Utilizing round optical fibers as communication channels in optical communication networks presents the problem of obtaining a high efficiency coupling between the optical fiber and the laser. A laser is made an integral part of the optical fiber channel by either diffusing active material into the optical fiber or surrounding the optical fiber with the active material. Oscillation within the active medium to produce lasing action is established by grating the optical fiber so that distributed feedback occurs.
FIBER DISTRIBUTED FEEDBACK LASER

BACKGROUND OF THE INVENTION

The invention described herein was made in the performance of work under a NASA Contract and is subject to the provisions of Section 305 of the National Aeronautics and Space Act of 1958, Public Law 85-568 (72 STAT 455; 42 USC 2457).

ORIGIN OF THE INVENTION

This invention generally relates to distributed feedback lasers. More particularly, the present invention pertains to optical fiber lasers utilizing distributed feedback.

DESCRIPTION OF THE PRIOR ART

Present day optical communication systems utilize fiber optical transmission lines to couple a laser signal from one functional unit to another, for example, from a scanner to a demodulator or detector. FIG. 1 illustrates a prior art arrangement wherein a laser device 11 is coupled to an optical fiber transmission line 13. An active medium 19 such as, a ruby rod is placed within a resonating cavity created by mirrors 21, 23. The active medium is pumped by an optical energy source 17 driven by a power supply 15. The coherent photon energy leaves the cavity by way of partially silvered mirror 23 and is directed into an end of the optical line 13. This type of prior art arrangement exhibits a loss of signal at the interface 27 between the laser device and the optical transmission line 13.

OBJECTS AND SUMMARY OF THE INVENTION

An object of this invention is to reduce signal loss between a laser mechanism and an optical fiber transmission channel.

A further object of this invention is to provide a laser mechanism that utilizes an optical fiber with gratings therein spaced to induce distributed feedback in the active medium.

Yet another object of this invention is to provide a laser mechanism that is an integral part of an optical fiber transmission channel.

These objects and the general purpose of the invention are accomplished by integrating the optical fiber with the active material. Oscillation in the active medium is obtained by gratings the fiber so that distributed feedback occurs as the result of Bragg reflection.

BRIEF DESCRIPTION OF THE DRAWINGS

The exact nature of this invention as well as other objects and advantages thereof will be readily apparent from consideration of the following specification related to the annexed drawings in which like reference numerals designate like parts throughout the figures thereof and wherein:

FIG. 1 is a block diagram illustrating, partially in perspective, a prior art laser mechanism.

FIG. 2 is a block diagram illustrating a distributed feedback laser according to the present invention.

FIG. 3 is a block diagram illustrating another embodiment of a distributed feedback laser according to the present invention.

DESCRIPTION OF THE PREFERRED EMBODIMENT

Referring first to FIG. 2, which illustrates a preferred embodiment of the present invention, a laser device 43 is made an integral part of an optical communication line 33. The laser mechanism comprises a certain length of the optical fiber 33, from one end thereof, being doped with an active material 41 such as, neodymium or an organic dye. A grating 34 is micromachined into the optical fiber 33 at a precise depth 37 and displacement 35 along that length. A polychromatic energy source 31 may be spirally wound around the end of the optical fiber 33 that contains the active medium to provide the pumping energy required to produce population inversion in the active medium. The polychromatic radiator could take the form of a discharge lamp with a cylindrical reflector therearound (not shown). An alternate source of pumping energy that may be utilized is a xenon lamp with an elliptical reflector (not shown). A power source 29 provides energy for the pumping source 31.

FIG. 3 illustrates an alternate preferred embodiment of the laser mechanism of this invention as comprising, a laser mechanism 45 that is an integral part of an optical fiber communication line 53. The laser mechanism comprises a certain length at one end of the communication fiber 53 being grated with gratings that have a specified depth 57 and width 55. The grating length of the fiber is inserted in a bath of active material 51 which may be either in a gaseous or liquid state such as, a liquid solution of neodymium oxide (Nd2O3) dissolved in selenium oxychloride (SeOCl2) acidified with tin tetrachloride (SnCl4). Other types of lasing dyes such as, rhodamine for example, in liquids such as, ethyl alcohol.

Instead of immersing the grated end of fiber 53 in a liquid bath of active material, a solid active material may be deposited, by sputtering for example, around the grated optical fiber 53.

A source of polychromatic radiation 49 may be spirally wound around the end of the optical fiber 53 having the active material therearound to provide the pumping energy required for population inversion within the active medium.

FIG. 4 presents a perspective view of a portion of a machined glass rod that is part of the laser mechanism. This portion 61 has grooves 63 micromachined therein that have a certain depth 67 and occur in a certain periodicity. 65. Photore sist and ion-milling techniques are known that will produce gratings 59 with a periodicity of approximately 0.2 microns at a peak-to-peak height of approximately 0.1 micron. A report on such a
where:

- $\eta = (d/r \alpha) \ (D/2a)^{1/2}$
- $d = \text{depth of surface corrugation}$, and $d << a$. 

The effective gain coefficient and the coupling coefficient for TE modes in a circular waveguide, can be evolved as follows. In case of TE propagation, the normalized electric field is given by:

$$E_r = E_z = 0$$

$$E_\theta = [J_1(\alpha r)/J_1(\alpha a)] \exp(i\beta z - io\omega t) \quad \text{where} \quad r < a$$

$$E_\theta = [K_1(\alpha r)/K_1(\alpha a)] \exp(i\beta z - io\omega t) \quad \text{where} \quad r > a$$

where $J_1$ is the Bessel function and $K_1$ is the modified Bessel function. The magnetic field can then be derived from Maxwell's equations. The corresponding dispersion relations are:

$$\delta K_1(\delta a)/K_1(\delta a) = -s J_1(\delta a)/J_1(\delta a)$$

$$-\delta^2 + \beta^2 = \epsilon_1 k^2$$

where $\delta$, $s$, and $\beta$ are the wavevectors, $K = \omega/c$ and $\epsilon_1$, $\epsilon_2$ are the relative dielectric constants in the fiber and the surrounding material.

Assuming that an active medium has a gain coefficient $G$, whether the optical fiber contains the active medium or the active medium is surrounding the optical fiber, the effective gain coefficient will be $CG$. The efficiency coefficient can be computed by taking a complex dielectric constant and solving equations 4, 5 and 6 for $\beta$, which is now complex. For the small gain case, the well known Taylor development will produce:

$$C = (k \sqrt{\epsilon_1/\beta}) \frac{1}{1 + F}$$

for a fiber doped with an active medium, and

$$C = (k \sqrt{\epsilon_1/\beta}) \frac{1}{1 + F}$$

for a fiber surrounded by an active medium where $F = (1 - J_1^2/J_1^2) / (1 - K_1 K_2^2/K_2^2)$

The same expression for the efficiency coefficient in equation No. 7 above, can be derived from the relation:

$$C = \frac{k \sqrt{\gamma}}{\beta} \left( P_1 / P_r \right)$$

Where $P_1$ is the power in the fiber and $P_r$ is the total power. The first term in equation No. 9 expresses the fact that the optical ray travels a zig-zag line in the guide.

The coupling coefficient between the different TE modes due to the surface corrugations machined into the optical fiber can be determined by using the fact that the surface corrugation is equivalent to a periodic surface current. The coupling coefficient between the pth and qth mode is:
material surrounds the optical fiber. The efficiency curve coefficient \( C \) is close to one because the energy is in the area surrounding the fiber and the active medium is in this area. The threshold gain GL curve 101 illustrates that for the laser structure of FIG. 3, the gain required is relatively smaller at cut-off, probably because the efficiency coefficient is approaching one, and larger at higher frequencies, probably because the efficiency coefficient is approaching zero. The coupling coefficient \( \chi_L \) curve 102, however, is pretty much the same in the structure of FIG. 3 as in the structure of FIG. 2.

**FIG. 6** illustrates the relationships of the efficiency coefficient \( \chi_L \) curve 91 and threshold gain GL for 0-1 mode coupling in the laser structure shown in FIG. 2. The Y axis 105 represents the coupling coefficient \( \chi_L \) scale. The Y axis 107 represents the efficiency coefficient C scale. The Y axis 111 represents the threshold gain GL scale. The X axis 109 represents the increasing frequency of the photon energy emitted by the active medium. As can be seen from FIG. 8, the variables, threshold gain, coupling coefficient and efficiency coefficient, for the 0-1 mode behave similar to these variables for the 0-0 mode, illustrated in FIG. 6.

The minimum threshold gain point is the optimum point for design of a laser according to this invention. To illustrate, a specific example will now be given. Consider the case where

\[
d/2a = 0.01
\]

\[
\eta = 6 \times 10^{-4}
\]

\[
L/a = 6600, \text{ and}
\]

\[
\lambda = 1.2
\]

For an active material having a wavelength

\[
\lambda = 1\mu
\]

this corresponds to a fiber radius

\[
a = 0.83\mu
\]

having micromachined grooves, as shown in FIG. 4 to a depth \( d \) of 0.016\( \mu \), a width of 0.5\( \mu \) with a 0.5\( \mu \) spacing for an overall length \( L \) of 5.5 millimeters. The corresponding threshold gain coefficient is GL=3, which is approaching a total gain of approximately 25 \( \text{dB} \). This is true for the laser mechanism shown in FIG. 2, having the active medium diffused in the optical fiber. For the laser mechanism shown in FIG. 3, where the active material surrounds the optical fiber, the gain coefficient GL=4.2 which approaches a total gain of approximately 35 \( \text{dB} \). These gains can be easily achieved with many active materials, such as, neodymium and the organic dyes, for example. It should be also noted that a larger value of \( d/2a \) would lead to an even lower threshold gain.

In summary, what has been described is a way of reducing the signal loss between a laser mechanism and an optical fiber transmission line. This is accomplished by integrating the laser and the optical fiber transmission line through the technique of distributed feedback. It should be understood, of course, that the foregoing disclosure relates only to preferred embodiments of the
invention and that numerous modifications may be
made therein without departing from the spirit and the
scope of the invention as set forth in the appended
claims.

What is claimed is:
1. A laser mechanism comprising:
an optical fiber having an active material diffused
therein;
pumping means for exciting the atoms in said active
material; and
means for establishing a periodic perturbation in said
optical fiber that has a periodicity capable of sup-
porting Bragg reflection.
2. The laser mechanism of claim 1 wherein said est-
ablishing means comprises a grating in said optical
fiber.
3. The laser mechanism of claim 2 wherein said ac-
tive material is neodymium.
4. The laser mechanism of claim 3 wherein said
pumping means comprises an optical energy source.
5. The laser mechanism of claim 4 wherein said opti-
cal energy source comprises: a high intensity light
source spirally wound around said optical fiber.
6. The laser mechanism of claim 2 wherein said ac-
tive material is an organic dye.
7. The laser mechanism of claim 6 wherein said
pumping means comprises an optical energy source.
8. The laser mechanism of claim 7 wherein said
pumping means comprises a high intensity light source
spirally wound around said optical fiber.
9. The laser mechanism of claim 2 wherein said grat-
ing has a periodicity equal to N times \( \lambda/2 \), where N is
any integer and \( \lambda \) is the wavelength of photons emi-

ted by the active material.
10. A laser mechanism comprising:
an optical fiber immersed in a bath of liquid active
material;
pumping means for exciting the atoms in said active
material; and
means for establishing a periodic perturbation in said
bath of liquid active material capable of supporting
Bragg reflection.
11. The laser mechanism of claim 10 wherein said
establishing means comprises a grating in said optical
fiber.
12. The laser mechanism of claim 11 wherein said active
material is neodymium oxide dissolved in sele-
nium oxychloride.
13. The laser mechanism of claim 12 wherein said
pumping means comprises an optical energy source.
14. The laser mechanism of claim 13 wherein said
optical energy source comprises a high intensity light
source spirally wound around said bath of liquid active
material.
15. The laser mechanism of claim 11 wherein said active
material is a fluorescent dye dissolved in a solu-
tion.
16. The laser mechanism of claim 15 wherein said
pumping means comprises an optical energy source.
17. The laser mechanism of claim 16 wherein said
optical energy source comprises a high intensity light
source spirally wound around said bath of liquid active
material.
18. The laser mechanism of claim 11 wherein said grat-
ing has a periodicity equal to N times \( \lambda/2 \), where N is
any integer and \( \lambda \) is the wavelength of photons emi-
ted by the active material.
19. A laser mechanism comprising:
an optical fiber immersed in a container of gaseous
active material;
pumping means for exciting the atoms in said active
material; and
means for establishing a periodic perturbation in said
optical fiber that has a periodicity capable of sup-
porting Bragg reflection.
20. The laser mechanism of claim 19 wherein said
establishing means comprises a grating in said optical
fiber.
21. The laser mechanism of claim 20 wherein said
grating has a periodicity equal to N times \( \lambda/2 \), where N is
any integer and \( \lambda \) is the wavelength of photons emit-
ted by the active material.
22. A laser mechanism comprising:
an optical fiber having an active material deposited
thereon;
pumping means for exciting the atoms in said active
material; and
means for establishing a periodic perturbation in said
optical fiber that has a periodicity capable of sup-
porting Bragg reflection.
23. The laser mechanism of claim 22 wherein said
establishing means comprises a grating in said optical
fiber.
24. The laser mechanism of claim 23 wherein said
grating has a periodicity equal to N times \( \lambda/2 \), where N is
any integer and \( \lambda \) is the wavelength of photons emi-
ted by the active material.
25. An optical energy distribution system for trans-
porting energy between point A and point B, compris-
ing:
an optical fiber extending between point A and point
B, said fiber having an active material diffused
therein for a short distance at point A and being
grated for that distance with a periodicity equal to
N times \( \lambda/2 \), where N is any integer and \( \lambda \) is the
wavelength of photons emitted by the active mate-
rial; and
pumping means for exciting the atoms in said active
material.
26. The optical energy distribution system of claim
25 wherein said active material is neodymium.
27. The optical energy distribution system of claim
26 wherein said pumping means comprises an optical
energy source.
28. The optical energy distribution system of claim
27 wherein said optical source is spirally wound around
said optical fiber for the length of grating at point A.
29. An optical energy distribution system for trans-
porting energy between point A and point B, compris-
ing:
an optical fiber extending between point A and point
B, said fiber being immersed in a bath of liquid
active material for a short distance at point A and being
grated for that distance with a periodicity equal to
N times \( \lambda/2 \), where N is any integer and \( \lambda \) is the
wavelength of photons emitted by the active mate-
rial; and
pumping means for exciting the atoms in said active
material.
30. The optical energy distribution system of claim
29 wherein said active material is neodymium oxide
dissolved in selenium oxychloride.
31. The optical energy distribution system of claim
30 wherein said pumping means comprises an optical
energy source.
32. The optical energy distribution system of claim 31 wherein said optical energy source comprises a high intensity light source spirally wound around said fiber for the length of grating at point A.

33. An optical energy distribution system for transporting energy between point A and point B, comprising:
   an optical fiber extending between point A and point B, said fiber having, an active material deposited thereon for a short distance at point A and being grated for that distance with a periodicity equal to \( N \times \frac{\lambda}{2} \), where \( N \) is any integer and \( \lambda \) is the wavelength of photons emitted by the active material; and
   pumping means for exciting the atoms in said active material.

34. The optical energy distribution system of claim 33 wherein said active material is an organic dye.

35. The optical energy distribution system of claim 34 wherein said pumping means comprises an optical energy source.

36. The optical energy distribution system of claim 35 wherein said optical energy source comprises a high intensity light source spirally wound around said optical fiber for the length of grating at point A.