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METHODS FOR THE COMPUTATION OF DETAILED GEOIDS AND THEIR ACCURACY

by

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and
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Columbus, Ohio 43210

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Foreword

This report was prepared by Professor Richard H. Rapp, and Reiner Rummel, Visiting Research Associate, Department of Geodetic Science, The Ohio State University. This work was supported through NASA, Contract No. NAS6-2484, The Ohio State University Research Foundation Project No. 3904 which is under the direction of Professor Richard H. Rapp. The contract supporting this research is administered through the Wallops Flight Center, Wallops Island, Virginia 23337.
Abstract

Two methods for the computation of geoid undulations using potential coefficients and 1° x 1° terrestrial anomaly data are examined. It was found that both methods give the same final result but that the method suggested by Molodenskii allows a more simplified error analysis than the method used by Vincent and Marsh.

Specific equations were considered for the effect of the mass of the atmosphere and a cap dependent zero-order undulation term was derived. Although a correction to a gravity anomaly for the effect of the atmosphere is only about \(-0.87\) mgal, this correction causes a fairly large undulation correction (e.g. 2.3 m with a cap size of 20°) that has not previously been considered.

The accuracy of a geoid undulation computed by these techniques was estimated considering anomaly data errors, potential coefficient errors, and truncation (only a finite set of potential coefficients being used) errors. It was found that an optimum cap size of 20° should be used.

The geoid and its accuracy were computed in the Geos-3 calibration area using the GEMG potential coefficients and 1° x 1° terrestrial anomaly data. The accuracy of the computed geoid is on the order of \(\pm 2\) m with respect to an unknown set of best earth parameter constants. This geoid was compared to that computed by Vincent and Marsh where we found a systematic difference of 3.9 m, an undulation difference variance of \((2.6\) m\(^2\)), and a maximum difference of 12 meters.
Preface

Under NASA contract NAS6-2484, we are to investigate the recovery of mean gravity anomalies from altimeter data that is obtained from Geos-3. In developing the methods for such recovery it became clear that it could be helpful to have an external check on the altimeter determined geoid. This check could be obtained by computing geoid undulations from a combination of satellite and terrestrial gravity material. This latter set of geoid undulations could be used to remove systematic bias that might occur in the altimeter data due to orbit determination inaccuracies and errors in the altimeter itself.

Although work had been done in the computation of detailed geoids in the Geos-3 calibration area (as well as other areas), no comprehensive analysis of the complete theoretical and numerical procedures has been carried out. Thus, as one of the first steps in our gravity anomaly recovery work we have prepared this report which attempts to define computational procedures for a detailed undulation computation and its accuracy in a precise way.
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1. Introduction

The purpose of this report is to consider two procedures for the computation of detailed geoids using potential coefficients and 1° x 1° terrestrial gravity material. In doing this we are interested in the results obtained from the two methods, as well as in the error analysis associated with each. The specific computation area is the Geos-3 calibration area since for this area an accurate computation of the geoid undulation is needed. For our purposes the calibration area was considered to be between 40° and 20° north latitude and from 277° to 297° east longitude. Although the resulting geoid may not be the most accurate available geoid, in terms of data used for its computation, we intend the analysis given to demonstrate an accurate procedure for the computation of such a geoid.

Instead of giving extensive references to past work in this area we shall restrict ourselves to references directly applicable to the current discussion.

Method A for computing detailed geoid undulation has been used extensively by Vincent and Marsh (1974) and Marsh and Vincent (1973). A detailed accuracy analysis of Method A was given by Rapp (1973). Method B is described in Molodenskii, et. al. (1962, page 146) and Heiskanen and Moritz (1967, page 259) and has been used by Groten and Rummel (1974). Details of both methods will be given in subsequent sections.

2. Details of Method A and B

2.1 Method A

In Method A, the geoid is considered to be composed of three components \( N_1, N_2 \) and \( N_3 \) such that this sum yields the undulation:

\[
N = N_1 + N_2 + N_3
\]

Specifically we have \( N_1 \) being the undulation implied by a given set of potential coefficients. The computation of such undulations has been discussed by Rapp (1971). There are two methods of interest here. The first, Method One, is based on the solution of the geodetic boundary value problem. The result is:
\[ N_1 = \frac{GM}{r\gamma} \sum_{k=2}^{k_{max}} \left( \frac{a}{r} \right)^k \sum_{\ell = 0}^{\ell_{max}} (\bar{C}_{\ell k} \cos m\lambda + \bar{S}_{\ell k} \sin m\lambda) \frac{P_{\ell k}(\sin\gamma)}{r}. \]

where:
- \( GM \) is the geocentric gravitational constant;
- \( r \) is the geocentric distance to the point of which the undulation is being computed;
- \( a \) is the equatorial radius;
- \( \gamma \) is the normal gravity at the computation point;
- \( \bar{C}_{\ell k}, \bar{S}_{\ell k} \) are the differences between the actual potential coefficients and those implied by the adopted reference ellipsoid.

In practice, we have:

\[ \bar{C}_{2,0} = \bar{C}_{2,0}(\text{obs}) - \bar{C}_{2,0}(\text{ref}) \]

\[ \bar{C}_{4,0} = \bar{C}_{4,0}(\text{obs}) - \bar{C}_{4,0}(\text{ref}) \]

with all other \( C \) and \( S \) values equal to their observed values. In our computations, the reference coefficients were computed from,

\[ \bar{C}_{2,0}(\text{ref}) = -J_2 / \sqrt{5} \]

\[ \bar{C}_{4,0}(\text{ref}) = -J_4 / \sqrt{9} \]

where the \( J \) coefficients are (Cook, 1959):

\[ J_2 = 2/3 \left( f(1 - f/2) - m/2(1 - 2f/7 + 11f^2/49) \right) \]

\[ J_4 = -4/35 \left( f(1 - f/2)(7f(1 - f/2) - 5m(1 - 2f/7)) \right) \]

with:
- \( m = \omega^2 a^2 (1 - f) / GM \)
- \( \omega \) is the angular velocity of the earth taken as \( 7.2921151467 \times 10^{-5} \) rad/sec.

**ORIGINAL PAGE IS OF POOR QUALITY**
We also note that in (2) $P_{l,s}$ is the fully normalized Legendre polynomial for the geocentric latitude $\phi$.

A second method for determining $N_l$ is to first find a $r$ value that satisfies the following equation that describes the potential ($W_0$) of the geoid:

$$W_0 = \frac{GM}{r} \left[ 1 + \sum_{l=2}^{2l+1} \left( \frac{a}{r} \right)^l \sum_{s=0}^{l} \left( \frac{C_{l,s}}{l} \sin \lambda \right) + \frac{S_{l,s}}{l} (\sin \phi) \right] + \frac{\omega^2 r^2}{2} \cos^2 \phi.$$

The solution for $r$ is found by iteration in (8) after the geoid potential and other quantities in (8) are given. The undulation, $N_l$, is found by differencing $r$ with the corresponding $r$ of a specified reference ellipsoid. Specifically we have:

$$N_l = r - \frac{a \sqrt{1 - e^2}}{\sqrt{1 - e \cos^2 \phi}} - \frac{\omega^2 r^2}{2} \cos^2 \phi.$$

The procedure using (8) and (9) is essentially that used by Vincent and Marsh. The results from this procedure will be the same as the results obtained from (2) provided that consistent constants of $GM$, $a$, $\omega$, $f$, and $W_0$ are used. In both cases a zero-order undulation of the geoid is taken to be zero. (See section 9 where the removal of this restriction is discussed).

The $N_2$ component of (1) is computed in this method as follows:

$$N_2 = \frac{R}{4 \pi G} \int \frac{\Delta g_2}{\sigma^2} (\Delta g_2 - \Delta g_4) S(\phi) d\sigma$$

where:
- $R$ is a mean earth radius (6371 km);
- $G$ is a mean value of gravity (979.8 gals);
\[ \Delta \hat{g} \] is close to the mean free air anomaly and will be discussed in a subsequent section.

\[ \Delta \hat{g} \] is the mean anomaly implied by the potential coefficients used in computing \( N_3 \) as in (2);

\( \sigma \) is a limited cap about the computation point;

\( S(\psi) \) is the Stokes' function.

In practice the integration in (10) is replaced by a numerical integration. The value of \( \Delta g_s \) is:

\[ \Delta g_s = \frac{1}{A} \int_A \Delta g_s \delta A \]  

where:

\( A \) is the area in which the mean anomaly \( \Delta g_s \) is being determined. Specifically in the computation to be given here \( A \) will correspond to a \( 1^\circ \times 1^\circ \) mean anomaly. The value of \( \Delta g_s \) is computed from (Rapp, 1967):

\[ \Delta g_s = \frac{GM}{r^2} \sum_{l=2}^{l_{\text{max}}} (l-1) \left( \frac{a}{r} \right)^l \sum_{m=0}^l \left( \tilde{C}^m_l \cos m\lambda \right) 
+ \sum_{l=2}^{l_{\text{max}}} \left( \tilde{S}_l^m \sin m\lambda \right) \overline{P}_l^m (\sin \phi). \]  

The actual evaluation of (11) with (12) was carried out by the analytic integration of the \( \cos m\lambda \), \( \sin m\lambda \) terms and the numerical integration of the \( P_l^m \) term.

The \( N_3 \) term of (1) is formally given by:

\[ N_3 = \frac{R}{4\pi G} \int_{\sigma-\sigma_c}^{\sigma} (\Delta \hat{g}^2 - \Delta \hat{g}^*_s) S(\psi) \, d\sigma, \]  

where:

\( \sigma-\sigma_c \) represents the remaining global cap not included in \( \sigma_c \). The cap \( \sigma_c \) is chosen in such a way that \( N_3 \) can be neglected. A cap size discussion will be given in section seven.
2.2 Method B

This method has been used by Groten and Rummel (1974), for detailed geoid computations. Here we write:

\[ N = N_1' + N_2' + N_3' \]

where the primes have been used to distinguish these values from \( N_1, N_2, \) and \( N_3 \) given in (1). We have:

\[ N_1' = \frac{R}{2G} \sum_{\ell=2}^{\ell_{\text{max}}} Q_\ell(\phi_0) \Delta g_\ell \]

where:

\( Q_\ell(\phi_0) \ldots \) is the Molodenskii truncation function (Heiskanen and Moritz, 1967, p. 200) and is given as:

\[ Q_\ell(\phi_0) = \int_{\psi_0}^{\pi} S(\cos \psi) P(\cos \phi) \sin \psi \, d\psi \]

where:

\( \psi_0 \ldots \) is the cap size of gravity data to be included in \( N_3 \) and \( P_\ell \) are the Legendre polynomials. In the computation to be given here we have use a program supplied by M. K. Paul based on his accurate and fast algorithm (Paul, 1973).

The value of \( \Delta g_\ell \) is the \( \ell \)th degree component of the gravity anomaly implied by a set of potential coefficients and is given by:

\[ \Delta g_\ell = \frac{GM}{r^2} (\ell-1) \left( \frac{a}{r} \right)^\ell \sum_{s=0}^{\ell} \left( \frac{\ell^s_s}{\ell_s} \right) c_{\ell s} \cos m\lambda \]

\[ + \frac{S_{\ell s}}{\ell_s} \sin m\lambda \left( \frac{P_{\ell s}}{\ell_s} \right) (\sin \phi), \]
We have for \( N'_a \):

\[
(18) \quad N'_a = \frac{R}{4 \pi G} \int_{\sigma_e} \Delta \mathbf{R} \cdot \mathbf{S}(\psi) d\sigma
\]

where the \( \sigma_e \) cap has a radius \( \psi_e \). The anomaly \( \Delta \mathbf{R} \) is the same as in (10).

The \( N'_a \) term can be written as:

\[
(19) \quad N'_a = \frac{R}{2G} \sum_{l \geq l_{\text{max}}} Q_l(\psi_e) \mathcal{K}_l
\]

This term represents the information above degree \( l_{\text{max}} \) that has not been included in \( N'_a \).

3. The Effect of the Mass of the Atmosphere

In developing the Stokes' equation for computing the disturbing potential or geoid undulation it was assumed that there were no masses external to the geoid. In fact, there are topographic masses and atmospheric masses. A consideration of the topographic masses can be made by alternate solution of the boundary value problem. It turns out that the corrections to the results of Stokes' equation are small except in mountainous areas. Specifically, the corrections are zero in ocean areas, such as being considered here. In any event, procedures for handling the topography in this type of computation are discussed in Mortiz (1974, 1975) and are considered negligible for this paper.

In considering the atmosphere, we first define the potential of the geoid to be the sum of the gravity potential of the solid earth and oceans plus the potential of the atmosphere. Consequently, the computation of the geoid undulation using (8) requires that GM be that value including the mass of the atmosphere.

In the other phases of the geoid computations we must carry out the computations after the mass of the atmosphere has been removed from consideration, and then add any net effects back in. To solve this problem Moritz has shown that the mass of the atmosphere can be condensed onto the reference ellipsoid, so
that the mass of the latter will be equal to the mass of the solid earth and oceans plus the atmosphere. In this case equation (2), (12), and (17) are valid as they stand. To see this more clearly, we write the gravity potential at a point in the atmosphere as:

\[
W = W^0 + \frac{GM_a}{r} - G \frac{\int_0^\infty M(r')}{r'^2} dr'
\]

where \(M_a\) is the mass of the atmosphere and \(M(r')\) is the mass outside a sphere of radius \(r\) surrounding the earth. Equation (20) is written in slightly an approximated form. \(W^0\) is the gravity potential due only to the solid earth plus oceans. The normal potential is now defined (approximately) as:

\[
U = U^0 + \frac{GM_a}{r}
\]

where \(U^0\) is the normal potential due to a reference ellipsoid that has a mass equal to that of the solid earth plus oceans. The disturbing potential, \(T\), is:

\[
T = W - U = W^0 - U^0 - G \int_0^\infty \frac{M(r')}{r'^2} dr'
\]

\[
T = T^0 - G \int_0^\infty \frac{M(r')}{r'^2} dr'
\]

where, in terms of potential coefficients:

\[
T^0 = \frac{GM}{r} \sum_{L} \sum_{\lambda} \sum_{m} \left( \frac{a}{r} \right)^L \left( \frac{a}{r} \right) \frac{\cos m\lambda}{r} \frac{\cos m\lambda}{r} \sin m\lambda
\]

\[
+ \frac{\cos m\lambda}{r} \frac{\cos m\lambda}{r} \sin m\lambda \cdot (\sin^2 \lambda).
\]

The second term on the right hand side of (23) can be evaluated numerically. For
the case of \( r \) referring to the surface of the ellipsoid, the second term has a value of about 0.006 kga\( \cdot \) meter which would be about 0.6 cm in geoid height. Thus this term is negligible. Consequently, we can use (24) dividing by \( \gamma \) to obtain \( N \) (from potential coefficients). The resultant expression is (2).

The computation of the gravity anomaly in the case that the atmosphere is condensed onto the ellipsoid can be expressed as:

\[
\Delta g = \Delta g^0 + \delta g_a
\]

where:
- \( \Delta g^0 \) would be the gravity anomaly in a system where all atmosphere mass is condensed into the ellipsoid;
- \( \Delta g \) would be the usual anomaly where the atmosphere is not condensed into the ellipsoid;
- \( \delta g_a \) is a correction that can be computed knowing the elevation of the point and a model for the atmosphere.

In terms of potential coefficients, \( \Delta g^0 \) is given by (12), or by degree in terms of (17). Consequently, the computation of \( \Delta g_a \) in (10) or \( \delta g_a \) in (15) is not affected by the condensation of the atmosphere mass to the ellipsoid.

The anomaly to be used in the Stokes' integration based on terrestrial data, must be one to which the atmosphere correction term has been applied. Specifically, we must use in (10) and (15):

\[
\Delta g = \Delta g^0 - \delta g_a
\]

where:
- \( \Delta g^0 \) will be the usually given free-air anomaly and;
- \( \delta g_a \) will be given based on the mean height of the (in our case) \( 1^\circ \times 1^\circ \) block.

Values of \( \delta g_a \) can be taken as \( -\delta g \) where \( \delta g \) is tabulated for the Geodetic Reference System 1967 (IAG, 1971). If we assume that \( \delta g_a \) is constant within the integration cap used in the Stokes' integration, the effect of the atmosphere on the geoid undulation is:
\[ \delta N_4 = \frac{-R \delta \phi_0}{4 \pi G} \int_{\sigma_0}^{\infty} S(\psi) d\psi \]

Since (27) is evaluated in a circular cap whose radius is \( \psi_0 \), we can write (27) in the form:

\[ \delta N_4 = \frac{-R \delta \phi_0}{2G} \int_{\sigma_0}^{\psi_0} S(\psi) \sin \psi d\psi \]

Equation (28) can be written in the form:

\[ \delta N_4 = \frac{-R \delta \phi_0}{G} \cdot \xi(\psi_0) \]

where:

\[ \xi(\psi) = \frac{1}{2} \int_{0}^{\psi} S(\psi) \sin \psi d\psi \]

which is evaluated and tabulated in Lambert and Darling (1936). Using these values of \( \xi(\psi) \) and values of \( \delta \phi_0 \) from the Geodetic Reference System 1967, the following \( \delta N_4 \) values were computed.

**Table One. Effect of Atmosphere on Geoid Undulation Computations (meters)**

<table>
<thead>
<tr>
<th>( \psi ) (°)</th>
<th>Mean Elevation</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>0</td>
</tr>
<tr>
<td>5°</td>
<td>0.56</td>
</tr>
<tr>
<td>10°</td>
<td>1.17</td>
</tr>
<tr>
<td>15°</td>
<td>1.75</td>
</tr>
<tr>
<td>20°</td>
<td>2.26</td>
</tr>
<tr>
<td>25°</td>
<td>2.67</td>
</tr>
<tr>
<td>30°</td>
<td>2.97</td>
</tr>
</tbody>
</table>
The corrections in Table One should be added to the undulation component computed from (10) and (18) when \( \Delta g^2 \) is taken simply as the observed free air anomaly, \( \Delta g \).

From Table One we see that the correction is quite sensitive to the cap size, but insensitive to the elevation within the range tested.

In the actual geoid computations to be made for this report, 70% of the gravity material is in ocean areas where the elevation would be zero. The remaining areas would be in the eastern and central United States, which have a small mean elevation. Consequently, for this report we will use the \( \delta N_c \) value for a mean elevation of 0 meters. A more accurate procedure would require knowledge of the \( 1^\circ \times 1^\circ \) mean elevations. For this report this is not necessary, but for high elevation continental areas, such accurate computation for various cap sizes needs to be done in the future.

4. Numerical Integration of Stokes' Equation

The evaluation of (10) or (18) is carried out by summation in which an average \( S(\psi) \) value is needed. We write (18) (for example) as:

\[
N_s = \frac{R}{4\pi G} \sum \Delta g^2 \overline{S(\psi)} \Delta \sigma
\]

where:

\( \Delta \sigma \) is the area of the \( 1^\circ \times 1^\circ \) block and:

\[
S(\psi) = \frac{1}{\Delta \sigma} \iint S(\psi) \delta \sigma
\]

In practice (32) is evaluated by computing one, or several values of \( S(\psi) \) from the computation point to points in the block in which \( \Delta g^2 \) is given, and meaning the result. The number of values needed will depend on the size of \( \psi \) and the accuracy desired. Since \( S(\psi) \) changes rapidly for small \( \psi \) values, more points are required for an accurate mean when \( \psi \) is small than when \( \psi \) is large.
To investigate a proper integration procedure, we equate the undulation (in equation form) obtained by Method A and Method B. The following equality should then hold:

\[
\frac{R}{4\pi G} \int \frac{\Delta \varphi(\psi)}{\delta_c} S(\psi) d\varphi = \frac{GM}{2Gr} \sum \left( \frac{a}{r} \right) (1-Q_r) \sum \left( \frac{C^1_s}{l_s} \cos m\lambda \right) + \left( \frac{\delta}{l_s} \sin m\lambda \right) \frac{\bar{V}}{l_s} (\sin \bar{\psi}).
\]

Using the GEM 6 potential coefficients to \( L = 16 \), the right hand side of (33) can rigorously be computed yielding a "true" value. The left hand side of (33) can be evaluated by subdivision schemes until one is found that yields results consistent with the "true" value. Four subdivision schemes were tested:

**Subdivision One (1):**
Stokes' function is computed only for the center point of each anomaly block (the undulation computation point is at the corner of a \( 1^\circ \times 1^\circ \) block);

**Subdivision Two (4-1):**
Inside a spherical cap of \( \psi = 2^\circ \) around the computation point every \( 1^\circ \times 1^\circ \) block is divided into four equal (in terms of latitude/longitude increments) blocks for which the Stokes' function is evaluated at the center point and averaged.Outside \( \psi = 2^\circ \), the Stokes' function is evaluated based only on the center point of the \( 1^\circ \times 1^\circ \) block.

**Subdivision Three (16-4):**
Inside a spherical cap of \( \psi = 2^\circ \) a 16 sub-block system is used, while beyond \( 2^\circ \) a 4 sub-block system is implemented.

**Subdivision Four (64-16-4-1):** The following sub-block system is used here:

\[
\begin{align*}
\psi & \leq 2^\circ; \quad 64 \text{ sub-blocks} \\
2^\circ < \psi & \leq 5^\circ; \quad 16 \text{ sub-blocks} \\
5^\circ < \psi & \leq 10^\circ; \quad 4 \text{ sub-blocks} \\
10^\circ < \psi & < 20^\circ; \quad 1 \text{ sub-block}
\end{align*}
\]

Using these various sub-division schemes, the left hand side of (33) was evaluated.
with the results shown in Table Two, along with the "true" value computed from the right hand side of (33), for four points in the calibration test area.

Table Two. Influence on Undulation Computation of Various Subdivision Schemes Used in the Evaluation of the Stokes' Formula. (meters)

<table>
<thead>
<tr>
<th>Test Point (c, λ)</th>
<th>1(40°, 277°)</th>
<th>2(40°, 297°)</th>
<th>3(20°, 277°)</th>
<th>4(20°, 297°)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>-18.4</td>
<td>-26.8</td>
<td>4.0</td>
<td>-52.1</td>
</tr>
<tr>
<td>2</td>
<td>-18.4</td>
<td>-26.9</td>
<td>4.1</td>
<td>-52.5</td>
</tr>
<tr>
<td>3</td>
<td>-18.4</td>
<td>-27.0</td>
<td>4.1</td>
<td>-52.8</td>
</tr>
<tr>
<td>4</td>
<td>-18.5</td>
<td>-27.0</td>
<td>4.2</td>
<td>-52.9</td>
</tr>
<tr>
<td>&quot;true&quot;</td>
<td>-18.5</td>
<td>-27.1</td>
<td>4.2</td>
<td>-53.0</td>
</tr>
</tbody>
</table>

The best agreement with the "true" value exists for subdivision model four, which is thus chosen for use in the actual geoid computations in the calibration area. Since the actual integration error will depend on the magnitude of the anomalies in the Stokes' kernel, we would expect Method A would be somewhat less sensitive to integration errors than Method B, since in A an anomaly difference is used while in Method B, the actual anomaly is used. The exact sensitivity will depend on the magnitude and smoothness of Δg used in A (or in other words on the value of f_{max}). Consequently, we recommend the above subdivision model for use in either Method A or Method B of undulation computation.

5. Accuracy Analysis

5.1 Introduction

In this section we will try to estimate the accuracy of the geoids computed by the methods described in section two. In such an analysis we will try to estimate the optimum truncation angle θ_{max}. Several of the error terms have been discussed previously (Rapp, 1973) but they will be rediscussed here for the specific area of computation.

There are basically two data source errors. These arise from the errors in the potential coefficients, and the errors in the gravity anomalies. The vari-
The covariance matrix of the potential coefficients is designated $\Sigma_c$, and that
of the anomalies as $\Sigma g$. We will assume that these matrices are diagonal.
This assumption is true for the gravity anomalies since they are estimated inde-
dependently, but not exactly true for the potential coefficients.

5.2 Analysis for Method A

Method A is represented by (1). The first two terms on the right hand side
of (1) represent errors of commission, while $N_2$ represents an error of omis-
sion. For a single undulation error variance we write:

\begin{equation}
 \sigma^2 = \sigma_c^2 + \sigma_o^2
\end{equation}

where:
- $\sigma_c$ is associated with the commission errors;
- $\sigma_o$ is associated with the omission errors.

There should be no confusion with this $\sigma$, and that used previously to designate
the integration cap. To compute $\sigma$, we write:

\begin{equation}
 N_o = N_1 + N_2
\end{equation}

Considering (2) and (10), (35) can be written in matrix form as:

\begin{equation}
 N_o = H C + A (\Delta g' - \Delta g)
\end{equation}

where the elements of $H$ are the coefficients of the potential coefficients
(designated $C$ in (36)). The elements of $A$ are taken from (10). We can repre-
sent the computation of $\Delta g_o$ as:

\begin{equation}
 \Delta g_o = H^T C
\end{equation}
where the elements of \( P \) are found as the coefficients of the potential coefficients in (12). Inserting (37) into (36) we have:

\[
N_\sigma = B^T C + A^T \Delta g^2 + A^T B^T C
\]

Applying the propagation of error formulas we have:

\[
\sigma_\sigma^2 = \frac{1}{4} \Sigma_{\Delta g} B^T A + \frac{1}{2} \Sigma_{\Delta g} \Sigma_{\Delta g} A + \frac{1}{2} \Sigma_{\Delta g} B^T \Sigma_{\Delta g} B \cdot A
\]

- \( 2 \Sigma_{\Delta g} B \cdot A \).

The evaluation of this equation is complex and will not be attempted in this report, as a simpler formula will be found when using Method B for the undulation computation.

The specific evaluation of \( N_\sigma \) can not be done as we do not know the high degree potential coefficients. At best we can find a global average effect by writing (Rapp, 1973):

\[
\sigma_\sigma^2 = \frac{R^2}{4 G^2} \sum_{\ell=2}^{\infty} \sum_{m=1}^{\ell+1} s(\ell+2) Q_L^2(\psi) c_\ell(\Delta g)
\]

where \( c(\Delta g) \) are anomaly degree variances and \( s \) is (Tscherning and Rapp, 1974): 0.999617. Although the summation is taken to \( \nu \), in practice we would take the summation to about 200 as we are using 1\(^\circ\) data as the smallest terrestrial data block. For \( \psi = 10^\circ \), we get for \( \sigma_\sigma^2 \) about 1.1 meters and for \( \psi = 20^\circ \), about 0.7 meters.

Other error sources in the computation of point undulation include (for the computation in this paper) the fact that smaller anomalies than 1\(^\circ\) x 1\(^\circ\) anomalies may be needed, and that the reference set of constants may yield an equatorial gravity different from that implied by the best set of constants. These effects have been discussed in Rapp (1973). For our purposes we will assume that 1\(^\circ\) x 1\(^\circ\) data is the only data used: (there appears to be about ±0.4 m of more detailed information in ano-
maly data in blocks smaller than \(1^\circ \times 1^\circ\); and we will assume our equatorial gravity is true; if it is not, errors up to \(2.6\, \text{m}(\psi=20^\circ)\) for a 1 mgal error in equatorial gravity can be expected, exclusive of \(N_0\) considerations (see sec. 9).

5.3 Analysis for Method B

As in Method A, we have for Method B errors of commission and errors of omission. The commission errors arise in (15) and (17) due to potential coefficient errors, and in (18) due to anomaly errors. The omission error is caused by the fact that the summation in (15) is taken to \(\ell_{vs},\) instead of \(\ell\). This latter error is the same as given in (40) and the discussion given with respect to (40) is equally valid here.

To carry out this analysis we express the computational procedure in the form:

\[
N_c = H Q C + A' \Delta g^0
\]

where:

\[
\ldots \ldots \ldots A, B, \text{ and } C \text{ are as before and } Q \text{ is a diagonal matrix whose elements are composed of values of } Q_j(\psi_0). \text{ Error propagation thru } (41) \text{ yields for Method B:}
\]

\[
\alpha_s^2 = H Q \Sigma_{\Delta g} \Sigma_{B} + A' \Sigma_{\Delta g} A
\]

Comparing (42) with the corresponding result (39), for method A indicates that the error analysis for method B is considerably simpler than for method A. The actual implementation of (42) can be done through minor modifications of programs used in the evaluation of (15) and (18) since \(\Sigma_{\Delta g}\) and \(\Sigma_{\Delta g}\) are to be regarded as diagonal matrices. The accuracy of the geoid we will compute will be evaluated using (42) and (40) in (34).
6. Data Accuracy

6.1 Gravity Anomaly Accuracy

The gravity data to be used in these computations will be 1° x 1° mean anomalies. Each of these anomalies that has been estimated has an assigned standard deviation. In some cases an anomaly will be needed, within a cap, for which no estimate of that anomaly is available. In this case we will assume that the anomaly is zero and that its standard deviation is ±30 mgals, which is the root mean square variation of 1° x 1° mean free-air gravity anomalies.

The 1° x 1° data distribution within and around the calibration area is shown in Figure One. In this Figure One, zero (0) indicates those blocks for which an anomaly estimate is available and an * indicates that no anomaly exists. The outer borders of a 10° cap and a 20° cap are also shown.

6.2 Potential Coefficient Accuracy

The formal standard deviations for the GEM 6 potential coefficients were provided to us by Frank Lerch. These formal statistics are considered optimistic and we therefore used two approaches in estimating realistic standard deviations for the potential coefficients.

In the first approach the formal standard deviations were multiplied by a scale factor of 3.4 as suggested by Lerch, et. als. (1974). An average percentage error, by degree, can be defined as:

$$\frac{\text{RMS}(m_\ell,s)}{\text{RMS}(C_\ell,S_\ell)}$$

where:

- \text{RMS}(m_\ell,s) \ldots is the root mean square value of the standard deviation of the coefficients of degree \(\ell\), and,
- \text{RMS}(C_\ell,S_\ell) \ldots is the root mean square value of the coefficients of the GEM 6 solution of degree \(\ell\).

Values of (43) are plotted in Figure Two where it is seen that the percentage error increases so that it is about 80% at \(\ell = 16\), and even higher for the coefficients above 16 to 22.
Figure One. $1^\circ \times 1^\circ$ data distribution within and around the calibration area. Outer borders of calibration area, $10^\circ$ cap and $20^\circ$ cap are shown.

.. block where no anomaly was available
0... block with an anomaly estimate
Figure Two.

\[ \left( \frac{\%}{l} \right) = \frac{\text{RMS}(m_{\text{tot}})_l}{\text{RMS}(C,S)_l} \times \text{GEM} \]

- Dashed line: pessimistic error model
- Solid line: actual ratio (%)_l derived from (m_\eta)_l

Legend:
- Dashed line: pessimistic error model
- Solid line: actual ratio (%)_l derived from (m_\eta)_l
- Circles: ratio derived from GEM 6: SSE3 comparison
A second approach to potential coefficient accuracy determination starts with determining the percentage difference, by degree, between the GEM 6 coefficients and the coefficients of the Standard Earth III (Gaposchkin, 1974). This difference increases to a maximum of 130% at degree 12 as seen in Figure Two. With these differences a curve was drawn to represent the percentage accuracies with the specification that this percentage be 100% at degree 16. We then could estimate the standard deviation of the potential coefficients (but only by degree) by multiplying the root mean square coefficient value by the percentage error. Clearly, this second approach yields accuracy estimates more pessimistic than found in the first approach.

7. Optimum Cap Size

We now wish to determine an optimum \( \psi_0 \) that gives a minimum error in the determination of the geoid undulation. In order to do this we consider the various error sources that are associated with method B.

First we consider the commission error due to the errors in the gravity anomalies. This error will clearly depend on the geographic location of the computation point. In order to obtain a representative value, computations were carried out for nine representative points in the calibration area, as the cap size was varied from 0° to 30°. The standard deviations for the nine points were averaged and are plotted as a function of \( \psi \) in Figure Three. We see that the standard deviation, due to the anomalies increases from 1.0 meters at \( \psi = 0° \) to 1.2 meters at \( \psi = 30° \).
We next consider the commission errors due to the potential coefficients. Again values have been computed at nine points and averaged to obtain a representative number. Specifically, we have made computations for different $l_{max}$ values and different $\phi$ values for the two error models of the GEM 6 solution previously discussed in section 6.2. The resulting standard deviations are shown in Figure Four for error model one with $l_{max} = 8, 12, 16$ and $22$, and for $l_{max} = 16$ with error model two. Values are also given in Table Three.

In computing the values for the $l_{max} = 22$ solution it is necessary to adopt standard deviations for the potential coefficients not present in the GEM 6 set as we have in essence assumed these coefficients to be zero. Specifically, we have taken for their standard deviation, the root mean square coefficient variation implied by the following anomaly degree variance model given in Tscherning and Rapp (1974, p. 20):

\[
\sigma_{\ell} = \frac{A(\ell-1)}{(\ell-2)(\ell+1)}
\]

with $A = 425.28$ mgal$^2$, and $B = 24$.

Table Three. Undulation Standard Deviations Due to Potential Coefficient Errors (meters)

<table>
<thead>
<tr>
<th>$\phi$</th>
<th>$l_{max}$ 8 Error Model</th>
<th>$l_{max}$ 12 Error Model</th>
<th>$l_{max}$ 16 Error Model</th>
<th>$l_{max}$ 22 Error Model</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>1.3 3.7</td>
<td>2.0 5.0</td>
<td>2.8 5.7</td>
<td>3.7</td>
</tr>
<tr>
<td>2.5</td>
<td>1.0 2.8</td>
<td>1.3 3.4</td>
<td>1.5 3.6</td>
<td>1.6</td>
</tr>
<tr>
<td>5.0</td>
<td>0.7 1.9</td>
<td>0.7 2.0</td>
<td>0.8 2.0</td>
<td>1.3</td>
</tr>
<tr>
<td>7.5</td>
<td>0.5 1.2</td>
<td>0.6 1.4</td>
<td>1.1 1.8</td>
<td>1.7</td>
</tr>
<tr>
<td>10.0</td>
<td>0.4 0.9</td>
<td>0.7 1.6</td>
<td>1.2 2.1</td>
<td>1.4</td>
</tr>
<tr>
<td>12.5</td>
<td>0.4 1.0</td>
<td>0.8 1.6</td>
<td>1.1 2.1</td>
<td>1.2</td>
</tr>
<tr>
<td>15.0</td>
<td>0.4 1.2</td>
<td>0.8 1.9</td>
<td>0.8 2.0</td>
<td>1.1</td>
</tr>
<tr>
<td>17.5</td>
<td>0.4 1.3</td>
<td>0.6 1.7</td>
<td>0.7 1.7</td>
<td>1.0</td>
</tr>
<tr>
<td>20.0</td>
<td>0.4 1.2</td>
<td>0.5 1.4</td>
<td>0.7 1.5</td>
<td>0.8</td>
</tr>
<tr>
<td>22.5</td>
<td>0.4 1.1</td>
<td>0.4 1.2</td>
<td>0.6 1.3</td>
<td>0.7</td>
</tr>
<tr>
<td>25.0</td>
<td>0.3 0.9</td>
<td>0.4 1.0</td>
<td>0.5 1.1</td>
<td>0.6</td>
</tr>
<tr>
<td>27.5</td>
<td>0.3 0.8</td>
<td>0.3 0.9</td>
<td>0.4 0.9</td>
<td>0.5</td>
</tr>
<tr>
<td>30.0</td>
<td>0.2 0.6</td>
<td>0.3 0.7</td>
<td>0.3 0.8</td>
<td>0.4</td>
</tr>
</tbody>
</table>
Figure Four. Undulation Standard Deviations Due to Potential Coefficient Errors. (meters)

Model One for $l_{\max} = 8, 12, 16, \text{ and } 22$

Model Two for $l_{\max} = 16$
The differences in the results from the two error models have a maximum at $\psi = 0^\circ$ and decreases as $\psi$ increases.

The last error source considered here is that due to the neglect of the higher degree potential coefficients. This error is given by (40) where the summation is taken to 200 and (44) was used for the anomaly degree variance model. These results are given in Table Four and Figure Five for various $\lambda_{\max}$ and $\psi$ values.

Table Four. Undulation Error Caused by Potential Coefficient Truncation at Specified $\lambda_{\max}$. (meters)

<table>
<thead>
<tr>
<th>$\psi^\circ$</th>
<th>$\lambda_{\max}$</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>8</td>
</tr>
<tr>
<td>0</td>
<td>7.6</td>
</tr>
<tr>
<td>2.5</td>
<td>3.5</td>
</tr>
<tr>
<td>5.0</td>
<td>2.1</td>
</tr>
<tr>
<td>7.5</td>
<td>2.6</td>
</tr>
<tr>
<td>10.0</td>
<td>2.9</td>
</tr>
<tr>
<td>12.5</td>
<td>2.9</td>
</tr>
<tr>
<td>15.0</td>
<td>2.5</td>
</tr>
<tr>
<td>17.5</td>
<td>2.0</td>
</tr>
<tr>
<td>20.0</td>
<td>1.5</td>
</tr>
<tr>
<td>22.5</td>
<td>1.2</td>
</tr>
<tr>
<td>25.0</td>
<td>1.0</td>
</tr>
<tr>
<td>27.5</td>
<td>0.8</td>
</tr>
<tr>
<td>30.0</td>
<td>0.7</td>
</tr>
</tbody>
</table>

We can now quadratically add the three error sources together to obtain the final representative undulation standard deviation in the calibration area. The resultant standard deviation are plotted in Figure Six.

In considering Figure Six for the 8, 12, 16, and 22 solutions with potential coefficient error model one we see that the error at first decreases as $\psi$ increases, then it increases somewhat and finally decreases. At the $\psi$ values such as 7.5° for $\lambda_{\max}$ 12 we would expect a larger error than at smaller or larger $\psi$ values. This would indicate that one should choose an optimum $\psi$ value based on the $\lambda_{\max}$ of the potential coefficient field being used. Based on Figure Six we feel a $\psi$ 20° cap is reasonable.
Figure Five. Undulation Errors Caused By Potential Coefficient Truncation At \( l_{\text{max}} = 8, 12, 16, \) and 22.
The standard deviation of the undulation when the pessimistic error model for the potential coefficients is used is shown in Figure Six for the case of \( k_{zz} = 16 \). Although the errors are larger, the difference decreases as \( \phi \) increases so that at \( \phi = 20^\circ \) and \( k_{zz} = 16 \), the total standard deviation of the undulation using the optimistic potential coefficient error model is \( \pm 1.5 \) m while it is \( \pm 2.1 \) m when using the pessimistic error model.
For the final undulation computations the GEM 6 solution was used with \( l_{max} = 16 \). This was done so that the error analysis could be done without making assumptions about the coefficients between degree 17 and 22 not estimated in the GEM 6 solution. It will be shown that no significant undulation difference occurs when using a \( l_{max} = 16 \) or 22 in the case of the GEM 6 set.

8. The Geoid in the Calibration Area

The previous discussions have dealt with the method for detailed undulation computation and the method of accuracy analysis. We now turn to the computation of the detailed geoid and its accuracy in the calibration area using the GEM 6 potential coefficients and 1\(^\circ\) x 1\(^\circ\) gravity anomalies given on a tape dated July 1975.

We first define a set of constants identical to that used by Marsh and Vincent (1973) so that our undulations may be compared. These constants are:

\[
\begin{align*}
\omega &= 7.2921151467 \times 10^{-5} \text{ rad/s} \\
A &= 6378142 \text{ m} \\
f &= 1/298.255 \\
GM &= 3.986009 \times 10^{14} \text{ m}^3/\text{s}^2 \\
W_0 &= 6263687.52 \text{ kgal m} \\
\gamma_s &= 978032.14 \text{ mgal}
\end{align*}
\]

The GM includes the mass of the atmosphere and thus the effect of the atmosphere is included in the geoid potential \( W_0 \) and equatorial gravity, \( \gamma_s \). The normal gravity formula corresponding to these constants is then:

\[
\gamma_{grav} = \gamma_s (1 + 0.0053024269 \sin^2 \phi - 0.0000059 \sin^2 2\phi)
\]

Now the anomalies on the July 1975, 1\(^\circ\) tape were given with respect to the gravity formula of the Geodetic Reference System 1967 and thus need to be converted to be given with respect to the new constants. We have:

- If it did not, then the \( N_0 \) term from equation (51) would have to be evaluated.
Although this correction is small, it is systematic and its neglect could cause errors on the order of 0.8 meters in the computed undulation.

For the final results several different computations were performed using the GEM 6 potential coefficients and the 1° x 1° mean anomalies converted to a gravity formula consistent with the adopted constants. We first computed the geoid undulations using Method B with the GEM 6 coefficients truncated at degree 16 and with a cap size of 20°. These undulations are given in Table Five and in contour form in Figure Seven. These undulations include an atmospheric correction of 2.26 m obtained from Table One. The undulation standard deviations for the calibration area when using the potential coefficient error model one is shown in Table Six and when using the potential coefficient error model two in Table Seven. In the first case the standard deviations have a maximum of ±2.0 m with a minimum standard deviation of ±1.1 m. The corresponding values when using the second error model are ±2.4 m and ±1.8 m. These error estimates are all given with respect to the adopted set of constants, and exclude the error contribution due to the neglect of detailed gravity information in blocks below 1° x 1° in size. The accuracy of these standard deviations depends on how well the accuracy models for the anomalies, potential coefficients and truncation effects have been handled. We believe that the latter two effects have been handled reasonably. However, the anomaly error contribution has been based on the anomaly standard deviations that may be optimistic.

We next computed the geoid undulations using Method A described in section 2.1 with the identical data as used in Method B. A comparison of the resultant geoids showed a maximum discrepancy of 0.2 m with other statistics on the comparison given in Table Eight. We conclude that either method consistently applied will give the same undulation at the ±0.1 meter level.

A computation was made using method B when a truncation angle of 10° was used instead of 20°. The largest difference found was 3.6 meters with the
Figure Seven. Geoid Undulation Using Method B with GEM 6 Coefficients Truncated at Degree 16 and with a Cap Size of 20°.
Table Seven. Standard Deviations of the Grout Undulation (Table Five) Using the Potential Coefficient Error Model Two.
square root of the variance of the difference being ±1.55 meters. Based on
the standard deviations shown in Figure Six, we would expect the above dif-
ference to be ±1.3 m when using the optimistic potential coefficient error
model and ±1.8 m when using the pessimistic model. (The values are arrived
at by computing $\sigma_{\text{diff}}^2 = \sigma_{\text{opt}}^2 - \sigma_{\text{pess}}^2$). These expected values are very com-
patible with the result actually found.

In the computation described in the above paragraph, the atmospheric cor-
rection was rigorously applied with mean difference between the two results be-
ing -0.24 meters. A test computation was made when the atmosphere was not
considered in the anomaly data within the 10° and 20° caps. In this case the
resulting mean undulation difference was found to be -1.34 meters which is a
considerable increase from the -0.24 meters when the atmosphere was prop-
erly treated. These results indicate the practical value and need of the atmo-
spheric correction to gravity anomalies when the undulations of the geoid are
being computed.

Another computation that was made was with the GEM 6 potential coeffi-
cients taken to $\ell = 22$ with $\psi = 20^\circ$. The resulting undulations were compared
to the values computed using the coefficients to $\ell = 16$. The differences be-
tween the undulations was a maximum of 0.3 m with a negligible mean differ-
ence and variance as is shown in Table Eight.

Table Eight. Comparison of Various Undulation Computations (meters)

<table>
<thead>
<tr>
<th>Mean Diff</th>
<th>A</th>
<th>B</th>
<th>C</th>
<th>D</th>
<th>E</th>
</tr>
</thead>
<tbody>
<tr>
<td>$\sigma$</td>
<td>±0.09</td>
<td>±1.55</td>
<td>±0.18</td>
<td>±2.58</td>
<td>±3.52</td>
</tr>
<tr>
<td>Max (+) Diff</td>
<td>0.2</td>
<td>2.9</td>
<td>0.3</td>
<td>12.0</td>
<td>10.4</td>
</tr>
<tr>
<td>Max (-) Diff</td>
<td>-0.2</td>
<td>-3.6</td>
<td>-0.3</td>
<td>-0.6</td>
<td>-5.3</td>
</tr>
</tbody>
</table>

A: Difference between Method A minus Method B ($\ell_{\text{max}} = 16$, $\psi = 20^\circ$);
B: Difference between Method B ($\ell = 20^\circ$) minus Method B ($\psi = 10^\circ$);
C: Difference between Method B ($\ell_{\text{max}} = 22$) minus Method B ($\ell_{\text{max}} = 16$);
D: Difference between Method B ($\ell = 20^\circ$) minus solution of Vincent-Marsh;
E: Difference between Method B ($\psi = 10^\circ$) minus solution of Vincent-Marsh.

The final comparison that was carried out was the comparison of the cali-
bration geoid of this report to that geoid of Vincent and Marsh (1973), which was provided to us by Jim Marsh at 1° x 1° corner points. The results of the comparison are shown in Table Eight. Here we see that there is a strong systematic difference in the undulation of 3.87 m, about 1.2 meters of which is caused by the neglect by Vincent and Marsh of the influence of the atmosphere. The square root of the variance of the undulation differences is ±2.58 meters with the largest discrepancy being 12.0 m. (Again part of this latter discrepancy is due to their neglect of the atmosphere). The main cause of the non-systematic differences between the undulations is probably the 1° x 1° gravity data used in the computations.

9. The Zero-Order Undulation

The zero-order undulation of the geoid has been discussed by Heiskanen and Moritz (1967, p. 102) for the case of an undulation computation using Stokes equation in a global integration process. Specifically we have:

\[
N_0 = \frac{k \delta M}{2 GR} - \frac{R \delta g_2}{2 G}
\]

where \( k \delta M \) is the difference between a true value of the geocentric gravitational constant of the earth plus the atmosphere, and that adopted for the reference field. In addition \( \delta g_2 \) is the mean gravity anomaly, of those anomalies (after the atmospheric correction has been applied) referred to the adopted constants. Thus:

\[
\Delta g_0 = \frac{1}{4\pi} \iint (\Delta g - \delta g_2) \, \mathrm{d} \sigma
\]

This \( \Delta g_0 \) must also be subtracted from the \( \Delta g^2 \) given in (26) to assure that the anomalies used in Stokes' equation have a global average equal to zero. In this case an additional term will appear from (10) and (18) equal to:

\[
- \frac{R \Delta g_2}{4\pi G} \iint \frac{S(\psi)}{\delta g} \, \mathrm{d} \sigma = - \frac{R \Delta g_2}{G} \psi_0
\]
Equation (50) is now added to (48) to obtain the modified $N_0$ term that applies for both methods of computation of geoid undulations described in this report. We have:

$$N_0 = \frac{k \delta M}{2GR} - \frac{R \Delta g_0}{G} \left( \frac{1}{2} + \frac{1}{4} (\psi_0) \right)$$

If $\psi_0$ is 180° we have $N_0 = \overline{N_0}$. If $k \delta M$ and $\Delta g_0$ are zero $\overline{N_0}$ is zero. If $k \delta M = 0$, and $\Delta g_0 = 1$ mgal, $N_0$ is -4.6 m for $\psi_0 = 10^\circ$ and -5.8 m for $\psi_0 = 20^\circ$.

The value of $\Delta g_0$ can be determined from (49) if we have a global gravity field or from:

$$\Delta g_0 = \gamma' - \gamma$$

where $\gamma'$ is the true equatorial gravity based on the mass of the earth plus the atmosphere and $\gamma$ is the corresponding value adopted for use in the computations.

Thus, we have derived a new $N_0$ term that is cap size dependent. This $N_0$, if it can be determined, must be added to the undulations obtained from equation (1) or equation (14) to obtain the true undulation with respect to the adopted constants. If $N_0$ is set to zero, the computed undulations will refer to a set of unknown constants such that $k \delta M$ and $\Delta g_0$ are zero.

10. Summary

This paper documents two procedures that can be used for the computation of geoid undulations combining potential coefficient data and terrestrial gravity data. We found that the two methods yield essentially the same results (at the ±0.09 m level). However, the error analysis for Method B is simpler than that for Method A.

In developing the procedures for each method two important techniques must be used. First, it was found that the atmospheric correction is signifi-
cant and cannot be neglected as its neglect can cause errors in the computed undulation on the order of 2 meters with a truncation cap of 20°. Second, the numerical integration of Stokes' equation must be done in a precise manner or integration errors of about 1 meter will result.

A preliminary error analysis was done considering the error sources due to potential coefficient errors, gravity anomaly errors, and the truncation error caused by taking the potential coefficients to a certain maximum degree only. This analysis indicated that certain cap sizes (around 10°) would give poorer results than more optimum sizes, such as 20°, which was selected for use here.

The actual geoid undulations were computed in the Geos-3 calibration area using the GEM6 potential coefficients to degree 16 and the 1° x 1° mean anomalies available in July 1975. The results obtained showed a mean difference of 3.87 m from the Vincent-Marsh geoid with a difference variance of (2.58 m)². The estimated standard deviation of the undulations computed here were on the order of 1 to 2 meters with respect to the defined constants. This error analysis neglects the effect of using anomaly blocks of a size smaller than 1° x 1°, and the effect of ellipsoidal correction terms to Stokes' equation.

Although these computations have been done for the GEM6 coefficients they can easily be repeated for other coefficient sets with a corresponding error analysis provided a realistic variance-covariance matrix for the potential coefficients is available.
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