE

C WING CONTRIBUTION EVALUATED AT EACH GRID POINT BY INTERPOLATION
174 SL1=(ACM-ACB)/(FRC(K)-FRB(K))
   SL2=(ACE-ACM)/(FRB(K+1)-FRC(K))
   DO 156 I=IIG
      DIF=FRG(I)-FRB(K)
      IF (DIF-DELA) 157,158,158
157 ACW(I)=ACB+SL1*DIF
      GO TO 156
158 ACW(I)=ACM+SL2*(DIF-DELA)
      CONTINUE

C TOTAL ABSORPTION COEFFICIENTS EVALUATED AT EACH GRID POINT
   DO 161 I=1,IG
      LB=LC+1
      CONST=O.*TNIP*IH/PNIP
   C TRANSMITTANCE EVALUATED AT EACH GRID POINT
      DO 163 I=IIG
         PL=0.
         TR(I,LB)=EXP(-PL)
         DO 163 M=2,LB
            L=LB+1-M
            SPTR=PREC(L)*OG(L)*AC(I,L)/TEMC(L)
            PL=PL+CONST*SPTR
         163 TR(I,L)=EXP(-PL)
      C AVERAGE TRANSMITTANCE EVALUATED FOR EACH INTERVAL AT EACH ALTITUDE
      DO 164 L=1,LB
         TRA(L,K)=O.
         DO 164 N=1,NQ
            VAR=O.*5*(FRS(N+1)-FRS(N))
            I=4*(N-1)+1
            SUM1=TR(I,L)+TR(I+3,L)
            SUM2=TR(I+1,L)+TR(I+2,L)
            SUM=WL1*SUM1+WL2*SUM2
         164 TRA(L,K)=TRA(L,K)+SUM*VAR/DEL
      123 CONTINUE
      RETURN
      END
QUASI-RANDOM COMPUTER PROGRAM TO CALCULATE
ATMOSPHERIC TRANSMITTANCE AND UPWELLING RADIANCE

C-1. Computer Program QRANDOM

PROGRAM QRANDOM(INPUT,OUTPUT)
INTEGER X,G,W
DIMENSION FR1(100),SI1(100),EL1(100)
DIMENSION FR2(400),SI2(400),EL2(400)
DIMENSION FRD(100),SID(100),ELD(100)
DIMENSION QVD(10),OV(10),4VF(10),WN(5),HS(5),GR(5),
/TRA(26,11),TRF(51,11,8),HL(25),PCK(25,11),TRFM(11,8),TRT(25,8),
/RADNC(25,8),TRM(8),RADNC(8)
COMMON DEL.X1(26),D2(26),X2(21),D2(21),TRG(26,11),FRB(27),FRC(26),
PSEC(10),XEMC(10),QG(10),VP(10),PNTP,INTP,TEM,LC,VR,J,THC
READ 10,FRU,FRU,DEL,TIHC,PNTP,INTP,TEM,LEM,LEM
READ 11,LC,JO,NG,JB,LE1,LE2,LE3,LE4,LE5
READ 10,(QVD(J),J=1,JO)
READ 10,(VPF(L),L=1,LC)
READ 10,(TEMC(L),L=1,LC)
READ 12,(OV(l,G),L=1,LC),G=1,NG)
READ 14,(AL1,AL2,AL3,AL4,ALD)
READ 10,(RP1,RP2,RP3,RP4,RPD)
READ 11,(MP1,MP1,MP2,MP2,MP3,MP3,MP4,MP4,MPD,MPD)
READ 15,(X1(W),W=1,26)
READ 15,(T1(W),W=1,26)
READ 15,(X2(W),W=1,21)
READ 15,(T2(W),W=1,21)
READ 15,(VPF(L,G),L=1,LC),G=1,NG)
READ 11,(NG1,NG2,NG3,NG4)
READ 18,(W(N),N=1,5),(HS(N),N=1,5)
READ 17,(FRU(X),SI1(X),EL1(X),X=1,LE1)
READ 17,(FR2(X),SI2(X),EL2(X),X=1,LE2)
READ 17,(FRD(X),SID(X),ELD(X),X=1,LED)
10 FORMAT(1UF8.2)
11 FORMAT(1615)
12 FORMAT(BE10.3/2E15.3)
14 FORMAT(10F8.3)
15 FORMAT(10F8.4)
17 FORMAT(2(F11.3,E13.4,F11.3,5X))
18 FORMAT(5F8.2,5E8.3)

C CALCULATES THE FREQUENCY, INTERVAL BOUNDARIES AND CENTER FOR C UNSHIFTED MESH AND Initializes THE RESULTANT TRANSMITTANCES
RK=(FRU-FRU)/DEL+O.1
KR=KR
DEL=0.5*DEL
FRB(1)=FRU
DO 100 K=1,KR
FRB(K+1)=FRB(K)+DEL
FRC(K) = FRB(K) + DELA
LB = LC + 1
DO 101 L = 1, LB
DO 101 K = 1, KR
101 TRA(K, L) = 1.

C DECIDES WHICH GASES ARE TO BE TAKEN INTO CONSIDERATION IN THE ORDER
C WATER VAPOR, CARBON DIOXIDE, NITROUS OXIDE AND OZONE AND COMBINES
C THEIR TRANSMITANCE OBTAINED FROM THE SUBROUTINE WITH THE RESULANT
C TRANSMITTANCE
IF (NG1-2) 102, 103, 102.
103 CONTINUE
DO 104 L = 1, LC
QG(L) = QV(L, 1) / 104.
104 VP(L) = VPF(L, 1)
CALL SMITH(FR1, SI, EL1, LE1, AL1, RP1, MP1, NR1)
DO 105 L = 1, LB
DO 105 K = 1, KR
105 TRA(K, L) = TRA(K, L) * TRG(K, L)
102 IF (NG2-12) 106, 107, 106
107 CONTINUE
DO 108 L = 1, LC
QG(L) = QV(L, 2)
108 VP(L) = VPF(L, 2)
CALL SMITH(FR2, SI2, EL2, LE2, AL2, RP2, MP2, NR2)
DO 109 L = 1, LB
DO 109 K = 1, KR
109 TRA(K, L) = TRA(K, L) * TRG(K, L)
106 IF (NG3-7) 110, 111, 110
111 CONTINUE
DO 112 L = 1, LC
QG(L) = QV(L, 3)
112 VP(L) = VPF(L, 3)
CALL SMITH(FR3, SI3, EL3, LE3, AL3, RP3, MP3, NR3)
DO 113 L = 1, LB
DO 113 K = 1, KR
113 TRA(K, L) = TRA(K, L) * TRG(K, L)
110 IF (NG4-19) 114, 115, 114
115 CONTINUE
DO 116 L = 1, LC
QG(L) = QV(L, 4)
116 VP(L) = VPF(L, 4)
CALL SMITH(FR4, SI4, EL4, LE4, AL4, RP4, MP4, NR4)
DO 117 L = 1, LB
DO 117 K = 1, KR

C-2
117 \( \text{TRA}(K,L) = \text{TRA}(K,L) \times \text{TRG}(K,L) \)

114 CONTINUE
    DO 154 L = 1, LB
    DO 154 K = 1, KR
      KK = 2*K
  154 \( \text{TRF}(K,K+1) = \text{TRA}(K,L) \)
    DO 118 J = 2, JQ
    DO 119 L = 1, LC
      QG(L) = QVD(J)
  119 \( \text{VP}(L) = \text{VPF}(L,1) \)
        CALL SMITH(FRD, S12, ELD, LED, ALD, RPD, MPD, NRD)
    DO 120 L = 1, LB
    DO 120 K = 1, KR
      KK = 2*K
  120 \( \text{TRF}(K+1,L) = \text{TRA}(K,L) \times \text{TRG}(K,L) \)
118 CONTINUE

C CALCULATES THE FREQUENCIES AT THE INTERVAL BOUNDARIES AND CENTERS
C FOR SHIFTED MESH AND INITIALIZES RESULTANT TRANSMITTANCES
KR = KR + 1
    FRB(1) = FRL - DELA
    DO 121 K = 1, KR
      FRB(K+1) = FRB(K) + DEL
  121 \( \text{FRC}(K) = \text{FRB}(K) + \text{DEL} \)
    DO 122 L = 1, LB
    DO 122 K = 1, KR
  122 \( \text{TRA}(K,L) = 1 \).
123 \( \text{FRC}(K) = \text{FRB}(K) + \text{DEL} \)
    DO 126 L = 1, LB
    DO 126 K = 1, KR
  126 \( \text{TRA}(K,L) = \text{TRA}(K,L) \times \text{TRG}(K,L) \)
124 CONTINUE
    DO 129 L = 1, LC
    QG(L) = QV(L,1)/245.
  125 \( \text{VP}(L) = \text{VPF}(L,1) \)
        CALL SMITH(FR1, S12, E1, L1, AL1, RP1, MP1, N1)
    DO 126 L = 1, LB
    DO 126 K = 1, KR
  126 \( \text{TRA}(K,L) = \text{TRA}(K,L) \times \text{TRG}(K,L) \)
123 IF (NG2-12) 127, 124, 123
128 CONTINUE
    DO 129 L = 1, LC
    QG(L) = QV(L,2)
  129 \( \text{VP}(L) = \text{VPF}(L,2) \)
        CALL SMITH(FR2, S12, E2, L2, AL2, RP2, MP2, N2)
    DO 130 L = 1, LB

C-3
DO 130 K=1,KR
130 TRA(K,L)=IRA(K,L)*IRG(K,L)
127 IF (NG3-7) 131,132,131
132 CONTINUE
   DO 133 L=1,LC
   QG(L)=QV(L,3)
133 VP(L)=VPF(L,3)
   CALL SMITH(FR3,S13,EL3,LE3,AL3,RP3,MP3,NR3)
   DO 134 L=1,LB
      DO 134 K=1,KR
      TRA(KL)=IRA(K,L)*IRG(K,L)
131 IF (NG4-19) 135,136,135
136 CONTINUE
   DO 137 L=1,LC
   QG(L)=QV(L,4)
137 VP(L)=VPF(L,4)
   CALL SMITH(FR4,S14,EL4,LE4,AL4,RP4,MP4,NR4)
   DO 138 L=1,LB
      DO 138 K=1,KR
      TRA(K,L)=IRA(K,L)*IRG(K,L)
135 CONTINUE
   DO 139 L=1,LC
      DO 139 J=2,JQ
         DO 139 L=1,LC
            QG(L)=QV(L,J)
139 CONTINUE
   VP(L)=VPF(L,1)
   CALL SMITH(FR5,S15,EL5,LE5,AL5,RP5,MP5,NR5)
   DO 141 L=1,LB
      DO 141 K=1,KR
         KK=2*K-1
      TRF(KK,L,J)=IRA(K,L)
140 CONTINUE
   DO 143 J=1,JQ
      DO 143 L=1,LB
         DO 143 K=1,KR
            KX=2*K-1
         TRF(KK,L,J)=IRA(K,L)*IRG(K,L)
139 CONTINUE
   CONTINUE
   CR=KR-1
C CALCULATES MEAN TRANSMITTANCES BY AVERAGING RESULTS FROM SHIFTED AND
C UNSHIFTED MESH CALCULATIONS AND FINALLY OBTAINING THE AVERAGE TRANSMITTANCE
C FOR THE ENTIRE FREQUENCY RANGE
   DO 144 J=1,JQ
      DO 144 L=1,LB
         DO 144 K=1,KR
            KY=2*K
C-4
KZ=2*K+1
145 TRF(K*L*J)=(TRF(K*K*L*J)+TRF(K*Y*L*J)+TRF(K*Z*L*J))/3.
   TRFM(L*J)=0.
   DO 144 K=1,KR
144 TRFM(L*J)=TRFM(L*J)+TRF(K*L*J)/KR
   DO 143 K=1,KR
143 TRT(K*L*J)=TRF(K*1*L*J)

C CALCULATES SOLAR IRRADIANCE AT THE TOP OF THE ATMOSPHERE FROM THE
C TABULATED VALUES OF LINEAR INTERPOLATION IN EACH INTERVAL
   DO 146 N=1,4
146 GR(N)=(HS(N+1)-HS(N))/(WN(N+1)-WN(N))
   DO 147 K=1,KR
      N=0
   147 CONTINUE

C CALCULATES PLANCK FUNCTION FOR EACH ALTITUDE AND FREQUENCY INTERVAL
   CONS=18.6.625*1.E-07
   DO 142 K=1,KR
      RNUM=DEL*CONS*FRC(K)**3
      EEX=CNST*FRC(K)**3
      PCK(K,L)=RNUM/(EXP(EEX/IEM(L))-1.)
   DO 142 L=1,LB
      PCK(K,L+1)=RNUM/(EXP(EEX/IEMC(L))-1.)
   142 CONTINUE

C CALCULATES RADIANCE AT THE TOP OF THE ATMOSPHERE INCLUDING THE
C REFLECTED SOLAR COMPONENT
   ZEN=COS(ZEN/57.29578)
   GAM=1.*1/ZEN
   DO 151 J=1,JQ
   DO 152 K=1,KR
      RCOM=(1.-EMI)*ZEN*HL(K)*(TRT(K*J)**GAM
      RADNC(K,J)=EMI*PCK(K,1)*TRT(K,J)*L.E-07+RCOM
   DO 152 L=2,LB
      COMP=PCK(K,L)*(TRF(K*L*J)-TRF(K*L-1,J))*L.E-07
   152 RADNC(K,J)=RADNC(K,J)+COMP
   TRM(J)=0.
   RADNCE(J)=0.
   DO 153 K=1,KR
      TRM(J)=TRM(J)+TRT(K*J)/KR.
   153 RADNCE(J)=RADNCE(J)+RADNC(K,J)
   151 CONTINUE
   PRINT 60, ((TRT(K*J),J=1,JQ),K=1,KR)
   PRINT 62, ((RADNC(K*J),J=1,JQ),K=1,KR).
   PRINT 60, ((TRFM(L*J),J=1,JQ),L=1,LB)
   PRINT 61, (TRM(J),J=1,JQ), (RADNCE(J),J=1,JQ)
   60 FORMAT(1H1//(8F15.5/))
   61 FORMAT(1H1//(/(8F15.5///8E15.4))
   62 FORMAT(1H1//(/8E15.4/))
   STOP
C-2. Subroutine SMITH for Program QRANDOM

SUBROUTINE SMITH(FR, SL, EL, AL, RP, MP, NR)
INTEGER XW
DIMENSION FR(1220), SL(1220), EL(1220), SIE(200, 26), SLE(200, 26),
/ ELE(200, 26), SFE(100, 5, 26), BIGI(26), BIG(6, 26), NSI(5, 26), SS1(5, 26),
/ AVSI(5, 26), SUMSI(5, 26), PART(10), FACT(10), WIDF(10)
COMMON DELXI(26), T1(26), X2(21), T2(21), TRG(26, 11), FRB(27), FRC(26),
/ PREC(10), TEMC(10), QG(10), VP(10), PNTP, TNP, TEMR, LC, KR, JB, THC
C SETS INTEGRATED INTENSITIES AND ENERGIES FOR EACH LINE TO ZERO
DO 120 K=1, KR
    SIE(M, K)=0.
    120 ELE(M, K)=0.
    X=0
C DISTRIBUTES THE LINES INTO FREQUENCY INTERVALS
DO 121 K=1, KR
    M=0
    124 IF (X<LE) 122, 123, 123
    122 X=X+1
    IF (FR(X)-FRB(K)) 124, 125, 125
    125 IF (FR(X)-FRB(K+1)) 126, 127, 127
    126 M=M+1
    SIE(M, K)=S1(X)
    ELE(M, K)=EL(X)
    GO TO 124
    127 IF (K<KR) 128, 123, 123
    128 X=X-1
    121 CONTINUE
    123 CONTINUE
C SETS OPTICAL DEPTH IN EACH INTERVAL AT THE TOP OF THE ATMOSPHERE TO ZERO
DO 151 K=1, KR
    DO 151 I=1, 5
        SUMSI(I, K)=0.
        LB=LC+1
        PI=3.141592654
        DELA=0.5*DEL
        CONST=0.1*TNTP*THC/PNTP
        CST=SQRT(TEMR)/PNTP
        ULB=0.
        BSU=0.
C EACH LAYER IS CONSIDERED SEPARATELY FROM TOP DOWN
DO 150 MM=1, LC
    L=LC+1-MM
    PART(L)=VP(L,)* (TEMR/TEMC(L)***RP
    FACT(L)=1.0/39**(TEMC(L)-TEMR)/(TEMC(L)*TEMR)
\[ \text{WIDF}(L) = \text{CST} \times \text{PREC}(L) / \sqrt{\text{TEM}(L)} \]
\[ \text{SPTR} = \text{PREC}(L) \times \text{OG}(L) / \text{TEM}(L) \]
\[ \text{ALA} = \text{AL} \times \text{WIDF}(L) \]
\[ \text{ULA} = \text{CONST} \times \text{SPTR} / (\pi \times \text{AL}\text{AY}, \text{ULB} = \text{UL}\text{B} + \text{ULA} \]
\[ \text{BSU} = \text{BSU} + \text{ULA} \times \text{AL}\text{A} \]
\[ \text{ALB} = \text{BSU} / \text{ULB} \]
\[ \text{RHO} = \text{ALB} / \text{DELA} \]

C calculates the altitude dependent intensity

\[ \text{DO } 137 \text{ K}=1,\text{KR} \]
\[ \text{DO } 137 \text{ M}=1,\text{MP} \]
\[ 137 \text{ SLE}(M,K) = \text{SIE}(M,K) \times \text{PART}(L) \times \text{EXP} \left( \text{FACT}(L) \times \text{ELE}(M,K) \right) \]
\[ \text{DO } 129 \text{ K}=1,\text{KR} \]
\[ \text{DO } 129 \text{ I}=1,5 \]
\[ \text{DO } 129 \text{ N}=1,\text{NR} \]
\[ 129 \text{ SFE}(N,I,K) = 0. \]

C assigns lines in the interval to the five intensity decades

\[ \text{DO } 130 \text{ K}=1,\text{KR} \]
\[ \text{BIGI}(K) = \text{SLE}(1,K) \]
\[ \text{DO } 131 \text{ M}=2,\text{MP} \]
\[ \text{IF } (\text{BIGI}(K) - \text{SLE}(M,K)) \text{ 132,134} \]
\[ 132 \text{ BIGI}(K) = \text{SLE}(M,K) \]
\[ 131 \text{ CONTINUE} \]
\[ \text{DO } 133 \text{ I}=1,6 \]
\[ \text{IX} = -I+1 \]
\[ 133 \text{ BIG}(I,K) = \text{BIGI}(K) \times 10^{\text{**IX}} \]
\[ \text{DO } 130 \text{ I}=1,5 \]
\[ \text{N}=0 \]
\[ \text{DO } 130 \text{ M}=1,\text{MP} \]
\[ \text{IF } (\text{SLE}(M,K) - \text{BIG}(I,K)) \text{ 134,134,130} \]
\[ 134 \text{ IF } (\text{SLE}(M,K) - \text{BIG}(I+1,K)) \text{ 130,130,135} \]
\[ 135 \text{ N}=N+1 \]
\[ \text{SFE}(N,I,K) = \text{SLE}(M,K) \]
\[ 130 \text{ CONTINUE} \]

C calculates average intensity for each decade

\[ \text{DO } 138 \text{ K}=1,\text{KR} \]
\[ \text{DO } 138 \text{ I}=1,5 \]
\[ \text{NSI}(I,K) = 0 \]
\[ \text{SSI}(I,K) = 0. \]
\[ \text{DO } 139 \text{ N}=1,\text{NR} \]
\[ \text{IF } (\text{SFE}(N,I,K)) \text{ 140,140,141} \]
\[ 141 \text{ NSI}(I,K) = \text{NSI}(I,K)+1 \]
\[ 139 \text{ SSI}(I,K) = \text{SSI}(I,K) + \text{SFE}(N,I,K) \]
\[ 140 \text{ IF } (\text{NSI}(I,K)) \text{ 142,142,136} \]
Continued...

C Calculates transmittance in each interval at all altitudes considering direct and wing contribution

DO 143 K=1,KR
FRUC=FRC(K)
TRG(K,L)=1.
DO 143 J=1,KR
JA=IABS(J-K)
IF (JA-JB) 152,152,153
153 TRD=1.
GO TO 143
152 FRBI=FRB(J)
ZI=FRUC-FRBI-DOLA
EPSI=ZI/DOLA
TRD=1.
DO 144 I=1,5
NSJ=NSI(I,J)
XI=SUMSI(I,J)
RES=0.
IF (J-K) 145,146,145
146 DO 147 W=1,26
Y=EXP(-RHO*RHO*XI/(X1(W)*X1(W)+RHO*RHO))
RES=RES+Y*T1(W)
GO TO 144
145 DO 148 W=1,21
Y=EXP(-RHO*RHO*XI/(EPSI-X2(W))**2)
RES=RES+Y*T2(W)
RES=RES/6.
144 TRD=TRD*RES**NSJ
143 TRG(K,L)=TRG(K,L)*TRD
150 CONTINUE

C Defines transmittances at the top of the atmosphere as unity

DO 149 K=1,KR
149 TRG(K,LB)=1.
RETURN
END