HOT-WIRE AND HOT-FILM ANEMOMETRY

C. Rasmussen and B. B. Madsen

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1. Introduction

Thanks to manifold advantages, the hot-wire and hot-film anemometer has gained increasing importance investigating the micro-structure of time and space variable velocity fields of flowing gases and fluids. What is meant here by "micro-structure of velocity fields" is always the instantaneous value for the velocity of particles which in terms of volume are small compared to the total flow but large compared to molecular dimensions.

Such studies are important for understanding and describing various complicated macriscopic flow actions, as for example the static and dynamic forces having an effect upon a body found in the flow, the response time of valves and other flow controlling equipment, the flow resistance of pipes, the research of actions in flow boundary layers, heat exchange problems, the blending of gases and many more others.

A small, sensitive transducer is needed in addition to this with the shortest possible response time and no disturbing effect on the flow to be investigated.

In this paper the measuring principle and the design of the measuring sensors are to be explained to begin with; then follows a short description of the circuit techniques of anemometers, and in conclusion some typical examples for use will be covered.
2. Hot-wire and Hot-film Transducer

The measuring sensor of the anemometer is either a thin wire stretched between two tips or a thin metal film coated on a glass body. This wire or film is heated up electrically, with the dissipated heat of the flow or the supplied electrical input being a gauge for the velocity of the flow medium.

The strength of wire probes is sufficient to be usable in gases up to high flow velocities (for example in atmospheric, pure air up to low supersonic velocities) in the same way wire probes are employable in non-conductive fluids at low flow velocities.

Diagram 1 shows the model types of various hot-wire and hot-film probes.

Diagram 1. Model types of various hot-wire and hot-film probes.

2.1. Static properties of probes

The laws of convective heat dissipation are the basis for the use of heated sensor elements to measure the particle velocities in flows. The connection between the particle velocity and the heat dissipation is in general too complicated for a theoretical
consideration; it therefore has to be determined experimentally apply-
the laws of similarity.

What is more, the heat is dissipated both by natural convection
and the wire terminals or the material of the film carrier.

A theoretical solution was found by L. V. King [1] in 1914 for the
heat dissipation of a uniformly heated cylinder, pre-supposing a two-
dimensional incompressible and friction-free potential flow. For
the product from Prandtl's number (= Péclet's number) larger than 0.08,
King's solution can be approximated by the following equation, using
the symbols given in the appendix:

\[ Q = \frac{kU}{l} \left( 1 + \frac{2\pi \alpha \rho dU}{k} \right)(T - T_0) \]  
(1)

or — dimensionless — by

\[ N_u = \frac{1}{\pi} + \frac{2}{\pi} Re Pr \]  
(2)

But the pre-conditions assumed by King are not completely correct,
and even the heat dissipation is of a more complex nature. More
recent experiments by Collis and Williams [2] have shown that the
equation

\[ N_u = \left( \frac{T_m}{T_0} \right)^{0.24} (0.24 + 0.56 Re^{0.45}) \]  
(3)

for hot-wires operated in air in the range 0.02 < Re < 44 produces
the best approximation.

The results achieved by King, Collis and Williams are applicable
to wires with a large ratio I/d, so that the heat dissipation can
be viewed as two-dimensional. For the hot-wires used in general with
a ratio I/d in the order of magnitude of 100, the heat dissipation
through the wire mounting makes itself felt, whereby a direct cali-
bration becomes necessary.

It is true for the thermal state of equilibrium that the heat
loss Q of the hot-wire has to be equal to the supplied electrical
input, thus \( I^2 \cdot R \).
What is interesting more than anything else from the aspect of anemometry is the relationship between the particle velocity and the electrical input. This relationship can be expressed for hot-wire and hot-film probes at a certain overheating ratio, in a given flow medium with constant temperature by the equation:

\[ \frac{rR}{R-R_0} I^2 = A + BU^n, \]

with A, B and n being constants.

The output voltage of an anemometer is accumulated at a bridge circuit, the square of this voltage is proportional to the heat loss of the wire at the respective velocity.

Diagrams 2 and 3 show typical calibration curves of a hot-wire and hot-film transducer, respectively.

![Diagram 2](image)

Diagram 2. Calibration curve of a constant temperature anemometer (DISA type 55D01) in air with a hot-wire transducer of the type 55A22. V bridge voltage, U flow velocity, approached curve \( V^2 = 5.9 + 5.2 U \)

Diagram 4 shows schematically the most common calibration methods.

2.2. Dynamic properties of probes

To be able to describe the behavior of the hot-wire to time changes in the flow velocities, equation (4), determined empirically, will have to be supplemented for dynamic actions by an additional term considering the thermal inertia of the wire.
Diagram 3. Calibration curve of a constant-temperature anemometer (DISA type 44D0l) in water with a hot-film transducer of the type 55A81 at two different overheating ratios a. V bridge voltage, U flow velocity.

Assuming a uniform temperature distribution along the wire, we obtain

$$\frac{R}{R-R_0}T^2 = A + B(U)^n + \frac{C}{R-R_0} \frac{dR}{dr},$$

(5)

In this

$$C = \frac{C_m}{\alpha R_0}$$

is the modified heat capacity of the wire.
In the following discussion of the modes of operation of a hot-wire, we shall return to this equation (5).

The first and simplest mode of operation is the heating of the wire with time constant-current from a constant-current source with high internal resistance. The change in resistance caused by cooling or the voltage loss at the wire is then a gauge for the flow velocity. In the second method the wire temperature is kept constant, with the heating current changing with the velocity. The third, known as the method of the constant-overheating ratio, uses two wires. This special technique is applied then, whenever the velocity changes are attended by temperature changes. At a constant-overheating ratio in relation to the temperatures of the flow medium, the probe then responds to only velocity changes.

Returning to equation (5), the dynamic behavior of the wire at a constant-heating current is to be considered now.

The instantaneous wire resistance is composed of two parts. The long-time mean value is to be marked by a bar and the time variable value by a small letter:

\[
R = \overline{R} + r \\
U = \overline{U} + u
\]  

(6)

By insertion into equation (5), the following differential equation is obtained for resistance changes:

\[
\frac{dr}{dt} = \frac{R_0(A+B(U)^n)}{RC} \cdot \frac{Bn(U)^{n-1}(R-R_0)}{C} \cdot u.
\]  

(7)

This differential equation of the first degree is characterized by the time constant:

\[
T = \frac{RC}{R_0(A+B(U)^n)}
\]  

(8)

Hence, if the wire for example is subjected to a sudden rise in velocity, then the wire resistance drops and assumes a new value on an exponential curve. As a result the time constant is proportional to the heat capacity and to the resistance ratio of the wire and
decreases with rising flow velocity (hereto see also Diagram 5).

The dynamic characteristic can be described in addition by the behavior with sinusoidal changes of the flow velocity, as is shown in Diagram 6.

The upper limiting frequency of a wolfram wire of 5 μm diameter amounts to about 500 Hz, whenever it is operated in atmospheric air at a resistance ratio of 1.8 and at a flow velocity of 100 m/s. This limiting frequency can be raised, however, several hundredfold by electronic aids.

The frequency variation of a hot-film probe (see Diagram 7) is strongly dependent upon the thermal properties of the carrier material. The thermal inertia of the thin platinum film even with a thickness of about 100 Å is negligible on the other hand.

A sinusoidal change of the hot-film temperature causes a strongly attenuated temperature wave in the surface of the carrier material. The wavelength is many times over larger than the skin effect which is of the following magnitude:

\[ \delta \approx \frac{k_b}{\sqrt{\omega c_b}} \]
The phase of the heat flow in the carrier material will lag the surface temperature as a result by an angle \( \phi \).

With Pyrex-glass as a carrier material we obtain \( \delta \approx 0.4f \) (\( f \) in Hz, \( \delta \) in mm). The thermal boundary layer affects the frequency variation even at very low frequencies. For higher frequencies the attenuation amounts, however, to only 3 dB/octave, and the phase shift approaches \( 45^\circ \).

3. Electronics of the Anemometer

The electronic part of the anemometer is to enable the stable operation of the probe and to expand its properties, above all relating to the frequency variation.

3.1. Constant-current operation.

In the constant-current operation of a Wheatstone bridge, in the one branch of which the transducer is located, is fed from a current source in series with an adjustable resistance. The series resistance is to be as large as possible compared to the total resistance of the bridge in order that the same current always flows through the network.

The voltage resulting at the vertical diagonal of the bridge is then a gauge for the flow velocity.

For the velocity components above the limiting frequency of the transducers there is produced an amplitude drop of 6 dB/octave, \( /R^2 \) and the phase of the output signal will lag with an angle \( \varphi = \arctan \omega R \) compared to the actual flow action. The frequency variation is characterized, however, by a single time constant and can be compensated, therefore, by a simple RC-member which increases the amplification for higher frequencies.

Diagram 8 shows the block circuit diagram of a constant-current anemometer with a compensation network and an additional amplifier.
With the time constant of the transducer corresponding to equation (8) depending upon the mean flow velocity, the compensation network has to be re-adjusted with a change of the latter.

The frequency variation of a hot-film probe can not be characterized by a single time constant. It would be very difficult to realize a compensation amplifier like the probe with opposite properties; for that reason, hot-film transducers are practically not used in the constant-current operation.

3.2. Constant-temperature operation

This mode of operation offers basic advantages in operation in regard to accuracy and simplicity, but more than anything else it is practicable, too, for large velocity fluctuations.

The fundamental idea of this mode of operation consists of reducing the affect of the probe's thermal inertia by keeping the sensing element always at a constant temperature (resistance) and using the necessary heating current for it as a gauge for the velocity.

This principle was proposed by Kennelly [3] previously in 1909; of course the necessary highly developed electronic system could not be realized until much later. Its block circuit diagram is depicted in Diagram 9.

In the state of equilibrium a certain voltage lies at the vertical diagonal of the bridge which is delivered by the servo amplifier. If the convective cooling at the probe is altered, then a small voltage will result at the

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**Diagram 8.** Principle circuit diagram of a constant-current anemometer.

**Diagram 9.** Principle circuit diagram of a constant-temperature anemometer.
horizontal diagonal which — amplified many times — is coupled back to the vertical diagonal. Consequently the polarity of this coupled-back voltage is selected in such a way that the bridge balances automatically, and it can be shown [4], that by this the upper limiting frequency is increased by the factor

$$g \approx 2aRS$$

With this $$n = \frac{(R - R_n)/R_n}$$ is the overheating ratio and S the gradient of the servo amplifier.

Because of the inclination to high frequency oscillations in a closed loop of this kind, it is found difficult to expand the frequency range by enlarging the gradient of the amplifier, as this too is known from control engineering. The art of constant-temperature anemometry lies consequently in the design of a stable controlled system with high loop amplification.

The amplification of the DISA-constant-temperature anemometer of the type 55D01 can be adjusted, for example, in 11 stages from 150 to 5000, with a maximum upper limiting frequency of 400 kHz in the bridge ratio 1:1 (active to inactive branch) and 150 kHz in the bridge ratio 1:20 being produced with a standard hot-wire probe.

While the bandwidth is limited by the spatial resolving of the probe in measuring turbulence, the large bandwidth of the system reduces, nevertheless, phase shifts and can be used to advantage in measuring spasmodic passing flow actions, as for example in impulse wave tubes.

4. Applications

In general the probe will respond to every change of heat dissipation. This can be caused for example even by a change of temperature or pressure of the flow medium. Although even these magnitudes can be measured with the aid of the anemometer, only applications in anemometry are to be considered in the following.
4.1. Measurements of the mean flow velocity

The basic non-linear relationship between flow velocity $U$ and output voltage $V$, given by the equation

$$V^2 = A + BU^n,$$

(10)

can be linearized electronically, for example, by an analog computing element with the transmission characteristic

$$V_{\text{out}} = k(V_{\text{in}}^2 - V_{\text{in}}^2)^m.$$  

(11)

With $V = V_{\text{in}}$,

$$V_{\text{in}}^2 = A, \quad m = \frac{1}{n},$$

we obtain from the two equations:

$$V_{\text{out}} = K(A + BU^n - A)^m = KBU^n,$$

(12)

thus a velocity proportional output voltage.

Often we shall dispense with a linearization for stationary actions or for turbulence degrees under 10% and use the direct calibration curve.

4.2. Measurement of dynamic flow actions

With an ideal anemometer we would be able to measure at one point the instantaneous value of the flow velocity in three directions.

Although these requirements are not completely met, the hot-wire anemometer is still the best approach to this ideal, and practically the entire empirical knowledge on turbulence was gained with the aid of instruments of this kind.

Because of its large frequency range the hot-wire anemometer is particularly well suited for investigating the dynamic response of flow mechanical elements (Fluidies) which are used in pneumatic and hydraulic controlled systems.
Because of the small dimensions of transducers the boundary layer flows are disturbed only to a slight extent whenever a probe is brought in from without. In this manner, velocity profiles in boundary layers can be determined immediately.

Of course a correction becomes necessary [6] for wall clearances smaller than 0.2 mm as a result of a heat transfer to the wall.

With the aid of film transducers inserted flush into the wall it is likewise possible to measure the wall stresses [7].

The measuring procedure can be applied in gaseous and liquid media. For measurements in electrolytic conducting liquids (for example tap water) quartz-coated film probes come into question more than anything else.

4.3. Directional measurements

The hot-wire is dependent upon direction, and it has its maximum sensitivity with vertical incident flow. In the range $45^\circ < \theta < 135^\circ$ the ensuing effective velocity, for example, in equation (10) can be approximated by [5]:

$$U_{eff} = U \sin \theta$$

(13)

This effect can be used directly to advantage for stationary or periodic passing actions by locating the sharply pronounced minimum for directional measurements by twisting the probe.

So-called X-probes are used for static running off actions. These consist of two wires forming an angle of 45° with the mean flow direction and connected respectively to an anemometer. By adding or subtracting the instantaneous values of both output signals of the anemometers and formation of effective values, the velocity components can be determined then simply and directly for non-isotropic turbulence.
Other applications are not to be discussed here; however reference is made to the bibliography.

Appendix

Symbols used:

- $Q$: Heat losses
- $T$: Temperature of the heated transducer
- $T_o$: Temperature of the ambient flow medium
- $R$: Operating resistance of the heated transducer
- $R_o$: Resistance of the transducer at ambient temperature
- $U$: Flow velocity
- $V$: Bridge voltage
- $V_{out}$: Output voltage of the linearizer
- $V_{in}$: Input voltage of the linearizer
- $V_{in_o}$: Input voltage of the linearizer at 0 voltage output voltage
- $I$: Probe current
- $S$: Amplifier gradient
- $I_m$: $(I - I_0)/2$ Mean temperature
- $R_c$: $dU/dR$ Reynolds' number
- $P_r$: Prandtl number
- $P_c$: Peclét number
- $C_w$: Heat capacity of the wire
- $a$: $\frac{R - R_m}{R_m}$ Overheating ratio
- $d$: Diameter of the wire
- $L$: Length of the wire
- $c_w$: Specific heat of the wire
- $c_b$: Specific heat of the carrier material
- $c_p$: Specific heat of the fluid at constant pressure
- $K$: Heat conductibility of the fluid
- $K_b$: Heat conductibility of the carrier material
- $r$: Alternating component of the resistance
- $u$: Alternating component of the velocity
- $f$: Frequency in Hz
- $v$: Kinematic viscosity of the fluid
- $\omega$: Circular frequency
δ  Skin effect
φ  Phase angle
ρ  Density of the flow medium
ρ  Density of the wire
α  Temperature coefficient of the resistance
τ  Time constant
θ  Angle of rotation

References


Other literature without reference to this paper:


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