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200-KILOWATT WIND TURBINE PROJECT

A part of the
DEPARTMENT OF ENERGY
Federal Wind Energy Program

National Aeronautics and Space Administration
Lewis Research Center
Cleveland, Ohio 44135

January 1978
200-kilowatt wind turbine project

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Wind-energy systems have been used for centuries as a source of energy for man. The applications have ranged from pumping water and grinding grain to generating electricity. At times considerable interest existed in both the United States and Europe in developing large wind-driven generating systems as a source of electric power. However, interest in such systems declined because they were not cost competitive with the fossil fuel systems of that era. Also, these efforts were generally privately financed and thus suffered from the lack of a sustained research and development effort.

The continuing increase in energy requirements, increases in fuel costs, depletion of our fuel reserves, and dependence on foreign sources have made it necessary to investigate and develop alternate energy sources. Wind energy, being a clean, nondepletable source of energy, could be a viable alternate source. Thus, a Federal Wind Energy Program was established to enable research and development on the many applications and concepts of wind energy systems. This program, which originated at the National Science Foundation, is currently directed and funded by the newly created Department of Energy.

One phase of the Federal Wind Energy Program is to develop the technology necessary for the successful design, fabrication, and operation of large, horizontal wind turbine systems. This phase of the program is being managed by the National Aeronautics and Space Administration's Lewis Research Center for the Department of Energy. The three 200-kilowatt wind turbines described in this report compose the first of three separate systems currently under development. Wind turbines of the two other systems, although similar in design, will be larger in both physical size and rated power generation.

The overall objective of this project is to obtain early operation and performance data while gaining initial exper-
ience in the operation of large, horizontal-axis wind turbines in typical utility environments. Several of the key issues that will be addressed include the following:

- Impact of the variable power output (due to varying wind speeds) on the utility grid
- Compatibility with utility requirements (voltage and frequency control of generated power)
- Demonstration of unattended, fail-safe operation
- Reliability of the wind turbine system
- Required maintenance
- Initial public reaction and acceptance

**approach**

The approach used in managing this project, in addition to satisfying the overall objective, fulfilled the following two requirements:

- Involve utility companies in the project not only to provide a test site but to identify their particular requirements while gaining direct operational experience. This is necessary for their potential role of successful owner/operators of future wind turbine systems.

- Build up industry capability in the design, fabrication, and operation of wind turbine systems. This is necessary to achieve rapid commercial application once the technology has been developed.

The selection of utility company sites for experimental wind turbines was made on the basis of proposals submitted by the utility companies. Over sixty-four utility companies submitted detailed information about their company and the site they proposed for installation of a wind turbine. These proposed sites were evaluated on the basis of available wind energy, need for supplemental power, interest in supplying personnel for the program, and variations in climatic and topographical conditions. The 17 sites selected for more detailed evaluation are shown and listed in figure 1 along with the participating utility company. Identical meteorological towers and wind instrumentation were installed at each site so that the wind potential of the sites could be evaluated on a common basis.
<table>
<thead>
<tr>
<th>Site</th>
<th>Organization</th>
<th>Site</th>
<th>Organization</th>
</tr>
</thead>
<tbody>
<tr>
<td>Point Arena, California</td>
<td>Pacific Gas and Electric Co.</td>
<td>Boone, North Carolina&lt;sup&gt;b&lt;/sup&gt;</td>
<td></td>
</tr>
<tr>
<td>San Gorgonio Pass, California</td>
<td>Southern California Edison</td>
<td>Boardman, Oregon</td>
<td></td>
</tr>
<tr>
<td>Kaena Point, Oahu, Hawaii</td>
<td>Hawaiian Electric Co.</td>
<td>Island of Culebra, Puerto Rico&lt;sup&gt;b&lt;/sup&gt;</td>
<td></td>
</tr>
<tr>
<td>Russell, Kansas</td>
<td>City of Russell, Kansas</td>
<td>Block Island, Rhode Island&lt;sup&gt;b&lt;/sup&gt;</td>
<td></td>
</tr>
<tr>
<td>Holyoke, Massachusetts</td>
<td>City of Holyoke Gas and Electric Department</td>
<td>Huron, South Dakota</td>
<td></td>
</tr>
<tr>
<td>Ludington, Michigan</td>
<td>Consumers Power Co.</td>
<td>Amarillo, Texas</td>
<td></td>
</tr>
<tr>
<td>Kingsley Dam, Nebraska</td>
<td>Central Nebraska Public Power and Irrigation District</td>
<td>Augspurger Mountain, Washington</td>
<td></td>
</tr>
<tr>
<td>Clayton, New Mexico&lt;sup&gt;a&lt;/sup&gt;</td>
<td>Town of Clayton</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

<sup>a</sup>Three sites selected for 200-kW systems.

<sup>b</sup>Site selected for future installation of 2000-kW system.

Figure 1. - Candidate wind turbine sites.
The three sites selected for the installation of a 200-kilowatt wind turbine are Clayton, New Mexico, Island of Culebra, Puerto Rico, and Block Island, Rhode Island. All three sites currently use diesel or natural gas fueled reciprocating engines to drive their generators. The peak power demand for each of these utilities is in the 1500- to 2500-kilowatt range. The wind turbine installation at Clayton is shown in figure 2, with the crane used to hoist the tower mounted equipment shown in the background. An overall view of the Clayton site is shown in figure 3. The wind turbine at Clayton is currently undergoing checkout operations, having achieved first rotation on November 30, 1977. The wind turbines at Culebra and at Block Island are scheduled to become operational in June and December of 1978, respectively.

The overall wind turbine design, component specifications, engineering drawings, and testing requirements and procedures were established by the Lewis Research Center. Project responsibilities are as follows:

<table>
<thead>
<tr>
<th>Wind turbine site</th>
<th>Procurement/fabrication</th>
<th>Assembly/shop test</th>
<th>Installation</th>
</tr>
</thead>
<tbody>
<tr>
<td>Clayton</td>
<td>Lewis</td>
<td>Lewis</td>
<td>Contractor</td>
</tr>
<tr>
<td>Culebra</td>
<td>Lewis</td>
<td>Contractor</td>
<td>Contractor</td>
</tr>
<tr>
<td>Block Island</td>
<td>Contractor</td>
<td>Contractor</td>
<td>Contractor</td>
</tr>
</tbody>
</table>

Figure 2. - Clayton wind turbine.
The Special Services Division of Westinghouse Electric Corporation was selected by competitive bidding to be the contractor. Both Lewis and contractor personnel will be involved in the estimated 3-month checkout operation for each wind turbine. Following the acceptance testing for each wind turbine, the participating utility company will be responsible for maintaining the operation of each wind turbine for 2 years.

The rated power output of the wind turbine is 200 kilowatts, which is achieved at a turbine rotor speed of 40 rpm and a rated wind speed of 18.3 mph. The rated wind speed is defined as the lowest wind speed at which full power is achieved. The power output as a function of wind speed, shown in figure 4, is regulated by varying the pitch angle of the blades. At wind speeds below cut-in and above cut-out the rotor blades are placed in a feathered position and no power is pro-
produced. The cut-in wind speed, defined as the lowest wind speed at which power can be generated, is 6.9 mph. The cut-out wind speed, defined as the lowest wind speed at which wind turbine operation would result in excessive blade stress, is 34.2 mph. All of these wind speeds are measured at a 30-foot elevation.

**mechanical system**

The 200-kilowatt wind turbine system, shown schematically in figure 5, consists of the turbine rotor, nacelle, tower, hoist, and control building. The two propeller type rotor blades, which rotate about a horizontal axis, are located downstream of the tower. The drive train assembly, which converts the 40 rpm rotor speed to the 1800 rpm generator speed, is enclosed in a fiberglass nacelle for environmental protection. The nacelle and rotor assembly are positioned at the top of a tower to provide the necessary blade tip to ground clearance. The hoist provides access to the equipment mounted at the top of the tower. The onsite controls and electrical switchgear are housed in the control building at the base of the tower. A cutaway drawing of the tower mounted equipment with all major components identified is shown in figure 6. A photograph taken during the shop assembly of the Clayton machine, included as figure 7, shows the relative size and positioning of the various components. The primary design specifications and operating parameters are summarized in table I. Some of the components are now discussed in detail.
Figure 6. - Cutaway drawing of tower mounted equipment.

Figure 7. - 200-Kilowatt wind turbine assembly.
### TABLE I. 200-KILOWATT WIND TURBINE DESIGN SPECIFICATIONS

<table>
<thead>
<tr>
<th>Rotor</th>
<th>Generator</th>
</tr>
</thead>
<tbody>
<tr>
<td>Number of blades</td>
<td>Type: Synchronous ac</td>
</tr>
<tr>
<td>Diameter, ft</td>
<td>Rating, kVA: 250</td>
</tr>
<tr>
<td>Speed, rpm</td>
<td>Power factor: 0.8</td>
</tr>
<tr>
<td>Direction of rotation</td>
<td>Voltage, V: 480 (three phase)</td>
</tr>
<tr>
<td>Location relative to tower</td>
<td>Speed, rpm: 1800</td>
</tr>
<tr>
<td>Type of hub</td>
<td>Frequency, Hz: 60</td>
</tr>
<tr>
<td>Method of power regulation</td>
<td>Orientation drive</td>
</tr>
<tr>
<td>Cone angle, deg</td>
<td>Type: Ring gear</td>
</tr>
<tr>
<td>Tilt angle, deg</td>
<td>Yaw rate, rpm: 1/6</td>
</tr>
<tr>
<td></td>
<td>Yaw drive: Electric motors</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Blade</th>
</tr>
</thead>
<tbody>
<tr>
<td>Length, ft</td>
</tr>
<tr>
<td>Material</td>
</tr>
<tr>
<td>Weight, lb/blade</td>
</tr>
<tr>
<td>Airfoil</td>
</tr>
<tr>
<td>Twist, deg</td>
</tr>
<tr>
<td>Solidity, percent</td>
</tr>
<tr>
<td>Tip chord, ft</td>
</tr>
<tr>
<td>Root chord, ft</td>
</tr>
<tr>
<td>Chord taper</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Tower</th>
</tr>
</thead>
<tbody>
<tr>
<td>Type</td>
</tr>
<tr>
<td>Height, ft</td>
</tr>
<tr>
<td>Ground clearance, ft</td>
</tr>
<tr>
<td>Hub height, ft</td>
</tr>
<tr>
<td>Access</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Transmission</th>
</tr>
</thead>
<tbody>
<tr>
<td>Type</td>
</tr>
<tr>
<td>Ratio</td>
</tr>
<tr>
<td>Rating, hp</td>
</tr>
</tbody>
</table>

**Blades.** - The rotor blades are made of aluminum, except for the cylindrical blade root shank, which is made of steel. The blade, shown in figure 8, consists of a main load carrying spar and ribs covered by a thin sheet metal skin. The construction is similar to that of a conventional airplane wing.

**Hub.** - The rotor hub (shown in fig. 9) connects the blades to the low speed shaft and houses the pitch change mechanism. The hub is a rigid type; that is, the blade is rigidly attached to the hub and the blade is permitted only the pitch change degree of freedom. The hub transmits the torque developed by the rotor blades to the shaft and transmits all other blade loads into the bedplate through the low speed shaft bearings.

**Pitch change assembly.** - The pitch change assembly consists of a hydraulic supply, a rack and pinion actuator, and gears to rotate the blades in the hub. This type of pitch
change mechanism is similar to that used in the aircraft industry on variable pitch propellers. As shown in figure 10, a pair of racks is moved linearly back and forth by hydraulic pressure. This pair of racks rotates a pinion that turns a master gear, which in turn rotates the blades through bevel gears bolted to the blade spindle. The hydraulic supply is mounted separately inside the front of the nacelle as shown in figure 6. Hydraulic fluid is brought into the main shaft through rotating seals and transmitted to the rack and pinion actuator mounted on the rotor hub. The maximum rate of pitch change is $8^\circ$ per second.

Drive train assembly. - The drive train assembly that transmits the mechanical power of the spinning rotor to the generator, which generates the electrical power, is shown in figure 6. The hub transmits the high-torque-low-speed power to the gearbox through a low-speed shaft. A 1 to 45 fixed ratio gearbox transmits this power to the high-speed shaft at low-torque-high-speed power. This power is then transferred to the generator through a belt and pulley drive system. The belt and pulley drive system offers the flexibility of making small changes in the nominal 40 rpm of the low-speed shaft, while still maintaining the constant 1800 rpm required by the generator. If test data show that a higher or lower turbine rotor speed would be desirable, the
Figure 9. - Hub and pitch change with actuator.

Figure 10. - Blade pitch change diagram.
ratio of the shaft speeds may be changed.

**Disk brake.** - A disk brake system, located on an extension of the high-speed shaft, serves as both a parking brake and a dynamic brake to stop the rotor during an emergency shutdown.

**Bedplate.** - The bedplate is the steel structural member that supports the entire rotor and nacelle assembly.

**Yaw assembly.** - The entire machine on top of the tower is supported on a turntable bearing which permits rotation to maintain proper alignment with the wind. Rotation is achieved by driving a large bull gear with two pinion gears as shown in figure 6. The two pinion gears, which are pre-loaded against each other to increase torsional stiffness, are driven by separate motors and yaw drives. If necessary, yaw control can be achieved by using only one unit. The yaw rate, which is 1/6 rpm, is operational whenever the wind speed exceeds the cut-in wind speed of the wind turbine.

**Yaw brake.** - The torsional stiffness of the rotating machinery is further increased by activating the three yaw disk brakes shown in figure 6. Even during the yawing motion some brake pressure is applied to damp out any torsional oscillations by maintaining a drag force. Once the machine has aligned itself to the wind, this brake pressure is increased to the maximum.

**Fluid coupling.** - The function of the fluid coupling on the high-speed shaft is to damp out the power oscillations resulting from the continuously varying wind velocity that the blades must withstand due to the tower shadow and the wind shear effects.

**Generator.** - The generator is a commercially available synchronous machine having the specifications given in table I.

**Tower.** - The open truss type tower uses round pipe members rather than other structural steel shapes to maximize the airflow through the tower. The increased airflow through the tower reduces the cyclic stresses on the rotor blades as they pass through the tower wake. The tower is anchored to a concrete slab foundation.

**Hoist.** - Access to the tower mounted components is provided by a cable mounted hoist. This system was selected over conventional stairs to further maximize the airflow through the tower.
control system

The wind turbine control system shown schematically in figure 11 must provide for the safe and reliable operation of the wind turbine at a remote, unattended site. To achieve this, the control system must automatically perform the following three major functions:

- Control production of electric power over a wide range of wind velocities - including all necessary startup, shutdown, and synchronizing activities
- Alignment of the rotor assembly with the wind direction
- Protection against damage due to abnormal operating conditions and/or extreme environmental conditions

Each of the five major elements of the control system now discussed is designed to provide high reliability while using proven off-the-shelf components.

Microprocessor. - The microprocessor provides the control logic for operating the wind turbine by continuously monitoring the output of the wind speed sensor. When the wind speed is above the cut-in value, the controller starts the wind turbine, brings it up to speed, and synchronizes it to the utility grid. The microprocessor automatically shuts down and secures the wind turbine whenever the wind speed either drops below cut-in or exceeds cut-out.

Figure 11. - Simplified wind turbine control schematic.
**Blade pitch controller.** - Input from the wind sensor and the generator is fed into the pitch control logic of the microprocessor, which in turn controls blade pitch. Below cut-in wind speed and above cut-out wind speed the blades are feathered. Between cut-in wind speed and rated wind speed the blade pitch is held at a fixed value. For wind speeds between rated and cut-out the blade pitch is controlled to maintain a constant power output of 200 kilowatts.

**Yaw controller.** - The yaw controller detects wind direction from a wind direction sensor located on top of the nacelle, and it keeps the wind turbine properly aligned with the wind whenever the wind speed is above the cut-in speed. Orienting the wind turbine at wind speeds below cut-in serves no useful purpose, and it would decrease the effective service life of the yaw drive system.

**Safety system.** - The safety system, which is an automatic shutdown system that operates independently of all other wind turbine controls, is designed to protect the wind turbine from catastrophic failure. Various sensors monitor key parameters such as the rotor speed, generator current, electrical load, vibration, yaw error, pitch system hydraulic fluid level, bearing temperatures, gearbox oil temperatures, microprocessor failure, etc. If any sensor signal is outside the normal safe operating range, the safety system will automatically shut down the wind turbine. For example, in the event of rotor overspeed, a speed sensor would issue the command to feather the blades; this automatically stops the rotor by reversing the direction of torque on the rotor. A backup pneumatic system assures that the blades will feather even if the hydraulic system fails. However, if for any reason the blades fail to feather and the machine continues to overspeed, a second totally redundant and physically separate speed sensor acutates an emergency brake which stops the rotor within a few seconds.

**Remote control and monitoring system.** - The remote control and monitoring (supervisory) system at the utility power dispatcher's center permits manual start-stop control of the microprocessor by the power dispatcher. A digital readout of wind speed, rotor speed, power, VARS, current, and voltage is provided by the supervisory system. In the event of automatic shutdown by the safety system, an indication of overspeed,
blades feathered, yaw error, over-
current, fluid system fault, vibration
fault, overtemperature, and micro-
processor status associated with the
shutdown is provided.

**annual energy output**

The calculated annual energy out-
put for the 200-kilowatt wind turbine
operating in various average wind
speed environments is shown in fig-
ure 12. The average wind speed is
the arithmetic average of all hourly
wind speeds in a given year at that
particular site measured 30 feet above
ground level. The energy output is a
strong function of the average wind
speed, since the available energy in
the wind is proportional to the cube
of the wind speed. The energy output
was computed using a rotor power
coefficient of 0.36 and a rotor shaft
to generator output efficiency of 0.9.
Velocity profile curves for the wind
were assumed to be Weibull distri-
buted. Energy capture by the rotor
was computed using the wind speed
occurring at the hub height of 100
feet. Wind speeds at various eleva-
tions are calculated by using the
wind shear gradient typical of most
of the candidate wind turbine sites.
It was estimated that the machine
would be shut down 10 percent of
the time when the wind velocity was
between cut-in and cut-out speeds.
This shutdown time was allowed for
both scheduled and unscheduled
maintenance.

**concluding remarks**

The 200-kilowatt wind turbine
project described in this report is
one phase of the Federal Wind Energy
Program managed by the NASA Lewis
Research Center for the Department
of Energy. The overall objective is
to obtain early operation and perfor-
mance data by operating the three
200-kilowatt wind turbines installed
in utility networks representative of
future applications. Involving the utilities insures that their needs, concerns, and requirements are understood and met, and it also enables the utilities to gain initial operating experience. The operation of these wind turbines will provide valuable early data to help establish both the technical and economic feasibility of using wind turbines as a supplemental source of energy.

FOR MORE INFORMATION on wind energy and other alternative energy resources, write to:

DOE Technical Information Center
P.O. Box 62
Oak Ridge, Tennessee 37830

A general overview on wind energy is given in the 72-page booklet "Wind Machines," which can be ordered as document 038-000-00272-4 for $2.25 from:

Superintendent of Documents
U.S. Government Printing Office
Washington, D.C. 20402

Detailed technical reports about wind systems and other energy technology subjects may be purchased from:

National Technical Information Service
U.S. Department of Commerce
5285 Port Royal Road
Springfield, Virginia 22161