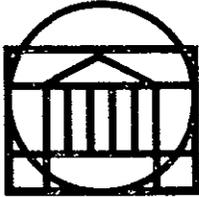


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RESEARCH LABORATORIES FOR THE ENGINEERING SCIENCES



# SCHOOL OF ENGINEERING AND APPLIED SCIENCE

UNIVERSITY OF VIRGINIA

Charlottesville, Virginia 22901

A Final Report

OPTIMIZATION OF MLS RECEIVERS FOR MULTIPATH  
ENVIRONMENTS

NASA Grant NSG 1128

Submitted to:

NASA Scientific and Technical Information Facility  
P. O. Box 8757  
Baltimore/Washington International Airport

Submitted by:

G. A. McAlpine  
Associate Professor

J. H. Highfill III  
Senior Scientist

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June 1979

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## SECTION I

### INTRODUCTION

This is the final report of research under Grant NSG 1128, awarded to the University in December 1974. The project is concerned principally with the angle-tracking problems in Microwave Landing System (MLS) receivers, the goal of the research being a receiver design capable of optimal performance in the multipath environments found in air terminal areas. The scope of the work included various theoretical and evaluative studies associated with the project goal, e.g.

- i. Signal model development
- ii. Derivation of optimal receiver structures
- iii. Development and use of computer simulations for receiver algorithm evaluation

and also, at least initially, the development of an experimental receiver for flight testing. Reference is made to the progress reports [1-5] for details of the research. This report provides an overview of the work and a summary of principal results and conclusions.

During the 1976-77 annum a study of the DME was also undertaken along with the ongoing angle receiver research. The DME work included some preliminary theoretical analysis but mostly simulation studies of the various designs, i.e. fixed threshold, adaptive threshold and delay and compare DME receivers. The simulations showed the delay and compare receiver to be the most robust of the three designs simulated. The DME study was peripheral to the focal research on the angle receiver and is not discussed further in this report. Reference is made to [4, pp. 51-100] for more detail.

The early study established that multipath propagation in air terminal areas is due principally to reflections from hangars and other buildings, other aircraft and the ground -- all cases where the multipath interference is very nearly specular in nature and either an actual or virtual specular point can be identified. A math model for the received signal in such a case contains parameters which, together with selected time derivatives, constitute a vector which is easily conceptualized into the "state" of a state space model of the problem dynamics. And the latter provides the mathematical framework necessary for applying recursive state estimation techniques to the optimal receiver design problem. This was the approach taken in the research.

Two algorithms resulting were studied extensively:

- i. An Optimal receiver: The state vector included signal-to-noise ratios, angular coordinates, angular rates, the phase difference and scalloping frequency parameters.
- ii. A Suboptimal receiver: A structure similar in some respects to the optimal receiver but the phase difference and scalloping frequency parameters were not estimated.

Both algorithms generally outperformed in simulation a "threshold receiver" design which was approximately representative of the current Phase III Receiver. The Optimal design generally was the best, at least when the scalloping rate was less than half the angle function repetition rate and hence the phase difference parameter could be tracked successfully. The suboptimal design, at least in the simulation, suffered from extremely complex and lengthy computations. The optimal design (and presumably the suboptimal design, would also) exhibited a

high sensitivity to error in the (presumed) beam width of the MLS ground antenna. These and other simulation results are discussed at length in the report, and approaches are suggested for possible improvements in performance.

Some considerations relating to an experimental receiver design are also offered.



## SECTION II

### SIGNAL MODEL AND ESTIMATOR DESIGNS

The signal available to the processor is a log video signal with bandwidth approximately half that of the i-f channel of the receiver. We begin at this point with the adaptation of this signal, in part A below, for use by the processor. Part B presents a state space model of the evolving problem geometry. Part C describes the general approach used to optimal receiver design, and Part D develops specific designs studied in the research. The reader is assumed to be familiar with the MLS system concepts and signal formats; for this orientation, refer to [6], [7] and [8].

#### A. THE AMPLITUDE-SQUARED ENVELOPE SIGNAL

The receiver log-envelope signal, a continuous-time signal within a scan, is sampled throughout a window on each semi-scan (centered on the expected centroid of the direct path pulse) at a sampling rate approximately equal to the i-f bandwidth and then suitably exponentiated and squared; the resulting  $J$  samples of the amplitude-squared envelope taken within a given scan are then normalized to a suitable measure of receiver noise power and assembled into an observations, or measurement, vector  $u$ , which clearly is nonlinear in the problem parameters of interest and also corrupted non-additively by receiver noise. Specifically, for the  $k$ th scan,  $k = 0, 1, 2, \dots$ , and in terms of a discrete-time variable  $\tau_j$  local to the scan, and assuming the presence of a direct-path component, a single multipath component and receiver noise, the  $j$ th component of  $u$ , say  $u_j$ ,  $j = 1, \dots, J$  is modeled as follows:

$$u_j = \{ \alpha_P [\theta - \theta_A(\tau_j)] + \alpha_{RP} [\theta_R - \theta_A(\tau_j)] \cos \beta_j + n_{c_j} \}^2 + \{ \alpha_{RP} [\theta_R - \theta_A(\tau_j)] \sin \beta_j + n_{s_j} \}^2 \quad (2.1)$$

where

$$\alpha = \alpha(k) = \text{direct path signal-to-noise ratio} \quad (2.2)$$

$$\theta = \theta(k) = \text{angular coordinate of own A/C} \quad (2.3)$$

$$\alpha_R = \alpha_R(k) = \text{multipath signal-to-noise ratio} \quad (2.4)$$

$$\theta_R = \theta_R(k) = \text{angular coordinate of reflector specular point} \quad (2.5)$$

$\beta_j = \beta(k, \tau_j) = \text{direct path-to-multipath phase difference at the } j\text{th sample of the } k\text{th scan, propagating as follows:}$

$$\beta_j = \beta(k) + w_{sc} \tau_j + \frac{\dot{w}_{sc}}{2} \tau_j^2 + \dots \quad (2.6a)$$

where

$\beta(k) = \text{phase difference at the start of the } k\text{th scan, propagating similarly, i.e.}$

$$\beta(k+1) = \beta(k) + w_{sc} T_k + \frac{\dot{w}_{sc}}{2} T_k^2 + \dots \quad (2.6b)$$

in which

$$T_k = \text{time interval, } k\text{th-to-}(k+1)\text{th scans.} \quad (2.7)$$

$$w_{sc} = \text{the scalloping rate (also derivatives may be present)} \quad (2.8)$$

$$\theta_A(.) = \text{the transmitting antenna scanning function} \quad (2.9)$$

(see equation (2.124) below)

$$p[.] = \text{the transmitting antenna selectivity function} \quad (2.10)$$

(square root of power density at a constant radius) and

$$n_{c_j}, n_{s_j} \text{ are independent Gaussian random variables with mean zero, variance 0.5.} \quad (2.11)$$

This model neglects second-order effects ([3], p. 9) chiefly

- a. Doppler effects not influencing the scalloping rate
- b. Differential propagation delays (e.g.  $(\frac{r_{\text{reflect}} - r_{\text{direct}}}{c})$ ), which tend to distort the mirror symmetry that exists between the T0-, FRO-scan signals.

## B. THE STATE-SPACE MODEL

The various parameters appearing in  $u_j$ , (2.1) above, together with time derivatives of interest, are assembled into an  $N_s$ -dimensional state vector,  $x$ , modeled as the solution of a suitable linear difference equation evolving in discrete-time, from scan-to-scan, and excited by a white, zero-mean random process, representing external influences. Hence, the composite generator-of-observations model is taken as a state space formulation with form as follows:

$$\begin{aligned} x(k+1) &= F(k)x(k) + G(k)z(k) \\ u(k) &= h(x(k), n(k)) \end{aligned} \quad (2.12)$$

where

$$x(k) = \text{state } N_s\text{-vector} \quad (2.13)$$

$z(k)$  = a representation of the various external influences on the modeled environment, taken as an  $M$ -vector random process, white with mean zero and covariance matrix  $Q(k)$ ,

$$\text{where} \quad (2.14)$$

$$Q(k) \triangleq \langle z(k)z^T(k) \rangle \quad (2.15)$$

$$F(k) = \text{state 1-step transition matrix} \quad (2.16)$$

$G(k)$  = an  $N_s \times M$  input constraint matrix of rank  $M$ , where

$$M \leq N_s \quad (2.17)$$

$$u(k) = \text{observations } J\text{-vector} \quad (2.18)$$

$n(k)$  = a  $2J$ -vector of the quadrature components  $n_{c_j}$ ,  
 $n_{s_j}$  of receiver noise associated with the  $J$  samples  
of the noisy envelope ( $n(j)$  and  $n(k)$  are independent  
if  $j \neq k$ ). (2.19)

$h(\cdot, \cdot)$  = a nonlinear vector-valued function of its arguments,  
constructing  $u(k)$  as a  $J$ -vector of envelope samples  
 $u_j$ , equation (2.1). (2.20)

### C. THE ESTIMATION APPROACH

In developing a procedure for estimating the angular coordinate  $\theta$ ,  
it was clear from (2.1) that performance would be better if more of the  
state variables than just  $\theta$  were estimated. It was also clear that not  
all of the state variables influence the vector  $u(k)$  of observation's  
taken within a single scan; in the present formulation, for example,  $\theta$   
and  $\theta_R$  are considered constants during the active scan, hence  $\dot{\theta}$  and  $\dot{\theta}_R$   
are absent from (2.1), nevertheless they are necessarily included as  
variables in the state vector to afford modeling tractably a varying  
geometry over a sequence of scans. The functional dependence of  $u(k)$  on  
only a subset of the state variables posed a choice:

1. Estimate only the subset of state variables associated  
with  $u(k)$ .
2. Estimate the full state vector  $x(k)$ .

The first option very likely would result in severe degeneration in  
performance, during signal fades, including possibly loss of lock. The  
benefits promised by a modest filter memory, however, (represented by  
rate estimates in a receiver state estimator, e.g.) prompted the second  
choice, and we began to consider the criterion under which a suitable

estimate of the full state  $x(k)$  could be calculated recursively, given the complexity of the observations.

Ideally, given a sequence of observations  $u$ , (2.12b), say from some initial scan through the present ( $k$ th) scan, represented as follows:

$$U(k) \triangleq \{u(1), u(2), \dots, u(k)\}, \quad (2.21)$$

we might adopt as a candidate criterion of performance the mean square error criterion and seek to calculate the conditional mean  $\langle x(k) | U(k) \rangle$  as a basis for an optimal MLS receiver design. Without loss of generality, however, the conditional mean can be written as

$$\langle x(k) | U(k) \rangle = \langle x(k) | U(k-1) \rangle + \langle E(k) | U(k) \rangle \quad (2.22)$$

where

$$\langle x(k) | U(k-1) \rangle = F(k+1) \langle x(k-1) | U(k-1) \rangle \quad (2.23)$$

is the extrapolation of the prior estimate to the present, and

$\langle E(k) | U(k) \rangle$  is the conditional mean of the error

$$E(k) \triangleq x(k) - \langle x(k) | U(k-1) \rangle \quad (2.24)$$

in the extrapolated estimate (2.23). Hence, via (2.22), a conditional mean receiver is essentially equivalent to a calculation of  $\langle E(k) | U(k) \rangle$ , a task which, generally,

1. As the notation suggests, may involve individually each and every observation constituting the sequence  $U(k)$ , and in addition,
2. May not even be computable in a finite number of operations, or even easily approximated.

A class of notable exceptions exists in which not only is  $\langle E(k) | U(k) \rangle$  computable or easily approximated, but all the historical information in dated observations necessary for the calculation of  $\langle E(k) | U(k) \rangle$  is

carried in the extrapolated prior state estimate  $\langle x(k) | U(k-1) \rangle$ , (2.23);

that is  $\langle E(k) | U(k) \rangle$  can be written

$$\langle E(k) | U(k) \rangle = f(\langle x(k) | U(k-1) \rangle, u(k)), \text{ for some } f(\cdot, \cdot). \quad (2.25)$$

Two examples are the following:

1. The Kalman filter, applicable when  $h(x,n)$  is linear in both  $x$  and  $n$ , gives an exact calculation of  $\langle E(k) | U(k) \rangle$ ;
2. The Extended Kalman filter, applicable when  $h(x,n)$  represents an additive corruption of the observations by  $n$ , gives an approximate calculation of  $\langle E(k) | U(k) \rangle$  when  $h(x,n)$  is nonlinear in  $x$ .

Because of the complexity of the observation  $h(x,n)$  [recall  $h_j$ , (2.1)] and the computability requirement (for simulation and also, potentially, hardware), the estimation approach used in this research was, of necessity, an approximation. An adaptation of the preceding was used, producing a state estimate (generally now suboptimal), denoted  $\hat{x}(k|k)$  to distinguish it from the exact conditional mean, and obtained, as follows:

$$\hat{x}(k|k) = \hat{x}(k|k-1) + \hat{\xi}(k|k) \quad (2.26)$$

where

$$\hat{x}(k|k-1) = F(k-1)\hat{x}(k-1|k-1) \quad (2.27)$$

and  $\hat{\xi}(k|k)$  is a "suitable" estimate to be defined below, of the error  $\xi(k)$  in  $\hat{x}(k|k-1)$ , given  $\hat{x}(k|k-1)$  and  $u(k)$ , where

$$\xi(k) \triangleq x(k) - \hat{x}(k|k-1) \quad (2.28)$$

The estimate  $\hat{\xi}(k|k)$  will be functionally dependent only upon  $\hat{x}(k|k-1)$  and  $u(k)$ . A final error definition needed and an easily proved result of interest are, as follows:

$$e(k) \triangleq \xi(k) - \hat{\xi}(k|k) \quad (2.29)$$

$$= x(k) - \hat{x}(k|k) \quad (2.30)$$

i.e., the error in the estimate  $\hat{\xi}(k|k)$  is the residual error in the updated state estimate  $\hat{x}(k|k)$ .

Since the observations  $u(k)$  are functionally dependent upon only a subset of the state variables, the calculation of  $\hat{\xi}(k|k)$ , i.e. the estimation of the error  $\xi(k)$  in  $\hat{x}(k|k-1)$ , given  $\hat{x}(k|k-1)$  and  $u(k)$ , was accomplished in 2 stages, characterized respectively as the Scan Data Processor (SDP) and the Tracking Loop Filter. The SDP essentially does a curve-fitting of a noiseless, internal version of the observations with the noisy, actual ones, calculating perturbations (error estimates) of the associated elements of  $\hat{x}(k|k-1)$  to improve the fit. The Tracking Loop, closed around the SDP in a conventional recursive structure, develops an estimate of the full error vector  $\xi(k)$ , taking the assumed state evolution dynamics into account. A detailed discussion of these two stages is given below.

The approach taken was modified, in part, by two factors, as follows:

1. The presumed low-bandwidth of the state evolution model wrt the repetition rate, implying, quantitatively,

$$x(k) \approx F(k-1)x(k-1) \tag{2.31}$$

(i.e.  $G(k-1)w(k-1)$  in (2.12) is small).

2. The "tracking" nature of the estimation task implying, presumably,

$$x(k) \approx \hat{x}(k|k) \tag{2.32}$$

(i.e. the estimation error  $e(k)$ , (2.31), is "small").

Equations (2.27), (2.28), (2.30) and (2.31) above imply that  $\xi(k)$  may be approximated, as follows:

$$\xi(k) \approx F(k-1)e(k-1) \quad (2.33)$$

and this, with (2.32) above implies that

$$\xi(k) \text{ is "small",} \quad (2.34)$$

a result important to the design of the SDP described next.

#### Scan Data Processor

Let  $\gamma$  denote the parameter vector comprising the subset of  $N_G$  state variables on which  $u_j$ , (2.1), is functionally dependent. The general relation

$$\gamma = Hx \quad (2.35)$$

then defines a masking matrix  $H$ ,  $N_G \times N_s$ , having rank  $N_G \leq N_s$  and consisting appropriately of 1's and 0's. Other  $N_G$ -vector quantities of interest are obtained, as follows:

$$\text{Extrapolated Prior Est:} \quad \hat{\gamma}(k|k-1) = H\hat{x}(k|k-1) \quad (2.36)$$

$$\text{Error in } \hat{\gamma}(k|k-1): \quad \varepsilon(k) = H\xi(k) \quad (2.37)$$

By (2.34),  $\varepsilon(k)$  in (2.37) is "small", and Murphy's Locally Optimum Estimation (LOE) theory, [9], was brought to bear on the calculation of an estimate which, around  $\varepsilon=0$ , should be optimal in an intuitively appealing sense. The LOE criterion is summarized, in the notation of the SDP, as follows:

Locally Optimum Estimation: The estimate  $\hat{\varepsilon}$  of the error  $\varepsilon$  (in the present estimate  $\hat{\gamma}$  of the parameter  $\gamma$ ) is locally optimum at the point  $\varepsilon=0$ , if and only if (iff) the following two conditions are satisfied:

- 1)  $\hat{\varepsilon}$  is a locally unbiased estimate of  $\varepsilon$  at the point of  $\varepsilon=0$ , and

- 2)  $\hat{\varepsilon}$  is a locally minimum mean-squared error (MMSE) estimate of  $\varepsilon$  at the point  $\varepsilon=0$ ,

where 'locally unbiased' and 'locally MMSE' estimations are defined as follows:

Locally Unbiased Estimation: Defining the error in the estimate  $\hat{\varepsilon}$  of the quantity  $\varepsilon$  as follows:

$$\eta(k) \triangleq \hat{\varepsilon}(k|k) - \varepsilon(k) \quad (2.38)$$

and then defining the bias of the estimate  $\hat{\varepsilon}$  of the error  $\varepsilon$  (in the estimate  $\hat{\gamma}$  of the parameter  $\gamma$ ), as follows:

$$b(\varepsilon) \triangleq \langle \eta(k) | \gamma - \hat{\gamma} = \varepsilon \rangle \quad (2.39)$$

then the estimate  $\hat{\varepsilon}$  of the error  $\varepsilon$  (in the estimate  $\hat{\gamma}$  of the parameter  $\gamma$ ) is locally unbiased at the point  $\varepsilon=0$  iff the following two conditions are satisfied:

$$1) \quad b(0) = 0, \text{ on } N_G\text{-vector} \quad (2.40a)$$

$$2) \quad \left[ \frac{db(\varepsilon)}{d\varepsilon} \right]_{\varepsilon=0} = 0, \text{ on } N_G \times N_G \text{ matrix} \quad (2.40b)$$

and

Locally MMSE Estimation: Defining the mean-squared error of  $\hat{\varepsilon}$  in terms of  $\eta$ , (2.38) above, as follows:

$$\Sigma_{\hat{\varepsilon}}(\varepsilon) \triangleq \langle \eta(k)\eta^T(k) | \gamma - \hat{\gamma} = \varepsilon \rangle, \quad ( )^T = \text{transpose}, \quad (2.41)$$

then the estimate  $\hat{\varepsilon}$  of the error  $\varepsilon$  (in the estimate  $\hat{\gamma}$  of the parameter  $\gamma$ ) is locally MMSE at the point  $\varepsilon=0$  iff, for any estimate,  $\hat{\delta}$ , if  $\varepsilon$  locally unbiased at  $\varepsilon=0$ , the mean-squared errors of  $\hat{\varepsilon}$  and  $\hat{\delta}$  satisfy, in the usual non-negative definite sense,

$$\Sigma_{\hat{\delta}}(0) \geq \Sigma_{\hat{\varepsilon}}(0), \quad N_G \times N_G \text{ matrices} \quad (2.42)$$

The error  $\eta(k)$  is induced by the noise  $n(k)$  which is white (recall (2.11) and (2.19)); hence, clearly, local to the point  $\varepsilon=0$ , when  $\langle n \rangle = 0$  via (2.39), it is true also that  $\eta(k)$  is white, i.e.

$$\langle \eta(j)\eta^T(k) \rangle = 0, \quad j \neq k \quad (2.43)$$

We take note, in passing, of the important and beneficial property given in (2.40b), requiring that errors made in estimating the various components of the vector  $\varepsilon$  be decoupled when  $\varepsilon=0$ . In addition to making the estimate unique, this is probably effective in extending the properties in (2.40a) and (2.42) into the open region around the point  $\varepsilon=0$ .

Murphy has meticulously expounded the theory and solution of the locally optimum estimation problem in his scholarly work [9] and illustrated his results in diverse examples in communications. The solution, applied to the SDP design problem at hand, involves, first, the definition of several additional quantities:

1. The noiseless quadratic envelope vector  $q$  with element  $q_j$ .
2. The linear envelope vectors  $m$  and  $v$  (and associated elements), corresponding respectively to quadratic envelopes  $q$  and  $u$ .
3. The conditional probability density function (pdf)  $p(v|m)$
4. The likelihood ration  $\lambda(u|\gamma)$  Let  $m_{c_j}$  and  $m_{s_j}$  respectively be the linear envelope functions associated with a cosine and sine orthogonal decomposition of the noiseless i-f (or r-f) signal:

$$m_{c_j} = \alpha_P[\theta - \theta_A(\tau_j)] + \alpha_{RP}[\theta_R - \theta_A(\tau_j)] \cos \beta_j \quad (2.44a)$$

$$m_{s_j} = \alpha_{RP}[\theta - \theta_A(\tau_j)] \sin \beta_j \quad (2.44b)$$

various parameters of which are as defined, following (2.1). Then, in the same manner that the J-vector  $u$  of observations  $u_j$  was constructed, a noiseless quadratic envelope vector  $q$  is defined with elements  $q_j$ ,  $j=1,2,\dots,J$ , where

$$q_j = m_{c_j}^2 + m_{s_j}^2 \quad (2.45)$$

$$= \alpha^2 p_j^2(\theta) + 2\alpha\alpha_R p_j(\theta)p_j(\theta_R)\cos\beta_j + \alpha_R^2 p_j^2(\theta_R) \quad (2.46)$$

in which  $p_j(\theta)$  is short-hand for  $p[\theta-\theta_A(\tau_j)]$ , and similarly for  $p_j(\theta_R)$ .

The observations sample  $u_j$ , (2.1) may then be written as

$$u_j = (m_{c_j} + n_{c_j})^2 + (m_{s_j} + n_{s_j})^2 \quad (2.47)$$

or, equivalently

$$u_j = q_j + 2n_{c_j} [q_j]^{1/2} + n_{c_j}^2 + n_{s_j}^2 \quad (2.48)$$

Now, let  $m$  and  $v$  respectively represent noiseless and noisy linear envelope vectors with elements  $m_j$  and  $v_j$ , respectively, for  $j=1,2,\dots,J$ , where

$$m_j \triangleq q_j^{1/2} = [m_{c_j}^2 + m_{s_j}^2]^{1/2} \quad (2.49)$$

$$v_j \triangleq u_j^{1/2} = [(m_{c_j} + n_{c_j})^2 + (m_{s_j} + n_{s_j})^2]^{1/2} \quad (2.50)$$

Since the sampling rate within the scan equals the i-f bandwidth, the noise samples are all nearly independent (and zero mean, Gaussian with variance 0.5; recall (2.11)). Hence, referring to [10, eq. (8-115)] for the conditional pdf  $p(v_j | m_j)$ , the conditional pdf  $p(v | m)$  can be written

$$p(v | m) = \prod_{j=1}^J p(v_j | m_j) \quad (2.51)$$

$$= 2^J \prod_{j=1}^J v_j I_0(2m_j v_j) \exp(-m_j^2 - v_j^2) \quad (2.52)$$

where  $I_0(\cdot)$  is the modified Bessel function of the first kind, zeroth order. The likelihood ratio of interest is the following:

$$\lambda = \frac{p(\mathbf{v}|\mathbf{m})}{p(\mathbf{v}|0)} = \prod_{j=1}^J I_0(2m_j v_j) \exp(-m_j^2) \quad (2.53)$$

or, defining a new function  $M_0(\cdot): \mathbb{R}^+ \rightarrow \mathbb{R}^+$ , as follows, in relation to the even function  $I_0(\cdot)$  ([3], p. 13):

$$M_0(x^2) = I_0(x), \quad x \in \mathbb{R}^1 \quad (2.54)$$

then, in terms of  $q_j$  and  $u_j$ , we may write

$$\lambda(\mathbf{u}|\gamma) = \prod_{j=1}^J M_0(4q_j u_j) \exp(-q_j) \quad (2.55)$$

$$= \prod_{j=1}^J \lambda_j(u_j | q_j) \quad (2.56)$$

where the conditioning variable on the left is shown as  $\gamma$ , rather than  $q(=q(\gamma))$ , to emphasize the parameter values.

The theory provides, further, that if one of the parameters upon which  $q$  is dependent is, in fact, a random variable, say  $\zeta$ , in which there is no estimation interest, then it is to be averaged out before proceeding, i.e. the average likelihood ratio

$$\lambda(\mathbf{u}|\gamma) = \left\langle \prod_{j=1}^J \lambda_j(u_j | q_j(\gamma, \zeta)) \mid \mathbf{u}, \gamma \right\rangle \quad (2.57)$$

is used in the work below. In this approach (which formed the basis of one variant of MLS receiver design studied) clearly the noiseless envelope vector  $q$  has no further significance.

The Scan Data Processor design by the LOE approach can now be completed. In the notation of the SDP design problem (but otherwise quite generally) the estimate  $\hat{\varepsilon}(k|k)$  of the error  $\varepsilon(k)$  (in the estimate

$\hat{\gamma}(k|k-1)$  of the parameter vector  $\gamma$ ) which is locally optimum at  $\varepsilon=0$  is given by

$$\hat{\varepsilon}(k|k) = \phi^{-1}(\hat{\gamma})\Lambda(u|\hat{\gamma}) \quad (2.58)$$

where, recognizing  $u(k) = u(\gamma(k), n(k))$ ,

$$\Phi(\hat{\gamma}) \triangleq \langle \Lambda(u(\gamma, n)|\hat{\gamma}) \Lambda^T(u(\gamma, n)|\hat{\gamma}) \mid \gamma = \hat{\gamma} \rangle \quad (2.59)$$

denoted as the LOE (Fisher) Information Matrix, and

$$\Lambda(u|\hat{\gamma}) \triangleq \begin{cases} \frac{\partial}{\partial \hat{\gamma}} \ln \lambda(u|\hat{\gamma}) & \lambda(u|\hat{\gamma}) \neq 0 \\ 0, & \text{otherwise} \end{cases} \quad (2.60)$$

Further, the mean-squared error,  $\Sigma$ , (2.41), of this estimate local to the point  $\varepsilon=0$  is

$$\Sigma(o) = \phi^{-1}(\gamma) \quad (2.61)$$

As indicated above, several variants to the basic MLS receiver design using this approach were studied, differing initially in their definitions of the state and/or parameter vectors,  $x$  and  $\gamma$  respectively. Detailed development of the LOE quantities defined above is deferred until the next section of this chapter where the various designs specific to particular state and/or parameter vector formulations will be described. We conclude this discussion of the Scan Data Processor by noting that, in view of (2.58) and (2.61) above, the principle calculations done by the SDP are those of  $\Phi(\hat{\gamma})$  and  $\Lambda(u|\hat{\gamma})$ . These, in fact, are the quantities passed to the Tracking Loop Filter, discussed next.

#### Tracking Loop Filter

Inputs to the Tracking Loop Filter from the Scan Data Processor are the quantities  $\Lambda(u|\hat{\gamma}(k|k-1))$  and  $\Phi(\hat{\gamma}(k|k-1))$ . If we form the estimate

$\hat{\varepsilon}(k|k)$ , as prescribed in (2.58), that is:

$$\hat{\varepsilon}(k|k) = R(\hat{y})\Lambda(u|\hat{y}) \quad (2.62)$$

where  $\hat{y} = \hat{y}(k|k-1)$  (2.63)

and  $R(\hat{y}) \triangleq \Phi^{-1}(\hat{y}(k|k-1))$  (2.64)

and then tentatively form a "pre-estimate",  $\hat{y}(k|k)$ , in the following manner:

$$\hat{y}(k|k) = \hat{y}(k|k-1) + \hat{\varepsilon}(k|k), \quad (2.65)$$

we find that  $\hat{y}$  can be written

$$\hat{y} = \hat{y}(k|k-1) + \varepsilon(k) + \hat{\varepsilon}(k|k) - \varepsilon(k) \quad (2.66)$$

$$= \gamma(k) + \eta(k) \quad (2.67)$$

$$= Hx(k) + \eta(k) \quad (2.68)$$

i.e. the pre-estimate  $\hat{y}(k|k)$ , in a neighborhood of  $\varepsilon=0$ , is in fact, a "pseudo-observation" which is both linear in  $x$  and corrupted additively by the zero mean, white noise  $\eta(k)$  with covariance  $R(\hat{y}(k|k-1))$ , (2.63).

Following conventional Kalman filter theory and forming the innovations process,  $\hat{y}(k|k-1) - \hat{y}(k|k)$ , gives

$$\hat{y}(k|k-1) - \hat{y}(k|k) = \hat{\varepsilon}(k|k) \quad (2.69)$$

i.e. the innovations process is the estimate  $\hat{\varepsilon}(k|k)$ , (2.62), produced (effectively) by the LOE-theory-based Scan Data Processor. The filter state update equation has the form

$$\hat{x}(k|k) = \hat{x}(k|k-1) + \kappa(k)\hat{\varepsilon}(k|k) \quad (2.70)$$

where  $\kappa(k)$ , the Kalman gain, is calculated by cycling through 3 equations for each value of  $k$ ,  $k = 1, 2, \dots$ , usually as follows:

Extrapolated Error Covariance:

$$P(k|k-1) = F(k-1)P(k-1|k-1)F^T(k-1) + G(k-1)Q(k-1)G^T(k-1) \quad (2.71)$$

Kalman Gain:

$$\kappa(k) = P(k|k-1)H^T [HP(k|k-1)H^T + R(\hat{Y})]^{-1} \quad (2.72)$$

Updated Error Covariance:

$$P(k|k) = (I - \kappa(k)H)P(k|k-1)(I - \kappa(k)H)^T + \kappa(k)R(\hat{Y})\kappa^T(k) \quad (2.73)$$

In the present application some simplification is possible, however.

Comparing (2.26) and (2.70) above indicates that

$$\xi(k|k) = \kappa(k)\hat{\varepsilon}(k|k) \quad (2.74)$$

$$= \kappa(k)R(\hat{Y})\Lambda(u|\hat{Y}) \quad (2.75)$$

and substituting from (2.72) into the latter gives

$$\xi(k|k) = P(k|k-1)H^T [HP(k|k-1)H^T + R(\hat{Y})]^{-1}R(\hat{Y})\Lambda(u|\hat{Y}) \quad (2.76)$$

or, after simplifying,

$$\xi(k|k) = \Gamma(k)\Lambda(u|\hat{Y}) \quad (2.77)$$

where

$$\Gamma(k) = P(k|k-1)H^T [I + \Phi(\hat{Y})HP(k|k-1)H^T]^{-1} \quad (2.78)$$

is a new  $N_s \times N_G$  gain matrix not requiring the inversion of the matrix  $\Phi(\hat{Y})$  (produced by the SDP) for its calculation (by (2.64),  $R^{-1}(\hat{Y})$  appearing in the simplification, was replaced by  $\Phi(\hat{Y})$ ). The refined state-estimate update equation, corresponding to (2.70) is the following:

$$\hat{x}(k|k) = \hat{x}(k|k-1) + \Gamma(k)\Lambda(u|\hat{Y}) \quad (2.79)$$

Comparing (2.75) and (2.77) indicates that

$$\kappa(k)R(\hat{Y}) = \Gamma(k) \quad (2.80)$$

or that

$$\kappa(k) = \Gamma(k)R^{-1}(\hat{Y}) = \Gamma(k)\Phi(\hat{Y}) \quad (2.81)$$

Substituting this into (2.73) and simplifying gives the following:

Updated Error Covariance:

$$P(k|k) = (I - \Gamma(k)\Phi(\hat{\gamma})H)P(k|k-1)(I - \Gamma(k)\Phi(\hat{\gamma})H)^T + \Gamma(k)\Phi(\hat{\gamma})\Gamma^T(k) \quad (2.82)$$

which also does not require the inversion of  $\Phi(\gamma)$ .

In summary, the MLS receiver design developed, a tracking receiver, will operate as a recursive state estimator and begin the (kth) data processing cycle by extrapolating the prior state estimate  $\hat{x}(k-1|k-1)$  to the present, producing the

$$\text{Extrapolated State Estimate, } \hat{x}(k|k-1), \quad (2.27)$$

and then masking it, giving the

$$\text{Extrapolated Parameter Estimate, } \hat{\gamma}(k|k-1), \quad (2.36)$$

this, an estimate of parameter vector  $\gamma(k)$  with error  $\varepsilon(k)$ . Next, given  $\hat{\gamma}(k|k-1)$  and the vector  $u(k)$  of observations, the Scan Data Processor, designed under a criterion of producing an estimate  $\hat{\varepsilon}(k|k)$  of error  $\varepsilon(k)$  that is locally optimum at  $\varepsilon=0$ , stops short of this result and instead calculates the following:

$$\text{Log Likelihood Ratio, } \Lambda(u|\hat{\gamma}), \quad (2.60)$$

$$\text{LOE Information Matrix, } \Phi(\hat{\gamma}), \quad (2.59)$$

The Tracking Loop Filter accepts  $\Lambda$  and  $\Phi$  from the SDP and completes the data processing cycle with following sequence of calculations.

$$\text{Extrapolated Error Covariance, } P(k|k-1), \quad (2.71)$$

$$\text{Filter Gain, } \Gamma(k), \quad (2.78)$$

$$\text{Updated State Estimate, } \hat{x}(k|k), \quad (2.79)$$

$$\text{Updated Error Covariance, } P(k|k), \quad (2.82).$$

This concludes the derivation at the general level. The results are specialized to particular state- and parameter-vector formulations next.

#### D. SPECIFIC DESIGNS

Throughout the research program three specializations of the above general design structure received most of the attention. These are characterized by the formulations of their parameter and state estimate vectors, as follows:

##### i. "Non-adaptive" Design

$$N_G = 2, \quad \hat{y} = (\hat{\alpha}, \hat{\theta})^T \quad (2.83)$$

$$N_S = 3, \quad \hat{x} = (\hat{\alpha}, \hat{\theta}, \hat{\dot{\theta}})^T \quad (2.84)$$

##### ii. "Optimal" Design (Adaptive)

$$N_G = 5, \quad \hat{y} = (\hat{\alpha}, \hat{\theta}, \hat{\alpha}_R, \hat{\theta}_R, \hat{\beta})^T \quad (2.85)$$

$$N_S = 8, \quad \hat{x} = (\hat{\alpha}, \hat{\theta}, \hat{\dot{\theta}}, \hat{\alpha}_R, \hat{\theta}_R, \hat{\dot{\theta}}_R, \hat{\beta}, \hat{w}_{sc})^T \quad (2.86)$$

##### iii. "Suboptimal" Design (Adaptive)

$$N_G = 4, \quad \hat{y} = (\hat{\alpha}, \hat{\theta}, \hat{\alpha}_R, \hat{\theta}_R)^T \quad (2.87)$$

$$N = 6, \quad \hat{x} = (\hat{\alpha}, \hat{\theta}, \hat{\dot{\theta}}, \hat{\alpha}, \hat{\theta}, \hat{\dot{\theta}})^T \quad (2.88)$$

The non-adaptive design was identified and studied as a baseline design in accessing the benefits of adaptivity as supplied by the other designs. The optimal design was the principal focus of the study; the definitions (2.85) and (2.86), and the resulting design, are predicated on the assumption that the multipath interference phenomenon, when present (in q, (2.46), e.g.), is one which is fully described by samples taken at the angle function repetition rate, or more concisely, via the sampling theorem,

$$\omega_{sc} < \pi(\text{Rep. Rate}) = \frac{\pi}{T} \quad (2.89)$$

where T is the interval between scans. Under this assumption then,  $\beta$  on the active scan is nearly constant, i.e. in q, (2.46),

$$\beta_j \approx \beta(k), \text{ for all } j = 1, 2, \dots, J \quad (2.90)$$

(where  $\beta(k)$  is the phase difference at the start of the  $k$ th scan) and hence  $\hat{w}_{sc}$  does not appear in the  $\hat{y}$ -formulation for this design. The relation (2.89) is a restriction that would not always be met in practice, of course, and the suboptimal design represented an effort to formally relax this condition and simultaneously reduce the dimensions of the vectors and hence the complexity of the algorithm. This design was accomplished by

- i. Assuming the  $\beta_j$  in  $q$  (2.46) were all independent random variables, uniformly distributed on the interval  $(-\pi, \pi)$  (corresponding to the assumption that  $w_{sc} \rightarrow \infty$ ); then
- ii. Following (2.57) and taking the average of the likelihood ratio over all the  $\beta_j$  and then using it in the subsequent design.

Both the state and parameter vectors are devoid of both  $\beta$  and  $w_{sc}$  in this third design.

A fourth and very recently conceived design, motivated also by the desire to relax the restriction (2.89), though more complex than the "Optimal" design, is characterized as follows:

"6D LOE" Design (adaptive)

$$N_G = 6, \quad \hat{y} = (\hat{\alpha}, \hat{\theta}, \hat{\alpha}_R, \hat{\theta}_R, \hat{\beta}, \hat{w}_{sc})^T \quad (2.91)$$

and

$$N_S = 8, \quad \hat{x} = (\hat{\alpha}, \hat{\theta}, \hat{\theta}, \hat{\alpha}_R, \hat{\theta}_R, \hat{\theta}_R, \hat{\beta}, \hat{w}_{sc})^T \quad (2.92)$$

or

$$N_S = 9, \quad \hat{x} = (\hat{\alpha}, \hat{\theta}, \hat{\theta}, \hat{\alpha}_R, \hat{\theta}_R, \hat{\theta}_R, \hat{\beta}, \hat{w}_{sc}, \hat{\dot{w}}_{sc})^T \quad (2.93)$$

The assumption here is that there is sufficient information in the  $J$

samples taken within a single scan ( $J/2$  on each semi-scan, centered on the expected centroid of the direct path pulse) to produce an estimate of  $w_{sc}$  using just one scan's data; it appears also the fractional accuracy of such an estimate would improve with increasing  $w_{sc}$ , though it may be somewhat  $\theta$ -dependent, since the interval between the TO-scan and FRO-scan pulses is both  $\theta$ -dependent and relevant to the  $w_{sc}$ -estimate produced (or, more specifically, the LOE estimate of the error in  $\hat{w}_{sc}(k|k-1)$ ). The "6D LOE" design will be described in Appendix C with any results obtained at the time of grant closure.

Here we focus on the earlier designs, in particular, the details for the optimal and suboptimal designs. The non-adaptive design is clearly imbedded, in a sense, in both of these designs and needn't be treated separately.

#### Optimal Design

For this case, referencing (2.56),  $\lambda(u|\hat{y})$  can be written as follows:

$$\lambda(u|\hat{y}) = \prod_{j=1}^J \lambda_j(u_j|\hat{q}_j) \quad (2.94)$$

where

$$\lambda_j(u_j|\hat{q}_j) \triangleq M_o(4\hat{q}_j u_j) \exp(-\hat{q}_j) \quad (2.95)$$

$$> 0, \text{ for all } u_j, \text{ and finite } \hat{q}_j \quad (2.96)$$

and

$$\hat{q}_j \triangleq q_j(\hat{y}) \quad (2.97)$$

$$= \hat{\alpha}^2 p_j^2(\hat{\theta}) + 2\hat{\alpha}\hat{\alpha}_{RPj}(\hat{\theta})p_j(\hat{\theta}_R)\cos\hat{\beta} + \hat{\alpha}_{RPj}^2(\hat{\theta}_R) \quad (2.98)$$

Hence, via (2.60)

$$\Lambda(u|\hat{y}) \triangleq \frac{\partial \ln}{\partial \hat{y}} \lambda(u|\hat{y}) = \sum_{j=1}^J \Lambda_j(u_j|\hat{q}_j) \quad (2.99)$$

where

$$\begin{aligned} \Lambda_j(u_j|\hat{q}_j) &\triangleq \frac{\partial}{\partial \hat{y}} \ln \lambda_j(u_j|\hat{q}_j) = \frac{\frac{\partial \lambda_j}{\partial \hat{y}}(u_j|\hat{q}_j)}{\lambda_j(u_j|\hat{q}_j)} \\ &= \left( \frac{d\hat{q}_j}{d\hat{y}} \right) \left( \frac{\frac{\partial \lambda_j}{\partial \hat{q}_j}(u_j|\hat{q}_j)}{\lambda_j(u_j|\hat{q}_j)} \right) \end{aligned} \quad (2.100)$$

or

$$\Lambda(u|\hat{y}) = D(\hat{y})w(u|q(\hat{y})) \quad (2.101)$$

in which

$$\begin{aligned} D(\hat{y}) \triangleq \frac{d\hat{q}}{d\hat{y}} &= \begin{pmatrix} \frac{\partial \hat{q}_1(\hat{y})}{\partial \hat{y}_1} & \cdots & \frac{\partial \hat{q}_J(\hat{y})}{\partial \hat{y}_1} \\ \cdots & \cdots & \cdots \\ \frac{\partial \hat{q}_1(\hat{y})}{\partial \hat{y}_{N_G}} & \cdots & \frac{\partial \hat{q}_J(\hat{y})}{\partial \hat{y}_{N_G}} \end{pmatrix}, \quad N_G \times J \quad (2.102) \\ &\begin{pmatrix} \text{--- } 2\hat{\alpha}p_j^2(\hat{\theta}) + 2\hat{\alpha}_R p_j(\hat{\theta})p_j(\hat{\theta}_R)\cos\hat{\beta} \text{---} \\ \text{--- } 2\hat{\alpha}^2 p_j(\hat{\theta})\dot{p}_j(\hat{\theta}) + 2\hat{\alpha}\hat{\alpha}_R \dot{p}_j(\hat{\theta})p_j(\hat{\theta}_R)\cos\hat{\beta} \text{---} \\ \text{--- } 2\hat{\alpha}p_j(\hat{\theta})p_j(\hat{\theta}_R)\cos\hat{\beta} + 2\hat{\alpha}_R p_j^2(\hat{\theta}_R) \text{---} \\ \text{--- } 2\hat{\alpha}\hat{\alpha}_R p_j(\hat{\theta})\dot{p}_j(\hat{\theta}_R)\cos\hat{\beta} + 2\hat{\alpha}_R^2 \dot{p}_j(\hat{\theta}_R)p_j(\hat{\theta}_R) \text{---} \\ \text{--- } (-2\hat{\alpha}\hat{\alpha}_R p_j(\hat{\theta})p_j(\hat{\theta}_R)\sin\hat{\beta}) \text{---} \end{pmatrix} \quad (2.103) \end{aligned}$$

where

$$\dot{p}_j(\theta) \triangleq \frac{d}{d\theta_e} p[\theta_e] \Big|_{\theta_e = \theta - \theta_A(\tau_j)} \quad (\text{and similarly for } \dot{p}_j(\theta_R)), \quad (2.104)$$

and

$$w(u|\hat{y}) \triangleq (---, w_j(u_j|\hat{y}), ---)^T, \quad \text{J-vector} \quad (2.105)$$

where

$$w_j(u_j|\hat{y}) \triangleq \frac{\frac{\partial \lambda_j}{\partial \hat{q}_j}(u_j|\hat{q}_j)}{\lambda_j(u_j|\hat{q}_j)} \quad (2.106)$$

$$= 4u_j \frac{M_1}{M_0}(4q_j(\hat{y})u_j) - 1 \quad (2.107)$$

in which

$$\frac{M_1}{M_0}(\cdot) \triangleq \frac{M_1(\cdot)}{M_0(\cdot)} \quad (2.108)$$

and, for any real  $z > 0$ ,

$$M_1(z) \triangleq \frac{d}{dz} M_0(z) \quad (2.109)$$

where  $M_0(\cdot)$  was as defined in (2.54) in relation to  $I_0(\cdot)$ , as follows for any real  $x$ :

$$M_0(x^2) = I_0(x) \quad (2.110)$$

A corresponding relation for  $M_1(\cdot)$  is as follows:

$$M_1(x^2) = \frac{1}{2x} I_1(x) \quad (2.111)$$

where  $I_1(\cdot)$  is the modified Bessel function of the first kind, first order. The well-known soft-limiter characteristic of

$$\frac{I_1}{I_0}(\cdot) \quad (\text{initial slope of } \frac{1}{2}, \text{ saturation value of } 1)$$

corresponds to the following for  $\frac{M_1}{M_0}(x)$ ,  $x \geq 0$ :

$$\left. \frac{M_1}{M_0}(x) \right|_{x=0} = \frac{1}{4} \quad (2.112)$$

$$\left. \frac{d}{dx} \frac{M_1}{M_0}(x) \right|_{x=0} = -\frac{1}{32} \quad (2.113)$$

$$\left. \frac{M_1}{M_0}(x) \right|_{x \text{ large}} \rightarrow \frac{1}{2x} \quad (2.114)$$

These conditions are satisfied exactly by the approximation ([3], pp. 15-17)

$$\frac{M_1}{M_0}(x) \approx \frac{1}{2(4+x)^{1/2}} \quad (2.115)$$

whose error peaks at only 4% around  $x=30$ . Substituting this in (2.107)

above for  $w_j(u_j | \hat{y})$  gives the expression

$$w_j(u_j | \hat{y}) \approx \frac{u_j}{(1 + q_j(\hat{y})u_j)^{1/2}} - 1 \quad (2.116)$$

which was used in this design.

Substituting (2.101) above in the defining equation (2.59) for the LOE Information Matrix  $\Phi$  gives

$$\Phi(\hat{y}) \triangleq \langle \Lambda(u(\gamma, n) | \hat{y}) \Lambda^T(u(\gamma, n) | \hat{y}) | \gamma = \hat{y} \rangle \quad (2.117)$$

$$= D(\hat{y}) H_w(q(\hat{y})) D^T(\hat{y}) \quad (2.118)$$

where

$$H_w(q(\hat{y})) \triangleq \langle w(u(\gamma, n) | \hat{y}) w^T(u(\gamma, n) | \hat{y}) | \gamma = \hat{y} \rangle \quad (2.119)$$

The criterion for locally optimum estimation (more specifically, locally unbiased estimation) at  $\varepsilon=0$  assures that

$$0 = \langle \Lambda(u(\gamma, n) | \hat{y}) | \gamma = \hat{y} \rangle = D(\hat{y}) \langle w(u(\gamma, n) | \hat{y}) | \gamma = \hat{y} \rangle \quad (2.120)$$

A simulation study ([4], p.15) of the process  $w(u | \hat{y})$ , using the approximation (2.116) gave support for (2.120) as well as strong evidence that  $w(u | \hat{q})$  is white, i.e.

$$\langle w_i(u_i(\gamma, n_i) | \hat{\gamma}) w_j(u_j(\gamma, n_j) | \hat{\gamma}) | \gamma = \hat{\gamma} \rangle = \begin{cases} 0, & \text{for } i \neq j \\ h_{w_j}(\hat{\gamma}), & \text{for } i = j \end{cases} \quad (2.121)$$

and on this basis  $H_w(\hat{q})$ , (2.119), which is the covariance of  $w(u | \hat{q})$  local to  $\gamma - \hat{\gamma} = 0$ , was taken as diagonal, i.e.

$$H_w(\hat{q}) = \text{Diag}(\dots, h_{w_j}(\hat{\gamma}), \dots), \quad J \times J \quad (2.122)$$

where  $h_w(\hat{\gamma})$ , it was also found ([4], Appendix A), could be approximated, as follows:

$$h_{w_j}(\hat{\gamma}) \approx \frac{1}{1 + 2 q_j(\hat{\gamma})} \quad (2.123)$$

with an error that peaked at about 20% for  $\hat{q}_j = 2$ .

The antenna scanning function,  $\theta_A(\tau)$ , used was the following

$$\theta_A(\tau_j) \triangleq \begin{cases} \theta_{A_{\max}} + \Omega \tau_j & , & 0 \leq \tau_j < T_s \\ \theta_{A_{\min}} & , & T_s \leq \tau_j < T_F \\ \theta_{A_{\min}} - \Omega(\tau_j - T_F) & , & T_F \leq \tau_j < T_1 \end{cases} \quad (2.124)$$

where the parameters are defined, as follows: (see Figure 2.1)

$$\Omega \triangleq - \frac{\theta_{A_{\max}} - \theta_{A_{\min}}}{T_s} \quad (2.125)$$

$$T_F \triangleq T_s + T_R - 2 \frac{\theta_{A_{\min}}}{\Omega} \quad (2.126)$$

$$T_s \triangleq \text{duration of the TO-scan} \quad (2.127)$$

$$T_R \triangleq \text{interval between zero intercepts} \quad (2.128)$$

$$T_1 \triangleq T_s + T_F \quad (2.129)$$

Values for the parameters  $\theta_{A_{\max}}$ ,  $\theta_{A_{\min}}$ ,  $T_s$  and  $T_R$  are essentially prescribed by the MLS specifications and will be given in the simulation

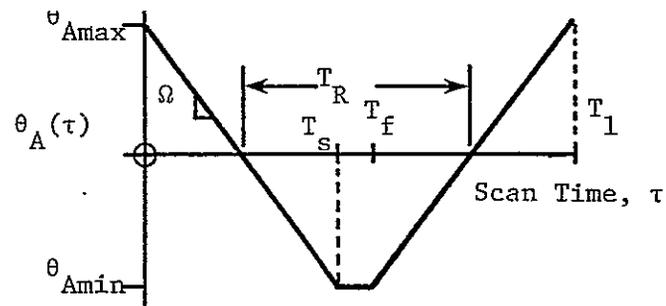


Figure 2.1 MLS Antenna Scanning Function

discussion. The antenna selectivity function,  $p(\ )$ , and its derivative  $\dot{p}(\ )$ , are not prescribed in the specifications; plausible functions were chosen for simulation use, however, and these will be described later, also. This completes the description of the scan data processor for the optimal design.

The  $\hat{y}$  and  $\hat{x}$  vector formulations in (2.85) and (2.86) require matrices F and H in the tracking loop, as follows:

$$F = \begin{pmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & T & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & T & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & T \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix} \quad (2.130)$$

$$H = \begin{pmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \end{pmatrix} \quad (2.131)$$

The product matrix  $GQG^T$  used was a diagonal one in which the diagonal elements represented generally measures (variances) of the intuitive uncertainty in the elements of  $x(k)$ , given those of  $x(k-1)$ . The following values were selected as part of the tracking loop design:

$$GQG_{11}^T = GQG_{44}^T = \text{Max} \left\{ \left(\frac{1}{2}\right)^2, \left(\frac{\hat{y}}{10}\right)^2 \right\} \quad (2.132)$$

representing 10% uncertainty for  $S/N \geq 14$  db (in the direct path signal strength only; the assignment of the same value to the '44' component was arbitrary);

$$GQG_{22}^T = GQG_{55}^T = GQG_{77}^T = 0 \quad (2.133)$$

representing full reliance in these coordinates on integrations of derivatives;

$$GQG_{33}^T = GQG_{66}^T = \left| \ddot{\theta}_{\max} \right|_{AZ}^2 T = .01T \quad (2.134)$$

where  $\left| \ddot{\theta}_{\max} \right| = 0.1 \text{ deg/sec}^2$  in Azimuth, was determined from a study of a representative set of landing patterns ([3], pp. 40ff);

$$GQG_{88}^T = \left( \frac{\Delta\beta}{T} \right)^2 = \frac{0.04}{T^2} \left( \ll \left( \frac{\pi}{T} \right)^2 \right) \quad (2.135)$$

representing an error  $\Delta\beta$  in phase (due to  $w_{sc}$  uncertainty (i.e. error)) of 0.2 radians between scans, well within the limit of  $\pi$  radians associated with the sampling theorem.

Finally, in recognition of the limitations on the true values of the states, imposed by system geometry, modeling ambiguities, etc., the results obtained from the estimation algorithm described thus far were subjected to various additional constraint operations before being designated and subsequently evaluated as "the estimates". Each of these constraints are described pictorially in Figure 2.2 in the conventional format of an input--output graph of a function of one variable. In all cases the abscissa (input) is the result of the estimation update, (2.79) above, and the ordinate is the estimate to be output (or used in the next estimation cycle).

### Suboptimal Design

For this case, the  $\beta_j$ ,  $j=1,2, \dots, J$ , are taken as independent random variables, each uniformly distributed on  $[-\pi, \pi]$ . Conceptually,  $\hat{q}_j$  is also random and can be written

$$\hat{q}_j = \hat{q}_{A_j} + \hat{q}_{B_j} \cos\beta_j = q_j(\hat{y}, \beta_j) \quad (2.136)$$

where

$$\hat{q}_{A_j} \triangleq \hat{\sigma}^2 p_j^2(\hat{\theta}) + \hat{\sigma}_R^2 p_j^2(\hat{\theta}_R) = q_{A_j}(\hat{y}), > 0 \quad (2.137)$$

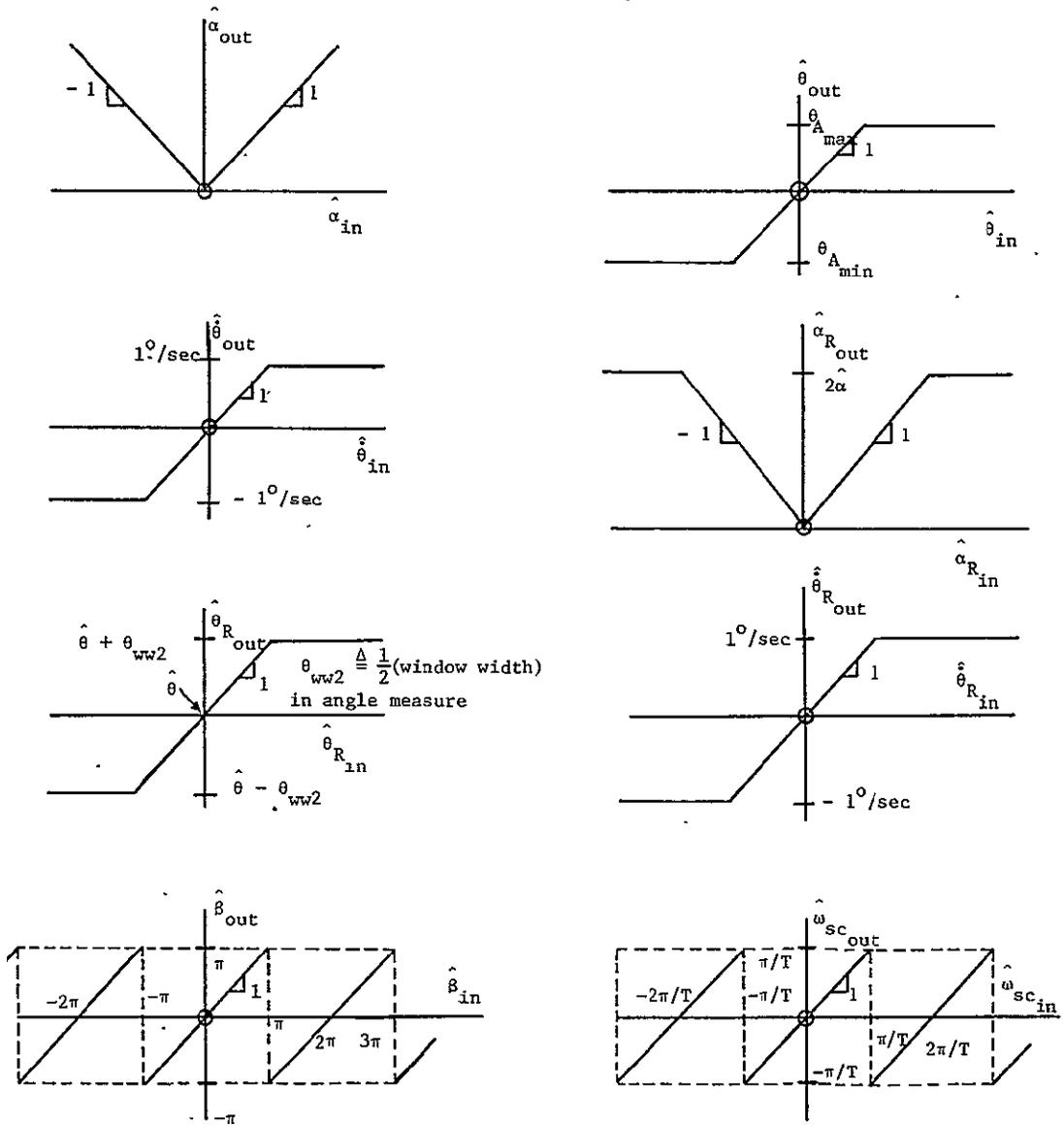


Figure 2.2 Constraints on Estimates

$$\hat{q}_{B_j} \triangleq 2\hat{\alpha}_R p_j(\hat{\theta}) p_j(\hat{\theta}_R) = q_{B_j}(\hat{Y}), \text{ indefinite} \quad (2.138)$$

and

$$- \hat{q}_{A_j} \leq \hat{q}_{B_j} \leq \hat{q}_{A_j} \quad (2.139)$$

We seek  $\lambda(u|\hat{Y})$ , which, applying (2.57), is given by

$$\lambda(u|\hat{Y}) = \left\langle \prod_{j=1}^J \lambda_j(u_j | q_j(\hat{Y}, \beta_j)) \middle| u, \hat{Y} \right\rangle \quad (2.140)$$

in which the averaging is done wrt the  $\beta_j$ ,  $j=1,2, \dots, J$ . Because the  $\beta_j$  are independent this can be written in a form similar to (2.94) as follows:

$$\lambda(u|\hat{Y}) = \prod_{j=1}^J \lambda_j(u_j | \hat{q}_{A_j}, \hat{q}_{B_j}) \quad (2.141)$$

where

$$\lambda_j(u_j | \hat{q}_{A_j}, \hat{q}_{B_j}) \triangleq \left\langle \lambda_j(u_j | q_j(\hat{Y}, \beta_j)) \middle| u_j, \hat{Y} \right\rangle \quad (2.142)$$

$$> 0 \text{ (by virtue of (2.95), (2.96))} \quad (2.143)$$

And, as in (2.99),

$$\Lambda(u|\hat{Y}) = \sum_{j=1}^J \lambda_j(u_j | \hat{Y}) \quad (2.144)$$

where, here,

$$\lambda_j(u_j | \hat{Y}) \triangleq \frac{\partial}{\partial \hat{Y}} \ln \lambda_j(u_j | \hat{q}_{A_j}, \hat{q}_{B_j}) \quad (2.145)$$

$$= \frac{\frac{\partial}{\partial \hat{Y}} \lambda_j(u_j | \hat{q}_{A_j}, \hat{q}_{B_j})}{\lambda_j(u_j | \hat{q}_{A_j}, \hat{q}_{B_j})} \quad (2.146)$$

$$= \left( \frac{d\hat{q}_{A_j}}{d\hat{Y}} \right) \left( \frac{\frac{\partial}{\partial \hat{q}_{A_j}} \lambda_j(u_j | \hat{q}_{A_j}, \hat{q}_{B_j})}{\lambda_j(u_j | \hat{q}_{A_j}, \hat{q}_{B_j})} \right) + \left( \frac{d\hat{q}_{B_j}}{d\hat{Y}} \right) \left( \frac{\frac{\partial}{\partial \hat{q}_{B_j}} \lambda_j(u_j | \hat{q}_{A_j}, \hat{q}_{B_j})}{\lambda_j(u_j | \hat{q}_{A_j}, \hat{q}_{B_j})} \right) \quad (2.147)$$

Consequently,  $\Lambda(u|\hat{Y})$  in (2.144) above, may be written

$$\Lambda(u|\hat{Y}) = D_A(\hat{Y})w_A(u|\hat{Y}) + D_B(\hat{Y})w_B(u|\hat{Y}) \quad (2.148)$$

where

$$D_A(\hat{Y}) \triangleq \begin{pmatrix} \text{---} & \frac{\partial q_{A_j}(\hat{Y})}{\partial \hat{Y}_1} & \text{---} \\ \text{-----} & & \text{-----} \\ \text{---} & \frac{\partial q_{A_j}(\hat{Y})}{\partial \hat{Y}_{N_G}} & \text{---} \end{pmatrix}, \quad N_G \times J \quad (2.149)$$

$$\begin{pmatrix} \text{---} & 2\hat{\alpha}p_j^2(\hat{\theta}) & \text{---} \\ \text{---} & 2\hat{\alpha}^2 p_j(\hat{\theta}) \dot{p}_j(\hat{\theta}) & \text{---} \\ \text{---} & 2\hat{\alpha}_R p_j^2(\hat{\theta}_R) & \text{---} \\ \text{---} & 2\hat{\alpha}_R^2 p_j(\hat{\theta}_R) \dot{p}_j(\hat{\theta}_R) & \text{---} \end{pmatrix}, \quad (2.150)$$

$$D_B(\hat{Y}) \triangleq \begin{pmatrix} \text{---} & \frac{\partial q_{B_j}(\hat{Y})}{\partial \hat{Y}_1} & \text{---} \\ \text{-----} & & \text{-----} \\ \text{---} & \frac{\partial q_{B_j}(\hat{Y})}{\partial \hat{Y}_{N_G}} & \text{---} \end{pmatrix}, \quad N_G \times J \quad (2.151)$$

$$\begin{pmatrix} \text{---} & 2\hat{\alpha}_R p_j(\hat{\theta}_R) \dot{p}_j(\hat{\theta}) & \text{---} \\ \text{---} & 2\hat{\alpha} \hat{\alpha}_R \dot{p}_j(\hat{\theta}) p_j(\hat{\theta}_R) & \text{---} \\ \text{---} & 2\hat{\alpha} p_j(\hat{\theta}) p_j(\hat{\theta}_R) & \text{---} \\ \text{---} & 2\hat{\alpha} \hat{\alpha}_R p_j(\hat{\theta}) \dot{p}_j(\hat{\theta}_R) & \text{---} \end{pmatrix} \quad (2.152)$$

$$w_A(u|\hat{Y}) \triangleq (\text{---} w_{A_j}(u_j|\hat{Y}) \text{---})^T, \quad J\text{-vector} \quad (2.153)$$

$$w_B(u|\hat{Y}) \triangleq (---w_{B_j}(u_j|\hat{Y})---)^I, \text{ J-vector} \quad (2.154)$$

in which

$$w_{A_j}(u_j|\hat{Y}) \triangleq \frac{\frac{\partial}{\partial \hat{q}_{A_j}} \lambda_j(u_j|\hat{q}_{A_j}, \hat{q}_{B_j})}{\lambda_j(u_j|\hat{q}_{A_j}, \hat{q}_{B_j})} \quad (2.155)$$

$$\begin{aligned} & \frac{\partial}{\partial \hat{q}_{A_j}} \lambda_j(u_j|q_j(\hat{Y}, \beta_j))|u_j, \hat{Y}) \\ &= \frac{\frac{\partial}{\partial \hat{q}_{A_j}} \lambda_j(u_j|q_j(\hat{Y}, \beta_j))|u_j, \hat{Y})}{\langle \lambda_j(u_j|q_j(\hat{Y}, \beta_j))|u_j, \hat{Y} \rangle} \end{aligned} \quad (2.156)$$

$$\begin{aligned} & \frac{\langle (\frac{\partial \hat{q}_j}{\partial \hat{q}_{A_j}}) (\frac{\partial \lambda_j}{\partial \hat{q}_{A_j}}) (u_j|\hat{q}_j)|u_j, \hat{Y} \rangle}{\langle \lambda_j(u_j|\hat{q}_j)|u_j, \hat{Y} \rangle} \\ &= \end{aligned} \quad (2.157)$$

$$\begin{aligned} & \frac{\frac{\partial \lambda_j}{\partial \hat{q}_j} (u_j|\hat{q}_j)|u_j, \hat{Y}}{\langle \lambda_j(u_j|\hat{q}_j)|u_j, \hat{Y} \rangle} \\ &= \end{aligned} \quad (2.158)$$

and, similarly

$$w_{B_j}(u_j|\hat{Y}) \triangleq \frac{\frac{\partial}{\partial \hat{q}_{B_j}} \lambda_j(u_j|\hat{q}_{A_j}, \hat{q}_{B_j})}{\lambda_j(u_j|\hat{q}_{A_j}, \hat{q}_{B_j})} \quad (2.159)$$

$$\begin{aligned} & \frac{\langle (\frac{\partial \hat{q}_j}{\partial \hat{q}_{B_j}}) (\frac{\partial \lambda_j}{\partial \hat{q}_{B_j}}) (u_j|\hat{q}_j)|u_j, \hat{Y} \rangle}{\langle \lambda_j(u_j|\hat{q}_j)|u_j, \hat{Y} \rangle} \\ &= \end{aligned} \quad (2.160)$$

$$\begin{aligned} & \frac{\langle \cos \beta_j \frac{\partial \lambda_j}{\partial \hat{q}_j} (u_j|\hat{q}_j)|u_j, \hat{Y} \rangle}{\langle \lambda_j(u_j|\hat{q}_j)|u_j, \hat{Y} \rangle} \\ &= \end{aligned} \quad (2.161)$$

Making use of (2.106) in (2.158) and (2.161) [and noting that  $\hat{y}$  in (2.106) included the phase difference parameter ] gives

$$w_{A_j}(u_j | \hat{y}) = \frac{\langle w_j(u_j | \hat{y}, \beta_j) \lambda_j(u_j | \hat{q}_j) | u_j, \hat{y} \rangle}{\langle \lambda_j(u_j | \hat{q}_j) | u_j, \hat{y} \rangle} \quad (2.162)$$

$$= \langle w_j(u_j | \hat{y}, \beta_j) W(u_j | \hat{y}, \beta_j) | u_j, \hat{y} \rangle \quad (2.163)$$

$$w_{B_j}(u_j | \hat{y}) = \langle w_j(u_j | \hat{y}, \beta_j) \cos \beta_j W(u_j | \hat{y}, \beta_j) | u_j, \hat{y} \rangle \quad (2.164)$$

where

$$W(u_j | \hat{y}, \beta_j) \triangleq \frac{\lambda_j(u_j | \hat{q}_j)}{\langle \lambda_j(u_j | \hat{q}_j) | u_j, \hat{y} \rangle} > 0 \quad (2.165)$$

is a weighting factor which essentially modifies the (uniform) a priori distribution of  $\beta_j$ , giving an a posteriori one conditioned on  $u_j$  and  $\hat{y}$ , i.e.

$$p(\beta_j | u_j, \hat{y}) = W(u_j | \hat{y}, \beta_j) p(\beta_j) \quad (2.166)$$

(Clearly

$$\int_{-\frac{\pi}{2}}^{\frac{\pi}{2}} p(\beta_j | u_j, \hat{y}) d\beta_j = \langle W(u_j | \hat{y}, \beta_j) | u_j, \hat{y} \rangle = 1, \quad (2.167)$$

independent of  $u_j$ ,  $\hat{y}$ , as expected.) A more explicit form for  $w_{A_j}$  results from the substitution of (2.95) for  $\lambda_j$  and (2.107) for  $w_j$  into (2.162);

writing the expectations in integral form and taking advantage of the even symmetry wrt  $\beta_j$  (i.e. as  $\cos \beta_j$  in  $\hat{q}_j$ ) gives:

$$w_{A_j}(u_j | \hat{y}) = \frac{\int_0^\pi [4u_j \frac{M_1}{M_0} (4\hat{q}_j u_j)^{-1} - 1] M_0(4\hat{q}_j u_j) \exp(-q_j) d\beta_j}{\int_0^\pi M_0(4\hat{q}_j u_j) \exp(-q_j) d\beta_j} \quad (2.168)$$

or, in terms of the more familiar modified Bessel functions of the first kind,  $I_0$ , and  $I_1$ ,

$$w_{A_j}(u_j | \hat{y}) = \frac{\int_0^\pi \left[ \left( \frac{u_j}{\hat{q}_j} \right)^{\frac{1}{2}} \frac{I_1}{I_0} (2 (\hat{q}_j u_j)^{\frac{1}{2}}) - 1 \right] I_0 (2 (\hat{q}_j u_j)^{\frac{1}{2}}) \exp(-\hat{q}_j) d\beta_j}{\int_0^\pi I_0 (2 (\hat{q}_j u_j)^{\frac{1}{2}}) \exp(-\hat{q}_j) d\beta_j} \quad (2.169)$$

Substituting the approximations (for any real z)

$$\frac{I_1}{I_0}(z) \approx \frac{z}{(4 + z^2)^{\frac{1}{2}}} \quad (\text{good to about 4\%}) \quad (2.170)$$

$$I_0(z) \approx \frac{\exp[(4 + z^2)^{\frac{1}{2}} - \frac{2}{1+z}]}{(1 + 2\pi z)^{\frac{1}{2}}} \quad (\text{good to about 7\%}) \quad (2.171)$$

and the following expansion for  $\hat{q}_j$

$$\hat{q}_j = \hat{q}_{A_j} (1 + B_j \cos \beta_j) \quad (2.172)$$

where

$$B_j \triangleq \frac{\hat{q}_{B_j}}{\hat{q}_{A_j}} \quad (2.173)$$

(and, by virtue of (2.139)

$$-1 \leq B_j \leq +1) \quad (2.174)$$

gives

$$w_{A_j} = \frac{\int_0^\pi w_j L_j d\beta_j}{\int_0^\pi L_j d\beta_j} \quad (2.175)$$

$$w_{B_j} = \frac{\int_0^\pi w_j \cos \beta_j L_j d\beta_j}{\int_0^\pi L_j d\beta_j} \quad (2.176)$$

where

$$w_j \triangleq \frac{u_j}{(1 + \hat{q}_{A_j} u_j (1 + B_j \cos \beta_j))^{\frac{1}{2}}} - 1 \quad (2.177)$$

and

$$L_j^{\Delta} = \frac{\exp[2((1+\hat{q}_{A_j} u_j (1+B_j \cos\beta_j))^{\frac{1}{2}} - \frac{1}{1 + 2(\hat{q}_{A_j} u_j)^{\frac{1}{2}} (1+B_j \cos\beta_j)^{\frac{1}{2}}}) - q_A (1+B_j \cos\beta_j)]}{(1 + 4\pi(\hat{q}_{A_j} u_j)^{\frac{1}{2}} (1 + B_j \cos\beta_j)^{\frac{1}{2}})^{\frac{1}{2}}} \quad (2.178)$$

These last models, (2.175) and (2.176), were the basis of the calculations below.

Substituting (2.148) for  $\Lambda(u|\hat{\gamma})$  into (2.59) for  $\Phi(\hat{\gamma})$  gives

$$\begin{aligned} \Phi(\hat{\gamma}) = & D_A(\hat{\gamma})H_{w_A}(\hat{\gamma})D_A^T(\hat{\gamma}) + D_A(\hat{\gamma})H_{w_{AB}}(\hat{\gamma})D_B^T(\hat{\gamma}) \\ & + (D_A(\hat{\gamma})H_{w_{AB}}(\hat{\gamma})D_B^T(\hat{\gamma}))^T + D_B(\hat{\gamma})H_{w_B}(\hat{\gamma})D_B^T(\hat{\gamma}) \end{aligned} \quad (2.179)$$

where, noting that now

$$u = u(\gamma, \beta_u, n), \quad (2.180)$$

the  $J \times J$  matrices  $H_{w_A}$ ,  $H_{w_B}$ , and  $H_{w_{AB}}$  are given by the following:

$$H_{w_A}(\hat{\gamma}) \triangleq \langle w_A(u(\gamma, \beta_u, n) | \hat{\gamma}) w_A^T(u(\gamma, \beta_u, n) | \hat{\gamma}) | \gamma = \hat{\gamma} \rangle \quad (2.181)$$

$$H_{w_B}(\hat{\gamma}) \triangleq \langle w_B(u(\gamma, \beta_u, n) | \hat{\gamma}) w_B^T(u(\gamma, \beta_u, n) | \hat{\gamma}) | \gamma = \hat{\gamma} \rangle \quad (2.182)$$

$$H_{w_{AB}}(\hat{\gamma}) \triangleq \langle w_A(u(\gamma, \beta_u, n) | \hat{\gamma}) w_B^T(u(\gamma, \beta_u, n) | \hat{\gamma}) | \gamma = \hat{\gamma} \rangle \quad (2.183)$$

in which these averages are taken wrt to the noise  $n$  and phase difference  $\beta_j$  in  $u$ . Assurances given by the LOE theory that

$$0 = \langle \Lambda(u(\gamma, \beta_u, n) | \hat{\gamma}) | \gamma = \hat{\gamma} \rangle \quad (2.184)$$

$$= D_A(\hat{\gamma}) \langle w_A(u(\gamma, \beta_u, n) | \hat{\gamma}) | \gamma = \hat{\gamma} \rangle + D_B(\hat{\gamma}) \langle w_B(u(\gamma, \beta_u, n) | \hat{\gamma}) | \gamma = \hat{\gamma} \rangle \quad (2.185)$$

strongly suggest that

$$\langle w_A(u(\gamma, \beta_u, n) | \hat{\gamma}) | \gamma = \hat{\gamma} \rangle = 0 \quad (2.186)$$

$$\langle w_B(u(\gamma, \beta_u, n) | \hat{\gamma}) | \gamma = \hat{\gamma} \rangle = 0 \quad (2.187)$$

and a simulation study of the processes  $w_A(u|\hat{y})$  and  $w_B(u|\hat{y})$ , using numerical approximations of (2.175) and (2.176) (discussed below) respectively, gave support for (2.186) and (2.187), as well as strong evidence that

$$\langle w_{A_i}(u_i(\gamma, \beta_{u_i}, n_i) | \hat{y}) w_{A_j}(u_j(\gamma, \beta_{u_j}, n_j) | \hat{y}) | \gamma = \hat{y} \rangle = \begin{cases} 0 & i \neq j \\ h_{w_{A_j}}(\hat{y}), & i=j \end{cases} \quad (2.188)$$

$$\langle w_{B_i}(u_i(\gamma, \beta_{u_i}, n_i) | \hat{y}) w_{B_j}(u_j(\gamma, \beta_{u_j}, n_j) | \hat{y}) | \gamma = \hat{y} \rangle = \begin{cases} 0 & i \neq j \\ h_{w_{B_j}}(\hat{y}), & i=j \end{cases} \quad (2.189)$$

$$\langle w_{A_i}(u_i(\gamma, \beta_{u_i}, n_i) | \hat{y}) w_{B_j}(u_j(\gamma, \beta_{u_j}, n_j) | \hat{y}) | \gamma = \hat{y} \rangle = \begin{cases} 0 & i \neq j \\ h_{w_{AB_j}}(\hat{y}), & i=j \end{cases} \quad (2.190)$$

and, on the basis of these conclusions, the matrices  $H_{w_A}(\hat{y})$  and  $H_{w_B}(\hat{y})$  which are the covariances of processes  $w_A(u|\hat{y})$  and  $w_B(u|\hat{y})$  local to  $\gamma - \hat{y} = 0$ , and the matrix  $H_{w_{AB}}(\hat{y})$ , the cross-variance of the processes  $w_A$  and  $w_B$  local to  $\gamma - \hat{y} = 0$ , were taken as diagonal, i.e.

$$H_{w_A}(\hat{y}) = \text{Diag}(\dots, h_{w_{A_j}}(\hat{y}), \dots), J \times J \quad (2.191)$$

$$H_{w_B}(\hat{y}) = \text{Diag}(\dots, h_{w_{B_j}}(\hat{y}), \dots), J \times J \quad (2.192)$$

$$H_{w_{AB}}(\hat{y}) = \text{Diag}(\dots, h_{w_{AB_j}}(\hat{y}), \dots), J \times J \quad (2.193)$$

where definitions for  $h_{w_{A_j}}(\hat{y})$ ,  $h_{w_{B_j}}(\hat{y})$  and  $h_{w_{AB_j}}(\hat{y})$  were taken from equations (2.188), (2.189) and (2.190), respectively, above.

Efforts to use (2.175), (2.176), (2.188), (2.189) and (2.190) and

obtain approximations, respectively, for  $w_{A_j}$ ,  $w_{B_j}$ ,  $h_{w_{A_j}}$ ,  $h_{w_{B_j}}$  and  $h_{w_{AB_j}}$ , analogous to those in (2.116) and (2.123) for  $w_j$  and  $h_{w_j}$ , respectively, in the optimal design, were not successful. As indicated above, it was necessary to use numerical procedures to perform the averaging indicated in the calculations of  $w_{A_j}(u_j|\hat{Y})$ ,  $w_{B_j}(u_j|\hat{Y})$  and  $\Phi(\hat{Y})$ . Numerical versions of (2.175) and (2.176) were used to calculate  $w_{A_j}(u|\hat{Y})$  and  $w_{B_j}(u|\hat{Y})$  in which integrations wrt  $\beta$  were replaced by simulation averages -- i.e. by summations over an index set of LMAX values of  $\beta$  taken uniformly over the interval  $[0, \pi]$ , with due regard for the dynamic range of the computing machine. The forms used are, as follows, suppressing the "j" subscript temporarily:

$$w_A = \left( \frac{\max(1, |h_{a_l}|)}{\max(1, h_l)} \right) \left( \frac{f_{sA}}{f_s} \right) \quad (2.194)$$

$$w_B = \left( \frac{\max(1, |h_{b_l}|)}{\max(1, h_l)} \right) \left( \frac{f_{sB}}{f_s} \right) \quad (2.195)$$

where

$$h_l = \frac{1}{(1 + 4\pi (q_A u)^{\frac{1}{2}} (1 + B \cos \beta_l)^{\frac{1}{2}})^{\frac{1}{2}}} \quad (2.196)$$

$$h_{a_l} = \left( -1 + \frac{u}{(1 + q_A u (1 + B \cos \beta_l))^{\frac{1}{2}}} \right) h_l \quad (2.197)$$

$$h_{b_l} = h_{a_l} \cos \beta_l \quad (2.198)$$

$$f_s = \sum_{\ell}^{LMAX} h_{\ell} \exp(g_{\ell} - g_m) \quad (2.199)$$

$$f_{sA} = \sum_{\ell}^{LMAX} h_{a_{\ell}} \exp(g_{\ell} - g_{m_a}) \quad (2.200)$$

$$f_{s_B} = \sum_{\ell}^{\text{LMAX}} h_{b\ell} \exp(g_{\ell} - g_{m_b}) \quad (2.201)$$

$$g_m = \ln(\text{LMAX}) + \ln(\max_{\ell}(1, h_{\ell}) + \max_{\ell}(g_{\ell})) - \text{EXPMAX} \quad (2.202)$$

$$g_{m_a} = \ln(\text{LMAX}) + \ln(\max_{\ell}(1, |h_{a\ell}|)) + \max_{\ell}(g_{\ell}) - \text{EXPMAX} \quad (2.203)$$

$$g_{m_b} = \ln(\text{LMAX}) + \ln(\max_{\ell}(1, |h_{b\ell}|)) + \max_{\ell}(g_{\ell}) - \text{EXPMAX} \quad (2.204)$$

and

$$\text{EXPMAX} \triangleq \ln(\text{largest REAL variable representable on the computer}) \quad (2.205)$$

$$(\approx 88. \text{ on the PDP-11, } 322. \text{ on the CDC Cyber 172}) \quad (2.206)$$

These equations were the basis for the simulation study that led to the conclusions of whiteness, equations (2.186) thru (2.190), and the consequent diagonality of  $H_{w_A}$ ,  $H_{w_B}$ , and  $H_{w_{AB}}$ , (2.191) thru (2.193). These same equations were used in a numerical study of  $w_{A_j}$  and  $w_{B_j}$  as functions  $u_j$ ,  $q_{A_j}$  and  $B_j$  in an effort to find approximating functions,

$$w_{A_j}(u_j | q_{A_j}, B_j), w_{B_j}(u_j | q_{A_j}, B_j)$$

"after the fact", again without success. As a result

- i. The numerical computation of  $w_{A_j}$ ,  $w_{B_j}$ , given  $u_j$ ,  $q_{A_j}$ , and  $B_j$ , equations (2.194) thru (2.204) had to be programmed as part of the receiver design, to run "on-line" (with a substantial increment in processing time). More will be said about this in the simulation discussion in the next chapter.
- ii. Also, the second-order averages,  $h_{w_{A_j}}$ ,  $h_{w_{B_j}}$  and  $h_{w_{AB_j}}$ , associated with the calculation of  $\phi$  could not be adequately approximated

in closed-form, and numerical averages based on (2.188) thru (2.190) had to be done.

These latter calculations will be summarized at this point in the discussion since they were done "off-line" and hence were not part of the receiver simulation per se, but more a part of the design.

As (2.188) thru (2.190) suggests, the second-order averages had to be taken wrt the  $\beta_{u_j}$ -variable and the noise  $n_j$  in the observation sample,  $u_j$ , appearing as an argument of the conditional mean processes  $w_{A_j}$ ,  $w_{B_j}$  -- clearly a very lengthy process but one fortunately that could be done off-line. Such an approach was used, but the effort then to find approximating functions "after the fact" was again not successful, and a plan was pursued involving calculating and storing many values of the second-order averages in tables off-line, then using table-lookup procedures indexed by  $q_{A_j}$  and  $B_j$  and interpolation on-line to calculate  $\Phi(\hat{y})$ .

To improve the accuracy of these results and more nearly guarantee the non-negativeness of the calculated  $\Phi(\hat{y})$ , the  $\Phi$ -matrix was determined element-wise, as follows:

$$\begin{aligned} \phi_{li} = \phi_{il} = \sum_{j=1}^J [s_{w_{A_j}} D_{A_{ij}} - s_{w_{B_j}} D_{B_{ij}}] (s_{w_{A_j}} D_{A_{lj}} - s_{w_{B_j}} D_{B_{lj}}) \\ + (1 + R_{AB_j}) s_{w_{A_j}} s_{w_{B_j}} (D_{A_{ij}} D_{B_{lj}} + D_{A_{lj}} D_{B_{ij}})] \end{aligned} \quad (2.207)$$

where

$$s_{w_{A_j}} \triangleq (h_{w_{A_j}})^{\frac{1}{2}}, \quad s_{w_{A_j}} > 0 \quad (2.208)$$

$$s_{w_{B_j}} \triangleq (h_{w_{B_j}})^{\frac{1}{2}}, \quad s_{w_{B_j}} > 0 \quad (2.209)$$

$$R_{ABj} \triangleq \frac{h_{wABj}}{s_{wAj} s_{wBj}}, \quad -1 \leq R_{ABj} \leq +1 \quad (2.210)$$

The averaging associated with these calculations also was done by simulation rather than by using numerical integration of the associated probability integrals. In particular, suppressing the above "j" subscript temporarily and considering (2.136) and (2.172) then clearly  $u_{(j)}$  in (2.48) can be written without confusion as

$$u = q(q_A, B, \beta_u) + 2n_c [q(q_A, B, \beta_u)]^{\frac{1}{2}} + n_c^2 + n_s^2 \quad (2.211)$$

$$= u(\beta_u, n | q_A, B) \quad (2.212)$$

where, of course  $q_A = q_A(\gamma)$  and  $B=B(\gamma)$ . Then  $w_{A(j)}$  can be denoted as

$$w_A(u | \hat{q}_A, \hat{B}) = w_A(u(\beta_u, n | q_A, B) | \hat{q}_A, \hat{B}) \quad (2.213)$$

and with this notation the calculation of  $s_{wA}$  is described, as follows

$$s_{wA} = \left[ \frac{1}{L_{\max} J_{n_{\max}}} \sum_{\ell=1}^{L_{\max}} \sum_{i=1}^{J_{n_{\max}}} w_A^2(u(\beta_{u\ell}, n_i | \hat{q}_A, \hat{B}) | \hat{q}_A, \hat{B}) \right]^{\frac{1}{2}} \quad (2.214)$$

$$= S_{wA}(\hat{q}_A, \hat{B}) \quad (2.215)$$

and similarly for  $s_{wB}$ , etc. where the components  $n_{c_i}, n_{s_i}$  of the  $J_{n_{\max}}$  noise vectors  $n_i$  were drawn from a Gaussian pseudorandom noise generator (with mean zero, variance 0.5, see (2.11)) and the  $L_{\max}$  values of  $\beta_{u\ell}$  were taken uniformly from the interval  $[0, \pi]$ . Values for  $L_{\max}$  and  $J_{n_{\max}}$  used were

$$L_{\max} = 11 \quad (2.216)$$

$$J_{n_{\max}} = 400 \quad (2.217)$$

for each  $(q_{A_j}, B_j)$  point. In building the tables 300  $(q_{A_j}, B_j)$  points were employed distributed generally, as follows

$$0.1 \leq q_{A_j} \leq 10^8 \quad (25 \text{ values}) \quad (2.218)$$

$$0.01 \leq B_j \leq 0.990 \quad (12 \text{ values}) \quad (2.219)$$

and values for  $\ln(s_{w_{A_j}})$ ,  $\ln(s_{w_{B_j}})$  and  $R_{AB_j}$  were calculated and stored. These off-line calculations were done by PROGRAM WLOGSW, associated subroutines WAVGS and WAWB, and FUNCTION GAUSS, which are all included in Appendix A. Values calculated for  $\ln(s_{w_{A_j}})$ ,  $\ln(s_{w_{B_j}})$ , and  $R_{AB_j}$  are given in Tables 2.1, 2.2 and 2.3 respectively.

Then, in the receiver, for each  $(\hat{q}_{A_j}, \hat{B}_j)$  point associated with the estimate  $\hat{y}(k|k-1)$ , the tables were entered and

- i. Values  $\hat{q}_{A_i}, \hat{q}_{A_{i+1}}, \hat{B}_i, \hat{B}_{i+1}$  from the tables were found, such that

$$\hat{q}_{A_i} \leq \hat{q}_{A_j} < \hat{q}_{A_{i+1}} \quad (2.220)$$

$$\hat{B}_i \leq \hat{B}_j < \hat{B}_{i+1} \quad (2.221)$$

- ii. Then, linear interpolation between calculated averages in the table was done, using the general formula

$$\begin{aligned} f(x_1 + \Delta x, y_1 + \Delta y) = & f(x_1, y_1) + \frac{f(x_2, y_1) - f(x_1, y_1)}{x_2 - x_1} \Delta x \\ & + \frac{f(x_1, y_2) - f(x_1, y_1)}{y_2 - y_1} \Delta y \\ & + \frac{f(x_1, y_1) + f(x_2, y_2) - f(x_1, y_2) - f(x_2, y_1)}{(x_2 - x_1)(y_2 - y_1)} \Delta x \Delta y \end{aligned} \quad (2.222)$$

- iii. The interpolated values of  $\ln(s_{w_{A_j}})$ ,  $\ln(s_{w_{B_j}})$  were exponentiated),

Table 2.1  $\text{Ln}(s_{wA_j}(q_{A_j}, B_j))$

B *	.010	.020	.040	.060	.100	.200	.300	.500	.700	.900	.950	.990
QA:												
.1000	-.11	-.11	-.11	-.11	-.11	-.11	-.11	-.11	-.11	-.11	-.11	-.11
.1778	-.16	-.16	-.16	-.16	-.16	-.16	-.16	-.16	-.16	-.16	-.16	-.16
.3162	-.23	-.23	-.23	-.23	-.23	-.23	-.23	-.23	-.23	-.23	-.24	-.24
.5623	-.33	-.33	-.33	-.33	-.33	-.33	-.33	-.33	-.34	-.34	-.35	-.35
1.000	-.47	-.47	-.47	-.47	-.47	-.47	-.47	-.48	-.49	-.50	-.50	-.51
1.778	-.65	-.65	-.65	-.65	-.66	-.66	-.66	-.68	-.69	-.71	-.72	-.72
3.162	-.90	-.90	-.91	-.91	-.91	-.91	-.92	-.95	-.97	-.98	-.97	-.97
5.623	-1.2	-1.2	-1.2	-1.2	-1.2	-1.2	-1.2	-1.3	-1.3	-1.2	-1.2	-1.2
10.00	-1.5	-1.5	-1.5	-1.5	-1.5	-1.5	-1.6	-1.7	-1.7	-1.5	-1.4	-1.3
17.78	-1.8	-1.8	-1.8	-1.8	-1.8	-1.9	-1.9	-2.1	-2.0	-1.7	-1.6	-1.4
31.62	-2.1	-2.1	-2.1	-2.1	-2.1	-2.2	-2.3	-2.4	-2.4	-2.0	-1.8	-1.6
56.23	-2.3	-2.3	-2.4	-2.4	-2.4	-2.6	-2.7	-2.8	-2.7	-2.4	-2.1	-1.7
100.0	-2.6	-2.6	-2.7	-2.7	-2.8	-3.0	-3.1	-3.1	-3.0	-2.7	-2.4	-1.9
177.8	-2.9	-2.9	-3.0	-3.0	-3.1	-3.3	-3.4	-3.4	-3.4	-3.0	-2.7	-2.0
316.2	-3.2	-3.2	-3.3	-3.3	-3.5	-3.7	-3.8	-3.8	-3.6	-3.2	-2.9	-2.2
562.3	-3.5	-3.5	-3.6	-3.7	-3.9	-4.0	-4.1	-4.1	-3.8	-3.3	-3.1	-2.3
1000.	-3.8	-3.8	-4.0	-4.1	-4.3	-4.4	-4.4	-4.3	-3.9	-3.5	-3.2	-2.6
1778.	-4.1	-4.2	-4.4	-4.4	-4.6	-4.7	-4.7	-4.4	-4.1	-3.7	-3.4	-2.8
3162.	-4.4	-4.5	-4.7	-4.9	-5.0	-5.1	-4.9	-4.5	-4.3	-3.9	-3.7	-3.1
5623.	-4.7	-4.8	-5.1	-5.2	-5.3	-5.3	-5.0	-4.7	-4.6	-4.2	-4.0	-3.4
10000	-5.1	-5.3	-5.5	-5.5	-5.6	-5.4	-5.1	-5.0	-4.8	-4.5	-4.3	-3.7
.1000E+00	-5.5	-5.7	-6.0	-6.0	-6.3	-6.2	-6.1	-6.0	-5.9	-5.6	-5.4	-4.9
.1000E+07	-7.9	-7.7	-7.4	-7.3	-7.3	-7.2	-7.2	-7.2	-7.1	-6.8	-6.6	-6.0
.1000E+08	-8.6	-8.5	-8.4	-8.4	-8.4	-8.4	-8.4	-8.3	-8.2	-7.9	-7.7	-7.2
.1000E+09	-9.0	-9.0	-9.0	-9.0	-9.0	-9.0	-9.0	-9.0	-9.0	-9.1	-8.9	-8.3

Table 2.2  $\ln (s_{w\beta_j}(q_{A_j}, B_j))$

B =	.010	.020	.040	.060	.100	.200	.300	.500	.700	.900	.950	.990
QA:												
.1000	-7.6	-7.1	-6.4	-6.0	-5.5	-4.8	-4.4	-3.9	-3.5	-3.2	-3.1	-3.1
.1778	-7.4	-6.7	-6.0	-5.6	-5.1	-4.4	-4.0	-3.5	-3.1	-2.8	-2.7	-2.7
.3162	-6.4	-6.2	-5.5	-5.1	-4.6	-3.9	-3.5	-3.0	-2.7	-2.4	-2.3	-2.3
.5623	-6.5	-5.8	-5.1	-4.7	-4.2	-3.5	-3.1	-2.6	-2.2	-2.0	-1.9	-1.9
1.000	-6.1	-5.4	-4.7	-4.3	-3.8	-3.1	-2.7	-2.2	-1.8	-1.6	-1.6	-1.5
1.778	-5.7	-5.1	-4.4	-4.0	-3.4	-2.8	-2.4	-1.9	-1.6	-1.4	-1.3	-1.3
3.162	-5.0	-4.4	-4.2	-3.8	-3.3	-2.6	-2.2	-1.7	-1.5	-1.3	-1.2	-1.2
5.623	-5.5	-4.9	-4.2	-3.8	-3.3	-2.6	-2.2	-1.8	-1.5	-1.3	-1.3	-1.2
10.00	-5.6	-4.9	-4.2	-3.8	-3.3	-2.6	-2.3	-1.9	-1.7	-1.5	-1.4	-1.3
17.78	-5.6	-4.9	-4.2	-3.8	-3.3	-2.7	-2.4	-2.2	-2.0	-1.7	-1.6	-1.4
31.62	-5.6	-4.9	-4.2	-3.8	-3.3	-2.8	-2.6	-2.5	-2.4	-2.0	-1.8	-1.6
56.23	-5.6	-4.9	-4.2	-3.8	-3.4	-2.9	-2.8	-2.8	-2.7	-2.4	-2.1	-1.7
100.0	-5.6	-4.9	-4.2	-3.9	-3.5	-3.1	-3.1	-3.1	-3.0	-2.7	-2.4	-1.9
177.8	-5.6	-4.9	-4.2	-3.9	-3.6	-3.4	-3.4	-3.4	-3.4	-3.0	-2.7	-2.0
316.2	-5.6	-4.9	-4.3	-4.0	-3.8	-3.7	-3.8	-3.8	-3.7	-3.2	-3.0	-2.2
562.3	-5.6	-4.9	-4.4	-4.1	-4.0	-4.0	-4.1	-4.1	-3.9	-3.5	-3.2	-2.4
1000.	-5.6	-5.0	-4.5	-4.3	-4.3	-4.4	-4.4	-4.4	-4.1	-3.7	-3.4	-2.6
1778.	-5.6	-5.0	-4.6	-4.6	-4.6	-4.7	-4.8	-4.6	-4.4	-3.9	-3.5	-2.9
3162.	-5.6	-5.1	-4.9	-4.9	-4.9	-5.1	-5.1	-4.8	-4.6	-4.1	-3.8	-3.2
5623.	-5.7	-5.3	-5.1	-5.2	-5.3	-5.4	-5.3	-5.1	-4.9	-4.3	-4.1	-3.5
10000	-5.6	-5.2	-5.5	-5.5	-5.6	-5.7	-5.5	-5.3	-5.1	-4.6	-4.4	-3.7
.1000E+06	-6.6	-6.7	-6.2	-6.8	-6.7	-6.6	-6.5	-6.3	-6.1	-5.8	-5.5	-4.9
.1000E+07	-7.9	-8.0	-7.8	-7.7	-7.7	-7.5	-7.5	-7.4	-7.3	-6.9	-6.7	-6.0
.1000E+08	-9.0	-8.9	-8.8	-8.7	-8.7	-8.7	-8.7	-8.6	-8.4	-8.1	-7.8	-7.2
.1000E+09	-10.	-9.8	-9.8	-9.8	-9.8	-9.8	-9.8	-9.7	-9.6	-9.2	-9.0	-8.3

Table 2.3  $R_{AB_j}(q_{A_j}, B_j)$

RAB:												
B =	.010	.020	.040	.060	.100	.200	.300	.500	.700	.900	.950	.990
QA:												
.1000	.14	.14	.14	.14	.14	.14	.14	.16	.18	.21	.21	.20
.1778	-.43E-01	-.43E-01	-.43E-01	-.43E-01	-.43E-01	-.41E-01	-.37E-01	-.26E-01	-.44E-02	.34E-01	.48E-01	.49E-01
.3162	-.16	-.16	-.16	-.16	-.16	-.16	-.16	-.15	-.14	-.12	-.10	-.96E-01
.5623	-.24	-.24	-.24	-.24	-.24	-.24	-.24	-.24	-.25	-.24	-.24	-.23
1.0000	-.32	-.32	-.32	-.32	-.32	-.32	-.32	-.33	-.35	-.37	-.37	-.37
1.778	-.37	-.37	-.37	-.37	-.37	-.37	-.38	-.40	-.44	-.48	-.49	-.50
3.162	-.35	-.35	-.35	-.35	-.35	-.36	-.38	-.43	-.50	-.59	-.61	-.63
5.623	-.28	-.28	-.28	-.28	-.28	-.30	-.33	-.42	-.55	-.69	-.73	-.75
10.00	-.22	-.22	-.22	-.22	-.22	-.24	-.28	-.39	-.57	-.77	-.81	-.84
17.78	-.18	-.18	-.18	-.18	-.19	-.21	-.25	-.39	-.59	-.81	-.86	-.90
31.62	-.15	-.15	-.16	-.16	-.16	-.20	-.25	-.41	-.60	-.83	-.89	-.94
56.23	-.14	-.14	-.14	-.14	-.15	-.19	-.26	-.43	-.61	-.84	-.91	-.96
100.0	-.13	-.13	-.13	-.13	-.14	-.20	-.28	-.45	-.63	-.84	-.91	-.97
177.8	-.12	-.12	-.12	-.13	-.14	-.21	-.29	-.46	-.64	-.85	-.91	-.98
316.2	-.11	-.11	-.12	-.12	-.14	-.22	-.30	-.47	-.65	-.85	-.90	-.98
562.3	-.11	-.11	-.11	-.12	-.15	-.23	-.31	-.48	-.66	-.83	-.90	-.98
1000	-.11	-.11	-.11	-.12	-.15	-.23	-.31	-.48	-.66	-.82	-.89	-.97
1778	-.10	-.10	-.11	-.12	-.15	-.24	-.32	-.48	-.62	-.81	-.89	-.97
3162	-.10	-.99E-01	-.11	-.13	-.16	-.24	-.31	-.47	-.62	-.81	-.89	-.97
5623	-.98E-01	-.96E-01	-.11	-.13	-.16	-.23	-.30	-.41	-.55	-.82	-.89	-.96
10000	-.95E-01	-.97E-01	-.11	-.13	-.16	-.22	-.29	-.37	-.59	-.82	-.88	-.96
.1000E+06	-.93E-01	-.10	-.12	-.10	-.10	-.14	-.26	-.42	-.56	-.78	-.86	-.96
.1000E+07	-.93E-01	-.01E-01	-.35E-01	-.43E-01	-.87E-01	-.15	-.22	-.38	-.56	-.78	-.86	-.96
.1000E+08	-.19E-01	-.15E-01	-.36E-01	-.47E-01	-.74E-01	-.15	-.22	-.38	-.56	-.78	-.86	-.96
.1000E+09	-.54E-02	-.15E-01	-.30E-01	-.44E-01	-.74E-01	-.15	-.22	-.38	-.56	-.78	-.86	-.96

and the results with the interpolated value of  $R_{AB}$  were used in calculating  $\phi_{\ell i}$  via (2.207).

This completes the calculation of  $\Lambda(u|\hat{y})$  and  $\Phi(\hat{y})$ , hence the description of the Scan Data Processor, for the Suboptimal Design.

The Tracking Loop for the Suboptimal Design is identical with that of the Optimal Design, except for changes due to the lower dimensions of the state and parameter vectors. Generally

- i. The last two rows of the state vector estimate and corresponding rows and/or columns of associated matrices were eliminated;
- ii. The last row of the parameter-vector (estimate) and corresponding rows and/or columns of associated matrices were eliminated.

This simple adaptation procedure results from the special formulations of the state- and parameter-vectors adopted. It was employed in the simulation easily and without problem.

This same general procedure was used also in obtaining the Non-Adaptive Design (recall (2.83), (2.84)) -- simply by (initializing  $\hat{y}_R=0$  and then) pruning the several vectors and matrices back to the appropriate dimensions, starting with either the optimal or suboptimal designs (both give the same results). This too was used in simulation without problem.

This concludes the formal development of the receiver algorithms. We turn next to the simulation studies and discussion of results.



### SECTION III

#### SIMULATION STUDIES

The principal simulation result used in evaluating the performance of the various receiver designs was the calculated root mean square error (RMSE) (sample) statistic. A large number of studies of RMSE versus  $\theta_{sep}$  were conducted, where

$$\theta_{sep} \triangleq \theta - \theta_R \quad (3.1)$$

These studies were parameterized, in general, by the following:

$$\text{DSNRDB (or S/N)} \triangleq 20 \log_{10} \alpha \quad (3.2)$$

$$\rho \triangleq \alpha_R / \alpha \quad (3.3)$$

$$\beta, \text{ the phase difference at the beginning of the simulation run} \quad (3.4)$$

$$F_{sc} = \omega_{sc} / 2\pi, \text{ the scalloping rate (Hz)} \quad (3.5)$$

$$B_{MLS} \triangleq \text{the 3 db beam width of the MLS transmitting antenna} \quad (3.6)$$

$$B_{RCVR} \triangleq \text{the presumed 3 db beam width in the receiver of the MLS transmitting antenna} \quad (3.7)$$

Other RMSE studies performed included:

1. RMSE versus  $(B_{RCVR}/B_{MLS})$ , parameterized by S/N,  $\rho$ ,  $\beta$ ,  $F_{sc}$  and  $\theta_{sep}$ ; this study was deemed important because of the presumption in the Optimal and Suboptimal receivers of a value for the MLS ground (transmitting) antenna beam width, a parameter not currently transmitted in the preamble of the MLS signal.
2. RMSE versus  $F_{sc}$ , parameterized by S/N,  $\rho$ ,  $\beta$ ,  $\theta_{sep}$ ,  $B_{MLS}$ ,  $B_{RCVR}$ .

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Two series of error time-history studies were conducted also, all runs in both cases being parameterized by the full set,  $S/N$ ,  $\rho$ ,  $\beta$ ,  $F_{sc}$ ,  $\theta_{sep}$ ,  $B_{MLS}$ ,  $B_{RCVR}$ , as well as other variants, such as the presence or absence of the constraints imposed on the estimates, etc. One set of error time-history studies, termed Interference Acquisition scenario runs, evaluated the "pull-in" ability of the interference tracker for potential use in interference acquisition. The second set of error time-history studies, termed Crossing Multipath scenario runs, evaluated the tracking performance of the receiver designs in dynamic environments involving multipath interference which is initially out-of-beam, then closes to in-beam, crosses, and finally opens to out-of-beam.

A major portion of the research was devoted to simulation studies -- both program development and receiver performance evaluation. The programs used in the receiver performance studies, totaling about 100 pages of FORTRAN code, are listed in Appendix A and are briefly discussed in the first part of this section. The second part of this section presents a representative selection of data from the various simulation runs, and discusses the results.

#### A. SIMULATION MODELS

The bulk of the computation performed in the simulation was done in FORTRAN subroutines described as follows:

MLSSUB: Simulation of the environment (via a state-space model with "true"-state,  $x(k)$ ) and the received (envelope) signal vector,  $u(k)$ ; we note here that within a scan the quantity

$$\beta_j = \beta + w_{sc} T_j \quad (3.7a)$$

is used as a better approximation of the phase difference (rather than simply  $\beta$ ) in computing the  $j$ th sample,  $u_j$ , of the received envelope signal.

RCVR: Computation of the estimate,  $\hat{\theta}(k|k)$ , of the angular coordinate  $\theta(k)$ , given the observations vector,  $u(k)$ ;

CONTRL: Conduct of the simulation run, including performing all I/O operations, special initializations and performance evaluation calculations.

The macro-flow-charts in Figure 3.1 show the organizations of these routines and their interrelations.

The simulation main program, MLSSIM, simply establishes COMMON storages and calls MLSSUB. Subroutine MLSSUB calls a library gaussian pseudorandom number generator function GAUSS and the following two MLS functions, in addition to RCVR and CONTRL:

PMLS: The antenna selectivity function,  $p_{MLS}(\theta_e)$ , of the MLS transmitting antenna, used in constructing the observations vector  $u(k)$ . The following -23 db sidelobe function was used in the study:

$$p_{MLS}(\theta_e) = \begin{cases} \pi/4, & |z| = 1 \\ \frac{\cos \frac{\pi}{2} z}{1 - z^2}, & |z| \neq 1 \end{cases} \quad (3.8)$$

$$\text{where } z \triangleq 2.4\theta_e / B_{MLS} \quad (3.9)$$

$$\theta_e \triangleq \text{angle from beam center} \quad (3.10)$$

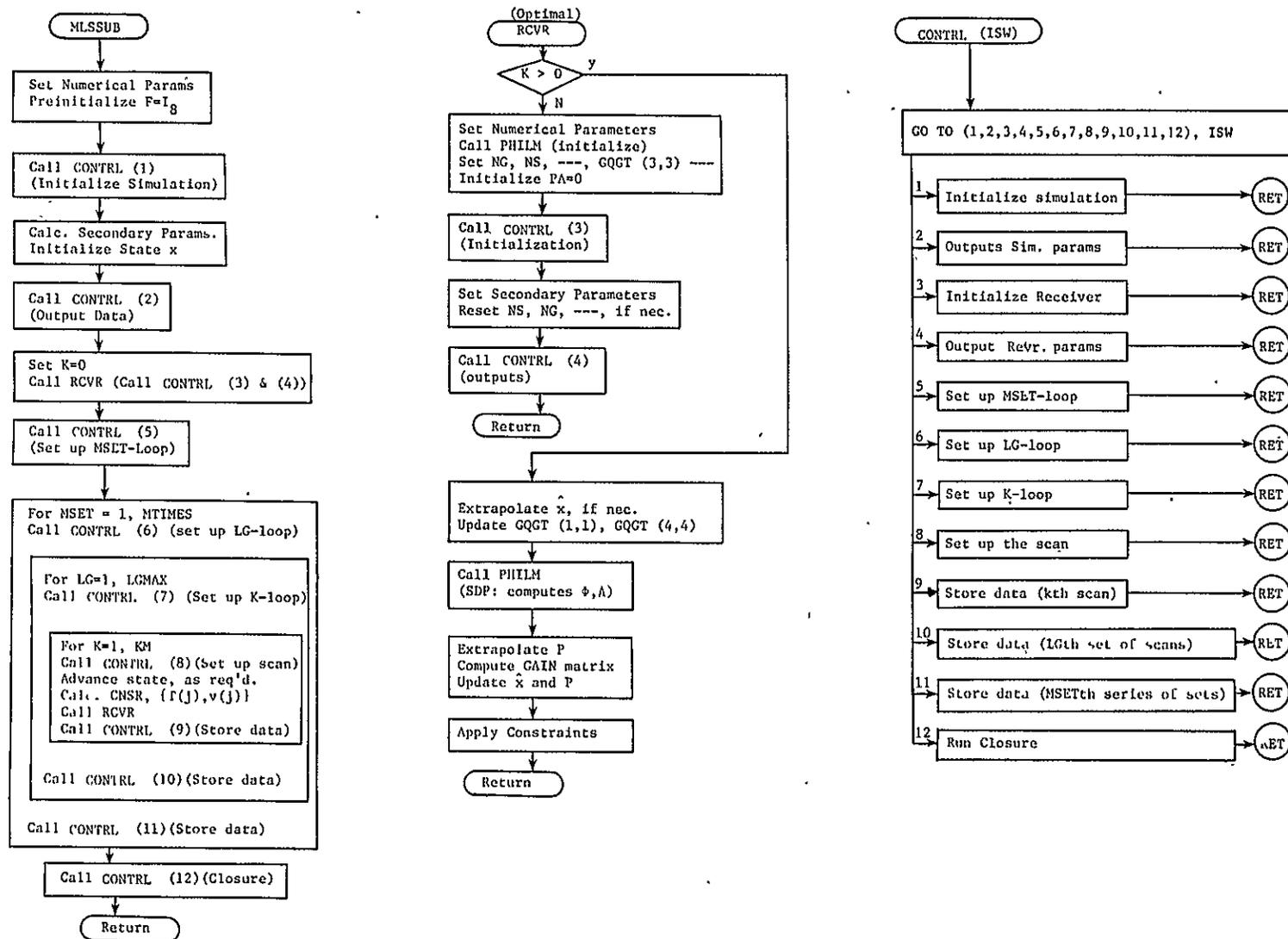


Figure 3.1 Flow Charts for MLSSUB, (OPT) RCVR, and CONTRL

THA: The antenna scanning function,  $\theta_A(\tau)$ , of the MLS transmitting antenna, used in constructing the vector  $u(k)$ . The function in (2.124) above was specified in the MLS specifications and used in the study.

The programs MLSSIM, MLSSUB, THA, DFLTR1 (a 1st-order digital filtering subroutine used when the threshold receiver is running) and a BLOCK DATA program, MLS, collectively constituted a software module (or file), denoted MLSSIM. The function PMLS, and BLOCK DATA program PMLSID were put into a separate module, PMLS1, to facilitate changing the  $p_{MLS}(\cdot)$  function. The listouts of these and other programs found in Appendix A are grouped into modules.

Two scenarios of subroutine RCVR were used, which are distinguished by module (or file) names suggestive of their natures, as follows:

OPTRVR: The optimal structure, comprising the Scan Data Processor and the Tracking Loop; calls subroutine PHILM (which calculates SDP quantities  $\Phi$ ,  $\Lambda$ , and is described below) as well as matrix arithmetic subroutines MATSM, MATMUL and MATINV.

THDRVR: A design similar to present commercial approaches using thresholding principles [11]. The simulation model, which involved

- i) A 3db-below-peak threshold (referred to the linear envelope)
- ii) A 300 microsec tracking gate for interference exclusion.

- iii) A dwell gate for "loss-of-track" decisions
- iv) Input of the log envelope signal, filtered by a 25 KHz low pass filter.
- v) Error filtered with a 10 r/s bandwidth low pass filter for evaluation,

was developed to provide baseline data for performance comparisons. See the references [11], [4, pp. 25,26] and the program in Appendix A for further details. The program calls subroutine DFLTR1 to provide the 25 kHz filtering.

Two versions of PHILM were used, distinguished by module names, as follows:

PLOPT: The Scan Data Processor calculations of  $\Phi$ ,  $\Lambda$  for the Optimal design. This uses function THA, (2.124) above, and functions P and PDOT given below. We note here that in the calculation of matrix D in PLOPT, analogous to (3.7a), the quantity

$$\hat{\beta}_j = \hat{\beta} + \hat{w}_{sc} \tau_j \quad (3.10a)$$

was used for  $\hat{\beta}$  in (2.103) in an effort to improve the receiver performance by making use of the  $\hat{w}_{sc}$  information at this point.

PLSUB: The SDP calculations of  $\Phi$ ,  $\Lambda$  for the Suboptimal design. This calls the same functions THA, P, PDOT used by PLOPT, preceding, but also calls subroutines WAWBJ (which calculated "on-line" conditional averages

$w_A(u_j, \gamma)$  and  $w_B(u_j, \gamma)$  using (2.194), (2.195) and succeeding equations) and subroutine SWFCNS (which did the table look-up and necessary interpolation to produce the values  $s_{w_{A_j}}$ ,  $s_{w_{B_j}}$  and  $R_{AB_j}$  (2.208), (2.209) and (2.210) respectively needed to calculate matrix  $\Phi$  via (2.207). See the program in Appendix A for further details.

The functions P, PDOT constitute the module POPT1 and are used by both versions of PHILM. They are described as follows:

P: The antenna selectivity function  $p(\theta_e)$  assumed in the receiver design to be in effect in the received signal vector  $u(k)$ . The following -23 db sidelobe function was used in the study:

$$p(\theta_e) = \begin{cases} \pi/4, & |z| = 1 \\ \frac{\cos \frac{\pi}{2} z}{1 - z^2}, & |z| \neq 1 \end{cases} \quad (3.11)$$

$$\text{where } z \triangleq 2.4 \theta_e / B_{\text{RCVR}} \quad (3.12)$$

$$\theta_e \triangleq \text{angle from beam center} \quad (3.13)$$

This is the same function as  $p_{\text{MLS}}(\theta_e)$ , (3.8), but it was programmed twice with distinct names to allow different functions to be used (alternate function were not studied, however). Figure 3.2 shows the function  $p(\cdot)$ , (3.11) above, centered in the same 65-sample window on the same sampling grid (FSAMP = 160 kHz, OMEGA = 20,000 Deg./sec.) as in the receiver.

```

RUN P PLOT
  BMLS = 1.00000
  OMEGA = 20000.0
  FSAHP = 160000.
  DTHETA = 0.125000
  JMAX = 65
  THEMIN = -4.00000
  THEMAX = 4.00000

```

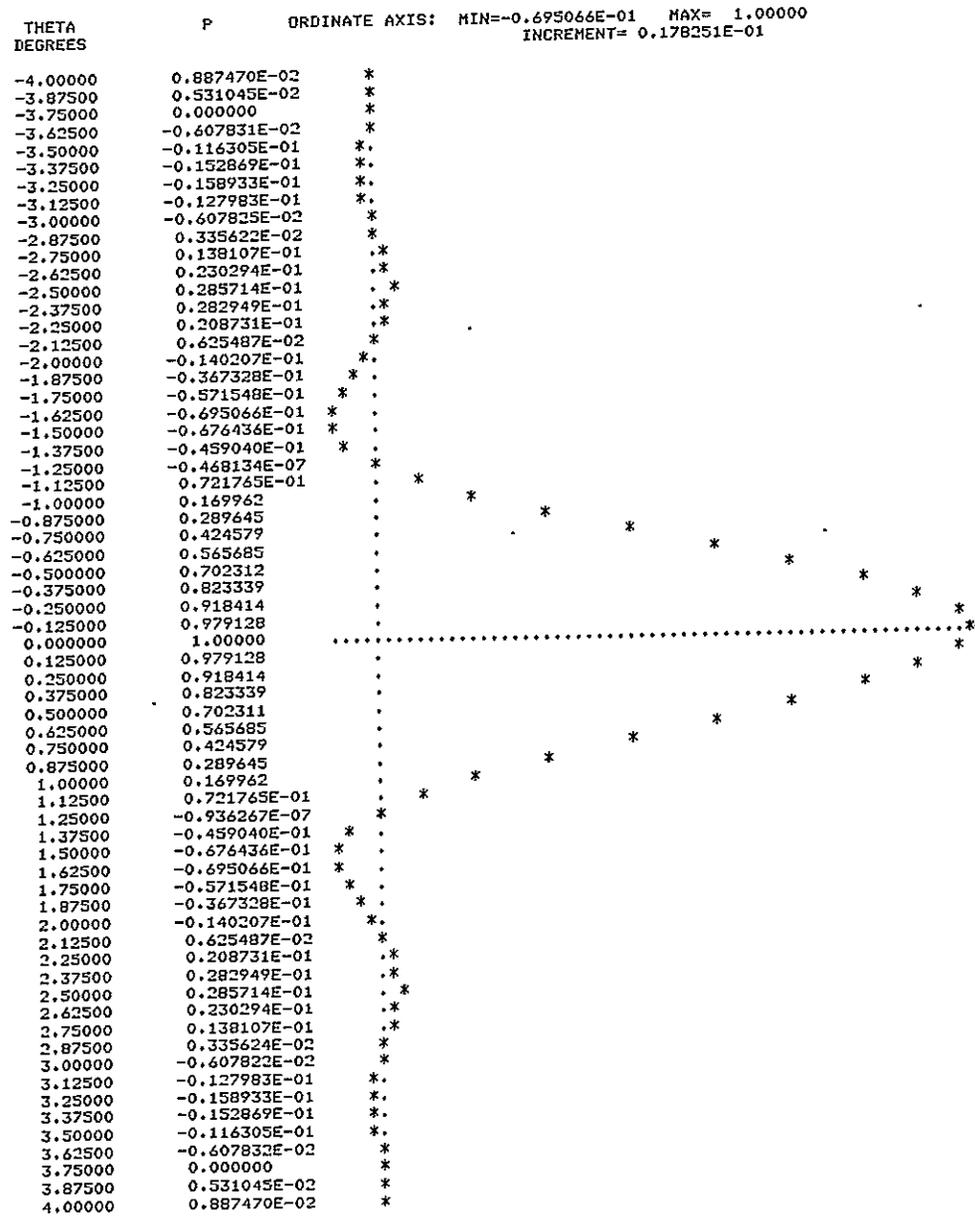


Figure 3.2 Antenna Selectivity function,  $p(\theta)$ , used

PDOT: The function  $\frac{dp(\theta_e)}{d\theta_e}$ . On the basis of (3.11) thru (3.13) the following was used:

$$\frac{dp(\theta_e)}{d\theta_e} = \begin{cases} \frac{-0.3\pi}{B_{RCVR}} \text{signum}(z), & |z| = 1 \\ \frac{0.3\pi^2}{B_{RCVR}} \left\{ \frac{\cos(z+1)\pi/2 - \frac{\sin(z+1)\pi/2}{(z+1)\pi/2}}{(z+1)\pi/2} + \frac{\cos(z-1)\pi/2 - \frac{\sin(z-1)\pi/2}{(z-1)\pi/2}}{(z-1)\pi/2} \right\}, & |z| \neq 1 \end{cases} \quad (3.14)$$

Several versions of subroutine CONTRL, distinguished by module names, as follows, were used, conducting the simulation through various types of scenarios and test runs:

CTLACQN: An interference acquisition scenario, testing the "pull-in" power of the interference tracking algorithm. Initially no interference is present and the interference tracker states are tethered to "idler" values, as follows:

$$\hat{\alpha}_{R_0} = 0.5 \hat{\alpha} \quad (3.15)$$

$$\hat{\theta}_{R_0} = \hat{\theta} - 1.5 \text{ degrees} \quad (3.16)$$

$$\hat{\dot{\theta}}_{R_0} = 0 \text{ degrees/second} \quad (3.17)$$

$$\hat{\beta}_0 = \pi/2 \text{ radians} \quad (3.18)$$

$$\hat{\omega}_{sc_0} = 0 \text{ radians/second} \quad (3.19)$$

A step of interference then occurs with prescribed parameter values, the interference tracker is untethered and the estimate error-time-histories are generated.

CTLCRMP: A crossing multipath scenario, testing the tracking abilities of a receiver design from an out-of-beam interference condition, thru a crossing in-beam condition to a out-of-beam situation again under prescribed conditions; error-time-histories are generated.

CTLMSTH: An RMS error versus  $\theta_{sep}$  study in which, by a suitable nonzero assignment of  $w_{sc}$ , the effects of  $\beta$  are approximately averaged out as the statistical sample of desired size, 100 scans, evolves. 110 scans are calculated and the first 10 discarded in computing error statistics for each value of  $\theta_{sep}$ . The program increments  $\theta_{sep}$  and repeats the calculation for up to 13 values of  $\theta_{sep}$ .

CTL0E: Another, more expensive, RMS error versus  $\theta_{sep}$  study in which for each value of  $\theta_{sep}$   $\beta$  is stepped through 20 values uniformly spaced on the  $(-\pi, \pi)$  interval and, for each value of  $\beta$ , 30 scans are generated, the first 10 being discarded and the latter 20 being used in the statistical calculations.

CTLMSSBB: An RMS error versus  $B_{ratio}$  study, where

$$B_{ratio} \triangleq B_{RCVR}/B_{MLS}. \quad (3.20)$$

The study is performed in a manner similar to that in CTLMSTH above, including the use of nonzero  $w_{sc}$ .

7 values of  $B_{\text{ratio}}$  were used in the range

$$(10)^{-\frac{1}{2}} \leq B_{\text{ratio}} \leq (10)^{\frac{1}{2}} \quad (3.21)$$

with

$$\left. \begin{array}{l} B_{\text{RCVR}} = 1^\circ \\ B_{\text{MLS}} > 1^\circ \end{array} \right\} , \text{ when } B_{\text{ratio}} < 1 \quad (3.22)$$

and

$$\left. \begin{array}{l} B_{\text{RCVR}} > 1^\circ \\ B_{\text{MLS}} = 1^\circ \end{array} \right\} , \text{ when } B_{\text{ratio}} > 1 \quad (3.23)$$

CTLMSFS: An RMS Error versus  $F_{\text{sc}}$  study. This study is also performed in a manner similar to that in CTLMSTH above, except that  $\omega_{\text{sc}}$  is assigned higher and higher integer multiples of the minimum value (0.135 Hz in AZIMUTH) which would integrate  $\beta$  over a  $2\pi$  interval during a 100-scan time period.

Block data programs were included in many modules to initialize COMMON storages. A library of general math and utility programs was also used and is included in the program listings in Appendix A.

All simulation runs were made with Azimuth angle function data, though the option for elevation simulation was included in the programs.

Parameter values written in storages are, as follows:

	<u>AZ</u>	<u>EL</u>	
$\theta_{A_{\text{max}}} =$	62.666667°	30.666667°	(3.24)

$\theta_{A_{\text{min}}} =$	-62.0°	0.0°	(3.25)
-----------------------------	--------	------	--------

$T =$	6.233333 ms	1.533333 ms	(3.26)
-------	-------------	-------------	--------

$T^{\text{S}} =$	6.6 ms	0.4 ms	(3.27)
------------------	--------	--------	--------

$T^{\text{R}} \text{ Rep. Rate} = 1/T =$	13.5 Hz	40.5 Hz	(3.28)
--	---------	---------	--------

Except as noted above for  $B_{\text{ratio}}$  studies, values assigned  $B_{\text{MLS}}$  and  $B_{\text{RCVR}}$  were, as follows:

$$B_{\text{MLS}} = B_{\text{RCVR}} = 1^\circ \quad (3.29)$$

Specification of the intensity of the interference was made using the parameter  $\rho$  defined in (3.3). As indicated above in connection with Figure 3.2, 65 samples were taken in each semiscan, i.e.

$$J = 130 \quad (3.30)$$

at the sampling rate

$$F_{\text{samp}} = 160 \text{ KHz} \quad (3.31)$$

with the 33rd and 98th samples occurring where the peaks of the direct path pulses were expected, based on  $\hat{\theta}(k|k-1)$ .

Estimation error was calculated in the expected manner, i.e.  $x-x$ , except for components associated with  $\beta$ ,  $\dot{\hat{w}}_{\text{sc}}$  (and  $\hat{w}_{\text{sc}}$  in the 6D LOE model). In these components, the differences in absolute values, e.g.  $|\beta| - |\hat{\beta}|$ , were used for error evaluation to accommodate the ambiguity in these variables.

## B. SIMULATION RUNS AND RESULTS

The results of nearly 50 runs are reported here in 23 plots and 23 tables. Table 3.1 summarizes the runs made--by type of run and CONTRL module, parameter values used, RCVR type used and figure numbers and table numbers in which the results appear. [In these discussions "OPTRVR" implies the use of modules OPTRVR and PLOPT (an abuse of terminology, perhaps), "SUBOPT" implies the use of modules OPTRVR and PLSUB.]

Figure 3.3 shows the computed RMS error ( $\theta$  component) versus  $\theta_{\text{sep}}$  for several S/N values for the OPTRVR,  $\rho=0.8$ . Figure 3.4 presents the

Table 3.1 Summary of Simulation Runs

TYPE OF RUN (CONTINUED)	S/N	P	$\theta_{SEP}$	$\beta$	F <sub>SC</sub>	IS <sub>ALS</sub>	B <sub>SEVR</sub>	FIGURE NOS. (3-)			TABLE NOS. (3-)		REMARKS
								OPTVR	SUBOPT	THDRVR	OPTVR	SUBOPT	
RMSE (B <sub>SEP</sub> ) (MULITH)	40	0.8	-3.75° to 1.575°	180°	0.135 Hz	1°	1°	3			2		
	40	0.5						4			3		
	30	0.8						3,5	5	5	4	10	
	30	0.5						4			5		
	20	0.5						3,6	6,8	6	6	11	16n-Adapt also
	20	0.5						4,7	7	7	7	12	
RMSE (B <sub>SEP</sub> ) (MULTI)	14	0.5											
	14	0.5						3			8		
RMSE (B <sub>SEP</sub> ) (MULTI)	20	0.8	-3.75° to 1.625°	180° only every 180° 20 values 180° only	0 Hz	1°	1°						
	30	0.8											
	30	0.5											
	20	0.5											
RMSE (F <sub>SC</sub> )	20	0.8	1.5°	-180°	0.35 Hz	3.16° to 1°	1° to 3.16°	9			13		
	30	0.8						9			14		
	30	0.5						9			15		
	20	0.5						9			16		
	30	0.8	1.5°	0°	0.1675 Hz 47.25° to 60.75°	1°	1°	10			17		
Interfer. Ang. (MULTI)	30	0.8						11			18	20	NO CONSTRAINTS WITH CONSTA, Tethers, N.C. Tethers, W.C.
	30	0.8						11	11		19	21	
	30	0.8						11			22		
	30	0.8						11			23		
	40	0.8	0.25°	45°	0.6 Hz	1°	1°	12					
	20	0.8	2°		2.5 Hz			13					
	20	0.8	3°		0.6 Hz			14					
Crossy, Multipath (TELETYPE)	20	0.8	2.5°		0.6 Hz			15					
	14	0.8	3°		0.6 Hz			16	22				
	40	0.8	0.5°		2.5 Hz			17					
	40	0.8	1°		0.6 Hz			18					
	40	0.8	1°	-168°	51.3 Hz			19					
	40	0.8	0.5	45°	0.6 Hz			20	23				
	40	0.8	0.5	45°	0.6 Hz			20	23				
Crossy, Multipath (TELETYPE)	20	0.8	-2.75° to 2.3°	-168°	51.3 Hz	1°	1°	24	24	24			
	20	0.8	-2.75° to 2.3°	-168°	51.3 Hz	1°	1°	25	25	25			

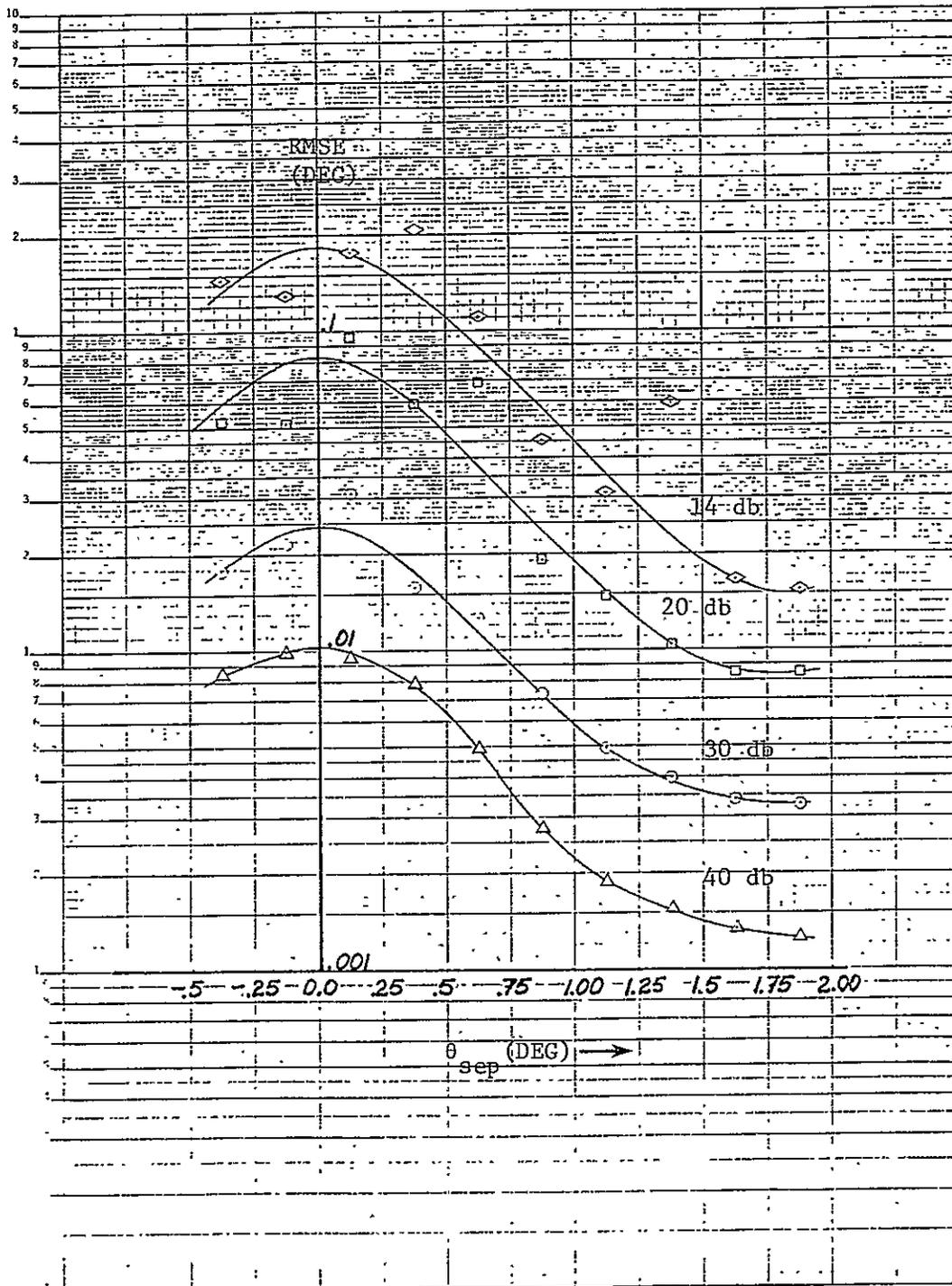


Figure 3.3 RMSE ( $\theta_{sep}$ ), OPTRVR,  $\rho=0.8$

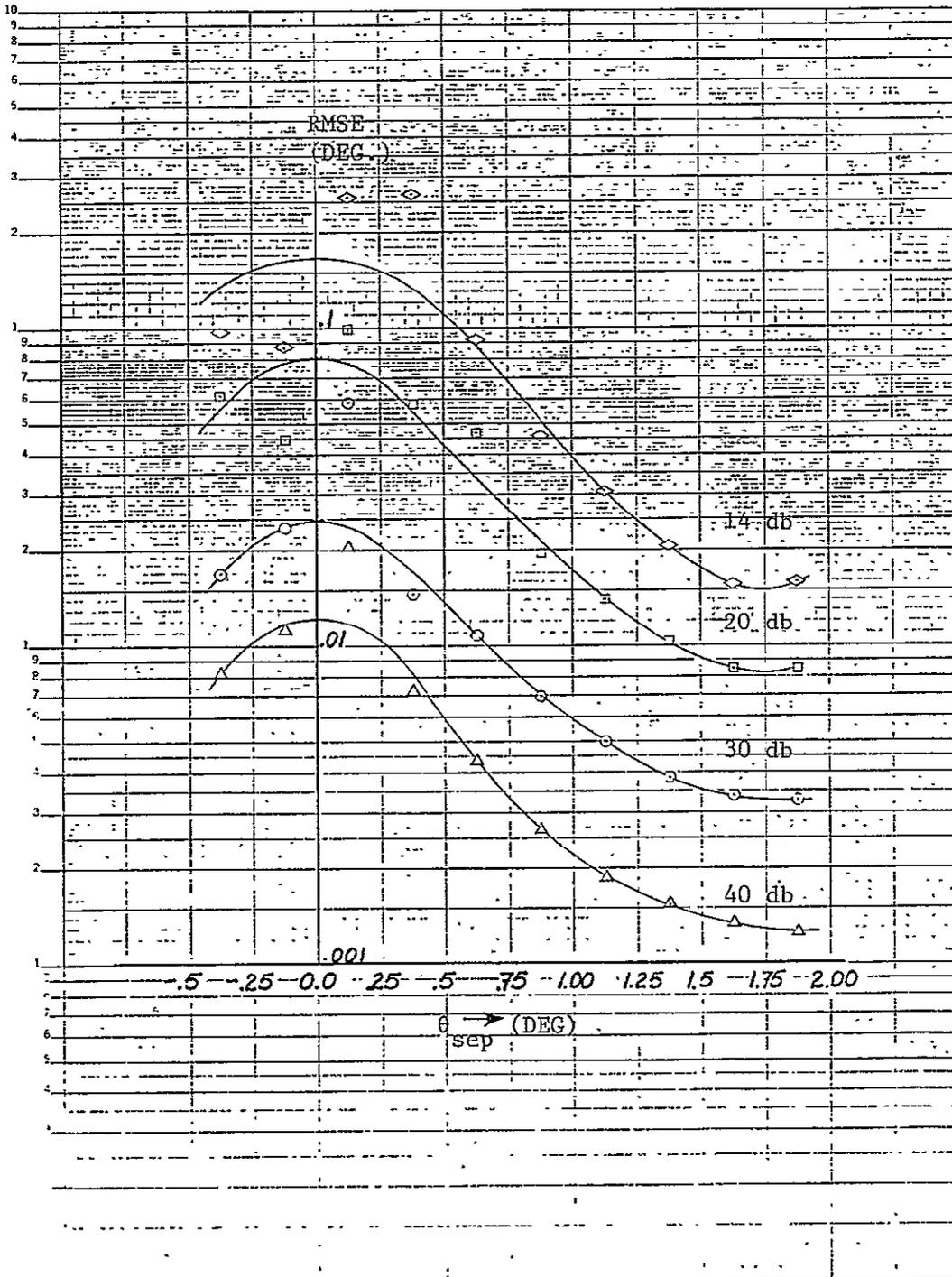


Figure 3.4 RMSE ( $\theta_{sep}$ ), OPTRVR,  $\rho=0.5$

same type of data for  $\rho=0.5$ . The scatter in the points for the lower S/N cases is due to noise; the apparent odd symmetry in the scatter about the origin is due to several causes:

- i. The lack of symmetry between the TO, FRO scans wrt the noise samples;
- ii. The effect of noise on the  $\beta$ -estimate (in one run, not included here,  $\hat{\beta}$  was tethered to the true value  $\beta$  and the calculated RMSE ( $\theta_{sep}$ )( $\theta$ -component) exhibited more nearly the expected even symmetry wrt  $\theta_{sep}$ .
- iii. The use of the same noise sample function for each data point.

Figures 3.5 thru 3.7 show comparisons of RMSE ( $\theta_{sep}$ ) for the receivers for various values of S/N and  $\rho$ . Figure 3.6, for example, shows that with S/N=20 db,  $\rho=0.8$ , the optimal design offers improvement by a factor up to about 30 over the threshold receiver. The suboptimal design, without tracking phase difference, shows improvement by a factor up to about 15 over the threshold receiver. The non-adaptive design, basically of optimal structure, but premised on interference-free reception, shows approximately equivalent performance as the threshold receiver.

Tables 3.2 thru 3.12 give the full results of the OPTRVR and SUBOPT simulation runs associated with Figures 3.3 thru 3.7 -- error statistics for each coordinate of the state estimate as a function of  $\theta_{sep}$ . One observation that can be made from this data is that the mean error at small separation angles becomes a more significant contributor to the RMSE as the S/N diminishes. This probably signals a diminishing validity of the LOE criterion (error being in a neighborhood of zero), due

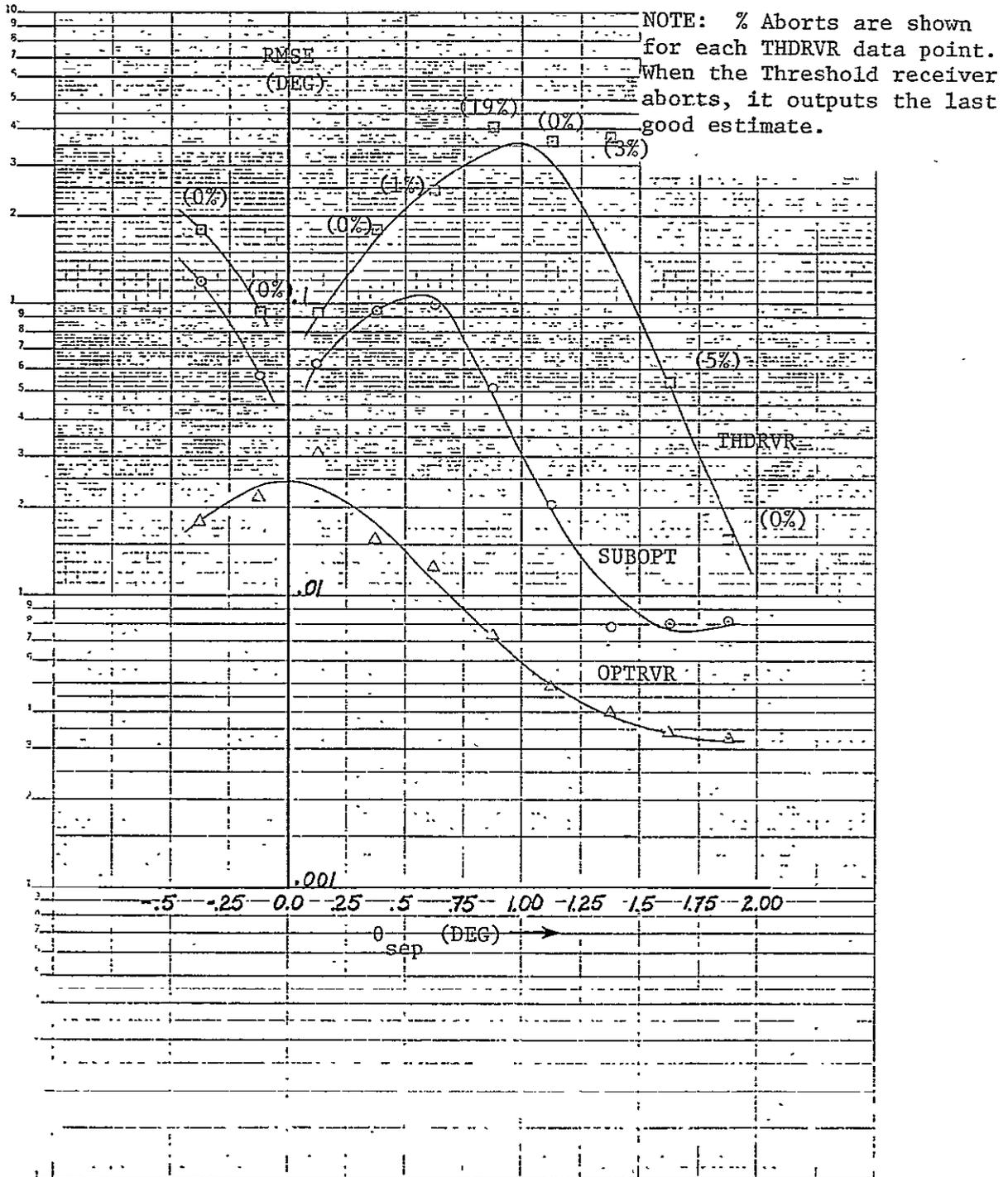


Figure 3.5 RMSE ( $\theta_{sep}$ ), comparison of receivers,  
 S/N=30 db,  $\rho=0.8$

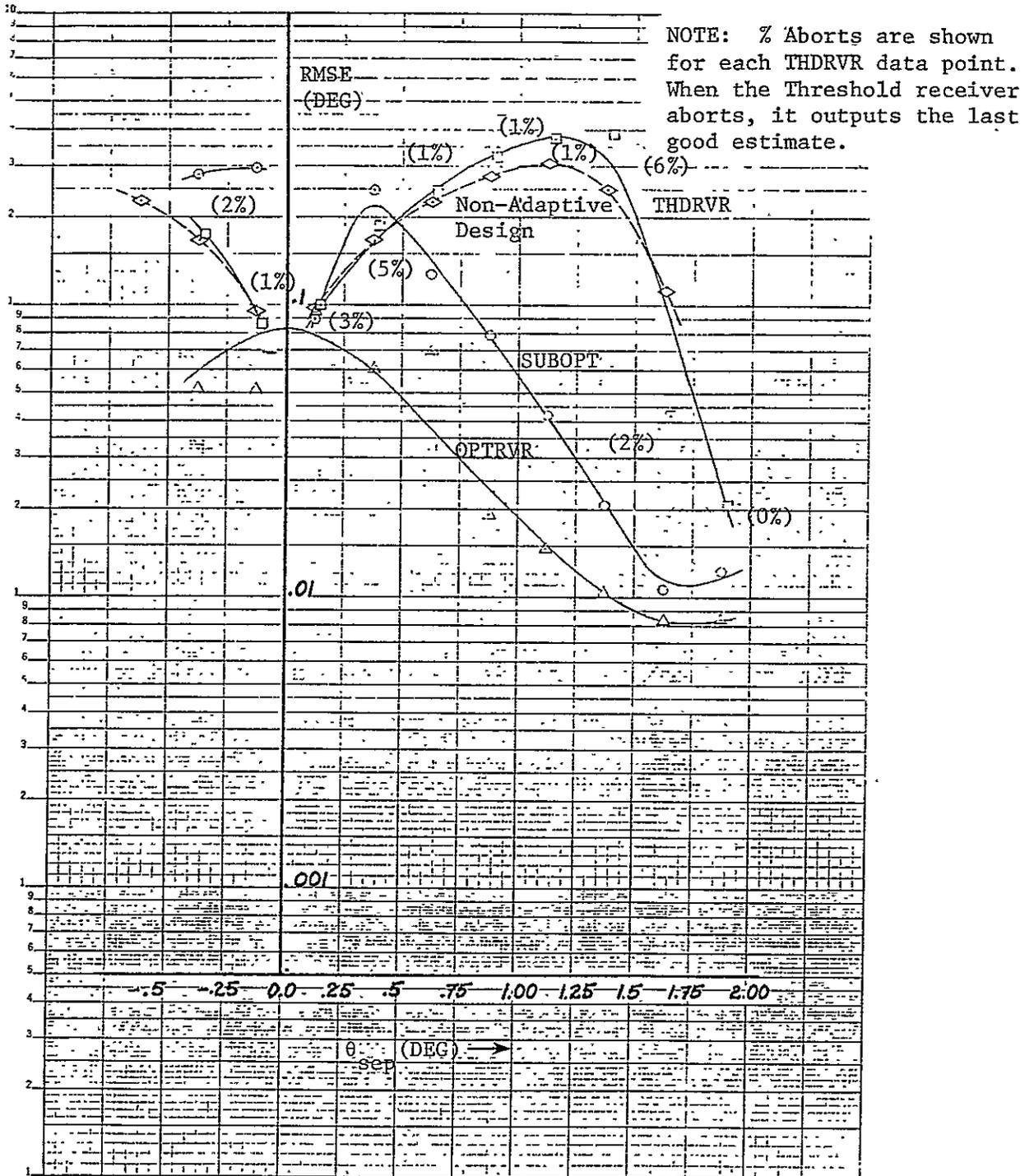


Figure 3.6 RMSE ( $\theta_{sep}$ ), comparison of receivers, S/N=20db,  $\rho=0.8$

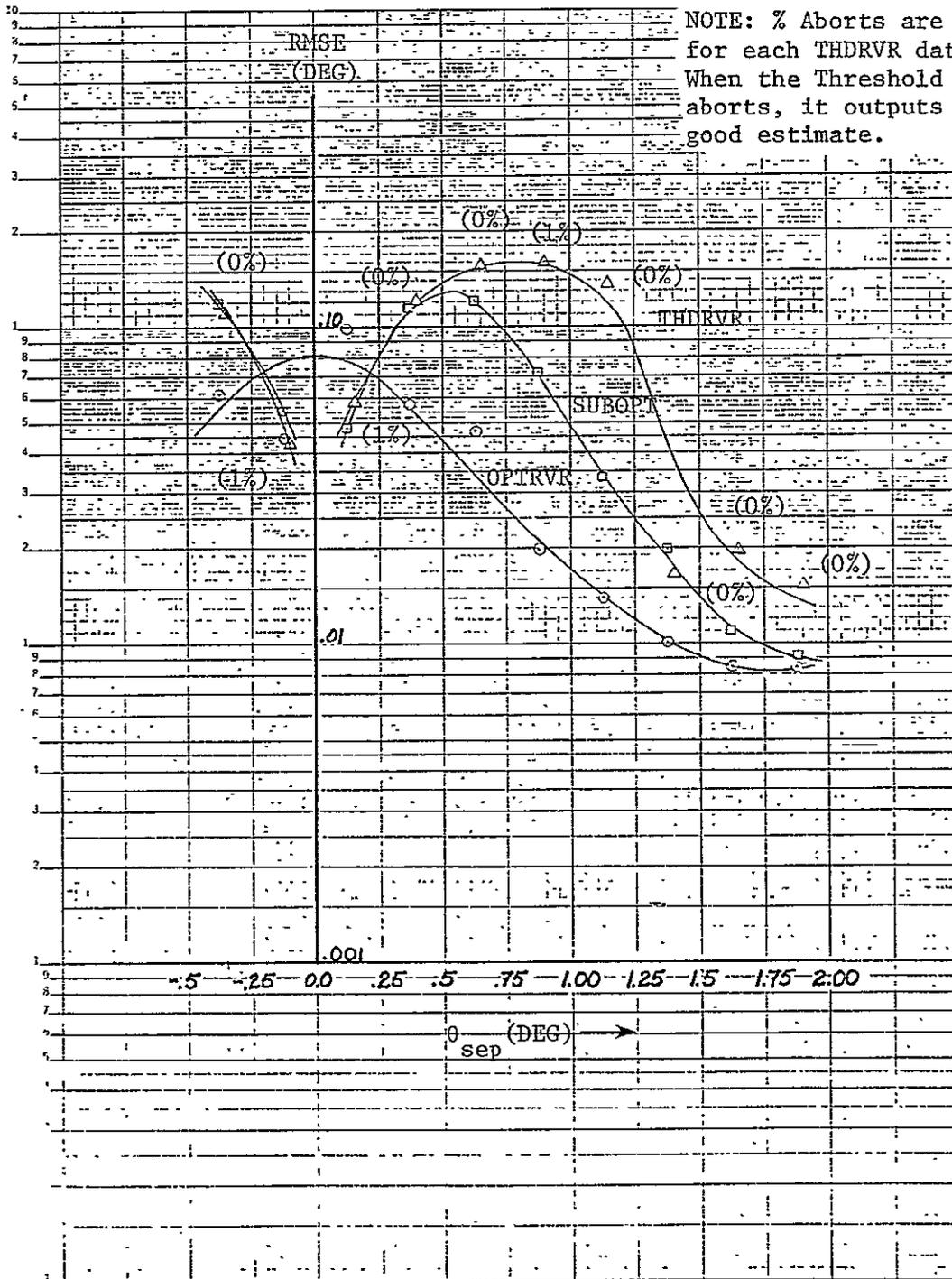


Figure 3.7 RMSE ( $\theta_{sep}$ ), comparison of receivers  
 $S/N = 20\text{db}$ ,  $\rho=0.5$

	QTY	THESEP	ALFA	THETA	THEDOT	ALFAR	THETAR	THRDOT	B	WSC
cMEAN:	-.375	-1.43	-.286E-02	.146E-02	-1.07	.260E-02	-.163E-02	-.272E-01	-.441E-01	
	-.125	-3.82	-.292E-02	.649E-03	12.1	-.164E-01	-.200E-02	.378E-01	-.233	
	.125	1.25	-.228E-02	-.102E-02	8.26	.105E-01	.144E-02	.603E-01	-.369	
	.375	-.581	.144E-02	.112E-02	-2.27	-.626E-02	-.218E-02	-.208E-01	-.154E-01	
	.625	-.280	.149E-02	.990E-03	-.609	-.339E-02	-.171E-02	-.186E-01	-.269E-02	
	.875	.257E-01	-.118E-04	.451E-04	-.774E-01	-.731E-03	-.414E-03	-.464E-02	-.176E-02	
	1.13	.254E-01	-.137E-03	-.145E-03	.562E-02	-.344E-04	-.929E-04	.231E-03	.190E-02	
	1.38	.215E-01	-.138E-03	-.493E-04	.107E-01	.127E-05	-.231E-03	.191E-02	-.566E-01	
	1.63	.150E-01	-.734E-04	-.134E-04	.120E-01	-.141E-05	-.310E-03	.123E-02	.930E-02	
	1.88	.103E-01	.586E-04	.938E-04	.144E-01	.304E-05	-.312E-03	.583E-03	-.413E-01	
	ERMS:	-.375	4.12	.846E-02	.236E-01	4.15	.113E-01	.295E-01	.678E-01	.438
-.125		12.7	.998E-02	.209E-01	15.0	.209E-01	.269E-01	.163	.857	
.125		10.9	.956E-02	.208E-01	13.9	.188E-01	.280E-01	.181	.948	
.375		3.67	.793E-02	.237E-01	3.87	.105E-01	.244E-01	.489E-01	.437	
.625		1.13	.492E-02	.223E-01	1.18	.638E-02	.212E-01	.407E-01	.348	
.875		.441	.276E-02	.172E-01	.456	.358E-02	.193E-01	.224E-01	.241	
1.13		.247	.188E-02	.152E-01	.232	.233E-02	.167E-01	.251E-01	.259	
1.38		.183	.154E-02	.148E-01	.184	.186E-02	.154E-01	.234E-01	.429	
1.63		.161	.132E-02	.142E-01	.174	.162E-02	.157E-01	.313E-01	.357	
1.88		.161	.125E-02	.137E-01	.177	.145E-02	.152E-01	.391E-01	.474	
tSTD:		-.375	3.87	.796E-02	.236E-01	4.01	.110E-01	.294E-01	.622E-01	.435
	-.125	12.1	.954E-02	.209E-01	8.79	.130E-01	.268E-01	.158	.825	
	.125	10.6	.928E-02	.207E-01	11.2	.157E-01	.280E-01	.171	.873	
	.375	3.63	.780E-02	.237E-01	3.13	.840E-02	.243E-01	.443E-01	.437	
	.625	1.10	.469E-02	.223E-01	1.01	.540E-02	.212E-01	.362E-01	.348	
	.875	.440	.276E-02	.172E-01	.449	.350E-02	.193E-01	.219E-01	.241	
	1.13	.246	.188E-02	.152E-01	.232	.232E-02	.167E-01	.251E-01	.259	
	1.38	.182	.153E-02	.148E-01	.184	.186E-02	.154E-01	.233E-01	.425	
	1.63	.161	.132E-02	.142E-01	.174	.162E-02	.157E-01	.312E-01	.357	
	1.88	.161	.124E-02	.137E-01	.177	.145E-02	.152E-01	.391E-01	.473	

Table 3.2 Error Statistics vs  $\theta_{sep}$ , OPTRVR, S/N=40db,  $\rho=0.8$

	QTY	THESEP	ALFA	THETA	THEDOT	ALFAR	THETAR	THRDDOT	B	WSC
E MEAN:	-.375	-.975	-.186E-02	.126E-02	-1.49	.528E-02	-.223E-02	-.319E-01	-.348E-01	
	-.125	-5.19	-.391E-02	.170E-02	13.9	-.348E-01	-.584E-02	.521E-03	-.256	
	.125	-5.23	.133E-02	-.686E-02	17.5	.555E-01	.163E-01	.592E-01	-1.61	
	.375	-.689	.153E-02	.137E-02	-2.22	-.950E-02	-.211E-02	-.274E-01	-.192E-01	
	.625	-.117	.829E-03	.894E-03	-.634	-.560E-02	-.223E-02	-.190E-01	.302E-02	
	.875	.310E-01	-.188E-04	.600E-04	-.649E-01	-.927E-03	-.723E-03	-.663E-02	-.936E-02	
	1.13	.154E-01	-.778E-04	-.563E-04	.934E-02	.208E-03	-.318E-03	.683E-03	-.635E-01	
	1.38	.202E-01	-.119E-03	-.163E-04	.706E-02	.578E-04	-.456E-03	.101E-02	-.746E-01	
	1.63	.156E-01	-.740E-04	.460E-04	.843E-02	.658E-04	-.503E-03	.107E-01	-.644E-01	
	1.88	.106E-01	.526E-04	.557E-04	.102E-01	.508E-04	-.455E-03	.374E-02	-.447E-01	
ERMS:	-.375	4.11	.820E-02	.221E-01	4.37	.183E-01	.354E-01	.796E-01	.482	
	-.125	14.5	.111E-01	.199E-01	16.6	.415E-01	.346E-01	.174	.818	
	.125	21.6	.202E-01	.278E-01	24.4	.831E-01	.669E-01	.513	4.82	
	.375	3.44	.721E-02	.218E-01	3.97	.169E-01	.305E-01	.585E-01	.430	
	.625	1.09	.434E-02	.199E-01	1.29	.110E-01	.270E-01	.389E-01	.306	
	.875	.404	.262E-02	.168E-01	.449	.548E-02	.218E-01	.315E-01	.311	
	1.13	.241	.187E-02	.153E-01	.243	.371E-02	.190E-01	.370E-01	.404	
	1.38	.180	.152E-02	.147E-01	.187	.281E-02	.179E-01	.292E-01	.512	
	1.63	.161	.132E-02	.142E-01	.177	.242E-02	.179E-01	.430E-01	.473	
	1.88	.160	.124E-02	.136E-01	.179	.219E-02	.176E-01	.414E-01	.522	
ESTD:	-.375	3.99	.799E-02	.221E-01	4.11	.176E-01	.353E-01	.729E-01	.481	
	-.125	13.6	.104E-01	.198E-01	9.19	.226E-01	.341E-01	.174	.777	
	.125	20.9	.202E-01	.269E-01	16.9	.618E-01	.649E-01	.510	4.54	
	.375	3.37	.705E-02	.217E-01	3.29	.139E-01	.304E-01	.516E-01	.429	
	.625	1.08	.426E-02	.199E-01	1.12	.951E-02	.269E-01	.339E-01	.306	
	.875	.402	.262E-02	.168E-01	.444	.540E-02	.218E-01	.308E-01	.311	
	1.13	.240	.186E-02	.153E-01	.243	.370E-02	.190E-01	.370E-01	.399	
	1.38	.179	.152E-02	.147E-01	.187	.281E-02	.179E-01	.292E-01	.506	
	1.63	.160	.132E-02	.142E-01	.177	.242E-02	.179E-01	.417E-01	.468	
	1.88	.160	.123E-02	.136E-01	.178	.219E-02	.176E-01	.413E-01	.520	

Table 3.3 Error Statistics vs  $\theta_{sep}$ , OPTRVR, S/N=40db,  $\rho=0.5$

	QTY	THESEP	ALFA	THETA	THEDOT	ALFAR	THETAR	THROOT	B	WSC	
EMEAN:	-.375	-1.29	-.740E-02	.943E-03	-.876	.446E-02	-.117E-02	-.695E-01	-.145		
	-.125	-4.30	-.855E-02	.388E-02	9.89	-.598E-01	-.931E-02	.441E-01	-.324		
	.125	6.01	-.225E-01	-.342E-02	-1.29	-.358E-02	.357E-02	.612E-01	-.214		
	.375	-.670	.364E-02	.991E-03	-1.40	-.114E-01	-.873E-03	-.569E-01	-.126		
	.625	-.163	.228E-02	.997E-03	-.368	-.534E-02	-.217E-02	-.391E-01	-.902E-02		
	.875	.346E-01	-.959E-03	.110E-02	-.302E-01	-.988E-04	-.181E-02	.119E-01	-.640E-01		
	1.13	.260E-01	-.932E-03	.499E-03	.264E-02	.407E-03	-.759E-03	.128E-01	-.133		
	1.38	.147E-01	-.666E-03	.499E-03	.466E-02	.535E-03	-.743E-03	.827E-02	-.158		
	1.63	.599E-02	-.361E-03	.461E-03	.232E-02	.425E-03	-.804E-03	.963E-02	-.222		
	1.88	-.263E-03	.727E-04	.204E-03	.111E-02	.191E-03	-.504E-03	.132E-01	-.259		
	ERMS:	-.375	2.79	.179E-01	.301E-01	2.82	.237E-01	.358E-01	.145	.647	
		-.125	9.81	.216E-01	.237E-01	11.3	.720E-01	.316E-01	.234	.864	
.125		7.00	.310E-01	.264E-01	5.70	.224E-01	.291E-01	.205	.715		
.375		2.32	.157E-01	.306E-01	2.60	.214E-01	.309E-01	.127	.675		
.625		.956	.125E-01	.322E-01	1.51	.166E-01	.310E-01	.136	.517		
.875		.378	.726E-02	.231E-01	.371	.845E-02	.241E-01	.633E-01	.510		
1.13		.228	.493E-02	.204E-01	.222	.617E-02	.218E-01	.596E-01	.505		
1.38		.175	.398E-02	.202E-01	.183	.457E-02	.203E-01	.541E-01	.715		
1.63		.159	.340E-02	.201E-01	.174	.411E-02	.207E-01	.740E-01	.776		
1.88		.160	.326E-02	.200E-01	.177	.370E-02	.202E-01	.110	.873		
ESTD:		-.375	2.47	.103E-01	.301E-01	2.68	.233E-01	.358E-01	.127	.631	
		-.125	8.82	.198E-01	.234E-01	5.55	.402E-01	.302E-01	.230	.801	
	.125	3.60	.213E-01	.262E-01	5.55	.221E-01	.289E-01	.196	.683		
	.375	2.23	.153E-01	.306E-01	2.19	.181E-01	.308E-01	.114	.663		
	.625	.942	.123E-01	.322E-01	.944	.157E-01	.309E-01	.985E-01	.517		
	.875	.376	.720E-02	.231E-01	.370	.845E-02	.240E-01	.622E-01	.500		
	1.13	.227	.484E-02	.204E-01	.222	.615E-02	.218E-01	.582E-01	.570		
	1.38	.174	.393E-02	.202E-01	.183	.453E-02	.200E-01	.535E-01	.697		
	1.63	.159	.338E-02	.201E-01	.174	.409E-02	.207E-01	.734E-01	.743		
	1.88	.160	.326E-02	.200E-01	.177	.370E-02	.202E-01	.114	.833		

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Table 3.4 Error Statistics vs  $\theta_{sep}$ , OPTRVR, S/N=30db,  $\rho=0.8$

NRUN \*

	QTY	THESEP	ALFA	THETA	THEDOT	ALFAR	THETAR	THRDOT	B	WSC
E MEAN:	-0.375	-0.483	-0.214E-02	.214E-02	-0.428	-0.250E-02	-0.733E-02	-0.638E-01	-0.143	
	-0.125	-1.06	.182E-02	.404E-02	7.02	-0.673E-01	-0.887E-02	.919E-01	-0.453	
	.125	5.74	-0.388E-01	-0.863E-02	-0.773	-0.522E-01	-0.350E-01	.183	-0.165	
	.375	.375	-0.247E-02	.252E-03	-1.43	-0.173E-01	.239E-02	-0.517E-01	-0.186	
	.625	.470E-01	-0.363E-03	.656E-03	-0.263	-0.445E-02	-0.949E-03	-0.192E-01	-0.749E-01	
	.875	.162E-01	-0.500E-03	.964E-03	.139E-01	.213E-02	-0.243E-02	.873E-02	-0.725E-01	
	1.13	.138E-01	-0.573E-03	.767E-03	-0.239E-02	.112E-02	-0.143E-02	.909E-02	-0.198	
	1.38	.143E-01	-0.617E-03	.482E-03	.219E-03	.158E-02	-0.109E-02	.932E-02	-0.185	
	1.63	.641E-02	-0.343E-03	.292E-03	-0.613E-02	.105E-02	-0.109E-02	.150E-01	-0.314	
	1.88	.711E-03	.383E-04	.128E-03	-0.801E-02	.293E-03	-0.293E-03	.230E-01	-0.300	
	ERMS:	-0.375	2.40	.169E-01	.277E-01	2.68	.420E-01	.474E-01	.174	.757
-0.125		7.58	.235E-01	.302E-01	7.75	.770E-01	.300E-01	.422	1.12	
.125		7.83	.582E-01	.331E-01	5.08	.110	.748E-01	.444	.876	
.375		2.05	.145E-01	.276E-01	2.55	.329E-01	.353E-01	.146	.733	
.625		.892	.108E-01	.290E-01	1.05	.275E-01	.415E-01	.100	.611	
.875		.359	.694E-02	.229E-01	.383	.141E-01	.292E-01	.585E-01	.560	
1.13		.223	.498E-02	.207E-01	.229	.994E-02	.255E-01	.632E-01	.756	
1.38		.173	.383E-02	.198E-01	.186	.697E-02	.228E-01	.619E-01	.747	
1.63		.158	.338E-02	.200E-01	.176	.625E-02	.239E-01	.939E-01	.915	
1.88		.159	.326E-02	.200E-01	.178	.550E-02	.226E-01	.999E-01	.926	
ESTD:		-0.375	2.35	.168E-01	.276E-01	2.65	.419E-01	.468E-01	.162	.743
	-0.125	7.51	.234E-01	.300E-01	3.30	.374E-01	.286E-01	.412	1.03	
	.125	5.32	.433E-01	.320E-01	5.02	.963E-01	.661E-01	.405	.860	
	.375	2.01	.143E-01	.276E-01	2.11	.280E-01	.353E-01	.137	.709	
	.625	.891	.108E-01	.290E-01	1.02	.271E-01	.415E-01	.986E-01	.606	
	.875	.359	.692E-02	.229E-01	.383	.140E-01	.291E-01	.578E-01	.555	
	1.13	.223	.495E-02	.207E-01	.229	.987E-02	.255E-01	.626E-01	.730	
	1.38	.172	.378E-02	.198E-01	.186	.679E-02	.228E-01	.612E-01	.724	
	1.63	.158	.337E-02	.200E-01	.176	.616E-02	.239E-01	.927E-01	.860	
	1.88	.159	.326E-02	.200E-01	.178	.549E-02	.226E-01	.972E-01	.876	

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Table 3.5 Error Statistics vs  $\theta_{sep}$ , OPTRVR, S/N=30db,  $\rho=0.5$

	QTY	THESEP	ALFA	THETA	THEDOT	ALFAR	THETAR	THRDOT	B	WSC
EMEAN:	-.375	.514	.269E-01	.108E-01	1.17	-.586E-01	-.197E-01	.727E-01	-.323	
	-.125	.256	.247E-01	.140E-01	3.47	-.100	-.200E-01	.220	-.499	
	.125	3.20	-.747E-01	-.174E-01	1.09	.738E-02	-.112E-02	.484	-.450	
	.375	1.41	-.451E-01	-.131E-01	.499	.262E-01	.177E-01	.119	-.325	
	.625	.662	-.459E-01	.204E-02	.841	.786E-01	.142E-02	.389	-.516	
	.875	.106	-.963E-02	.606E-03	.420E-01	.867E-02	.292E-03	.330E-01	-.296	
	1.13	.259E-01	-.543E-02	.229E-02	-.128E-01	.398E-02	-.231E-02	.332E-01	-.376	
	1.38	-.139E-02	-.318E-02	.165E-02	-.155E-01	.439E-02	-.127E-02	.364E-01	-.378	
	1.63	-.164E-01	-.150E-02	.102E-02	-.262E-01	.313E-02	-.461E-03	.485E-01	-.523	
	1.88	-.256E-01	.324E-03	.706E-03	-.316E-01	.504E-04	-.428E-03	.638E-01	-.610	
ERMS:	-.375	1.62	.521E-01	.330E-01	1.70	.783E-01	.385E-01	.312	.964	
	-.125	3.55	.515E-01	.345E-01	3.83	.119	.342E-01	.612	1.16	
	.125	3.86	.958E-01	.433E-01	2.63	.366E-01	.385E-01	.595	1.09	
	.375	1.76	.596E-01	.375E-01	1.51	.603E-01	.416E-01	.245	.835	
	.625	1.05	.686E-01	.683E-01	1.25	.113	.964E-01	.647	1.13	
	.875	.307	.191E-01	.259E-01	.320	.247E-01	.364E-01	.170	.926	
	1.13	.212	.148E-01	.281E-01	.219	.192E-01	.344E-01	.139	.869	
	1.38	.165	.102E-01	.256E-01	.181	.126E-01	.260E-01	.118	.821	
	1.63	.156	.848E-02	.257E-01	.175	.111E-01	.281E-01	.146	1.12	
	1.88	.159	.845E-02	.267E-01	.177	.968E-02	.269E-01	.228	1.27	
ESTD:	-.375	1.54	.446E-01	.312E-01	1.23	.519E-01	.331E-01	.303	.908	
	-.125	3.54	.451E-01	.315E-01	1.62	.635E-01	.277E-01	.571	1.04	
	.125	2.16	.600E-01	.396E-01	2.40	.358E-01	.385E-01	.346	.992	
	.375	1.04	.391E-01	.351E-01	1.43	.543E-01	.377E-01	.215	.769	
	.625	.812	.510E-01	.683E-01	.924	.805E-01	.964E-01	.517	1.00	
	.875	.288	.165E-01	.259E-01	.318	.231E-01	.364E-01	.167	.878	
	1.13	.211	.137E-01	.280E-01	.219	.188E-01	.343E-01	.135	.783	
	1.38	.165	.974E-02	.255E-01	.181	.118E-01	.260E-01	.112	.729	
	1.63	.155	.835E-02	.257E-01	.173	.106E-01	.281E-01	.137	.994	
	1.88	.157	.844E-02	.267E-01	.174	.968E-02	.269E-01	.219	1.12	

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Table 3.6 Error Statistics vs  $\theta_{sep}$ , OPTKVR, S/N=20db,  $\rho=0.8$

	QTY	THESEP	ALFA	THETA	THEDDT	ALFAR	THETAR	THRDOT	B	WSC
E MEAN:	-.375	.746	.373E-01	.173E-01	1.23	-.137	-.478E-01	.175	-.501	
	-.125	.777	.291E-01	.107E-01	2.06	-.724E-01	-.285E-02	.323	-.468	
	.125	2.80	-.670E-01	-.159E-01	.739	-.143E-01	-.224E-01	.922	-.304	
	.375	1.19	-.405E-01	-.588E-02	.164	.194E-01	.189E-01	.182	-.535	
	.625	.369E-01	-.148E-01	-.169E-02	1.16	.163	.164E-01	.352	-.586	
	.875	.125	-.120E-01	-.143E-02	.133	.327E-01	.440E-02	.131	-.318	
	1.13	.203E-01	-.469E-02	.251E-02	-.226E-01	.868E-02	-.277E-02	.379E-01	-.433	
	1.38	-.381E-02	-.269E-02	.151E-02	-.332E-01	.744E-02	-.245E-02	.506E-01	-.495	
	1.63	-.157E-01	-.146E-02	.247E-03	-.479E-01	.520E-02	-.809E-03	.717E-01	-.659	
	1.88	-.242E-01	.179E-03	.698E-03	-.502E-01	.408E-03	-.321E-03	.784E-01	-.667	
ERMS:	-.375	1.58	.619E-01	.409E-01	1.79	.191	.665E-01	.423	1.19	
	-.125	2.41	.446E-01	.308E-01	2.45	.938E-01	.365E-01	.644	1.04	
	.125	4.05	.987E-01	.477E-01	1.30	.864E-01	.621E-01	1.32	.920	
	.375	1.68	.577E-01	.430E-01	1.34	.769E-01	.547E-01	.312	1.18	
	.625	1.00	.465E-01	.564E-01	1.30	.186	.897E-01	.504	1.19	
	.875	.280	.195E-01	.284E-01	.309	.429E-01	.360E-01	.215	.863	
	1.13	.201	.140E-01	.267E-01	.221	.315E-01	.442E-01	.148	.908	
	1.38	.166	.101E-01	.254E-01	.187	.215E-01	.338E-01	.151	1.07	
	1.63	.155	.842E-02	.252E-01	.182	.164E-01	.321E-01	.195	1.33	
	1.88	.158	.842E-02	.264E-01	.182	.154E-01	.325E-01	.277	1.27	
ESTD:	-.375	1.39	.495E-01	.371E-01	1.30	.133	.462E-01	.385	1.08	
	-.125	2.28	.337E-01	.289E-01	1.33	.596E-01	.364E-01	.557	.934	
	.125	2.93	.724E-01	.450E-01	1.07	.852E-01	.579E-01	.942	.869	
	.375	1.19	.411E-01	.426E-01	1.33	.744E-01	.514E-01	.254	1.05	
	.625	1.00	.441E-01	.564E-01	.580	.888E-01	.882E-01	.361	1.03	
	.875	.250	.154E-01	.283E-01	.279	.278E-01	.357E-01	.171	.802	
	1.13	.260	.132E-01	.266E-01	.220	.303E-01	.441E-01	.144	.798	
	1.38	.166	.974E-02	.253E-01	.184	.201E-01	.337E-01	.142	.945	
	1.63	.155	.830E-02	.252E-01	.176	.155E-01	.321E-01	.181	1.15	
	1.88	.156	.842E-02	.264E-01	.175	.154E-01	.325E-01	.266	1.08	

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Table 3.7 Error Statistics vs  $\theta_{sep}$ , OPTRVR, S/N=20db,  $\rho=0.5$

	QTY	THESEP	ALFA	THETA	THEDDT	ALFAR	THETAR	THRDDT	B	WSC
EMEAN:	-.375	.935	.112	.292E-01	.716	-.126	-.501E-01	.460	-.757	
	-.125	1.23	.937E-01	.300E-01	1.27	-.118	-.329E-01	.735	-.630	
	.125	1.03	-.102	-.403E-01	1.73	.637E-01	.130E-01	1.03	-.511	
	.375	.957	-.130	-.347E-01	.720	.989E-01	.588E-01	.458	-.862	
	.625	.422	-.675E-01	-.601E-02	.540	.103	.173E-01	.414	-.686	
	.875	.153	-.305E-01	-.395E-02	.716E-01	.284E-01	.606E-02	.118	-.603	
	1.13	-.416E-02	-.929E-02	.357E-02	-.317E-01	.108E-01	-.362E-02	.628E-01	-.661	
	1.38	.283E-01	-.170E-01	-.114E-01	.130E-01	.216E-01	.175E-01	-.349E-01	-35.9	
	1.63	-.412E-01	-.268E-02	.247E-02	-.548E-01	.744E-02	-.277E-02	.107	-.698	
	1.88	-.502E-01	.183E-02	.547E-03	-.590E-01	.567E-03	-.657E-04	.108	-1.05	
	EPMS:	-.375	1.30	.146	.575E-01	1.17	.178	.844E-01	.658	1.56
-.125		1.76	.129	.555E-01	1.76	.167	.585E-01	.950	1.56	
.125		2.19	.177	.784E-01	1.93	.849E-01	.407E-01	1.36	1.06	
.375		1.66	.208	.102	1.39	.199	.137	.816	1.66	
.625		.836	.110	.786E-01	.784	.141	.888E-01	.691	1.24	
.875		.293	.451E-01	.389E-01	.263	.482E-01	.468E-01	.263	1.26	
1.13		.201	.310E-01	.416E-01	.203	.373E-01	.479E-01	.253	1.26	
1.38		.202	.590E-01	.644E-01	.204	.820E-01	.845E-01	.794	36.6	
1.63		.154	.164E-01	.321E-01	.176	.218E-01	.357E-01	.286	1.30	
1.88		.157	.152E-01	.327E-01	.176	.175E-01	.335E-01	.419	1.83	
ESTD:		-.375	.900	.932E-01	.495E-01	.930	.126	.679E-01	.471	1.37
	-.125	1.27	.889E-01	.466E-01	1.23	.118	.483E-01	.602	1.43	
	.125	1.93	.145	.672E-01	.864	.561E-01	.386E-01	.885	.926	
	.375	1.35	.163	.963E-01	1.19	.173	.124	.675	1.42	
	.625	.722	.864E-01	.784E-01	.568	.963E-01	.871E-01	.554	1.04	
	.875	.249	.332E-01	.387E-01	.253	.389E-01	.464E-01	.235	1.11	
	1.13	.201	.296E-01	.414E-01	.200	.356E-01	.477E-01	.245	1.08	
	1.38	.200	.565E-01	.633E-01	.203	.791E-01	.827E-01	.793	7.06	
	1.63	.148	.161E-01	.320E-01	.167	.205E-01	.356E-01	.265	1.10	
	1.88	.149	.151E-01	.327E-01	.166	.175E-01	.335E-01	.405	1.50	

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Table 3.8 Error Statistics vs  $\theta_{sep}$ , OPTRVR, S/N=14 db,  $\rho=0.8$

	QTY	THESEP	ALFA	THETA	THEDOT	ALFAR	THETAR	THROOT	B	WSC
E MEAN:	-.375	.674	.756E-01	.226E-01	.444	-.147	-.514E-01	.358	-.807	
	-.125	.803	.570E-01	.141E-01	.872	-.813E-01	-.140E-01	.838	-.210	
	.125	1.50	-.158	-.577E-01	.248	-.168E-01	-.195E-01	.716	-1.28	
	.375	1.64	-.168	-.431E-01	-.149	-.136	-.561E-01	.784	-.863	
	.625	.221	-.468E-01	-.112E-01	.611	.179	.440E-01	.477	-.889	
	.875	.128	-.293E-01	-.138E-02	.104	.661E-01	.837E-02	.225	-.824	
	1.13	.801E-02	-.126E-01	.323E-02	-.198E-01	.280E-01	-.214E-03	.125	-.760	
	1.38	-.299E-01	-.493E-02	.305E-02	-.579E-01	.125E-01	-.581E-02	.124	-.666	
	1.63	-.429E-01	-.113E-02	.121E-02	-.651E-01	.894E-02	-.294E-02	.108	-.815	
	1.88	-.465E-01	.200E-02	.323E-03	-.668E-01	.313E-02	-.696E-03	.124	-1.03	
E RMS:	-.375	.966	.975E-01	.506E-01	.906	.228	.864E-01	.630	1.46	
	-.125	1.36	.872E-01	.386E-01	1.17	.130	.505E-01	1.21	.848	
	.125	2.23	.258	.985E-01	.939	.152	.815E-01	.990	3.48	
	.375	2.19	.263	.116	.747	.231	.990E-01	1.21	1.48	
	.625	.788	.917E-01	.764E-01	.751	.220	.108	.723	1.51	
	.875	.284	.456E-01	.443E-01	.302	.103	.757E-01	.431	1.43	
	1.13	.194	.305E-01	.382E-01	.210	.683E-01	.697E-01	.314	1.29	
	1.38	.161	.206E-01	.335E-01	.165	.493E-01	.569E-01	.309	1.23	
	1.63	.154	.155E-01	.310E-01	.186	.323E-01	.423E-01	.346	1.39	
	1.88	.157	.159E-01	.333E-01	.186	.298E-01	.433E-01	.522	1.76	
E STD:	-.375	.642	.615E-01	.453E-01	.789	.175	.695E-01	.518	1.21	
	-.125	1.10	.660E-01	.359E-01	.774	.101	.486E-01	.869	.821	
	.125	1.65	.203	.798E-01	.905	.151	.791E-01	.684	3.23	
	.375	1.46	.201	.168	.732	.187	.816E-01	.915	1.20	
	.625	.756	.789E-01	.776E-01	.436	.128	.986E-01	.542	1.22	
	.875	.253	.350E-01	.443E-01	.283	.790E-01	.752E-01	.368	1.16	
	1.13	.194	.277E-01	.381E-01	.209	.623E-01	.697E-01	.288	1.04	
	1.38	.158	.200E-01	.333E-01	.176	.477E-01	.566E-01	.283	1.04	
	1.63	.148	.155E-01	.309E-01	.174	.311E-01	.422E-01	.329	1.13	
	1.88	.149	.157E-01	.333E-01	.173	.296E-01	.433E-01	.508	1.43	

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Table 3.9 Error Statistics vs  $\theta_{sep}$ , OPTRVR, S/N=14db,  $\rho=0.5$

	QTY	THESEP	ALFA	THETA	THEDOT	ALFAR	THETAR	THRODT
EMEAN:	-.375	-11.9	-.101	.234E-02	3.80	-.305E-01	-.918E-02	
	-.125	-9.05	-.375E-01	.955E-02	17.1	-.971E-01	-.417E-01	
	.125	-9.53	.271E-01	-.175E-01	13.7	.415E-01	.704E-01	
	.375	-9.52	.795E-01	-.793E-03	5.77	.531E-01	.447E-02	
	.625	-2.01	.192E-01	-.178E-01	.767	.402E-01	.188E-01	
	.875	.310	-.332E-02	-.399E-02	.328	.748E-02	.611E-02	
	1.13	.222	-.486E-02	-.100E-02	.225	.673E-02	.576E-03	
	1.38	.630E-01	-.113E-02	.233E-03	.570E-01	.200E-02	-.632E-03	
	1.63	-.299E-01	.753E-03	.201E-03	.375E-02	-.642E-03	-.617E-03	
	1.88	-.166E-01	.911E-03	.149E-03	-.529E-02	-.114E-02	-.391E-03	
ERMS:	-.375	16.0	.119	.200	5.01	.863E-01	.189	
	-.125	15.1	.562E-01	.100E+00	18.3	.201	.246	
	.125	16.9	.624E-01	.119	16.4	.153	.255	
	.375	11.5	.945E-01	.762E-01	6.66	.102	.146	
	.625	6.51	.990E-01	.749E-01	4.97	.116	.108	
	.875	1.76	.518E-01	.595E-01	2.23	.789E-01	.861E-01	
	1.13	.705	.206E-01	.522E-01	.686	.227E-01	.497E-01	
	1.38	.372	.787E-02	.236E-01	.408	.972E-02	.276E-01	
	1.63	.271	.801E-02	.193E-01	.310	.116E-01	.271E-01	
	1.88	.191	.820E-02	.184E-01	.199	.108E-01	.224E-01	
ESTD:	-.375	10.7	.629E-01	.200	3.26	.807E-01	.188	
	-.125	12.1	.419E-01	.995E-01	6.64	.176	.242	
	.125	14.0	.563E-01	.118	8.95	.147	.245	
	.375	6.54	.510E-01	.762E-01	3.32	.873E-01	.146	
	.625	6.19	.971E-01	.728E-01	4.91	.109	.107	
	.875	1.73	.517E-01	.594E-01	2.20	.785E-01	.859E-01	
	1.13	.669	.200E-01	.522E-01	.648	.217E-01	.497E-01	
	1.38	.366	.779E-02	.236E-01	.404	.952E-02	.276E-01	
	1.63	.269	.798E-02	.193E-01	.310	.116E-01	.271E-01	
	1.88	.190	.815E-02	.184E-01	.199	.108E-01	.224E-01	

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Table 3.10 Error Statistics vs  $\theta_{sep}$ , SUBOPT, S/N=30db,  $\rho=0.8$

	QTY	THESEP	ALFA	THETA	THEDOT	ALFAR	THETAR	THRDOT
E MEAN:	-.375	4.73	.254	.389E-01	-.802	-.332E-01	-.755E-01	
	-.125	5.61	-.280	-.464E-01	-.568	.198	.421E-01	
	.125	-1.55	-.207E-03	-.301E-01	7.03	.577	.102	
	.375	4.06	-.215	-.338E-01	-.105	.488E-01	.734E-01	
	.625	-.260	-.182E-01	-.286E-01	2.81	.233	.377E-01	
	.875	.432	-.392E-01	-.112E-01	.879	.905E-01	.157E-01	
	1.13	.244	-.240E-01	-.259E-02	.228	.326E-01	.416E-02	
	1.38	.388E-01	-.686E-02	.618E-03	.300E-01	.106E-01	.114E-03	
	1.63	-.291E-01	.990E-03	.129E-02	-.308E-01	.209E-02	-.950E-03	
	1.88	-.341E-01	.289E-02	.985E-03	-.429E-01	-.273E-02	-.964E-03	
ERMS:	-.375	4.81	.280	.169	3.52	.200	.181	
	-.125	5.94	.294	.109	3.75	.210	.749E-01	
	.125	5.45	.895E-01	.969E-01	7.07	.640	.171	
	.375	4.29	.248	.149	2.94	.188	.178	
	.625	2.43	.128	.114	2.89	.249	.106	
	.875	.920	.791E-01	.666E-01	1.00	.116	.862E-01	
	1.13	.349	.416E-01	.391E-01	.356	.623E-01	.605E-01	
	1.38	.178	.202E-01	.305E-01	.195	.273E-01	.369E-01	
	1.63	.174	.108E-01	.267E-01	.213	.143E-01	.318E-01	
	1.88	.171	.121E-01	.263E-01	.203	.171E-01	.289E-01	
ESTD:	-.375	.879	.117	.165	3.43	.197	.164	
	-.125	1.93	.908E-01	.986E-01	3.70	.711E-01	.619E-01	
	.125	5.23	.895E-01	.921E-01	.762	.276	.137	
	.375	1.38	.123	.145	2.94	.182	.163	
	.625	2.42	.127	.110	.661	.879E-01	.985E-01	
	.875	.813	.667E-01	.657E-01	.478	.732E-01	.847E-01	
	1.13	.250	.340E-01	.390E-01	.274	.531E-01	.604E-01	
	1.38	.174	.190E-01	.305E-01	.193	.252E-01	.369E-01	
	1.63	.171	.107E-01	.267E-01	.211	.141E-01	.318E-01	
	1.88	.167	.117E-01	.263E-01	.198	.169E-01	.289E-01	

Table 3.11 Error Statistics vs  $\theta_{sep}$ , SUBOPT, S/N=20db,  $\rho=0.8$

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	QTY	THESEP	ALFA	THETA	THEDOT	ALFAR	THETAR	THRODT
EMEAN:	-.375	-.743	-.848E-02	.260E-01	3.90	-.811	-.165	
	-.125	-.712	.118E-02	.155E-01	4.43	-.245	-.361E-01	
	.125	-.690	.247E-02	-.122E-01	4.48	.380	.781E-01	
	.375	-.743	.137E-01	-.245E-01	3.99	.842	.152	
	.625	-.547	.118E-01	-.194E-01	2.58	.418	.659E-01	
	.875	.150E-01	-.108E-01	-.868E-02	1.00	.178	.308E-01	
	1.13	.112	-.135E-01	-.199E-02	.252	.653E-01	.111E-01	
	1.38	.179E-01	-.462E-02	.781E-03	.258E-01	.216E-01	.161E-02	
	1.63	-.294E-01	.197E-02	.103E-02	-.432E-01	.648E-02	-.168E-02	
	1.88	-.292E-01	.290E-02	.953E-03	-.622E-01	-.281E-02	-.302E-02	
	ERMS:	-.375	3.05	.119	.100	3.93	.868	.271
-.125		3.43	.553E-01	.552E-01	4.45	.305	.849E-01	
.125		3.44	.480E-01	.491E-01	4.50	.444	.102	
.375		3.05	.114	.963E-01	4.02	.901	.274	
.625		2.28	.121	.100	2.63	.422	.143	
.875		.948	.718E-01	.635E-01	1.03	.201	.123	
1.13		.336	.372E-01	.367E-01	.352	.106	.964E-01	
1.38		.170	.196E-01	.286E-01	.192	.500E-01	.569E-01	
1.63		.154	.112E-01	.264E-01	.215	.210E-01	.369E-01	
1.88		.156	.917E-02	.254E-01	.210	.285E-01	.370E-01	
ESTD:		-.375	2.96	.119	.966E-01	.497	.311	.215
	-.125	3.35	.553E-01	.530E-01	.431	.182	.769E-01	
	.125	3.37	.479E-01	.476E-01	.409	.229	.656E-01	
	.375	2.96	.113	.931E-01	.512	.322	.228	
	.625	2.21	.120	.983E-01	.495	.561E-01	.127	
	.875	.947	.710E-01	.629E-01	.258	.937E-01	.120	
	1.13	.317	.346E-01	.366E-01	.246	.841E-01	.958E-01	
	1.38	.169	.191E-01	.286E-01	.190	.454E-01	.568E-01	
	1.63	.151	.110E-01	.264E-01	.210	.200E-01	.369E-01	
	1.88	.153	.870E-02	.254E-01	.201	.284E-01	.369E-01	

Table 3.12 Error Statistics vs  $\theta_{sep}$ , SUBOPT, S/N=20db,  $\rho=0.5$

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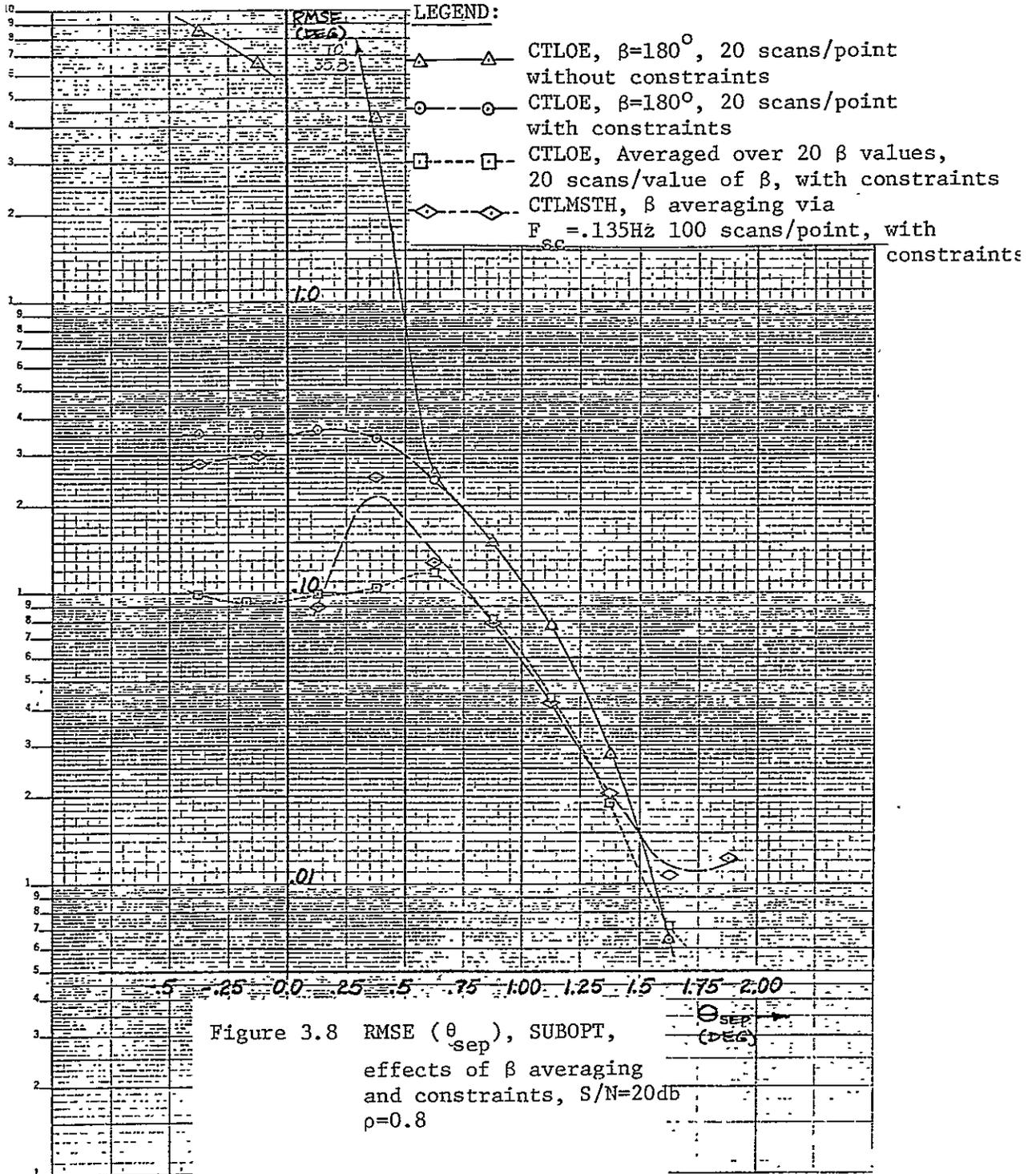
in part to the relatively large value of GQGT (8.8) used,  $\approx(2.7\text{r/s})^2$  (in AZ). This value was selected to facilitate tracking a varying  $\omega_{sc}$  under the condition that it is changing at the maximum rate at which it can be tracked in the present structure, based on angle function rep. rate considerations (recall (3.135)) (i.e. without extracting its derivative and integrating (as in the 6D LOE design)). This was a practical consideration that penalized some the performance in the steady state (when  $\omega_{sc}$  was not changing).

Figure 3.8 summarizes a study of the SUBOPT receiver; it shows that

1. In the worst cast wrt  $\beta$ , i.e.  $\beta=180^\circ$ , the constraints on the estimate helped for small  $\theta_{sep}$  and did not influence the performance for larger  $\theta_{sep}$ ; and that
2. Averaging over noise effects and  $\beta$  simultaneously by using a small non-zero  $\dot{\beta}$  ( $=\omega_{sc}$ ) to sweep  $\beta$  over a  $2\pi$  interval seems adequate generally, with some error possibly arising for small  $\theta_{sep}$ . This method of averaging over  $\beta$  was used generally.

Figure 3.9 and Tables 3.13 thru 3.16 following show the effects of a form of mismatch between the receiver design and its signal environment, specifically a mismatch in the presumed and actual values of the transmitting antenna beamwidth, (given the antenna selectivity functions,  $p$ ,  $p_{MLS}$ , are otherwise identical). Much can be said about the necessity of tuning a high-performance signal processor to its signal environment, but the manifest RMSE sensitivity here to  $B_{RCVR}/B_{MLS}$  is nevertheless striking. The tables provide some insight, for example

K&E SEMI LOGARITHMIC 46 6010  
 A CYCLES X 70 DIVISIONS MADE IN U.S.A.  
 KEUFFEL & ESSER CO.



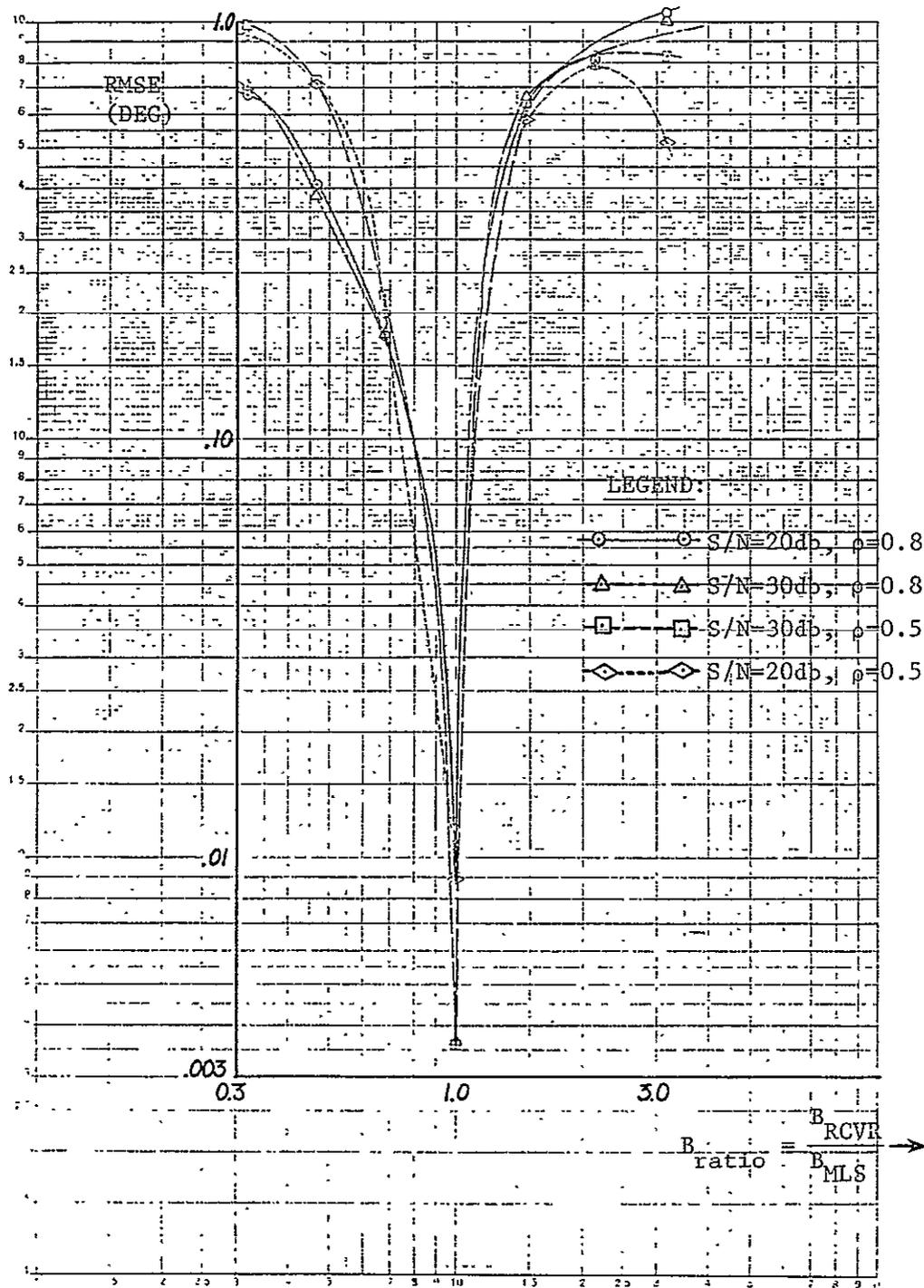


Figure 3.9 RMSE ( $B_{RCVR}/B_{MLS}$ ), OPTRV,  $\theta_{sep}=1.5^\circ$

NRUN = 1

QTY	BRATIO	ALFA	THETA	THEDOT	ALFAR	THETAR	THPDOOT	B	WSC
EMEAN:	.316	-3.75	-.553	-.130	-4.76	.721E-01	.335E-01	.734E-01	-20.6
	.464	-2.47	-.345	-.599E-01	-3.20	.252	.101	.598	-16.6
	.681	-1.27	-.151	-.221E-01	-1.67	.906E-01	.362E-01	.662	-5.05
	1.00	-.961E-02	-.234E-02	.127E-02	-.210E-01	.392E-02	-.110E-02	.390E-01	-.456
	1.47	-49.2	.636	.646E-01	-49.5	-.687	-.748E-01	-1.43	.728
	2.15	-6.92	.798	.774E-01	-1.24	-.422	-.118	-1.11	-.289
	3.16	.587	1.13	.170	4.94	1.11	.189	-1.14	-2.90
ERMS:	.316	5.87	.676	.463	7.39	.208	.352	1.18	24.1
	.464	3.49	.409	.337	4.82	.474	.452	1.08	19.7
	.681	1.48	.177	.114	2.16	.225	.196	1.06	6.29
	1.00	.158	.915E-02	.257E-01	.177	.114E-01	.261E-01	.124	.931
	1.47	55.2	.638	.171	55.5	.689	.186	1.68	.746
	2.15	8.25	.817	.235	4.35	.492	.156	1.81	1.33
	3.16	1.79	1.16	.317	5.15	1.48	.421	1.67	3.51
ESTD:	.316	4.51	.389	.445	5.65	.196	.351	1.18	12.5
	.464	2.47	.218	.331	3.60	.402	.441	.896	10.6
	.681	.768	.922E-01	.112	1.38	.206	.193	.823	3.75
	1.00	.158	.885E-02	.257E-01	.176	.107E-01	.261E-01	.118	.812
	1.47	24.8	.467E-01	.158	25.0	.538E-01	.171	.883	.161
	2.15	4.48	.174	.222	4.17	.252	.101	1.42	1.29
	3.16	1.69	.266	.267	1.43	.979	.376	1.21	1.98

Table 3.13 Error Statistics vs B<sub>ratio</sub>, OPTRVR, S/N=20db, ρ=0.8, θ<sub>sep</sub>=1.5°

	QTY	BRATIO	ALFA	THETA	THEDOT	ALFAR	THETAR	THRDOT	B	WSC
E	MEAN:	.316	-11.8	-.589	-.557E-01	-14.8	.296	.122	-.126	-18.9
		.464	-7.96	-.331	-.149E-02	-10.4	.232	.922E-02	.631E-01	-20.7
		.681	-4.04	-.158	-.157E-01	-5.24	.103	.181E-01	.774	-9.57
		1.00	.122E-01	-.634E-03	.493E-03	.398E-02	.654E-03	-.904E-03	.108E-01	-.173
		1.47	-294.	.661	.179E-01	-295.	-.715	-.193E-01	-1.46	.787
		2.15	-13.8	.770	.444E-01	6.62	-.546	-.142	-.960	-1.66
		3.16	14.8	-.110	.237	-.672E-01	-4.71	-.327	.150	-17.0
E	ERMS:	.316	18.5	.703	.510	22.9	.454	.515	1.26	22.1
		.464	11.0	.384	.358	15.0	.442	.437	1.15	24.1
		.681	4.68	.178	.116	6.71	.210	.194	1.08	10.5
		1.00	.164	.368E-02	.203E-01	.177	.440E-02	.206E-01	.608E-01	.712
		1.47	371.	.663	.101	372.	.716	.106	1.70	.793
		2.15	22.8	.781	.240	18.3	.588	.240	1.87	3.08
		3.16	32.5	1.06	.589	36.0	6.41	.626	1.29	22.4
E	ESTD:	.316	14.2	.364	.507	17.5	.345	.500	1.26	11.6
		.464	7.65	.193	.358	10.9	.377	.437	1.15	12.4
		.681	2.35	.806E-01	.115	4.19	.183	.194	.749	4.39
		1.00	.164	.362E-02	.203E-01	.177	.435E-02	.206E-01	.598E-01	.690
		1.47	226.	.391E-01	.990E-01	227.	.414E-01	.105	.859	.988E-01
		2.15	18.1	.135	.236	17.1	.218	.194	1.61	2.59
		3.16	28.9	1.05	.539	36.0	4.35	.534	1.28	14.5

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Table 3.14 Error Statistics vs  $B_{ratio}$ , OPTRVR, S/N=30db,  $\rho=0.8$ ,  $\theta_{sep}=1.5^\circ$

	QTY	BRATIO	ALFA	THETA	THEDOT	ALFAR	THETAR	THRDOT	B	WSC
EMEAN:	.316		-7.05	-.856	-.136	-23.0	-.555	-.881E-01	.777E-02	-19.5
	.464		-1.93	-.654	-.917E-01	-16.5	-.561	-.624E-01	.474	-17.6
	.681		-2.33	-.267	-.198E-01	-6.15	-.129E-02	.294E-01	.815	-8.59
	1.00		.107E-01	-.524E-03	.486E-03	-.125E-02	.154E-02	-.130E-02	.142E-01	-.212
	1.47		-349.	.595	.746E-01	-351.	-.741	-.813E-01	-1.46	-.112
	2.15		-128.	.834	.481E-01	-121.	-.535	-.799E-01	-1.55	.373
	3.16		10.7	.772	.442E-01	11.0	1.35	-.286E-01	-.384	-14.1
ERMS:	.316		12.7	.983	.543	24.9	.757	.557	1.23	23.7
	.464		7.70	.729	.429	17.9	.697	.503	1.37	21.2
	.681		2.41	.210	.846E-01	8.05	.301	.301	1.15	9.29
	1.00		.163	.360E-02	.200E-01	.179	.678E-02	.239E-01	.750E-01	.793
	1.47		434.	.608	.210	436.	.763	.243	1.74	4.28
	2.15		146.	.837	.163	141.	.544	.155	1.80	.780
	3.16		11.4	.828	.442	11.5	2.22	.590	1.31	18.3
ESTD:	.316		10.6	.483	.525	9.60	.515	.550	1.23	13.5
	.464		7.45	.322	.419	6.85	.414	.500	1.28	11.9
	.681		.626	.326E-01	.823E-01	5.19	.301	.299	.816	3.55
	1.00		.163	.356E-02	.200E-01	.179	.660E-02	.239E-01	.737E-01	.764
	1.47		258.	.127	.197	259.	.180	.229	.947	4.28
	2.15		71.1	.691E-01	.156	71.6	.984E-01	.133	.917	.685
	3.16		3.94	.300	.440	3.22	1.76	.589	1.25	11.7

Table 3.15 Error Statistics vs B<sub>ratio</sub>, OPTRVR, S/N=30db, ρ =0.5, θ<sub>sep</sub> =1.5°

QTY	BRATIO	ALFA	THETA	THEDOT	ALFAR	THETAR	THRDOT	B	WSC
EMEAN:	.316	-2.26	-.817	-.187	-7.08	-.522	-.167	.205	-18.0
	.464	-.699	-.634	-.162	-5.25	-.577	-.144	.945	-9.36
	.681	-.756	-.197	-.156E-01	-2.03	-.302E-01	.697E-01	.915	-4.57
	1.00	-.108E-01	-.198E-02	.981E-03	-.403E-01	.681E-02	-.163E-02	.575E-01	-.531
	1.47	-38.0	.581	.612E-01	-38.8	-.729	-.892E-01	-1.44	.683
	2.15	-9.21	.774	.889E-01	-7.39	-.368	-.666E-01	-1.42	-.144
	3.16	3.39	.485	.377E-01	4.16	-.965	-.249	-.608E-01	-29.2
ERMS:	.316	4.00	.933	.542	7.75	.717	.566	1.34	21.4
	.464	2.47	.709	.397	5.73	.704	.479	1.37	11.0
	.681	.603	.200	.727E-01	2.63	.312	.254	1.27	6.87
	1.00	.158	.891E-02	.250E-01	.182	.177E-01	.307E-01	.165	1.19
	1.47	41.5	.584	.150	42.3	.733	.204	1.70	.730
	2.15	10.7	.784	.214	9.15	.398	.841E-01	1.75	1.15
	3.16	3.70	.515	.302	4.33	1.09	.291	1.34	29.9
ESTD:	.316	3.30	.451	.508	3.17	.492	.541	1.32	11.6
	.464	2.36	.318	.362	2.29	.404	.456	.996	5.84
	.681	.264	.345E-01	.710E-01	1.68	.311	.245	.884	5.14
	1.00	.158	.869E-02	.250E-01	.177	.163E-01	.307E-01	.155	1.07
	1.47	16.7	.569E-01	.137	16.9	.728E-01	.183	.899	.257
	2.15	5.38	.121	.194	5.40	.150	.521E-01	1.01	1.14
	3.16	1.50	.171	.300	1.22	.500	.152	1.34	6.61

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Table 3.16 Error Statistics vs B<sub>ratio</sub>, OPTRVR, S/N=20db, ρ=0.5, θ<sub>sep</sub>=1.5°

1. An estimation of  $\alpha$  and  $\alpha_R$  by integration of the signal, such as in done here, may be especially vulnerable to uncertainties in other parameters that affect signal energy, such as beam width; and
2. The errors in the  $\theta$  and  $\theta_R$  components are heavily biased, when  $\beta_{\text{ratio}} \neq 1$ , indicating loss of LOE validity, specifically with decoupling of estimates of errors.

Perhaps peak detection, maybe in conjunction with an integration approach, would provide more robust estimates of  $\alpha$  and  $\alpha_R$ . Smaller errors in the  $\theta$  and  $\theta_R$  components should then result, but the residual errors might be reduced further by having the nominal beam width at each air terminal coded and transmitted in the MLS preamble. Additional robustness and possibly some simplification advantages might result from use in the receiver of a  $p(\cdot)$  function which doesn't model exactly any particular transmitting antenna selectivity function but does produce a best fit in some sense over the class of transmitting antenna selectivity functions to which the receiver is exposed. This is a problem area that needs further study.

Figure 3.10 presents an RMSE ( $F_{sc}$ ) study for scalloping rates in the first lobe of the rep. rate sampled signal spectrum, i.e.

$$F_{sc} \leq \frac{13.5}{2} \text{ Hz} = 6.75 \text{ Hz} \quad (3.32)$$

All the values of  $F_{sc}$  for which the RMSE was calculated, except 0.0 Hz, cause  $\beta$  to integrate an integral number of times around a  $2\pi$  interval as the run progresses hence the results should be independent of the initial  $\beta$ . The RMSE value at 0.0 Hz is probably dependent upon the

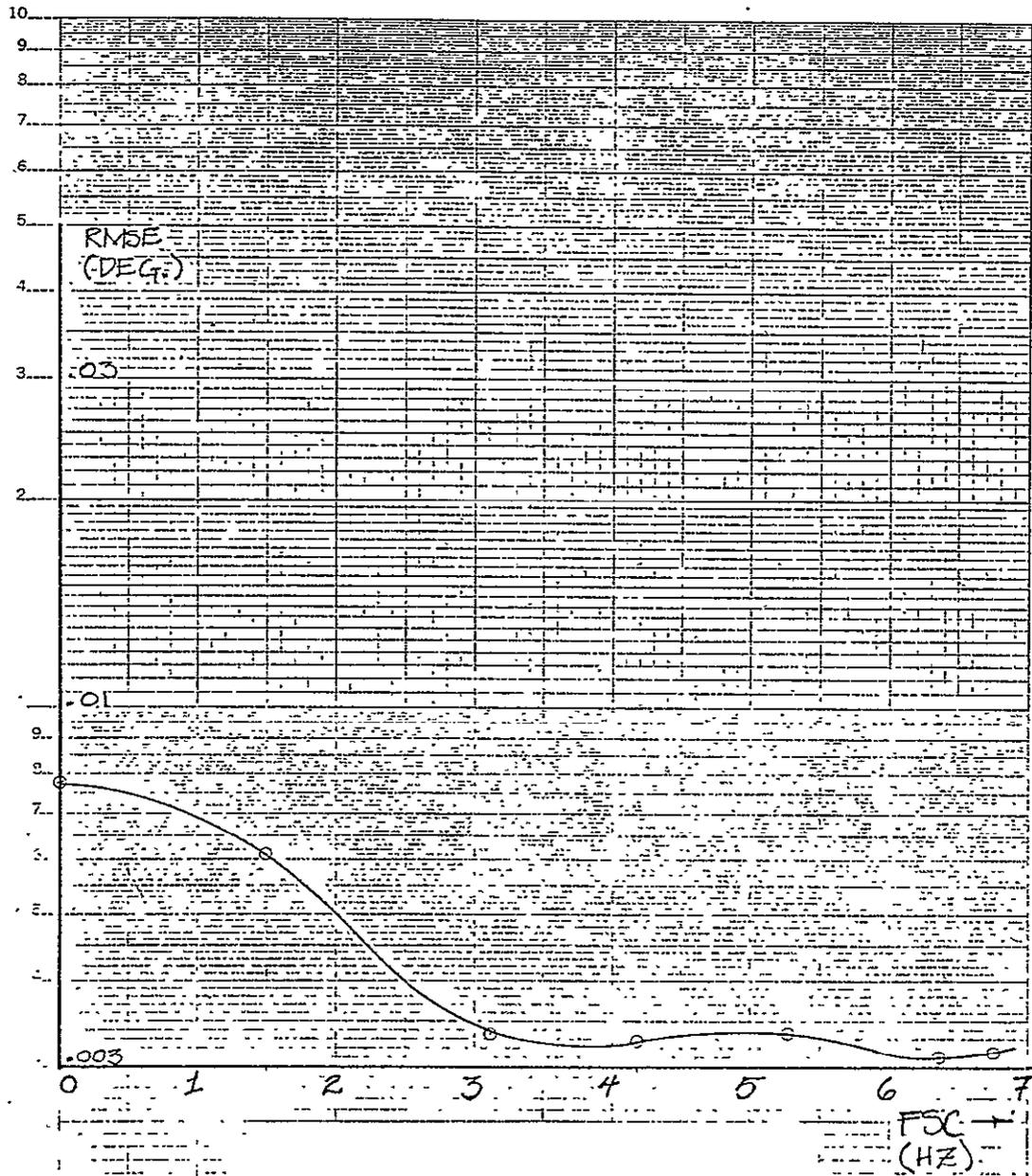


Figure 3.10 RMSE ( $F_{sc}$ ), OPTRVR,  
 1st Lobe, S/N=30db,  
 $\rho=0.8$ ,  $\theta_{sep}=1.5^\circ$

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value of  $\beta$ ,  $0^\circ$ , during the run. Table 3.17 shows all computed statistics of all error components for this simulation run.

Figure 3.11 and the associated Tables 3.18 thru 3.23 present the results of several statistical error studies versus  $F_{sc}$  with the latter ranging on the fifth lobe of the rep. rate sampled signal spectrum, i.e.

$$47.25 \leq F_{sc} \leq 60.75 \text{ Hz.} \quad (3.23)$$

These studies indicate

1. The OPTRVR without constraints is definitely superior to the same receiver with constraints (Tables 3.18 and 3.19).
2. The SUBOPT performance is the same with and without constraints (Tables 3.20 and 3.21).
3. The OPTRVR with tethered estimates  $\beta$ ,  $\hat{w}_{sc}$  as shown performs the same with and without constraints (Tables 3.22 and 3.23).
4. Items (2) and (3) above suggest it is the constraint on  $\hat{w}_{sc}$  only that degrades the OPTRVR performance referenced in item (1) above.

Relaxing the constraint on  $\hat{w}_{sc}$  in OPTRVR may be beneficial here without harming the performance for low  $F_{sc}$  cases, but there is no certainty of that without more tests. The benefits of the constraints generally were established in Figure 3.8 but that involved the SUBOPT receiver where there was no  $w_{sc}$  estimate. Clearly, relaxing the  $\hat{w}_{sc}$  constraint in the OPTRVR will not in any sense enable tracking of  $w_{sc}$  above half the rep. rate, since the 5D LOE does not exploit individually (for  $w_{sc}$ -information) the TO and FRO scan pulses (as the 6D LOE would do). Further study at other values of S/N,  $\rho$  and  $\theta_{sep}$  are needed here.

	QTY	FSC	ALFA	THETA	THEDOT	ALFAR	THETAR	THRDOT	B	WSC
	E MEAN:	0.	.296E-02	-.148E-03	.587E-03	-.272E-02	.123E-03	-.892E-03	-.153	-1.13
		1.49	.118E-01	-.549E-03	-.186E-03	.404E-03	.517E-03	-.133E-02	.133E-01	-.878E-02
		3.11	.132E-01	-.328E-03	-.816E-03	.104E-01	.105E-02	-.972E-03	.128E-01	-.286E-01
		4.19	.147E-01	-.470E-03	-.290E-03	.428E-02	.517E-03	-.364E-03	.378E-02	-.325E-01
		5.27	.932E-02	-.247E-03	-.624E-03	.737E-02	.581E-03	-.453E-03	.183E-01	-.224E-01
		6.35	.810E-02	-.240E-03	-.530E-03	.714E-02	.722E-03	-.588E-03	.865E-02	-.270E-01
		6.75	.749E-03	-.378E-04	.227E-03	.150E-02	.617E-03	-.110E-02	-.114E-01	.825
	ERMS:	0.	.167	.377E-02	.210E-01	.179	.423E-02	.207E-01	.186	1.42
		1.49	.161	.361E-02	.203E-01	.174	.412E-02	.195E-01	.588E-01	.834
		3.11	.168	.334E-02	.194E-01	.177	.412E-02	.200E-01	.469E-01	.781
		4.19	.164	.327E-02	.193E-01	.177	.417E-02	.210E-01	.552E-01	.792
		5.27	.167	.337E-02	.197E-01	.181	.414E-02	.207E-01	.523E-01	.813
		6.35	.165	.310E-02	.192E-01	.171	.403E-02	.196E-01	.500E-01	.797
		6.75	.159	.315E-02	.195E-01	.180	.368E-02	.189E-01	.103	1.09
	ESTD:	0.	.167	.377E-02	.210E-01	.179	.423E-02	.207E-01	.105	.873
		1.49	.161	.357E-02	.203E-01	.174	.409E-02	.195E-01	.572E-01	.834
		3.11	.168	.333E-02	.194E-01	.177	.399E-02	.200E-01	.451E-01	.781
		4.19	.164	.324E-02	.193E-01	.177	.414E-02	.210E-01	.550E-01	.791
		5.27	.166	.336E-02	.197E-01	.181	.410E-02	.207E-01	.490E-01	.813
		6.35	.165	.309E-02	.192E-01	.170	.397E-02	.196E-01	.492E-01	.796
		6.75	.159	.315E-02	.195E-01	.180	.363E-02	.189E-01	.103	.713

Table 3.17 Error Statistics vs  $F_{se}$ , OPTVR, 1st Lobe S/N=30db,  $\rho=0.8$ ,  $\theta_{sep}=1.5^\circ$

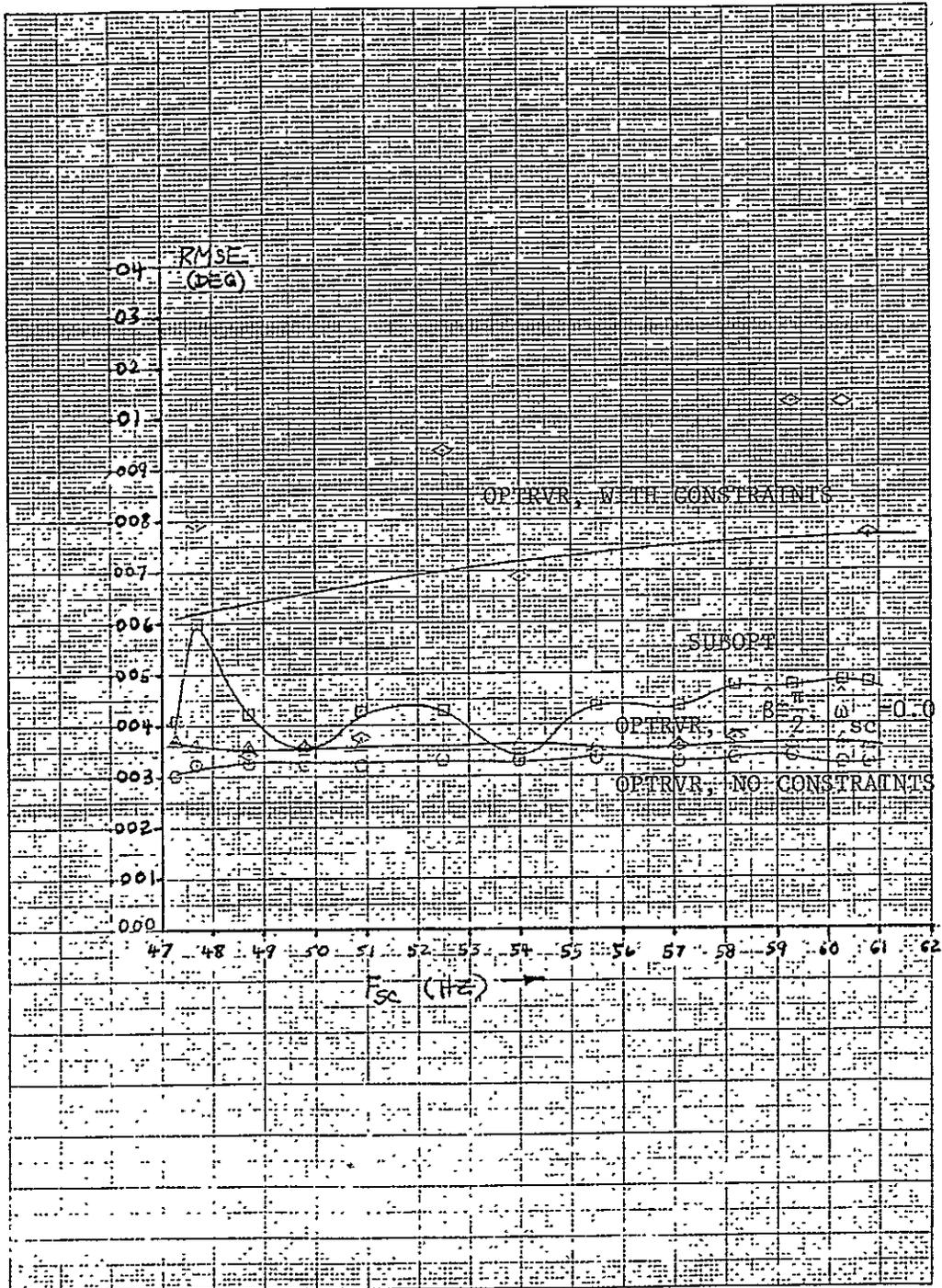


Figure 3.11 RMSE ( $F_{sc}$ ), comparison of receivers and effects of constraints, 5th lobe, S/N=30db,  $\rho=0.8$ ,  $\theta_{sep}=1.5^\circ$

NRUN = 6

	CTY	FSC	ALFA	THETA	THEDOT	ALFAR	THETAR	THRDDOT	B	WSC
	MEAN:	47.3	.274E-02	.106E-03	.542E-04	.857E-02	.700E-03	-.268E-03	-.739E-02	.201E-01
		47.7	.706E-02	-.455E-04	.168E-03	.235E-03	-.681E-04	-.885E-03	-.245E-02	-.360E-02
		48.7	.534E-02	.118E-03	.203E-03	.561E-02	.414E-03	-.466E-03	-.103E-03	.377E-01
		49.8	.114E-01	-.510E-03	.112E-03	.450E-03	-.489E-04	-.107E-02	-.635E-02	.712E-03
		50.9	.943E-02	-.201E-03	.240E-03	.702E-02	.646E-03	-.103E-02	-.599E-02	-.341E-01
		52.9	.807E-02	-.285E-03	.281E-03	.112E-02	.208E-03	-.748E-03	-.209E-02	.163E-01
		54.0	.540E-02	-.190E-03	.287E-03	.263E-02	.462E-04	-.419E-03	-.215E-01	-.536E-02
		55.5	.733E-02	-.211E-03	.439E-03	.552E-02	.298E-03	-.386E-03	.275E-02	.258E-01
		57.1	.642E-02	-.956E-04	.294E-03	.454E-02	.347E-03	-.218E-03	.360E-03	.335E-02
		58.2	.632E-02	-.554E-04	.606E-03	-.250E-04	-.163E-04	-.143E-02	-.376E-02	.462E-01
		59.3	.532E-02	.140E-03	.194E-03	.837E-03	.233E-04	-.839E-03	-.114E-02	.602E-02
		60.3	.459E-02	.180E-04	.101E-03	.292E-02	.214E-03	.292E-04	.505E-02	-.572E-03
		60.8	.290E-02	.175E-03	.126E-03	.442E-02	.317E-03	-.454E-03	.929E-03	.674E-02
	ERMS:	47.3	.165	.301E-02	.192E-01	.176	.368E-02	.194E-01	.647E-01	.935
		47.7	.158	.326E-02	.205E-01	.175	.393E-02	.204E-01	.474E-01	.698
		48.7	.162	.325E-02	.199E-01	.174	.369E-02	.202E-01	.591E-01	.972
		49.3	.163	.322E-02	.198E-01	.174	.379E-02	.205E-01	.528E-01	.885
		50.9	.160	.320E-02	.202E-01	.178	.367E-02	.188E-01	.671E-01	1.01
		52.9	.162	.330E-02	.204E-01	.178	.388E-02	.203E-01	.410E-01	.681
		54.0	.162	.328E-02	.204E-01	.174	.374E-02	.199E-01	.390E-01	.670
16		55.5	.161	.333E-02	.203E-01	.179	.372E-02	.194E-01	.470E-01	.753
		57.1	.161	.326E-02	.202E-01	.176	.378E-02	.201E-01	.446E-01	.720
		58.2	.165	.331E-02	.203E-01	.173	.390E-02	.200E-01	.412E-01	.653
		59.3	.160	.337E-02	.205E-01	.176	.375E-02	.201E-01	.411E-01	.703
		60.3	.164	.324E-02	.200E-01	.178	.391E-02	.201E-01	.581E-01	.859
		60.8	.165	.324E-02	.198E-01	.178	.375E-02	.196E-01	.347E-01	.615
	USTD:	47.3	.165	.301E-02	.192E-01	.175	.361E-02	.194E-01	.643E-01	.934
		47.7	.158	.326E-02	.205E-01	.175	.393E-02	.204E-01	.473E-01	.698
		48.7	.162	.325E-02	.199E-01	.174	.367E-02	.202E-01	.591E-01	.971
		49.3	.163	.321E-02	.198E-01	.174	.379E-02	.205E-01	.525E-01	.885
		50.9	.159	.319E-02	.202E-01	.178	.361E-02	.187E-01	.669E-01	1.01
		52.9	.162	.328E-02	.204E-01	.176	.388E-02	.203E-01	.409E-01	.681
		54.0	.162	.327E-02	.204E-01	.174	.374E-02	.199E-01	.230E-01	.670
		55.5	.161	.332E-02	.203E-01	.178	.370E-02	.193E-01	.469E-01	.753
		57.1	.161	.326E-02	.202E-01	.176	.377E-02	.201E-01	.446E-01	.720
		58.2	.165	.331E-02	.203E-01	.173	.390E-02	.200E-01	.410E-01	.681
		59.3	.160	.336E-02	.205E-01	.176	.375E-02	.201E-01	.410E-01	.703
		60.3	.164	.324E-02	.200E-01	.178	.390E-02	.201E-01	.579E-01	.859
		60.8	.165	.324E-02	.198E-01	.178	.374E-02	.196E-01	.347E-01	.615

Table 3.18 Error Statistics vs  $F_{sc}$ , OPTRVR, 5th Lobe, S/N=30db,  $\rho=0.8$ ,  $\theta_{sep}=1.5^\circ$ , NO CONSTRAINTS

	QTY	FSC	ALFA	THETA	THEDOT	ALFAR	THETAR	THRDOT	B	WSC
MEAN:	47.3		.176	-.223E-02	.116E-02	.282	.477E-02	-.169E-02	-.179	295.
	47.7		.144	-.268E-02	.479E-02	.220	.478E-02	-.617E-02	-.118	293.
	48.7		.100	-.710E-03	.918E-03	.163	.199E-02	-.126E-02	-.113	304.
	49.8		.102	-.839E-03	.847E-03	.170	.229E-02	-.819E-03	-.106	311.
	50.9		.110	-.126E-02	.199E-02	.179	.295E-02	-.253E-02	-.104	317.
	52.5		.152	-.490E-02	-.473E-04	.224	.827E-02	-.915E-03	-.560E-02	290.
	54.0		.100	.142E-03	.616E-02	.152	.567E-03	-.777E-02	-1.59	299.
	55.5		.922E-01	-.103E-02	.428E-04	.147	.238E-02	-.318E-03	-.940E-01	347.
	57.1		.115	-.132E-02	.122E-02	.182	.288E-02	-.239E-02	-.109	356.
	58.2		.105	-.792E-03	.753E-03	.174	.219E-02	-.969E-03	-.111	363.
	59.3		.192	-.805E-02	.910E-03	.249	.132E-01	-.201E-02	-.601E-02	333.
	60.3		.202	-.753E-02	.607E-02	.296	.123E-01	-.761E-02	-.111	355.
	60.8		.139	-.531E-02	.644E-02	.192	.789E-02	-.623E-02	-.115	343.
ERMS:	47.3		.242	.404E-02	.196E-01	.334	.642E-02	.208E-01	1.66	295.
	47.7		.239	.795E-02	.424E-01	.304	.108E-01	.464E-01	.973	293.
	48.7		.205	.341E-02	.196E-01	.249	.469E-02	.206E-01	.947	304.
	49.8		.205	.355E-02	.200E-01	.278	.491E-02	.212E-01	.935	311.
	50.9		.210	.370E-02	.210E-01	.279	.513E-02	.205E-01	.927	317.
	52.5		.277	.934E-02	.477E-01	.341	.128E-01	.554E-01	.977	290.
	54.0		.236	.687E-02	.492E-01	.269	.935E-02	.567E-01	1.59	299.
	55.5		.201	.345E-02	.192E-01	.238	.483E-02	.206E-01	.877	347.
	57.1		.206	.359E-02	.196E-01	.267	.500E-02	.204E-01	.851	356.
	58.2		.217	.372E-02	.206E-01	.256	.462E-02	.197E-01	.807	363.
	59.3		.288	.128E-01	.518E-01	.369	.182E-01	.579E-01	.802	333.
	60.3		.329	.126E-01	.613E-01	.387	.170E-01	.647E-01	.938	355.
	60.8		.215	.771E-02	.388E-01	.286	.113E-01	.471E-01	1.45	343.
ESTD:	47.3		.166	.333E-02	.196E-01	.179	.429E-02	.207E-01	1.65	.532
	47.7		.191	.748E-02	.421E-01	.209	.973E-02	.460E-01	.966	9.54
	48.7		.179	.334E-02	.196E-01	.188	.424E-02	.206E-01	.940	1.48
	49.8		.178	.345E-02	.200E-01	.219	.434E-02	.212E-01	.929	1.49
	50.9		.179	.355E-02	.209E-01	.214	.420E-02	.203E-01	.921	1.23
	52.5		.231	.795E-02	.477E-01	.256	.980E-02	.554E-01	.977	2.33
	54.0		.214	.687E-02	.489E-01	.222	.934E-02	.562E-01	.167	1.34
	55.5		.179	.329E-02	.192E-01	.187	.420E-02	.206E-01	.872	.768
	57.1		.174	.333E-02	.195E-01	.195	.409E-02	.202E-01	.844	1.73
	58.2		.178	.364E-02	.206E-01	.188	.407E-02	.197E-01	.799	2.10
	59.3		.215	.918E-02	.517E-01	.272	.126E-01	.578E-01	.802	2.45
	60.3		.260	.101E-01	.610E-01	.249	.118E-01	.643E-01	.932	15.7
	60.8		.164	.560E-02	.383E-01	.212	.811E-02	.467E-01	1.45	3.28

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Table 3.19 Error Statistics vs F<sub>sc</sub>, OPTRVR, 5th Lobe, S/N=30db, ρ=0.8, θ<sub>sep</sub>=1.5°, WITH CONSTRAINTS

	QTY	FSC	ALFA	THETA	THEDOT	ALFAR	THETAR	THRDOT
MEAN:	47.3		-.554E-01	.222E-02	.152E-03	-.437E-01	-.195E-02	-.464E-04
	47.7		.594E-01	-.171E-02	.628E-03	.520E-01	.253E-02	-.129E-02
	48.7		-.217E-01	.547E-03	.187E-03	-.291E-01	.232E-03	-.249E-03
	49.8		-.173E-01	-.144E-03	.529E-03	-.173E-01	.585E-03	-.613E-03
	50.9		-.195E-01	-.126E-03	-.112E-03	-.102E-01	.120E-02	-.378E-03
	52.5		-.249E-02	-.591E-03	.409E-03	.196E-01	.954E-03	-.315E-03
	54.0		-.102E-01	.403E-04	.272E-03	-.117E-01	.460E-03	-.698E-03
	55.5		-.606E-02	-.146E-03	.876E-03	-.132E-01	.789E-03	-.303E-03
	57.1		-.145E-01	-.500E-03	.577E-03	-.346E-01	.139E-03	-.165E-03
	58.2		-.101E-01	-.393E-03	.232E-03	-.454E-01	-.152E-03	-.965E-03
	59.3		-.265E-01	.217E-03	.700E-03	-.469E-02	.113E-03	-.383E-03
	60.3		.234E-01	-.126E-02	.172E-03	.149E-01	.161E-02	-.322E-03
	60.8		.672E-01	-.314E-02	.335E-03	.550E-01	.342E-02	-.711E-03
	ERMS:	47.3		.220	.410E-02	.193E-01	.231	.449E-02
47.7			.224	.598E-02	.253E-01	.215	.663E-02	.253E-01
48.7			.210	.421E-02	.231E-01	.227	.510E-02	.219E-01
49.8			.198	.353E-02	.191E-01	.214	.441E-02	.208E-01
50.9			.195	.425E-02	.223E-01	.225	.543E-02	.243E-01
52.5			.193	.429E-02	.219E-01	.226	.457E-02	.216E-01
54.0			.193	.340E-02	.180E-01	.211	.419E-02	.188E-01
55.5			.220	.437E-02	.239E-01	.221	.503E-02	.225E-01
57.1			.200	.437E-02	.227E-01	.207	.503E-02	.221E-01
58.2			.219	.474E-02	.230E-01	.259	.501E-02	.220E-01
59.3			.203	.476E-02	.230E-01	.267	.552E-02	.260E-01
60.3			.200	.482E-02	.224E-01	.239	.712E-02	.286E-01
60.8			.216	.480E-02	.177E-01	.207	.547E-02	.170E-01
ESTD:		47.3		.213	.344E-02	.193E-01	.227	.404E-02
	47.7		.218	.562E-02	.253E-01	.208	.613E-02	.253E-01
	48.7		.209	.418E-02	.231E-01	.225	.509E-02	.219E-01
	49.8		.197	.353E-02	.191E-01	.214	.437E-02	.208E-01
	50.9		.195	.425E-02	.223E-01	.224	.530E-02	.243E-01
	52.5		.198	.425E-02	.219E-01	.225	.447E-02	.216E-01
	54.0		.193	.340E-02	.180E-01	.211	.416E-02	.188E-01
	55.5		.220	.437E-02	.239E-01	.220	.502E-02	.225E-01
	57.1		.199	.434E-02	.227E-01	.204	.503E-02	.221E-01
	58.2		.219	.472E-02	.230E-01	.255	.501E-02	.220E-01
	59.3		.203	.476E-02	.230E-01	.267	.552E-02	.260E-01
	60.3		.207	.485E-02	.224E-01	.238	.693E-02	.286E-01
	60.8		.203	.364E-02	.177E-01	.200	.426E-02	.169E-01

Table 3.20 Error Statistics vs  $F_{sc}$ , SUBOPT, 5th Lobe, S/N=30db,  $\rho=0.8$ ,  $\theta_{sep} = 1.5^\circ$  NO CONSTRAINTS

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	QTY	FSC	ALFA	THETA	THEDOT	ALFAR	THETAR	THRDOT
	EMEAN:	47.3	-.554E-01	.222E-02	.152E-03	-.437E-01	-.195E-02	-.464E-04
		47.7	.494E-01	-.171E-02	.628E-03	.520E-01	.253E-02	-.129E-02
		48.7	-.217E-01	.547E-03	.167E-03	-.291E-01	.232E-03	-.249E-03
		49.8	-.173E-01	-.144E-03	.529E-03	-.173E-01	.585E-03	-.613E-03
		50.9	-.195E-01	-.126E-03	-.112E-03	-.102E-01	.120E-02	-.378E-03
		52.5	-.249E-02	-.591E-03	.409E-03	.196E-01	.954E-03	-.315E-03
		54.0	-.102E-01	.403E-04	.272E-03	-.117E-01	.460E-03	-.688E-03
		55.5	-.606E-02	-.148E-03	.876E-03	-.132E-01	.789E-03	-.303E-03
		57.1	-.145E-01	-.500E-03	.577E-03	-.346E-01	.139E-03	-.165E-03
		58.2	-.101E-01	-.398E-03	.232E-03	-.454E-01	-.152E-03	-.985E-03
		59.3	-.285E-01	.217E-03	.700E-03	-.469E-02	.115E-03	-.383E-03
		60.3	.234E-01	-.126E-02	.172E-03	.149E-01	.161E-02	-.323E-03
		60.8	.672E-01	-.314E-02	.335E-03	.530E-01	.343E-02	-.711E-03
	ERMS:	47.3	.220	.410E-02	.193E-01	.231	.449E-02	.197E-01
		47.7	.224	.588E-02	.253E-01	.215	.663E-02	.253E-01
		48.7	.210	.421E-02	.231E-01	.227	.510E-02	.219E-01
		49.8	.198	.353E-02	.191E-01	.214	.441E-02	.206E-01
		50.9	.196	.425E-02	.228E-01	.225	.543E-02	.243E-01
		52.5	.198	.429E-02	.219E-01	.226	.457E-02	.216E-01
		54.0	.193	.340E-02	.180E-01	.211	.419E-02	.188E-01
76		55.5	.220	.437E-02	.239E-01	.221	.508E-02	.225E-01
		57.1	.200	.437E-02	.227E-01	.207	.503E-02	.221E-01
		58.2	.219	.474E-02	.230E-01	.259	.501E-02	.220E-01
		59.3	.205	.476E-02	.230E-01	.267	.552E-02	.260E-01
		60.3	.208	.482E-02	.224E-01	.239	.712E-02	.286E-01
		60.8	.216	.480E-02	.177E-01	.207	.547E-02	.170E-01
	ESTD:	47.3	.213	.344E-02	.193E-01	.227	.404E-02	.197E-01
		47.7	.218	.562E-02	.253E-01	.208	.613E-02	.253E-01
		48.7	.209	.418E-02	.231E-01	.225	.509E-02	.219E-01
		49.8	.197	.353E-02	.191E-01	.214	.437E-02	.206E-01
		50.9	.195	.425E-02	.228E-01	.224	.530E-02	.243E-01
		52.5	.198	.425E-02	.219E-01	.225	.447E-02	.216E-01
		54.0	.193	.340E-02	.180E-01	.211	.416E-02	.188E-01
		55.5	.220	.437E-02	.239E-01	.220	.502E-02	.225E-01
		57.1	.199	.434E-02	.227E-01	.204	.503E-02	.221E-01
		58.2	.219	.472E-02	.230E-01	.255	.501E-02	.220E-01
		59.3	.203	.476E-02	.230E-01	.267	.552E-02	.260E-01
		60.3	.207	.465E-02	.224E-01	.238	.693E-02	.286E-01
		60.8	.205	.364E-02	.177E-01	.200	.426E-02	.169E-01

Table 3.21 Error Statistics vs  $F_{sc}$ , SUBOPT, 5th Lobe, S/N=30db,  $\rho=0.8$ ,  $\theta_{sep}=1.5^\circ$ , WITH CONSTRAINTS

	QTY	FSC	ALFA	THETA	THEDDT	ALFAR	THEYAR	THRDDT	B	WSC
E MEAN:	47.3		.162	-.142E-02	-.761E-03	.259	.331E-02	.191E-03	-.817E-13	297.
	47.7		.952E-01	-.104E-02	-.308E-03	.146	.213E-02	-.186E-03	.439E-12	299.
	48.7		.941E-01	-.101E-02	-.267E-03	.146	.224E-02	-.226E-03	.108E-13	306.
	49.8		.939E-01	-.100E-02	-.292E-03	.146	.222E-02	-.223E-03	.881E-14	313.
	50.9		.938E-01	-.973E-03	-.278E-03	.146	.216E-02	-.268E-03	.384E-12	320.
	52.5		.936E-01	-.100E-02	-.281E-03	.146	.219E-02	-.217E-03	-.204E-14	320.
	54.0		.118	-.113E-02	-.243E-03	.173	.238E-02	-.272E-03	-1.57	339.
	55.5		.939E-01	-.994E-03	-.265E-03	.146	.218E-02	-.241E-03	.319E-12	349.
	57.1		.949E-01	-.104E-02	-.268E-03	.146	.215E-02	-.203E-03	-.427E-12	359.
	58.2		.944E-01	-.102E-02	-.272E-03	.145	.215E-02	-.251E-03	.182E-12	366.
	59.3		.937E-01	-.992E-03	-.295E-03	.146	.219E-02	-.191E-03	.421E-12	372.
	60.3		.941E-01	-.101E-02	-.288E-03	.146	.218E-02	-.215E-03	-.335E-12	379.
	60.8		.749E-01	-.922E-03	-.124E-03	.113	.184E-02	-.373E-03	-.284E-12	382.
ERMS:	47.3		.232	.369E-02	.199E-01	.314	.542E-02	.210E-01	1.57	297.
	47.7		.213	.359E-02	.201E-01	.257	.498E-02	.217E-01	.907	299.
	48.7		.205	.356E-02	.199E-01	.239	.479E-02	.208E-01	.907	306.
	49.8		.201	.356E-02	.200E-01	.260	.485E-02	.213E-01	.907	313.
	50.9		.200	.356E-02	.200E-01	.255	.475E-02	.209E-01	.907	320.
	52.5		.204	.357E-02	.200E-01	.261	.479E-02	.211E-01	.907	330.
	54.0		.203	.361E-02	.200E-01	.246	.483E-02	.209E-01	1.57	339.
	55.5		.205	.354E-02	.200E-01	.238	.474E-02	.207E-01	.907	349.
	57.1		.199	.357E-02	.199E-01	.239	.474E-02	.208E-01	.907	359.
	58.2		.198	.361E-02	.203E-01	.237	.469E-02	.205E-01	.907	366.
	59.3		.195	.363E-02	.202E-01	.261	.482E-02	.213E-01	.907	372.
	60.3		.193	.364E-02	.203E-01	.249	.473E-02	.210E-01	.907	379.
	60.8		.182	.353E-02	.200E-01	.208	.464E-02	.208E-01	1.57	382.
ESTD:	47.3		.167	.340E-02	.199E-01	.179	.429E-02	.210E-01	1.57	.748E-04
	47.7		.191	.343E-02	.201E-01	.211	.450E-02	.217E-01	.907	.607E-04
	48.7		.182	.341E-02	.199E-01	.139	.423E-02	.208E-01	.907	1
	49.8		.178	.341E-02	.200E-01	.216	.431E-02	.213E-01	.907	.716E-04
	50.9		.177	.343E-02	.200E-01	.210	.423E-02	.209E-01	.907	1
	52.5		.177	.343E-02	.200E-01	.216	.426E-02	.211E-01	.907	.143E-03
	54.0		.166	.342E-02	.200E-01	.175	.426E-02	.209E-01	.559E-06	.131E-03
	55.5		.183	.340E-02	.200E-01	.188	.421E-02	.207E-01	.907	.131E-03
	57.1		.175	.341E-02	.199E-01	.189	.422E-02	.208E-01	.907	1
	58.2		.174	.346E-02	.202E-01	.186	.417E-02	.205E-01	.907	.226E-03
	59.3		.171	.346E-02	.202E-01	.216	.430E-02	.213E-01	.907	.200E-03
	60.3		.168	.350E-02	.203E-01	.202	.419E-02	.210E-01	.907	.143E-03
	60.8		.169	.341E-02	.200E-01	.175	.426E-02	.208E-01	1.57	.205E-03

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Table 3.22 Error Statistics vs  $F_{sc}$ , OPTVRV, 5th Lobe,  $(\hat{\beta}, \hat{\omega}_{sc})$  tethered to  $(\pi/2, 0)$   
 $S/N=30\text{db}$ ,  $\rho=0.8$ ,  $\theta_{sep}=1.5^\circ$ , NO CONSTRAINTS

	QTY	FSC	ALFA	THETA	THEDOT	ALFAR	THETAR	THRDDT	B	WSC
	MEAN:	47.3	.162	-.142E-02	-.761E-03	.259	.331E-02	.191E-03	-.017E-13	297.
		47.7	.952E-01	-.104E-02	-.300E-03	.146	.213E-02	-.186E-03	.439E-12	299.
		48.7	.941E-01	-.101E-02	-.267E-03	.146	.224E-02	-.226E-03	.105E-13	306.
		49.8	.939E-01	-.100E-02	-.292E-03	.146	.222E-02	-.223E-03	.631E-14	313.
		50.9	.958E-01	-.973E-03	-.278E-03	.146	.216E-02	-.208E-03	.384E-12	320.
		52.5	.938E-01	-.100E-02	-.281E-03	.146	.219E-02	-.217E-03	-.284E-14	330.
		54.0	.118	-.113E-02	-.243E-03	.173	.238E-02	-.272E-03	-1.57	339.
		55.5	.939E-01	-.994E-03	-.260E-03	.146	.213E-02	-.241E-03	.319E-12	349.
		57.1	.949E-01	-.104E-02	-.268E-03	.146	.215E-02	-.203E-03	-.427E-12	359.
		58.2	.945E-01	-.102E-02	-.272E-03	.145	.215E-02	-.251E-03	.182E-12	366.
		59.3	.937E-01	-.992E-03	-.295E-03	.146	.219E-02	-.191E-03	.421E-12	372.
		60.3	.941E-01	-.101E-02	-.280E-03	.146	.218E-02	-.215E-03	-.335E-12	379.
		60.8	.749E-01	-.922E-03	-.124E-03	.113	.164E-02	-.373E-03	-.184E-12	382.
	ERMS:	47.3	.232	.369E-02	.199E-01	.314	.542E-02	.210E-01	1.57	297.
		47.7	.213	.359E-02	.201E-01	.257	.498E-02	.217E-01	.907	299.
		48.7	.205	.356E-02	.199E-01	.239	.479E-02	.259E-01	.957	306.
		49.8	.201	.358E-02	.200E-01	.260	.485E-02	.213E-01	.907	313.
		50.9	.200	.356E-02	.200E-01	.255	.475E-02	.209E-01	.907	320.
		52.5	.200	.357E-02	.200E-01	.261	.479E-02	.211E-01	.907	330.
		54.0	.203	.361E-02	.200E-01	.246	.488E-02	.209E-01	1.57	339.
		55.5	.205	.354E-02	.200E-01	.236	.474E-02	.207E-01	.907	349.
		57.1	.199	.357E-02	.199E-01	.239	.474E-02	.208E-01	.907	359.
		58.2	.198	.361E-02	.203E-01	.237	.469E-02	.205E-01	.907	366.
		59.3	.195	.360E-02	.202E-01	.251	.482E-02	.213E-01	.907	372.
		60.3	.193	.364E-02	.203E-01	.249	.473E-02	.210E-01	.907	379.
		60.8	.182	.353E-02	.200E-01	.208	.464E-02	.208E-01	1.57	382.
	ESTD:	47.3	.167	.340E-02	.190E-01	.179	.420E-02	.210E-01	1.57	.748E-04
		47.7	.191	.343E-02	.201E-01	.211	.450E-02	.217E-01	.907	.807E-04
		48.7	.182	.341E-02	.199E-01	.109	.423E-02	.230E-01	.907	I
		49.8	.179	.341E-02	.200E-01	.216	.433E-02	.213E-01	.907	.716E-04
		50.9	.177	.343E-02	.200E-01	.216	.423E-02	.209E-01	.907	I
		52.5	.177	.340E-02	.200E-01	.216	.426E-02	.211E-01	.907	.143E-03
		54.0	.166	.342E-02	.200E-01	.175	.426E-02	.209E-01	.559E-06	.131E-03
		55.5	.183	.340E-02	.200E-01	.188	.421E-02	.207E-01	.907	.131E-03
		57.1	.175	.341E-02	.199E-01	.169	.422E-02	.208E-01	.907	I
		58.2	.174	.346E-02	.202E-01	.188	.417E-02	.205E-01	.907	.226E-03
		59.3	.171	.346E-02	.202E-01	.216	.430E-02	.213E-01	.907	.200E-03
		60.3	.165	.350E-02	.203E-01	.202	.419E-02	.210E-01	.907	.143E-03
		60.8	.165	.341E-02	.200E-01	.175	.426E-02	.208E-01	1.57	.203E-03

Table 3.23 Error Statistics vs  $F_{sc}$ , OPTRVR, 5th Lobe,  $(\hat{\beta}, \hat{\omega}_{sc})$  tethered to  $(\pi/2, 0)$ S/N=30db,  $\rho=0.8$ ,  $\theta = 1.5^\circ$ , WITH CONSTRAINTS

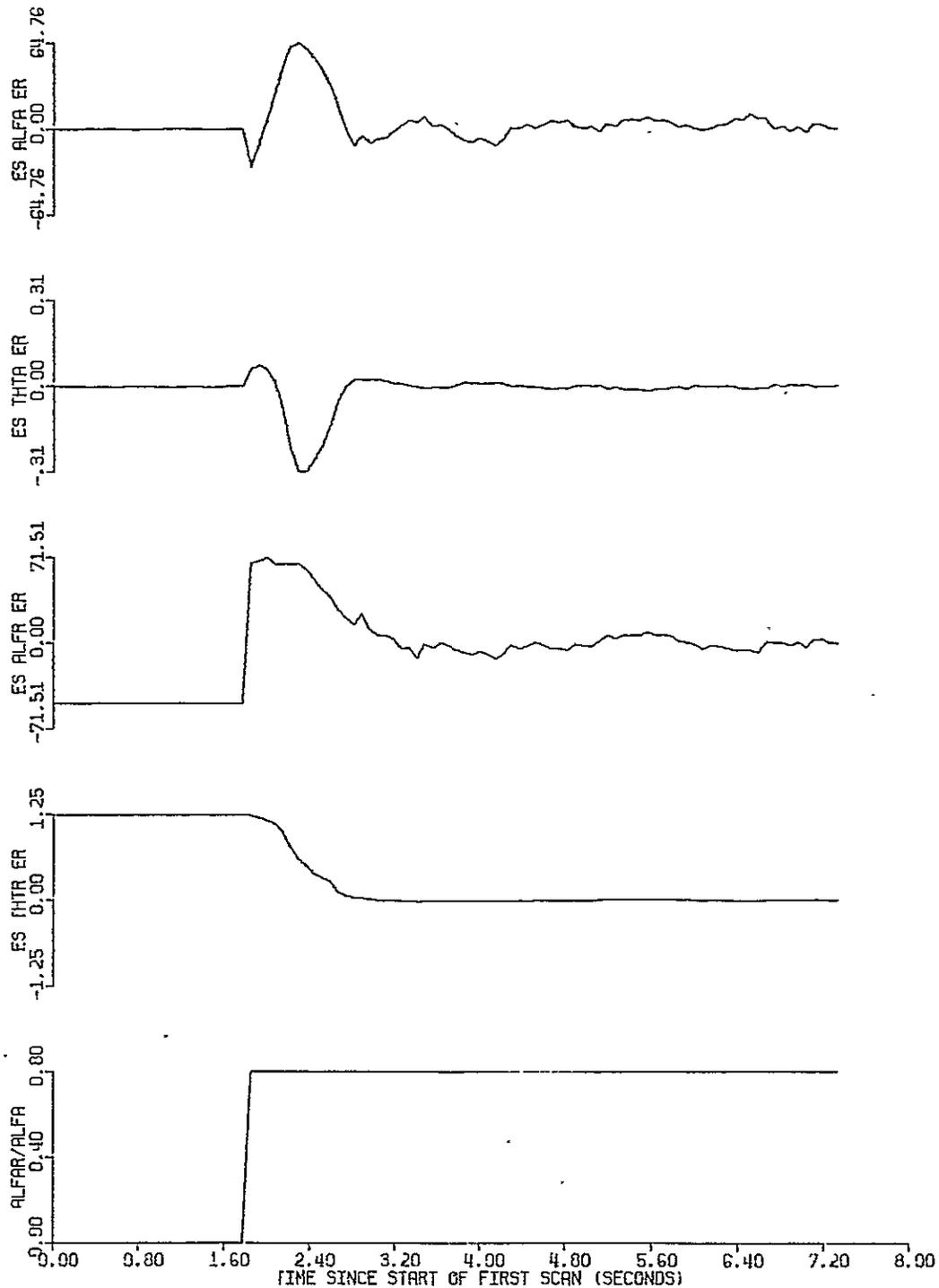
Figures 3.12 thru 3.23 present a study of the interference acquisition capabilities of the interference trackers in the OPTRVR and SUBOPT designs. The 4 top traces on each figure are error time histories respectively (from the top) of the  $\alpha$ ,  $\theta$ ,  $\alpha_R$  and  $\theta_R$  estimate components; the bottom tract shows when the step of interference ( $\rho=0.8$ ) occurs and simultaneously when the interference tracker estimate-vector elements are released from the idler values (equations 3.15 thru 3.19 above). The direct path pulse is being tracked from time zero. All plots have the same time-axis scaling.

Figures 3.11 thru 3.20 for the OPTRVR design (with constraints) show the following:

1. Successful pull-in for small scalloping rates and separation angles as small as the following:
  - a.  $\theta_{sep} = 0.25^\circ$  @ S/N = 40 db (Figure 3.12)
  - b.  $\theta_{sep} = 0.5^\circ$  @ S/N = 20 db (Figure 3.16)
  - c.  $\theta_{sep} = 1^\circ$  @ S/N = 14 db (Figure 3.19)
2. Successful pull-in for small scalloping rates and separation angles probably extending nearly to the window edge ( $4^\circ$ ).
3. Successful pull-in @ S/N 40 db,  $\theta_{sep} = 1^\circ$  and  $F_{sc}$  in the 5th lobe (Figure 3.20). The exact  $F_{sc}$  (51.3 Hz) and initial  $\beta$  ( $-168^\circ$ ) were selected to produce, in the middle of the run, a maximum enhancement of the TO pulse and a maximum cancellation of the FRO pulse.

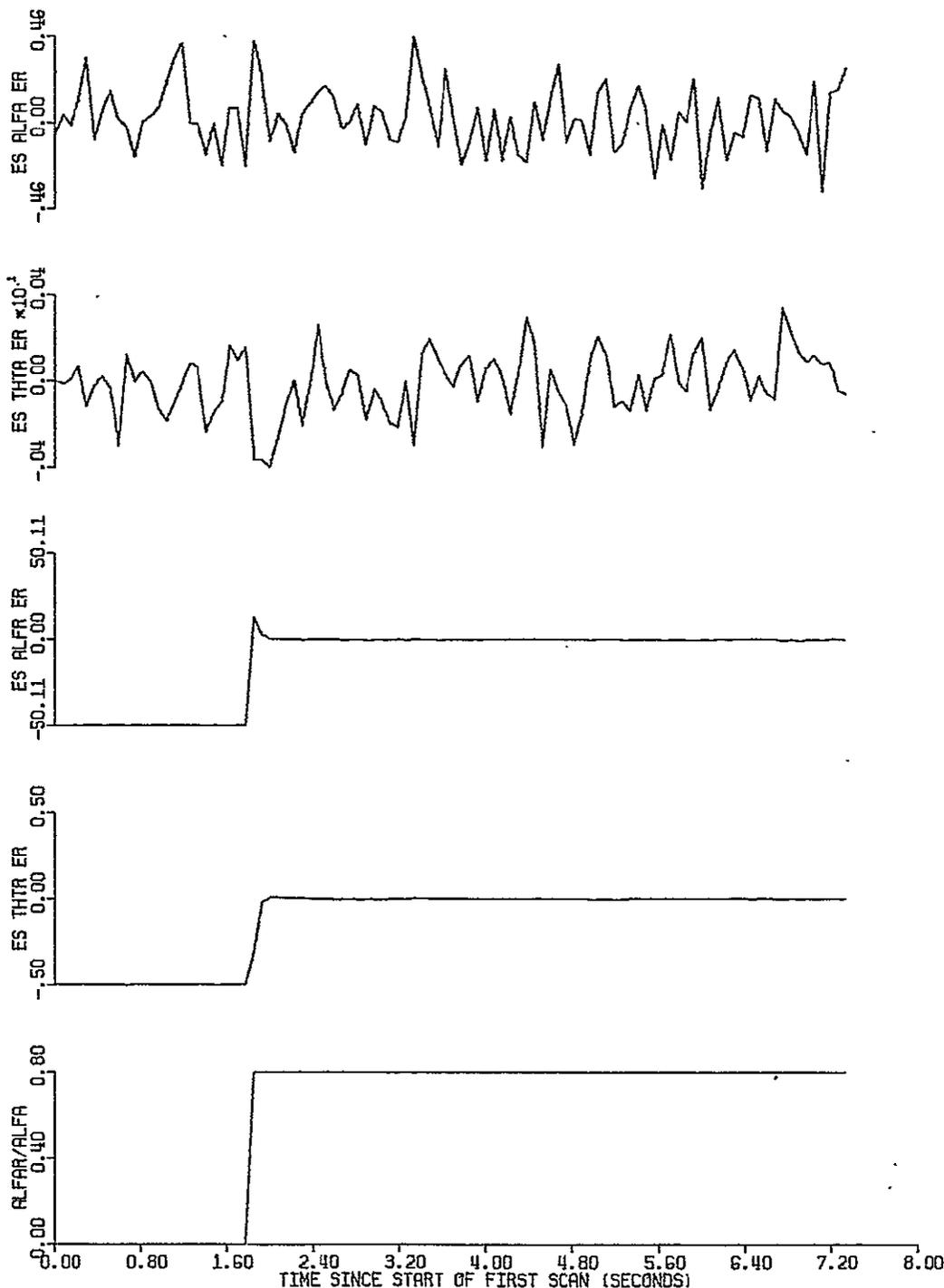
Figures 3.21 thru 3.23 for the SUBOPT design show the following:

1. Results for  $\theta_{sep} = 0.5^\circ$  and  $F_{sc} = 0.6$  Hz (low):



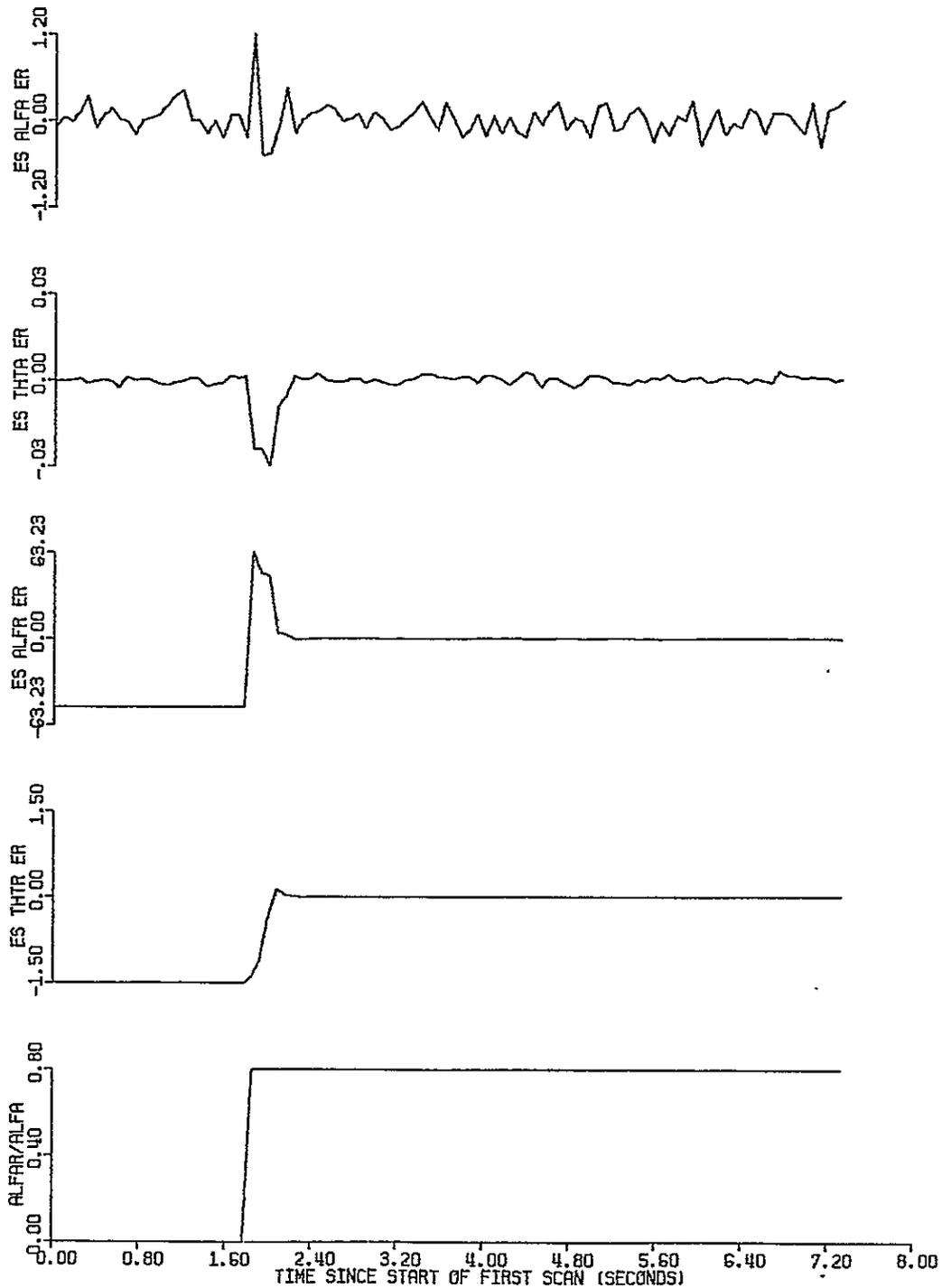
SCENARIO: ACOSITN3, PMLS1, BMLS= 1.0 DEG, DELT= .0740741 SEC, KM=100, KSTART= 26  
 S/N= 40.0 DB, RHO= .8, BETA= 45.0 DEG, FSC=, .600 HZ, THESEP= .250 DEG  
 RECEIVER: OPTIML, ADAPTIV, UNTETHRD, POPT1, BRVVR= 1.0 DEG  
 INTERFERENCE TRACKER IDLER VALUES: .5, 1.5 DEG, 0.0 DEG/SEC, 90.0 DEG, 0.0 HZ  
 BETA ESTIMATE ERROR: INITIAL= -45.0 ,FINAL= -.390 DEG  
 FSC ESTIMATE ERROR: INITIAL= .600 ,FINAL= .241E-01HZ

Figure 3.12 Interference Acquisition, OPTRVR, S/N=30db,  $\rho=0.8$ ,  
 $\theta_{sep}=0.25^\circ$ ,  $\beta=45^\circ$ ,  $F_{sc}=0.6\text{Hz}$



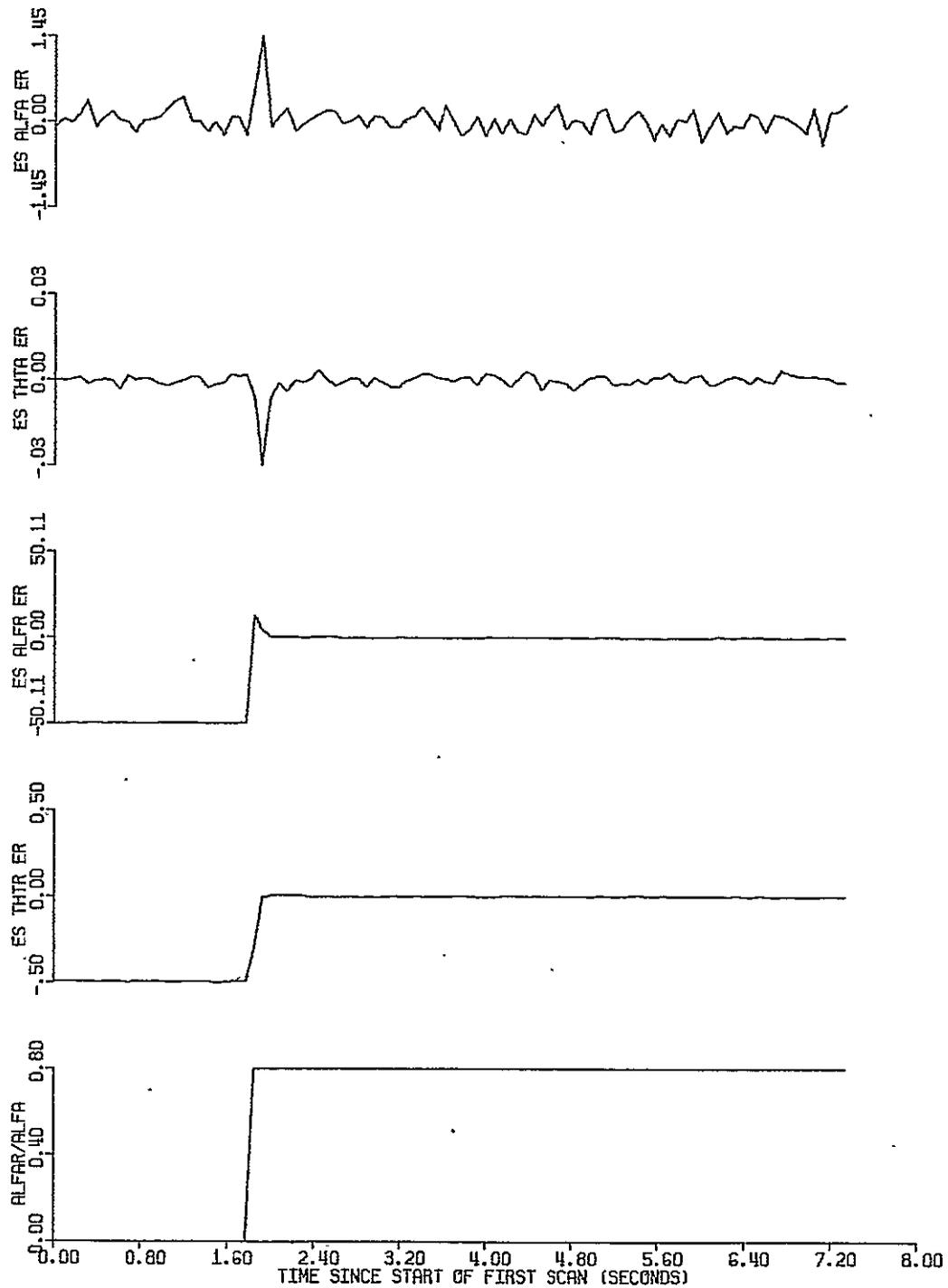
SCENARIO: ACQSITN3, PMLS1, BMLS= 1.0 DEG, DELT= .0740741 SEC, KM=100, KSTART= 26  
 S/N= 40.0 DB, RHO= .8, BETA= 45.0 DEC, FSC=, .600 HZ, THESEP= 2.000 DEG  
 RECEIVER: OPTIML, ADAPTIV, UNTETHRD, POPT1, BRVCR= 1.0 DEG  
 INTERFERENCE TRACKER IDLER VALUES: .5, 1.5 DEG, 0.0 DEG/SEC, 90.0 DEG, 0.0 HZ  
 BETA ESTIMATE ERROR: INITIAL= -45.0 ,FINAL= 5.61 DEG  
 FSC ESTIMATE ERROR: INITIAL= .600 ,FINAL= -.118 HZ

Figure 3.13 Interference Acquisition, OPTRVR, S/N=40db,  $\rho=0.8$   
 $\theta_{sep}=2^\circ$ ,  $\beta=45^\circ$ ,  $F_{sc}=0.6\text{Hz}$



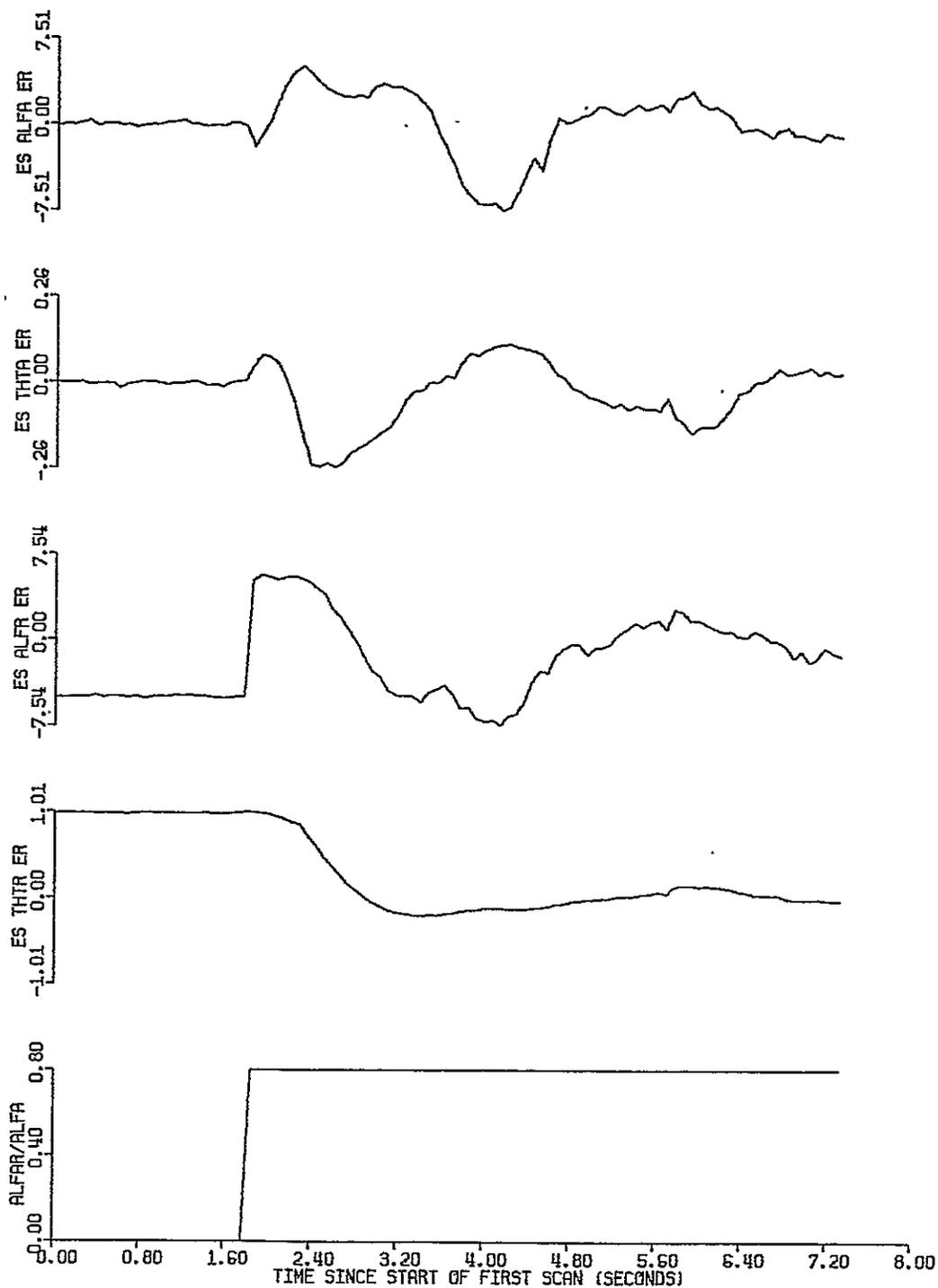
SCENARIO: ACOSITN3, PMLS1, BMLS= 1.0 DEG, DELT= .0740741 SEC, KM=100, KSTART= 26  
 S/N= 40.0 DB, RHO= .8, BETA= 45.0 DEG, FSC=, .600 HZ, THESEP= 3.000 DEG  
 RECEIVER: OPTIML, ADAPTIV, UNTETHRD, POPT1, BRCVR= 1.0 DEG  
 INTERFERENCE TRACKER IDLER VALUES: .5, 1.5 DEG, 0.0 DEG/SEC, 90.0 DEG, 0.0 HZ  
 BETA ESTIMATE ERROR: INITIAL= -45.0 ,FINAL= -2.47 DEG  
 FSC ESTIMATE ERROR: INITIAL= .600 ,FINAL= .946E-01HZ

Figure 3.14 Interference Acquisition, OPTRVR, S/N=40db,  $\rho=0.8$   
 $\theta_{sep}=3^\circ$ ,  $\beta=45^\circ$ ,  $F_{sc}=0.6\text{Hz}$



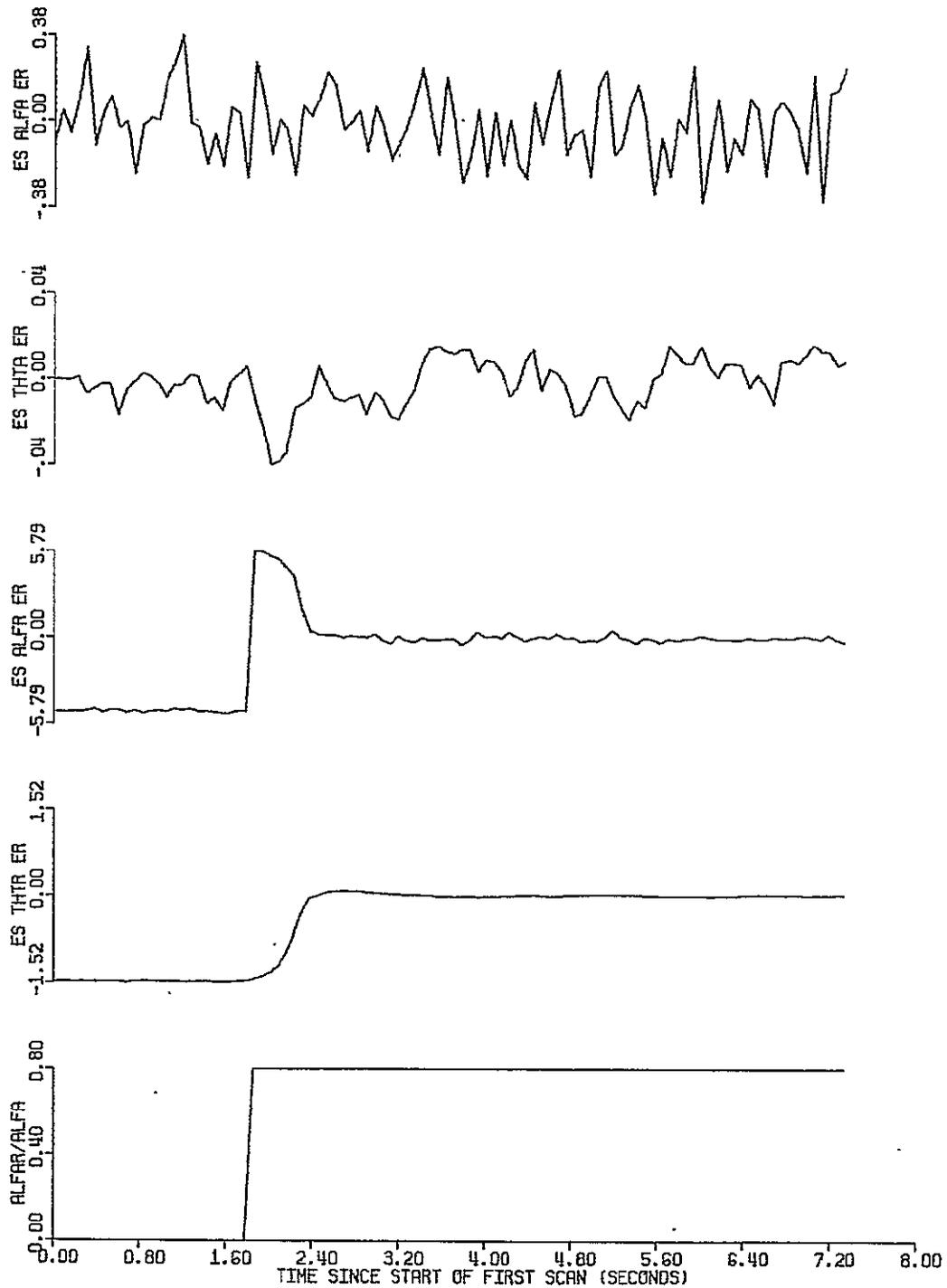
SCENARIO: ACOSITN3, PMLS1, BMLS= 1.0 DEG, DELT= .0740741 SEC, KM=100, KSTART= 26  
 S/N= 40.0 DB, RHO= .8, BETA= 45.0 DEG, FSC=, 2.500 HZ, THESEP= 2.000 DEG  
 RECEIVER: OPTIML, ADAPTIV, UNTETHRD, P0PT1, BRCVR= 1.0 DEG  
 INTERFERENCE TRACKER IDLER VALUES: .5, 1.5 DEG, 0.0 DEG/SEC, 90.0 DEG, 0.0 HZ  
 BETA ESTIMATE ERROR: INITIAL= -45.0 ,FINAL= 4.97 DEG  
 FSC ESTIMATE ERROR: INITIAL= 2.50 ,FINAL= .203 HZ

Figure 3.15 Interference Acquisition, OPTRVR, S/N=40db,  $\rho=0.8$ ,  
 $\theta_{sep}=2^\circ$ ,  $\beta=45^\circ$ ,  $F_{sc}=2.5\text{Hz}$



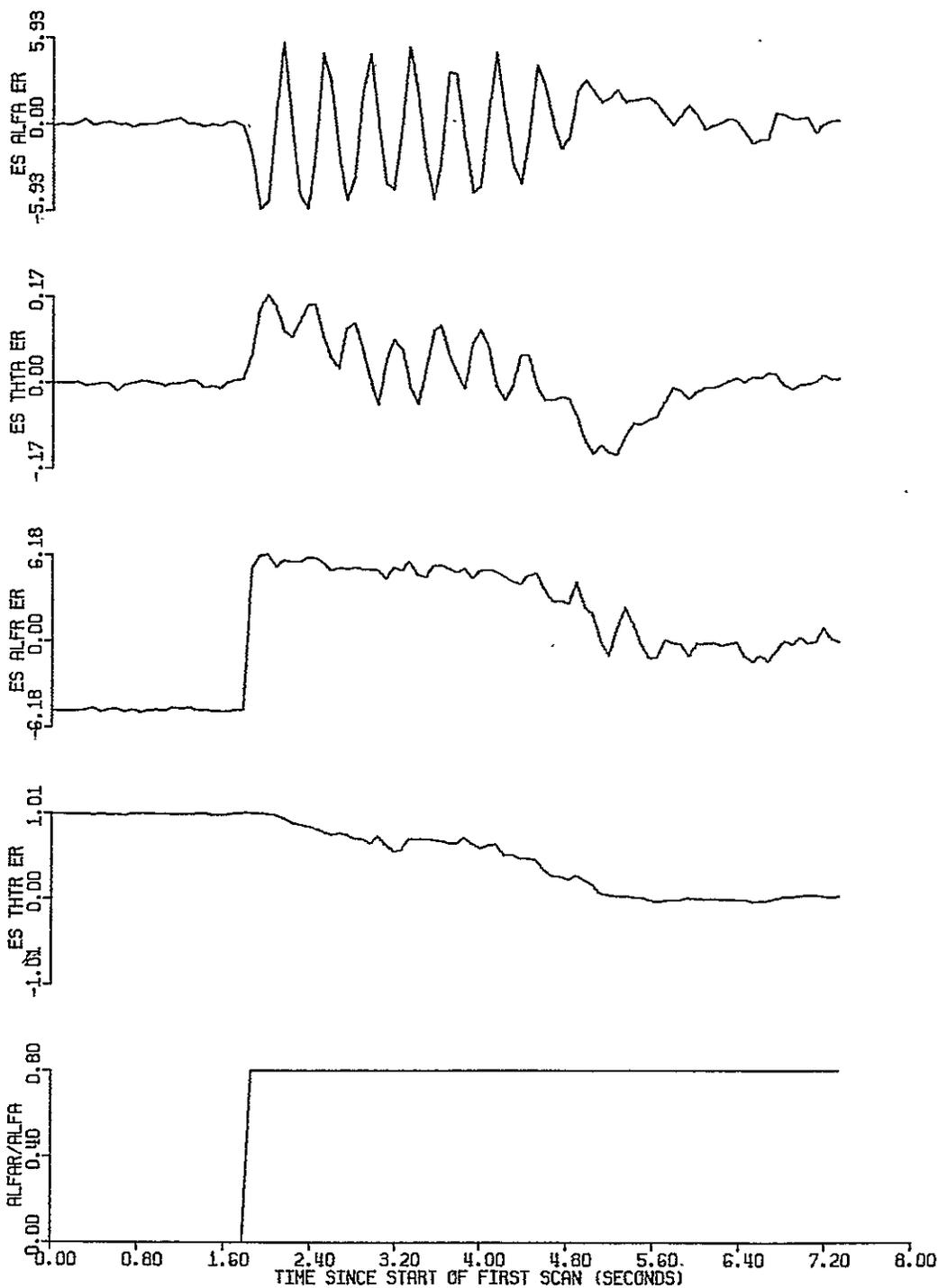
SCENARIO: ACOSITN3, PMLS1, BMLS= 1.0 DEG, DELT= .0740741 SEC, KM=100, KSTART= 26  
 S/N= 20.0 DB, RHO= .8, BETA= 45.0 DEG, FSC=, .600 HZ, THESEP= .500 DEG  
 RECEIVER: OPTIML, ADAPTIV, UNTETHRD, POPT1, BRCVR= 1.0 DEG  
 INTERFERENCE TRACKER IDLER VALUES: .5, 1.5 DEG, 0.0 DEG/SEC, 90.0 DEG, 0.0 HZ  
 BETA ESTIMATE ERROR: INITIAL= -45.0 ,FINAL= -2.98 DEG  
 FSC ESTIMATE ERROR: INITIAL= .600 ,FINAL= .124 HZ

Figure 3.16 Interference Acquisition, OPTRVR, S/N=20db,  $\rho=0.8$ ,  
 $\theta_{sep}=0.5^\circ$ ,  $\beta=45^\circ$ ,  $F_{sc}=0.6\text{Hz}$



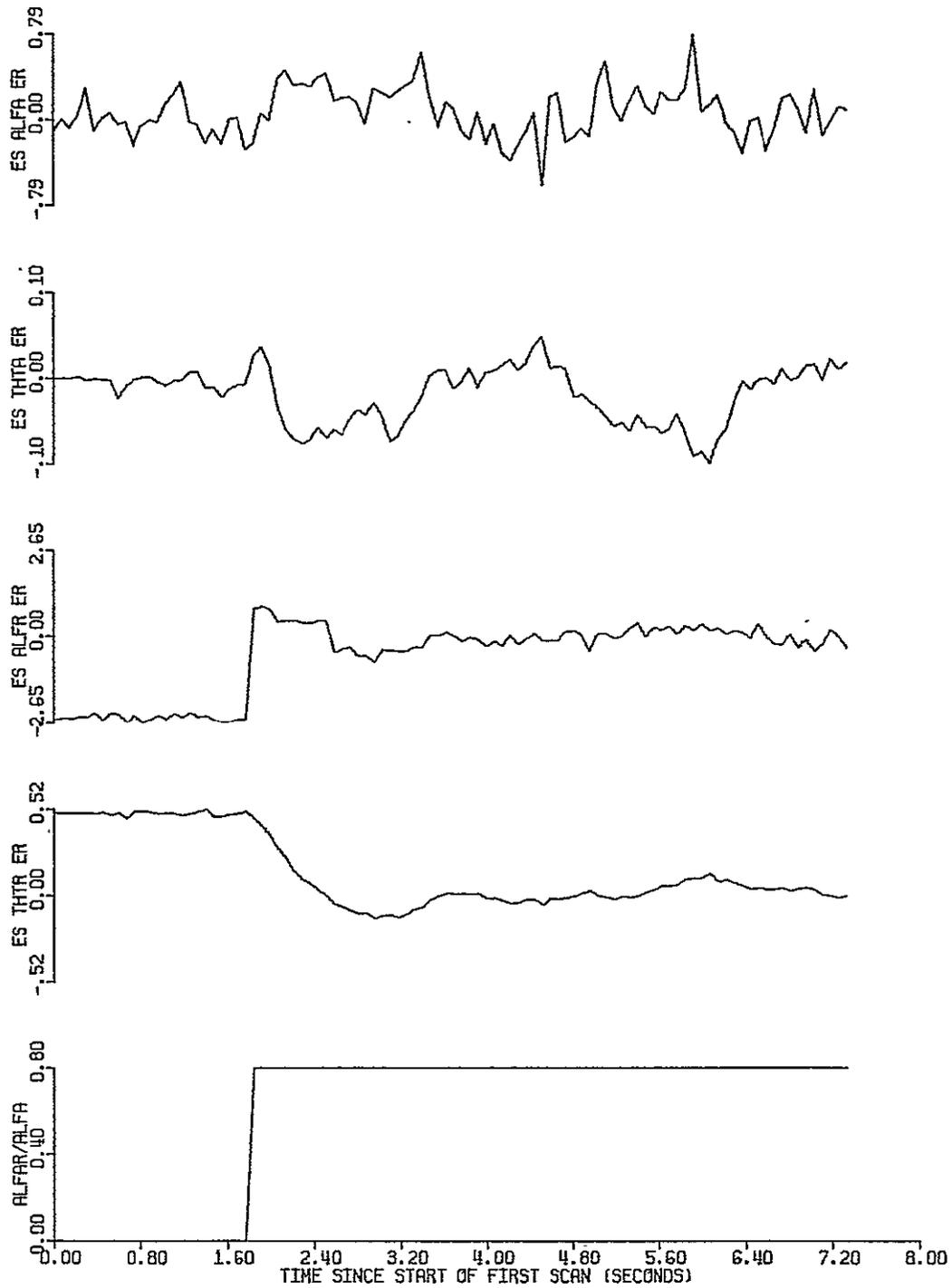
SCENARIO: ACQSITN3, PMLS1, BMLS= 1.0 DEG, DELT= .0740741 SEC, KM=100, KSTART= 26  
 S/N= 20.0 DB, RHO= .8, BETA= 45.0 DEG, FSC=, .600 HZ, THESEP= 3.000 DEG  
 RECEIVER: OPTIML, ADAPTIV, UNTETHRD, POPT1, BRVVR= 1.0 DEG  
 INTERFERENCE TRACKER IDLER VALUES: .5, 1.5 DEG, 0.0 DEG/SEC, 90.0 DEG, 0.0 HZ  
 BETA ESTIMATE ERROR: INITIAL= -45.0 ,FINAL= 6.88 DEG  
 FSC ESTIMATE ERROR: INITIAL= .600 ,FINAL= .174 HZ

Figure 3.17 Interference Acquisition, OPTRVR, S/N=20db,  $\rho=0.8$ ,  
 $\theta_{sep}=3^{\circ}$ ,  $\beta=45^{\circ}$ ,  $F_{sc}=0.6\text{Hz}$



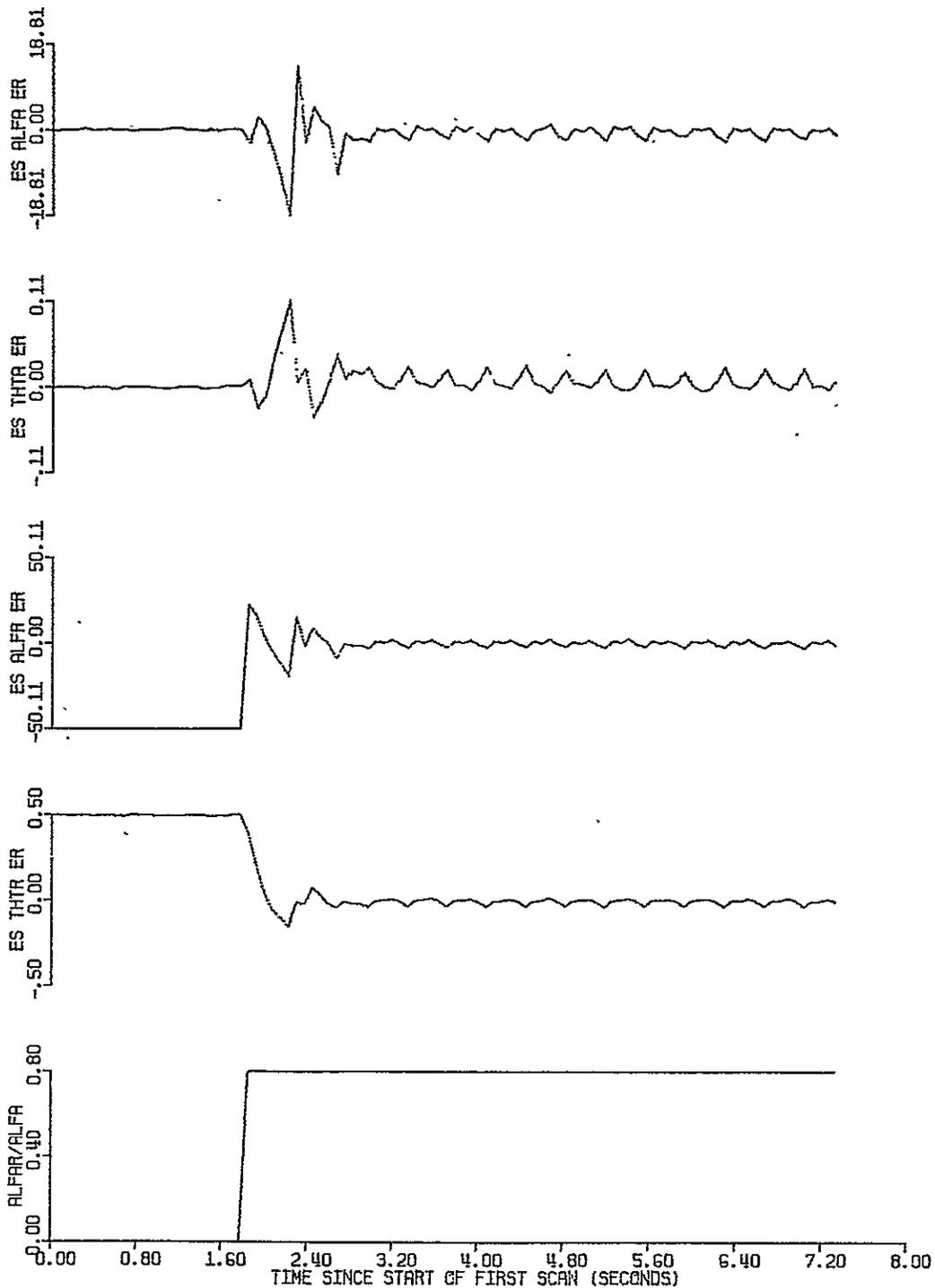
SCENARIO: ACQSITN3, PMLS1, BMLS= 1.0 DEG, DELT= .0740741 SEC, KM=100, KSTART= 26  
 S/N= 20.0 DB, RHO= .8, BETA= 45.0 DEG, FSC=, 2.500 HZ, THESEP= .500 DEG  
 RECEIVER: OPTIML, ADAPTIV, UNETHRD, POPT1, BRVVR= 1.0 DEG  
 INTERFERENCE TRACKER IDLER VALUES: .5, 1.5 DEG, 0.0 DEG/SEC, 90.0 DEG, 0.0 HZ  
 BETA ESTIMATE ERROR: INITIAL= -45.0 ,FINAL= -10.4 DEG  
 FSC ESTIMATE ERROR: INITIAL= 2.50 ,FINAL= -.257 HZ

Figure 3.18 Interference Acquisition, OPTRVR, S/N=20db,  $\rho=0.8$ ,  
 $\theta_{sep}=0.5^\circ$ ,  $\beta=45^\circ$ ,  $F_{sc}=2.5\text{Hz}$



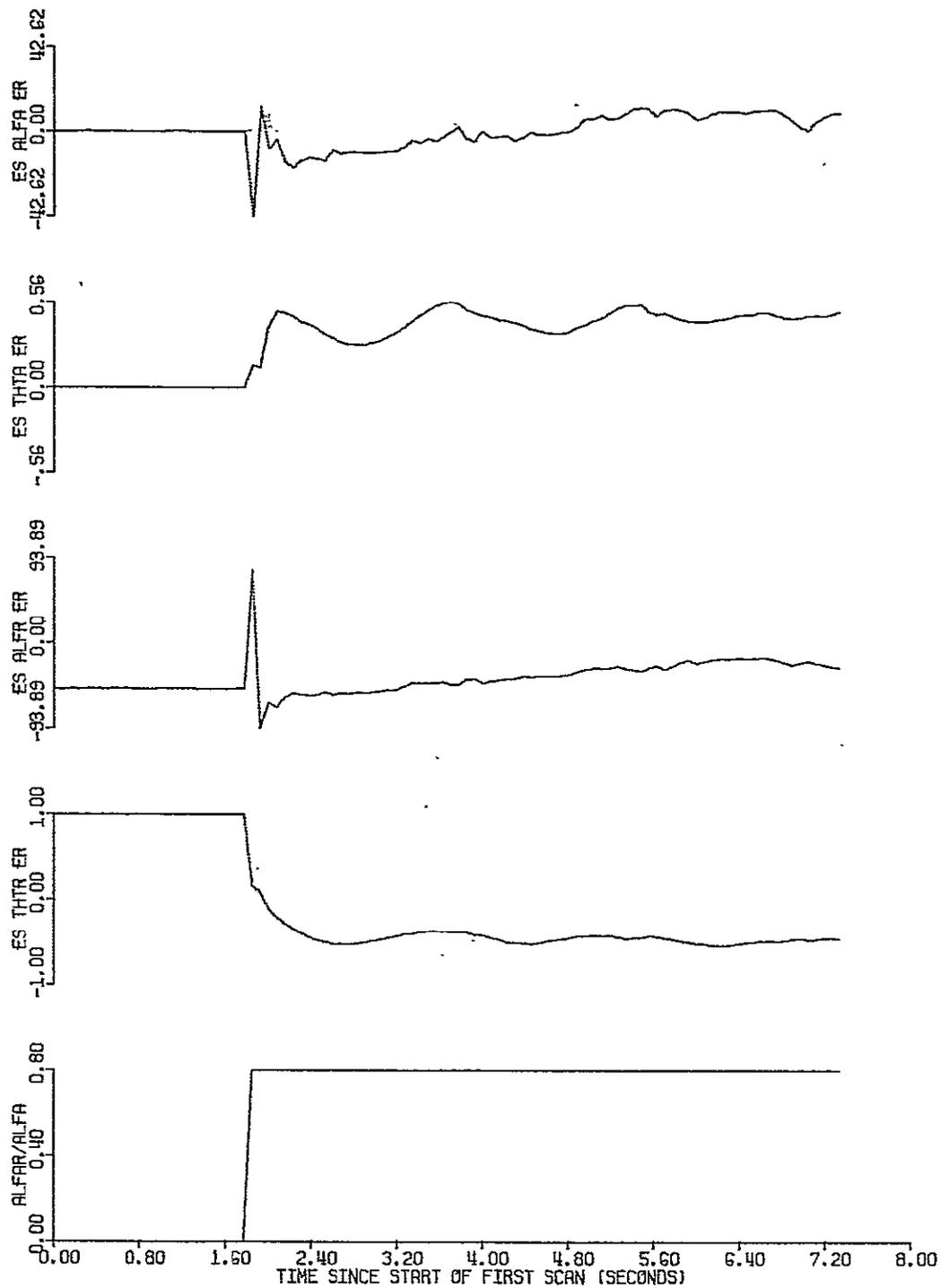
SCENARIO: ACQSITN3, PMLS1, BMLS= 1.0 DEG, DELT= .0740741 SEC, KM=100, KSTART= 26  
 S/N= 14.0 DB, RHO= .8, BETA= 45.0 DEG, FSC=, .600 HZ, THESEP= 1.000 DEG  
 RECEIVER: OPTIML, ADAPTIV, UNTETHRD, POPT1, BRCVR= 1.0 DEG  
 INTERFERENCE TRACKER IDLER VALUES: .5, 1.5 DEG, 0.0 DEG/SEC, 90.0 DEG, 0.0 HZ  
 BETA ESTIMATE ERROR: INITIAL= -45.0 ,FINAL= -1.64 DEG  
 FSC ESTIMATE ERROR: INITIAL= .600 ,FINAL= -.482E-01HZ

Figure 3.19 Interference Acquisition, OPTRVR, S/N=14db,  $\rho=0.8$ ,  
 $\theta_{sep}=1^\circ$ ,  $\beta=45^\circ$ ,  $F_{sc}=0.6\text{Hz}$



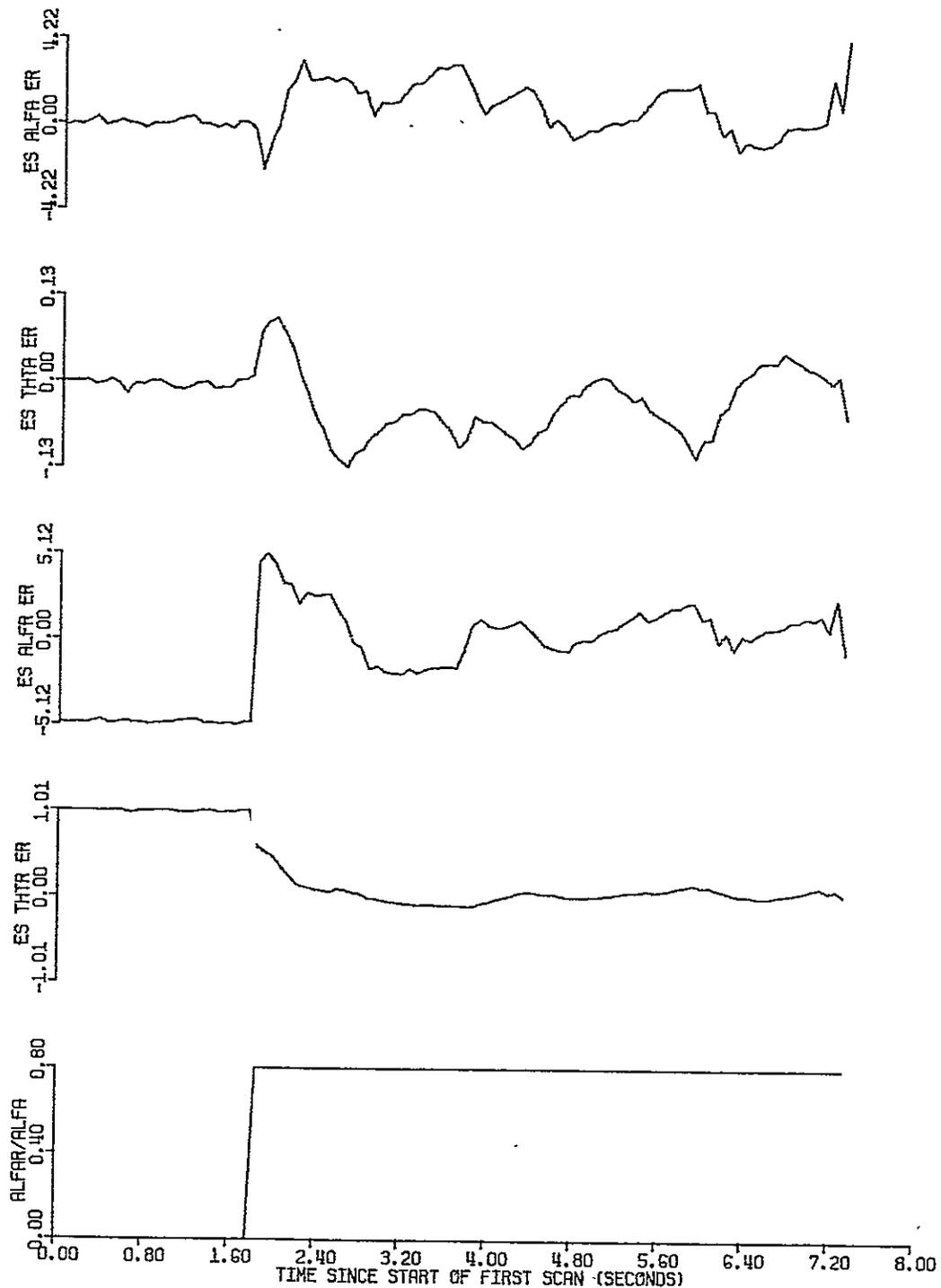
SCENARIO: ACQSITN3, PMLS1, BMLS= 1.0 DEG, DELT= .0740741 SEC, KM=100, KSTART= 26  
 S/N= 40.0 DB, RHO= .8, BETA=-168.0 DEG, FSC=, 51.300 HZ, THESEP= 1.000 DEG  
 RECEIVER: OPTIML, ADAPTIV, UNTETHRD, POPPL, BRCVR= 1.0 DEG  
 INTERFERENCE TRACKER IDLER VALUES: .5, 1.5 DEG, 0.0 DEG/SEC, 90.0 DEG, 0.0 HZ  
 BETA ESTIMATE ERROR: INITIAL= 78.0 ,FINAL= 5.11 DEG  
 FSC ESTIMATE ERROR: INITIAL= 51.3 ,FINAL= 50.6 HZ

Figure 3.20 Interference Acquisition, OPTRVR, S/N=40db,  $\rho=0.8$   
 $\theta_{sep}=1^\circ$ ,  $\beta=-168^\circ$ ,  $F_{sc}=51.3\text{Hz}$



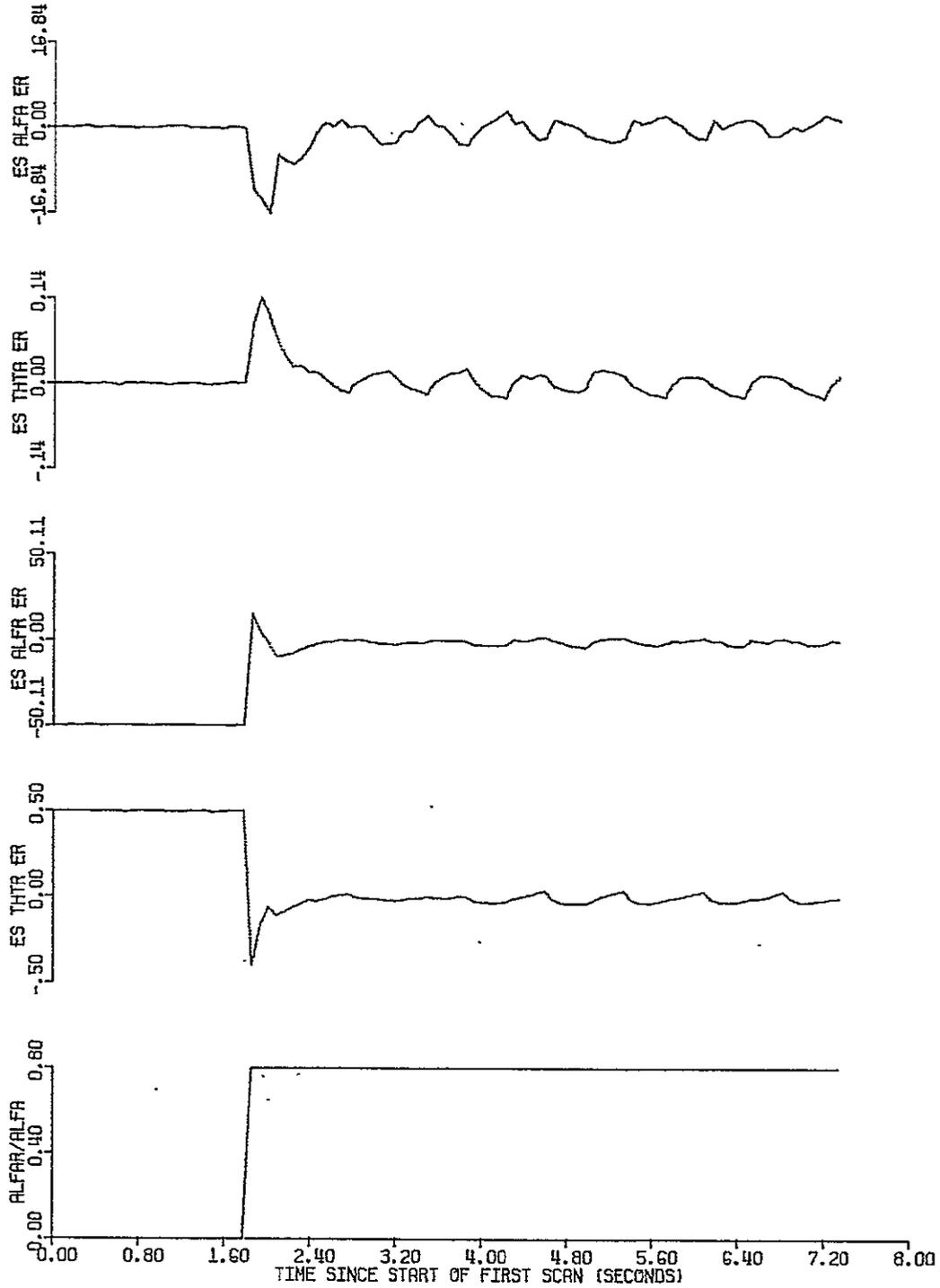
SCENARIO: ACQSITN3, PMLS1, BMLS= 1.0 DEG, DELT= .0740741 SEC, KM=100, KSTART= 26  
 S/N= 40.0 DB, RHO= .8, BETA= 45.0 DEG, FSC=, .600 HZ, THESEP= .500 DEG  
 RECEIVER: SUBOPT, ADAPTIV, UNTETHRD, POPT1, BRCVR= 1.0 DEG

Figure 3.21 Interference Acquisition, SUBOPT, S/N=40db,  $\rho=0.8$ ,  
 $\theta_{sep}=0.5^\circ$ ,  $\beta=45^\circ$ ,  $F_{sc}=0.6\text{Hz}$



SCENARIO: ACQSIN3, PMLS1, BMLS= 1.0 DEG, DELT= .0740741 SEC, KM=100, KSTART= 26  
 S/N= 20.0 DB, RHO= .8, BETA= 45.0 DEG, FSC=, .600 HZ, THESEP= .500 DEG  
 RECEIVER: SUBOPT, ADAPTIV, UNTETHRD, POPT1, BRCVR= 1.0 DEG

Figure 3.22 Interference Acquisition, SUBOPT, S/N=20db,  $\rho=0.8$ ,  
 $\theta_{sep} = 0.5^\circ$ ,  $\beta=45^\circ$ ,  $F_{sc} = 0.6$  Hz



SCENARIO: ACQSITN3, PMLS1, BMLS= 1.0 DEG, DELT= .0740741 SEC, KM=100, KSTART= 26  
 S/N= 40.0 DB, RHO= .8, BETA=-168.0 DEG, FSC=, 51.300 HZ, THESEP= 1.000 DEG  
 RECEIVER: SUBOPT, ADAPTIV, UNTETHRD, POPT1, BRCVR= 1.0 DEG

Figure 3.23 Interference Acquisition, SUBOPT, S/N=40db,  $\rho=0.8$ ,  
 $\theta_{sep}=1^\circ$ ,  $\beta= - 168^\circ$ , 51.3 Hz

- a.  $S/N = 40$  db -- unsuccessful pull-in, in fact loss of track of the direct path pulse (Figure 3.21);
  - b.  $S/N = 20$  db -- successful pull-in (Figure 3.22);
2. Successful pull-in @  $S/N = 40$  db,  $\theta_{sep} = 1^\circ$  and  $F_{sc}$  in the 5th lobe, again maximum enhancement of TO pulse, maximum cancellation of FRO pulse (Figure 3.23).

The poor performance shown in Figure 3.21 is probably attributable to the low scalloping rate, the successful pull-in of Figure 3.22 notwithstanding. The SUBOPT design is essentially premised upon an arbitrarily high scalloping rate, and under these circumstances the results of Figure 3.21 are probably more to be expected than those of Figure 3.22. The successful pull-in of Figure 3.22 is probably only a testament to the beneficial effects of noise acting as dither; or worse, it may be sample function dependent. More study here should be done.

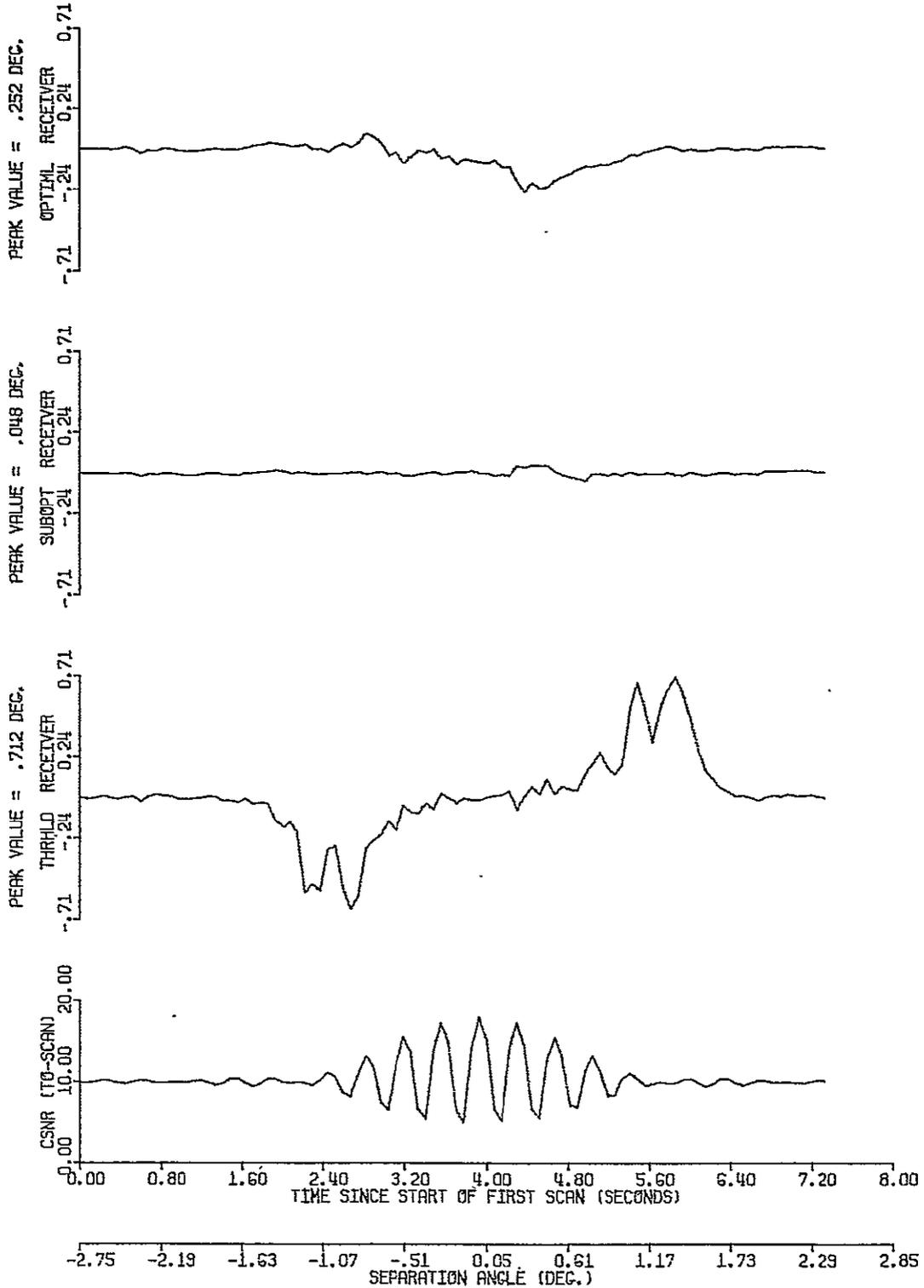
Finally, Figures 3.24 and 3.25 provide comparisons of the three receivers OPTRVR, SUBOPT and the threshold receiver, in a crossing multipath scenario, beginning with the receivers in track and the interference initially out-of-beam. The same noise sample function was used to construct the envelope signal applied to the receiver in each case, and the error time histories are all plotted to the same scale. Two significant differences in the figures, one intentional, one not, are, as follows:

1. In Figure 3.24, the OPTRVR and SUBOPT designs include constraints, in Figure 3.25 these are without constraints.
2. In the two figures that OPTRVR and SUBOPT error time history traces are interposed; in Figure 3.24, that for OPTRVR is on top; in Figure 3.25, that for SUBOPT is on top.

SIM. JOB: HALENIA  
 HALENIU  
 HALENJS  
 PLOT JOB: CRPLOLH

FILE NO: 112211U101  
 113211U101  
 111110U101  
 PROGRAM: PCRMP1

DATE: 05/03/79  
 05/03/79  
 05/03/79  
 DATE: 05/03/79



S/N= 20.0 DB,  $\rho=$  .80,  $\beta=-168.0$  DEG, FSC= 51.3 HZ, KM= 100 SCANS, BMLS= 1.00, PMLS1

OPTIML: ADAPTIY, UNTETHRD, POPT1, BRCVR=1.00 DEG., ERMS= .690944E-01 DEG.  
 SUBOPT: ADAPTIY, UNTETHRD, POPT1, BRCVR=1.00 DEG., ERMS= .136560E-01 DEG.  
 THRLD: -3 DB, UNTETHRD, 6.00% OF SCANS ABORTED, ERMS= .243510 DEG.

Figure 3.24 Crossing Multipath, OPTRVR and SUBOPT with constraints  
 $S/N=20\text{db}$ ,  $\rho=0.8$ ,  $\beta= -168$ ,  $F_{sc} = 51.3$  Hz

SIM. JOB: MLSSU0G  
 MLSDPOF  
 MLSTHYX

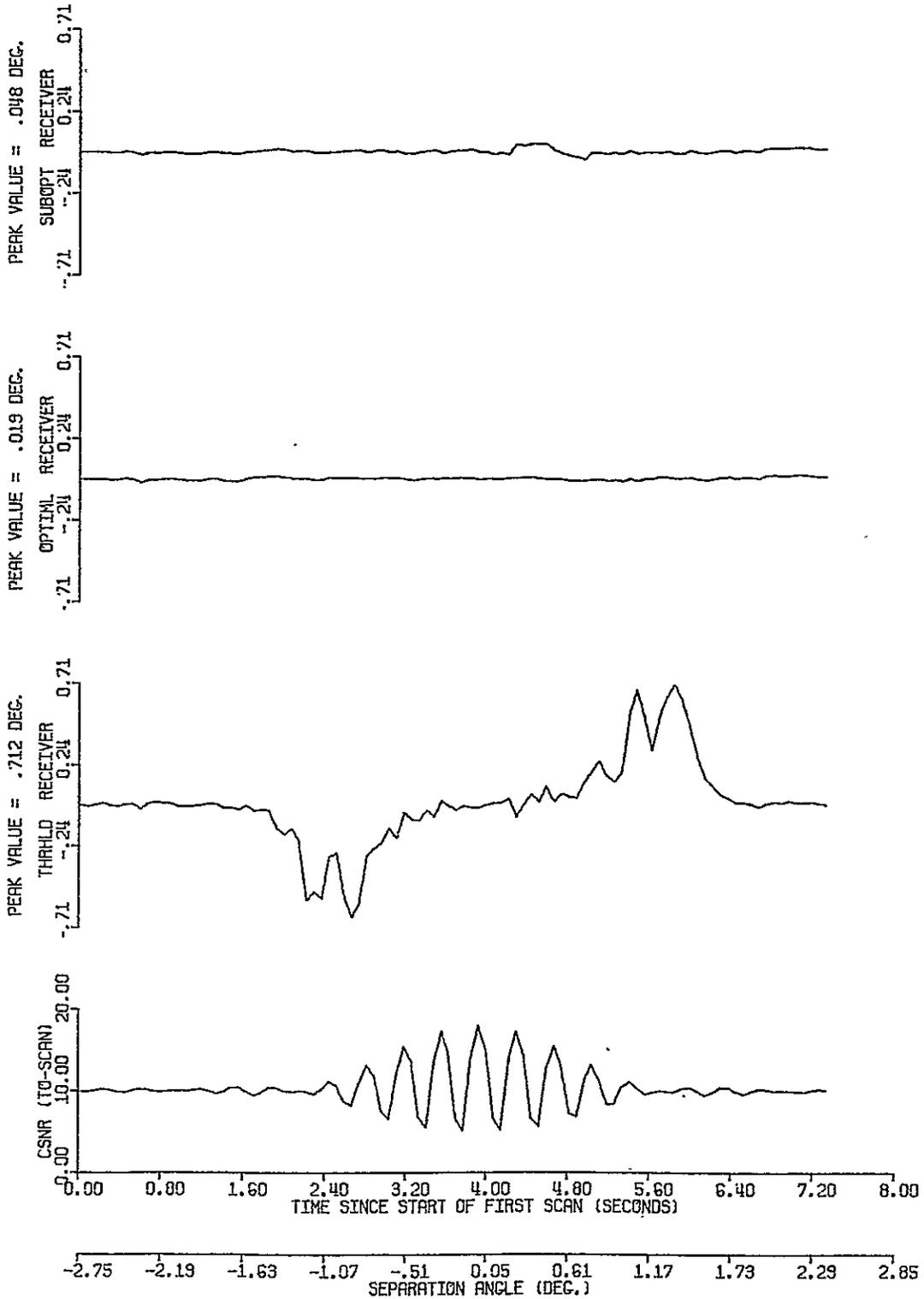
FILE NO: 113211U117  
 112211U117  
 111110U117

DATE: 05/24/78  
 05/24/78  
 05/23/78

PLOT JOB: CRPL02U

PROGRAM: PCRMP1

DATE: 06/22/78



S/N= 20.0 DB, RHO= .80, BETA=-168.0 DEG, FSC= 51.3 HZ, KM= 100 SCANS, BMLS= 1.00, PMLS1

SUBOPT: ADAPTIV, UNTETHRD, POPT1, BRCVR=1.00 DEG., ERMS= .136560E-01 DEG.  
 OPTIML: ADAPTIV, UNTETHRD, POPT1, BRCVR=1.00 DEG., ERMS= .755801E-02 DEG.  
 THRHD: -3 DB, UNTETHRD, 6.00% OF SCANS ABORTED, ERMS= .243510 DEG.

Figure 3.25 Crossing Multipath, OPTRVR and SUBOPT without constraints  
 $S/N=20\text{db}$ ,  $\rho=0.8$ ,  $\beta= -168^\circ$ ,  $F_{sc} = 51.3\text{ Hz}$

Another very significant difference is in the OPTRVR error time histories themselves -- that without constraints peaks at about  $1/50^\circ$ , and that with constraints, at about  $1/4^\circ$ , worse than the SUBOPT response, which peaks at about  $1/20^\circ$  with and without constraints. Again, we suspect the  $\hat{\omega}_{sc}$  constraint for the deterioration of the OPTRVR performance. Nevertheless, all optimal structure receivers performed better in this demonstration than did the threshold receiver, which peaked at  $0.71^\circ$ . The lowest trace shows the carrier signal-to-noise ratio CSNR, evaluated at the peak of the direct path pulse on the TO-scan, as the simulation evolves. The  $F_{sc}$  used here is in the 5th lobe, the exact  $\beta$ ,  $F_{sc}$ , values used being again that combination producing maximum enhancement of the TO-pulse and maximum cancellation of the FRO-pulse at crossover.

In summary, a simulation study involving principally statistical error studies but also some error time histories has been carried out; a substantial collection of FORTRAN programs was developed. Simulation results show for the OPTRVR design

1. RMSE performance improvement factors wrt the threshold receiver sometimes approaching 30 at 20 db S/N;
2. Full track capability limited to scalloping rates below  $1/2$  of rep. rate (below 6.75 Hz in AZ).
3. Some deterioration in performance when constraints are used believed attributable to the  $\hat{\omega}_{sc}$  constraint. Removal of this one constraint may restore the generally higher RMSE performance of the unconstrained OPTRVR without reducing the resistance to loss of track apparently characterizing the constrained receiver (see SUBOPT below). Also perhaps a depend-

able angle-tracking capability at higher scalloping rates might result from removal of the  $\hat{\omega}_{sc}$ -constraint.

The results show for the SUBOPT design

1. Lesser performance than the OPTRVR design, improvement factors wrt the threshold receiver sometimes approaching 15 at 20 db S/N;
2. Performance probably better at higher scalloping rates, deteriorating at lower rates;
3. Very definite improvement in track-holding ability at small separation angles when the receiver constraints are applied. There is no  $\omega_{sc}$ -estimate, hence no  $\hat{\omega}_{sc}$ -constraint in the SUBOPT design.

Based on studies of the OPTRVR, we expect both the OPTRVR and SUBOPT design performance to be quite sensitive to error, in the receiver model, of the transmitting antenna selectivity function, particularly the beam width parameter. Possible approaches to reduce the effects on performance were discussed. Finally, in error time history studies

1. Strong interference pull-in capabilities at various S/N's and  $F_{sc}$ 's were demonstrated, which might be used in an interference acquisition scheme; and
2. A high performance in a representative crossing multipath situation was demonstrated, and is to be generally expected, particularly if the removal of the  $\hat{\omega}_{sc}$ -constraint will have the effects expected and discussed.

## SECTION IV

### EXPERIMENTAL SYSTEM CONSIDERATIONS

An experimental receiver development project was included in the original research proposal and begun in 1976 in parallel with tracking algorithm development then in progress. The project was short-lived, however, and abandoned the following year, principally because the computational demands of the evolving tracking algorithms simply could not be met with any economically feasible microcomputer that was available at the time. The general design philosophy and the allocation of tasks among

1. the interface hardware
2. the foreground software
3. the background software

were described in [3, pp. 52-60]; the approach to the interface design, involving specifically a state controller, is conveyed in Appendix B of this final report.

At the present time, both the MLS tracking algorithm development and the state-of-the-art in microcomputing are more advanced. It seems safe to conjecture, in conclusion, that one way the requisite computer power might be obtained economically, certainly in the near future, is to make use of a bank, or an array, of now diminishingly expensive microprocessors. One or more microprocessors might serve the executive function, allocating the resources provided by the others to the various computational needs as they arise. Advantages of such an arrangement might be, as follows:

1. It would be able to exploit the large potential for parallel computation in the tracking receiver calculations;
2. It would have high protection against total system failure due to isolated failures;
3. It would easily accomodate the randomized repetition rates in the MLS.

## SECTION V

### SUMMARY AND CONCLUSIONS

This report has described research performed at the University and concerned with optimal MLS receiver theory, design and simulation evaluation. The program has produced a general receiver structure which, it is believed, gives close to limiting performance; it consists of a Scan Data Processor (SDP) based on the theory of Locally Optimum Estimation enclosed in a Tracking Loop Filter (TLF) based on MMSE recursive state estimation. Three concrete specializations of the general structure were carried out, characterized by both the dimension of the Scan Data Processor and the method of extraction of phase difference ( $\beta$ ) and scalloping frequency ( $\omega_{sc}$ ) information, as follows:

5D SDP: Denoted the Optimal design (OPTRVR); SDP extracts  $\beta$  information from each scan; TLF extracts  $\omega_{sc}$  information from the sequence of scans;

4D SDP: Denoted the Suboptimal design (SUBOPT); Both  $\beta$  and  $\omega_{sc}$  are suppressed from the model and not estimated,

6D SDP: Denoted the 6D LOE design; SDP extracts  $\beta$  and  $\omega_{sc}$  information from each scan; TLF may optionally extract  $\dot{\omega}_{sc}$  information.

Two of these, the OPTRVR and SUBOPT designs were studied extensively in simulation studies, including:

- a. Statistical error studies under various conditions;
- b. Studies of interference acquisition capability using "pull-in",

- c. Performance evaluations with "crossing" multipath interference.

and comparisons of performances were made with a simulated "threshold" receiver approximately representative of the Phase III design. Finally, a limited effort to implement an experimental receiver was undertaken, but was aborted with little more result than the tentative approach planned and the insights gained.

In the simulation studies of RMSE the OPTRVR and SUBOPT designs showed improvements over the threshold receiver by factors approaching 30 and 15, respectively, at low scalloping rates. Constraints were imposed on the computed estimates, based largely on natural limitations on the true state values, and as a result, improved ability to maintain track was noted in the SUBOPT design at small separation angles and moderate S/N. At higher values of scalloping rate,  $\omega_{sc}$ , the SUBOPT design was superior to the OPTRVR with constraints. The data suggests, however, that the  $\hat{\omega}_{sc}$ -constraint in OPTRVR may be hurting performance some, though even with its removal, successful full-state tracking can't be expected in OPTRVR in the strict sense at higher scalloping frequencies. A high sensitivity to error in the receiver model of the MLS transmitting antenna selectivity function, particularly the beam width parameter, was observed in the SUBOPT design (and believed to be characteristic of the OPTRVR design also). Approaches were discussed to reduce this problem. Both the OPTRVR and SUBOPT designs exhibited sufficient multipath "pull-in" capability to merit a "pull-in" approach to interference acquisition. In summary, the receiver designs developed in this research have demonstrated in simulation superior levels of

performance for MLS receivers. Some areas of consideration need further study, however, to fine-tune the designs to the signal and state dynamics environment and other aspects of the application. On the basis of available data the SUBOPT design appears to be the more appropriate for the MLS aircraft receiver application, where the scalloping rates experienced are generally greater than one-half the MLS angle function repetition rate, and thus beyond the full-track capability of the OPTVRV design.

From the viewpoint of implementation, it would appear that, on the basis of trends in the microprocessor art,

1. Input of the envelope samples to the computer should be made by direct memory access (DMA), and
2. The computer should, perhaps, be a bank of microprocessors performing many operations in parallel (to supply the requisite computing power) and operating as a unified system under an executive function microprocessor.

Finally, an operational receiver should probably be structurally adaptive also with an ability to expand the state vector (by appending a "sentry" tracker channel tethered to "idler" values) as additional interference pulses are recognized and acquired. The "sentry" should move from a position one side of the sampling window to the opposite side and then back on alternate scans to preserve the integrity of the main pulse track. Also when the separation angle for an interference pulse drops below a certain threshold and information needed to distinguish the pulse becomes less available, track of that interference pulse should then be dropped and the state dimension suitably decremented.



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#### REFERENCES

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## APPENDIX A

### COMPUTER PROGRAMS

Programs in this appendix are listed below in the order presented, generally alphabetized by Module name in two groups. Programs within each Module are listed with a brief characterization of the Module.

Programs for the 6D LOE design are given in Appendix C.

#### SIMULATION PROGRAMS

CTLACQN3:     CONTRL, Interference Acquisition Scenario  
CTLCRMP:     CONTRL, Crossing Multipath Scenario  
CTLMSBB1:     CONTRL, RMSE ( $B_{ratio}$ )  
CTLMSFS1:     CONTRL, RMSE ( $F_{sc}$ )  
CTLMSFS2:     CONTRL, RMSE ( $F_{sc}$ ), ( $\hat{\beta}$ ,  $\hat{\omega}_{sc}$ ) tethered to  $(\pi/2, 0)$   
CTLMSTH2:     CONTRL, RMSE ( $\theta_{sep}$ ), averaging with  $F_{sc} \neq 0$   
CTLOE:        CONTRL, RMSE ( $\theta_{sep}$ ), averaging with  $F_{sc} = 0$   
MLSSIM:       MLSSIM, MLSSUB, THA, DFLTR1, MLS  
OPTRNC:       RCVR, ORVRID, No constraints, except on  $\hat{\beta}$   
OPTRVR:       RCVR, ORVRID, with constraints  
PLSUB:        PHILM, WAWBJ, SWFCNS, PLUSID, Suboptimal SDP  
PLOPT:        PHILM, PLOPID, Optimal SDP  
PMLS1:        PMLS, PMLSID, p-function used in generating signal  
POPT1:        P, PDOT, POPTID, p-function presumed in receiver  
THDRVR:       RCVR, TRVRID, threshold receiver

#### UTILITY AND SERVICE PROGRAMS

ACQMP1:       ACQMP1, Acquisition plot generator  
LABLIB:       CLIP, GAUSS, INTIO, LOGIO, MATIN, MATMUL, MATOUT, MATSM,  
              MULPLT, PLOTR, PVALUE, REALIO, RETURN, SATU, library  
              of utility routines  
PCRMP1:       PCRMP1, Crossing multipath plot generator  
RLOGSW:       RLOGSW, Reads and lists out SWAJ, SWBJ, & RABJ data  
              from file  
WLOGSW:       WLOGSW, WAWB, WAVGS, computes SWAJ, SWBJ, & RABJ data  
              and writes files

```

SUBROUTINE CONTRL(ISW)
C
C THIS CONDUCTS THE MLS SIMULATION THROUGH A
C CROSSING MULTIPATH SCENARIO
5 C
REAL LAMDA
INTEGER XNAME(2),YNAME(2),DATIN(4),DATOUT(4),DOUT
INTEGER YNAM1(2),YNAM2(2),YNAM3(2),YNAM4(2),YNAM5(2),FUNCTN(2)
10 INTEGER YNAM7(2),YNAM8(2)
LOGICAL NOKLMN,NOLOE,NOAC,KALMAN,LOE,TETHRD,MORE,NFIRST,ADAPTIV
LOGICAL FILOUT,FILEIN
COMMON/IDDATA/ISIM,IPMLS,IRCVR,IADAP,ITETHR,IPOPT
COMMON/RCVRO0/THAMX,THAMIN,TS,TR,OMEGA,TF
COMMON/RCVRO1/NGMIN,NGMAX,DELBL,NGM,IR,IAE
15 COMMON/RCVRO2/RHOMAX,DTHO,TDRD,BD,WSCD,NSQ(4),NGD(4)
COMMON/RCVRO3/PI,F(8,8),FL25(4),FSAMP,K,KM,TETHRD,NG,NS,JM
COMMON/RCVRO4/DELT,ED(8),GGGT(8,8),H(5,8),ICOUNT,SIGMA
COMMON/RCVRO5/NOLOE,NOKLMN,NOAC,GAMAES(5),RODIAG(5),PHDIAG(8)
COMMON/RCVRO6/PPDIAG(8),RMAT(5,5),PHI(5,5),PA(8,8),LAMDA(5)
20 COMMON/RCVRO7/T(130),V(130)
COMMON/RCVRO8/XSLOE(8),ESLOE(8),ES(8)
COMMON/RCVRO9/BRCVR,BB,POCRIT,CC
COMMON/RCVR10/XS1(8),XS(8)
COMMON/MLS000/ALFA,THE,THEODT,ALFAR,THR,THRODT,8,WSC
COMMON/MLS001/CSNRT,CSNRF,DSNRDB,RHO,BETA,FSC,LGMAX
25 COMMON/MLS002/DCSNR,CSNR,LG,TPKT,TPKF
COMMON/MLS003/FL10AE(4,2),FL10(4),DELTAT(2),XD(8,2),YD(4,2)
COMMON/MLS004/BMLS,BBB,MTIMES,MSET,MORE
DIMENSION IDNRS(6),IDASCI(24),IDENTS(6),RMSVAL(8)
30 DIMENSION EALFA(100),ETHET(100),EALFR(100),ETHER(100),XFOUR(100)
DIMENSION X(8),SCANNR(100)
DIMENSION EBETA(100),EFSC(100)
EQUIVALENCE (ALFA,X(1)),(ISIM,IDNRS(1)),(DOUT,DATOUT(2))
DATA ABORT/1HA/,SPACE/1H /,NFIRST/.FALSE./,ADAPTIV/.TRUE./
35 DATA DATIN/10HMLSSIMDATA,10H500000F000,2*0/
DATA DATOUT/10HMLSSIMDATA,3*0/
DATA IDASCI/7HCROSSHP,7HRHSE(T),7HRHSE(B),7HRHSE(F),7HACQSITN,
*3*7H /,7HGENERAL,8H PMLS1,8H PMLS2,
40 *8H PMLS3,8H THRLD,8H OPTIML,8H SUBOPT,8H -3 DB,8HADAPTIV,
*8HNONADAP,8HUNTETHRD,8HTETHERED,2H /,8H POPT1,8H POPT2,
*8H POPT3 /
DATA NSTART/3/,IRSIGN/1/,KSTART/26/,FILOUT/.FALSE./,
CFILEIN/.FALSE./
45 DATA FUNCTN/7HAZIMUTH,7HELEVAT./
DATA XNAME/8H SCAN,8H NUMBER /,YNAM2/8H ETHET,8HDEGREES /
DATA YNAM1/8H EALFA,8H /,YNAM3/8H EALFAR,8H /
DATA YNAM4/8H ETHER,8HDEGREES /,YNAM5/8H RHO,8H /
DATA YNAM7/8HEABS BETA,8H DEGREES /
50 DATA YNAM8/8HEABS FSC,8H HERTZ /
C
GO TO (100,200,300,400,500,600,700,800,900,1000,1100,1200),ISW
1 FORMAT(1H )
10 FORMAT(9(/))
11 FORMAT(1H1)
55 C
C *****
C

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A-2

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100 CONTINUE
C THIS IDENTIFIES THE SCENARIO AND REINITIALIZES, AS NECESSARY,
60 CTHE FOLLOWING RECEIVER PARAMETERS
   CSIGMA,IAC,OSNRDB,RHO,FSC,BETA,JM,BMLS
   IF(NFIRST) GO TO 155
   NOAC=.FALSE.
   NFIRST=.TRUE.
65   JONAM=JOBNAME(I)
   ISIM=5
   IMOD=3
   WRITE (7,110)
110  FORMAT(34HINTERFERENCE ACQUISITION SCENARIO/)
   IF (IRCVR.NE.1) GO TO 118
   WRITE (7,115)
115  FORMAT (35H THIS IS NOT FOR THRESHOLD RECEIVER)
   STOP * ABORTED--NOT FOR THORVR*
118  CONTINUE
75 118  WRITE(7,120) (DATIN(I),I=1,2)
120  FORMAT(26H THIS MAY READ INPUT FILE ,2A10/)
   CALL LOGIO(6HFILEIN,FILEIN,0)
   IF(.NOT.FILEIN) NSTART=0
   CALL INTIO(6HNSTART,NSTART,100,0)
60  NSTOP=NSTART
   CALL INTIO(6H NSTOP,NSTOP,100,0)
   CALL LOGIO(6HFILOUT,FILOUT,0)
   CALL LOGIO(6HTETHRO,TETHRO,0)
   CALL LOGIO(6HADAPTV,ADAPTV,0)
85  IF(TETHRO) ITETHR=2
   IF(ADAPTV) GO TO 135
   IRSIGN=-1
   IADAP=3
135  CONTINUE
90  DO 145 I=2,6
   IASC=3+(I-1)+IDNRS(I)+6
   IDENTS(I)=IDASCI(IASC)
145  CONTINUE
   ENCODE(8,150,IDENTS(1)) IDASCI(ISIM),IMOD
95 150  FORMAT(A7,I1)
   WRITE (7,152) IDNRS,IMOD
152  FORMAT (1H ,6I1,1X,I1/)
   WRITE (7,153) IDENTS
153  FORMAT (1H ,A8)
100  CALL REALIO (6HRRHOMAX,RHOMAX,0)
   CALL REALIO(6H DTHO,OTHO,0)
   CALL REALIO(6H TORO,TORO,0)
   BETAO=BD*180./PI
   FSCO=WSCO*.5/PI
105  CALL REALIO(6H BETAO,BETAO,0)
   CALL REALIO(6H FSCO,FSCO,0)
   BO=BETAO*PI/180.
   WSCO=FSCO*(2.*PI)
110 155  CONTINUE
   IF (FILEIN) GO TO 158
   NRUN=0
   OSNRDB=20.
   RHO=0.5
   BETA=45.

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115      FSC=0.
        BMLS=1.
        BRCVR=1.
        THESEP=1.88
120      CALL INTIO(6H NRUN,NRUN,100,0)
        CALL REALIO(6HDSNRDB,DSNRDB,0)
        CALL REALIO(6H RHO,RHO,0)
        CALL REALIO(6H BETA,BETA,0)
        CALL REALIO(6H FSC,FSC,0)
        CALL REALIO(6H BMLS,BMLS,0)
125      CALL REALIO(6H BRCVR,BRCVR,0)
        CALL REALIO(6HTHESEP,THESEP,0)
        CALL INTIG(6HKSTART,KSTART,100,0)
        MORE=.FALSE.
        GO TO 170
130      158 CONTINUE
        READ(15,160) NRUN,DSNRDB,RHO,BETA,FSC,BMLS,BRCVR,THESEP,KSTART
        160 FORMAT(15,7G10.3,I5)
        IF(NRUN.LT.NSTART) GO TO 158
        IF(NRUN.GE.NSTOP) MORE=.FALSE.
135      170 CONTINUE
        XO(3,IAE)=XO(6,IAE)=0.
        XO(5,IAE)=XO(2,IAE)-THESEP
        EBETA=ABS(BETA)-ABS(BETA0)
        EFSC=ABS(FSC)-ABS(FSC0)
140      RETURN
        C
        C*****
        C
        200 CONTINUE
145      C THIS OUTPUTS BASIC SIMULATION DATA OF INTEREST, SUCH AS
        C THE ANGLE FUNCTION, INITIAL STATE, ETC.
        WRITE(7,209)
        209 FORMAT(5H1NRUN,4X,6HDSNRDB,7X,3HRHO,8X,4HBETA,8X,3HFSC,9X,
        C4HBMLS,8X,5HBRCVR,7X,6HTHESEP,6X,6HKSTART)
150      WRITE(7,210) NRUN,DSNRDB,RHO,BETA,FSC,BMLS,BRCVR,THESEP,KSTART
        210 FORMAT(1H0,I4,7(2X,G10.3),2X,I4)
        IF(.NOT.FILOUT) GO TO 245
        IF(NRUN.LE.9) ENCODE(10,220,DOUT) IDNRS,1HU,IMOD,1H0,NRUN
        220 FORMAT(6I1,A1,I1,A1,I1)
155      IF(NRUN.GE.10) ENCODE(10,230,DOUT) IDNRS,1HU,IMOD,NRUN
        230 FORMAT(6I1,A1,I1,I2)
        IX=IREQST(6LTAPE17,3L*PF)
        IF(IX.NE.0) CALL INTIO(6HIX(RQ),IX,1,1)
        IF(IX.NE.0) STOP OUTPUT FILE REQUEST NOT SATISFACTORY#
160      WRITE(7,240) (DATOUT(I),I=1,2)
        240 FORMAT(25H0THIS WRITES OUTPUT FILE ,2A10)
        245 CALL DATE(TODAY)
        WRITE(7,250) FUNCTN(IAE),IAE
        250 FORMAT(1H0,A7,15H FUNCTION(IAE=,I1,1H))
165      X(4)=XO(4,IAE)=0.
        WRITE(7,260) ((I,X(I)),I=1,8)
        260 FORMAT(15H0INITIAL STATE://(3H X(,I1,4H) = ,G13.6))
        WRITE(7,270) IOENTS(2)
        270 FORMAT(1H0,A7)
170      RETURN

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A-4

CONTINUED  
 ON P. 3

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C*****
C
175 30J CONTINUE
C THIS IDENTIFIES THE BASIC RECEIVER STRUCTURE (THRHL,OPT,SUBOPT)
CAND REINITIALIZES, AS NECESSARY, THE FOLLOWING RCVR DATA.
CIR (NEGATE ONLY), NOAC,NOKLMN,NOLOE,BRCVR,DELBL,TETHRD
ITIT=MIND(IRCVR,2)
C
180 C NEGATE IR WITH THE FOLLOWING FOR NONADAPTIVE RECEIVER
IF(IRSIGN.LT.0) IR=-IR
C
RETURN
C
185 C*****
C
40J CONTINUE
C THIS OUTPUTS BASIC RECEIVER DATA OF INTEREST.
WRITE(7,410) (IDENTS(I),I=3,4),IR,NG,NS
190 410 FORMAT (1H0,A8,4HRCVR/1H0,A8,6HDESIGN/5H (IR=,I2,4H,NG=,I1,
* 4H,NS=,I1,1H))
WRITE(7,420) (IDENTS(I),I=5,6)
420 FORMAT(1H0,A8/1H0,A7/)
RETURN
195 C
C*****
C
50J CONTINUE
C THIS SETS-UP THE MSET-LOOP
200 RETURN
C
C*****
C
60J CONTINUE
C THIS SETS-UP THE LG-LOOP FOR THE (MSET)-TH SERIES OF SETS
205 RETURN
C
C*****
C
70J CONTINUE
C THIS SETS-UP THE K-LOOP FOR THE (LG)-TH SET OF KM SCANS
CALL INTID(6H KM,KM,1,1)
WRITE(7,710)
210 710 FORMAT (4H0 K, 3X,6HCSNRTO,5X,6HCSNRFR,6X,3HQTY,7X,
* 4HALFA,5X,5HTHETA,6X,6HTHEDOT,5X,5HALFAR,6X,6HTHETAR,5X,
C 6HTHRDDOT,6X,4H B ,7X,3HWSC/)
RETURN
C
C*****
C
220 80J CONTINUE
C THIS INITIALIZES THE K-TH SCAN
IF(K.EQ.KSTART) X(4)=RHO*X(1)
IF(K.EQ.KSTART) NGM=NG
225 RETURN
C
C*****
C

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230      900 CONTINUE
      C THIS SAVES/PREPROCESSES DATA FROM THE K-TH SCAN
      THEKK=X(2)-XS(2)
      DTMC=X(2)-X(5)
      COLB=SQRT(PPDIAG(2))
      DO 910 I=1,NS
235      ES(I)=X(I)-XS(I)
      RMSVAL(I)=SQRT(PPDIAG(I))
      910 CONTINUE
      IF (NS.GE.7) ES(7) = ABS(X(7))-ABS(XS(7))
      IF (NS.GE.8) ES(8) = ABS(X(8))-ABS(XS(8))
240      SCANNR(K)=K
      EALFA(K)=ES(1)
      ETHET(K)=ES(2)
      EALFR(K)=ES(4)
      ETHER(K)=ES(5)
245      XFOUR(K)=X(4)/X(1)
      IF (NS.LE.6) GO TO 915
      EBETA(K)=180.*ES(7)/PI
      EFSC(K)=0.5*ES(8)/PI
      915 CONTINUE
250      WRITE (7,920) K, CSNRT,CSNRF,1HX,(X(I),I=1,8)
      920 FORMAT(1H,13, 2(1X,G10.3),8X,A1,1X,8(1X,G10.3))
      WRITE (7,930) 7H XS,(X(I),I=1,NS)
      WRITE (7,930) 7H ERR,(ES(I),I=1,NS)
      WRITE (7,930) 7HSQ(PI),RMSVAL(I),I=1,NS)
255      930 FORMAT (1H,27X,A7,1X,8(1X,G10.3))
      WRITE (7,1)
      RETURN
      C
      C*****
260      C
      1000 CONTINUE
      C THIS SAVES/PROCESSES/OUTPUTS DATA FROM THE (LG)-TH SET OF KM SCANS
      WRITE(7,1060) (GGGT(I,I),I=1,NS)
265      1060 FORMAT (10(/),35H ON LAST SCAN, DIAGONAL OF GGGT WAS/
      *1H,G11.4,7(1H,G11.4))
      YMIN=YMAX=0.
      WRITE (7,11)
      CALL PLOTR(SCANNR, EALFA,KM,XNAME,YNAM1,YMIN,YMAX,0)
      CALL REALIO(6H YMIN,YMIN,1)
270      CALL REALIO(6H YMAX,YMAX,1)
      YMIN=YMAX=0.
      WRITE (7,11)
      CALL PLOTR(SCANNR, ETHET,KM,XNAME,YNAM2,YMIN,YMAX,0)
      CALL REALIO(6H YMIN,YMIN,1)
275      CALL REALIO(6H YMAX,YMAX,1)
      YMIN=YMAX=0.
      WRITE (7,11)
      CALL PLOTR(SCANNR, EALFR,KM,XNAME,YNAM3,YMIN,YMAX,0)
      CALL REALIO(6H YMIN,YMIN,1)
280      CALL REALIO(6H YMAX,YMAX,1)
      YMIN=YMAX=0.
      WRITE (7,11)
      CALL PLOTR(SCANNR, ETHER,KM,XNAME,YNAM4,YMIN,YMAX,0)
285      CALL REALIO(6H YMIN,YMIN,1)
      CALL REALIO(6H YMAX,YMAX,1)

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      YMIN=YMAX=C.
      WRITE (7,11)
      CALL PLOTR(SCANNR, XFOUR,KM,XNAME,YNAM5,YMIN,YMAX,0)
      CALL REALIO(6H YMIN,YMIN,1)
290  CALL REALIO(6H YMAX,YMAX,1)
      IF (NS.LC.6) GO TO 1065
      WRITE (7,11)
      YMIN=YMAX=0.
      CALL PLOTR(SCANNR, EBETA,KM,XNAME,YNAM7,YMIN,YMAX,0)
295  CALL REALIO(6H YMIN,YMIN,1)
      CALL REALIO(6H YMAX,YMAX,1)
      YMIN=YMAX=0.
      WRITE (7,11)
      CALL PLOTR(SCANNR, EFSC,KM,XNAME,YNAM8,YMIN,YMAX,0)
300  CALL REALIO(6H YMIN,YMIN,1)
      CALL REALIO(6H YMAX,YMAX,1)
1065 CONTINUE
      IF (.NOT.FILOUT) RETURN
      WRITE (7,11)
305  WRITE (7,1070) (DATOUT(I),I=1,2)
1070  FORMAT(13H OUTPUT FILE ,2A10,1H:/)
      WRITE (7,1072) DOUT,DELT,MTIMES,LGMAX,KM,TODAY,JBNAM
1072  FORMAT(1H ,A10,8X,G13.6,5X,3(5X,I3,10X),A10,8X,A10/)
      WRITE (7,1074) IDENT5,KSTART
310 1074  FORMAT(1H ,6(1X,A8,9X),I3/)
      WRITE (7,1076) NRUN,DSNRDB,RHO,BETA,FSC,BHLS,BRCVR,THESEP
1076  FORMAT(1H ,I2,3X,7(3X,G12.6)/)
      IKM=MIN0(35,KM-9)
      DO 1077 I=1,IKM
315 1077  WRITE (7,1078) EALFA(I),ETHET(I),EALFR(I),ETHER(I),XFOUR(I)
1078  FORMAT(1H ,5(G13.6,5X))
      DO 1079 I=1,5
1079  WRITE (7,1080)
320 1080  FORMAT(1H,5(6X,1H.,11X))
      KM3=KM-3
      DO 1081 I=KM3,KM
1081  WRITE (7,1078) EALFA(I),ETHET(I),EALFR(I),ETHER(I),XFOUR(I)
      WRITE (7,1063) RHOMAX,DTHD,TDRO,BETA0,FSC0,EBETA0,EBETA(KM),EFSC0,
      CEFSC(KM)
325 1083  FORMAT (1H0,9(G12.6,2X))
      WRITE (17) DOUT,DELT,MTIMES,LGMAX,KM,TODAY,JBNAM
      WRITE (17) IDENT5,KSTART
      WRITE (17) NRUN,DSNRDB,RHO,BETA,FSC,BHLS,BRCVR,THESEP
      DO 1090 I=1,KM
330 1090  WRITE (17) EALFA(I),ETHET(I),EALFR(I),ETHER(I),XFOUR(I)
1090  CONTINUE
      WRITE (17) RHOMAX,DTHD,TDRO,BETA0,FSC0,EBETA0,EBETA(KM),EFSC0,EFSC(
      CKM)
335  REWIND 17
      IX=IATTACH(6LTAPE20,DATOUT)
      CALL RETURN(6LTAPE20)
      IF (IX.NE.0) GO TO 1095
      IX=ICATALO(6LTAPE17,DATOUT,2LPR,8RHIGHFILL,2LRP,365)
      GO TO 1096
340 1095  IX=ICATALO(6LTAPE17,DATOUT,2LXR,8RHIGHFILL,2LRP,365)
1096  IF (IX.NE.0) CALL INTIO(6HIX(CA),IX,1,1)
      IF (IX.NE.0) STOP OUTPUT FILE CATALOG NOT SATISFACTORY#

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      CALL RETURN(6LTAPE17)
      WRITE (7,1099) (DATOUT(I),I=1,2)
345      FORMAT(13HCOUTPUT FILE ,2A10,33H IS WRITTEN, CATALOGED AND CLOSED)
      RETURN
      C
      C*****
      C
350      1100 CONTINUE
      C THIS SAVES/PROCESSES/OUTPUTS DATA FROM THE (MSET)-TH SERIES OF
      CLGMAX SETS OF KM SCANS
      RETURN
      C
355      C*****
      C
      1200 CONTINUE
      C THIS EFFECTS CLOSURE OF THE SIMULATION RUN
      WRITE (7,11)
360      RETURN
      C*****
      C
      C
      END

```

440JOB CH STORAGE USED 6.147 SECONDS

A-8

SUBROUTINE CONTRL(ISW)

C THIS CONDUCTS THE MLS SIMULATION THROUGH A  
C CROSSING MULTIPATH SCENARIO

5

REAL LAMDA  
INTEGER XNAME(2),YNAME(2),DATIN(4),DATOUT(4),DOUT  
INTEGER TITLE1(3),TITLE2(2,2),FUNCTN(2)  
LOGICAL NOKLNN,NOLDE,NOAC,KALMAN,LOE,TETHRD,HORE,NFIRST,ADAPTIV  
COMMON/IODATA/ISIM,IPHLS,IRCVR,IADAP,ITETHR,IPOPT  
COMMON/RCVR00/THAMAX,THAMIN,TS,TR,OMEGA,TF  
COMMON/RCVR01/NGMIN,NGMAX,DELBL,NGM,IR,IAE  
COMMON/RCVR02/RHOMAX,DTHO,TDRD,BO,WSCO,NSD(4),NGD(4)  
COMMON/RCVR03/PI,F(8,8),FL25(4),FSAMP,K,KH,TETHRD,NG,NS,JH  
COMMON/RCVR04/DELT,ED(8),GGGT(8,8),H(5,8),ICOUNT,SIGMA  
COMMON/RCVR05/NOLDE,NOKLNN,NOAC,GAMAES(5),RDIAG(5),PHDIAG(8)  
COMMON/RCVR06/PPDIAG(8),RHAT(5,5),PHI(5,5),PA(8,8),LAMDA(5)  
COMMON/RCVR07/T(130),V(130)  
COMMON/RCVR08/XSLOE(8),ESLOE(8),ES(8)  
COMMON/RCVR09/BRCVR,BB,PDCRIT,CC  
COMMON/RCVR10/XS1(8),XS(8)  
COMMON/MLS000/ALFA,THE,THEDOT,ALFAR,THR,THRDOT,B,WSC  
COMMON/MLS001/CSNRT,CSNRF,DSNRDB,RHD,BETA,FSC,LGNAX  
COMMON/MLS002/DCSNR,CSNR,LG,TPKT,TPKF  
COMMON/MLS003/FL10AE(4,2),FL10(4),DELTAT(2),XO(8,2),YO(4,2)  
COMMON/MLS004/BMLS,BBB,MTINES,MSET,HORE  
DIMENSION CSNRTO(100),X(8),THESE(100),THESE(100),ABBORT(100)  
DIMENSION IDNRS(6),IDASCI(18),IDENTS(6),CSNRFR(100)  
EQUIVALENCE (ALFA,X(1)),(ISIM,IDNRS(1)),(DOUT,DATOUT(2))  
DATA ABORT/1HA/,SPACE/1H/,NFIRST/.FALSE./,ADAPTIV/.TRUE./  
DATA DATIN/10HMLSSIMDATA,10H100000F000,2\*0/  
DATA DATOUT/10HMLSSIMDATA,3\*0/  
DATA IDASCI/7HCRDSSMP,7HRMSE(T),7HRMSE(B),8H PMLS1 ,8H PMLS2 ,  
\*8H PMLS3 ,8H THRHLD ,8H OPTIML ,8H SUBOPT ,8H -3 DB ,8HADAPTIV ,  
\*8HNONADAP ,8HUNTETHRD,8HTETHERED,2H ,8H POPT1 ,8H POPT2 ,  
\*8H POPT3 /  
DATA NSTART/15/,IRSIGN/1/  
DATA TITLE1/6H X(2) ,6HX2-X5 ,6HXS(2) /  
DATA TITLE2/6HFIL ER,6HX2-XS2,6HX2-XS2,6HSQRP22/  
DATA FUNCTN/7HAZINUTH,7HELEVAT. /  
DATA XNAME/8HTHETASEP,8HDEGREES /,YNAME/8HTHES ERR,8HDEGREES /

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GO TO (100,200,300,400,500,600,700,800,900,1000,1100,1200),ISW  
FORMAT(1H )  
10 FORMAT(9(/))  
11 FORMAT(1H1)  
C \*\*\*\*\*  
C  
100 CONTINUE  
C THIS IDENTIFIES THE SCENARIO AND REINITIALIZES, AS NECESSARY,  
CTHE FOLLOWING RECEIVER PARANETERS  
CSIGMA,IAE,DSNRDB,RHD,FSC,BETA,JH,BMLS  
IF(NFIRST) GO TO 155  
NFIRST=.TRUE.  
JBNAM=JOBNAME(I)  
ISIM=1

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-----
      IMOD=1
      WRITE (7,110)
60      110  FORMAT (28H1CROSSING-MULTIPATH SCENARIO/)
          GO TO 122
          COLD IX=IATTACH(6LTAPE15,DATIN)
          COLD IF (IX.NE.0) CALL INTIO(6HIX(AT),IX,1,1)
          COLD IF (IX.NE.0) STOP#INPUT FILE ATTACH NOT SATISFACTORY#
65      COLD WRITE(7,120) (DATIN(I),I=1,2)
          120  FORMAT(23H THIS READS INPUT FILE ,2A10/)
          122  CONTINUE
          *   NULL TRANSFER STATEMENT -- TRANSFER IGNORED
          CALL INTIO(6HNSTART,NSTART,100,0)
          NSTOP=NSTART
70      CALL INTIO(6H NSTOP,NSTOP,100,0)
          CALL LOGIO(6HTETHRD,TETHRD,0)
          IF (IRCVR.EQ.1) GO TO 125
          CALL LOGIO(6HADAPTV,ADAPTV,0)
          125  CONTINUE
75      IF (TETHRD) ITETHR=2
          IF (ADAPTV) GO TO 135
          IRSIGN=-1
          IADAP=3
          135  CONTINUE
80      DO 145 I=2,6
          IASC=3*(I-1)+IDNRS(I)
          IDENTS(I)=IDASCI(IASC)
          145  CONTINUE
          ENCODE(8,150,IDENTS(1)) IDASCI(ISIN),IMOD
85      150  FORMAT(A7,I1)
          WRITE (7,152) IDNRS,IMOD
          152  FORMAT (1H ,6I1,1X,I1/)
          WRITE (7,153) IDENTS
          153  FORMAT (1H ,A8)
90      155  CONTINUE
          READ(10,160) NRUN,DSNRDB,RHO,BETA,FSC,BHLS,BRCVR
          160  FORMAT(15,6G10.3)
          IF (NRUN.LT.NSTART) GO TO 155
          IF (NRUN.GE.NSTOP) MDRE=.FALSE.
95      RETURN
          C
          C*****
          C
          200  CONTINUE
          C THIS OUTPUTS BASIC SIMULATION DATA OF INTEREST, SUCH AS
          C THE ANGLE FUNCTION, INITIAL STATE, ETC.
          WRITE(7,210) NRUN,DSNRDB,RHO,BETA,FSC,BHLS,BRCVR
          210  FORMAT(5H1NRUN,12X,6HDSNRDB,16X,3HRHO,16X,4HBETA,17X,3HFSC,16X,
          *4HBHLS,15X,5HBRCVR/1H0,I4,6(10X,G10.3))
          IF (NRUN.LE.9) ENCODE(10,220,DOUT) IDNRS,1HU,IMOD,1H0,NRUN
          105  220  FORMAT(6I1,A1,I1,A1,I1)
          IF (NRUN.GE.10) ENCODE(10,230,DOUT) IDNRS,1HU,IMOD,NRUN
          230  FORMAT(6I1,A1,I1,I2)
          IX=IREQST(6LTAPE17,3L*PF)
          110  IF (IX.NE.0) CALL INTIO(6HIX(RQ),IX,1,1)
          IF (IX.NE.0) STOP#OUTPUT FILE REQUEST NOT SATISFACTORY#
          WRITE(7,240) (DATOUT(I),I=1,2)
          240  FORMAT(25H0THIS WRITES OUTPUT FILE ,2A10)
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115      CALL DATE(TODAY)
        WRITE (7,250) FUNCTN (IAE),IAE
        250  FORMAT (1H0,A7,15H FUNCTION (IAE=,I1,1H))
        WRITE (7,260) ((I,X(I)),I=1,8)
        260  FORMAT (15H0INITIAL STATE://(3H X(,I1,4H) = ,G13,6))
        WRITE(7,270) IDENT5(2)
120      270  FORMAT(1H0,A7)
        RETURN
C
C*****
C
125      300  CONTINUE
C THIS IDENTIFIES THE BASIC RECEIVER STRUCTURE (THRHLD,OPT,SUBOPT)
C AND REINITIALIZES, AS NECESSARY, THE FOLLOWING RCVR DATA
CIR (NEGATE ONLY), NOAC,NOKLMN,NOLDE,BRCVR,DELBL,TETHRD
        ITIT=MINO(IRCVR,2)
130      C
C NEGATE IR WITH THE FOLLOWING FOR NONADAPTIVE RECEIVER
        IF(IRSIGN.LT.0) IR=-IR
C
C      RETURN
135      C
C*****
C
        400  CONTINUE
C THIS OUTPUTS BASIC RECEIVER DATA OF INTEREST
        WRITE(7,410) (IDENTS(I),I=3,4),IR,NG,NS
140      410  FORMAT (1H0,A8,4HRCVR/1H0,A8,6HDESIGN/5H (IR=,I2,4H,NG=,I1,
        *      4H,NS=,I1,1H))
        WRITE(7,420) (IDENTS(I),I=5,6)
        420  FORMAT(1H0,A8/1H0,A7/)
145      -RETURN
C
C*****
C
        500  CONTINUE
C THIS SETS-UP THE MSET-LOOP
        ICOUNT=0
        RETURN
C
C*****
155      C
        600  CONTINUE
C THIS SETS-UP THE LG-LOOP FOR THE (MSET)-TH SERIES OF SETS
        RETURN
C
C*****
160      C
        700  CONTINUE
C THIS SETS-UP THE K-LOOP FOR THE (LG)-TH SET OF KM SCANS
        CALL INTIO(6H KM,KM,1,1)
        WRITE(7,710) (TITLE1(I),I=1,3),(TITLE2(I,ITIT),I=1,2)
165      710  FORMAT (4H0 K,6X,5HCSNRT,6X,5HCSNRF,5(5X,A6,4X)/)
        EMEAN=0.
        EMS=0.
        LASTCT=0
170      RETURN

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C
C*****
C
175 C 800 CONTINUE
C THIS INITIALIZES THE K-TH SCAN
SEP=SPACE
RETURN
C
180 C*****
C
900 CONTINUE
C THIS SAVES/PREPROCESSES DATA FROM THE K-TH SCAN
IF(ICOUNT.NE.LASTCT) SEP=ABORT
THERR=X(2)-XS(2)
185 COLB=THERR
DTHE=X(2)-X(5)
IF (IRCVR .NE. 1) COLB=SQRT(PPDIAG(2))
IF (IRCVR .EQ. 1) CALL DFLTR1(COLB,THERR,FL10)
WRITE(7,910) K,CSNRT,CSNRF,X(2),DTHE,XS(2),SEP,THERR,COLB
190 910 FORMAT (1H ,I3,2(2X,F9.3),3(2X,G13.6),1X,A1,1X,G13.6,2X,G13.6)
CSNRTO(K)=CSNRT
CSNRFR(K)=CSNRF
THESEP(K)=DTHE
195 THESER(K)=THERR
ABORT(K)=SEP
LASTCT=ICOUNT
EMEAN=EMEAN+THERR
EMS=EMS+THERR**2
RETURN
200 C
C*****
C
1000 CONTINUE
C THIS SAVES/PROCESSES/OUTPUTS DATA FROM THE (LG)-TH SET OF KH SCANS
205 EMEAN=EMEAN/KH
EMS=EMS/KH
ERMS=SQRT(EMS)
ESTDEV=SQRT(EMS-EMEAN**2)
XW=ICOUNT
210 TCOUNT=100.*XW/KH
WRITE(7,1010)
1010 FORMAT (31H0THETA-ERROR SAMPLE STATISTICS:)
IF (IRCVR .EQ. 1) WRITE(7,1020)
215 1020 FORMAT (17H (FILTERED ERROR))
WRITE(7,1030) EMEAN,ERMS,ESTDEV
1030 FORMAT (10H0 EMEAN = ,G13.6/10H ERMS = ,G13.6/
*10H ESTDEV = ,G13.6)
IF (IRCVR .EQ. 1) WRITE(7,1040) TCOUNT
220 1040 FORMAT (//1H0,F7.2,22HZ OF SCANS ARE ABORTED)
YMIN=YMAX=0.
WRITE (7,11)
CALL PLOTR(THESEP,THESER,KH,XNAME,YNAME,YMIN,YMAX,0)
WRITE (7,11)
CALL REALID(6H YMIN,YMIN,1)
225 CALL REALID(6H YMAX,YMAX,1)
IF (IRCVR .NE. 1) WRITE(7,1060) (GQGT(I,I),I=1,NS)
1060 FORMAT (10(//),35H ON LAST SCAN, DIAGONAL OF GQGT WAS/

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*1H ,G11.4,7(1H,G11.4))
WRITE(7,11)
230 1070 WRITE(7,1070) (DATOUT(I),I=1,2)
      FORMAT(13H OUTPUT FILE ,2A10,1H://)
      WRITE(7,1072) DOUT,DELTA,MTIMES, LGMAX, KM, TODAY, JBNAM
235 1072 FORMAT(1H ,A10,8X,G13.6,5X,3(5X,I3,10X),A10,8X,A10/)
      WRITE(7,1074) IDENT5
      FORMAT(1H ,6(1X,A8,9X)/)
      WRITE(7,1076) NRUN,DSNRDB,RHO,BETA,FSC,BHLS,BRCVR
240 1076 FORMAT(1H ,5X,I2,6X,6(5X,G13.6)/)
      IKM=MINO(35,KM-9)
      DO 1077 I=1,IKM
240 1077 WRITE(7,1078) CSNRTO(I),CSNRFR(I),THESER(I),ABBORT(I),THESEP(I),I
      1078 FORMAT(1H ,3(G13.6,5X),6X,A1,11X,G13.6,5X,I7)
      DO 1079 I=1,5
      1079 WRITE(7,1080)
      1080 FORMAT(1H,6(6X,1H,,11X))
245 1080 KM3=KM-3
      DO 1081 I=KM3,KM
245 1081 WRITE(7,1078) CSNRTO(I),CSNRFR(I),THESER(I),ABBORT(I),THESEP(I),I
      1082 WRITE(7,1082) EMEAN,ERMS,ESTDEV,TCOUNT,YMIN,YMAX
      1082 FORMAT(1H,6(G13.6,5X)/)
250 1082 WRITE(17) DOUT,DELTA,MTIMES, LGMAX, KM, TODAY, JBNAM
      1082 WRITE(17) IDENT5
      1082 WRITE(17) NRUN,DSNRDB,RHO,BETA,FSC,BHLS,BRCVR
      DO 1090 I=1,KM
255 1090 WRITE(17) CSNRTO(I),CSNRFR(I),THESER(I),ABBORT(I),THESEP(I),I
      1090 CONTINUE
      1090 WRITE(17) EMEAN,ERMS,ESTDEV,TCOUNT,YMIN,YMAX
      1090 REWIND 17
      1090 IX=IATTACH(6LTAPE20,DATOUT)
      1090 CALL RETURN(6LTAPE20)
260 1090 IF(IX.NE.0) GO TO 1095
      1090 IX=ICATALD(6LTAPE17,DATOUT,2LPW,8RHIGHFILL,2LRP,365)
      1090 GO TO 1096
      1095 IX=ICATALD(6LTAPE17,DATOUT,2LXR,8RHIGHFILL,2LRP,365)
      1096 IF(IX.NE.0) CALL INTID(6HIX(CA),IX,1,1)
265 1096 IF(IX.NE.0) STOP OUTPUT FILE CATALOG NOT SATISFACTORY#
      1096 CALL RETURN(6LTAPE17)
      1096 WRITE (7,1099) (DATOUT(I),I=1,2)
      1099 FORMAT(13HOUTPUT FILE ,2A10,3H IS WRITTEN, CATALOGED AND CLOSED)
      1099 RETURN
270 C
      C*****
      C
      1100 CONTINUE
      C THIS SAVES/PROCESSES/OUTPUTS DATA FROM THE (MSET)-TH SERIES OF
275 CLGMAX SETS OF KM-SCANS
      RETURN
      C
      C*****
      C
      1200 CONTINUE
      C THIS EFFECTS CLOSURE OF THE SIMULATION RUN
      RETURN
      C
      C*****

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C

END

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1      SUBROUTINE CONTRL(ISW)
      C
      C THIS CONDUCTS THE MLS SIMULATION THROUGH A
      C RMSE VS. BRATIO ( = BRCVR/BMLS).
      C
5      REAL LAMDA
      INTEGER XNAME1(2),YNAME1(2),YNAM1(2,9)
      INTEGER XNAME(2),YNAME(2),DATIN(4),DATOUT(4),DOUT
      INTEGER TITLE1(9),FUNCTN(2)
10     LOGICAL NOKLMN,NOLQE,NOAC,KALMAN,LOE,TETHRD,MORE,NFIRST,ADAPTIV,
      CFILEIN,FILOUT
      COMMON/IODATA/ISIM,IPMLS,IRCVR,IADAP,ITETHR,IPOPT
      COMMON/RCVROO/THAMAX,THAMIN,TS,TR,OMEGA,TF
      COMMON/RCVRO1/NGMIN,NGMAX,DELBL,NGH,IR,IAE
15     COMMON/RCVRO2/RHOMAX,DTHO,TDRD,BO,WSCD,NSO(4),NGO(4)
      COMMON/RCVRO3/PI,F(8,8),FL25(4),FSAMP,K,KH,TETHRD,NG,NS,JH
      COMMON/RCVRO4/DELTA,EO(8),GGGT(8,8),H(5,8),ICOUNT,SIGMA
      COMMON/RCVRO5/NOLQE,NOKLMN,NOAC,GAMAES(5),RODIAG(5),PHDIAG(8)
      COMMON/RCVRO6/PPDIAG(8),RMT(5,5),PHI(5,5),PA(8,8),LAMDA(5)
20     COMMON/RCVRO7/T(130),V(130)
      COMMON/RCVRO8/XSLOE(8),ESLOE(8),ES(8)
      COMMON/RCVRO9/BRCVR,BB,PDCRIT,CC
      COMMON/RCVRO10/XS1(8),XS(8)
      COMMON/MLS000/ALFA,THE,THEDQT,ALFAR,THR,THRDOT,B,WSC
      COMMON/MLS001/CSNRT,CSNRF,OSNRDB,RHD,BETA,FSC,LGHAX
25     COMMON/MLS002/DCSNR,CSNR,LG,TPKT,TPKF
      COMMON/MLS003/FL10AE(4,2),FL10(4),DELTAT(2),XO(8,2),YO(4,2)
      COMMON/MLS004/BMLS,BBB,HTIMES,MSET,MORE
      DIMENSION X(8),THESER(115),XDATUM(115),EEME(13),EERM(13)
30     DIMENSION IDNRS(6),IDASCI(20),IDENTS(6),EEST(13),TTCO(13),YYHI(13)
      DIMENSION YYMA(13)
      DIMENSION BRATIO(13)
      DIMENSION EMEA(13,9),EERMS(13,9),EESTD(13,9)
      DIMENSION EMEAN(9),EMS(9),ERMS(9),ESD(9)
35     EQUIVALENCE (EEME(1),EMEA(1,2)),(EERM(1),EERMS(1,2)),
      *(EEST(1),EESTD(1,2))
      EQUIVALENCE (THERR,ES(2))
      EQUIVALENCE (ALFA,X(1)),(ISIM,IDNRS(1)),(DOUT,DATOUT(2))
      DATA YNAM1/8HALF RMSE,8H ,8HTHE RMSE,8HDEGREES ,
40     *8HTDT RMSE,8HDEG/SEC ,8HALR RMSE,8H ,8HTHR RMSE,
      *8HDEGREES ,8HTRD RMSE,8HDEG/SEC ,8HBET RMSE,8HDEGREES ,
      *8HFSC RMSE,8H HZ ,8HFSCORMSE,8H HZ/SEC /
      DATA ABORT/1HA/,SPACE/1H /,NFIRST/,FALSE./,ADAPTIV/.TRUE./
45     DATA DATIN/10HMLSSIMDATA,10H200000F000,2*0/
      DATA DATOUT/10HMLSSIMDATA,3*0/
      DATA IDASCI/7HCROSSMP,7HRMSE(T),7HRMSE(B),7HRMSE(F),7H
      *8H PMLS1 ,8H PMLS2 ,
      *8H PMLS3 ,8H THRLD ,8H OPTIML ,8H SUBOPT ,8H -3 DB ,8HADAPTIV ,
      *8HNONADAP ,8HUNTETHRD,8HTETHERED,2H ,8H POPT1 ,8H POPT2 ,
50     *8H POPT3 /
      DATA NSTART/3/,IRSIGN/1/,KSTART/11/,BRARAT/10./,FILEIN
      */.FALSE./,FILOUT/.TRUE./
      DATA TITLE1/6H ALFA ,6H THETA,6HTHEDQT,6H ALFAR,6HTHETAR,6HTHRODT
      C,6H B ,6H WSC ,6HWSCDOT/
55     DATA XNAME/8H BETA ,8HDEGREES /,YNAME/8HTHES ERR,8HDEGREES /
      DATA XNAME1/8H BRATIO ,8H /
      DATA FUNCTN/7HAZIMUTH,7HELEVAT./

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C
60 1 GO TO (100,200,300,400,500,600,700,800,900,1000,1100,1200),ISW
    10 FORMAT(1H )
    11 FORMAT(9(/))
    111 FORMAT (1H1)
C
65 C*****
C
100 CONTINUE
C THIS IDENTIFIES THE SCENARIO AND REINITIALIZES, AS NECESSARY,
CTHE FOLLOWING RECEIVER PARAMETERS
CSIGMA,IAE,DSNRDB,RHO,PSC,BETA,JH,BMLS
70 IF(NFIRST) GO TO 155
    NOAC=.TRUE.
    NFIRST=.TRUE.
    JBNAM=JOBNAME(I)
75 ISIM=3
    IMOD=1
110 WRITE (7,110)
    FORMAT(30H1RMSE VS.BRATIO = BRCVR/BMLS SCENARIO/)
    CALL LOGIO(6HFILEIN,FILEIN,0)
    IF (.NOT.FILEIN) NSTART=0
80 IF(.NOT.FILEIN) GO TO 122
    IX=IATTACH(6LTAPE15,DATIN)
    IF(IX.NE.0) CALL INTIO(6HIX(AT),IX,1,1)
    IF(IX.NE.0) STOP#INPUT FILE ATTACH NOT SATISFACTORY#
    WRITE(7,120) (DATIN(I),I=1,2)
85 120 FORMAT(23H THIS READS INPUT FILE ,2A10/)
    122 CALL LOGIO(6HFILOUT,FILOUT,0)
    CALL INTIO(6HNSTART,NSTART,100,0)
    NSTOP=NSTART
    CALL INTIO(6H NSTOP,NSTOP,100,0)
90 CALL LOGIO(6HTETHRD,TETHRD,0)
    IF(IRCVR.EQ.1) GO TO 125
    CALL LOGIO(6HADAPT,ADAPT,0)
125 CONTINUE
    IF(TETHRD) ITETHR=2
95 IF(ADAPT) GO TO 135
    IRSIGN=-1
    IADAP=3
135 CONTINUE
    DO 145 I=2,6
100 IASC=3*(I-1)+IDNRS(I)+2
    IDENTS(I)=IDASCI(IASC)
145 CONTINUE
    ENCODE(8,150,IDENTS(1)) IDASCI(ISIM),IMOD
150 FORMAT(A7,I1)
105 152 WRITE (7,152) IDNRS,IMOD
    152 FORMAT (1H ,6I1,1X,I1/)
    WRITE (7,153) IDENTS
153 FORMAT (1H ,A8)
    CALL INTIO(6H LGMAX,LGMAX,13,0)
110 CALL INTIO(6H KM,KH,115,0)
    CALL REALIO(6HBRARAT,BRARAT,0)
    KSTART=MIND(KH,KSTART)
    BRATIO(1)=1.
    BRATMX=SQRT(BRARAT)

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115      ROOT=1./ (LGMAX-1)
        IF (LGMAX.LE.1) GO TO 156
        DD 154 I=1, LGMAX
154      BRATIO(I)=BRATHX** (2.*ROOT*(I-1)-1.)
156      CONTINUE
120      KHNET=KH-KSTART+1
        FSCMIN=1./ (DELTAT(IAE)*KHNET)
        NRUN=NSTART-1
        DSNRDB=20.
        RHO=0.5
125      BETA=45.
        IFS=1
        TSEP=1.
155      CONTINUE
        IF (FILEIN) GOTO 158
130      NRUN=NRUN+1
        WRITE(7,11)
        CALL INTIO(6H NRUN,NRUN,1,1)
        CALL REALIO(6HDSNRDB,DSNRDB,0)
        CALL REALIO(6H RHO,RHO,0)
135      CALL REALIO(6H BETA,BETA,0)
        CALL INTIO(6H IFS,IFS,100,0)
        CALL REALIO(6H TSEP,TSEP,0)
        GOTO 167
158      CONTINUE
140      READ(15,160) NRUN,DSNRDB,RHO,BETA,IFS,TSEP
        IF (EOF(15))170,165
160      FORMAT(I5,3G10.3,5X,I5,2G10.3)
165      IF (NRUN.LT.NSTART) GO TO 158
167      IF (NRUN.GE.NSTOP) MORE=.FALSE.
145      FSC=IFS*FSCMIN
        XO(5,IAE)=XO(2,IAE)-TSEP
        XO(3,IAE)=0.
        XO(6,IAE)=0.
        RETURN
150      170 STOP#EOF REACHED ON INPUT FILE#
        C
        C*****
        C
200      CONTINUE
155      C THIS OUTPUTS BASIC SIMULATION DATA OF INTEREST, SUCH AS
        C THE ANGLE FUNCTION, INITIAL STATE, ETC.
        WRITE(7,210) NRUN,DSNRDB,RHO,BETA,IFS,TSEP
210      FORMAT(5HNRUN,12X,6HDSNRDB,16X,3HRHO,16X,4HBETA,16X,4HIFSC,16X,
        *4HTSEP/1H0,I4,3(10X,610.3),12X,I5,3X,
160      *(10X,610.3))
        IF (.NOT.FILOUT) GOTO 245
        IF (NRUN.LE.9) ENCODE(10,220,DOUT) IDNRS,1HU,IMOD,1H0,NRUN
220      FORMAT(6I1,A1,I1,A1,I1)
        IF (NRUN.GE.10) ENCODE(10,230,DOUT) IDNRS,1HU,IMOD,NRUN
165      230      FORMAT(6I1,A1,I1,I2)
        IX=IREQST(6LTAPE17,3L*PF)
        IF (IX.NE.0) CALL INTIO(6HIX(RQ),IX,1,1)
        IF (IX.NE.0) STOP#OUTPUT FILE REQUEST NOT SATISFACTORY#
170      240      WRITE(7,240) (DATOUT(I),I=1,2)
        245      FORMAT(25H0THIS WRITES OUTPUT FILE ;2A10)
        CALL DATE(TODAY)

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```

      WRITE (7,250) FUNCTN (IAE),IAE
250  FORMAT (1H0,A7,15H FUNCTION (IAE=>I1,1H))
      WRITE (7,260) ((I,X(I)),I=1,8)
175  260  FORMAT (15H0INITIAL STATE:/(3H X(,I1,4H) = ,G13.6))
      WRITE(7,270) IDENT5(2)
      270  FORMAT(1H0,A7)
      RETURN
C
180  C*****
C
300  CONTINUE
C THIS IDENTIFIES THE BASIC RECEIVER STRUCTURE (THRHLD,DPT,SUBOPT)
C AND REINITIALIZES, AS NECESSARY, THE FOLLOWING RCVR DATA
185  CIR (NEGATE ONLY), NOAC,NOKLMN,NOLOE,BRCVR,DELBL,TETHRO
      ITIT=MINO(IRCVR,2)
C
C NEGATE IR WITH THE FOLLOWING FOR NONADAPTIVE RECEIVER
190  IR=ISIGN(IR,IRSIGN)
C
      RETURN
C
C*****
400  CONTINUE
195  C THIS OUTPUTS BASIC RECEIVER DATA OF INTEREST
      WRITE(7,410) (IDENTS(I),I=3,4),IR,NG,NS
410  FORMAT (1H0,A8,4HRCVR/1H0,A8,6HDESIGN/5H (IR=,I2,4H,NG=,I1,
      *      4H,NS=,I1,1H))
      WRITE(7,420) (IDENTS(I),I=5,6)
200  420  FORMAT(1H0,A8/1H0,A7/)
      RETURN
C
C*****
205  C
500  CONTINUE
C THIS SETS-UP THE MSET-LOOP
      ICDUNT=0
      DO 510 I=1,LGMAX
210  510  YYMI(I)=1.E322
      YYMA(I)=-1.E322
      RETURN
C
C*****
215  C
600  CONTINUE
C THIS SETS-UP THE LG-LOOP FOR THE (MSET)-TH SERIES OF SETS
      RETURN
C
C*****
220  C
700  CONTINUE
C THIS SETS-UP THE K-LOOP FOR THE (LG)-TH SET OF KM SCANS
      BMLS=AMAX1(1.,1./BRATIO(LG))
      BBB=2.4/BMLS
225  BRCVR=AMAX1(BRATIO(LG),1.)
      BB=2.4/BRCVR
      PDCRIT=PI*BB/8.
      CC=PI*PDCRIT

```

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```

230      X(7)=X0(7,IAE)
      DUM=GAUSS(1.0)
      WRITE(7,11)
      CALL INTIO(6H NRUN,NRUN,1,1)
      WRITE(7,705) LG,BRATIO(LG),BHLS,BRCVR
235      FORMAT(1H ,4X,3HLG=,I2,5X,9HBRATIO = ,G12.5/8H "BHLS" = ,G12.5,5X,
      *8HBRCVR = ,G12.5)
      CALL INTIO(6H KM,KM,1,1)
      WRITE(7,710) (TITLE1(I),I=1,NS)
240      FORMAT(6H0 K,4X,5HCSNRT,4X,5HQTY ,9(3X,A6,2X))
      DO 712 I=1,NS
      EMEAN(I)=0.
245      EMS(I)=0.
      LASTCT=0
      ICOUNT=0
      DO 730 IPA=1,NS
      DO 720 JPA=1,NS
      PA(IPA,JPA)=0.
      720 CONTINUE
      730 CONTINUE
      RETURN
250      C
      C*****
      C
      800 CONTINUE
      C THIS INITIALIZES THE K-TH SCAN
255      SEP=SPACE
      RETURN
      C
      C*****
      C
260      900 CONTINUE
      C THIS SAVES/PREPROCESSES DATA FROM THE K-TH SCAN
      IF(ICOUNT.NE.LASTCT) SEP=ABORT
      DO 905 I=1,NS
265      905 ES(I)=X(I)-XS(I)
      IF(NS.GE.7) ES(7)=ABS(X(7))-ABS(XS(7))
      IF(NS.GE.8) ES(8)=ABS(X(8))-ABS(XS(8))
      BETTA=(180./PI)*X(7)
      COLB=THERR
270      IF(IRCVR.NE.1) COLB=SQRT(PPDIAG(2))
      IF(IRCVR.EQ.1) CALL DFLTR1(COLB,THERR,FL10)
      IF((NRUN.EQ.NSTART.AND.LG.EQ.1).OR.(K.EQ.KM)) GOTO 906
      GO TO 950
      906 WRITE(7,910) K,CSNRT,(X(I),I=1,NS)
      910 FORMAT(3H0 ,I3,2X,G10.3,5H X= ,2X,9(G10.3,1X))
275      WRITE(7,920) (XS(I),I=1,NS)
      920 FORMAT(18X,5H XS= ,2X,9(G10.3,1X))
      WRITE(7,930) (ES(I),I=1,NS)
      930 FORMAT(18X,5H ES= ,2X,9(G10.3,1X))
      IF(IRCVR.EQ.1) WRITE(7,940) COLB
280      940 FORMAT(8X,15HUNFIL. ES(2)= ,13X,G10.3)
      950 XDATUM(K)=BETTA
      THESER(K)=THERR
      LASTCT=ICOUNT
      IF(K.LT.KSTART) RETURN
285      DO 960 I=1,NS

```

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```

          EMEAN(I)=EMEAN(I)+ES(I)
          EMS(I)=EMS(I)+ES(I)**2
          RETURN
290      C
          C*****
          C
          1000 CONTINUE
          C THIS SAVES/PROCESSES/OUTPUTS DATA FROM THE (LG)-TH SET OF KH SCANS
          DO 1005 I=1,NS
295      EMEAN(I)=EMEAN(I)/KMNET
          EMS(I)=EMS(I)/KMNET
          ERMS(I)=SQRT(EMS(I))
          ESD(I)=SQRT(EMS(I)-EMEAN(I)**2)
          1005 CONTINUE
300      XW=ICDUNT
          TCOUNT=100.*XW/KH
          WRITE(7,1009)
          1009 FORMAT(3(/))
          WRITE(7,1010)KMNET
305      1010 FORMAT(5X,26HERROR SAMPLE STATISTICS: (,I3,9H SAMPLES))
          IF(IRCVR.EQ.1) WRITE(7,1015)
          1015 FORMAT(5X,31HTHRESHOLD RCVR (FILTERED ERROR))
          WRITE(7,1020)(TITLE1(I),I=1,NS)
          1020 FORMAT(1H0,20X,4HQTY ,9(3X,A6,2X))
310      WRITE(7,1030)(EMEAN(I),I=1,NS)
          1030 FORMAT(1H0,16X,8HEMEAN = ,9(G10.3,1X))
          WRITE(7,1040)(ERMS(I),I=1,NS)
          1040 FORMAT(18X,7HERMS = ,9(G10.3,1X))
          WRITE(7,1050)(ESD(I),I=1,NS)
315      1050 FORMAT(19X,6HESD = ,9(G10.3,1X))
          IF(IRCVR.EQ.1)WRITE(7,1060)TCOUNT
          1060 FORMAT(/1H ,4X,F7.2,22HZ OF SCANS ARE ABORTED)
          IF(IRCVR.NE.1)WRITE(7,1070)(GQGT(I,I),I=1,NS)
          1070 FORMAT(5(/),4X,35H ON LAST SCAN, DIAGONAL OF GQGT WAS/26X
320      C9(G10.3,1X))
          DO 1071 I=1,NS
          EMEA(LG,I)=EMEAN(I)
          EERMS(LG,I)=ERMS(I)
          1071 EESD(LG,I)=ESD(I)
          DO 1072 I=1,KH
325      YYMI(LG)=AMINI(THESER(I),YYMI(LG))
          1072 YYMA(LG)=AMAX1(THESER(I),YYMA(LG))
          TTCO(LG)=TCOUNT
          IF(LG.NE.1) RETURN
          YMIN=YMAX=0.
          WRITE(7,11)
          CALL INTIO(6H NRUN,NRUN,1,1)
          CALL PLOT(XDATUM,THESER,KH,XNAME,YNAME,YMIN,YMAX,0)
          RETURN
335      C
          C*****
          C
          1100 CONTINUE
          C THIS SAVES/PROCESSES/OUTPUTS DATA FROM THE (MSET)-TH SERIES OF
340      CLGMAX SETS OF KH SCANS
          WRITE(7,11)
          CALL INTIO(6H NRUN,NRUN,1,1)

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1110 WRITE(7,1110) 6HBRATIO,(TITLE1(I),I=1,NS)
345 1110 FORMAT(1H0,10X,3HQTY ,9(3X,A6,2X))
      WRITE(7,1120)BRATIO(1),(EEMEA(1,I),I=1,NS)
1120 FORMAT(1H0, 7X,7HEMEAN: ,9(G10.3,1X))
      DO 1130 J=2,LGMAX
1130 WRITE(7,1161)BRATIO(J),(EEMEA(J,I),I=1,NS)
      WRITE(7,1140)BRATIO(1),(EERMS(1,I),I=1,NS)
350 1140 FORMAT(1H0, 8X,6HERMS: ,9(G10.3,1X))
      DO 1150 J=2,LGMAX
1150 WRITE(7,1161)BRATIO(J),(EERMS(J,I),I=1,NS)
      WRITE(7,1160)BRATIO(1),(EESTD(1,I),I=1,NS)
1160 FORMAT(1H0, 8X,6HESTD: ,9(G10.3,1X))
355 1160 DO 1165 J=2,LGMAX
1165 WRITE(7,1161)BRATIO(J),(EESTD(J,I),I=1,NS)
1161 FORMAT(15X,9(G10.3,1X))
      IF (.NOT.FILOUT) GOTO 1199
      WRITE(7,11)
360 1170 WRITE(7,1170) (DATOUT(I),I=1,2)
1170 FORMAT(13H OUTPUT FILE ,2A10,1H:/)
      WRITE(7,1172) DDUT,DELT,MTIMES,LGMAX,KM,TODAY,JBNAH
1172 FORMAT(1H ,A10,8X,G13.6,5X,3(5X,I3,10X),A10,8X,A10/)
      WRITE(7,1174) IDENTS,KSTART
365 1174 FORMAT(1H ,6(1X,A8,9X),6X,I3/)
      WRITE(7,1176) NRUN,DSNR0B,RHO,BETA,FSC,TSEP
1176 FORMAT(1H ,5X,I2,6X,5(5X,G13.6)/)
      DO 1175 LGN=1,LGMAX
1175 WRITE(7,1182) EEME(LGN),EERM(LGN),EEST(LGN),TTCD(LGN),YYMI(LGN),
370 *YYMA(LGN),BRATIO(LGN),LGN
1182 FORMAT(1H ,7(G13.6,5X),I5)
      WRITE(17) DDUT,DELT,MTIMES,LGMAX,KM,TODAY,JBNAH
      WRITE(17) IDENTS,KSTART
      WRITE(17)NRUN,DSNR0B,RHO,BETA,FSC,TSEP
375 1190 DO 1190 LGN=1,LGMAX
1190 WRITE(17) EEME(LGN),EERM(LGN),EEST(LGN),TTCD(LGN),YYMI(LGN),
      *YYMA(LGN),BRATIO(LGN),LGN
      IX=IATTACH(6LTAPE20,DATOUT)
      IF(IX.NE.0) GO TO 1195
380 READ(20) DUM,DUH,IDUM,DUH,DUH,DUH,DUH,DUH
      CALL RETURN(6LTAPE20)
      REWIND 17
      IX=ICATALO(6LTAPE17,DATOUT,2LPW,8RHIGHFILL,2LRP,365)
      GO TO 1196
385 1195 CALL RETURN(6LTAPE20)
      REWIND 17
      IX=ICATALO(6LTAPE17,DATOUT,2LXR,8RHIGHFILL,2LRP,365)
1196 IF(IX.NE.0) CALL INTID(6HIX(CA),IX,1,1)
      IF(IX.NE.0) STOP#OUTPUT FILE CATALOG NOT SAISFACTORY*
390 CALL RETURN(6LTAPE17)
      WRITE(7,1198) (DATOUT(I),I=1,2)
1198 FORMAT(13HOUTPUT FILE ,2A10,3H IS WRITTEN, CATALOGED AND CLOSED)
1199 CONTINUE
      DO 1103 I=1,NS
395 FACTOR=1.
      IF(I.EQ.7) FACTOR=180./PI
      IF(I.EQ.8) FACTOR=.5/PI
      IF(I.EQ.9) FACTOR=.5/PI
      YMIN=0.

```

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```
400          YMAX=0.
           DD 1101 LG1=1,LGHAX
1101      EEME(LG1)=EERMS(LG1,I)*FACTOR
           YNAME1(1)=YNAM1(1,I)
           YNAME1(2)=YNAM1(2,I)
405      K1=MOD(I,2)
           IF(K1.EQ.1)WRITE(7,11)
           IF(K1.EQ.1) CALL INTIO(6H NRUN,NRUN,1,1)
           IF(K1.EQ.0) WRITE(7,10)
           CALL PLOTR(BRATID,EEME,LGHAX,XNAME1,YNAME1,YMIN,YMAX,0)
410      1103 CONTINUE
           RETURN
C
C*****
C
415      1200 CONTINUE
C THIS EFFECTS CLOSURE OF THE SIMULATION RUN
           RETURN
C
C*****
420      C
           END
```

SUBROUTINE CONTRL(ISW)

C THIS CONDUCTS THE MLS SIMULATION THROUGH A  
C RMSE VS. FSC STUDY

5

```

C
REAL LAMDA
INTEGER XNAME1(2),YNAME1(2),YNAM1(2,9)
INTEGER XNAME(2),YNAME(2),DATIN(4),DATOUT(4),DOUT
INTEGER TITLE1(9),FUNCTN(2)
10 LOGICAL NOKLMN,NLOE,NOAC,KALMAN,LOE,TETHRD,MORE,NFIRST,ADAPTV,
C FILEIN,FILOUT
COMMON/IDDATA/ISIM,IPMLS,IRCVR,IADAP,ITETHR,IPOPT
COMMON/RCVRO0/THAMAX,THAMIN,TS,TR,OMEGA,TF
COMMON/RCVRO1/NGMIN,NGHAX,DELBL,NGM,IR,IAE
15 COMMON/RCVRO2/RHOMAX,DTHQ,TDRD,BD,WSCD,NSO(4),NGO(4)
COMMON/RCVRO3/PI,F(8,8),FL25(4),FSAHP,K,KM,TETHRD,NG,NS,JH
COMMON/RCVRO4/DELT,ED(8),GOGT(8,8),H(5,8),ICOUNT,SIGMA
COMMON/RCVRO5/NLOE,NOKLMN,NOAC,GAMAES(5),RDIAG(5),PHDIAG(8)
COMMON/RCVRO6/PPDIAG(8),RMAT(5,5),PHI(5,5),PA(8,8),LAMDA(5)
20 COMMON/RCVRO7/T(130),V(130)
COMMON/RCVRO8/XSLDE(8),ESLOE(8),ES(8)
COMMON/RCVRO9/BRCVR,BB,POCRIT,CC
COMMON/RCVR10/XS1(8),XS(8)
COMMON/MLS000/ALFA,THE,THEDOT,ALFAR,THR,THRDOT,B,WSC
25 COMMON/MLS001/CSNRT,CSNRF,DSNRDB,RHO,BETA,FSC,LGMAX
COMMON/MLS002/DCSNR,CSNR,LG,TPKT,TPKF
COMMON/MLS003/FL1OAE(4,2),FL1D(4),DELTAT(2),XD(8,2),YD(4,2)
COMMON/MLS004/BMLS,BBB,MTIMES,HSET,MORE
DIMENSION X(8),THESR(115),XDATUM(115),EEME(13),EERM(13)
30 DIMENSION IDNRS(6),IDASCI(20),IDENTS(6),EEST(13),TTCD(13),YYHI(13)
DIMENSION YYHA(13)
DIMENSION FSCA(13),IFSCA(13)
DIMENSION EEMEA(13,9),EERMS(13,9),EESTD(13,9)
DIMENSION EMEAN(9),EMS(9),ERMS(9),ESD(9)
35 EQUIVALENCE (EEME(1),EEMEA(1,2)),(EERM(1),EERMS(1,2)),
*(EEST(1),EESTD(1,2))
EQUIVALENCE (THERR,ES(2))
EQUIVALENCE (ALFA,X(1)),(ISIM,IDNRS(1)),(DOUT,DATOUT(2))
40 DATA YNAM1/8HALF RMSE,8H ,8H THE RMSE,8H DEGREES ,
*8H TD RMSE,8H DEG/SEC ,8HALR RMSE,8H ,8H THR RMSE,
*8H DEGREES ,8H TRD RMSE,8H DEG/SEC ,8HBET RMSE,8H DEGREES ,
*8HFSC RMSE,8H HZ ,8HFSCDRMSE,8H HZ/SEC /
DATA ABORT/1HA/,SPACE/1H/,NFIRST/,FALSE./,ADAPTV/.TRUE./
45 DATA DATIN/10HMLSSIMDATA,10H200000F000,2*0/
DATA DATOUT/10HMLSSIMDATA,3*0/
DATA IDASCI/7HCROSSMP,7HRMSE(T),7HRMSE(B),7HRMSE(F),7H
*8H PMLS1 ,8H PMLS2 ,
*8H PMLS3 ,8H THRLD ,8H OPTIHL ,8H SUBOPT ,8H -3 DB ,8HADAPTIV ,
*8HNONADAP ,8HUNTETHRD,8HTETHERED,2H ,8H POPT1 ,8H POPT2. ,
50 *8H POPT3 /
DATA NSTART/3/,IRSIGN/1/,KSTART/11/,FILEIN
*/.FALSE./,FILOUT/.TRUE./
DATA TITLE1/6H ALFA ,6H THETA,6HTHEDOT,6H ALFAR,6HTHETAR,6HTRDOT
C,6H B ,6H WSC ,6HWSCDOT/
55 DATA XNAME/8HSCAN NO.,8H K ./,YNAME/8HTHES ERR,8HDEGREES /
DATA XNAME1/8H FSC ,8H HZ /
DATA FUNCTN/7HAZIMUTH,7HELEVAT./

```

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```

C
60      1      GO TO (100,200,300,400,500,600,700,800,900,1000,1100,1200),ISW
        10      FDRMT(1H)
        11      FORMAT(9(/))
        11      FORMAT (1H1)
C
65      C*****
C
        100     CONTINUE
C THIS IDENTIFIES THE SCENARIO AND REINITIALIZES, AS NECESSARY,
C THE FOLLOWING RECEIVER PARAMETERS
        CSIGMA,IAE,DSNROB,RHO,FSC,BETA,JM,BHLS
70      IF(NFIRST) GO TO 155
        NDAC=.TRUE.
        NFIRST=.TRUE.
        JBNAM=JOBNAME(I)
75      ISIM=4
        IMOD=1
        WRITE (7,110)
        110     FORMAT(19H1RMSE VS. FSC STUDY)
        CALL LOGIO(6HFILEIN,FILEIN,0)
        IF (.NOT.FILEIN) NSTART=0
80      IF(.NOT.FILEIN) GO TO 122
        IX=IATTACH(6LTAPE15,DATIN)
        IF(IX.NE.0) CALL INTIO(6HIX(AT),IX,1,1)
        IF(IX.NE.0) STOP#INPUT FILE ATTACH NOT SATISFACTORY#
        WRITE(7,120) (DATIN(I),I=1,2)
85      120     FORMAT(23H THIS READS INPUT FILE ,2A10/)
        122     CALL LOGIO(6HFILOUT,FILOUT,0)
        CALL INTIO(6HNSTART,NSTART,100,0)
        NSTOP=NSTART
        CALL INTIO(6H NSTOP,NSTOP,100,0)
90      CALL LOGIO(6HTETHRD,TETHRD,0)
        IF(IRCVR.EQ.1) GO TO 125
        CALL LOGIO(6HADAPTV,ADAPTV,0)
        125     CONTINUE
95      IF(TETHRD) ITETHR=2
        IF(ADAPTV) GO TO 135
        IRSIGN=-1
        IADAP=3
        135     CONTINUE
        DO 145 I=2,6
100      IASC=3*(I-1)+IDNRS(I)+2
        IDENTS(I)=IDASCI(IASC)
        145     CONTINUE
        ENCODE(8,150,IDENTS(1)) IDASCI(ISIM),IMOD
105      150     FORMAT(A7,I1)
        WRITE (7,152) IDNRS,IMOD
        152     FORMAT (1H ,6I1,1X,I1/)
        WRITE (7,153) IDENTS
        153     FORMAT (1H ,A8)
        CALL INTIO(6H KM,KM,115,0)
110      KSTART=MIN0(KM,KSTART)
        KMNET=KM-KSTART+1
        FSCHIN=1./((DELTAT(IAE)*KMNET)
        READ(10,105) LGMAX,(IFSCA(I),I=1,LGMAX)
105      105     FORMAT(14I5)

```

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115      WRITE(7,106) LGMAX,(IFSCA(I),I=1,LGMAX)
106      FORMAT(9H0LGMAX = ,I2/IH ,I3(I7,2X))
154      DO 154 I=1,LGMAX
154      FSCA(I)=FSCMIN+IFSCA(I)
120      107      WRITE(7,107)(FSCA(I),I=1,LGMAX)
120      107      FORMAT(1H 13(F7.3,2X))
      NRUN=NSTART-1
      DSNRDB=20.
      RHO=0.5
      BETA=45.
125      BMLS=1.
      BRCVR=1.
      TSEP=1.
155      CONTINUE
      IF(FILEIN) GOTD 158
130      NRUN=NRUN+1
      WRITE(7,11)
      CALL INTIO(6H NRUN,NRUN,1,1)
      CALL REALIO(6HDSNRDB,DSNRDB,0)
135      CALL REALIO(6H RHO,RHO,0)
      CALL REALIO(6H BETA,BETA,0)
      CALL REALIO(6H BMLS,BMLS,0)
      CALL REALIO(6H BRCVR,BRCVR,0)
      CALL REALIO(6H TSEP,TSEP,0)
      GOTD 167
140      158      CONTINUE
      READ(15,160) NRUN,DSNRDB,RHO,BETA,BMLS,BRCVR,TSEP.
      IF(EQ(15))170,165
160      FORMAT(15,3G10.3,5X,3G10.3)
165      IF(NRUN.LT.NSTART) GO TO 158
145      167      IF(NRUN.GE.NSTOP) MORE=.FALSE.
      FSC=FSCA(I)
      XO(5,IAE)=XO(2,IAE)-TSEP.
      XO(3,IAE)=0.
      XO(6,IAE)=0.
150      RETURN
170      STOP*EOF REACHED ON INPUT FILE*
C
C*****
C
155      200      CONTINUE
C THIS OUTPUTS BASIC SIMULATION DATA OF INTEREST, SUCH AS
C THE ANGLE FUNCTION, INITIAL STATE, ETC.
      WRITE(7,210) NRUN,DSNRDB,RHO,BETA,BMLS,BRCVR,TSEP
160      210      FORMAT(5H0NRUN,5X,6HDSNRDB,12X,3HRHO,12X,4HBETA,12X,4HBMLS,11X,
      *5HBRCVR,12X,4HTSEP/1H0,14,6(6X,610.3))
      IF(.NOT.FILOUT) GOTD 245
      IF(NRUN.LE.9) ENCODE(10,220,DDUT) IDNRS,1HU,IMOD,1H0,NRUN
165      220      FORMAT(6I1,A1,I1,A1,I1)
      IF(NRUN.GE.10) ENCODE(10,230,DDUT) IDNRS,1HU,IMOD,NRUN
      230      FORMAT(6I1,A1,I1,I2)
      IX=IREQST(6LTAPE17,3L+PF)
      IF(IX.NE.0) CALL INTIO(6HIX(RQ),IX,1,1)
      IF(IX.NE.0) STOP*OUTPUT FILE REQUEST NOT SATISFACTORY*
170      240      WRITE(7,240) (DATOUT(I),I=1,2)
      245      FORMAT(25H0THIS WRITES OUTPUT FILE ,2A10)
      CALL DATE(TODAY)

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```

      WRITE (7,250) FUNCTN (IAE),IAE
175 250  FORMAT (1H0,A7,15H FUNCTION (IAE=,I1,1H))
      WRITE (7,260) ((1,X(I)),I=1,8)
      FORMAT (15H0INITIAL STATE://(3H X(,I1,4H) = ,G13.6))
      WRITE(7,270) IDENT5(2)
270  FORMAT(1H0,A7)
      RETURN
C
180 C*****
C
300  CONTINUE
C THIS IDENTIFIES THE BASIC RECEIVER STRUCTURE (THRHL0,DPY,SUBOPT)
C AND REINITIALIZES, AS NECESSARY, THE FOLLOWING RCVR DATA
185 CIR (NEGATE ONLY), NOAC,NOKLMN,NOL0E,BRCVR,DELBL,TETHRO
      ITIT=MINO(IRCVR,2)
C
C NEGATE IR WITH THE FOLLOWING FOR NONADAPTIVE RECEIVER
190 IR=ISIGN(IR,IRSIGN)
C
      RETURN
C
C*****
195 400  CONTINUE
C THIS OUTPUTS BASIC RECEIVER DATA OF INTEREST
      WRITE(7,410) (IDENTS(I),I=3,4),IR,NG,NS
410  FORMAT (1H0,A8,4HRCVR/1H0,A8,6HDESIGN/5H (IR=,I2,4H,NG=,I1,
      * 4H,NS=,I1,1H))
      WRITE(7,420) (IDENTS(I),I=5,6)
200 420  FORMAT(1H0,A8/1H0,A7/)
      RETURN
C
C*****
205 C
500  CONTINUE
C THIS SETS-UP THE MSET-LOOP
      ICDUNT=0
      DO 510 I=1,LGMAX
210 510  YYMI(I)=1.E322
      YYMA(I)=-1.E322
      RETURN
C
C*****
215 C
600  CONTINUE
C THIS SETS-UP THE LG-LOOP FOR THE (MSET)-TH SERIES OF SETS
      RETURN
C
C*****
220 C
700  CONTINUE
C THIS SETS-UP THE K-LOOP FOR THE (LG)-TH SET OF KM SCANS
      FSC=FSCA(LG)
225 X(8,IAE)=2.*PI*FSC
      X(8)=X(8,IAE)
      X(7)=X(7,IAE)
      DUM=GAUSS(1.0)
      WRITE(7,11)

```

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```

230      .. CALL INTIO(6H NRUN,NRUN,1,1)
        WRITE(7,705) LG,FSC
235      705  FORMAT(1H ,4X,3HLG=,I2,5X,6HFSC = ,G12.5)
        CALL INTIO(6H  KM,KH,1,1)
        WRITE(7,710) (TITLE1(I),I=1,NS)
235      710  FDRMAT(6HO  K,4X,5HCSNRT,4X,5HQTY ,9(3X,A6,2X))
        DO 712 I=1,NS
235      712  EMEAN(I)=0.
        EMS(I)=0.
        LASTCT=0
        ICDUNT=0
240      DO 730 IPA=1,NS
        DO 720 JPA=1,NS
        PA(IPA,JPA)=0.
240      720  CONTINUE
245      730  CONTINUE
        RETURN
C
C*****
C
250      800  CONTINUE
        C THIS INITIALIZES THE K-TH SCAN
        SEP=SPACE
        RETURN
C
C*****
255      C
        900  CONTINUE
        C THIS SAVES/PREPROCESSES DATA FROM THE K-TH SCAN
        IF (ICOUNT.NE.LASTCT) SEP=ABORT
        DO 905 I=1,NS
260      905  ES(I)=X(I)-XS(I)
        IF(NS.GE.7) ES(7)=ABS(X(7))-ABS(XS(7))
        IF(NS.GE.8) ES(8)=ABS(X(8))-ABS(XS(8))
        BETTA=(180./PI)*X(7)
        COL8=THERR
265      IF (IRCVR,NE. 1) COL8=SQRT(PPDIAG(2))
        IF (IRCVR,EQ. 1) CALL DFLTRI(COL8,THERR,FL10)
        IF((NRUN,EQ.NSTART.AND.LG,EQ.1).OR.(K,EQ,KH)) GOTO 906
        GO TO 950
270      906  WRITE(7,910) K,CSNRT,(X(I),I=1,NS)
        FORMAT(3HO ,I3,2X,G10.3,5H X= ,2X,9(G10.3,1X))
        WRITE(7,920) (XS(I),I=1,NS)
        FORMAT(18X,5H XS= ,2X,9(G10.3,1X))
        WRITE(7,930) (ES(I),I=1,NS)
        FORMAT(18X,5H ES= ,2X,9(G10.3,1X))
275      IF(IRCVR,EQ.1) WRITE(7,940) COL8
        FORMAT(8X,15HUNFILT. ES(2)= ,13X,G10.3)
        940  XDATUM(K)=K
        THESER(K)=THERR
        LASTCT=ICOUNT
280      IF(K.LT.KSTART) RETURN
        DO 960 I=1,NS
        EMEAN(I)=EMEAN(I)+ES(I)
285      960  EMS(I)=EMS(I)+ES(I)**2.
        RETURN
C

```

```

C*****
C
1000 CONTINUE
C THIS SAVES/PROCESSES/OUTPUTS DATA FROM THE (LG)-TH SET OF KM SCANS
290 DO 1005 I=1,NS
    EMEAN(I)=EMEAN(I)/KHNET
    EMS(I)=EMS(I)/KHNET
    ERMS(I)=SQRT(EMS(I))
    ESD(I)=SQRT(EMS(I)-EMEAN(I)**2)
295 1005 CONTINUE
    XW=ICOUNT
    TCOUNT=100.*XW/KM
    WRITE(7,1009)
    1009 FORMAT(3(/))
    WRITE(7,1010)KHNET
300 1010 FORMAT(5X,26HERRDR SAMPLE STATISTICS: (,13,9H SAMPLES))
    IF(IRCVR.EQ.1) WRITE(7,1015)
    1015 FDRMAT(5X,31HTHRESHOLD RCVR (FILTERED ERROR))
    WRITE(7,1020)(TITLE1(I),I=1,NS)
305 1020 FORMAT(1H0,20X,4HQT,9(3X,A6,2X))
    WRITE(7,1030)(EMEAN(I),I=1,NS)
    1030 FORMAT(1H0,16X,8HEMEAN = ,9(G10.3,1X))
    WRITE(7,1040)(ERMS(I),I=1,NS)
    1040 FORMAT(18X,7HERMS = ,9(G10.3,1X))
310 1040 WRITE(7,1050)(ESD(I),I=1,NS)
    1050 FORMAT(19X,6HESD = ,9(G10.3,1X))
    IF(IRCVR.EQ.1)WRITE(7,1060)TCOUNT
    1060 FORMAT(/1H ,4X,F7.2,22HZ OF SCANS ARE ABORTED)
    IF(IRCVR.NE.1)WRITE(7,1070)(GGGT(I),I=1,NS)
315 1070 FORMAT(5(/),4X,35H ON LAST SCAN, DIAGONAL OF GGGT WAS/26X
    C9(G10.3,1X))
    DO 1071 I=1,NS
    EEMEA(LG,I)=EMEAN(I)
    EERMS(LG,I)=ERMS(I)
320 1071 EESTD(LG,I)=ESD(I)
    DO 1072 I=1,KM
    YYMI(LG)=AMINI(THESER(I),YYMI(LG))
    1072 YYHA(LG)=AMAXI(THESER(I),YYHA(LG))
    TTCD(LG)=TCOUNT
    IF(LG.NE.1) RETURN
    YMIN=YMAX=0.
    WRITE(7,11)
325 11 CALL INTIO(6H NRUN,NRUN,1,1)
    CALL PLOT(XDATUM,THESER,KM,XNAME,YNAME,YMIN,YMAX,0)
330 RETURN
C
C*****
C
1100 CONTINUE
335 C THIS SAVES/PROCESSES/OUTPUTS DATA FROM THE (MSET)-TH SERIES OF
    CLGMAX SETS OF KM SCANS
    WRITE(7,11)
    CALL INTIO(6H NRUN,NRUN,1,1)
    WRITE(7,1110)6H FSC ,(TITLE1(I),I=1,NS)
340 1110 FORMAT(1H0,10X,3HQT,9(3X,A6,2X))
    WRITE(7,1120)FSCA(1),(EMEA(1,I),I=1,NS)
    1120 FORMAT(1H0,7X,7HEMEAN: ,9(G10.3,1X))

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```

DO 1130 J=2,LGMAX
1130 WRITE(7,1161) FSCA(J),(EEMEA(J,I),I=1,NS)
345 WRITE(7,1140) FSCA(1),(EERMS(1,I),I=1,NS)
1140 FORMAT(1H0, 8X,6HERMS: ,9(G10.3,1X))
DO 1150 J=2,LGMAX
1150 WRITE(7,1161) FSCA(J),(EERMS(J,I),I=1,NS)
350 WRITE(7,1160) FSCA(1),(EESTD(1,I),I=1,NS)
1160 FORMAT(1H0, 8X,6HESTO: ,9(G10.3,1X))
DO 1165 J=2,LGMAX
1165 WRITE(7,1161) FSCA(J),(EESTD(J,I),I=1,NS)
1161 FORMAT(15X,9(G10.3,1X))
DO 1103 I=1,NS
355 FACTOR=1.
IF(I.EQ.7) FACTOR=180./PI
IF(I.EQ.8) FACTOR=.5/PI
IF(I.EQ.9) FACTOR=.5/PI
YMIN=0.
360 YMAX=0.
DO 1101 LG1=1,LGMAX
1101 EEME(LG1)=EERMS(LG1,I)*FACTOR
YNAME1(1)=YNAMI(1,I)
YNAME1(2)=YNAMI(2,I)
365 K1=MOD(I,2)
IF(K1.EQ.1) WRITE(7,11)
IF(K1.EQ.1) CALL INTID(6H NRUN,NRUN,1,1)
IF(K1.EQ.0) WRITE(7,10)
CALL PLOTR(FSCA,EEME,LGMAX,XNAME1,YNAME1,YMIN,YMAX,0)
370 CONTINUE
IF(.NOT.FILDUT) RETURN
WRITE(7,11)
WRITE(7,1170) (DATOUT(I),I=1,2)
375 FORMAT(13H OUTPUT FILE ,2A10,1H:/)
1170 WRITE(7,1172) DDUT,DELT,MTIMES,LGMAX,KM,TODAY,JBNAM
1172 FORMAT(1H ,A10,8X,G13.6,5X,3(5X,I3,10X),A10,8X,A10/)
WRITE(7,1174) IDENT5,KSTART
1174 FORMAT(1H ,6(1X,A8,9X),6X,I3/)
WRITE(7,1176) NRUN,DSNRDB,RHO,BETA,FSC,TSEP
380 1176 FORMAT(1H ,5X,I2,6X,6(5X,G13.6)/)
DO 1175 LGN=1,LGMAX
1175 WRITE(7,1182) EEME(LGN),EERM(LGN),EEST(LGN),TTCD(LGN),YYMI(LGN),
*YYMA(LGN),FSCA(LGN),LGN
1182 FORMAT(1H ,7(G13.6,5X),I5)
385 WRITE(17) DDUT,DELT,MTIMES,LGMAX,KM,TODAY,JBNAM
WRITE(17) IDENT5,KSTART
WRITE(17)NRUN,DSNRDB,RHO,BETA,BHLS,BRCVR,TSEP
DO 1190 LGN=1,LGMAX
390 1190 WRITE(17) EEME(LGN),EERM(LGN),EEST(LGN),TTCD(LGN),YYMI(LGN),
*YYMA(LGN),FSCA(LGN),LGN
IX=IATTACH(6LTAPE20,DATOUT)
IF(IX.NE.0) GO TO 1195
READ(20) DUM,DUM,IDUM,IDUM,DUM,DUM,IDUM
CALL RETURN(6LTAPE20)
395 REWIND 17
IX=ICATALO(6LTAPE17,DATOUT,2LPW,8RHIGHFILL,2LRP,365)
GO TO 1196
1195 CALL RETURN(6LTAPE20)
REWIND 17

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```
400      IX=ICATALO(6LTAPE17,DATOUT,2LXR,8RHIGHFILL,2LRP,365)
      1196 IF(IX.NE.0) CALL INTID(6HIX(CA),IX,1,1)
      IF(IX.NE.0) STOP*OUTPUT FILE CATALOG NOT SATISFACTORY*
      CALL RETURN(6LTAPE17)
      WRITE (7,1198) (DATOUT(I),I=1,2)
405      1198 FORMAT(13H00OUTPUT FILE ,2A10,33H IS WRITTEN, CATALOGED AND CLOSED)
      RETURN
      C
      C*****
      C
410      1200 CONTINUE
      C THIS EFFECTS CLOSURE OF THE SIMULATION RUN
      WRITE(7,11)
      RETURN
      C
415      C*****
      C
      END
45000B CH STORAGE USED      13.054 SECONDS
```

SUBROUTINE CONTRL (ISW)

C THIS CONDUCTS THE MLS SIMULATION THROUGH A  
C RMSE VS. FSC STUDY

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REAL LANDA
INTEGER XNAME1(2),YNAME1(2),YNAME1(2,9)
INTEGER XNAME(2),YNAME(2),DATIN(4),DATOUT(4),DOUT
INTEGER TITLE1(9),FUNCTN(2)
LOGICAL NOKLMN,NOLOE,NOAC,KALMAN,LOE,TETHRD,MORE,NFIRST,ADAPTV,
CFILEIN,FILOUT
COMMON/IDDATA/ISIM,IPMLS,IRCVR,IADAP,ITETHR,IPOPT
COMMON/RCVROO/THAMAX,THAMIN,TS,TR,OMEGA,TF
COMMON/RCVR01/NGMIN,NGMAX,DELBL,NGM,IR,IAE
COMMON/RCVR02/RHORAX,OTHO,TDRO,BO,WSCO,NSO(4),NGO(4)
COMMON/RCVR03/PI,F(8,8),FL25(4),FSAMP,K,KM,TETHRD,NG,NS,JH
COMMON/RCVR04/DELT,ED(8),GOGT(8,8),H(5,8),ICOUNT,SIGMA
COMMON/RCVR05/NOLOE,NOKLMN,NOAC,GANAES(5),RDIAG(5),PHDIAG(8)
COMMON/RCVR06/PPDIAG(8),RMAT(5,5),PHI(5,5),PA(8,8),LANDA(5)
COMMON/RCVR07/T(130),V(130)
COMMON/RCVR08/XSLOE(8),ESLOE(8),ES(8)
COMMON/RCVR09/BRCVR,BB,PDCRIT,CC
COMMON/RCVR10/XS1(8),XS(8)
COMMON/MLS000/ALFA,THE,THEODT,ALFAR,THR,THRDOT,B,WSC
COMMON/MLS001/CSNRT,CSNRF,OSNR0B,RHO,BETA,FSC,LGMAX
COMMON/MLS002/DCSNR,CSNR,LG,TPKT,TPKF
COMMON/MLS003/FL10AE(4,2),FL10(4),DELTAT(2),XD(8,2),YD(4,2)
COMMON/MLS004/BMLS,BBB,MTIMES,MSET,MORE
DIMENSION X(8),THESER(115),XDATUM(115),EEME(13),EERM(13)
DIMENSION IDNRS(6),IDASCI(20),IDENTS(6),EEST(13),TTCO(13),YYMI(13)
DIMENSION YYMA(13)
DIMENSION FSCA(13),IFSCA(13)
DIMENSION EEMEA(13,9),EERMS(13,9),EESTD(13,9)
DIMENSION EMEAN(9),EMS(9),ERMS(9),ESD(9)
EQUIVALENCE (EEME(1),EEMEA(1,2)),(EERM(1),EERMS(1,2)),
*(EEST(1),EESTD(1,2))
EQUIVALENCE (THERR,ES(2))
EQUIVALENCE (ALFA,X(1)),(ISIM,IDNRS(1)),(DOUT,DATOUT(2))
DATA YNAME1/8HALF RMSE,8H ,8HTHE RMSE,8HDEGREES ,
*8HTDT RMSE,8HDEG/SEC ,8HALR RMSE,8H ,8HTHR RMSE,
*8HDEGREES ,8HTRD RMSE,8HDEG/SEC ,8HBET RMSE,8HDEGREES ,
*8HFSC RMSE,8H HZ ,8HFSCDRMSE,8H HZ/SEC /
DATA ABORT/1HA/,SPACE/1H /,NFIRST/.FALSE./,ADAPTV/.TRUE./
DATA DATIN/10HMLSSIMDATA,10H200000F000,2*0/
DATA DATOUT/10HMLSSIMDATA,3*0/
DATA IDASCI/7HCROSSMP,7HRMSE(T),7HRMSE(B),7HRMSE(F),7H ,
*8H PMLS1 ,8H PMLS2 ,
*8H PMLS3 ,8H THRHLD ,8H OPTIML ,8H SUBOPT ,8H -3 DB ,8HADAPTIV ,
*8HNONADAP ,8HUNTETHRD,8HTETHERED,2H ,8H POPT1 ,8H POPT2 ,
*8H POPT3 /
DATA NSTART/3/,IRSIGN/1/,KSTART/11/,FILEIN
*/.FALSE./,FILOUT/.TRUE./
DATA TITLE1/6H ALFA ,6H THETA,6HTHEODT,6H ALFAR,6HTHETAR,6HTHRDOT
C,6H B ,6H WSC ,6HWSCDOT/
DATA XNAME1/8H FSC ,8H K /,YNAME/8HTHES ERR,8HDEGREES /
DATA XNAME1/8H FSC ,8H HZ /
DATA FUNCTN/7HAZINUTH,7HELEVAT./

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C
60      GO TO (100,200,300,400,500,600,700,800,900,1000,1100,1200),ISW
       1  FORMAT(1H )
       10 FGMAT(9(/))
       11 FGMAT (1H1)
C
C*****
65      C
       100 CONTINUE
C THIS IDENTIFIES THE SCENARIO AND REINITIALIZES, AS NECESSARY,
C THE FOLLOWING RECEIVER PARAMETERS
       CSIGMA,IAE,DSNRDB,RHO,FSC,BETA,JM,BHLS
70      IF(NFIRST) GO TO 155
       NGAC=.TRUE.
       NFIRST=.TRUE.
       JBNAM=JOBNAME(I)
       ISIM=4
75      IMOD=2
       WRITE (7,110)
       110  FORMAT(19HIRMSE VS. FSC STUDY)
       CALL LOGIO(6HFILEIN,FILEIN,0)
       IF (.NOT.FILEIN) NSTART=0
80      IF(.NOT.FILEIN) GO TO 122
       IX=IATTACH(6LTAPE15,DATIN)
       IF(IX.NE.0) CALL INTIO(6HIX(AT),IX,1,1)
       IF(IX.NE.0) STOP*INPUT FILE ATTACH NOT SATISFACTORY*
       WRITE(7,120) (DATIN(I),I=1,2)
85      120  FORMAT(23H THIS READS INPUT FILE ,2A10/)
       122  CALL LOGIO(6HFILOUT,FILOUT,0)
       CALL INTIO(6HNSTART,NSTART,100,0)
       NSTOP=NSTART
90      CALL INTIO(6HTNSTOP,NSTOP,100,0)
       CALL LOGIO(6HTETHRD,TETHRD,0)
       IF(IRCVR.EQ.1) GO TO 125
       CALL LOGIO(6HADAPTV,ADAPTV,0)
125     CONTINUE
95     IF(TETHRD) ITETHR=2
       IF(ADAPTV) GO TO 135
       IRSIGN=-1
       IADAP=3
135     CONTINUE
100     DO 145 I=2,6
       IASC=3*(I-1)+IDNRS(I)+2
       IDENTS(I)=IDASCI(IASC)
145     CONTINUE
       ENCODE(8,150,IDENTS(1)) IDASCI(ISIM),IMOD
105     150  FORMAT(A7,I1)
       WRITE (7,152) IDNRS,IMOD
       152  FORMAT (1H ,6I1,1X,I1/)
       WRITE (7,153) IDENTS
       153  FORMAT (1H ,A8)
       CALL INTIO(6H KM,KM,115,0)
110     KSTART=MIN0(KM,KSTART)
       KMNET=KM-KSTART+1
       FSCIN=1./(DELTAT(IAE)*KMNET)
       READ(10,105) LGMAX,(IFSCA(I),I=1,LGMAX)
105     FORMAT(14I5)

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115      106      WRITE(7,106) LGMAX,(IFSCA(I),I=1,LGMAX)
          FORMAT(9H0LGMAX = ,I2/1H ,13(I7,2X))
          DO 154 I=1,LGMAX
          154      FSCA(I)=FSCMIN+IFSCA(I)
120      107      WRITE(7,107) FSCA(I),I=1,LGMAX)
          FORMAT(1H 13(F7.3,2X))
          NRUN=NSTART-1
          DSNRDB=20.
          RHG=0.5
          BETA=45.
125      BMLS=1.
          BRCVR=1.
          TSEP=1.
          155      CONTINUE
          IF(FILEIN) GOTO 158
130      NRUN=NRUN+1
          WRITE(7,11)
          CALL INTIO(6H NRUN,NRUN,1,1)
          CALL REALIO(6HDSNRDB,DSNRDB,0)
          CALL REALIO(6H RHO,RHO,0)
135      CALL REALIO(6H BETA,BETA,0)
          CALL REALIO(6H BMLS,BMLS,0)
          CALL REALIO(6H BRCVR,BRCVR,0)
          CALL REALIO(6H TSEP,TSEP,0)
          GOTO 167
140      158      CONTINUE
          READ(15,160) NRUN,DSNRDB,RHO,BETA,BMLS,BRCVR,TSEP
          IF(EOF(15))170,165
          160      FORMAT(15,3G10.3,5X,3G10.3)
          165      IF(NRUN.LT.NSTART) GO TO 158
145      167      IF(NRUN.GE.NSTOP) MORE=.FALSE.
          FSC=FSCA(1)
          XO(5,IAE)=XO(2,IAE)-TSEP
          XO(3,IAE)=0.
          XO(6,IAE)=0.
150      RETURN
          170      STOP#EOF REACHED ON INPUT FILE#
          C
          C*****
          C
155      200      CONTINUE
          C THIS OUTPUTS BASIC SIMULATION DATA OF INTEREST, SUCH AS
          C THE ANGLE FUNCTION, INITIAL STATE, ETC.
          WRITE(7,210) NRUN,DSNRDB,RHO,BETA,BMLS,BRCVR,TSEP
          210      FORMAT(5HNRUN,5X,6HDSNRDB,12X,3HRHO,12X,4HBETA,12X,4HBMLS,11X,
160      *5HBRCVR,12X,4HTSEP/1HC,14,6(6X,610.3))
          IF(.NOT.FILOUT) GOTO 245
          IF(NRUN.LE.9) ENCODE(10,220,DOUT) IDNRS,1HU,IMOD,1HO,NRUN
          220      FORMAT(6I1,A1,I1,A1,I1)
          IF(NRUN.GE.10) ENCODE(10,230,DOUT) IDNRS,1HU,IMOD,NRUN
165      230      FORMAT(6I1,A1,I1,I2)
          IX=IREQST(6LTAPE17,3L*PF)
          IF(IX.NE.0) CALL INTIO(6HIX(RQ),IX,1,1)
          IF(IX.NE.0) STOP#OUTPUT FILE REQUEST NOT SATISFACTORY#
          WRITE(7,240) (DATOUT(I),I=1,2)
170      240      FORMAT(25H0THIS WRITES OUTPUT FILE ,2A10)
          245      CALL DATE(TODAY)

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      WRITE (7,250) FUNCTN (IAE),IAE
      FORMAT (1H0,A7,15H FUNCTION (IAE=,I1,1H))
175 260 WRITE (7,260) ((I,X(I)),I=1,8)
      FORMAT (15H0INITIAL STATE:/(3H X(,I1,4H) = ,G13.6))
      WRITE (7,270) IDENTIS(2)
      FORMAT(1H0,A7)
      RETURN
C
180 C*****
C
      300 CONTINUE
C THIS IDENTIFIES THE BASIC RECEIVER STRUCTURE (THRHLD,OPT,SUBOPT)
C AND REINITIALIZES, AS NECESSARY, THE FOLLOWING RCVR DATA
185 CIR (NEGATE ONLY), NOAC,NOKLMN,NOLDE,BRCVR,DELBL,TETHRD
      ITIT=MINO(IRCVR,2)
C
C _NEGATE IR WITH THE FOLLOWING FOR NONADAPTIVE RECEIVER
      IR=ISIGN(IR,IRSIGN)
190 C
      RETURN
C
C*****
195 400 CONTINUE
C THIS OUTPUTS BASIC RECEIVER DATA OF INTEREST
      WRITE(7,410) (IDENTS(I),I=3,4),IR,NG,NS
      410 FORMAT (1H0,A8,4HRCVR/1H0,A8,6HDESIGN/5H (IR=,I2,4H,NG=,I1,
      * 4H,NS=,I1,1H))
      WRITE(7,420) (IDENTS(I),I=5,6)
200 420 FORMAT(1H0,A8/1H0,A7/)
      RETURN
C
C*****
205 C
      500 CONTINUE
C THIS SETS-UP THE MSET-LOOP
      ICDUNT=0
      DO 510 I=1,LGMAX
      YYMI(I)=1.E322
210 510 YYMA(I)=-1.E322
      RETURN
C
C*****
215 C
      600 CONTINUE
C THIS SETS-UP THE LG-LOOP FOR THE (MSET)-TH SERIES OF SETS
      RETURN
C
C*****
220 C
      700 CONTINUE
C THIS SLTS-UP THE K-LOOP FOR THE (LG)-TH SET OF KM SCANS
      FSC=FSCA(LG)
      XO(8,IAE)=2.*PI*FSC
225 X(8)=XO(8,IAE)
      X(7)=XO(7,IAE)
      DUM=GAUSS(1.0)
      WRITE(7,11)

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230 CALL INTIO(6H NRUN,NRUN,1,1)
      WRITE(7,705) LG,FSC
      705 FORMAT(1H,4X,3HLG=,I2,5X,6HFSC = ,G12.5)
      CALL INTIO(6H KH,KM,1,1)
      WRITE(7,710) (TITLE1(I),I=1,NS)
      710 FORMAT(6H0 K,4X,5HCSNRT,4X,5HQTY ,9(3X,A6,2X))
235 DO 712 I=1,NS
      EMEAN(I)=0.
      712 EMS(I)=0.
      LASTCT=0
      ICOUNT=0
240 DO 730 IPA=1,NS
      DO 720 JPA=1,NS
      PA(IPA,JPA)=0.
      720 CONTINUE
      730 CONTINUE
245 RETURN
C
C*****
C
800 CONTINUE
250 C THIS INITIALIZES THE K-TH SCAN
      SEP=SPACE
      RETURN
C
C*****
C
900 CONTINUE
255 C THIS SAVES/PREPROCESSES DATA FROM THE K-TH SCAN
      IF(ICOUNT.NE.LASTCT) SEP=ABORT
      XS(7)=0.5*PI
      XS(8)=0.0
      DO 905 I=1,NS
      905 ES(I)=X(I)-XS(I)
      IF(NS.GE.7) ES(7)=ABS(X(7))-ABS(XS(7))
      IF(NS.GE.8) ES(8)=ABS(X(8))-ABS(XS(8))
265 BETTA=(180./PI)*X(7)
      COL8=THERR
      IF (IRCVR .NE. 1) COL8=SQRT(PPDIAG(2))
      IF (IRCVR .EQ. 1) CALL DFLTR1(COL8,THERR,FL10)
      IF((NRUN.EQ.NSTART.AND.LG.EQ.1).OR.(K.EQ.KM)) GOTO 906
270 GO TO 950
      906 WRITE(7,910) K,CSNRT,(X(I),I=1,NS)
      910 FORMAT(3H0 ,I3,2X,G10.3,5H X= ,2X,9(G10.3,1X))
      WRITE(7,920) (XS(I),I=1,NS)
      920 FORMAT(18X,5H XS= ,2X,9(G10.3,1X))
275 WRITE(7,930) (ES(I),I=1,NS)
      930 FORMAT(18X,5H ES= ,2X,9(G10.3,1X))
      IF(IRCVR.EQ.1) WRITE(7,940) COL8
      940 FORMAT(8X,15HUNFILT. ES(2)= ,13X,G10.3)
      950 XDATUM(K)=K
280 THESER(K)=THERR
      LASTCT=ICOUNT
      IF(K.LT.KSTART) RETURN
      DO 960 I=1,NS
      EMEAN(I)=EMEAN(I)+ES(I)
285 960 EMS(I)=EMS(I)+ES(I)**2

```

ORIGINAL PAGE IS  
 OF POOR QUALITY

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```

      RETURN
C
C*****
C
290 1000 CONTINUE
C THIS SAVES/PROCESSES/OUTPUTS DATA FROM THE (LG)-TH SET OF KM SCANS
      DU 1005 I=1,NS
      EMEAN(I)=EMEAN(I)/KMNET
      EMS(I)=EMS(I)/KMNET
295 ERMS(I)=SQRT(EMS(I))
      ESD(I)=SQRT(EMS(I)-EMEAN(I)**2)
1005 CONTINUE
      XW=ICOUNT
      TCOUNT=100.*XW/KM
300 WRITE(7,1009)
10J9 FORMAT(3(/))
      WRITE(7,1010)KMNET
1010 FORMAT(5X,26HERROR SAMPLE STATISTICS: (,I3,9H SAMPLES))
      IF(IRCVR.EQ.1) WRITE(7,1015)
305 1015 FORMAT(5X,31HTHRESHOLD RCVR (FILTERED ERROR))
      WRITE(7,1020)(TITLE1(I),I=1,NS)
1020 FORMAT(1H0,20X,4HQTY ,9(3X,A6,2X))
      WRITE(7,1030)(EMEAN(I),I=1,NS)
1030 FORMAT(1H0,16X,8HEMEAN = ,9(G10.3,1X))
310 1040 WRITE(7,1040)(ERMS(I),I=1,NS)
      FORMAT(18X,7HERMS = ,9(G10.3,1X))
      WRITE(7,1050)(ESD(I),I=1,NS)
1050 FORMAT(19X,6HESD = ,9(G10.3,1X))
      IF(IRCVR.EQ.1)WRITE(7,1060)TCOUNT
315 1060 FORMAT(/1H ,4X,F7.2,22HZ OF SCANS ARE ABORTED)
      IF(IRCVR.NE.1)WRITE(7,1070){GGGT(I,I),I=1,NS)
1070 FORMAT(5(/),4X,35H ON LAST SCAN, DIAGONAL OF GGGT WAS/26X
      C9(G10.3,1X))
      DO 1071 I=1,NS
320 1071 EMEAN(LG,I)=EMEAN(I)
      ERMS(LG,I)=ERMS(I)
      ESD(LG,I)=ESD(I)
      DO 1072 I=1,KM
325 1072 YYMI(LG)=AMIN1(THESER(I),YYMI(LG))
      YYMA(LG)=AMAX1(THESER(I),YYMA(LG))
      TTCO(LG)=TCOUNT
      IF(LG.NE.1) RETURN
      YMIN=YMAX=0.
      WRITE(7,11)
330 CALL INTIO(6H NRUN,NRUN,1,1)
      CALL PLDTR(XDATUM,THESER,KM,XNAME,YNAME,YMIN,YMAX,0)
      RETURN
C
C*****
C
335 1100 CONTINUE
C THIS SAVES/PROCESSES/OUTPUTS DATA FROM THE (MSET)-TH SERIES OF
      CLGMAX SETS OF KM SCANS
      WRITE(7,11)
340 CALL INTIO(6H NRUN,NRUN,1,1)
      WRITE(7,1110) 6H FSC ,(TITLE1(I),I=1,NS)
1110 FORMAT(1H0,10X,3HQTY ,9(3X,A6,2X))

```

```

      WRITE(7,1120) FSCA(1), (EEMEA(1,I), I=1, NS)
      FORMAT(1H0, 7X, 7HEMEAN: , 9(G10.3, 1X))
345      DO 1130 J=2, LGMAX
      1130 WRITE(7,1161) FSCA(J), (EEMEA(J,I), I=1, NS)
      WRITE(7,1140) FSCA(1), (EERMS(1,I), I=1, NS)
      1140 FORMAT(1H0, 8X, 6HERMS: , 9(G10.3, 1X))
      DO 1150 J=2, LGMAX
      350      1150 WRITE(7,1161) FSCA(J), (EERMS(J,I), I=1, NS)
      WRITE(7,1160) FSCA(1), (EESTD(1,I), I=1, NS)
      1160 FORMAT(1H0, 8X, 6HESTD: , 9(G10.3, 1X))
      DO 1165 J=2, LGMAX
      355      1165 WRITE(7,1161) FSCA(J), (EESTD(J,I), I=1, NS)
      1161 FORMAT(15X, 9(G10.3, 1X))
      DO 1103 I=1, NS
      FACTOR=1.
      IF(I.EQ.7) FACTOR=180./PI
      IF(I.EQ.8) FACTOR=.5/PI
      360      IF(I.EQ.9) FACTOR=.5/PI
      YMIN=0.
      YMAX=0.
      DO 1101 LG1=1, LGMAX
      365      1101 EEME(LG1)=EERMS(LG1, I)*FACTOR
      YNAME1(1)=YNAM1(1, I)
      YNAME1(2)=YNAM1(2, I)
      K1=MOD(I, 2)
      IF(K1.EQ.1) WRITE(7, 11)
      IF(K1.EQ.1) CALL INTIO(6H NRUN, NRUN, 1, 1)
      370      IF(K1.EQ.0) WRITE(7, 10)
      CALL PLOT(FSCA, EEME, LGMAX, XNAME1, YNAME1, YMIN, YMAX, 0)
      1103 CONTINUE
      IF(.NOT.FILOUT) RETURN
      375      WRITE(7, 11)
      1170 WRITE(7, 1170) (DATOUT(I), I=1, 2)
      FORMAT(13H OUTPUT FILE , 2A10, 1H:/)
      1172 WRITE(7, 1172) DOUT, DELT, HTIMES, LGMAX, KH, TODAY, JBNAM
      FORMAT(1H , A10, 8X, G13.6, 5X, 3(5X, I3, 10X), A10, 8X, A10/)
      WRITE(7, 1174) IDENTS, KSTART
      380      1174 FORMAT(1H , 6(1X, A8, 9X), 6X, I3/)
      WRITE(7, 1176) NRUN, DSNRDB, RHO, BETA, BNS, FSC, TSEP
      1176 FORMAT(1H , 5X, I2, 6X, 6(5X, G13.6)/)
      DO 1175 LGN=1, LGMAX
      385      1175 WRITE(7, 1182) EEME(LGN), EERH(LGN), EEST(LGN), TTCD(LGN), YYMI(LGN),
      *YYMA(LGN), FSCA(LGN), LGN
      1182 FORMAT(1H , 7(G13.6, 5X), I5)
      WRITE(17) DOUT, DELT, HTIMES, LGMAX, KH, TODAY, JBNAM
      WRITE(17) IDENTS, KSTART
      WRITE(17) NRUN, DSNRDB, RHO, BETA, BNS, BRCVR, TSEP
      390      DO 1190 LGN=1, LGMAX
      1190 WRITE(17) EEME(LGN), EERH(LGN), EEST(LGN), TTCD(LGN), YYMI(LGN),
      *YYMA(LGN), FSCA(LGN), LGN
      IX=IATTACH(6LTAPE20, DATOUT)
      IF(IX.NE.0) GO TO 1195
      395      READ(20) DUM, DUM, IDUM, IDUM, DUM, DUM, IDUM
      CALL RETURN(6LTAPE20)
      REWIND 17
      IX=ICATALD(6LTAPE17, DATOUT, 2LPW, 8RHIGHFILL, 2LRP, 365)
      GO TO 1196

```

```
400      1195 CALL RETURN(6LTAPE20)
          REWIND 17
          IX=ICATALO(6LTAPE17,DATOUT,2LXR,8RHIGHFILL,2LRP,365)
          1196 IF(IX.NE.0) CALL INTIQ(6HIX(CA),IX,1,1)
          IF(IX.NE.0) STOP*OUTPUT FILE CATALOG NOT SATISFACTORY*
          435 CALL RETURN(6LTAPE17)
          WRITE (7,1198) (DATOUT(I),I=1,2)
          1198 FORMAT(13H00OUTPUT FILE ,2A10,33H IS WRITTEN, CATALOGED AND CLOSED)
          RETURN
          C
          410 C*****
          C
          1200 CONTINUE
          C THIS EFFECTS CLOSURE OF THE SIMULATION RUN
          WRITE(7,11)
          415 RETURN
          C
          C*****
          C
          END
45000B CH STORAGE USED      15.561 SECONDS
```

## SUBROUTINE CONTRL(ISW)

```

C
C THIS CONDUCTS THE HLS SIMULATION THROUGH A
C RMSE VS. THETA SEP.

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5

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C
REAL LAMDA
INTEGER XNAME1(2),YNAME1(2),YNAME1(2,9)
INTEGER XNAME(2),YNAME(2),DATIN(4),DATOUT(4),DOUT
INTEGER TITLE1(9),FUNCTN(2)
10 LOGICAL NOKLMN,NOLOE,NOAC,KALMAN,LOE,TETHRD,MORE,NFIRST,ADAPTIV,
CFILEIN,FILOUT
COMMON/IDDATA/ISIM,IPHLS,IRCVR,IADAP,ITETHR,IPOPT
COMMON/RCVRO0/THAMAX,THAHIN,TS,TR,OMEGA,TF
COMMON/RCVRO1/NGHIN,NGHAX,DELBL,NGH,IR,IAE
15 COMMON/RCVRO2/RHOMAX,OTHO,TORD,BO,WSCD,NSO(4),NGO(4)
COMMON/RCVRO3/PI,F(8,8),FL25(4),FSAMP,K,KH,TETHRD,NG,NS,JM
COMMON/RCVRO4/DELT,ED(8),GGGT(8,8),H(5,8),ICOUNT,SIGMA
COMMON/RCVRO5/NOLOE,NOKLMN,NOAC,GAMAES(5),RDIAG(5),PHDIAG(8)
COMMON/RCVRO6/PPDIAG(8),RMAT(5,5),PHI(5,5),PA(8,8),LAMDA(5)
20 COMMON/RCVRO7/T(130),V(130)
COMMON/RCVRO8/XSLOE(8),ESLOE(8),ES(8)
COMMON/RCVRO9/BRCVR,BB,PCRIT,CC
COMMON/RCVR10/XS1(8),XS(8)
COMMON/MLS00/ALFA,THE,THEDDT,ALFAR,THR,THRDDT,B,WSC
25 COMMON/MLS001/CSNRT,CSNRF,DSNRDB,RHO,BETA,FSC,LGMAX
COMMON/MLS002/DCSNR,CSNR,LG,TPKT,TPKF
COMMON/MLS003/FL10AE(4,2),FL10(4),DELTAT(2),XO(8,2),YO(4,2)
COMMON/MLS004/BHLS,BBB,MTIMES,MSET,MORE
DIMENSION X(8),THESE(115),XDATUM(115),EEME(13),EERM(13)
30 DIMENSION IDNRS(6),IDASCI(20),IDENTS(6),EEST(13),TTCC(13),YYMI(13)
DIMENSION YYMA(13)
DIMENSION TSEP(13)
DIMENSION EMEA(13,9),EERMS(13,9),EESTD(13,9)
DIMENSION EMEAN(9),EMS(9),ERMS(9),ESD(9)
35 EQUIVALENCE (EEME(1),EMEA(1,2)),(EERM(1),EERMS(1,2)),
*(EEST(1),EESTD(1,2))
EQUIVALENCE (THERR,ES(2))
EQUIVALENCE (ALFA,X(1)),(ISIM,IDNRS(1)),(DOUT,DATOUT(2))
DATA YNAME1/8HALF RMSE,8H ,8HTHE RMSE,8HDEGREES ,
40 *8HYDT RMSE,8HDEG/SEC ,8HALR RMSE,8H ,8HTHR RMSE ,
*8HDEGREES ,8HTRD RMSE,8HDEG/SEC ,8HBET RMSE,8HDEGREES ,
*8HFSC RMSE,8H HZ ,8HFSCDRMSE,8H HZ/SEC /
DATA ABORT/1HA/,SPACE/1H /,NFIRST/.FALSE./,ADAPTIV/.TRUE./
DATA DATIN/10HMLSSIMDATA,10H200000F000,2*0/
45 DATA DATOUT/10HMLSSIMDATA,3*0/
DATA IDASCI/7HCROSSMP,7HRMSE(T),7HRMSE(B),7HRMSE(F),7H
*8H PMLS1 ,8H PMLS2 ,
*8H PMLS3 ,8H THRHLD ,8H OPTIML ,8H SUBOPT ,8H -3 DB ,8HADAPTIV ,
*8HNONADAP ,8HUNTETHRD,8HTETHERED,2H ,8H POPT1 ,8H POPT2 ,
50 *8H POPT3 /
DATA NSTART/3/,IRSIGN/1/,KSTART/11/,TSEPC/-.75/,DTSEP/.25/,FILEIN
*/.FALSE./,FILOUT/.TRUE./
DATA TITLE1/6H ALFA ,6H THETA,6HTHEDDT,6H ALFAR,6HTHETAR,6HTHRD
C,6H B ,6H WSC ,6HWSCD0T/
55 DATA XNAME/8H BETA ,8HDEGREES /,YNAME/8HTHES ERR,8HDEGREES /
DATA XNAME1/8HTHETASEP,8HDEGREES /
DATA FUNCTN/THAZIMUTH,7HELEVAT./

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CTLMSTH2

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C
60      1      GO TO (100,200,300,400,500,600,700,800,900,1000,1100,1200),ISW
        1      FORMAT(1H )
        10     FORMAT(9(/))
        11     FORMAT (1H1)
C
65      C*****
C
        100    CONTINUE
C THIS IDENTIFIES THE SCENARIO AND REINITIALIZES, AS NECESSARY,
CTHE FOLLOWING RECEIVER PARAMETERS
        CSIGMA,IAE,OSNRDB,RHO,FSC,BETA,JH,BMLS
70      IF(NFIRST) GO TO 155
        NOAC=.TRUE.
        NFIRST=.TRUE.
        JBNAM=JOBNAME(I)
75      ISIM=2
        IMOD=2
        110    WRITE (7,110)
        FORMAT(25HIRMSE VS. THESEP SCENARIO/)
        CALL LOGIO(6HFILEIN,FILEIN,0)
        IF (.NOT.FILEIN) NSTART=0
80      IF(.NOT.FILEIN) GO TO 122
        IX=IATTACH(6LTAPE15,DATIN)
        IF(IX.NE.0) CALL INTIO(6HIX(AT),IX,1,1)
        IF(IX.NE.0) STOP#INPUT FILE ATTACH NOT SATISFACTORY#
85      120    WRITE(7,120) (DATIN(I),I=1,2)
        FORMAT(23H THIS READS INPUT FILE",2A10/)
        122    CALL LOGIO(6HFILOUT,FILOUT,0)
        CALL INTIO(6HNSTART,NSTART,100,0)
        NSTOP=NSTART
90      CALL INTIO(6H NSTOP,NSTOP,100,0)
        CALL LOGIO(6HTETHRD,TETHRD,0)
        IF(IRCVR.EQ.1) GO TO 125
        CALL LOGIO(6HADAPTIV,ADAPTIV,0)
        125    CONTINUE
        IF(TETHRD) ITETHR=2
95      IF(ADAPTIV) GO TO 135
        IRSIGN=-1
        IADAP=3
        135    CONTINUE
        DD 145 I=2,6
100     IASC=3*(I-1)+IDNRS(I)+2
        IDENTS(I)=IDASCI(IASC)
        145    CONTINUE
        ENCODE(8,150,IDENTS(1)) IDASCI(ISIM),IMOD
105     150    FORHAT(A7,I1)
        WRITE (7,152) IDNRS,IMOD
        152    FORMAT (1H ,6I1,1X,I1/)
        WRITE (7,153) IDENTS
        153    FORMAT (1H ,A8)
        CALL INTIO(6H LGMAX,LGMAX,13,0)
110     CALL INTIO(6H KM,KM,115,0)
        CALL REALIO(6H TSEPD,TSEPD,0)
        CALL REALIO(6H DTSEP,DTSEP,0)
        KSTART=MINO(KM,KSTART)
        DD 154 I=1,LGHAX

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115      154  TSEP(I)=TSEP0+DTSEP*(I-1)
          KMNET=KM-KSTART+1
          FSCMIN=1./(DELTA(IAE)*KMNET)
          NRUN=NSTART-1
          DSNRDB=20.
120      RHO=0.5
          BETA=45.
          IFS=1
          BMLS=1.
          BRCVR=1.
125      155  CONTINUE
          IF(FILEIN) GOTO 158
          NRUN=NRUN+1
          WRITE(7,11)
          CALL INTIO(6H NRUN, NRUN, 1, 1)
130      CALL REALIO(6HDSNRDB, DSNRDB, 0)
          CALL REALIO(6H RHO, RHO, 0)
          CALL REALIO(6H BETA, BETA, 0)
          CALL INTIO(6H IFS, IFS, 100, 0)
          CALL REALIO(6H BMLS, BMLS, 0)
135      CALL REALIO(6H BRCVR, BRCVR, 0)
          GOTO 167
          158  CONTINUE
          READ(15,160) NRUN, DSNRDB, RHO, BETA, IFS, BMLS, BRCVR
          IF(EOF(15))170,165
140      160  FORMAT(15,3G10.3,5X,15,2G10.3)
          165  IF(NRUN.LT.NSTART) GO TO 158
          167  IF(NRUN.GE.NSTOP) MORE=.FALSE.
          FSC=IFS*FSCMIN
          XO(5,IAE)=XO(2,IAE)-TSEP(1)
145      XO(3,IAE)=0.
          XO(6,IAE)=0.
          RETURN
170      STOP#EOF REACHED ON INPUT FILE#
          C
150      C*****
          C
          200  CONTINUE
          C THIS OUTPUTS BASIC SIMULATION DATA OF INTEREST, SUCH AS
          C THE ANGLE FUNCTION, INITIAL STATE, ETC.
155      WRITE(7,210) NRUN,DSNRDB,RHO,BETA,IFS,BMLS,BRCVR
          210  FORMAT(5HNRUN,12X,6HDSNRDB,16X,3HRHO,16X,4HBETA,16X,4HIFSC,16X,
          *4HBMLS,15X,5HBRCVR/1H0,14,3(10X,G10.3),12X,15,3X,
          *2(10X,G10.3))
          IF(.NOT.FILEOUT) GOTO 245
160      IF(NRUN.LE.9) ENCODE(10,220,DOUT) IDNRS,1HU,IMDD,1H0,NRUN
          220  FORMAT(6I1,A1,I1,A1,I1)
          IF(NRUN.GE.10) ENCODE(10,230,DOUT) IDNRS,1HU,IMDD,NRUN
          230  FORMAT(6I1,A1,I1,I2)
          IX=IREQST(6LTAPE17,3L*PF)
165      IF(IX.NE.0) CALL INTIO(6HIX(RQ),IX,1,1)
          IF(IX.NE.0) STOP#OUTPUT FILE REQUEST NOT SATISFACTORY#
          WRITE(7,240) (OATOUT(I),I=1,2)
          240  FORMAT(25HTHIS WRITES OUTPUT FILE",2A10)
          245  CALL DATE(TODAY)
170      WRITE(7,250) FUNCTN(IAE),IAE
          250  FORMAT(1H0,A7,15H FUNCTION (IAE=,I1,1H))

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260 WRITE (7,260) ((I,X(I)),I=1,8)
    FORMAT (15H0INITIAL STATE://(3H X(,I1,4H) = ,G13.6))
175 270 WRITE(7,270) IDENT5(2)
    FORMAT(1H0,A7)
    RETURN
C
C*****
C
180 300 CONTINUE
C THIS IDENTIFIES THE BASIC RECEIVER STRUCTURE (THRHLD,OPT,SUBOPT)
CAND REINITIALIZES, AS NECESSARY, THE FOLLOWING RCVR DATA
CIR (NEGATE ONLY), NOAC,NOKLMN,NOLDE,BRCVR,DELBL,TETHRD
    ITIT=MIN0(IRCVR,2)
185 C
C NEGATE IR WITH THE FOLLOWING FOR NONADAPTIVE RECEIVER
    IR=ISIGN(IR,IRSIGN)
C
    RETURN
190 C
C*****
C
    400 CONTINUE
C THIS OUTPUTS BASIC RECEIVER DATA OF INTEREST
195 WRITE(7,410) (IDENTS(I),I=3,4),IR,NG,NS
    410 FORMAT (1H0,A8,4HRCVR/1H0,A8,6HDESIGN/5H (IR=,I2,4H,NG=,I1,
    * 4H,NS=,I1,1H))
    WRITE(7,420) (IDENTS(I),I=5,6)
    420 FORMAT(1H0,A8/1H0,A7/)
200 RETURN
C
C*****
C
    500 CONTINUE
205 C THIS SETS-UP THE MSET-LOOP
    ICOUNT=0
    DO 510 I=1,LGHAX
    YYMI(I)=1.E322
    510 YYMA(I)=-1.E322
210 RETURN
C
C*****
C
    600 CONTINUE
215 C THIS SETS-UP THE LG-LOOP FOR THE (MSET)-TH SERIES OF SETS
    RETURN
C
C*****
C
220 700 CONTINUE
C THIS SETS-UP THE K-LOOP FOR THE (LG)-TH SET OF KM SCANS
    X(5)=X(2)-TSEP(LG)
    X(7)=X0(7,IAE)
    DUH=GAUSS(1.0)
225 CALL INTID(6H NRUN,NRUN,1,1)
    WRITE(7,705) LG,TSEP(LG),X(5)
    705 FORMAT(1H1,4X,3HLG=,I2,5X,7HTHESEP=,G13.6,5X,5HX(5)=,G13.6/)
    CALL INTID(6H KM,KM,1,1)

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230 710 WRITE(7,710) (TITLE(I),I=1,NS)
      FORMAT(6H0 K,4X,5HCSNRT,4X,5HQTY ,9(3X,A6,2X))
      DO 712 I=1,NS
      EMEAN(I)=0.
      EMS(I)=0.
      LASTCT=0
235 712 ICOUNT=0
      DO 730 IPA=1,NS
      DO 720 JPA=1,NS
      PA(IPA,JPA)=0.
      720 CONTINUE
240 730 CONTINUE
      RETURN
      C
      C*****
      C
245 800 CONTINUE
      C THIS INITIALIZES THE K-TH SCAN
      SEP=SPACE
      RETURN
      C
250 C*****
      C
      900 CONTINUE
      C THIS SAVES/PREPROCESSES DATA FROM THE K-TH SCAN
      IF(ICOUNT.NE.LASTCT) SEP=ABORT
255 DO 905 I=1,NS
      905 ES(I)=X(I)-XS(I)
      IF(NS.GE.7) ES(7)=ABS(X(7))-ABS(XS(7))
      IF(NS.GE.8) ES(8)=ABS(X(8))-ABS(XS(8))
      BETTA=(180./PI)*X(7)
260 COL8=THERR
      IF (IRCVR .NE. 1) COL8=SQRT(PPDIAG(2))
      IF (IRCVR .EQ. 1) CALL DFLTR1(COL8,THERR,FL10)
      IF((NRUN.EQ.NSTART.AND.LG.EQ.1).OR.(K.EQ.KM)) GOTD 906
      GO TO 950
265 906 WRITE(7,910) K,CSNRT,(X(I),I=1,NS)
      910 FORMAT(3H0 ,I3,2X,G10.3,5H X= ,2X,9(G10.3,1X))
      WRITE(7,920) (XS(I),I=1,NS)
      920 FORMAT(18X,5H XS= ,2X,9(G10.3,1X))
      WRITE(7,930) (ES(I),I=1,NS)
270 930 FORMAT(18X,5H ES= ,2X,9(G10.3,1X))
      IF(IRCVR.EQ.1) WRITE(7,940) COL8
      940 FORMAT(8X,15HUNFILT. ES(2)= ,13X,G10.3)
      950 XDATUM(K)=BETTA
      THESER(K)=THERR
      LASTCT=ICOUNT
275 IF(K.LT.KSTART) RETURN
      DO 960 I=1,NS
      EMEAN(I)=EMEAN(I)+ES(I)
      960 EMS(I)=EMS(I)+ES(I)**2
280 RETURN
      C
      C*****
      C
285 1000 CONTINUE
      C THIS SAVES/PROCESSES/OUTPUTS DATA FROM THE (LG)-TH SET OF KM SCANS

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DO 1005 I=1,NS
EMEAN(I)=EMEAN(I)/KMNET
EMS(I)=EMS(I)/KMNET
ERMS(I)=SQRT(EMS(I))
290   *ESD(I)=SQRT(EMS(I)-EMEAN(I)**2)
      1005 CONTINUE
      XW=ICOUNT
      TDCOUNT=100.*XW/KM
      WRITE(7,1009)
295   1009 FORMAT(3(/))
      WRITE(7,1010)KMNET
      1010 FORMAT(5X,26HERROR SAMPLE STATISTICS: (,I3,9H SAMPLES))
      IF(IRCVR.EQ.1) WRITE (7,1015)
      1015 FORMAT(5X,31HTHRESHOLD RCVR (FILTERED ERROR))
300   WRITE(7,1020)(TITLE1(I),I=1,NS)
      1020 FORMAT(1H0,20X,4HQTY ,9(3X,A6,2X))
      WRITE(7,1030)(EMEAN(I),I=1,NS)
      1030 FORMAT(1H0,16X,8HEMEAN = ,9(G10.3,1X))
      WRITE(7,1040)(ERMS(I),I=1,NS)
305   1040 FORMAT(18X,7HERMS = ,9(G10.3,1X))
      WRITE(7,1050)(ESD(I),I=1,NS)
      1050 FORMAT(19X,6HESD = ,9(G10.3,1X))
      IF(IRCVR.EQ.1)WRITE(7,1060)TDCOUNT
310   1060 FORMAT(/7H ,4X,F7.2,22HZ OF SCANS ARE ABORTED)
      IF(IRCVR.NE.1)WRITE(7,1070)(GGGT(I),I=1,NS)
      1070 FORMAT(5(/),4X,35H ON LAST SCAN, DIAGONAL OF GGGT WAS/26X
      C9(G10.3,1X))
      DO 1071 I=1,NS
315   EMEAN(LG,I)=EMEAN(I)
      ERMS(LG,I)=ERMS(I)
      1071 EESD(LG,I)=ESD(I)
      DO 1072 I=1,KM
      YYMI(LG)=AMINI(THESER(I),YYMI(LG))
320   1072 YYMA(LG)=AMAX1(THESER(I),YYMA(LG))
      TTCD(LG)=TDCOUNT
      IF(LG.NE.1) RETURN
      YMIN=YMAX=0.
      WRITE(7,11)
325   CALL PLOTTR(XDATUM,THESER,KM,XNAME,YNAME,YMIN,YMAX,0)
      RETURN
      C
      C*****
      C
330   1100 CONTINUE
      C THIS SAVES/PROCESSES/OUTPUTS DATA FROM THE (MSET)-TH SERIES OF
      CLGMAX SETS OF KM SCANS
      WRITE(7,11)
      CALL INTIO(6H NRUN,NRUN,1,1)
      WRITE(7,1110) 6HTHESEP, (TITLE1(I),I=1,NS)
335   1110 FFORMAT(1H0,10X,3HQTY ,9(3X,A6,2X))
      WRITE(7,1120)TSEP(1),(EEMEA(1,I),I=1,NS)
      1120 FORMAT(1H0, 7X,7HEMEAN: ,9(G10.3,1X))
      DO 1130 J=2,LGMAX
340   1130 WRITE(7,1161) TSEP(J),(EEMEA(J,I),I=1,NS)
      WRITE(7,1140)TSEP(1),(ERMS(1,I),I=1,NS)
      1140 FORMAT(1H0, 8X,6HERMS: ,9(G10.3,1X))
      DO 1150 J=2,LGMAX

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1150 WRITE(7,1161) TSEP(J),(EERHS(J,I),I=1,NS)
WRITE(7,1160)TSEP(1),(EESTD(1,I),I=1,NS)
345 1160 FORMAT(1H0, 8X,6HESTD: ,9(G10.3,1X))
      DD 1165 J=2,LGMAX
1165 WRITE(7,1161) TSEP(J),(EESTD(J,I),I=1,NS)
1161 FORMAT(15X,9(G10.3,1X))
      IF (.NOT.FILOUT) GOTO 1199
350 WRITE(7,11)
      WRITE(7,1170) (DATOUT(I),I=1,2)
1170 FORMAT(13H OUTPUT FILE ,2A10,1H:/)
      WRITE(7,1172) DOUT,DELT,MTIMES,LGMAX,KM,TODAY,JBNAM
1172 FORMAT(1H ,A10,8X,G13.6,5X,3(5X,13,10X),A10,8X,A10/)
355 WRITE(7,1174) IDENT, KSTART
1174 FORMAT(1H ,6(1X,A8,9X),6X,13/)
      WRITE(7,1176) NRUN,DSNRDB,RHO,BETA,FSC,BMLS,BRCVR
1176 FORMAT(1H ,5X,I2,6X,6(5X,G13.6)/)
      DD 1175 LGN=1,LGMAX
360 1175 WRITE(7,1182) EEME(LGN),EERM(LGN),EEST(LGN),TTCD(LGN),YYMI(LGN),
      *YYMA(LGN),TSEP(LGN),LGN
1182 FORMAT(1H ,7(G13.6,5X),I5)
      WRITE(17) DOUT,DELT,MTIMES,LGMAX,KM,TODAY,JBNAM
      WRITE(17) IDENT, KSTART
365 WRITE(17) NRUN,DSNRDB,RHO,BETA,FSC,BMLS,BRCVR
      DD 1190 LGN=1,LGMAX
1190 WRITE(17) EEME(LGN),EERM(LGN),EEST(LGN),TTCD(LGN),YYMI(LGN),
      *YYMA(LGN),TSEP(LGN),LGN
      IX=IATTACH(6LTAPE20,DATOUT)
370 IF(IX.NE.0) GO TO 1195
      READ(20) DUM,DUM,IDUM, IDUM, IDUM,DUM, IDUM
      CALL RETURN(6LTAPE20)
      REWIND 17
375 IX=ICATALOG(6LTAPE17,DATOUT,2LPW,8RHIGHFILL,2LRP,365)
      GO TO 1196
1195 CALL RETURN(6LTAPE20)
      REWIND 17
1196 IF(IX.NE.0) CALL INTIO(6HIX(CA),IX,1,1)
380 IF(IX.NE.0) STOP OUTPUT FILE CATALOG NOT SATISFACTORY#
      CALL RETURN(6LTAPE17)
      WRITE (7,1198) (DATOUT(I),I=1,2)
1198 FORMAT(13HOUTPUT FILE ,2A10,33H IS WRITTEN, CATALOGED AND CLOSED)
1199 CONTINUE
385 DO 1103 I=1,NS
      FACTOR=1.
      IF(I.EQ.7) FACTOR=180./PI
      IF(I.EQ.8) FACTOR=.5/PI
      IF(I.EQ.9) FACTOR=.5/PI
390 YMIN=0.
      YMAX=0.
      DO 1101 LG1=1,LGMAX
1101 EEME(LG1)=EERHS(LG1,I)*FACTOR
      YNAME1(1)=YNAM1(1,I)
395 YNAME1(2)=YNAM1(2,I)
      K1=MOD(I,2)
      IF(K1.EQ.1)WRITE(7,11)
      IF(K1.EQ.1) CALL INTIO(6H NRUN,NRUN,1,1)
      IF(K1.EQ.0) WRITE(7,10)

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SUBROUTINE CONTRL(ISW)
C
C THIS CONDUCTS THE MLS SIMULATION THROUGH A
C STUDY OF LOE PERFORMANCE
5 C THIS VERSION INVESTIGATES THE ERROR PERFORMANCE
C
REAL LAMDA
REAL E(2),TE(2),MSE
LOGICAL NOKLMN,NOLOE,NOAC,KALMAN,LOE,TETHRD,MORE,NFIRST,ADAPT
10 C INTEGER FUNCTN(2)
REAL XNA(2),YNA(2)
COMMON/IODATA/ISIM,IPMLS,IRCVR,IADAP,ITETHR,IPOPT
COMMON/RCVRO0/THAMAX,THAMIN,TS,TR,OMEGA,TF
COMMON/RCVRO1/NGMIN,NGMAX,DELBL,NGH,IR,IAE
15 COMMON/RCVRO2/RHOMAX,DTHD,TDRD,BO,WSCO,NSQ(4),NGD(4)
COMMON/RCVRO3/PI,F(8,8),FL25(4),FSAMP,K,KM,TETHRD,NG,NS,JH
COMMON/RCVRO4/DELT,ED(8),GGGT(8,8),H(5,8),ICOUNT,SIGMA
COMMON/RCVRO5/NLOE,NOKLMN,NOAC,GAAES(5),RDIAG(5),PHDIAG(8)
20 COMMON/RCVRO6/PPDIAG(8),RHAT(5,5),PHI(5,5),PA(8,8),LAMDA(5)
COMMON/RCVRO7/T(130),V(130)
COMMON/RCVRO8/XSLOE(8),ESLOE(8),ES(8)
COMMON/RCVRO9/BRCVR,BB,POCRIT,CC
COMMON/RCVR10/XS1(8),XS(8)
COMMON/MLSC00/ALFA,THE,THEDOT,ALFAR,THR,THRDOT,B,WSC
25 COMMON/MLS001/CSNRT,CSNRF,DSNRDB,RHO,BETA,FSC,LGMAX
COMMON/MLS002/OCSNR,CSNR,LG,TPKT,TPKF
COMMON/MLS003/FLIOAE(4,2),FLIO(4),DELTAT(2),XD(8,2),YD(4,2)
COMMON/MLS004/BMLS,BBB,MTIMES,MSET,MORE
DIMENSION X(8),TSEP(20),BETA(20),BULK(25,10),BULL(15,10),XE(8)
30 DIMENSION DMAT(5,5)
DIMENSION NAMES(11),NAME5(11),NAME8(5)
DIMENSION IDNRS(6),IDASCI(24),IDENTS(6)
DIMENSION AK(50),ATE(50),PABORT(10),PABMAX(10)
EQUIVALENCE (ALFA,X(1)),(ISIM,IDNRS(1))
35 DATA ABORT/1HA/,SPACE/1H/,ADAPT/TRUE./
DATA IDASCI/7HCROSSMP,7HRMSE(T),7HRMSE(B),7HRMSE(F),7HACQSITN,
*2*7H ,7HLOERMSE,7HGENERAL,8H PMLS1 ,8H PMLS2 ,
*8H PMLS3 ,8H THRLD ,8H OPTIML ,8H SUBOPT ,8H -3 DB ,8HADAPTIV ,
*8HNONADAP ,8HUNTETHRD,8HTETHERED,2H ,8H POPT1 ,8H POPT2 ,
40 *8H POPT3 /
DATA KSTART/11/,IRSIGN/1/,KMNET/20/
DATA FUNCTN/7HAZIMUTH,7HELEVAT./
DATA TSEPMN/-0.50/,DTSEP/0.25/
DATA NAMES/6H E1AVG,6H E2AVG,6H E1MIN,6H E2MIN,
45 * 6H E1MAX,6H E2MAX,6H E1RMS,6H E2RMS,6HARIAVG,6HGEOAVG,
* 6H RMSE/
DATA NAME5/3HAVG,3HAVG,3HMIN,3HMIN,3HMAX,3HMAX,3HRMS,3HRMS,
* 3HAVG,3HAVG,3HAVG/
DATA NAME8/6H TEAVG,6H TEMIN,6H TEMAX,6H TERMS,2H /
50 DATA BETMIN/0./
DATA XNA/6H SCAN ,8H K /
DATA YNA/8H X2-XS2 ,8H /
C
GO TO (100,200,300,400,500,600,700,800,900,1000,1100,1200),ISW
55 1 FORMAT(1H )
10 FORMAT(9(/))
11 FORMAT(1H1)

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```

C
C*****
60 C
C CONTINUE
C THIS IDENTIFIES THE SCENARIO AND REINITIALIZES, AS NECESSARY,
C THE FOLLOWING RECEIVER PARAMETERS
65 CSIGMA,IAE,DSNRDB,RHO,FSC,BETA,IM,BHLS
    MORE=.FALSE.
    JBNAM=JOBNAME(I)
    ISIM=6
    IMOD=3
    WRITE (7,110)
70 110 FORMAT (22H1LOE PERFORMANCE STUDY)
    CALL INTIO (6H KMNET,KMNET,100,0)
    DELBL=.01
    LGMAX=10
    MTIMES=20
75 TETHRO=.TRUE.
    NOLOE=.FALSE.
    NOKLMN=.TRUE.
    CALL REALIO (6HDSNRDB,DSNRDB,0)
    CALL REALIO (6H RHO,RHO,0)
80 CALL REALIO (6HTSEPMN,TSEPMN,0)
    CALL REALIO (6H DTSEP,DTSEP,0)
    CALL INTIO (6H NTSEP,LGMAX,20,0)
    CALL REALIO (6HBETHIN,BETHIN,0)
    CALL INTIO (6HNOBSEP,MTIMES,20,0)
85 DBETA=360./MTIMES
    DO 120 I=1, LGMAX
70 120 TSEP(I)=TSEPMN+(I-1)*DTSEP
    DO 126 I=1, MTIMES
90 126 BETA(I)=BETHIN+(I-1)*DBETA
    XO(3,IAE)=0.
    XO(5,IAE)=XO(2,IAE)-TSEPMN
    XO(6,IAE)=0.
    BETA=BETHIN
    FSC=C.
95 CALL LOGIO (6HTETHRO,TETHRO,0)
    IF (IRCVR.EQ.1) GO TO 125
    CALL LOGIO (6H NOLOE,NOLOE,0)
    CALL LOGIO (6HNOKLMN,NOKLMN,0)
    IF (NOKLMN) KSTART=1
100 CALL LOGIO (6HADAPTV,ADAPTV,0)
70 125 CONTINUE
    KM=KSTART+KMNET-1
    CALL INTIO (6HKSTART,KSTART,1,1)
    CALL INTIO (6H KM,KM,1,1)
105 IF (TETHRO) ITETHR=2
    IF (ADAPTV) GO TO 135
    IRSIGN=-1
    IADAP=3
135 CONTINUE
    DO 145 I=2,6
110 IASC=3+(I-1)*IDNRS(I)+6
    IDENTS(I)=IDASCI(IASC)
145 CONTINUE
    ENCODE(0,150,IDENTS(1)) IDASCI(ISIM),IHOD

```

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115      150  FORMAT(A7,I1)
          WRITE (7,152) IDNRS,IMOD
          152  FORMAT (1H,6I1,1X,I1/)
          WRITE (7,153) IDENT5
          153  FORMAT (1H,A8)
120      RETURN
          C
          C*****
          C
          200  CONTINUE
125      C THIS OUTPUTS BASIC SIMULATION DATA OF INTEREST, SUCH AS
          C THE ANGLE FUNCTION, INITIAL STATE, ETC.
          CALL DATE(TODAY)
          WRITE (7,250) FUNCTN (IAE),IAE
          250  FORMAT (1H0,A7,15H FUNCTION (IAE=,I1,1H))
          133  WRITE (7,260) ((I,X(I)),I=1,8)
          260  FORMAT (15H0INITIAL STATE://(3H X(,I1,4H) = ,G13.6))
          WRITE (7,270) IDENT5(2)
          270  FORMAT(1H0,A7)
          RETURN
135      C
          C*****
          C
          300  CONTINUE
          C THIS IDENTIFIES THE BASIC RECEIVER STRUCTURE (THRHL0,OPT,SUBOPT)
          C AND REINITIALIZES, AS NECESSARY, THE FOLLOWING RCVR DATA
140      CIR (NEGATE ONLY), NOAC,NOKLHN,NOLDE,BRCVR,DELBL,TETHRO
          ITIT=MING(IRCVR,2)
          C
          C NEGATE IR WITH THE FOLLOWING FOR NONADAPTIVE RECEIVER
145      IF(IRSIGN.LT.0) IR=-IR
          C
          RETURN
          C
          C*****
150      C
          400  CONTINUE
          C THIS OUTPUTS BASIC RECEIVER DATA OF INTEREST
          WRITE (7,410) (IDENT5(I),I=3,4),IR,NG,NS
          410  FORMAT (1H0,A8,4HRCVR/1H0,A8,6HDESIGN/5H (IR=,I2,4H,NG=,I1,
155      * 4H,NS=,I1,1H))
          WRITE (7,420) (IDENT5(I),I=5,6)
          420  FORMAT(1H0,A8/1H0,A7/)
          RETURN
160      C
          C*****
          C
          500  CONTINUE
          C THIS SETS-UP THE MSET-LOOP
          ICOUNT=0
165      DO 502 J=1,LGMAX
          BULL(11,J)=0.
          BULL(12,J)=+1.E322
          BULL(13,J)=-1.E322
          BULL(14,J)=0.
170      BULK(15,J)=0.
          BULK(16,J)=0.

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      BULK(17,J)=+1.E322
      BULK(18,J)=+1.E322
      BULK(19,J)=-1.E322
175     BULK(20,J)=-1.E322
      PABMAX(J)=-1.E322
      BULK(21,J)=0.
      BULK(22,J)=0.
      BULK(23,J)=0.
180     BULK(24,J)=0.
      BULK(25,J)=0.
      502 CONTINUE
      CALL INTID (6HMTIMES,HTIMES,1,1)
      WRITE(7,510)
185     510 FORMAT(1H1,40X,21HLOE ERROR PERFORMANCE/)
      WRITE(7,511) (TSEP(I),I=1,LGMAX)
      511 FORMAT(1H0,7HTHESEP=,7X,10(1X,F8.5,2X))
      WRITE(7,512)
190     512 FORMAT(1H0,5HBETA:)
      RETURN
C
C*****
C
600 CONTINUE
195     C THIS SETS-UP THE LG-LOOP FOR THE (MSET)-TH SERIES OF SETS
      BETA=BETA*(MSET)
      XO(7,IAE)=PI*BETA/180.
      X(7) = XO (7,IAE)
      IF(MOD(MSET,8).EQ.0) WRITE(7,511)(TSEP(I),I=1,LGMAX)
200     RETURN
C
C*****
C
700 CONTINUE
205     C THIS SETS-UP THE K-LOOP FOR THE (LG)-TH SET OF KM SCANS
      THESEP=TSEP(LG)
      X(5) = X(2)-THESEP
      DUM=GAUSS (1.0)
210     LASTCT=0
      ICGUNT=0
      FL10(4)=0.
      THETA=0.
      THETMN=+1.E322
      THETMX=-1.E322
215     THERMS=0.
      E1AVG=0.
      E2AVG=0.
      E1MIN=+1.E322
      E2MIN=+1.E322
220     E1MAX=-1.E322
      E2MAX=-1.E322
      E1RMS=0.
      E2RMS=0.
      MSE=0.
225     LASTCT=0
      DO 705 I=1,8
      DO 705 J=1,8
230     PA(I,J)=0.

```

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```

      RETURN
230 C *****
      C
      800 CONTINUE
      C THIS INITIALIZES THE K-TH SCAN
235 810 DO 810 I=1,5
      RDIAG(I)=1.
      IF(TETHKD) RETURN
      RETURN
      C
240 C *****
      C
      900 CONTINUE
      C THIS SAVES/PREPROCESSES DATA FROM THE K-TH SCAN
      C
245 C FOLG SHOULD BE IN RCVR
      C
      XS(1)=ABS(XS(1))
      XS(4)=ABS(XS(4))
      IF(ICOUNT.NE.LASTCT) SEP=ABORT
250 THERR=X(2)-XS(2)
      IF (IRCVR.EQ.1) CALL DFLTR1 (THERR,THERR,FL10)
      LASTCT=ICOUNT
      IF(K.LT.KSTART) RETURN
      TE(1)=X(1)-XS(1)
255 TE(2)=THERR
      THETA=THETA+TE(2)
      THETMN=AMIN1(THETMN,TE(2))
      THETMX=AMAX1(THETMX,TE(2))
      THERMS=THERMS+(TE(2)**2)
260 IF(IRCVR.EQ.1) RETURN
      IF((RDIAG(1).GT.1.E-293).AND.(RDIAG(2).GT.1.E-293)) GOTO 910
      CALL MATOUT(6H PHI =,PHI,NG,NG,5,1)
      CALL MATOUT(6HRMAT =,RMAT,NG,NG,5,1)
      CALL MATMUL(5,NG,NG,5,NG,NG,NG,NG,5,1)
265 CALL MATOUT(6HR*PHI =,DMAT,NG,NG,5,1)
      STOP *BAD MATRIX PHI*
      910 CONTINUE
      SIG1=SQRT(RDIAG(1))
      SIG2=SQRT(RDIAG(2))
270 E(1)=TE(1)/SIG1
      E(2)=TE(2)/SIG2
      E1AVG=E1AVG+E(1)
      E2AVG=E2AVG+E(2)
      E1MIN=AMIN1(E(1),E1MIN)
275 E2MIN=AMIN1(E(2),E2MIN)
      E1MAX=AMAX1(E(1),E1MAX)
      E2MAX=AMAX1(E(2),E2MAX)
      E1RMS=E1RMS+(E(1)**2)
      E2RMS=E2RMS+(E(2)**2)
280 DO 920 I=1,2
      DO 920 J=1,2
      920 HSE=HSE+TE(I)*TE(J)*PHI(I,J)
      RETURN
285 C *****

```

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```

C
1000 CONTINUE
C THIS SAVES/PROCESSES/OUTPUTS DATA FROM THE (LG)-TH SET OF KH SCANS
290 BULL(1, LG)=THETA/KMNET
      BULL(2, LG)=THETMN
      BULL(3, LG)=THETMX
      BULL(4, LG)=SQRT(THERMS/KMNET)
      BULL(11, LG)=BULL(11, LG)+BULL(1, LG)
      BULL(12, LG)=AMINI(BULL(12, LG), THETMN)
295 BULL(13, LG)=AMAX1(BULL(13, LG), THETMX)
      BULL(14, LG)=BULL(14, LG)+(THERMS/KMNET)
      PABORT(LG)=(100.*ICOUNT)/KH
      PABMAX(LG)=AMAX1(PABMAX(LG), PABORT(LG))
      IF (IRCVR.EQ.1) RETURN
300 BULK(1, LG)=E1AVG/KMNET
      BULK(2, LG)=E2AVG/KMNET
      BULK(3, LG)=E1MIN
      BULK(4, LG)=E2MIN
      BULK(5, LG)=E1MAX
305 BULK(6, LG)=E2MAX
      BULK(7, LG)=SQRT(E1RMS/KMNET)
      BULK(8, LG)=SQRT(E2RMS/KMNET)
      BULK(9, LG)=SQRT((BULK(7, LG)**2+BULK(8, LG)**2)/2)
      BULK(10, LG)=SQRT(BULK(7, LG)*BULK(8, LG))
310 BULK(11, LG)=SQRT(MSE/KMNET)
      BULK(15, LG)=BULK(15, LG)+BULK(1, LG)
      BULK(16, LG)=BULK(16, LG)+BULK(2, LG)
      BULK(17, LG)=AMINI(BULK(17, LG), BULK(3, LG))
      BULK(18, LG)=AMINI(BULK(18, LG), BULK(4, LG))
315 BULK(19, LG)=AMAX1(BULK(19, LG), BULK(5, LG))
      BULK(20, LG)=AMAX1(BULK(20, LG), BULK(6, LG))
      BULK(21, LG)=BULK(21, LG)+BULK(7, LG)**2
      BULK(22, LG)=BULK(22, LG)+BULK(8, LG)**2
      BULK(23, LG)=BULK(23, LG)+BULK(9, LG)**2
320 BULK(24, LG)=BULK(24, LG)+BULK(10, LG)**2
      BULK(25, LG)=BULK(25, LG)+BULK(11, LG)**2
      RETURN
C
C *****
325 C
      1100 CONTINUE
C THIS SAVES/PROCESSES/OUTPUTS DATA FROM THE (MSET)-TH SERIES OF
      CLGMAX SETS OF KH SCANS
330 WRITE(7, 1101) BETA
      1101 FORMAT(1H0, F7.2)
      DO 1160 I=1, 4
      WRITE(7, 1150) NAME8(I), (BULL(I, J), J=1, LGMAX)
      1150 FORMAT(1H, 7X, A6, 1H=, 10(1X, G10.3))
335 1160 CONTINUE
      IF(IRCVR.EQ.1) WRITE(7, 1150) 6HZABORT, (PABORT(J), J=1, LGMAX)
      IF(IRCVR.EQ.1) RETURN
      WRITE(7, 1103) (BULK(1, J), J=1, LGMAX)
      1103 FORMAT(1H, 7X, 7H E1AVG=, 10(1X, G10.3))
      DO 1190 I=2, 11
340 WRITE(7, 1115) NAMES(I), (BULK(I, J), J=1, LGMAX)
      1115 FORMAT(1H, 7X, A6, 1H=, 10(1X, G10.3))
      1190 CONTINUE

```

A-52

```

      RETURN
      C
345      C*****
      C
      1200 CONTINUE
      C THIS EFFECTS CLOSURE OF THE SIMULATION RUN
      DO1220 I=1, LGMAX
350      BULL(11,I)=BULL(11,I)/MTIMES
      BULL(14,I)=SQRT(BULL(14,I)/MTIMES)
      IF(IRCVR.EQ.1) GOTO 1220
      BULK(15,I)=BULK(15,I)/MTIMES
      BULK(16,I)=BULK(16,I)/MTIMES
355      BULK(21,I)=SQRT(BULK(21,I)/MTIMES)
      BULK(22,I)=SQRT(BULK(22,I)/MTIMES)
      BULK(23,I)=SQRT(BULK(23,I)/MTIMES)
      BULK(24,I)=SQRT(BULK(24,I)/MTIMES)
      BULK(25,I)=SQRT(BULK(25,I)/MTIMES)
360      1220 CONTINUE
      WRITE(7,1230)
      1230  FORMAT(1H0,9HWRT BETA: /)
      DO 1233 I=11,14
      I11=I-10
365      WRITE(7,1234) NAME5(2*I11),NAME8(I11),(BULL(I,J),J=1, LGMAX)
      1234  FORMAT(1H ,3X,A4,A6,1H=,10(1X,G10.3))
      1233 CONTINUE
      IF(IRCVR.EQ.1) WRITE(7,1234) 4HMAX ,6HZABGRT,(PABMAX(J),J=1, LGMAX)
      IF(IRCVR.EQ.1) GOTO 1248
370      DO 1245 I=15,25
      IT=I-14
      WRITE(7,1240) NAME5(IT),NAME8(IT),(BULK(I,J),J=1, LGMAX)
      1240  FORMAT(1H ,3X,A4,A6,1H=,10(1X,G10.3))
      1245 CONTINUE
375      1248 CONTINUE
      WRITE(7,511) (TSEP(I),I=1, LGMAX)
      WRITE(7,1250)
      1250  FORMAT(1H0)
      IF(IRCVR.NE.1) WRITE(7,1260)(GQGT(I,I),I=1, NS)
380      1260  FORMAT(13H GQGT(I,I) = ,G13.6,7(1X,G13.6))
      RETURN
      C
      C*****
      C
385      END
440008 CM STORAGE USED      7.674 SECONDS

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SUBROUTINE MLSSUB
REAL LAMDA
LOGICAL NGKLMN, NOLOE, NOAC, KALMAN, LOE, TETHRD, MORE
COMMON/RCVRO0/THAMAX, THAMIN, TS, TR, OMEGA, TF
5 COMMON/RCVRO1/NGMIN, NGMAX, DELBL, NGM, IR, IAE
COMMON/RCVRO2/RHOMAX, DTHO, TDRO, BO, WSCO, NSO(4), NGO(4)
COMMON/RCVRO3/PI, F(8,8), FL25(4), FSAMP, K, KM, TETHRD, NG, NS, JH
COMMON/RCVRO4/DELT, EO(8), GQGT(8,8), H(5,8), ICOUNT, SIGMA
10 COMMON/RCVRO5/NGLOE, NOKLMN, NOAC, GAHAES(5), RDIAG(5), PHDIAG(8)
COMMON/RCVRO6/PPDIAG(8), RMAT(5,5), PHI(5,5), PA(8,8), LAMDA(5)
COMMON/RCVRO7/T(130), V(130)
COMMON/RCVRO8/XSLOE(8), ESLOE(8), ES(8)
COMMON/RCVRO9/BRCVR, BB, PDCRIT, CC
COMMON/RCVR10/XS1(8), XS(8)
15 COMMON/MLS000/ALFA, THE, THEDOT, ALFAR, THR, THRODT, B, WSC
COMMON/MLS001/CSNRT, CSNRF, DSNRDB, RHO, BETA, FSC, LGMAX
COMMON/MLS002/DCSNR, CSNR, LG, TPKT, TPKF
COMMON/MLS003/FL10AE(4,2), FL10(4), DELTAT(2), XO(8,2), YO(4,2)
20 COMMON/MLS004/BMLS, BBB, MTIMES, MSET, MORE
C GENERAL SIMULATION: OPTIMIZATION OF MLS RECEIVERS FOR
C MULTIPATH ENVIRONMENTS
C DIMENSION X1(8), INDEX(2), Y(4), X(8)
C EQUIVALENCE (THAMAX, Y(1)), (ALFA, X(1))
25 C
C FOLG BEGINS EXECUTABLE STATEMENTS
C
PI2=2.*PI
SQ22=SQRT(.5)
30 C
C FOLG INITIALIZES THE DIAGONAL OF F(8,8)
C
9 DO 10 I=1,8
F(1,I)=1.
16 CONTINUE
35 CALL CONTRL(1)
SSQ2=SIGMA*SQRT(2.)
C
C FOLLOWING COMPLETES INITIALIZATION AND COMPUTES SECONDARY
C PARAMETERS.
40 C
DO 15 I=1,4
FL10(I)=FL10AE(I,IAE)
15 CONTINUE
DO 20 I=1,4
45 Y(I)=YO(I,IAE)
20 CONTINUE
OMEGA=-(THAMAX-THAMIN)/TS
SECPD=1./OMEGA
TF=TS+TR-2.*THAMIN*SECPD
50 C
C FOLG ARE CONSTANT PARAMETERS USED BY P
C
BBB=2.4/BMLS
DUM=GAUSS(1.0)
55 ALPHA=10.**((DSNRDB/20.))
XO(1,IAE)=ALPHA
ALPHAR=RHO*ALPHA

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```

PROGRAM MLSSIM(INPUT,OUTPUT,TAPE10=INPUT,TAPE12,TAPE15,
*TAPE7=OUTPUT,TAPE17,TAPE20)
REAL LAHDA
LOGICAL NOKLMN,NOLDE,NOAC,KALMAN,LOE,TETHRD,MORE
COMMON /IODATA/IDNRS(6)
5 COMMON/RCVRO0/THAMAX,THAMIN,TS,TR,OMEGA,TF
COMMON/RCVRO1/NGMIN,NGMAX,DELBL,NGH,IR,IAE
COMMON/RCVRO2/RHOMAX,DTHO,TORO,BO,WSCD,NSD(4),NGO(4)
10 COMMON/RCVRO3/PI,F(8,8),FL25(4),FSAMP,K,KH,TETHRD,NG,NS,JH
COMMON/RCVRO4/DELT,ED(8),GOGT(8,8),H(5,8),ICOUNT,SIGMA
COMMON/RCVRO5/NOLDE,NOKLMN,NOAC,GAMAES(5),ROIAG(5),PHOIAG(8)
COMMON/RCVRO6/PPDIAG(8),RMAT(5,5),PHI(5,5),PA(8,8),LAHDA(5)
COMMON/RCVRO7/T(130),V(130)
15 COMMON/RCVRO8/XSLDE(8),ESLDE(8),ES(8)
COMMON/RCVRO9/BRCVR,BB,PDCRIT,CC
COMMON/RCVR10/XSI(8),XS(8)
COMMON/MLS000/ALFA,THE,THEODT,ALFAR,THR,THRODT,B,WSC
COMMON/MLS001/CSNR,CSNRF,DSNRDB,RHO,BETA,FSC,LGMAX
20 COMMON/MLS002/DCSNR,CSNR,LG,TPKT,TPKF
COMMON/MLS003/FL10AE(4,2),FL10(4),DELTAT(2),XD(8,2),YD(4,2)
COMMON/MLS004/BHLS,BBB,MTIMES,MSET,MORE
C
16 CONTINUE
CALL MLSSUB
25 IF(MORE) GO TO 10
STOP
END

```

410008 CH STORAGE USED .134 SECONDS

```

FUNCTION THA(T)
C
C THIS COMPUTES THE ANTENNA SCAN ANGLE AT LOCAL SCAN TIME T.
C THE PARAMETERS OF THE SCAN WAVEFORM, HENCE THE IDENTITY OF
5 C THE ANGLE FUCTION, ARE PASSED THROUGH COMMON AND ARE DEFINED
C AS FOLLOWS:
C TR=TIME BETWEEN TRAVERSAL OF ZERO DEGREES IN A TO-PRD SCAN
C TS=DURATION OF THE TO SCAN
C TF=DURATION OF THE TO SCAN+INTERSCAN REST INTERVAL
10 C THAMAX=ANTENNA ANGLE AT BEGINNING OF TO SCAN
C THAMIN=ANTENNA ANGLE AT END OF TO SCAN
C OMEGA=ANTENNA ANGULAR SCAN RATE, DEG/SEC, DURING TO SCAN
C
C COMMON/RCVROO/THAMAX, THAMIN, TS, TR, OMEGA, TF
15 C T1=TS+TF
C IF(T.GE.0.0) GO TO 50
C THA=THAMAX
C RETURN
20 C 50 IF(T.GT.TS) GO TO 100
C THA=THAMAX+OMEGA*T
C RETURN
C 100 IF(T.GE.TF) GO TO 200
C THA=THAMIN
C RETURN
25 C 200 IF(T.GT.T1) GO TO 250
C THA=THAMIN-OMEGA*(T-TF)
C RETURN
30 C 250 THA=THAMAX
C RETURN
C END

41000B CH STORAGE USED .118 SECONDS

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60      XO(4,IAE)=ALPHAR
      XO(7,IAE)=PI*BETA/180.
      XO(8,IAE)=PI2*FSC
      TSAMP=1./FSAMP
      DELT=DELTA*(IAE)
      F(2,3)=DELT
      F(5,6)=DELT
65      F(7,8)=DELT
      JM1=JM+1
      JM2=JM/2
      TWM2=0.5*TSAMP*(JM2+1)
      DO 30 I=1,8
70      X(I)=XO(I,IAE)
      CONTINUE
      CALL CONTRL(2)
      C
      C FOLG CALLS RECEIVER FOR INITIALIZATION
75      C
      K=0
      CALL RCVR
      C
      C FOLLOWING BEGINS SIMULATION PER SE, LGMAX RUNS OF KM SCANS EACH
80      C
      CALL CONTRL(5)
      DO 777 MMSET=1,MTIMES
      MSET=MMSET
      C
85      CALL CONTRL(6)
      DO 1 LGG=1, LGMAX
      LG=LGG
      CALL CONTRL(7)
      DO 2 KK=1, KM
90      K=KK
      C
      CALL CONTRL(8)
      IF (K.EQ.1) GO TO 122
      C
95      C FOLLOWING ADVANCES THE TRUE STATE AND SAVE PRIOR VALUE
      C
      DO 100 I=1,8
      X1(I)=X(I)
      X(I)=0.
100      100 CONTINUE
      DO 120 I=1,8
      DO 110 J=1,8
      X(I)=X(I)+F(I,J)*X1(J)
      110 CONTINUE
105      120 CONTINUE
      B=PVALUE(B,PI,0.)
      C
      C FOLG SETS THES PRIOR TO COMPUTING SAMPLE TIMES
110      THES=XS(2)+DELT*XS(3)
      IF(.NOT.TETHRD) GO TO 124
      122 CONTINUE
      DO 123 I=1,8
      XS1(I)=X(I)-ED(I)
123      CONTINUE

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ORIGINAL PAGE NO.  
OF POOR QUALITY

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115      THES=XS1(2)
124      CONTINUE
C
C FOLG BEGINS COMPUTATION OF SIGNALS AND RELATED QUANTITIES
C FIRST, CALCULATION OF CONSTANTS ON THE PRESENT SCAN
120      C
          AL2=ALFA**2
          AR2=ALFAR**2
          AA2=2.*ALFA*ALFAR
          TPST=(THES-THAMAX)*SECPD
          TPSF=TF+(THAMIN-THES)*SECPD
125      TZI=TPST-TWW2
          TZF=TPSF+TWW2
C FOLG COMPUTES FOR THIS KTH SCAN THE SIGNAL PEAK TIMES TPKT, TPKF AND
C THE COMPOSITE SIGNAL-TO-NOISE RATIO, CSNR(K)
130      TPKT=(X(2)-THAMAX)*SECPD
          TPKF=TF+(THAMIN-X(2))*SECPD
C
C THAJ=THA(TPKT)=X(2), BY DEFINITION
C PJ=PMLS(THA-THA(TPKT))=1.0, BY DEFINITION
135      C AND SIMILARLY FOR TPKF
C
          PRJ=PMLS(X(5)-X(2))
          BT=PVALUE(B+WSC*TPKT,PI,0.)
          BF=PVALUE(B+WSC*TPKF,PI,0.)
140      QJT=AL2+AA2*PRJ*COS(BT)+AR2*(PRJ**2)
          QJF=AL2+AA2*PRJ*COS(BF)+AR2*(PRJ**2)
          CSNRT=SQRT(QJT)
          CSNRF=SQRT(QJF)
145      CSNRHM=AMIN1(CSNRT,CSNRF)
          CSNRMX=AMAX1(CSNRT,CSNRF)
          CSNR=CSNRHM
          DCSNR=CSNRMX-CSNRHM
C
C FOLG INITIATES A J-LOOP TO COMPUTE SAMPLE TIMES AND (LINEAR)
C ENVELOPE SAMPLE VALUES
150      C
          DO 130 J=1,JM2
          TINCR=J*TSAMP
          JFR=JH1-J
155      INDEX (1)=J
          INDEX (2)=JFR
C FOLG COMPUTES SAMPLE TIMES
          TJ=T2T+TINCR
          T(J)=TJ
160      T(JFR)=TZF-TINCR
          THAJ=THA(TJ)
          PJ=PMLS(THA-THAJ)
          PRJ=PMLS(THR-THAJ)
C FOLG COMPUTES ENVELOPE SAMPLES
165      DO 127 I=1,2
          JVAL=INDEX(I)
          XNC=SQ22*GAUSS(0.)
          XNS=SQ22*GAUSS(0.)
          BLOCAL=PVALUE(B+WSC*T(JVAL),PI,0.)
170      QJ=AL2*(PJ**2)+AA2*PJ*PRJ*COS(BLOCAL)+AR2*(PRJ**2)
          QJ=AMAX1(QJ,0.0)

```

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## BLOCK DATA MLS

REAL LAHDA

LOGICAL NOKLMN,NOLOE,NOAC,KALMAN,LOE,TETHRD,MORE

COMMON/1DDATA/IDNRS(6)

5 COMMON/RCVRO1/RHMIN,RHMAX,DELBL,NGH,IR,IAE

COMMON/RCVRO2/RHOMAX,DTHD,TDRD,BO,WSCD,NSD(4),NGO(4)

COMMON/RCVRO3/PI,F(8,8),FL25(4),FSAMP,K,KM,TETHRD,NG,NS,JM

COMMON/RCVRO4/DEL,ED(8),GQGT(8,8),H(5,8),ICOUNT,SIGMA

COMMON/RCVRO5/NOLOE,NOKLMN,NOAC,GAMAES(5),ROIAG(5),PHDIAG(8)

10 COMMON/RCVRO6/PPDIAG(8),RHAT(5,5),PHI(5,5),PA(8,8),LAHDA(5)

COMMON/RCVRO9/BRCVR,88,POCRIT,CG

COMMON/MLS001/CSNRT,CSNRF,DSNR08,RHO,BETA,FSC,LGMAX

COMMON/MLS003/FL10AE(4,2),FL10(4),DELTAT(2),XD(8,2),YD(4,2)

COMMON/MLS004/BMLS,888,MTIMES,MSET,MORE

15 DATA PI/3.1415927/,F/64\*0./,DSNR08/20./,RHO/.5/

DATA DELTAT/.074074074/,024691358/,SIGMA/.7071/

DATA XD/0.,30.,35,0.,32.75,-.35,0.,0.,

\* 0.,10.,0.,0.,12.,-.9,0.,2./

20 DATA YD/62.6666667,-62.,6.233333E-3,6.6E-3,

\*30.6666667,0.,1.533333E-3,0.4E-3/

DATA FL10AE/.5,0.,-.5,0.,.25,0.,-.75,0./

DATA FL25/.34831,34831,-.30336,0./

DATA JM/130/,TETHRD/.FALSE./,KM/100/,FSAMP/1.6E5/

DATA H/1.,5\*0.,1.,10\*0.,1.,5\*0.,1.,10\*0.,1.,5\*0./

25 DATA NSD/2,8,6,3/,NGO/2,5,4,2/

DATA DELBL/.01/,ED/8\*0./

DATA GQGT/64\*0./,PA/64\*0./

DATA RHOMAX/.8/,DTHD/2.75/,TDRD/0.0/,BO/0.0/,WSCD/0.0/

DATA NOLOE/.TRUE./,NOKLMN/.FALSE./,NOAC/.TRUE./

30 DATA IAE/1/,FSC/51.30/,BETA/-168.0/,LGMAX/1/

DATA BMLS/1.0/,BRCVR/1.0/,MTIMES/1/,MORE/.TRUE./

DATA IDNRS(5)/1/

END

41000B CH STORAGE USED

.209 SECONDS

```
SUBROUTINE DFLTR1(X,Y,C)
DIMENSION C(4)
S=X-C(3)*C(4)
Y=C(1)*S+C(2)*C(4)
C(4)=S
RETURN
END
```

5

410008 CH STORAGE USED .043 SECONDS

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```

SUBROUTINE RCVR
REAL LAHDA,MJM2
LOGICAL NOKLMN,NOLOE,NOAC,KALMAN,LOE,TETHRO
COMMON/RCVRO0/THAMAX,THAMIN,TS,TR,OMEGA,TF
5 COMMON/RCVRO1/NGMIN,NGMAX,DEL8L,NGH,IR,IAE
COMMON/RCVRO2/RHOMAX,DTHD,TDRD,BO,WSCO,NSD(4),NGO(4)
COMMON/RCVRO3/PI,F(8,8),FL25(4),FSAMP,K,KM,TETHRO,NG,NS,JM
COMMON/RCVRO4/DELT,EO(8),GQGT(8,8),H(5,8),ICOUNT,SIGMA
10 COMMON/RCVRO5/NOLOE,NOKLMN,NOAC,GAMAES(5),ROIAG(5),PMDIAG(8)
COMMON/RCVRO6/PPDIAG(8),RHAT(5,5),PHI(5,5),PA(8,8),LAHDA(5)
COMMON/RCVRO7/T(130),V(130)
COMMON/RCVRO8/XSLOE(8),ESLOE(8),ES(8)
COMMON/RCVRO9/BRCVR,BB,PDCRIT,CC
COMMON/RCVR10/XSI(8),XS(8)
15 COMMON/MLS000/X(8)
DIMENSION TPA1(8,8),PHT(8,5),TPA2(8,8),IVNG(5)
DIMENSION RVNG(5),GAIN(8,5)
C
20 C FOLG IS INITIALIZATION
PI2=.5*PI
SS2=.5/(SIGMA**2)
CALL PHILM
NS=NSD(IR)
25 NG=NGD(IR)
NGMIN=2
NGMAX=NGD(IR)
GQGT33=.01*DELT
GQGT(3,3)=GQGT33
30 GQGT(6,6)=GQGT33
GQGT(8,8)=.04/(DELT**2)
DO 20 I=1,NS
DO 10 J=1,NS
PA(I,J)=0.
35 10 CONTINUE
20 CONTINUE
CALL CONTRL(3)
BB=2.4/BRCVR
40 PDCRIT=PI*BB/8.
CC=PI*PDCRIT
IF(IR.GT.0) GO TO 30
NS=NSD(4)
NG=NGD(4)
45 30 CONTINUE
NGM=NGMIN
IF(NOAC) NGM=NG
KALMAN=.NOT. NOKLMN
LOE=.NOT. NOLOE
CALL CONTRL(4)
50 RETURN
CONTINUE
40 CONTINUE
IF(K.GT.1) GO TO 50
C
C DIAGNOSTIC OUTPUT OF INPUT DATA FOR K=1 GOES HERE
55 C
50 GO TO 90
CONTINUE

```

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```

C FOLG EXTRAPOLATES STATE ESTIMATE, AS REQ'D
C IF(TETHRD) GO TO 80
60 DO 70 I=1,NS
   XS1(I)=0.
   DO 60 J=1,NS
     XS1(I)=XS1(I)+F(I,J)*XS(J)
60 CONTINUE
65 70 CONTINUE
   80 CONTINUE
   90 CONTINUE
C
   GQGT11=AMAX1(.25,.01*(XS1(1)**2))
70 GQGT(1,1)=GQGT11
   GQGT(4,4)=GQGT11
C
C FOLLOWING COMPUTES VECTORS Q(JM),HW(JM),LAMDA(NG),AND MATRICES DT(JM,
C NG),PHI(NG,NS) ALSO SQUARED AMPLITUDE ENVELOPE VECTOR U(JM),AND
75 C INOVATION;S PROCESS VECTOR W(JM)
C
   CALL PHILH
   IF (NOLOE) GO TO 120
C
80 C FOLG COMPUTES RMAT=PHI-INVERSE AND THE LOE
   CALL MATINV(RMAT,5,NG,IVNG,RVNG)
   DO 100 I=1,NG
     RDIAG(I)=RMAT(I,I)
100 CONTINUE
85 CALL MATHUL(5,NG,NG,5,NG,1,5,1,RMAT,LAMDA,GAMAES,1)
   CALL MATHUL(5,NG,NS,5,NG,1,8,1,H,GAMAES,ESLOE,2)
   DO 110 I=1,NS
     XSLOE(I)=XS1(I)+ESLOE(I)
90 IF (NOKLMN) XS(I)=XSLOE(I)
110 CONTINUE
120 CONTINUE
   IF (NOKLMN) GO TO 170
C
95 C FOLLOWING EXTRAPOLATES STATE ESTIMATES,ERROR
C COVARIANCE MATRIX PA(NS,NS)
C
   CALL MATHUL(8,NS,NS,8,NS,NS,8,8,PA,F,TPA1,3)
   CALL MATHUL(8,NS,NS,8,NS,NS,8,8,F,TPA1,PA,1)
   CALL MATSM(PA,PA,GQGT,1,8,8,8,NS,NS,8,NS,NS,0)
100 DO 130 I=1,NS
   PDIAG(I)=PA(I,I)
130 CONTINUE
C
135 C FOLLOWING COMPUTES MODIFIED-KALMAN GAIN MATRIX GAIN(NS,NG)
C
   CALL MATHUL(8,NS,NS,5,NG,NS,8,5,PA,H,PHT,3)
   CALL MATHUL(5,NG,NG,5,NG,NS,8,8,PHI,H,TPA1,1)
   CALL MATHUL(8,NG,NS,8,NS,NG,8,8,TPA1,PHT,TPA2,1)
   DO 140 I=1,NG
     TPA2(I,I)=TPA2(I,I)+1.
110 140 CONTINUE
   CALL MATINV(TPA2,8,NG,IVNG,RVNG)
   CALL MATHUL(8,NS,NG,8,NG,NG,8,5,PHT,TPA2,GAIN,1)
C

```

```

115      C      FOLLOWING UPDATES STATE ESTIMATE
          CALL MATHUL (8,NS,NG,5,NG,1,8,1,GAIN,LAMDA,ES,1)
          CALL MATSM (XS,XS1,ES,1,8,1,8,NS,1,8,NS,1,0)
          C
          C      FOLLOWING UPDATES STATE ESTIMATE ,ERROR COVARIANCE MATRIX
120      C      P(NS,NS)
          C
          CALL MATHUL(8,NS,NG,8,NG,NS,8,8,GAIN,TPA1,TPA2,1)
          DO 150 I=1,NS
          TPA2(I,I)=TPA2(I,I)-1.
125      150  CONTINUE
          CALL MATHUL(8,NS,NS,8,NS,NS,8,8,PA,TPA2,TPA1,3)
          CALL MATHUL(8,NS,NS,8,NS,NS,8,8,TPA2,TPA1,PA,1)
          CALL MATHUL(5,NG,NG,8,NS,NG,8,8,PHI,GAIN,TPA1,3)
          CALL MATHUL(8,NS,NG,8,NG,NS,8,8,GAIN,TPA1,TPA2,1)
130      CALL MATSM(PA,PA,TPA2,1,8,8,8,NS,NS,8,NS,NS,0)
          DO 160 I=1,NS
          PPOIAG(I)=PA(I,I)
          160  CONTINUE
          170  CONTINUE
135      IF (NS.GE.7) XS(7)=PVALUE(XS(7),PI,0.)
          RETURN
          END

```

410008 CM STORAGE USED

1.082 SECONDS

BLOCK DATA DRVRID  
COMMON /10DATA/IDNRS(6)  
DATA IDNRS(4)/2/  
END

410008 CH STORAGE USED .014 SECONDS

A-65

```

SUBROUTINE RCVR
REAL LAMDA, MJM2
LOGICAL NOKLMN, NOLDE, NOAC, KALMAN, LOE, TETHRD
COMMON/RCVRO0/THAMAX, THAHIN, TS, TR, OMEGA, TF
5 COMMON/RCVRO1/NGMIN, NGMAX, DELBL, NGH, IR, IAE
COMMON/RCVRO2/RHOMAX, DTHD, TDRO, BQ, WSCD, NSD(4), NGO(4)
COMMON/RCVRO3/PI, F(8,8), FL25(4), FSAMP, K, KH, TETHRD, NG, NS, JM
COMMON/RCVRO4/DELT, ED(8), GQGT(8,8), H(5,8), ICDUNT, SIGMA
COMMON/RCVRO5/NOLOE, NOKLMN, NOAC, GAMAES(5), RDIAG(5), PHDIAG(8)
10 COMMON/RCVRO6/PPDIAG(8), RMAT(5,5), PHI(5,5), PA(8,8), LAMDA(5)
COMMON/RCVRO7/T(130), V(130)
COMMON/RCVRO8/XSLDE(8), ESLDE(8), ES(8)
COMMON/RCVRO9/BRCVR, BB, PDCRIT, CC
COMMON/RCVRO10/XS1(8), XS(8)
15 COMMON/MLS000/X(8)
DIMENSION TPA1(8,8), PHT(8,5), TPA2(8,8), IVNG(5)
DIMENSION RVNG(5), GAIN(8,5)
C
IF (K.GT. 0) GO TO 40
20 C FOLG IS INITIALIZATION
PI2=2.*PI
SS2=.5/(SIGMA**2)
CALL PHILM
NS=NSD(IR)
25 NG=NGD(IR)
NGMIN=2
NGMAX=NGD(IR)
GQGT33=.01*DELT
GQGT(3,3)=GQGT33
30 GQGT(6,6)=GQGT33
GQGT(8,8)=.04/(DELT**2)
DO 20 I=1,NS
DO 10 J=1,NS
PA(I,J)=0.
35 10 CONTINUE
20 CONTINUE
CALL CONTRL(3)
BB=2.4/BRCVR
40 PDCRIT=PI*BB/8.
CC=PI*PDCRIT
IF (IR.GT.0) GO TO 30
NS=NSD(4)
NG=NGD(4)
45 30 CONTINUE
NGH=NGMIN
IF(NOAC) NGH=NG
KALMAN=.NOT. NOKLMN
LOE=.NOT. NOLDE
CALL CONTRL(4)
50 RETURN
CONTINUE
40 IF(K.GT.1) GO TO 50
C
C DIAGNOSTIC OUTPUT OF INPUT DATA FOR K=1 GOES HERE
55 C
GO TO 90
50 CONTINUE

```

```

C FOLG EXTRAPOLATES STATE ESTIMATE, AS REQ'D
60 IF(TETHRD) GO TO 80
   DO 70 I=1,NS
     XS1(I)=0.
     DO 60 J=1,NS
       XS1(I)=XS1(I)+F(I,J)*XS(J)
65   CONTINUE
     70 CONTINUE
     80 CONTINUE
     90 CONTINUE
C
   GQGT11=AMAX1(.25,.01*(XS1(1)**2))
   GQGT(1,1)=GQGT11
   GQGT(4,4)=GQGT11
C
C FOLLOWING COMPUTES VECTORS Q(JH),HW(JH),LAMDA(NG),AND MATRICES DT(JH,
C NG),PHI(NG,NS) ALSO SQUARED AMPLITUDE ENVELOPE VECTOR U(JH),AND
75 C INOVATION;S PROCESS VECTOR W(JH)
C
   CALL PHILM
   IF (NOLOE) GO TO 120
C
80 C FOLG COMPUTES RMAT=PHI-INVERSE AND THE LOE
   CALL MATINV(RMAT,5,NG,IVNG,RVNG)
   DO 100 I=1,NG
     ROIAG (I)=RMAT (I,I)
100 CONTINUE
   CALL MATHUL (5,NG,NG,5,NG,1,5,1,RMAT,LAMDA,GAMAES,1)
   CALL MATHUL (5,NG,NS,5,NG,1,8,1,H,GAMAES,ESLOE,2)
   DO 110 I=1,NS
     XSLOE(I)=XS1(I)+ESLOE(I)
90   IF (NOKLHN) XS(I)=XSLOE(I)
110 CONTINUE
120 CONTINUE
   IF (NOKLHN) GO TO 170
C
95 C FOLLOWING EXTRAPOLATES STATE ESTIMATES,ERROR
C COVARIANCE MATRIX PA(NS,NS)
C
   CALL MATHUL(8,NS,NS,8,NS,NS,8,8,PA,F,TPA1,3)
   CALL MATHUL(8,NS,NS,8,NS,NS,8,8,F,TPA1,PA,1)
   CALL MATSM(PA,PA,GQGT,1,8,8,8,NS,NS,8,NS,NS,0)
100 DO 130 I=1,NS
     PDIAG (I)=PA(I,I)
130 CONTINUE
C
105 C FOLLOWING COMPUTES MODIFIED-KALMAN GAIN MATRIX GAIN(NS,NG)
C
   CALL MATHUL(8,NS,NS,5,NG,NS,8,5,PA,H,PHT,3)
   CALL MATHUL(5,NG,NG,5,NG,NS,8,8,PHI,H,TPA1,1)
   CALL MATHUL(8,NG,NS,8,NS,NG,8,8,TPA1,PHT,TPA2,1)
   DO 140 I=1,NG
     TPA2(I,I)=TPA2(I,I)+1.
110 CONTINUE
140 CALL MATINV(TPA2,8,NG,IVNG,RVNG)
   CALL MATHUL(8,NS,NG,8,NG,NG,8,5,PHT,TPA2,GAIN,1)
C

```

A-67

```

115      C      FOLLOWING UPDATES STATE ESTIMATE
          CALL MATHUL (8,NS,NG,5,NG,1,8,1,GAIN,LAMDA,ES,1)
          CALL MATSH (XS,XS1,ES,1,8,1,8,NS,1,8,NS,1,0)
          C
120      C      FOLLOWING UPDATES STATE ESTIMATE ,ERROR COVARIANCE MATRIX
          C      P(NS,NS)
          C
          CALL MATHUL(8,NS,NG,8,NG,NS,8,8,GAIN,TPA1,TPA2,1)
          DO 150 I=1,NS
          TPA2(I,I)=TPA2(I,I)-1.
125      150      CONTINUE
          CALL MATHUL(8,NS,NS,8,NS,NS,8,8,PA,TPA2,TPA1,3)
          CALL MATHUL(8,NS,NS,8,NS,NS,8,8,TPA2,TPA1,PA,1)
          CALL MATHUL(5,NG,NG,8,NS,NG,8,8,PHI,GAIN,TPA1,3)
          CALL MATHUL(8,NS,NG,8,NG,NS,8,8,GAIN,TPA1,TPA2,1)
130      CALL MATSH(PA,PA,TPA2,1,8,8,8,NS,NS,8,NS,NS,0)
          DO 160 I=1,NS
          PPOIAG (I)=PA(I,I)
          CONTINUE
          160      CONTINUE
          170
135      XS(1)=ABS(XS(1))
          AN=(THAMAX+THAMIN)/2.
          XS(2)=SATU(XS(2)-AN,(THAMAX-THAMIN)/2.)+AN
          IF(NS.GE.3) XS(3)=SATU(XS(3),1.)
          IF(NS.GE.4) XS(4)=SATU(ABS(XS(4)),2*XS(1))
140      MJM2=FLOAT(-(JH/2+1))
          THWW2=MJM2*OMEGA/(2.+FSAMP)
          AMX=XS(2)+THWW2
          AMN=XS(2)-THWW2
          AN2=(AMX+AMN)/2.
145      IF(NS.GE.5) XS(5)=SATU(XS(5)-AN2,(AMX-AMN)/2.)+AN2
          IF(NS.GE.6) XS(6)=SATU(XS(6),1.)
          IF (NS.GE.7) XS(7)=PVALUE(XS(7),PI,0.)
          IF(NS.GE.8) XS(8)=PVALUE(XS(8),PI/DELT,0.)
150      RETURN
          END

```

41000B CM STORAGE USED

1.381 SECONDS

A-68

ORIGINAL PAGE IS  
OF POOR QUALITY

BLOCKDATA DRVRID 73/172 TS

FTN 4.6+452

05/22/79 13.36.34

PAGE 1

BLOCK DATA DRVRID  
COMMON /IOWDATA/IDNRS(6)  
DATA IDNRS(4)/2/  
END

41000B CH STORAGE USED .015 SECONDS

A-69

4-3

## SUBROUTINE PHILM

```

C
C THIS SUBOPTIMAL VERSION OF PHILM IS
C BASED ON A 4-ELEMENT PARAMETER VECTOR
5 CA AND PROVIDES A CRUDE SEARCH AND ACQUISITION
CA FUNCTION ACCESSED AS FOLLOWS
CASEARCH MODE:NGM=NGMIN
CAACQUISITION MODE:NGMIN.LT.NGM.LT.NGMAX
CAFULL TRACK MODE:NGM=NGMAX
10 C
C
C THIS NEEDS NGMIN.LE.NGM (.LE.NG) .LE.NGMAX
REAL LAMDA
LOGICAL NOKLHN,NLOE,NOAC,KALMAN,LDE,TETHRD
15 COMMON/RCVRO1/NGMIN,NGMAX,DELBL,NGM,IR,IAE
COMMON/RCVRO2/RHOMAX,DTHO,TDRO,B0,WSCD,NSD(4),NGD(4)
COMMON/RCVRO3/PI,F(8,8),FL25(4),FSAMP,K,KH,TETHRD,NG,NS,JM
COMMON/RCVRO4/DELT,ED(8),GOGT(8,8),H(5,8),ICOUNT,SIGMA
COMMON/RCVRO5/NLOE,NOKLHN,NOAC,GAMAES(5),RDIAG(5),PHDIAG(8)
20 COMMON/RCVRO6/PPDIAG(8),RNAT(5,5),PHI(5,5),PA(8,8),LAMDA(5)
COMMON/RCVRO7/T(130),V(130)
COMMON/RCVR10/ALFA,THES,THESDT,ALFAR,THRS,THRSDT,B,WSC,XS(8)
DIMENSION PH(4,4),RL(4)
EQUIVALENCE (RL1,RL(1)),(RL2,RL(2)),(RL3,RL(3)),(RL4,RL(4))
25 EQUIVALENCE (PH11,PH(1,1)),(PH21,PH(2,1)),(PH22,PH(2,2)),
* (PH31,PH(3,1)),(PH32,PH(3,2)),(PH33,PH(3,3)),
* (PH41,PH(4,1)),(PH42,PH(4,2)),(PH43,PH(4,3)),(PH44,PH(4,4))
C
C
30 C FOLLOWING EFFECTS INITIATION
C
IF(K.GT.0) GO TO 10
JM2=JM/2
JM1=JM+1
35 SS2=.5/(SIGMA**2)
IR=3
RETURN
10 CONTINUE
CA
40 CA FOLLOWING PROGRAMS THE SEARCH
CA
IF(NGM.GT.NGMIN) GO TO 30
ALFAR=ALFA*RHOMAX
THRS=THES-DTHO
45 THRSDT=TDRO
B=B0
WSC=WSCD
CONTINUE
30 C
50 C FOLLOWING COMPUTES CONSTANTS FOR PRESENT SCAN
C
AL2=2.*ALFA
AL22=AL2*ALFA
AR2=2.*ALFAR
55 AR22=AR2*ALFAR
AA2=AL2*ALFAR
NGDEL=NGM-NGMAX

```

A-70

```

DO 35 I=1,NG
  RL(I)=0.
60      DO 34 L=1,I
      34  PH(I,L)=0.
      35  CONTINUE
      C
      C FOLLOWING INITIATES LOOP AND COMPUTES FUNCTIONS
65      C FOR EACH J
      C
      DO 60 JI=1,JM2
      THAJ=THA(T(JI))
      THEE=THES-THAJ
      70      PJ=P(THEE)
      PDJ=PDOT(THEE)
      P2J=PJ**2
      THER=THRS-THAJ
      75      PRJ=P(THER)
      PORJ=PDOT(THER)
      PR2J=PRJ**2
      PPRJ=PJ*PRJ
      QAJ=.5*AL22*P2J
      BA=0.
      80      DAJ1=AL2*P2J
      DAJ2=AL22*PJ*PDJ
      DBJ1=0.
      DBJ2=0.
      IF (NGDEL .LT. 0) GO TO 40
      85      QAJ=QAJ+.5*AR22*PR2J
      QBJ=AA2*PPRJ
      BA=SIGN(0.9899999,QBJ)
      IF (QAJ.GE.1.E-38) BA=SIGN(AMIN1(0.9899999,ABS(QBJ)/QAJ),QBJ)
      90      DBJ1=AR2*PPRJ
      DBJ2=AA2*PDJ*PRJ
      DAJ3=AR2*PR2J
      DBJ3=AL2*PPRJ
      DAJ4=AR22*PDRJ*PRJ
      DBJ4=AA2*PJ*PDRJ
      95      40  CONTINUE
      QAJ=AMIN1(0.9999999E8,QAJ)
      QAJ=AMAX1(0.1,QAJ)
      U1=SS2*V(JI)**2
      100      U2=SS2*V(JM1-JI)**2
      CALL WAWBJ (WA1,WB1,QAJ,BA,U1)
      CALL WAWBJ (WA2,WB2,QAJ,BA,U2)
      WA=WA1+WA2
      WB=WB1+WB2
      105      CALL SWFCNS (SA,SB,RAB,QAJ,BA)
      RAB1=RAB+1.
      RL1=RL1+DAJ1*WA+DBJ1*WB
      RL2=RL2+DAJ2*WA+DBJ2*WB
      SDA1=DAJ1*SA
      110      SDA2=DAJ2*SA
      SDB1=DBJ1*SB
      SDB2=DBJ2*SB
      OSD1=SDA1-SDB1
      OSD2=SDA2-SDB2
      PH11=PH11+OSD1**2+RAB1+2.*SDA1*SDB1

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```

115      PH21=PH21+DSD1+DSD2+RAB1*(SDA2+SDB1+SDA1+SDB2)
        PH22=PH22+DSD2**2+RAB1*2.*SDA2+SDB2
        IF (NGDEL .LT. 0) GO TO 50
        RL3=RL3+DAJ3*WA+DBJ3*WB
        RL4=RL4+DAJ4*WA+DBJ4*WB
120      SDA3=DAJ3*SA
        SDA4=DAJ4*SA
        SDB3=DBJ3*SB
        SDB4=DBJ4*SB
        OSD3=SDA3-SDB3
125      OSD4=SDA4-SDB4
        PH31=PH31+DSD1*OSD3+RAB1*(SDA3+SDB1+SDA1+SDB3)
        PH32=PH32+DSD2*OSD3+RAB1*(SDA3+SDB2+SDA2+SDB3)
        PH33=PH33+OSD3**2+RAB1*2.*SDA3+SDB3
        PH41=PH41+DSD1*OSD4+RAB1*(SDA4+SDB1+SDA1+SDB4)
130      PH42=PH42+DSD2*OSD4+RAB1*(SDA4+SDB2+SDA2+SDB4)
        PH43=PH43+OSD3*OSD4+RAB1*(SDA4+SDB3+SDA3+SDB4)
        PH44=PH44+OSD4**2+RAB1*2.*SDA4+SDB4
        50 CONTINUE
        60 CONTINUE
135      C FOLLOWING COMPUTES VECTOR LAMDA(NG) AND MATRICE PHI(NG,NG)
        C
        DD 110 I=1,NG
        LAMDA(I)=RL(I)
140      DD 100 L=1,I
        PHILI=2.*PH(I,L)
        PHI(L,I)=PHILI
        PHI(I,L)=PHILI
        IF (NOLOE) GO TO 90
145      RHAT(L,I)=PHILI
        RHAT(L,L)=PHILI
        90 CONTINUE
        100 CONTINUE
        110 CONTINUE
150      RETURN
        END

```

410008 CM STORAGE USED

1.381 SECONDS

```

C
C
C
C
5.  C
C
SUBROUTINE WAWBJ(WA, WB, QA, B, U)
C THIS COMPUTES A SAMPLE EACH OF THE PROCESSES WA % WB,
C GIVEN SAMPLES OF QA, B, AND U
10  C
C DIMENSION HA(11), HB(11), COSB(11), G(11), H(11)
C DATA LMAX/10/, NFIRST/.FALSE./
C
C IF(NFIRST) GO TO 10
15  LMAX1=LMAX+1
C RLMAX1=LMAX1
C ALNLMX=ALOG(RLMAX1)
C BETA2=3.1415927/LMAX
C DO 5 L=1, LMAX1
20  COSB(L)=COS((L-1)*BETA2)
C
C 5  CONTINUE
C NFIRST=.TRUE.
C 10  CONTINUE
C GMAX=-1.E+322
25  HMAX=1.
C HAMAX=1.
C HBMAX=1.
C DO 20 L=1, LMAX1
C COSBL=COSB(L)
30  C BCBL1=AMAX1(1.+B*COSBL, 0.)
C BCBL1=1.+B*COSBL
C ABC=QA*BCBL1
C UABC=U*ABC
C RAD=2.*SQRT(UABC)
35  RAD1=SQRT(1.+UABC)
C GL=2.*(RAD1-1./(1.+RAD))-ABC
C G(L)=GL
C HL=1./SQRT(1.+6.2831846*RAD)
C H(L)=HL
40  HAL=(-1.+U/RAD1)*HL
C HA(L)=HAL
C HBL=HAL*COSBL
C HB(L)=HBL
C GMAX=AMAX1(GL, GMAX)
45  HMAX=AMAX1(HL, HMAX)
C HAMAX=AMAX1(ABS(HAL), HAMAX)
C HBMAX=AMAX1(ABS(HBL), HBMAX)
C 20  CONTINUE
C GZ=GMAX-741.
50  FZ=ALOG(HMAX)+GZ
C GM=FZ+ALNLMX
C GZ=GZ+ALNLMX
C GMA=GZ+ALOG(HAMAX)
C GMB=GZ+ALOG(HBMAX)
55  FS=0.
C FSA=0.
C FSB=0.

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OF POOR QUALITY

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SUBROUTINE WAMBJ      73/172 TS      FTN 4.6+452      05/17/79 16.20.18      PAGE 2
DO 30 L=1,LMAX1
GL=G(L)
.60 GLM=GL-GM
GLMA=GL-GMA
GLMB=GL-GMB
IF(GLM.GE.-674.) FS=FS+EXP(GLM)*H(L)
IF(GLMA.GE.-674.) FSA=FSA+EXP(GLMA)*HA(L)
65 IF(GLMB.GE.-674.) FSB=FSB+EXP(GLMB)*HB(L)
30 CONTINUE
WA=(HAMAX/HMAX)*(FSA/FS)
WB=(HBMAX/HMAX)*(FSB/FS)
70 RETURN
END
41008 CH STORAGE USED .451 SECONDS

```

A-74

```

C
C
C
5 C
SUBROUTINE SWFCNS(HWAJ,HWBJ,RABJ,QAV,BA)
INTEGER FNA(4)
LOGICAL NFIRST
10 DIMENSION BULK(12,25,3),QA(25),B(25),DEX(24),DEY(11)
DIMENSION AA(3),BB(3),CC(3),DD(3),APPVA(3)
DIMENSION QAB(25,2),QB(2),IQBMAX(2),IQJB(2)
EQUIVALENCE (QA(1),QAB(1,1)),(B(1),QAB(1,2))
15 EQUIVALENCE (IQMAX,IQBMAX(1)),(JBMAX,IOBMAX(2))
EQUIVALENCE (IQ,IQJB(1)),(IB,IQJB(2)),(BV,QB(2))
DATA FNA/10HMLSLDGSWCD,1LC,2*0/
DATA NFIRST/.FALSE./
C
C FOLG GENERATES TABLE FROM DATA FILE
20 C
IF(NFIRST) GO TO 10
NFIRST=.TRUE.
IX=IATTACH(6LTAPE12,FNA,2LID,6RM3497E)
IF (IX.EQ.0) GO TO 5
25 CALL INTIO(6HIXAT12,IX,1,1)
STOP#INPUT FILE ATTACH (TAPE12) NOT SATISFACTORY#
5 CONTINUE
READ (12) IDUM, IDUM
READ (12) IQMAX,{QA(I),I=1,IQMAX}
30 READ (12) JBMAX,{B(J),J=1,JBMAX}
READ (12) ((BULK(J,I,K),J=1,JBMAX),I=1,IQMAX),K=1,3)
IQM1=IQMAX-1
DO 3 I=1,IQM1
3 DEX(I)=QA(I+1)-QA(I)
JBM1=JBMAX-1
DO 6 I=1,JBM1
6 DEY(I)=B(I+1)-B(I)
IQ=IQMAX/2
IB=JBMAX/2
40 CALL RETURN(6LTAPE12)
10 CONTINUE
C
C FOLG TRUNCATES ARGUMENTS AND HANDLES SMALL BV CASES
C
45 BV=ABS(BA)
IF (BV .GE. .01) GO TO 20
HWAJ=1./SQRT(1.+2.*QAV)
HWBJ=0.
RABJ=0.
50 RETURN
20 CONTINUE
C
C FOLG DETERMINES IQ,IB
55 QB(1)=QAV
DO 1500 L=1,2
OBL=QB(L)
1001 IF(OBL.LT.QAB(IQJB(L),L)) GO TO 1101

```

```

        IQJBP1=IQJB(L)+1
        IQBMMH=IQBMAX(L)
60      DD 1201 I=IQJBP1,IQBMMH
        IF(QBL.LT.QAB(I,L)) GO TO 1202
        1201 CONTINUE
        1202 IQJB(L)=I-1
        GO TO 1500
65      1101 IQJBM1=IQJB(L)-1
        DD 1301 I=1,IQJBM1
        MMII=IQJBM1-I+1
        IF(OBL.GE.QAB(MHII,L)) GO TO 1302
        1301 CONTINUE
70      1302 IQJB(L)=MMII
        1500 CONTINUE
        C
        C
        C FOLG DETERMINES INTERPOLATED VALUES
75      C
        DIX=QAV-QA(IQ)
        DIY=BV-B(IB)
        CX=DIX/DEX(IQ)
        CY=DIY/DEY(IB)
80      DD 301 K=1,3
        AA(K)=BULK(IB,IQ,K)
        BB(K)=BULK(IB+1,IQ,K)
        CC(K)=BULK(IB,IQ+1,K)
        DD(K)=BULK(IB+1,IQ+1,K)
85      APPVA(K)=AA(K)+(CC(K)-AA(K))*CX+(BB(K)-AA(K))*CY+CX*CY*(AA(K)
        *+DD(K)-CC(K)-BB(K))
        301 CONTINUE
        HWAJ=EXP(APPVA(1))
        HWBJ=EXP(APPVA(2))
90      RABJ=APPVA(3)
        IF(BA.LT.O.) RABJ=-RABJ
        RETURN
        END
410008 CM STORAGE USED .666 SECONDS

```

..BLOCK DATA PLSUID  
COMMON/IDDATA/IDNRS(6)  
DATA IDNRS(3)/3/  
END

41000B CH STORAGE USED .014 SECONDS

A-77

```

SUBROUTINE PHILM
C
C THIS OPTIMAL VERSION OF PHILM IS FOR ALL SCALLOPING RATES
C AND PROVIDES A CRUDE SEARCH-AND-ACQUISITION FUNCTION
5 C ACCESSED AS FOLLOWS:
C SEARCH MODE: NGM=NGMIN
C ACQUISITION MODE: NGMIN.LT.NGM.LT.NGMAX
C FULL TRACK MODE: NGM=NGMAX
10 C
C THIS NEEDS NGMIN,LE,NGM (.LE.NG) ,LE,NGMAX
C
REAL LAMDA
LOGICAL NOKLHN,NOLOE,NOAC,KALMAN,LOE,TETHRD
15 COMMON/RCVR01/NGMIN,NGMAX,DELBL,NGM,IR,IAE
COMMON/RCVR02/RHOMAX,DTHD,TDRO,BO,WSCO,NSQ(4),NGO(4)
COMMON/RCVR03/PI,F(8,8),FL25(4),FSAMP,K,KM,TETHRD,NG,NS,JH
COMMON/RCVR04/DELT,ED(8),GGGT(8,8),H(5,8),ICOUNT,SIGMA
20 COMMON/RCVR05/NOLOE,NOKLHN,NOAC,GAMAES(5),ROIAG(5),PHOAG(8)
COMMON/RCVR06/PPDIAG(8),RMT(5,5),PHI(5,5),PA(8,8),LAMO(5)
COMMON/RCVR07/T(130),V(130)
COMMON/RCVR08/XSLDE(8),ESLDE(8),ES(8)
COMMON/RCVR09/BRCVR,BB,PDCRIT,CC
COMMON/RCVR10/ALFA,THES,THESDT,ALFAR,THRS,THRSDT,B,WSC,XS(8)
25 DIMENSION INDEX(2),DT(130,5),HW(130),W(130)
C
C FOLLOWING EFFECTS INITIALIZATION
C
30 IF (K.GT.0) GO TO 10
JH2=JH/2
JH1=JH+1
SS2=.5/(SIGMA**2)
IR=2
RETURN
35 10 CONTINUE
C
C FOLLOWING PROGRAMS THE SEARCH
C
40 IF (NGM.GT.NGMIN) GO TO 30
ALFAR=ALFA*RHOMAX
THRSDT=TDRO
B=BO
WSC=WSCO
THRS=THES-DTHD
45 30 CONTINUE
C
C FOLLOWING COMPUTES CONSTANTS FOR PRESENT SCAN
C
50 AL2=2.*ALFA
AL22=AL2*ALFA
AR2=2.*ALFAR
AR22=AR2*ALFAR
AA2=AL2*ALFAR
C
55 C FOLLOWING INITIATES LOOP AND COMPUTES FUNCTIONS
C FOR EACH J
C

```

A-78

```

      DO 60 JI=1,JM2
      INDEX(1)=JI
      INDEX(2)=JMI-JI
      THAJ=THA(T(JI))
      THEE=THE(S-THAJ)
      PJ=P(THEE)
      POJ=POOT(THEE)
      P2J=PJ**2
      THER=THRS-THAJ
      PRJ=P(THER)
      PDRJ=PDOT(THER)
      PR2J=PRJ**2
      PPRJ=PJ*PRJ
      QNRJ=.5*AL22*P2J
      QRJ=QNRJ+.5*AR22*PR2J
      DINET=AL2*P2J
      C1=AR2*PPRJ
      D2NET=AL22*PJ*POJ
      C2=AA2*PDJ*PRJ
      D3J=AR2*PR2J
      C3=AL2*PPRJ
      D4J=AR22*PDRJ*PRJ
      C4=AA2*PJ*PDRJ
      D5J=-AA2*PPRJ
      C FOLG COMPLETES CALCULATIONS FOR TO,FRO SCANS, RESP.
      DO 50 I=1,2
      J=INDEX(I)
      BLOCAL=PVALUE(B+WSC*T(J),3.1415927,DELBL)
      SB=SIN(BLOCAL)
      CB=COS(BLOCAL)
      QJ=QNRJ
      QRJALL=QRJ-D5J*CB
      D1J=DINET
      D2J=D2NET
      IF (NGH.LT.NGHAX) GO TO 40
      QJ=QRJALL
      D1J=D1J+C1*CB
      D2J=D2J+C2*CB
      40 CONTINUE
      DT(J,1)=D1J
      DT(J,2)=D2J
      DT(J,3)=D3J+C3*CB
      DT(J,4)=D4J+C4*CB
      DTJ5=D5J*SB
      DT(J,5)=DTJ5
      C FOLG IS FOR A 6D LDE DESIGN
      C DT(J,6)=DTJ5*T(J)
      105 C FOLLOWING COMPUTES VECTOR HW(JH),AND INNOVATIONS PROCESS VECTOR W(JH)
      C
      HW(J)=1./(I**2+QJ)
      UJ=V(J)
      UJ=SS2*(UJ**2)
      W(J)=(UJ/SQRT(1.+QJ*UJ))-1.
      110 50 CONTINUE
      60 CONTINUE
      C
      C FOLLOWING COMPUTES VECTOR LAMDA(NG) AND MATRICE PHI(NG,NG)

```

ORIGINAL PAGE IS  
OF POOR QUALITY

A-79

```
115          C          DO 110 I=1,NG
              LAMDA(I)=0.0
              DO 70 J=1,JM
              LAMDA(I)=LAMDA(I)+DT(J,I)*W(J)
120          70          CONTINUE
              DO 100 L=1,I
              PHILI=0.
              DO 80 J=1,JM
              PHILI=PHILI+HW(J)*DT(J,I)+DT(J,L)
125          80          CONTINUE
              PHI(L,I)=PHILI
              PHI(I,L)=PHILI
              IF (NDLDE) GO TO 90
              RMAT(L,I)=PHILI
130          90          RMAT(I,L)=PHILI
              CONTINUE
              100          CONTINUE
              110          CONTINUE
              RETURN
135          END
```

410008 CH STORAGE USED

.805 SECONDS

OF LOGS 0101-0102

BLOCK DATA PLOPID  
COMMON /IDDATA/IONRS(6)  
DATA IONRS(3)/2/  
END

410008 CH STORAGE USED .015 SECONDS

A-81

```
FUNCTION PMLS(THETA)
C THIS COMPUTES THE TRANSMITTED SIGNAL INTENSITY(RELATIVE TO
C THAT AT BEAM CENTER AS A FUNCTION OF THE ANGLE-OFF-BORESIGHT.
C THE MODEL GIVES FIRST SIDE LOBES 23 DB BELOW THE MAIN LOBE.
```

5

```
C
LOGICAL MORE
COMMON/MLS004/BMLS, BBB, HTIMES, MSET, MORE
DATA PCRIT/.7853981635/, AA/1.570796327/
PMLS=PCRIT
Z=BBB*THETA
10 IF (ABS(ABS(Z)-1.) .LE. 1.E-7) RETURN
PMLS=(COS(AA*Z))/(1.-Z**2)
RETURN
END
```

41000B CM STORAGE USED

.071 SECONDS

BLOCK DATA PMLS1D  
COMMON/IDDATA/IDNRS(6)  
DATA IDNRS(2)/1/  
END

41000B CM STORAGE USED .016 SECONDS

ORIGINAL PAGE IS  
OF POOR QUALITY

A-83

## FUNCTION P(THETA)

C THIS COMPUTES THE TRANSMITTED SIGNAL INTENSITY(RELATIVE TO  
 C THAT AT BEAM CENTER AS A FUNCTION OF THE ANGLE-OFF-BORESIGHT.  
 C THE MODEL GIVES FIRST SIDE LOBES 23 DB BELOW THE MAIN LOBE.

5

C COMMON/RCVRO9/BRCVR,BB,PCCRIT,CC  
 DATA PCRIT/.7853981635/,AA/1.570796327/

P=PCRIT

Z=BB\*THETA

10

IF (ABS(ABS(Z)-1.) .LE. 1.E-7) RETURN

P=(COS(AA\*Z))/(1.-Z\*\*2)

RETURN

END

410008 CH STORAGE USED

6068 SECONDS

```

C
C FUNCTION PDDT (THETA)
C THIS COMPUTES THE DERIVATIVE DP(THETA)/DTHETA WHERE P(THETA)
C IS THE TRANSMITTED SIGNAL INTENSITY(RELATIVE TO THAT AT BEAM
5 C CENTER) AND THETA IS THE ANGLE-OFF-BORESIGHT.THE P-MODEL USED
C IS THAT GIVING FIRST SIDE LOBES 23 DB BELOW THE MAIN LOBE.
C
C COMMON/RCVR09/BRCVR, BB, PDCRIT, CC
10 C DATA AA/1.570796327/
C
C PDDT=SIGN(PDCRIT,-THETA)
C Z=BB*THETA
C IF (ABS(ABS(Z)-1.) .LE. 1.E-7) RETURN
C CP=AA*(Z+1.)
15 C CM=AA*(Z-1.)
C PDDT=CC*((COS(CP)-SIN(CP)/CP)/CP+(COS(CM)-SIN(CM)/CM)/CM)
C RETURN
C END

```

41000B CM STORAGE USED

.119 SECONDS

```
C.
BLOCK DATA POPTID
CGMMON/IODATA/IDNRS(6)
DATA IDNRS(6)/1/
END.
5
41000B CH STORAGE USED . . . . .013 SECONDS
```

```

SUBROUTINE RCVR
C THRESHOLD RECEIVER
REAL LAMDA
LOGICAL NOKLMN,NOLDE,NOAC,KALMAN,LOE,TETHRD
5 COMMON/RCVROO/THAMAX,THAMIN,TS,TR,OMEGA,TF
COMMON/RCVRO1/NGMIN,NGMAX,DELBL,NGM,IR,IAE
COMMON/RCVRO2/RHOMAX,DTHO,TDRO,BO,WSCO,NSO(4),NGO(4)
COMMON/RCVRO3/PI,F(8,8),FL25(4),FSAMP,K,KH,TETHRD,NG,NS,JM
COMMON/RCVRO4/DELT,EO(8),GOGT(8,8),H(5,8),ICOUNT,SIGMA
10 COMMON/RCVRO5/NOLDE,NOKLMN,NOAC,GAMAES(5),RDIAG(8),PHDIAG(8)
COMMON/RCVRO6/PPDIAG(8),RHAT(5,5),PHI(5,5),PA(8,8),LAMDA(5)
COMMON/RCVRO7/T(130),V(130)
COMMON/RCVRO8/XSLOE(8),ESLOE(8),ES(8)
COMMON/RCVRO9/BCVR,BO,POCRIT,CC
15 COMMON/RCVR10/XS1(8),XS(8)
DIMENSION VPK(2),VTH(2),N(2),U(130),W(130),TRG(2)
DATA GX/100./
C
IF (K.GT. 0) GO TO 50
20 C FOLG IS INITIALIZATION
IR=1
NS=NSO(IR)
NG=NGO(IR)
CALL CONTRL(3)
25 OMEGA=-20000.
JM2=JM/2
JM22=(JM2+1)/2
TSAMP=1./FSAMP
JDELAY=IFIX(2.*3.1415927*25000.*TSAMP+.5)
30 JM22=JM22+JDELAY
ICOUNT=0
XS1(3)=0.0
XS(3)=0.0
CALL CONTRL(4)
35 RETURN
50 CONTINUE
C
C FOLG PRODUCES TG1 AND TG2
40 TPST=(XS1(2)-THAMAX)/OMEGA
VPT=1+(THAMIN-XS1(2))/OMEGA
C
C FOLG PRODUCES LOG ENVELOPE SIGNAL FILTERED TO 25 KHZ
DO 70 L=1,2
45 VPEAK=0.0
DO 60 J=1,JM2
I1=J+(L-1)*JM2
JM21=JM2+1
U(I1)=20.0*ALOG10(1.+GX*V(I1))
IF((I1.EQ.1).OR.(I1.EQ.JM21)) FL25(4)=0.
50 CALL DFLTR1(U(I1),W(I1),FL25)
VPEAK=AMAX1(VPEAK,W(I1))
60 CONTINUE
VPK(L)=VPEAK
VTH(L)=VPEAK-3.
55 70 CONTINUE
IF(K.NE.1) GO TO 80
NABORT=0

```

```

NNOM=1+IFIX(2.*5.0E-5/TSAMP+.5)
N(1)=NNOM
60      N(2)=NNOM
      80      CONTINUE
      DO 140 I=1,2
      JJ=JM2-N(I)/2
      N2=(N(I)+1)/2
65      DJ=(N2-1)*TSAMP
      TG1=TPST-OJ
      TG2=TPSF-DJ
      TAUSTT=TG1
70      IF(I.EQ.2) TAUSTT=TG2
      VT=VTH(I)
      JO=(I-1)*JM2+JJ
      J1=JO+N(I)-2
      L=1
75      ISIGN=1
      DO 100 J=JO,J1
      VO=W(J)
      V1=W(J+1)
      TAU=TAUSTT+(J-JO)*TSAMP
      DELTAV=(V1-VT)*ISIGN
80      IF(DELTA.V.LT.0.0) GO TO 100
      TDWELL=TAU+TSAMP*((VT-VO)/(V1-VO))
      IF(J.NE.JO) GO TO 90
      IF(VO.GT.VT) TDWELL=TAU
85      90      IF(L.EQ.2) GO TO 130
      L=2
      ISIGN=-1
      TDWELL=TDWELL
90      100      CONTINUE
      IF(L.EQ.1) GO TO 190
      TDWELL=TAU+TSAMP
95      130      CONTINUE
      GWIDTH=TDWELL-TDWELL1
      IF((GWIDTH.LT.15.E-6).OR.(GWIDTH.GT.350.E-6)) GO TO 190
      TRG(I)=2.*GWIDTH
      TC=(TDWELL+TDWELL1)/2.
      IF(I.EQ.2) GO TO 150
      TC1=TC
140      CONTINUE
150      DELTET=TC-TC1
100      DDD=(.5E-6)*IFIX(DELLET/.5E-6+.5)
      XS1(2)=(-OMEGA/2.)*(DDD-TR)
      XS(2)=XS1(2)
      XS1(1)=(VPK(1)+VPK(2))/2.
105      XS1(1)=(10.**((XS1(1)/20.)-1.)/GX
      XS(1)=XS1(1)
      DO 160 I=1,2
      RG=TRG(I)/TSAMP
      N(I)=1+2*IFIX(RG/2.+5)
110      160      CONTINUE
      NABORT=0
      RETURN
190      ICGUNT=ICGUNT+1
      NABORT=NABORT+1
      IF(NABORT.LT.5) RETURN

```

115

```
N(1)=NNOM  
N(2)=NNOM  
XS(2)=XS1(2)  
RETURN  
END
```

```
41000B CM STORAGE USED .822 SECONDS
```

BLOCK DATA TRVRID  
COMMON/IODATA/IDNRS(6)  
DATA IDNRS(3),IDNRS(4),IDNRS(6) /1,1,0/  
END

410008'CH STORAGE USED .023 SECONDS

06-V .

```

PROGRAM ACQMP1(INPUT,OUTPUT,TAPE10=INPUT,TAPE15,TAPE7=OUTPUT,
*TAPE20)
INTEGER DATIN(4)
DIMENSION ERALFA(100),ERTHTA(100),ERALFR(100),ERTHTR(100)
5 DIMENSION X4TOX1(100),IDENTS(6),LABELS(5),NAME(10),NAME1(10)
DIMENSION NAME2(10),NAMTIM(4),TIM(102),TOTAL(100,5),YERROR(5)
DIMENSION YY(102)
EQUIVALENCE (RNAME2,NAME2(10)),(RNAME,NAME(10))
10 EQUIVALENCE (TOTAL(1,1),ERALFA(1)),(TOTAL(1,2),ERTHTA(1)),
*(TOTAL(1,3),ERALFR(1)),(TOTAL(1,4),ERTHTR(1)),
*(TOTAL(1,5),X4TOX1(1))
DATA NAME1/10HSIM. JOB: ,3*1H ,10H FILE NO: ,3*1H ,10H DATE: ,
*1H /
15 DATA NAME2/10HPLOT JOB: ,3*1H ,10H PROGRAM: ,10HACOMP1 ,2*1H ,
*10H DATE: ,1H /
DATA ALX/10./,ALY/2./,YERROR/14.,11.,8.,5.,2./,S/.,12/,H/.07/
DATA NAMTIM/10HTIME SINCE,10H START OF ,10HFIRST SCAN,10H (SECONDS
*),IBLANK/2H /
20 DATA DATIN/10HHLSSIMDATA,3*0/,YHMAX/1./
DATA LABELS/10HES ALFA ER,10HES THTA ER,10HES ALFR ER,
*10HES THTR ER,10HALFAR/ALFA/
CALL CALCOMP(20)
CALL FACTOR(1.)
CALL PLOT(+2.0,1.5,-3)
25 C
C PUT JOBNAME AND DATE IN APPROPRIATE ARRAY ELEMENTS.
C
NAME2(2)=JOBNAME(A)
RNAME2=DATE(A)
30 C
C READ NUMBER OF FILES TO BE PLOTTED.
C
READ(10,10) NPLOTS
10 FORMAT(I2)
35 C
C WRITE JOBNAME, DATE, AND NUMBER OF PLOTS TO BE MADE.
C
WRITE(7,20) NAME2(2),RNAME2,NPLOTS
20 FORMAT(10H1JOBNAME:,A10,15X,6HDATE: ,A10//1X,I2,20H FILES TO BE P
40 *LOTTED)
C
C*****300: LOOP TO PLOT EACH FILE.
C
DO 300 N=1,NPLOTS
45 C
C*****
C* READ DATA FROM DISK, WRITE ON LPR. *
C*****
C
50 C READ CURRENT FILE NAME;WRITE PLOT NUMBER AND FILE NAME.
C
READ(10,30) DATIN(2)
30 FORMAT(A10)
WRITE(7,40) (DATIN(I),I=1,2),N,NPLOTS
55 40 FORMAT (13H1INPUT FILE: ,2A10,10X,5HPLOT ,I2,4H OF ,I2/)
IR=IATTACH(6LTAPE15,DATIN)
IF(IR.EQ.0) GO TO 60

```

```

      WRITE (7,50)
60      FORMAT (20H FILE DID NOT ATTACH/)
      STOP#INPUT FILE ATTACH NOT SATISFACTORY#
      C
      C READ DATA FROM DISK AND PLACE IN PROPER LOCATION OR ARRAY.
      C
65      READ(15) DOUT,DELT,MTIMES,LGMAX,KH,TODAY,JBNAH
      READ(15) (IDENTS(I),I=1,6),KSTART
      READ(15)NRUN,OSNRDB,RHO,BETA,FSC,BHLS,BRCVR,THESEP
      C*****70
      DO 70 K=1,KH
      READ(15) ERALFA(K),ERTHTA(K),ERALFR(K),ERTHTR(K),X4TOX1(K)
70      CONTINUE
      READ(15) RHOMAX,DTHO,TDRO,BETA0,FSCO,EBETA0,EBETAH,EFSCO,EFSCM
      CALL RETURN(6LTAPE15)
      DSCODE (10,75,DOUT) NN1,IRCVR,NN2,NN3,NN4
75      FORMAT(I2,I1,I3,A1,I3)
      C
      C WRITE DATA READ FROM DISK ON THE LINEPRINTER.
      C
      WRITE(7,80) DOUT,DELT,MTIMES,LGMAX,KH,TODAY,JBNAH
80      FORMAT (1H ,A10,8X,G13.6,5X,3(5X,I3,10X),A10,8X,A10/)
      WRITE(7,90) IDENTS,KSTART
90      FORMAT (1H ,6(1X,A8,9X),3X,I3/)
      WRITE(7,100) NRUN,OSNRDB,RHO,BETA,FSC,BHLS,BRCVR,THESEP
100     FORMAT(1H ,2X,I2,4X,7(2X,G13.6)/)
      C
85      C WRITE FIRST 35 VALUES, 5 PERIODS, THEN THE LAST 3.
      C
      C*****120
      DO 120 K=1,35
      WRITE(7,110)(TOTAL(K,L),L=1,5)
90      FORMAT(1H ,5(G13.6,5X))
120     CONTINUE
      C*****140
      DO 140 K=1,5
      WRITE(7,130)
95      FORMAT(1H ,5(6X,1H.,11X))
140     CONTINUE
      KM3=KM-3
      C*****150
      DO 150 K=KM3,KM
100     WRITE(7,110) (TOTAL(K,L),L=1,5)
      CONTINUE
      WRITE(7,151)RHOMAX,DTHO,TDRO,BETA0,FSCO,EBETA0,EBETAH,EFSCO,EFSCM
151     FORMAT(1H0,9(G12.6,2X))
      C
105     C*****
      C* PLOTTING BEGINS HERE. *
      C*****
      C
      C DRAW LEFT EDGE OF THE PAGE
110     C
      CALL PLOT(-2.0,0.0,3)
      CALL PLOT(-2.0,7.0,2)
      C
      C WRITE FILE AND PLOT INFORMATION AT TOP OF PAGE.

```

```

115      C
          XH=-.5
          YH=8.7-S
          CALL SYMBOL(XH,YH,H,NAME1,0.0,90)
          C*****160.
120      DO 160 I=1,10
          NAME(I)=IBLANK
          160      CONTINUE
          NAME(2)=JBNAM
          DECODE(10,170,DOUT) NAME(6)
125      170      FORMAT(A10)
          RNAME=TODAY
          CALL SYMBOL(XH,YH,H,NAME,0.0,100)
          YH=YH-2.*S
          CALL SYMBOL(XH,YH,H,NAME2,0.0,100)
130      C
          C WRITE PLOT INFORMATION ON BOTTOM OF PAGE
          C
          200      ENCODE(81,210,NAME) (IDENTS(I),I=1,2),BMLS,DELT,KH,KSTART
          210      FORMAT(11HSCENARIO: ,A8,1H,,A6,7H, 8MLS=,F4.1,11H DEG, DELT=,
135      *F9.7,9H SEC, KH=,I3,9H, KSTART=,I3)
          YH=S
          CALL SYMBOL(XH,YH,H,NAME,0.0,81)
          220      ENCODE(81,230,NAME) DSNRDB,RHO,BETA,FSC,THESEP
          230      FORMAT(9H S/N=,F5.1,9H DB, RHO=,F5.1,7H, BETA=,F6.1,
140      *10H DEG,FSC=,F8.3,12H HZ, THESEP=,F6.3,4H DEG)
          YH=0.0
          CALL SYMBOL(XH,YH,H,NAME,0.0,81)
          240      ENCODE(59,250,NAME) (IDENTS(I),I=3,6),BRCVR
          250      FORMAT(10HRECEIVER: ,A7,2H, ,A7,2H, ,A8,1H,,A6,8H, BRCVR=,
145      *F4.1,4H DEG)
          YH=-S
          CALL SYMBOL(XH,YH,H,NAME,0.0,59)
          IF (IRCVR.NE.2) GO TO 258
          ENCODE(83,255,NAME) RHOHAX,OTHO,TORD,BETA0,FSC0
          150      255      FORMAT(39H INTERFERENCE TRACKER IDLER VALUES:,F4.1,1H,,
          CF4.1,5H DEG,,F4.1,9H DEG/SEC,F5.1,5H DEG,,F4.1,3H HZ)
          YH=-2*S
          CALL SYMBOL(XH,YH,H,NAME,0.0,83)
          ENCODE(64,256,NAME) EBETA0,EBETAM
          155      256      FORMAT(34H BETA ESTIMATE ERROR: INITIAL=,G10.3,7H,FINAL=,G10.3
          *,3HDEG)
          YH=-3.*S
          CALL SYMBOL(XH,YH,H,NAME,0.0,64)
          ENCODE(63,257,NAME) EFSC0,EFSCM
          160      257      FORMAT(34H FSC ESTIMATE ERROR: INITIAL=,G10.3,7H,FINAL=,G10.3
          *,2HHz)
          YH=-4.*S
          CALL SYMBOL(XH,YH,H,NAME,0.0,63)
          165      258      CONTINUE
          XH=0.0
          CALL FACTOR(.5)
          C
          C FILL ARPAY WITH HORIZONTAL AXIS DATA.
          C
          170      C*****260
          DO 260 K=1,KH

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A-93

```

      TIM(K)=DELT*(K-1)
260  CONTINUE
      CALL SCALE(TIM,ALX,KH,1)
175  C*****290: LOOP FOR 5 PLOTS.
      DO 290 L=1,5
          AMAX=-1.E+320
          AMIN=1.E+320
      C*****270
180  DO 270 K=1,KH
      C
      C FIND MIN AND MAX OF ERROR DATA.
      C
          AMIN=AMINI(TOTAL(K,L),AMIN)
          AMAX=AMAXI(TOTAL(K,L),AMAX)
185  270  CONTINUE
          YMAX=AMAXI(ABS(AMAX),ABS(AMIN))
          YMIN=-YMAX
190  IF(L.EQ. 5) YMIN=0.
          YINC=(YMAX-YMIN)/ALY
      C
      C FILL ARRAY WITH ERROR DATA INCLUDING YMIN AND YINC.
      C
      C*****280
195  DO 280 K=1,KH
          YY(K)=TOTAL(K,L)
          280  CONTINUE
          YY(KH+1)=YMIN
          YY(KH+2)=YINC
200  C
      C DRAW Y-AXIS AND WRITE LABEL.
      C
          YH=YERROR(L)
          YHM=-YH
205  CALL AXIS(XH,YH,LABELS(L),10,ALY,90.0,YMIN,YINC)
      C
      C MAKE PLOT OF ERROR DATA.
      C
          CALL PLOT(0.0,YH,-3)
          CALL LINE(TIM,YY,KH,1,0,0)
          CALL PLOT(0.0,YHM,-3)
210  290  CONTINUE
      C
      C MAKE HORIZONTAL AXIS FOR ALL 5 PLOTS.
215  C
          CALL AXIS(XH,YH,NAHTIM,-40,ALX,0.0,TIM(KH+1),TIM(KH+2))
      C
      C 5 PLOTS FOR THE FILE ARE NOW COMPLETED.
      C
220  CALL FACTOR(1.)
      C
      C RESET ORIGIN AT 8.5 INCHES ALONG X-AXIS
      C
          CALL PLOT(8.5,0.0,-3)
225  300  CONTINUE
      C
      C DRAW RIGHT EDGE OF FINAL PLOT.
      C

```

A-94

```
230      CALL PLOT(-2.0,0.0,3)
        CALL PLOT(-2.0,7.0,2)
        CALL ENDPLT
        STOP
        END
```

42000B CM STORAGE USED 2.817 SECONDS

A=95

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```

SUBROUTINE CLIP(A,KM,AMAX,AMIN,ISW,KC)
DIMENSION A(KH)
LOGICAL LA,LE
      C
      KC=KM
      LA=.FALSE.
      LE=.FALSE.
      ISW=0
      DO 100 KK=1,KH
      K=KH+1-KK
      IF(A(K).GE.AMIN) GO TO 10
      LE=.TRUE.
      A(K)=AMIN
      IF(ISW.EQ.0) ISW=-K
      GO TO 20
      15  IF(LA) GO TO 20
      IF((ISW.NE.0).AND.(KC.EQ.KM)) KC=K
      20  IF(A(K).LE.AMAX) GO TO 30
      A(K)=AMAX
      LA=.TRUE.
      IF(ISW.EQ.0) ISW=K
      GO TO 100
      30  IF(LE) GO TO 100
      IF((ISW.NE.0).AND.(KC.EQ.KM)) KC=K
      25  100 CONTINUE
      END

```

410008 CH STORAGE USED .171 SECONDS

## FUNCTION GAUSS(DUMMY)

```

C
C GAUSS PRODUCES INDEPENDENT PSEUDO-RANDOM NUMBERS DISTRIBUTED
C NORMALLY (0,1) BY THE DIRECT METHOD DESCRIBED IN THE FOLLOWING
5 C REFERENCE:
C M.ABRAMOWITZ,I.A.STEGUN,HANDBOOK OF MATHEMATICAL FUNCTIONS
C APPLIED MATHEMATIC SERIES#55,NATIONAL BUREAU OF STANDARD,U.S
C DEPT OF COMMERCE,NOV.1970,PAGE.953.
C THIS VERSION OF GAUSS TAKES INDEPENDENT PSEUDO-RANDOM NUMBERS
10 C UNIFORMLY DISRIBUTED ON (0,1).FROM THE COC-SUPPLIED FUNCTION
C SUBPROGRAM RANF(X).
C LOGICAL HAS
C DATA HAS/.FALSE./
C IF (DUMMY.EQ.0.0) GO TO 30
15 C CALL RANSET(0)
C HAS=.FALSE.
C 30 CONTINUE
C IF (HAS) GO TO 40
C X=SQRT(-2.*ALG(RANF(1.0)))
20 C T=6.283185308*RANF(1.)
C SAVED=X*SIN(T)
C GAUSS=X*COS(T)
C HAS=.TRUE.
C RETURN
C 25 40 GAUSS=SAVED
C HAS=.FALSE.
C RETURN
C END

```

41000B CH STORAGE USED .115 SECONDS

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OF POOR QUALITY

```

SUBROUTINE INTIO (SYMBOL,IVAL,IVALMX,I2)
INTEGER SWITCH,SLASH,SYMBOL
DATA SLASH/1H//
IF(I2)1,2,3
5 1 READ(10,10) IVAL
10 10 FORMAT(I6)
WRITE(7,20) IVAL
20 20 FORMAT(1H ,I6/)
GO TO 80
10 2 WRITE(7,30) SYMBOL,IVAL
30 30 FORMAT(1H ,A6,3H = ,I6)
READ(10,40) SWITCH,IVAL2
40 40 FORMAT(A1,I6)
IF (SWITCH .EQ. SLASH) GO TO 60
15 50 WRITE(7,50)
FORMAT(1H )
RETURN
60 60 IVAL=IVAL2
WRITE(7,70) SLASH,IVAL
20 70 70 FORMAT(1H+,15X,A1,I6/)
80 80 IF (IVAL .LE. IVALMX) RETURN
WRITE (7,90) SYMBOL,IVAL,IVALMX,SYMBOL,IVALMX
90 90 90 FORMAT (1H ,A6,2H (,I6,16H) > MAX. VALUE (,I6,1H)/
+1H ,A6,8H SET TO ,I6/)
25 IVAL=IVALMX
RETURN
3 3 WRITE(7,100) SYMBOL,IVAL
100 100 100 FORMAT(1H ,A6,3H = ,I6/)
RETURN
30 END

```

410008 CH STORAGE USED .131 SECONDS

21 05/18/79  
 11:47 AM  
 PAGE 13

```

SUBROUTINE LOGID (SYMBOL,VALUE,IZ)
LOGICAL VALUE,VAL2
INTEGER SWITCH,SLASH,SYMBOL
DATA SLASH/1H//
5      IF (IZ) 1,2,3
1      READ (10,10) VALUE
10     FORMAT (L5)
20     WRITE(7,20) VALUE
10     FORMAT(1H ,L5/)
20     RETURN
2      WRITE (7,30) SYMBOL,VALUE
30     FORMAT(1H ,A6,3H = ,L5)
40     READ (10,40) SWITCH,VAL2
15     IF (SWITCH .EQ. SLASH) GO TO 60
40     FORMAT (A1,L5)
50     WRITE(7,50)
50     FORMAT(1H )
60     RETURN
20     VALUE=VAL2
60     WRITE(7,70) SLASH,VALUE
70     FORMAT(1H+,14X,A1,L5/)
80     RETURN
3      WRITE (7,80) SYMBOL,VALUE
25     FORMAT (1H ,A6,3H = ,L5/)
80     RETURN
END

```

410008 CM STORAGE USED .104 SECONDS

A-99

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```
      SUBROUTINE MATIN (SYMBOL,A,M1,N1,M)
      C THIS INPUTS A MATRIX
      C PARAMETERS AS FOLLOWS
      C SYMBOL IS A 6 CHARACTER ALPHANUHERIC,, EG. *   A*
      5  C A IS THE ARRAY NAME
      C M1 AND N1 ARE THE DIMENSIONS OF THE DESIRED MATRIX
      C M IS THE COLUMN LENGTH OF THE ARRAY STORAGE
      DIMENSION A(M,N1)
      INTEGER SYMBOL
      10  WRITE (7,5) SYMBOL,M1,N1
      5   FORMAT(14HOINPUT MATRIX ,A6,2H (,I2,3H X ,I2,10H) BY ROWS:)
      DO 30 I=1,M1
      READ (10,10) (A(I,J),J=1,N1)
      10  FORMAT(10(G13.6))
      15  WRITE(7,20) (A(I,J),J=1,N1)
      20  FORMAT(1H ,10(G13.6))
      30  CONTINUE
      RETURN
      END
```

41000B CM STORAGE USED

.118 SECONDS

```

SUBROUTINE MATHUL(NRA,N2RA,NCA,NRB,N2RB,NCB,NRC,
*NCC,A,B,C,L)
DIMENSION A(NRA,NCA),B(NRB,NCB),C(NRC,NCC)
GO TO (101,102,103,104),L
5      101  IF(NCA.NE.N2RB) GO TO 1000
DO 200 I=1,N2RA
DO 200 J=1,NCB
C(I,J)=0.
10     200  DO 200 K=1,NCA
C(I,J)=C(I,J)+A(I,K)*B(K,J)
CONTINUE
RETURN
102   IF(N2RA.NE.N2RB) GO TO 1000
DO 400 I=1,NCA
DO 400 J=1,NCB
15     400  C(I,J)=0.
DO 400 K=1,N2RA
C(I,J)=C(I,J)+A(K,I)*B(K,J)
CONTINUE
20     400  RETURN
103   IF(NCA.NE.NCB) GO TO 1000
DO 600 I=1,N2RA
DO 600 J=1,N2RB
25     600  C(I,J)=0.
DO 600 K=1,NCA
C(I,J)=C(I,J)+A(I,K)*B(J,K)
CONTINUE
30     600  RETURN
104   IF(N2RA.NE.NCB) GO TO 1000
DO 800 I=1,NCA
DO 800 J=1,N2RB
35     800  C(I,J)=0.
DO 800 K=1,N2RA
C(I,J)=C(I,J)+A(K,I)*B(J,K)
CONTINUE
40     800  RETURN
1000  WRITE(7,2000)
2000  FORMAT(5X,'CHECK THE PROGRAM FOR MISTAKES')
RETURN
END

```

-41000B CM STORAGE USED :427 SECONDS

```

SUBROUTINE MATOUT(SYMBOL,A,M1,N1,M,IZ)
C THE VARIABLES IN SUBROUTINE MATOUT ARE AS FOLLOWS
C SYMBOL IS A 6-CHARACTER ALPHANUMERIC EG. A*
C A* IS THE ARRAY NAME
5 C M1, AND N1 ARE THE DIMENSIONS (VERT, HORIZ) OF THE
C PRINTOUT
C M IS THE COLUMN LENGTH OF A* AS DIMENSIONED IN THE
C CALLING PROGRAM
10 C IZ=0 CAUSES DOUBLE SPACING, OTHERWISE SINGLE SPACING
DIMENSION A(M,N1)
INTEGER SYMBOL
WRITE(7,5) SYMBOL
5 FORMAT(*0*,A6,/)
DO 10 I=1,M1
15 WRITE(7,20) (A(I,J),J=1,N1)
20 FORMAT(10(1X,G12.5))
IF(IZ.EQ.0) WRITE(7,15)
15 FORMAT(* *)
20 CONTINUE
RETURN
END

```

410008 CH STORAGE USED .098 SECONDS

```

SUBROUTINE MATSH(A,B,C,L,MA,NA,MB,MB,NB,MC,M2C,NC,K)
DIMENSION A(MA,NA),B(MB,NB),C(MC,NC)
GO TO (101,102,102,101),L
5      101 IF(M2B.NE.M2C.OR.(NB.NE.NC)) GO TO 1000
      GO TO 110
      102 IF(NB.NE.M2C.OR.(M2B.NE.NC)) GO TO 1000
      110 IMAX=MB
      JMAX=NB
      IF(L.LE.2) GO TO 200
10      IMAX=NB
      JMAX=M2B
      200 IF(IMAX.GT.MA.OR.JMAX.GT.NA) GO TO 1000
      DO 600 I=1,IMAX
      DO 600 J=1,JMAX
15      A(I,J)=B(I,J)+((-1)**K)*C(I,J)
      IF(L.EQ.2) A(I,J)=B(J,I)+((-1)**K)*C(I,J)
      IF(L.EQ.3) A(I,J)=B(I,J)+((-1)**K)*C(J,I)
      IF(L.EQ.4) A(I,J)=B(J,I)+((-1)**K)*C(J,I)
      600 CONTINUE
20      RETURN
      1000 WRITE(7,10000)
      10000 FORMAT(5X,'MATRICES NOT CONFORMABLE')
      RETURN
      END

```

41000B CM STORAGE USED .336 SECONDS

```

SUBROUTINE MULPLT(B,A,NRY,NP,NV,XNAME,YNAME,EYMIN,EYMAX,SYH)
INTEGER LINE(61),BLANK,DOT,SYH(NP),LO,HI
LOGICAL MANUAL
INTEGER XNAME(2),YNAME(2,NV)
5 DIMENSION KP1(10),YMAX(10),YMIN(10),KK(10),B(NP),A(NRY,NV)
DATA BLANK,DOT/1H,1H.,/HI,LO/94,1H2/
IF(NRY.LT.NP) STOP#NRY<NP,WRONG#
MANUAL=.TRUE.
IF(EYMAX.EQ.EYMIN) MANUAL=.FALSE.
10 IF(EYMIN.GT.EYMAX) PAUSE#YOU MADE A MISTAKE INPUTTING LIMITS#
DO 10 I=1,NV
YMIN(I)=1.E322
YMAX(I)=-1.E322
CONTINUE
15 DO 30 J=1,NV
DO 20 I=1,NP
IF(A(I,J).GT.YMAX(J)) YMAX(J)=A(I,J)
IF(A(I,J).LT.YMIN(J)) YMIN(J)=A(I,J)
CONTINUE
20 CONTINUE
IF(MANUAL) GO TO 41
YYMIN=YMIN(1)
YYMAX=YMAX(1)
DO 40 I=2,NV
IF(YMAX(I).GT.YMAX(I-1)) YYMAX=YMAX(I)
IF(YMIN(I).LT.YMIN(I-1)) YYMIN=YMIN(I)
40 CONTINUE
GO TO 45
30 41 YYMAX=EYMAX
YYMIN=EYMIN
45 RANGE=YYMAX-YYMIN
KAXIS=60.*(-YYMIN/RANGE)+1.5
IF(YYMIN.GT.0.0) KAXIS=1
IF(YYMAX.LT.0.0) KAXIS=61
35 DIS=RANGE/60.
MIN=1
XMIN=ABS(B(1))
DO 50 J=2,NP
IF(ABS(B(J)).GE.XMIN) GO TO 50
40 XMIN=ABS(B(J))
MIN=J
50 CONTINUE
60 CONTINUE
DO 70 K4=1,3
45 WRITE(7,80)
70 CONTINUE
80 FORMAT(1H0)
WRITE(7,90)
90 FORMAT(2X,7HLEGEND:)
50 DO 100 I=1,NV
WRITE(7,110) SYH(I),YNAME(1,I),YNAME(2,I),YMIN(I),YMAX(I)
100 CONTINUE
110 FORMAT(8X,A1,2X,A8,2X,A8,5X,4HMIN=,G13.6,3X,4HMAX=,
*G13.6)
55 WRITE(7,80)
WRITE(7,80)
WRITE(7,80)

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J. BOB O.  
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115 WRITE(7,115) XNAME(1),YYMIN,YYMAX
    FORMAT(2X,A8,5X,14HORDINATE AXIS:,6H MIN=,G13.6,
60 *7H MAX=,G13.6)
    WRITE(7,120) XNAME(2),DIS
120 FORMAT(3X,A8,30X,10HINCREMENT=,2X,G13.6,/)
    DO 130 J=1,61
    LINE(J)=BLANK
65 130 CONTINUE
    DO 170 J2=1,NP
    IF(J2.EQ.MIN) GO TO 180
    LINE(KAXIS)=DOT
    DO 140 I=1,NV
70 X=60.0*((A(J2,I)-YYMIN)/RANGE)
    KK(I)=X+1.5
    IF(KK(I).GT.61) LINE(61)=HI
    IF(KK(I).LT.1) LINE(1)=LO
    IF(KK(I).LT.1.OR.KK(I).GT.61) GO TO 135
75 LINE(KK(I))=SYH(I)
135 IF(KK(I).GT.61) KK(I)=61
    IF(KK(I).LT.1) KK(I)=1
140 CONTINUE
    WRITE(7,150) B(J2),LINE
80 150 FORMAT(1X,G13.6,6X,61A1)
    DO 160 I=1,NV
    LINE(KK(I))=BLANK
160 CONTINUE
170 CONTINUE
85 GO TO 211
180 CONTINUE
    DO 190 J=1,61
    LINE(J)=DOT
90 190 CONTINUE
    DO 200 I=1,NV
    X=60.0*((A(MIN,I)-YYMIN)/RANGE)
    KP1(I)=X+1.5
    IF(KP1(I).LT.1) LINE(1)=LO
    IF(KP1(I).GT.61) LINE(61)=HI
95 IF(KP1(I).LT.1.OR.KP1(I).GT.61) GO TO 200
    LINE(KP1(I))=SYH(I)
200 CONTINUE
    WRITE(7,150) B(J2),LINE
100 DO 210 J=1,61
    LINE(J)=BLANK
210 CONTINUE
    GO TO 170
211 DO 220 K5=1,3
    WRITE(7,80)
105 220 CONTINUE
    EYHAX=YYHAX
    EYMIN=YYMIN
230 CONTINUE
    RETURN
110 END

```

410008 CH STORAGE USED .016 SECONDS

```

SUBROUTINE PLOTR(B,A,NP,XNAME,YNAME,EMIN,EMAX,ISC)
DIMENSION B(NP),A(NP),LINE(61)
INTEGER HI,LO,LINE,BLANK,DOT,STAR
LOGICAL MANUAL,SYME
5  INTEGER XNAME(2),YNAME(2)
DATA BLANK,DOT,STAR/1H,1H,,1H*/,HI/94/,LO/1H2/
SYME=.FALSE.
MANUAL=.TRUE.
10 IF(EMAX.EQ.EMIN) MANUAL=.FALSE.
IF(EMIN.GT.EMAX) STOP*YOU MADE A MISTAKE INPUTTING EMIN % EMAX#
IISC=ISC
IF(MANUAL) IISC=1
IF(MANUAL) GO TO 11
15 YMIN=1.E38
YMAX=-1.E38
DO 10 I=1,NP
IF(A(I).GT.YMAX) YMAX=A(I)
IF(A(I).LT.YMIN) YMIN=A(I)
20 CONTINUE
GO TO 19
11 YMAX=EMAX
YMIN=EMIN
19 XMIN=ABS(B(1))
MIN=1
25 DO 20 J=2,NP
IF(ABS(B(J)).GE.XMIN) GO TO 20
XMIN=ABS(B(J))
MIN=J
20 CONTINUE
30 IF(IISC.EQ.0) GO TO 21
RANGE=YMAX-YMIN
KAXIS=60.*(-YMIN/RANGE)+1.5
IF(YMIN.GT.0.0) KAXIS=1
IF(YMAX.LT.0.0) KAXIS=61
35 DIS=RANGE/60.
GO TO 30
21 IF(YMIN.GT.0.) GO TO 22
IF(YMAX.LT.0.) GO TO 23
40 KAXIS=31
SYME=.TRUE.
ABY=ABS(YMIN)
RANGE=AMAX1(YMAX,ABY)
DIS=RANGE/30.
GO TO 30
45 22 KAXIS=1
RANGE=YMAX
DIS=RANGE/60.
GO TO 30
50 23 KAXIS=61
RANGE=-YMIN
DIS=RANGE/60.
30 CONTINUE
DO 40 K4=1,3
WRITE(7,50)
55 40 CONTINUE
50 FORMAT(1H0)
WRITE(7,60) XNAME(1),YNAME(1),YMIN,YMAX

```

```

60  FORMAT(2X,A8,7X,A8,3X,20HORDINATE AXIS: MIN=,G13.6,3X,4HMAX=,
    *G13.6)
60  WRITE(7,70) XNAME(2),YNAME(2),DIS
70  FORMAT(2X,A8,7X,A8,25X,10HINCREMENT=,G13.6,/)
    DO 80 J=1,61
    LINE(J)=BLANK
80  CONTINUE
65  DO 100 J2=1,NP
    IF(J2.EQ.MIN) GO TO 110
    X=60.0*((A(J2)-YMIN)/RANGE)
    IF(IISC.EQ.0.AND.YMIN.GT.0.) X=60.0*(A(J2)/RANGE)
    IF(SYME) X=30.0*(A(J2)/RANGE)+30.
70  K=X+1.5
    LINE(KAXIS)=DOT
    IF(K.GT.61) LINE(61)=HI
    IF(K.GT.61) KMAX=61
    IF(K.GT.61) GO TO 89
75  IF(K.LT.1) LINE(1)=LO
    IF(K.LT.1) KMAX=KAXIS
    IF(K.LT.1) GO TO 89
    LINE(K)=STAR
    KMAX=KAXIS
80  IF(K.GT.KMAX) KMAX=K
89  WRITE(7,90) B(J2),A(J2),(LINE(N4),N4=1,KMAX)
90  FORMAT(1X,G13.6,2X,G13.6,2X,61A1)
    IF(K.GT.61) LINE(61)=BLANK
    IF(K.GT.61) GO TO 100
85  IF(K.LT.1) LINE(1)=BLANK
    IF(K.LT.1) GO TO 100
    LINE(K)=BLANK
100 CONTINUE
    GO TO 145
90 110 CONTINUE
    DO 120 J=1,61
    LINE(J)=DOT
120 CONTINUE
    X=60.0*((A(MIN)-YMIN)/RANGE)
95  IF(IISC.EQ.0.AND.YMIN.GT.0.) X=60.0*(A(J2)/RANGE)
    IF(SYME) X=30.0*(A(J2)/RANGE)+30.
    KP1=X+1.5
    IF(KP1.GT.61) LINE(61)=HI
    IF(KP1.LT.1) LINE(1)=LO
100 IF(KP1.LT.1.OR.KP1.GT.61) GO TO 129
    LINE(KP1)=STAR
129 WRITE(7,130) B(J2),A(J2),LINE
130 FORMAT(1X,G13.6,2X,G13.6,2X,61A1)
    DO 140 J=1,61
105 LINE(J)=BLANK
140 CONTINUE
    GO TO 100
145 DO 150 K5=1,3
    WRITE(7,50)
110 CONTINUE
    EHAX=YMAX
    EHIN=YMIN
160 CONTINUE
    RETURN

```

115 ..... END .....  
410008 CH STORAGE USED ..... .817 SECONDS .....

A-108



```

SUBROUTINE REALIO(SYMBOL,VALUE,IZ)
INTEGER ISW,ISLASH,SYMBOL
DATA ISLASH/1H//
IF(IZ) 1,2,3
5      1  READ(10,10) VALUE
      10  FORMAT(G13.6)
      20  WRITE(7,20) VALUE
      20  FORMAT(1H,G13.6/)
      RETURN
10     2  WRITE(7,30) SYMBOL,VALUE
      30  FORMAT(1H,A6,3H = ,G13.6)
      READ(10,40) ISW,VAL2
      40  FORMAT(A1,G13.6)
      IF (ISW .EQ. ISLASH) GO TO 60
15     50  WRITE(7,50)
      50  FORMAT(1H )
      RETURN
      60  VALUE=VAL2
      20  70  WRITE(7,70) ISLASH,VALUE
      70  FORMAT(1H+,22X,A1,G13.6/)
      RETURN
      3  80  WRITE(7,80) SYMBOL,VALUE
      80  FORMAT(1H,A6,3H = ,G13.6/)
      RETURN
25     END
410008 CH STORAGE USED .098 SECONDS

```

A-110

```

SUBROUTINE RETURN(LFN)
DIMENSION FIT(1)
IX=INOXFIT(LFN,FIT)
CALL STOREF(FIT(IX),2LCF,1LU)
CALL CLOSEM(FIT(IX))
RETURN
END

```

5

41000B CM STORAGE USED

.047 SECONDS

A-111

```
FUNCTION SATU(X,XL)
IF (ABS(X).LE.XL) GO TO 2
SATU=SIGN(XL,X)
RETURN
SATU=X
RETURN
END
```

```
41000B CH STORAGE USED .046 SECONDS
```

```

PROGRAM PCRMP1(INPUT,OUTPUT,TAPE10=INPUT,TAPE15,TAPE7=OUTPUT,
*TAPE20)
INTEGER DATIN(4)
DIMENSION TIM(102),YY(102), TODAY(3),PKVAL(3),YPK(3),ALYSNR(3)
5 DIMENSION EMEAN(3),ERMS(3),ESTDEV(3),TCOUNT(3),YMIN(3),YMAX(3)
DIMENSION IDENT(6,3),CSNRTO(102),THESEP(102),JBNAM(3),CSNRFR(102)
DIMENSION DDUT(3),ABORT(100),THESE(100,3)
DIMENSION NAME1(10),NAME2(10),NAME(10),YPEAK(3),ALYERR(3)
10 DIMENSION NAMSEP(3),NAMSNR(2),NAMTIM(4)
DIMENSION YDRERR(3,3)
EQUIVALENCE (RNAME2,NAME2(10)),(RNAME,NAME(10))
DATA YHMAX/1.0/,H/O.07/,SIZE/O.5/,S/.12/
DATA NAME1/10HSIM. JOB: ,3*1H ,10H FILE NO: ,3*1H ,10H , DATE: ,
*1H /
15 DATA NAME2/10HPLOT JOB: ,3*1H ,10H PROGRAM: ,10HPCRMP1 ,2*1H ,
*10H DATE: ,1H /
DATA NAME/10*2H /
DATA DATIN/10HMLSSIMDATA,3*0/
DATA NAMSNR/10HCNR (TD-S,10HCAN) /
20 DATA NAMSEP/10H SEPARAT,10HIGN ANGLE ,10H(OEG.) /
DATA NAMTIM/10H TIME SINCE,10H START OF ,10HFIRST SCAN,10H,(SECONDS
*)/
DATA ALXTIM/5.0/
DATA ALYERR/4.0,2.0,1.5/
25 DATA ALYSNR/2.0,1.5,1./
DATA YPK/1.31,31,.07/
DATA YDRERR/4.0,0.0,0.0,6.0,3.25,0.0,6.5,4.5,2.5/
DATA YDRSNR/1.0/,IBLANK/2H /
30 C
C
C
CALL CALCOMP(20)
CALL FACTOR(1.)
CALL PLOT(2.00,1.50,-3)
35 NAME2(2)=JOBNAME(A)
RNAME2=DATE(A)
READ(10,10) NPLOTS
10 FORMAT(I2)
WRITE(7,20) NAME2(2),RNAME2,NPLOTS
40 20 FORMAT(11H1JOBNAME: ,A10,15X,7HDATE: ,A10//1H ,I3,
*17H PLOTS TO BE DONE)
C*****320
DO 320 NP=1,NPLOTS
45 30 READ(10,30) NFILES
FORMAT(I1)
C*****180
DO 180 N=1,NFILES
50 40 READ(10,40) DATIN(2)
FORMAT(53X,A10)
WRITE(7,50) NP,NPLOTS, (DATIN(I),I=1,2),N,NFILES
50 50 FORMAT(6H1PLOT ,I2,4H OF ,I2,12H INPUT FILE ,2A10,2H (,I3,
*4H OF ,I3,2H):/)
IR=IATTACH(6LTAPE15,DATIN)
IF(IR.EQ.0) GO TO 70
55 WRITE(7,60)
STOP*INPUT FILE ATTACH NOT SATISFACTORY*
60 60 FORMAT(20H FILE DID NOT ATTACH/)

```

A-113

ORIGINAL PAGE IS  
OF POOR QUALITY

```

C
C READ FILE INTO NTH ELEMENTS OF ARRAYS, WHERE NECESSARY
60 C
70 READ(15) DOUT(N), DELT, MTIMES, LGMAX, KM, TODAY(N), JBNAM(N)
   READ(15) (IDENTS(I,N), I=1,6)
   READ (15) NRUN, DSNRDB, RHD, BETA, FSC, BHLS, BRCVR
C*****80
65 DO 80 K=1, KM
   READ(15) CSNRTO(K), CSNRFR(K), THESER(K,N), ABBORT(K), THESEP(K)
80 CONTINUE
   READ(15) EMEAN(N), ERMS(N), ESTDEV(N), TDCUNT(N), YMIN(N), YMAX(N)
   CALL RETURN(6LTAPE15)
70 C
C WRITE DATA ON LINEPRINTER AS IN CONTROL
C
   WRITE(7,90) DOUT(N), DELT, MTIMES, LGMAX, KM, TODAY(N), JBNAM(N)
75   FORMAT(1H ,A10,8X,G13.6,5X,3(5X,I3,10X),A10,8X,A10/)
   WRITE(7,100) (IDENTS(I,N), I=1,6)
100  FORMAT(1H ,6(1X,A6,9X)/)
   WRITE(7,110) NRUN, DSNRDB, RHD, BETA, FSC, BHLS, BRCVR
110  FORMAT(1H ,5X,I2,6X,6(5X,G13.6)/)
C*****130
80 DO 130 K=1,35
   WRITE(7,120) CSNRTO(K), CSNRFR(K), THESER(K,N), ABBORT(K), THESEP(K),K
120  FORMAT(1H ,3(G13.6,5X),6X,A1,11X,G13.6,5X,I7)
130 CONTINUE
C*****150
85 DO 150 K=1,5
   WRITE(7,140)
140  FORMAT(1H ,5(6X,1H,,11X))
150 CONTINUE
   KM3=KM-3
90 C*****160
   DO 160 K=KM3,KM
   WRITE(7,120) CSNRTO(K), CSNRFR(K), THESER(K,N), ABBORT(K), THESEP(K),K
160 CONTINUE
   WRITE(7,170) EMEAN(N), ERMS(N), ESTDEV(N), TDCUNT(N), YMIN(N), YMAX(N)
95 170  FORMAT(1H0,6(G13.6,5X)/)
180 CONTINUE
C
C DRAW LEFT EDGE OF THE PAGE
100 CALL PLOT(-2.0,0.0,3)
   CALL PLOT(-2.0,7.0,2)
C
C WRITE INFORMATION ON THE TOP OF THE PAGE
C
   YH=8.8-S
105  XH=-0.5
   CALL SYMBOL(XH,YH,H,NAME1,0.0,90)
   Y2H=8.8-(NFILES+1)*S
C*****190
110 DO 190 I=1,10
   NAME(I)=IBLANK
190 CONTINUE
C*****200
   DO 200 N=1,NFILES
   NAME(2)=JBNAM(N)

```

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```

115      DECODE(10,195,DDUT(N)) NAME(6),
      195      FORMAT(A10)
      RNAME=TODAY(N)
      Y1H=8,8-N*S
120      200      CALL SYMBOL(XH,Y1H,H,NAME,0.0,100)
      CONTINUE
      CALL SYMBOL(XH,Y2H,H,NAME2,0.0,100)
      C
      C ORIGINATE TIME DELAY
      C
125      KM1=KM+1
      KM2=KM+2
      C*****210
      DG 210 K=1,KM
      K1=K-1
130      TIM(K)=DELT*K1
      C
      C FIND MAX,MIN,AND INCREMENT FOR CSNTRD
      C
      210      CONTINUE
135      CSNRTO(KM1)=0.0
      SNRINC=IFIX(CSNRTO(1))+.5)
      CSNRTO(KM2)=SNRINC
      YMM=YMMAX
      YPIX=-1.E+320
140      ALX=ALXTIM/SIZE
      CALL SCALE(TIM,KM,1)
      C*****220
      DO 220 N=1,NFILES
      YPEAK(N)=AMAX1(-YMIN(N),YMAX(N))
145      YMIX=AMAX1(YPEAK(N),YMIN(N))
      220      CONTINUE
      YMM=AMIN1(YMM,YMIX)
      C*****260
150      DG 260 N=1,NFILES
      C*****230
      DO 230 K=1,KM
      YY(K)=THESER(K,N)
      ZS=SIGN(YMM,YY(K))
      IF(ABS(YY(K)).GE.YMM) YY(K)=ZS*YMM
155      230      CONTINUE
      ENCODE(23,240,PKVAL) YPEAK(N)
      240      FORMAT(13HPEAK VALUE = ,F5.3,5H DEG.)
      YY(KM1)=-YMM
      YY(KM2)=2.*SIZE*YMM/ALYERR(NFILES)
160      CALL FACTOR(1.)
      CALL PLOT(0.0,YORERR(N,NFILES),-3)
      XB=-3.0*S
      YB=YPK(NFILES)
      CALL SYMBOL(XB,YB,H,PKVAL,90.0,23)
165      CALL FACTOR(SIZE)
      ALY=ALYERR(NFILES)/SIZE
      ENCODE(17,250,NAMERR) IDENT(3,N)
      250      FORMAT(A8,9H RECEIVER)
      CALL AXIS(0.0,0.0,NAMERR,17,ALY,90.0,YY(KM1),YY(KM2))
170      CALL LINE(TIM,YY,KH,1,0,0)
      CALL FACTOR(1.0)

```

```

260 CALL PLOT(0.0,-YDRERR(N,NFILES),-3)
CONTINUE
175 CALL PLOT(0.0,YDRSNR,-3)
CALL FACTOR(SIZE)
ALLY=ALYSNR(NFILES)/SIZE
CALL AXIS(0.0, 0.0,NAMTIM,-40,ALX,0.0,TIM(KH1),TIM(KH2))
CALL AXIS(0.0,0.0,NAMSNR,14,ALLY,90.0,CSNRTO(KM1),CSNRTO(KH2))
180 DTS=THESEP(2)-THESEP(1)
TSMIN=THESEP(1)
TSINC=(DTS/DELTA)*TIM(KH2)
EPS=-.5/SIZE
CALL AXIS(0.0, EPS,NAMSEP,-30,ALX,0.0,TSMIN,TSINC)
185 CALL LINE(TIM,CSNRTO,KH,1,0,0)
CALL FACTOR(1.0)
CALL PLOT(0.0,-YDRSNR,-3)
XH=-.44
YH=-S
190 ENCODE(93,270,NAME)DSNRDB,RHO,BETA,FSC,KM,BHLS,IDENTS(2,1)
270 FORMAT(4HS/N, F5.1,5H DB, 5H RHO=,F5.2,2H, 5HBETA=,F6.1,6H DEG,
*,4HFSC=,F6.1,5H HZ, 3HKM=,I4,8H SCANS, 5HBHLS=,F5.2,2H, A8)
CALL SYMBOL(XH,YH,H,NAME,0.0,93)
YH=YH-S
195 C*****310
OO 310 N=1,NFILES
YH=YH-S
DECODE(10,280,DDUT(N)) AA,BB,CC
280 FORMAT(A2,A1,A7)
DECODE(1,285,88) IRCVR
200 FORMAT(I1)
IF(IRCVR.EQ.1) ENCODE(78,290,NAME) (IDENTS(I,N),I=3,5),TCOUNT(N),
*ERMS(N)
290 FORMAT(A7,3H: ,A7,2H, ,A8,2H, ,F6.2,20HX OF SCANS ABORTED, ,
*5HERMS=,G13.6,5H DEG.)
205 IF(IRCVR.NE.1) ENCODE(78,300,NAME) (IDENTS(I,N),I=3,6),BRCVR,
*ERMS(N)
300 FORMAT(A7,3H: ,A7,2H, ,A8,2H, ,A6,8H, BRCVR=,F4.2,8H DEG., ,
*5HERMS=,G13.6,5H DEG.)
CALL SYMBOL(XH,YH,H,NAME,0.0,78)
210 310 CONTINUE
CALL PLOT(8.5,0.0,-3)
320 CONTINUE
CALL PLOT(-2.0,0.0,3)
CALL PLOT(-2.0,7.0,2)
215 CALL ENDPLT
STOP
END

```

42000B CM STORAGE USED 4.128 SECONDS

```

PROGRAM RLOGSW (OUTPUT,TAPE10,TAPE7=OUTPUT)
C THIS READS <SWA>, <SWB>, % <RAB>
REAL NC(1000),NS(1000)
INTEGER FNA(4)
5 COMMON/DATA1/QA,B,U,WAA,WBA,WA2A,WB2A,WABA,WA,WB
COMMON/DATA2/LMAX1,COSB,JNHAX,NC,NS,ALNLHX,RIJMAX
DIMENSION QAI(25),BJ(12),BULK(12,25,3),DATUM(5),COSB(101)
EQUIVALENCE (WAA,DATUM(1))
10 DATA PI/3.1415927/,LMAX/100/,JNHAX/1000/,JBMAX/12/
DATA FNA/10HLSLOGSWCD,1LC,2*0/

C FOLLOWING READS DATA FROM FILE
IX=IATTACH(6LTAPE10,FNA)
15 READ (10) LMAX1,JNHAX
READ (10) IQMAX,(QAI(I),I=1,IQMAX)
READ (10) JBMAX,(BJ(J),J=1,JBMAX)
READ (10) ((BULK(J,I,K),J=1,JBMAX),I=1,IQMAX),K=1,3)

C
20 DO 80 K=1,3
IF(K.EQ.1) WRITE(7,870)
IF(K.EQ.2) WRITE(7,871)
IF(K.EQ.3) WRITE(7,872)
870 FORMAT (1H1,///,5HOSWA:)
871 FORMAT (1H1,///,5HOSWB:)
25 872 FORMAT (1H1,///,5HORAB:)
WRITE (7,880) (BJ(J),J=1,JBMAX)
880 FORMAT (4HOB =,8X,12(2X,F6.3,2X))
WRITE (7,885)
885 FORMAT (4H QA:)
30 DO 70 I=1,IQMAX
WRITE (7,890) QAI(I),(BULK(J,I,K),J=1,JBMAX)
890 FORMAT (1H ,G11.4,12(1X,G9.2))
70 CONTINUE
80 CONTINUE
35 STOP
END

```

41008 CH. STORAGE USED .300 SECONDS

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```

PROGRAM WLOGSW(INPUT,OUTPUT,PUNCH,TAPE12,TAPE5=INPUT,TAPE7=OUTPUT,
1TAPE6=PUNCH)
C THIS COMPUTES <WA>, <WB>, <SWA>, <SWB>, X <RAB>
5 REAL NC(1000),NS(1000)
COMMON/DATA1/QA,B,U,WAA,WBA,WA2A,WB2A,WABA,WA,WB
COMMON/DATA2/LMAX1,COSB,JNMAX,NC,NS,ALNLHX,RIJMAX
DIMENSION QAI(25),BJ(12),DATUM(5)
10 DIMENSION DATA3(12,25,3),BULK(12,25,3),COSB(101),DATA4(937)
EQUIVALENCE (WAA,DATUM(1)),(QAI(1),DATA4(1)),(BJ(1),DATA4(26))
EQUIVALENCE (DATA4(38),DATA3(1,1,1))
C
DATA PI/3.1415927/,LMAX/100/
DATA JNMAX/1000/,IQMAX/25/,JBMAX/12/
15 DATA QAI/.1,.1778,.3162,.5623,1.,1.778,3.162,5.623,10.,
*17.78,31.62,56.23,100.,177.8,316.2,562.3,1000.,1778.,3162.,
*5623.,1.E4,1.E5,1.E6,1.E7,1.E8/
DATA BJ/.01,.02,.04,.06,.1,.2,.3,.5,.7,.9,.95,.99/
C
20 SQ22=SQRT(.5)
READ(5,8)LMAX,JNMAX
8 FORMAT(2I5)
WRITE(7,9) LMAX,JNMAX
9 FORMAT(7H LMAX= ,I5/8H JNMAX= ,I5/)
BETA2=PI/LMAX
25 LMAX1=LMAX+1
DO 10 L=1,LMAX1
COSB(L)=COS((L-1)*BETA2)
10 CONTINUE
DO 15 J=1,JNMAX
30 NC(J)=SQ22*GAUSS(0.)
NS(J)=SQ22*GAUSS(0.)
15 CONTINUE
ALMAX1=LMAX1
35 ALNLHX=ALOG(ALMAX1)
RIJMAX=JNMAX*ALMAX1
RIJMAX=1./RIJMAX
WRITE (7,800) LMAX1
800 FORMAT (1H ,I4,25H VALUES OF BETA (0 TO PI))
WRITE (7,810) LMAX1
40 810 FORMAT (1H ,I4,27H VALUES OF BETA=U (0 TO PI))
WRITE (7,820) JNMAX
820 FORMAT (1H ,I5,34H VALUES OF NOISE SAMPLES (NCJ,NSJ))
30 CONTINUE
45 830 WRITE (7,830) QAI(1),QAI(2),QAI(IQMAX),IQMAX
830 FORMAT (4H QA=,G13.6,2H , ,G13.6,6H , , , ,G13.6,2H (,I2,
* 8H) VALUES)
WRITE (7,840) BJ(1),BJ(2),BJ(JBMAX),JBMAX
840 FORMAT (3H B=,F7.4,2H , ,F7.4,6H , , , ,F7.4,2H (,I2,
* 8H) VALUES)
50 DO 60 I=1,IQMAX
QA=QAI(I)
DO 50 J=1,JBMAX
B=BJ(J)
CALL WAVGS
55 DO 45 K=1,3
BULK(J,I,K)=DATUM(K+2)
45 CONTINUE

```

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```

50 CONTINUE
60 CONTINUE
60 C CHANGES TO LOG
   DO 100 I=1,IQMAX
   DO 100 J=1,JBMAX
   DATA3(J,I,K)=ALOG(SQRT(BULK(J,I,K)))
65 100 CONTINUE
   DO 200 I=1,IQMAX
   DO 200 J=1,JBMAX
200 DATA3(J,I,3)=BULK(J,I,3)/SQRT(BULK(J,I,1)*BULK(J,I,2))
   C PUNCHES CARDS
70  IIJJ=3*IQMAX*JBMAX+IQMAX+JBMAX
   WRITE(6,900) LMAX1,JNMAX,IQMAX,JBMAX,1
900  FORMAT(4(I5,5X),26X,*MLSLOGSWCOC*,I3)
   WRITE(6,901) ((DATA4(I,I+1),I=1,IIJJ)
901  FORMAT(G23.16,43X,*MLSLOGSWCOC*,I3)
75  C WRITES ON DATA FILE LOGSW2.DAT
   WRITE(12) LMAX1,JNMAX
   WRITE(12) IQMAX,(QAI(I),I=1,IQMAX)
   WRITE(12) JBMAX,(BJ(J),J=1,JBMAX)
   WRITE(12) ((DATA3(J,I,K),J=1,JBMAX),I=1,IQMAX),K=1,3)
80  C WRITES ON DECRITER
   C
   DO 80 K=1,3
   IF(K.EQ.1) WRITE(7,870)
   IF(K.EQ.2) WRITE(7,871)
85  IF(K.EQ.3) WRITE(7,872)
   870  FORMAT(/,1H0,4HSA:)
   871  FORMAT(/,1H0,4HSWB:)
   872  FORMAT(/,1H0,4HRA:)
   WRITE(7,880) (BJ(J),J=1,JBMAX)
90  880  FORMAT(4HOB =,8X,12(2X,F6.3,2X))
   WRITE(7,885)
   885  FORMAT(4H QA:)
   DO 70 I=1,IQMAX
   WRITE(7,890) QAI(I),(DATA3(J,I,K),J=1,JBMAX)
95  890  FORMAT(1H ,G11.4,12(1X,G9.2))
   70  CONTINUE
   80  CONTINUE
   STOP
   END

```

410008 CH STORAGE USED .827 SECONDS

A-119

```

SUBROUTINE WAWB
  CTHIS COMPUTES A SAMPLE EACH OF THE PROCESSES WA % WB
  REAL NC(1000),NS(1000)
  COMMON/DATA1/QA,B,U,WAA,WBA,WA2A,WB2A,WAB,A,WA,WB
  COMMON/DATA2/LMAX1,COSB,JNHAX,NC,NS,ALNLMX,RIJMAX
  DIMENSION HA(101),HB(101),COSB(101),G(101),H(101)

  C
  GMAX=-1.E+322
  HMAX=1.
  HAMAX=1.
  HBMAX=1.
  DO 20 L=1,LMAX1
    COSBL=COSB(L)
    DCBL1=AMAX1(1.+B*COSBL,0.)
    ABC=QA*BCBL1
    UABC=U*ABC
    RAD=2.*SQRT(UABC)
    RAD1=SQRT(1.+UABC)
    GL=2.*(RAD1-1./(1.+RAD))-ABC
    G(L)=GL
    HL=1./SQRT(1.+6.2831846*RAD)
    H(L)=HL
    HAL=(-1.+U/RAD1)*HL
    HA(L)=HAL
    HBL=HAL*COSBL
    HB(L)=HBL
    GMAX=AMAX1(GL,GMAX)
    HMAX=AMAX1(HL,HMAX)
    HAMAX=AMAX1(ABS(HAL),HAMAX)
    HBMAX=AMAX1(ABS(HBL),HBMAX)
  20 CONTINUE
  GZ=GMAX-741.
  FZ=ALOG(HMAX)+GZ
  GM=FZ+ALNLMX
  GZ=GZ+ALNLMX
  GMA=GZ+ALOG(HAMAX)
  GMB=GZ+ALOG(HBMAX)
  FS=0.
  FSA=0.
  FSB=0.
  DO 30 L=1,LMAX1
    GL=G(L)
    GLM=GL-GM
    GLMA=GL-GMA
    GLMB=GL-GMB
    IF (GLM.GE.-674.) FS=FS+EXP(GLM)*H(L)
    IF (GLMA.GE.-674.) FSA=FSA+EXP(GLMA)*HA(L)
    IF (GLMB.GE.-674.) FSB=FSB+EXP(GLMB)*HB(L)
  30 CONTINUE
  WA=(HAMAX/HMAX)*(FSA/FS)
  WB=(HBMAX/HMAX)*(FSB/FS)
  RETURN
  END

```

41000B CM STORAGE USED

.399 SECONDS

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```

SUBROUTINE WAVGS
C GIVEN QA % B, THIS COMPUTES VARIOUS AVERAGES OF WA % WB OVER U
REAL NCJ,NSJ,NC(1000),NS(1000)
DIMENSION DATUM (5)
5 COMMON/DATA1/QA,B,U,WAA,WBA,WAZA,WBZA,WABA,WA,WB
COMMON/DATA2/LHAX1,COB(101),JNMAX,NC,NS,ALNLMX,RIJMAX
EQUIVALENCE (WAA,DATUM(1)),(IBUMAX,LHAX1)
C
10 DO 10 K=1,5
   DATUM(K)=0.
10 CONTINUE
DO 30 I=1,IBUMAX
   COSBUI=COSB(I)
   QU=QA*AMAX1(1.+B*COSBUI,0.)
15 SQRQU2=2.*SQRT(QU)
   DO 20 J=1,JNMAX
     NCJ=NC(J)
     NSJ=NS(J)
     U=QU+NCJ*SQRQU2+NCJ*NCJ+NSJ*NSJ
20 CALL WAWB
   WAA=WAA+WA
   WBA=WBA+WB
   WAZA=WAZA+WA*WA
   WBZA=WBZA+WB*WB
25 WABA=WABA+WA*WB
20 CONTINUE
30 CONTINUE
DO 40 K=1,5
   DATUM(K)=DATUM(K)*RIJMAX
30 CONTINUE
40 RETURN
END

```

41000B CM STORAGE USED .175 SECONDS

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APPENDIX B

EXPERIMENTAL SYSTEM DATA ACQUISITION

PDP-11/03 DRV 11 Parallel Line Unit signals which will be used:

Outputs:	OUT 00 through OUT 15*	Inputs:	IN 00 through IN 09*
	NEW DATA READY*		REQ A*
	DATA TRANSMITTED*		REQ B*
	CSR0*		

Signals which will be generated by the data acquisition hardware:

BIT 0 through BIT 9\*  
START CONVERT\*  
STATUS\*  
CLEAR CONTROLLER\*  
TO SCAN IN (DECODE 33)\*  
t<sub>S</sub> RECEIVED  
COMPARISON MATCH\*  
COUNTER ENABLE  
COUNTER DISABLE  
ID RECEIVED ≠ ID REQUESTED  
t<sub>S</sub> • TO SCAN IN  
ID RECEIVED = ID REQUESTED  
t<sub>S</sub> • TO SCAN IN  
S0 through S5\*

Signals which are expected from the BENDIX receiver:

t<sub>P</sub>\*                      Log Video(+)\* and Log Video(-)\*  
Elevation\*  
AZimuth\*

Signals which will be supplied from front panel switch: Basic Wide (BW)  
or Basic Narrow (BN)\*

Quick Overview of Normal Operation

After initialization, the hardware will ask the PDP 11/03 to select the

Note: \* indicates that the signal will be transmitted via the backplane  
of the VERO rack.

type of scan (Azimuth or Elevation), which should next be sampled. In response the PDP will read out the samples from the previously sampled scan which were stored in a semiconductor memory; then, the PDP will select the next type of scan to be sampled. This selection is referred to as "ID REQUESTED" (ID REQ).

Now, the hardware waits for the  $t_R$  signal from the BENDIX receiver which indicates the beginning of the next scan. (Note:  $t_R$  must come shortly after Bit 5 of the BARKER code (data Bits 1 through 5); however, scan function identification is associated with data bits 6 through 11. The current design assumes that Azimuth or Elevation scans are the only type being transmitted from the airport. If this is not the case design changes must be made. This problem will be discussed further in relation to the Function-ID logic.) After receipt of the  $t_R$  pulse, the hardware waits for either the Azimuth or the Elevation line from the BENDIX receiver to be raised. This is referred to as the "ID RECEIVED" (ID REC).

If the ID requested is unequal to the ID received, then the hardware waits until the desired scan is received. When the desired scan is received (ID requested = ID received), the hardware asks the PDP to tell it when to start sampling the TO scan: The PDP sends a 16-bit  $t_s$  word to the hardware. When a hardware timer operating at 3.84 MHz counts up to the  $t_s$  word, TO scan sampling commences. The  $t_s$  word measures time with respect to the  $t_R$  reference, but there are some delays which are involved which must be compensated for by adjusting the  $t_s$  word sent to the hardware. These adjustments will be discussed later.

The data samples have 10-bit resolution and are stored in a 256 x 12 semiconductor memory. After 33 samples are taken, the hardware asks the PDP to send a  $t_s$  word to tell it when to start FRO scan sampling. When the hardware timer counts up to this  $t_s$  word, FRO scan sampling commences. Then, 34 samples

are taken (the last one will be ignored when data are read out for processing).

Finally, the hardware returns to the state in which it asks the PDP to select the next type of scan to be sampled. The PDP reads out the 66 samples and sends out the next ID requested.

#### Detailed Description of the Data Acquisition Hardware

The detailed description will come in two parts. First, the hardware will be divided into functional units which will be described as separate entities. Second, a step-by-step description of the operation of the hardware will be given to show how the functional units interact by passing signals through the backplane of the VERO rack. The backplane wiring will be described after all of the functional units have been presented. The descriptions are most meaningful if they are read along with the logic diagrams of the hardware.

#### Functional Units

The hardware is divided into separate functional units, each of which has its own Vero Finger Board. These boards will be mounted in a Vero rack, and the backplane will provide the necessary interconnections from board-to-board and from the rack to the PDP 11/Ø3 computer. The functional units are:

- a. POWER SUPPLY
- b. OSCILLATOR (3.84 MHz Clock)
- c. A/D and Sample/Hold
- d. STATE CONTROLLER and FUNCTION ID LOGIC
- e. SCAN TIMER
- f. SAMPLE TIMER & BUFFER MEMORY

#### Power Supply (Figure B-1)

The power supply is a Datel Systems BPM 15/150-D5, which converts +5 volts to ±15 volts with COMMON. The supply has been mounted on a PC board with an aluminum plate for heat dissipation. Note: It is very important in a

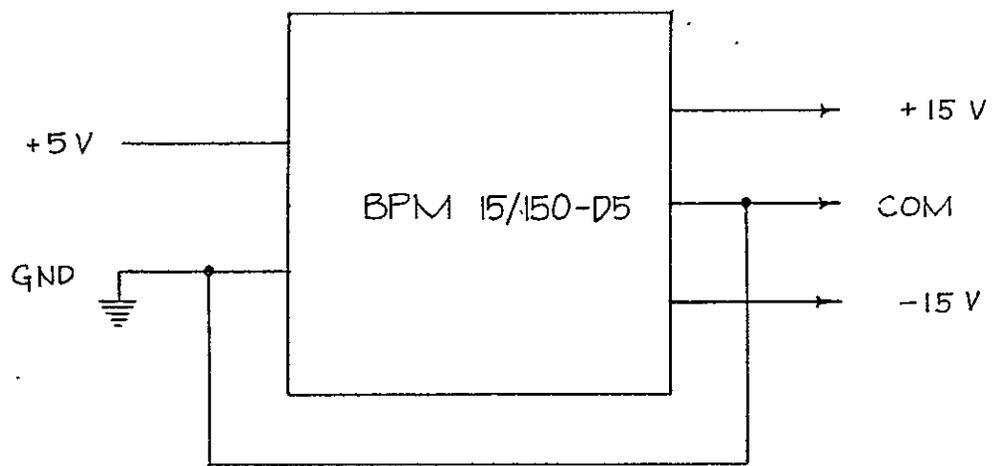


Figure B-1 Power Supply

system with both analog and digital signals present to maintain the correct distinction between analog and digital ground. However, these must ultimately be tied together -- preferably, as close to the power supply as possible. Therefore, GROUND and COMMON have been wired together on the power supply board. [Note: second thoughts suggest the two supplies should be tied together at the A/D Converter (see below); this will be considered further]

Inputs: +5 Volts, GROUND      Outputs: +15 Volts, -15 Volts, COMMON

#### Oscillator

The oscillator is a 3.84 MHz crystal oscillator which has been mounted on a special PC board which provides a ground plane underneath the entire unit.

Inputs: +5 Volts, GROUND      Outputs: CLOCK

#### A/D and Sample/Hold (Figure B-2)

This board will include an AD509J Op Amp and an ADC1109 Analog-to-Digital Converter, both by Analog Devices, plus an SHM-12 Sample and Hold by Datel. The op amp is used in the standard noninverting configuration, with high-frequency compensation, to provide a gain of four. This gain will boost the 0 - 2.5 Volts swing of the Log Video input to 0 - 10 Volts, which is the unipolar range of the A/D converter.

The board will operate as follows. The A/D converter will receive a START CONVERT command, via the backplane, from the SAMPLE TIMER & BUFFER MEMORY board. The converter will then raise its STATUS output signal, which will make the SHM-12 hold the current value of the Log Video input. Approximately four microseconds later, when the conversion is completed, the STATUS line will drop low. The 10 bits of digitized data are then valid. The negative-going edge of the STATUS signal will cause the 10 bits to be written into the buffer memory via the backplane. Note: While the schematic diagram for this board shows the

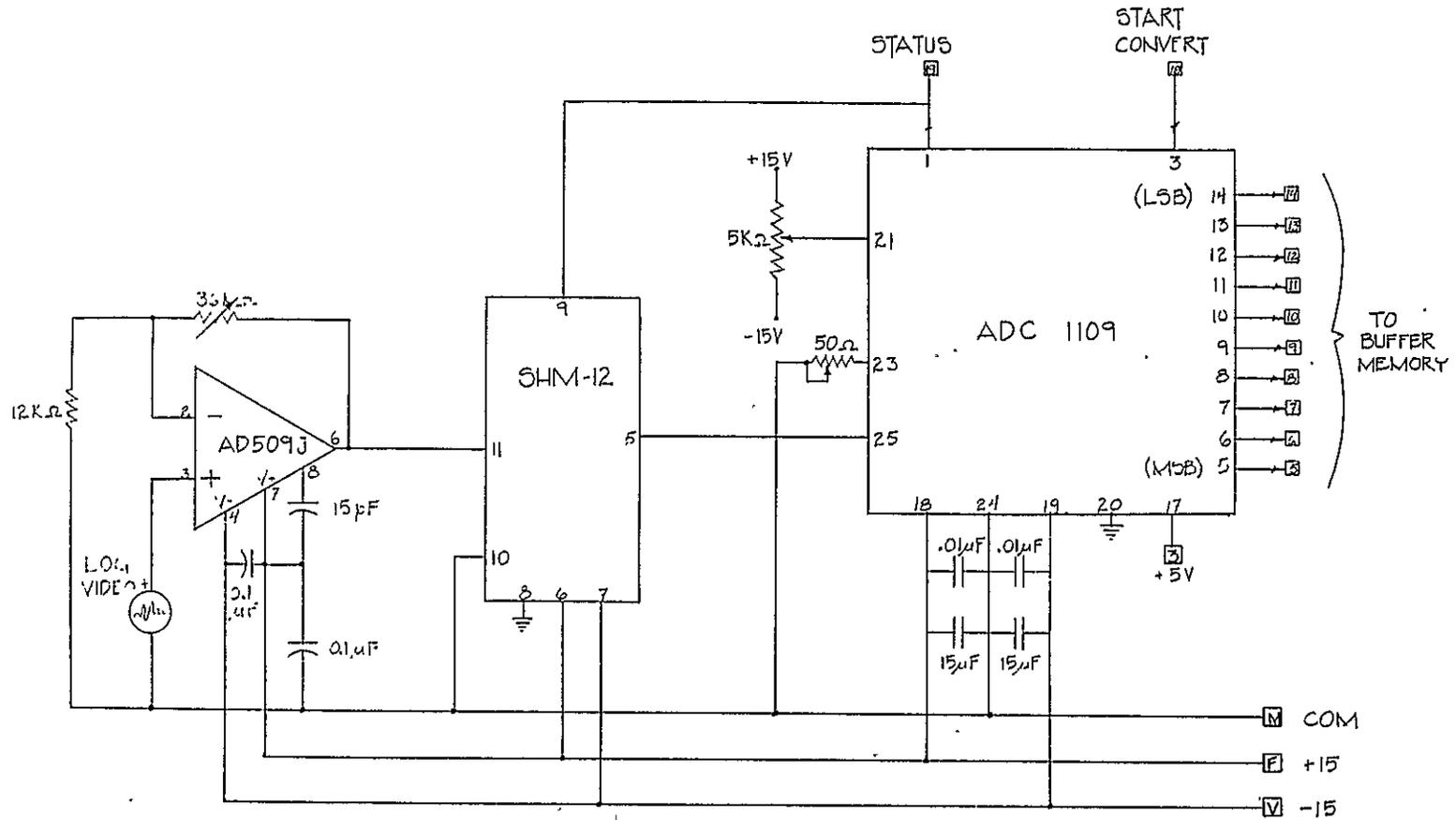


Figure B-2 A/D and Sample/Hold

ADC 1109 with trim pot adjustments for the zero adjust (Pin 21) and the gain adjust (Pin 23), these should be replaced ultimately with precision resistors. Also, it is assumed that Log Video will be brought to the backplane from the BENDIX receiver through a shielded cable.

Inputs: +5 Volts, GROUND, +15 Volts, -15 Volts, COMMON, START CONVERSION, Log Video(+), Log Video(-)

Outputs: STATUS, Bit 1(MSB) through Bit 10(LSB)

#### State Controller and Function ID Logic (Figures B-3 and B-4)

The state controller design is based on the control-state counter, presented in Section 5.11 of Thomas R. Blakeslee's book, Digital Design with Standard MSI and LSI. The controller consists of two 74151 data multiplexers, a 74193 presetable binary counter, and a 7442 demultiplexer. The inverters on the outputs of the demultiplexer are used for buffering and also establish positive logic; thus, when a line, such as S1, goes high, the controller is in State 1. The operation of the controller is discussed in Blakeslee's book and will not be described here. However, we may summarize its performance with the state diagram on the following page (Figure B-3).

The signals which cause the transitions from one state to another are produced at several different points in the data acquisition system:

<u>Signal</u>	<u>Origin</u>
CLEAR CONTROLLER	SAMPLE TIMER & BUFFER MEMORY LOGIC; the signal goes high at initialization when CSR $\emptyset$ is raised and, also, after FRO scan sampling.
NEW DATA READY	PDP 11/ $\emptyset$ 3 DRV 11; this signal is raised when the DRV 11 places data in its output buffer. The data in this case is a code indicating the type of scan which the computer wants to sample next.  BENDIX receiver.

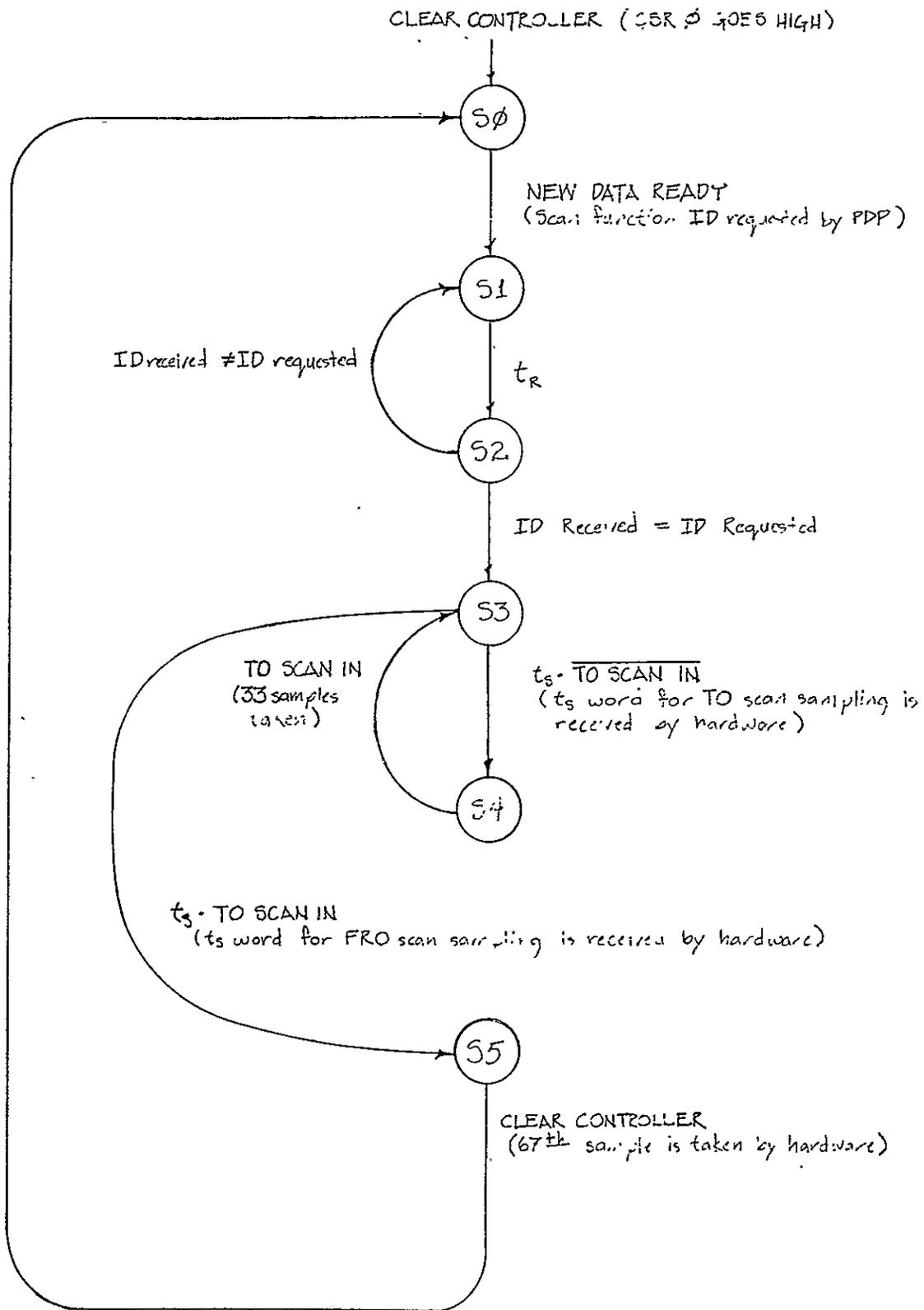


Figure B-3 State Diagram for State Controller

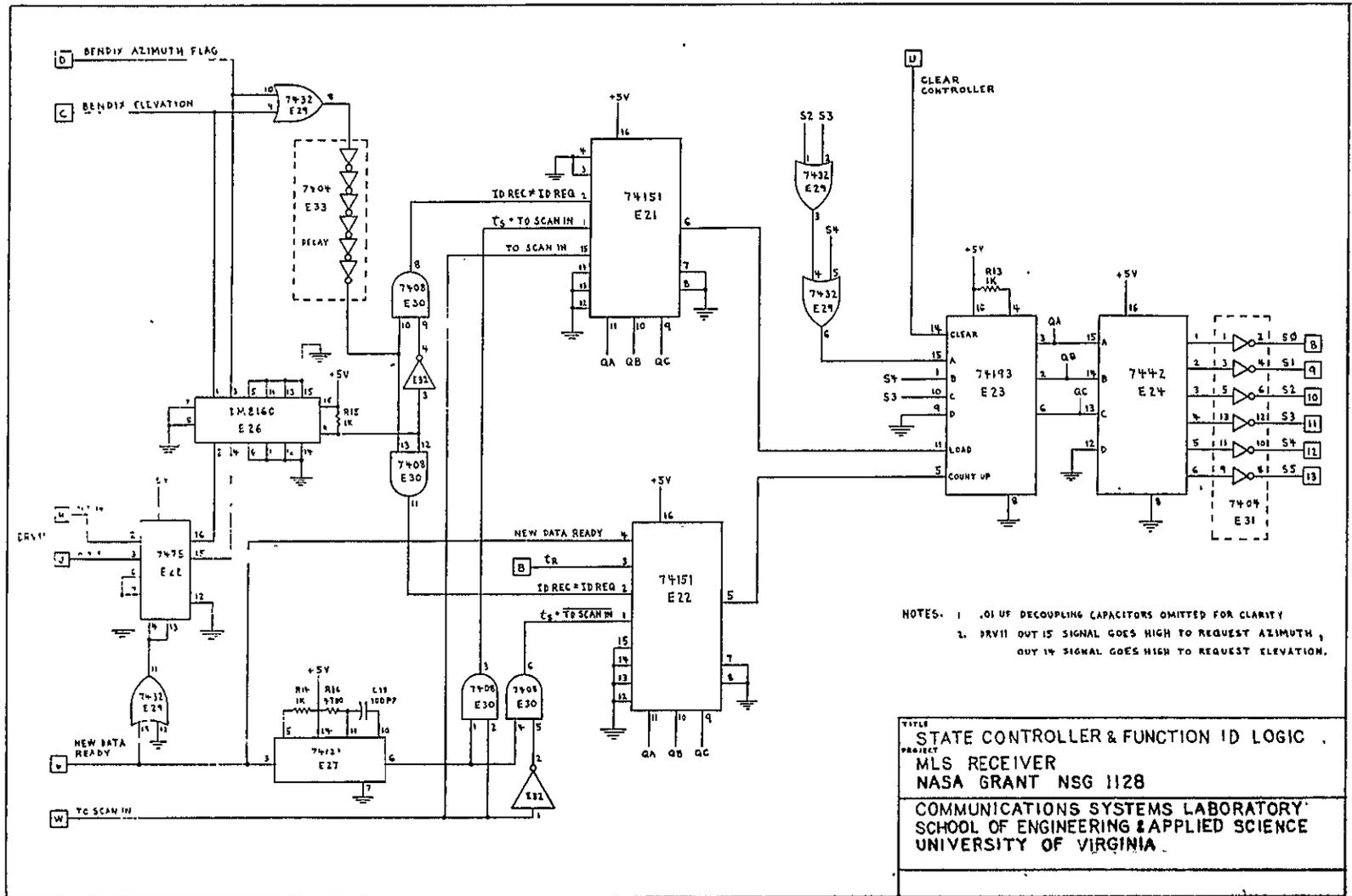


Figure B-4 State Controller and Function ID Logic

<u>Signal</u>	<u>Origin</u>
ID received = ID requested ID received $\neq$ ID requested	FUNCTION ID LOGIC; these signals are produced on the same board that contains the state controller. The Function ID logic is discussed below.
TO SCAN IN	SAMPLE TIMER & BUFFER MEMORY LOGIC; after 33 samples have been taken, this signal is raised to indicate that TO scan sampling is completed.
$t_S \cdot \overline{\text{TO SCAN IN}}$	STATE CONTROLLER & FUNCTION ID LOGIC; when the PDP sends out the <u>first</u> $t_S$ word, the NEW DATA READY signal is pulsed to indicate that data is in the DRV 11 output buffer. The <u>TO scan samples</u> have not yet been taken, so <u>TO SCAN IN</u> is true. We use the trailing edge of the NEW DATA READY signal to fire a <u>one-shot</u> , whose output is <u>logically ANDed</u> with <u>TO SCAN IN</u> to produce $t_S \cdot \text{TO SCAN IN}$ . By using the trailing edge, we insure that the data is stabilized in the output buffer before we accept it as valid.
$t_S \cdot \text{TO SCAN IN}$	Similar to above; however, when the PDP sends out the <u>second</u> $t_S$ word, <u>TO scan sampling has already been completed</u> and <u>TO SCAN IN</u> is true. Thus, <u>TO SCAN IN</u> and <u>TO SCAN IN</u> are used by the hardware to differentiate between TO and FRO scans.

#### Function ID Logic (Figure B-4)

As mentioned in the quick overview, the function ID logic, as currently designed, will work only if Azimuth and Elevation scans are the only scans being transmitted from the airport. The logic works as follows. When making an ID request, the computer will use signals OUT 15 and OUT 14 of the DRV 11. OUT 15 will be raised to request Azimuth; OUT 14 for Elevation. The NEW DATA READY pulse associated with this output will strobe the request into a 7475 buffer latch. Now, when the BENDIX receiver decodes the scan function ID, either the Azimuth flag or the Elevation flag will be raised. A DM8160 comparator will compare the ID received with the ID requested. It takes approximately 20 nsec for the comparator output to become valid. In order to prevent premature generation of invalid ID RECEIVED  $\neq$  ID REQUESTED or ID RECEIVED = ID

REQUESTED signals, the rising edge of either the Azimuth or Elevation flag is passed through a delay line and is used to gate the comparator output and its complement on to the state controller. Thus, both of the signals ID REQUESTED  $\neq$  ID RECEIVED and ID REQUESTED = ID RECEIVED remain low until the comparator output is valid, at which time only one of the signals goes high. This is necessary for the correct operation of the state controller (see Figure B-5).

If the airport were to broadcast more than just Azimuth and Elevation scans, the hardware as currently designed would not work. The BENDIX receiver would have to send out a  $t_R$  pulse at the beginning of each scan as it decodes the BARKER code; it has no way of knowing if the scan to follow is Azimuth, Elevation, or otherwise. Upon receipt of the  $t_R$  pulse, the state controller would enter STATE 2. Now, however, the controller would be stuck if neither the Azimuth nor Elevation flags were raised, as neither of the signals ID REC = ID REQ or ID REC  $\neq$  ID REQ would be enabled to take the controller to another state. There are two ways around this problem. One solution would be to have the Bendix receiver provide additional flag signals for the other scans and to expand on the current design using some of the extra inputs to the DM8160 comparator. The raising of any of the flag signals could be used to gate the comparator output on to the state controller. A second solution would be to obtain precise information about the delay between the output of the Bendix  $t_R$  pulse and the output of the Azimuth or Elevation flags. Since the  $t_R$  pulse starts a 3.84 MHz counter, logic could be designed around this counter to provide a pulse after this delay had elapsed. This pulse could be used to gate the comparator output on to the state controller.

Inputs: +5 Volts, GROUND, CLEAR CONTROLLER, TO SCAN IN, CLOCK  
BENDIX  $t_R$ , Azimuth, Elevation  
NEW DATA READY, OUT 14, OUT 15

Outputs:  $S\phi$ , S1, S2, S3, S4, S5

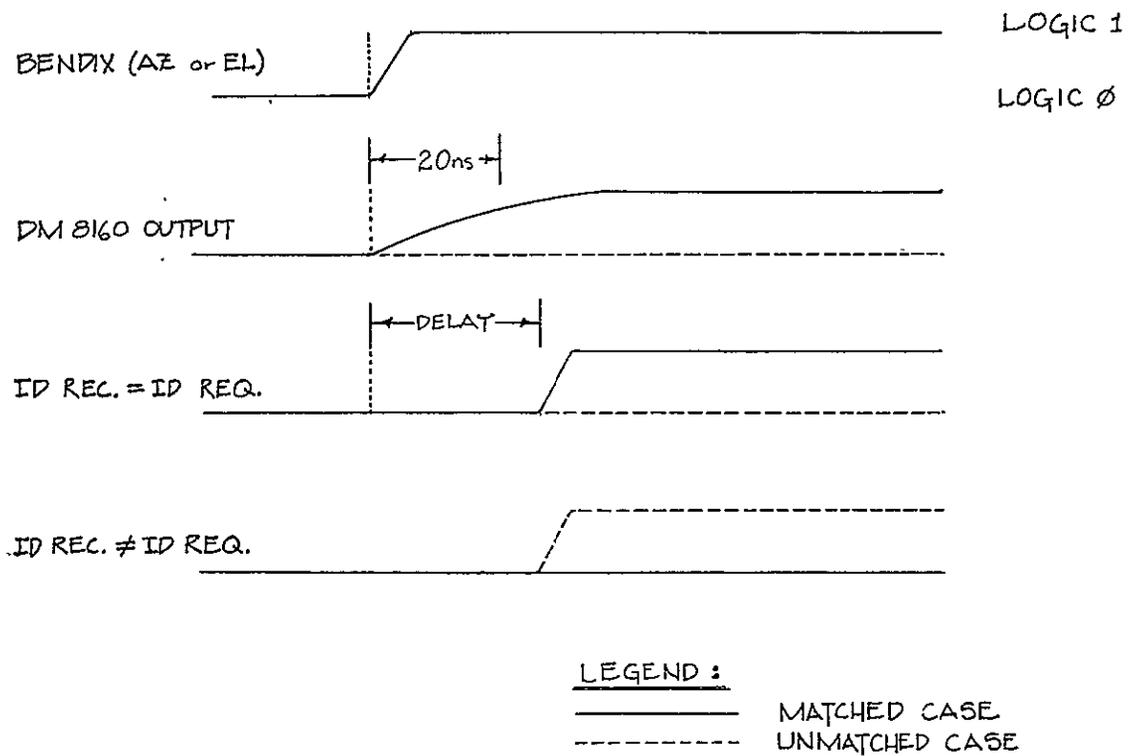


Figure B-5 Timing Diagram for Function ID Logic

### Scan Timer (Figure B-6)

The purpose of the scan timer is to initiate sampling of the TO and FRO scans at the times specified by the 16-bit  $t_s$  words sent from the PDP. The scan timer uses four 7475 four-input latches to hold the  $t_s$  word. Four 7493 binary counters are wired to provide a 16-bit binary counter. The combination of a DM8130 10-bit comparator and a DM 8160 6-bit comparator will be used for a 16-bit comparison between the latches and counters. Cross-coupled NOR gates are used to implement classic Set-Reset flip-flops. Two flip-flops are used and will be referred to as the clock flip-flop and the comparator flip-flop. The clock flip-flop controls the flow of the 3.84 MHz clock signal to the binary counter. The comparator flip-flop controls the passage to the backplane of the ANDed comparator outputs (referred to as COMPARISON MATCH).

The scan timer will operate as follows. When the state controller enters STATE 0, both flip-flops are reset. This will prevent the counter from being incremented and will disable the COMPARISON MATCH signal from reaching the backplane. When the controller enters STATE 1, the binary counter is cleared. Now, upon receipt of the BENDIX  $t_R$  pulse, the state controller enters STATE 2. This sets the clock flip-flop, and the binary counter begins counting at 3.84 MHz. If the ID received  $\neq$  ID requested signal is produced by the function ID logic, the controller re-enters STATE 1; and the counter is again cleared. It will remain cleared as long as the controller sits in STATE 1, even though the 3.84 MHz clock signal still flows to the counter input. On the other hand, if the ID received = ID requested signal is produced, then the controller enters STATE 3. Note that the  $t_s$  word has not yet been loaded into the latches; therefore, any matching between the counter and the latches cannot be valid. So STATE 3 is used to reset the comparator flip-flop, preventing the COMPARISON MATCH signal from being raised.



STATE 3 is used to signal an interrupt request (REQUEST B) to the PDP. In response, the PDP will output a 16-bit  $t_s$  word which indicates when TO scan sampling should start. As mentioned in the quick overview, this  $t_s$  word will measure time from the  $t_R$  pulse but must be corrected for a constant delay time which will be discussed in the next section. The NEW DATA READY signal associated with the output of the  $t_s$  word is used to strobe the 16 bits into the 7475 latches. The trailing edge of the NEW DATA READY signal is used to generate the  $t_s \cdot \overline{\text{TO SCAN IN}}$  signal which will make the controller enter STATE 4. At this point, the latches contain a valid  $t_s$  word; so STATE 4 is used to set the comparator flip-flop. Now, when the counter counts up to the  $t_s$  word, the comparator outputs go high. The comparator flip-flop is set; thus, the COMPARISON MATCH signal is raised. This signal is passed via the backplane to the SAMPLE TIMER & BUFFER MEMORY board and enables sampling to commence.

After 33 samples have been taken, the state controller re-enters STATE 3. The Request B line to the PDP is raised to request the FRO scan  $t_s$  word. Since the  $t_s$  word has not yet been received, STATE 3 resets the comparator flip-flop to prevent the COMPARISON MATCH signal from going high. When the  $t_s$  word is received, the  $t_s \cdot \overline{\text{TO SCAN IN}}$  signal will make the controller enter STATE 5. STATE 5 sets the comparator flip-flop to allow the COMPARISON MATCH signal to go high. Meanwhile, the counter continues to count at 3.84 MHz. When it counts up to the FRO scan  $t_s$  word, the comparator outputs again go high; and the COMPARISON MATCH signal is raised. This allows FRO scan sampling to commence. After the 67<sup>th</sup> sample is taken, the controller returns to STATE  $\emptyset$ .

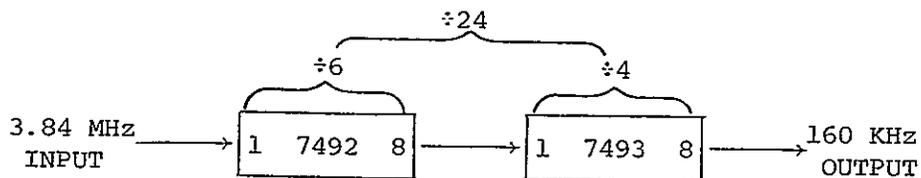
Inputs: +5 Volts, GROUND, OUT 00(LSB) through OUT 15(MSB), New Data Ready, CLOCK, S0 through S5

Output: COMPARISON MATCH

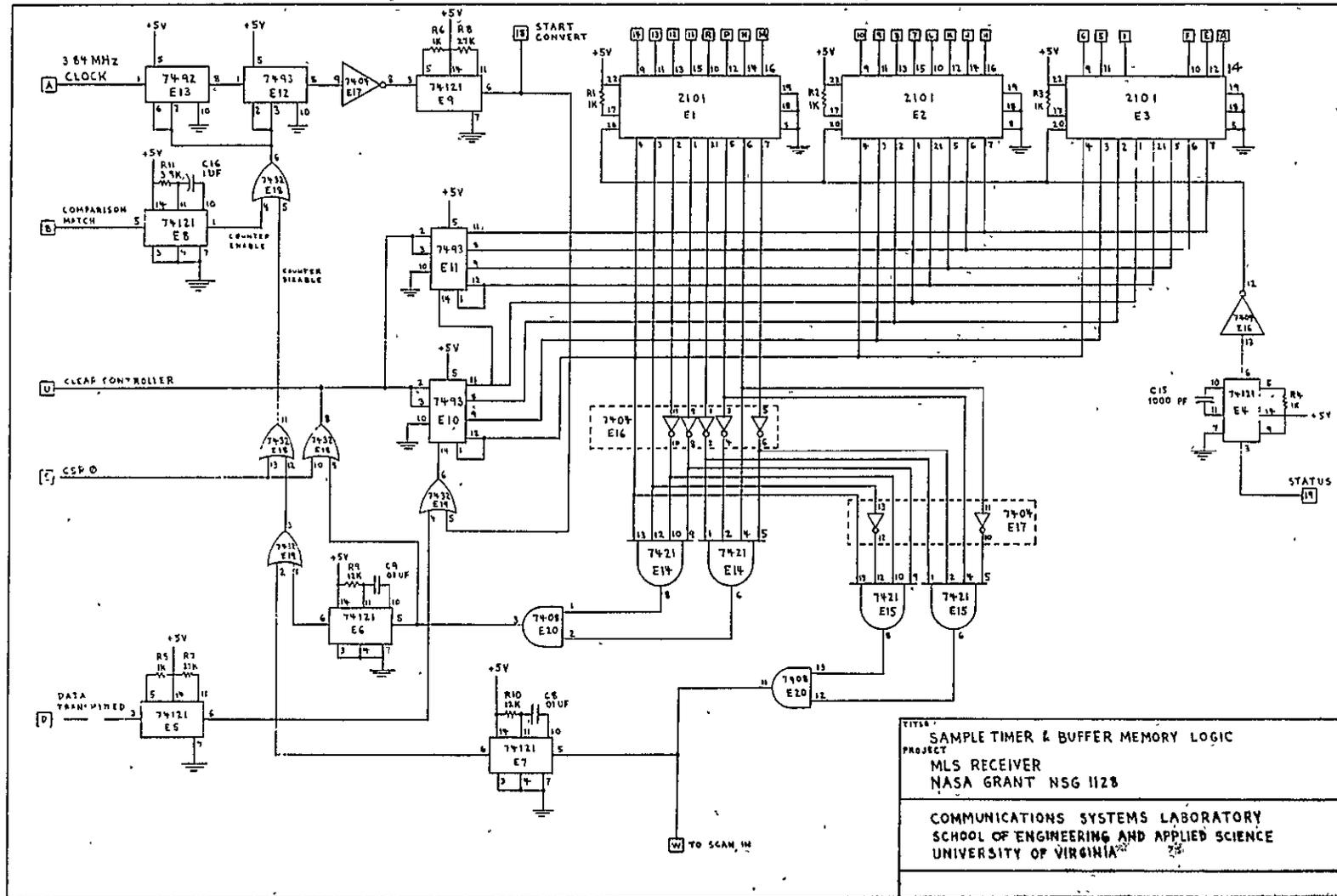
Sample Timer and Buffer Memory (Figure B-7)

The purpose of this board is to control the operation of the A/D and Sample/Hold board and to store the samples as they are taken so that they may be read back by the PDP 11/03. Three Intel 2101 256 x 4 Static MOS RAM's provide the memory storage. Although only 66 samples with 10-bit resolution need to be stored, space is at a premium on the VERO boards and the 2101's provide the necessary storage with only three 22-pin I.C. packages. The samples are taken at a rate of 160 KHz. This frequency is obtained from the 3.84 MHz clock by a divide-by-24 counter which consists of the series combination of a 7492 counter and a 7493 counter. The memory address logic for 2101 RAM's is provided by an 8-bit binary counter consisting of two 7493 counters. These will be referred to as the address counters. Additional logic is wired to the outputs of the address counters to provide signals which go high when the counters point to the 33<sup>rd</sup> and to the 67<sup>th</sup> locations in memory. This additional logic consists of two 7421 dual 4-input AND gates along with some inverters and 7408 AND gates.

NOTE: As was mentioned previously, the  $t_s$  words sent by the computer to the SCAN TIMER must be adjusted for a constant delay factor. This delay is due to two primary sources. One source of delay is the divide-by-24 counter.



A detailed analysis of the operation of this counter, based on its internal logic, yields the following result: the counter provides



TITLE: SAMPLE TIMER & BUFFER MEMORY LOGIC  
 PROJECT: MLS RECEIVER  
 NASA GRANT NSG 1128  
 COMMUNICATIONS SYSTEMS LABORATORY  
 SCHOOL OF ENGINEERING AND APPLIED SCIENCE  
 UNIVERSITY OF VIRGINIA

Figure B-7 Sample Timer and Buffer Memory

the proper frequency division, but the output is shifted in phase. The first output pulse comes at the end (trailing edge) of nine input pulses. At 3.84 MHz, this delay is approximately 2.34 microseconds.

A second source of delay will be the Bendix receiver. The receiver is to output the leading edge of its  $t_R$  pulse no later than 100 microseconds after reception of Bit 5 of the five-bit Barker code. The actual delay will have to be obtained from Bendix. Note that this delay will be compensated for partially or wholly by the delay in transmission of the Log Video envelope.

Other delays associated with gating and signal propagation are measured in nanoseconds and are insignificant when compared to the sources of delay above. Thus, the total delay may be expressed as:

$$\text{TOTAL DELAY} = (\text{COUNTER DELAY}) + (\text{BENDIX } t_R \text{ DELAY}) + (\text{BENDIX Log Video DELAY})$$

This total delay must be subtracted from the  $t_s$  words which are calculated by the computer before they are sent to the SCAN TIMER board.

The sample timer and buffer memory board will operate as follows. During the initialization following power-up, the computer will raise and then lower the  $\text{CSR}\emptyset$  signal of the DRV 11 Parallel Line Unit (DRCSR Bit  $\emptyset$ ). This pulsing of  $\text{CSR}\emptyset$  will do three things: (1) it will raise the CLEAR CONTROLLER signal, thus placing the state controller in STATE  $\emptyset$ ; (2) it will clear the divide-by-24 counter; (3) it will clear the address counter so that it points to memory location zero of the buffer memory.

Now, STATE 0 is the state in which the computer reads out the samples from the previously sampled scan. It does this by repeatedly reading the contents of the DRV 11 input buffer, DRINBUF. After each read operation, the DRV 11 automatically pulses the DATA TRANSMITTED signal. This signal will be used by the hardware to increment the address counter so that the next sample may be read. Thus, to read out the 66 samples the computer must do the following. First, it must read DRINBUF once and ignore this sample. This sample, stored in buffer memory location zero, is actually the 67<sup>th</sup> sample and that is why it is ignored. The 66 samples of interest are stored in Locations 1 through 66. So the computer now does 66 successive reads to obtain the 66 samples. The data is in the lower 10 bits of the 16-bit input buffer, with Bit 0 as the Least Significant Bit.

After the 66<sup>th</sup> sample has been read (67 read operations), the hardware automatically clears the address counters in preparation for the next set of samples to be taken. The hardware also raises the CLEAR CONTROLLER signal (this has no effect here since the controller is already in STATE 0) and fires a one-shot (the purpose of the one-shot will be explained later).

No more activity occurs on the board until the COMPARISON MATCH signal from the SCAN TIMER board is raised, signifying that sampling is to begin. The COMPARISON MATCH signal is fed into a one-shot (E8). The output of this one-shot, labeled COUNTER ENABLE, is normally high and is used to prevent the divide-by-24 counter from incrementing. When COMPARISON MATCH goes high, COUNTER ENABLE goes low for an interval somewhat longer than the time necessary to take 33 samples at 160 KHz. Thus, the divide-by-24 counter is allowed to start incrementing. Each output pulse of the counter fires a one-shot whose output is the START CONVERT signal. This signal causes the A/D and Sample/Hold board to take a sample and also increments the address counter so that it

addresses the location in the buffer memory where the sample will be stored. When the A/D conversion is completed; the STATUS line goes low. This transition fires a one-shot (E4) which provides a low-true write pulse for the buffer memory. The 10-bit digitized sample is thus written into the buffer memory at the address indicated by the address counters.

When the 33<sup>rd</sup> sample is taken, logic wired to the outputs of the address counters decodes the 33 and raises the TO SCAN IN signal. A one-shot (E7) is fired which raises the COUNTER DISABLE signal. This signal remains high for the duration of the TO scan and clears and disables the divide-by-24 counter, thus preventing any more samples from being taken during the scan. The raising of TO SCAN IN takes the state controller back to STATE 3.

The board is now inactive until the COMPARISON MATCH signal goes high, signifying that sampling for the FRO scan must begin. The COUNTER ENABLE signal goes low, and samples are taken and stored as before. However, during the FRO scan, 34 samples are taken, the last of which will be ignored. This is done so that the 66 samples of interest will be stored in consecutive memory locations, while still providing a self-clearing address counter. Thus, when the 67<sup>th</sup> sample is taken, logic wired to the outputs of the address counters decodes the 67 and clears the address counter so that the 67<sup>th</sup> sample gets written into memory location zero. A one-shot (E6) is fired whose output raises the COUNTER DISABLE line, thus preventing anymore samples from being taken during the FRO scan. The CLEAR CONTROLLER line is also raised, so the state controller is sent back to STATE  $\emptyset$ .

STATE  $\emptyset$  is used to signal the PDP 11/ $\emptyset$ 3 with an interrupt (Request A). The PDP responds by reading out 67 samples (ignoring the first) and then by sending out the code for the next type of scan to be sampled.

Note: The Basic Wide/Basic-Narrow option will be transmitted to the

buffer memory from a front panel switch. The option will be stored in memory along with the data samples and may be checked by looking at Bit 15 of the input buffer after any of the data samples have been read.

Inputs: +5 V; GROUND, Bit 0(LSB) through Bit 9(MSB), BW/BN, COMPARISON MATCH, CLOCK, STATUS CSR 0, DATA TRANSMITTED  
Outputs: START CONVERT, TO SCAN IN, CLEAR CONTROLLER, IN 00(LSB) through IN 09(MSB), IN 15

### Backplane Wiring

The table on the following page gives terminal pin assignments for each of the VERO FINGER BOARDS which will be used to implement the functional units described above (Figure B-8).

## II. Step-by-Step Operation

We may now summarize and clarify all of the previous discussion by giving a step-by-step description of the operation of the data acquisition hardware. The state transitions of the state controller will provide a convenient outline structure for the description.

### Power Up

During the initialization following power-up, the computer must pulse the CSR 0 signal. On the sample timer and buffer memory board this pulse will clear the divide-by-24 counter and the address counter and will also raise the CLEAR CONTROLLER signal. The CLEAR CONTROLLER signal is transmitted to the state controller and function ID logic board, where it places the state controller in STATE 0.

### State 0

The STATE 0 line is connected to the Request A line of the DRV 11; so

POWER SUPPLY		OSCILLATOR		A/D and Sample/Hold		State Controller & Function ID Logic		Scan Times		Sample Times & Buffer Memory	
1	+5 Volts	1	+5 Volts	1	+5 Volts	1	+5 Volts	1	+5 Volts	1	+5 Volts
2		2		2	Bit 7 (MSB)	2		2		2	Bit 7 (MSB)
3		3		3	Bit 6	3	NEW DATA READY	3	NEW DATA READY	3	Bit 6
4		4		4	Bit 5	4		4		4	Bit 5
5		5		5	Bit 4	5		5		5	Bit 4
6		6		6	Bit 3	6		6		6	Bit 3
7		7		7	Bit 2	7		7		7	Bit 2
8		8		8	Bit 1	8		8		8	Bit 1
9		9		9	Bit 0 (LSB)	9		9		9	Bit 0 (LSB)
10	GROUND	10	GROUND	10	GROUND	10	GROUND	10	GROUND	10	GROUND
11		11		11	START CONVERT	11		11		11	START CONVERT
12		12		12	STATUS	12		12		12	STATUS
13		13		13		13		13		13	
14		14		14		14		14		14	
15		15		15		15		15		15	
16		16		16		16		16		16	
17		17		17		17		17		17	
18		18		18		18		18		18	
19		19		19		19		19		19	
20		20		20		20		20		20	
21		21		21		21		21		21	
22		22		22		22		22		22	
23		23		23		23		23		23	
24		24		24		24		24		24	
25		25		25		25		25		25	
26		26		26		26		26		26	
27		27		27		27		27		27	
28		28		28		28		28		28	
29		29		29		29		29		29	
30		30		30		30		30		30	
31		31		31		31		31		31	
32		32		32		32		32		32	
33		33		33		33		33		33	
34		34		34		34		34		34	
35		35		35		35		35		35	
36		36		36		36		36		36	
37		37		37		37		37		37	
38		38		38		38		38		38	
39		39		39		39		39		39	
40		40		40		40		40		40	
41		41		41		41		41		41	
42		42		42		42		42		42	
43		43		43		43		43		43	
44		44		44		44		44		44	
45		45		45		45		45		45	
46		46		46		46		46		46	
47		47		47		47		47		47	
48		48		48		48		48		48	
49		49		49		49		49		49	
50		50		50		50		50		50	
51		51		51		51		51		51	
52		52		52		52		52		52	
53		53		53		53		53		53	
54		54		54		54		54		54	
55		55		55		55		55		55	
56		56		56		56		56		56	
57		57		57		57		57		57	
58		58		58		58		58		58	
59		59		59		59		59		59	
60		60		60		60		60		60	
61		61		61		61		61		61	
62		62		62		62		62		62	
63		63		63		63		63		63	
64		64		64		64		64		64	
65		65		65		65		65		65	
66		66		66		66		66		66	
67		67		67		67		67		67	
68		68		68		68		68		68	
69		69		69		69		69		69	
70		70		70		70		70		70	
71		71		71		71		71		71	
72		72		72		72		72		72	
73		73		73		73		73		73	
74		74		74		74		74		74	
75		75		75		75		75		75	
76		76		76		76		76		76	
77		77		77		77		77		77	
78		78		78		78		78		78	
79		79		79		79		79		79	
80		80		80		80		80		80	
81		81		81		81		81		81	
82		82		82		82		82		82	
83		83		83		83		83		83	
84		84		84		84		84		84	
85		85		85		85		85		85	
86		86		86		86		86		86	
87		87		87		87		87		87	
88		88		88		88		88		88	
89		89		89		89		89		89	
90		90		90		90		90		90	
91		91		91		91		91		91	
92		92		92		92		92		92	
93		93		93		93		93		93	
94		94		94		94		94		94	
95		95		95		95		95		95	
96		96		96		96		96		96	
97		97		97		97		97		97	
98		98		98		98		98		98	
99		99		99		99		99		99	
100		100		100		100		100		100	

Figure B-8 Terminal Pin Assignments

when STATE 0 occurs, an interrupt is generated. The STATE 0 signal also is transmitted to the scan timer board, where it resets the clock flip-flop and comparator flip-flop, thus preventing the COMPARISON MATCH signal from being raised.

#### Response to Interrupt Request A

The computer must respond to the Request A interrupt by reading its input buffer 67 times. The first read will be ignored and is used merely to increment the address counter so that it points to buffer memory location one, which holds the first sample. The DATA TRANSMITTED signal generated by each read operation is transmitted to the buffer memory to increment the address counter.

After reading in the samples, the computer will send out a code for the type of scan that it wants to have sampled. To request Azimuth the OUT 15 signal will be raised; to request Elevation the OUT 14 signal will be raised. The NEW DATA READY signal generated by this output will latch the ID requested on the STATE CONTROLLER & Function ID Logic board and will take the state controller to STATE 1.

#### State 1

The STATE 1 signal is transmitted to the scan timer board, where it clears a 16-bit binary counter which will operate at 3.84 MHz. Now, the controller waits until the Bendix receiver generates a  $t_R$  pulse. This pulse will take the controller to STATE 2.

#### State 2

The STATE 2 signal is transmitted to the scan timer board, where it sets the clock flip-flop. This makes the 16-bit binary counter begin to count at 3.84 MHz.

Meanwhile, the Bendix receiver will be decoding the function ID of the current scan. It will raise either the Azimuth or Elevation flag. The function ID logic, in turn, will generate either the signal "ID received  $\neq$  ID requested" or the signal "ID received = ID requested." If ID rec  $\neq$  ID req is generated, the state controller goes back to STATE 1, thus stopping and clearing the 16-bit counter. If ID rec = ID req is generated, the state controller goes to STATE 3.

### State 3

The STATE 3 line is connected to the Request B line of the DRV 11; so when STATE 3 occurs, an interrupt is generated. The STATE 3 signal is also transmitted to the scan timer board, where it resets the comparator flip-flip, thus preventing the COMPARISON MATCH signal from being raised.

### Response to Interrupt Request B

The computer must respond to the first Request B by sending out a 16-bit  $t_s$  word (with adjustments as noted before) which tells the hardware when to begin TO scan sampling. In response to the second Request B (STATE 3 is generated twice), the computer must send out a 16-bit  $t_s$  word which tells the hardware when to begin FRO scan sampling.

If the TO scan has not been sampled, then the TO SCAN IN signal from the sample timer board will be low. The state controller board will use the trailing edge of the NEW DATA READY signal associated with the first  $t_s$  word output to generate the signal  $t_s \cdot \overline{\text{TO SCAN IN}}$ ; this signal will take the controller to STATE 4.

On the other hand, if the TO scan has already been sampled, then the state controller board will generate the signal  $t_s \cdot \text{TO SCAN IN}$ ; this signal will take the controller to STATE 5.

#### State 4

The STATE 4 signal is transmitted to the scan timer board, where it sets the comparator flip-flop, thus allowing the COMPARISON MATCH signal to go high when the 16-bit counter counts up to the TO scan  $t_s$  word. When the COMPARISON MATCH signal is raised, sampling begins as described in Section I. After 33 samples have been taken, the TO SCAN IN signal from the sample timer board is raised. This signal takes the state controller back to STATE 3.

#### State 5

The STATE 5 signal is transmitted to the scan timer board, where it sets the comparator flip-flop, thus allowing the COMPARISON MATCH signal to go high when the 16-bit counter counts up to the FRO scan  $t_s$  word. When COMPARISON MATCH is raised, sampling begins as described in Section I. After 34 additional samples have been taken, the sample timer board raises the CLEAR CONTROLLER signal, which takes the state controller back to STATE  $\emptyset$ .

#### Test Program

The computer program used to test the completed data acquisition system is shown in Figure B-9.

DATA INTERFACE  
WITH CONTROLLER  
TEST  
S/C 17C

.MAIN. RT-11 MACRO VM02-12 PAGE 1

```

1      000000      -ASECT
2      167770 DRCSR =      167770
3      167772 OUTBUF =      167772
4      167774 INBUF =      167774
5      -MCALL      -REGDEF
6      000000      -REGDEF
7      001000      =      1000
8      001000 000005      RESET      ;INITIALIZE
9      001002 012706      MOV      #1000,SP
10     01006 012767      MOV      #1,DRCSR
11     01014 012767      MOV      #0,DRCSR
12     01022 032767 A:      BIT      #200,DRCSR      ;WAIT FOR REQ A
13     01030 001774      BEQ      A
14     01032 016700      MOV      INBUF,R0      ;BRING IN SAMPLES
15     01036 012700      MOV      #BUFFER,R0
16     01042 016720 B:      MOV      INBUF,(R0)+
17     01046 022700      CMP      #BUFEND,R0
18     01052 001373      BNE      B
19     01054 000000      HALT
20     01056 016767 C:      MOV      FUNC,OUTBUF      ;OUTPUT FUNCTION
21     01064 032767 D:      BIT      #100000,DRCSR      ;WAIT FOR REQ B
22     01072 001774      BEQ      D
23     01074 016767      MOV      TS1,OUTBUF      ;OUTPUT TS1
24     01102 032767 E:      BIT      #100000,DRCSR      ;WAIT FOR REQ B
25     01110 001774      BEQ      E
26     01112 016767      MOV      TS2,OUTBUF      ;OUTPUT TS2
27     01120 000740      BR      A      ;REPEAT
28     002000      =      2000
29     02000      BUFFER: -BLKW      1D66      ;DEFINE 66 WORD BLOCK
30     02204      BUFEND:
31     003000      =      3000
32     03000 000000      FUNC: -WORD      0      ;DEFINE PARAMETERS
33     03002 000000      TS1: -WORD      0
34     03004 000000      TS2: -WORD      0
35     000001      -END

```

$$TS1 = 4 \text{ msec} \approx 1544 \phi_{10} = 3612 \phi_{10}$$

$$TS3 = 11 \text{ msec} \approx 4246 \phi_{10} = 12273 \phi_{10}$$

SYMBOL TABLE

A	001022	B	001042	BUFEND	002204
BUFFER	002000	C	001056	D	001064
DRCSR =	167770	E	001102	FUNC	003000
INBUF =	167774	OUTBUF =	167772	PC	=1000007
R0	=1000000	R1	=1000001	R2	=1000002
R3	=1000003	R4	=1000004	R5	=1000005
SP	=1000006	TS1	003002	TS2	003004

.ABS. 003006 000  
000000 001  
ERRORS DETECTED: 0  
FREE CORE: 1707. WORDS  
MLSTES,MLSTES=MLSTES  
? \*EOF\*?  
\*

Figure B-9 Data Acquisition System Test Program

## APPENDIX C

### A 6D LOE OPTIMAL RECEIVER

In this design, a 6th component,  $\hat{\omega}_{sc}$ , is appended to the definition of  $\hat{\gamma}$ , requiring basically only two changes:

1. Appending a 6th row to matrix  $D(\hat{\gamma})$  so that instead of (2.103)

it now reads

$$D(\hat{\gamma}) = \begin{pmatrix} \text{--- } 2\hat{\alpha}p_j^2(\hat{\theta}) + 2\hat{\alpha}_R p_j(\hat{\theta})p_j(\hat{\theta}_R)\cos\hat{\beta}_j \text{ ---} \\ \text{--- } 2\hat{\alpha}^2 p_j(\hat{\theta})\dot{p}_j(\hat{\theta}) + 2\hat{\alpha}\hat{\alpha}_R \dot{p}_j(\hat{\theta})p_j(\hat{\theta}_R)\cos\hat{\beta}_j \text{ ---} \\ \text{--- } 2\hat{\alpha}p_j(\hat{\theta})p_j(\hat{\theta}_R)\cos\hat{\beta}_j + 2\hat{\alpha}_R p^2(\hat{\theta}_R) \text{ ---} \\ \text{--- } 2\hat{\alpha}\hat{\alpha}_R p_j(\hat{\theta})\dot{p}_j(\hat{\theta}_R)\cos\hat{\beta}_j + 2\hat{\alpha}_R^2 \dot{p}_j(\hat{\theta}_R)p_j(\hat{\theta}) \text{ ---} \\ \text{--- } (-2\hat{\alpha}\hat{\alpha}_R p_j(\hat{\theta})p_j(\hat{\theta}_R)\sin\hat{\beta}_j) \text{ ---} \\ \text{--- } (-2\hat{\alpha}\hat{\alpha}_R p_j(\hat{\theta})p_j(\hat{\theta}_R)\tau_j \sin\hat{\beta}_j) \text{ ---} \end{pmatrix} \quad (C-1)$$

where, as indicated in (3.10a), the quantity

$$\hat{\beta}_j = \hat{\beta} + \hat{\omega}_{sc} \tau_j \quad (C-2)$$

is one which has already been in use in the SD LOE (see PLOPT, Appendix A) (in spite of the assumption (2.90) used in the derivation of the LOE that all the  $\beta_j$  are equal); and

2. Changing the dimensions of all affected arrays in the programs.

Both changes affect module PLOPT, the latter additionally affects modules MLSSIM, OPTRVR and CTLACQN, the (interference acquisition) version of CONTRL which was selected for this study. Listings of the modified versions of these modules, CTLACQ6, MLSIM6, OPRVR6 and PLOPT6 follow below. Two options of this basic design were provided in the programs.

1.  $N_s = 8$ , and the state vector  $x$  is as defined for the Optimal design;
2.  $N_s = 9$ , and an additional component,  $\dot{\omega}_{sc}$ , is appended to the end of the state vector definition.

It was not possible to run any simulation studies involving the 6D LOE, the computing resources having practically been exhausted at this point (including the \$4700 University grant); as a debug exercise, however, the programs, by parameter inputs, were specialized to the prior SD LOE OPTRVR design and an earlier interference acquisition run with OPTRVR duplicated.

## SUBROUTINE CONTRL(ISW)

C  
 C THIS CONDUCTS THE MLS SIMULATION THROUGH A  
 C INTERFERENCE ACQUISITION SCENARIO,6D LOE  
 C

5

REAL LAMDA

INTEGER XNAME(2),YNAME(2),DATIN(4),DATOUT(4),DOUT  
 INTEGER YNAM1(2),YNAM2(2),YNAM3(2),YNAM4(2),YNAM5(2),FUNCTN(2)

INTEGER YNAM7(2),YNAM8(2),YNAM9(2),STITLE(9)

10

LOGICAL NOKLMN,NOLDE,NOAC,KALMAN,LOE,TETHRD,MORE,NFIRST,ADAPTV  
 LOGICAL FILOUT,FILEIN

COMMON/IDDATA/ISIM,IPMLS,IRCVR,IADAP,ITETHR,IPOPT

COMMON/RCVROO/THAMAX,THAMIN,TS,TR,OMEGA,TF

COMMON/RCVR01/NGMIN,NGMAX,DELBL,NGH,IR,IAE

15

COMMON/RCVR02/RHOMAX,DTHD,TDRD,BO,WSCD,NSQ(6),NGD(6)

COMMON/RCVR03/PI,FI(9),FL25(4),FSAMP,K,KM,TETHRD,NG,NS,JM

COMMON/RCVR04/DELT,EO(9),GQGT(9,9),H(6,9),ICOUNT,SIGMA

COMMON/RCVR05/NOLDE,NOKLMN,NOAC,GAMES(6),RDIAG(6),PMDIAG(9)

COMMON/RCVR06/PPDIAG(9),RMAT(6,6),PHI(6,6),PA(9,9),LAMDA(6)

20

COMMON/RCVR07/T(130),V(130)

COMMON/RCVR08/XSLOE(9),ESLOE(9),ES(9)

COMMON/RCVR09/BRCVR,BB,PDCRIT,CC

COMMON/RCVR10/XS1(9),XS(9)

COMMON/MLS000/ALFA,THE,THEDDT,ALFAR,THR,THROOT,B,WSC,WSCDOT

25

COMMON/MLS001/CSNRT,CSNRF,DSNRDB,RHO,BETA,FSC,LGMAX

COMMON/MLS002/DCSNR,CSNR,LG,TPKT,TPKF

COMMON/MLS003/FL10AE(4,2),FL10(4),DELTAT(2),XD(9,2),YD(4,2)

COMMON/MLS004/BHLS,BBB,HTIMES,MSET,MORE

DIMENSION IDNRS(6),IDASCI(24),IDENTS(6),RMSVAL(9)

30

DIMENSION EALFA(100),ETHET(100),EALFR(100),ETHER(100),XFOUR(100)

DIMENSION X(9), SCANNR(100)

DIMENSION EBETA(100),EFSC(100)

DIMENSION EFSCOT(100)

EQUIVALENCE (ALFA,X(1)),(ISIM,IDNRS(1)),(DOUT,DATOUT(2))

35

DATA ABDRT/1HA/,SPACE/1H/,NFIRST/.FALSE./,ADAPTV/.TRUE./

DATA DATIN/10HMLSSIMDATA,10H500000F000,2\*0/

DATA DATOUT/10HMLSSIMDATA,3\*0/

DATA IDASCI/7HCROSSHP,7HRMSE(T),7HRMSE(B),7HRMSE(F),7HACQSITN,

\*3\*7H ,7HGENERAL,8H PMLS1 ,8H PMLS2 ,

40

\*8H PMLS3 ,8H THRHL0 ,8H OPTIML ,8H SUBOPT ,8H -3 DB ,8HADAPTIV ,

\*8HNDNADAP ,8HUNTETHRD,8HTETHERED,2H ,8H POPT1 ,8H POPT2 ,

\*8H POPT3 /

DATA NSTART/3/,IRSIGN/1/,KSTART/26/,FILOUT/.FALSE./,

CFILEIN/.FALSE./

45

DATA FUNCTN/7HAZIMUTH,7HELEVAT./

DATA GQGT88/7.3/,GQGT99/1.E4/

DATA STITLE/6H ALFA ,6H THETA ,6H THEDDT ,6H ALFAR ,6H THETA ,

6H THROOT ,6H B ,6H WSC ,6H WSCDOT/

50

DATA XNAME/8H SCAN ,8H NUMBER /,YNAM2/8H ETHET ,8H DEGREES /

DATA YNAM1/8H EALFA ,8H /,YNAM3/8H EALFAR ,8H /

DATA YNAM4/8H ETHER ,8H DEGREES /,YNAM5/8H RHO ,8H /

DATA YNAM7/8HEABS BETA ,8H DEGREES /

DATA YNAM8/8HEABS FSC ,8H HERTZ /

55

DATA YNAM9/8HEABS FSCDOT ,8H HZ/SEC /

C

GO TO (100,200,300,400,500,600,700,800,900,1000,1100,1200),ISW

1

FORMAT(1H )

```

10  FORMAT(9(/))
11  FORMAT (1H1)
60  C
    C*****
    C
100 CONTINUE
    C THIS IDENTIFIES THE SCENARIO AND REINITIALIZES, AS NECESSARY,
65  C THE FOLLOWING RECEIVER PARAMETERS
    CSIGMA,IAE,DSNRDB,RHO,FSC,BETA,JH,BMLS
    IF(NFIRST) GO TO 155
    NOAC=.FALSE.
70  NFIRST=.TRUE.
    JBNAM=JOBNAME(1)
    ISIM=5
    IMOD=4
    WRITE (7,110)
110  FORMAT(34HIINTERFERENCE ACQUISITION SCENARIO/7H 6D LOE/)
75  IF (IRCVR.NE.1) GO TO 118
    WRITE (7,115)
115  FORMAT (35H THIS IS NOT FOR THRESHOLD RECEIVER)
    STOP * ABORTED--NOT FOR THDRVR*
118  CONTINUE
80  CALL LOGIO(6HFILEIN,FILEIN,0)
    IF(.NOT.FILEIN) NSTART=0
    IF(.NOT.FILEIN) GO TO 122
    IX=IATTACH(6LTAPE15,DATIN)
85  IF (IX.NE.0) CALL INTIO(6HIX(AT),IX,1,1)
    IF (IX.NE.0) STOP*INPUT FILE ATTACH NOT SATISFACTORY*
    WRITE(7,120) (DATIN(I),I=1,2)
120  FORMAT(29H THIS READS INPUT FILE ,2A10/)
122  CALL LOGIO(6HFILOUT,FILOUT,0)
    CALL INTIO(6HNSTART,NSTART,100,0)
90  NSTOP=NSTART
    CALL INTIO(6H NSTOP,NSTOP,100,0)
    CALL LOGIO(6HTETHRO,TETHRO,0)
    CALL LOGIO(6HADAPTV,ADAPTV,0)
95  IF(TETHRO) ITETHR=2
    IF(ADAPTV) GO TO 135
    IRSIGN=-1
    IADAP=3
135  CONTINUE
    DO 145 I=2,6
100  IASC=3*(I-1)+IDNRS(I)+6
    IDENTS(I)=IDASCI(IASC)
145  CONTINUE
    ENCODE(8,150,IDENTS(1)) IDASCI(ISIM),IMOD
150  FORMAT(A7,I1)
105  WRITE (7,152) IDNRS,IMOD
152  FORMAT (1H ,6I1,1X,I1/)
    WRITE (7,153) IDENTS
153  FORMAT (1H ,A8)
    CALL INTIO(6H IR,IR,6,0)
110  CALL REALIO (6HRHOMAX,RHOMAX,0)
    CALL REALIO(6H DTHO,DTHO,0)
    CALL REALIO(6H TORO,TORO,0)
    BETAD=BD*180./PI
    FSCD=WSCD*1./(2.*PI)

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NOTE * MULTIPLY BY 1 -- IGNORED
115 CALL REALIO(6H BETA0,BETA0,0)
CALL REALIO(6H FSCO,FSCO,0)
IF (IR.GE.5) CALL REALIO(6HGQGT08,GQGT08,0)
IF (IR.GE.6) CALL REALIO(6HGQGT99,GQGT99,0)
120 BQ=BETA0*PI/180.
WSCO=FSCO*2*PI
NRUN=NSTART-1
DSNRDB=20.
RHO=0.5
BETA=45.
125 FSC=0.
BMLS=1.
BRCVR=1.
THESEP=1.88
FSCDDT=X0(9,IAE)*.5/PI
130 155 CONTINUE
IF (FILEIN) GO TO 158
NRUN=NRUN+1
WRITE(7,11)
135 CALL INTIO(6H NRUN,NRUN,1,1)
CALL REALIO(6HDSNRDB,DSNRDB,0)
CALL REALIO(6H RHO,RHO,0)
CALL REALIO(6H BETA,BETA,0)
CALL REALIO(6H FSC,FSC,0)
140 IF (IR.EQ.6) CALL REALIO(6HFSCDDT,FSCDDT,0)
CALL REALIO(6H BMLS,BMLS,0)
CALL REALIO(6H BRCVR,BRCVR,0)
CALL REALIO(6HTHESEP,THESEP,0)
CALL INTIO(6HKSTART,KSTART,100,0)
GO TO 170
145 158 CONTINUE
READ(15,160) NRUN,DSNRDB,RHO,BETA,FSC,FSCDDT,BMLS,BRCVR,
THESEP,KSTART
IF (EOF(15)) 180,165
160 165 FORMAT (I5,8G10.3,I5)
IF (NRUN.LT.NSTART) GO TO 158
IF (NRUN.GE.NSTOP) MORE=.FALSE.
170 IF (NRUN.GE.NSTOP) MORE=.FALSE.
X0(3,IAE)=X0(6,IAE)=0.
X0(5,IAE)=X0(2,IAE)-THESEP
155 X0(9,IAE)=FSCDDT*(2.*PI)
EBETA0=ABS(BETA)-ABS(BETA0)
EFSCO=ABS(FSC)-ABS(FSCO)
RETURN
180 STOP*EOF REACHED ON INPUT FILE*
160 C
C*****
C
200 CONTINUE
C THIS OUTPUTS BASIC SIMULATION DATA OF INTEREST, SUCH AS
165 C THE ANGLE FUNCTION, INITIAL STATE, ETC.
WRITE(7,209)
209 FORMAT(5H1NRUN,4X,6HDSNRDB,7X,3HRHO,8X,4HBETA,8X,3HFSC,7X,6HFSCDDT
C,8X,4HBMLS,8X,5HBRCVR,6X,6HTHESEP,5X,6HKSTART)
WRITE(7,210) NRUN,DSNRDB,RHO,BETA,FSC,FSCDDT,BMLS,
170 CBRCVR,THESEP,KSTART

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210  FORMAT(1H0,I4,8(2X,G10.3),2X,I4)
      IF(.NOT.FILOUT) GO TO 245
      IF(NRUN.LE.9) ENCODE(10,220,DOUT) IONRS,1HU,IMOD,1HO,NRUN
175  220  FORMAT(6I1,A1,I1,A1,I1)
      IF(NRUN.GE.10) ENCODE(10,230,DOUT) IONRS,1HU,IMOD,NRUN
230  FORMAT(6I1,A1,I1,I2)
      IX=IREQST(6LTAPE17,3L*PF)
      IF(IX.NE.0) CALL INTIO(6HIX(RQ),IX,1,1)
      IF(IX.NE.0) STOP OUTPUT FILE REQUEST NOT SATISFACTORY#
180  WRITE(7,240) (DATOUT(I),I=1,2)
240  FORMAT(25H0THIS WRITES OUTPUT FILE ,2A10)
245  CALL DATE(TODAY)
      WRITE (7,250) FUNCTN (IAE),IAE
185  250  FORMAT (1H0,A7,15H FUNCTION (IAE=,I1,1H))
      X(4)=XD(4,IAE)=0.
      WRITE (7,260) ((I,X(I)),I=1,9)
260  FORMAT (15H0INITIAL STATE://(3H X(,I1,4H) = ,G13.6))
      WRITE(7,270) IDENTS(2)
270  FORMAT(1H0,A7)
190  RETURN
      C
      C*****
      C
300  CONTINUE
195  C THIS IDENTIFIES THE BASIC RECEIVER STRUCTURE (THRHD,OPT,SUBOPT)
      CAND REINITIALIZES, AS NECESSARY, THE FOLLOWING RCVR DATA
      CIR (NEGATE ONLY), NOAC,NOKLHN,NOLOE,BRCVR,DELBL,TETHRD
      IF(IR.GE.5) GQGT(8,8)=GQGT88
      IF(IR.GE.6) GQGT(9,9)=GQGT99
200  ITIT=HINO(IRCVR,2)
      C
      C NEGATE IR WITH THE FOLLOWING FOR NONADAPTIVE RECEIVER
      IR=ISIGN(IR,IRSIGN)
      C
205  RETURN
      C
      C*****
      C
400  CONTINUE
210  C THIS OUTPUTS BASIC RECEIVER DATA OF INTEREST
      WRITE(7,410) (IDENTS(I),I=3,4),IR,NG,NS
410  FORMAT (1H0,A8,4HRCVR/1H0,A8,6HDESIGN/5H (IR=,I2,4H,NG=,I1,
      * 4H,NS=,I1,1H))
      WRITE(7,420) (IDENTS(I),I=5,6)
215  420  FORMAT(1H0,A8/1H0,A7/)
      RETURN
      C
      C*****
      C
500  CONTINUE
220  C THIS SETS-UP THE MSET-LOOP
      RETURN
      C
      C*****
225  C
600  CONTINUE
      C THIS SETS-UP THE LG-LOOP FOR THE (MSET)-TH SERIES OF SETS

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      RETURN
230 C*****
      C
      700 CONTINUE
      C THIS SETS-UP THE K-LOOP FOR THE (LG)-TH SET OF KM SCANS
      CALL INTIO(6H KH,KM,1,1)
235 WRITE(7,710) (STITLE(I),I=1,9)
      710 FORMAT(4H0 K ,3X,6HCSNRTO,5X,6HCSNRF,3X,3HQTY,3X,9(2X,A6,3X)/)
      RETURN
      C
240 C*****
      C
      800 CONTINUE
      C THIS INITIALIZES THE K-TH SCAN
      IF(K.EQ.KSTART) X(4)=RHO*X(1)
245 IF(K.EQ.KSTART) NGM=NG
      RETURN
      C
      C*****
      C
      900 CONTINUE
250 C THIS SAVES/PREPROCESSES DATA FROM THE K-TH SCAN
      THERR=X(2)-XS(2)
      DTHE=X(2)-X(5)
      COLB=SQRT(PPDIAG(2))
      DO 910 I=1,NS
255 ES(I)=X(I)-XS(I)
      RMSVAL(I)=SQRT(PPDIAG(I))
      910 CONTINUE
      IF(NS.GE.7) ES(7) = ABS(X(7))-ABS(XS(7))
260 IF(NS.GE.8) ES(8) = ABS(X(8))-ABS(XS(8))
      IF(NS.GE.9) ES(9)=ABS(X(9))-ABS(XS(9))
      SCANNR(K)=K
      EALFA(K)=ES(1)
      ETHET(K)=ES(2)
      EALFR(K)=ES(4)
265 ETHER(K)=ES(5)
      XFOUR(K)=X(4)/X(1)
      IF(NS.GE.7) EBETA(K)=180.*ES(7)/PI
      IF(NS.GE.8) EFSC(K)=0.5*ES(8)/PI
      IF(NS.GE.9) EFSCDT(K)=0.5*ES(9)/PI
270 IF(NRUN.NE.NSTART.AND.K.NE.KM) RETURN
      WRITE(7,920) K, CSNR,CSNRF,1HX,(X(I),I=1,9)
      920 FORMAT(1H ,I3,2(1X,G10.3),8X,A1,1X,9(1X,G10.3))
      WRITE(7,930) 7H XS,(XS(I),I=1,NS)
      WRITE(7,930) 7H ERR,(ES(I),I=1,NS)
275 WRITE(7,930) 7HSQ(PII),(RHSVAL(I),I=1,NS)
      930 FORMAT(1H ,27X,A7,1X,9(1X,G10.3))
      WRITE(7,1)
      RETURN
      C
280 C*****
      C
      1000 CONTINUE
      C THIS SAVES/PROCESSES/OUTPUTS DATA FROM THE (LG)-TH SET OF KM SCANS
      WRITE(7,1060) (GQGT(I,I),I=1,NS)

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285      1060  FORMAT(10(/),18H ON THE LAST SCAN:,7X,9HGQGT(I,I),1X,9(1X,G10.3))
          YMIN=YMAX=0.
          WRITE (7,11)
          CALL INTIO (6H NRUN,NRUN,1,1)
          CALL PLOTR(SCANNR, EALFA,KH,XNAME,YNAM1,YMIN,YMAX,0)
290      CALL REALIO(6H YMIN,YMIN,1)
          CALL REALIO(6H YMAX,YMAX,1)
          YMIN=YMAX=0.
          WRITE (7,11)
          CALL INTIO (6H NRUN,NRUN,1,1)
295      CALL PLOTR(SCANNR, ETHET,KH,XNAME,YNAM2,YMIN,YMAX,0)
          CALL REALIO(6H YMIN,YMIN,1)
          CALL REALIO(6H YMAX,YMAX,1)
          YMIN=YMAX=0.
          WRITE (7,11)
          CALL INTIO (6H NRUN,NRUN,1,1)
300      CALL PLOTR(SCANNR, EALFR,KH,XNAME,YNAM3,YMIN,YMAX,0)
          CALL REALIO(6H YMIN,YMIN,1)
          CALL REALIO(6H YMAX,YMAX,1)
          YMIN=YMAX=0.
          WRITE (7,11)
          CALL INTIO (6H NRUN,NRUN,1,1)
305      CALL PLOTR(SCANNR, ETHER,KH,XNAME,YNAM4,YMIN,YMAX,0)
          CALL REALIO(6H YMIN,YMIN,1)
          CALL REALIO(6H YMAX,YMAX,1)
          YMIN=YMAX=0.
          WRITE (7,11)
          CALL INTIO (6H NRUN,NRUN,1,1)
310      CALL PLOTR(SCANNR, XFOUR,KH,XNAME,YNAM5,YMIN,YMAX,0)
          CALL REALIO(6H YMIN,YMIN,1)
          CALL REALIO(6H YMAX,YMAX,1)
          YMIN=YMAX=0.
          WRITE (7,11)
          CALL INTIO (6H NRUN,NRUN,1,1)
315      CALL PLOTR(SCANNR, EBETA,KH,XNAME,YNAM7,YMIN,YMAX,0)
          CALL REALIO(6H YMIN,YMIN,1)
          CALL REALIO(6H YMAX,YMAX,1)
          YMIN=YMAX=0.
          WRITE (7,11)
          CALL INTIO (6H NRUN,NRUN,1,1)
320      CALL PLOTR(SCANNR, EFSC,KH,XNAME,YNAM8,YMIN,YMAX,0)
          CALL REALIO(6H YMIN,YMIN,1)
          CALL REALIO(6H YMAX,YMAX,1)
          YMIN=YMAX=0.
          WRITE (7,11)
          CALL INTIO (6H NRUN,NRUN,1,1)
325      CALL PLOTR(SCANNR, EFSCDT,KH,XNAME,YNAM9,YMIN,YMAX,0)
          CALL REALIO(6H YMIN,YMIN,1)
          CALL REALIO(6H YMAX,YMAX,1)
          YMIN=YMAX=0.
          WRITE (7,11)
          CALL INTIO (6H NRUN,NRUN,1,1)
330      CALL PLOTR(SCANNR, EFSCDT,KH,XNAME,YNAM9,YMIN,YMAX,0)
          CALL REALIO(6H YMIN,YMIN,1)
          CALL REALIO(6H YMAX,YMAX,1)
          YMIN=YMAX=0.
          WRITE (7,11)
          CALL INTIO (6H NRUN,NRUN,1,1)
335      1065  CONTINUE
          IF(.NOT.FILOUT) RETURN
          WRITE(7,11)
          WRITE(7,1070) (DATOUT(I),I=1,2)
340      1070  FORMAT(13H OUTPUT FILE ,2A10,1H:))
          WRITE(7,1072) DOUT,DELT,MTIMES,LGMAX,KH,TODAY,JBNAM

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1072 FORMAT(1H ,A10,8X,G13.6,5X,3(3X,I3,10X),A10,8X,A10/)
WRITE(7,1074) IDENT5,KSTART
345 1074 FORMAT(1H ,6(1X,A8,9X),I3/)
WRITE(7,1076) NRUN,OSNRDB,RHO,BETA,FSC,FSCDOT,BMLS,BRCVR,THESEP
1076 FORMAT(1H ,I2,3X,8(3X,G12.6)/)
IKH=MINO(35,KH-9)
DO 1077 I=1,IKH
1077 WRITE(7,1078)EALFA(I),ETHET(I),EALFR(I),ETHER(I),XFOUR(I)
350 1078 FORMAT(1H ,5(G13.6,5X))
DO 1079 I=1,5
1079 WRITE(7,1080)
1080 FORMAT(1H,5(6X,1H.,11X))
KM3=KM-3
355 DO 1081 I=KM3,KM
1081 WRITE(7,1078)EALFA(I),ETHET(I),EALFR(I),ETHER(I),XFOUR(I)
WRITE(7,1083)RHOMAX,OTHO,TORD,BETA0,FSC0,EBETA0,EBETA(KM),EFSC0,
CEFSC(KM)
1083 FORMAT(1HC,9(G12.6,2X))
360 WRITE(17) DOUT,DELT,MTIMES,LGMAX,KM,TODAY,JBNAH
WRITE(17) IDENT5,KSTART
WRITE(17) NRUN,OSNRDB,RHO,BETA,FSC,FSCDOT,BMLS,BRCVR,THESEP
DO 1090 I=1,KH
365 1090 CONTINUE
WRITE(17) RHOMAX,OTHO,TORD,BETA0,FSC0,EBETA0,EBETA(KM),EFSC0,EFSC(
CKM)
REWIND 17
IX=IATTACH(6LTAPE20,DATOUT)
370 CALL RETURN(6LTAPE20)
IF(IX.NE.0) GO TO 1095
IX=ICATALD(6LTAPE17,DATOUT,2LPW,8RHIGHFILL,2LRP,365)
GO TO 1096
1095 IX=ICATALD(6LTAPE17,DATOUT,2LXR,8RHIGHFILL,2LRP,365)
375 1096 IF(IX.NE.0) CALL INTIO(6HIX(CA),IX,1,1)
IF(IX.NE.0) STOP OUTPUT FILE CATALOG NOT SATISFACTORY
CALL RETURN(6LTAPE17)
WRITE(7,1099) (DATOUT(I),I=1,2)
380 1099 FORMAT(13HOOUTPUT FILE ,2A10,33H IS WRITTEN, CATALOGED AND CLOSED)
RETURN
C
C*****
C
1100 CONTINUE
385 C THIS SAVES/PROCESSES/OUTPUTS DATA FROM THE (MSET)-TH SERIES OF
CLGMAX SETS OF KH SCANS
RETURN
C
C * * * * *
390 C
1200 CONTINUE
C THIS EFFECTS CLOSURE OF THE SIMULATION RUN
WRITE(7,11)
RETURN
395 C
C*****
C
END

```

C-19

ORIGINAL PAGE IS OF POOR QUALITY

45000B CM STORAGE USED 11.349 SECONDS

G-10

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PROGRAM MLSSIM(INPUT,OUTPUT,TAPE10=INPUT,TAPE12,TAPE15,
*TAPE7=OUTPUT,TAPE17,TAPE20)
REAL LAMDA
LOGICAL NOKLMN,NOLOE,NOAC,KALMAN,LOE,TETHRD,MORE
5..... COMMON /IOWATA/IONRS(6)
COMMON/RCVROO/THAMAX,THAMIN,TS,TR,DHEGA,TF
COMMON/RCVRO1/NGMIN,NGMAX,DELBL,NGM,IR,IAE
COMMON/RCVRO2/RHOMAX,DTRD,TDRO,BD,WSCD,NSD(6),NGD(6)
10..... COMMON/RCVRO3/P1,F(9,9),FL25(4),FSAMP,K,KH,TETHPD,NG,NS,JH
COMMON/RCVRO4/DELT,ED(9),GGGT(9,9),H(6,9),ICDUNT,SIGMA
COMMON/RCVRO5/NOLOE,NOKLMN,NOAC,GAMES(6),RDIAG(6),PMDIAG(9)
COMMON/RCVRO6/PPDIAG(9),RHAT(6,6),PHI(6,6),PA(9,9),LAMDA(6)
COMMON/RCVRO7/T(130),V(130)
15..... COMMON/RCVRO8/XSLDE(9),ESLDE(9),ES(9)
COMMON/RCVRO9/BRCVR,8B,PDCRIT,CC
COMMON/RCVR10/XSI(9),XS(9)
COMMON/MLS000/ALFA,THE,THEDOT,ALFAR,THR,THRDOT,B,WSC,WSCDOT
COMMON/MLS001/CSNRT,CSNRF,DSNRDB,RHD,BETA,FSC,LGMAX
20..... COMMON/MLS002/DCSNR,CSNR,LC,TPKT,TPKF
COMMON/MLS003/FL10AE(4,2),FL10(4),DELTAT(2),XD(9,2),YD(4,2)
COMMON/MLS004/8MLS,8BB,MTIMES,MSET,MORE
C
10..... CONTINUE
CALL MLSSUB
25..... IF(MORE) GO TO 10
STOP
END

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41000B.CH. STORAGE USED .....131 SECONDS.

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SUBROUTINE MLSSUB
PEAL LAMDA
LOGICAL NOKLMN, NOLDE, NOAC, KALMAN, LOE, TETHRD, MORE
COMMON/RCVROO/THAMAX, THAMIN, TS, TR, OMEGA, TF
5 COMMON/RCVRO1/NGMIN, NGMAX, DELBL, NGH, IR, IAE
COMMON/RCVRO2/RHDMAX, DTHG, TDRD, BO, WSCD, NSD(4), NGO(4)
COMMON/RCVRO3/PI, F(9,9), FL25(4), FSAHP, K, KM, TETHRD, NG, NS, JM
COMMON/RCVRO4/DELT, ED(9), GQGT(9,9), H(6,9), ICOUNT, SIGMA
10 COMMON/RCVRO5/NOLDE, NOKLMN, NOAC, GAMES(6), RDIAG(6), PHDIAG(9)
COMMON/RCVRO6/PPDIAG(9), RMAT(6,6), PHI(6,6), PA(9,9), LAMDA(6)
COMMON/RCVRO7/T(130), V(130)
COMMON/RCVRO8/XSLDE(9), ESLDE(9), ES(9)
COMMON/RCVRO9/BRCVR, BB, PDCRIT, CC
COMMON/RCVR10/XS1(9), XS(9)
15 COMMON/MLS000/ALFA, THE, THEDOT, ALFAR, THR, THROOT, B, WSC, WSCDOT
COMMON/MLS001/CSNRT, CSNRF, DSNRDB, RHD, BETA, FSC, LGMAX
COMMON/MLS002/DCSNR, CSNR, LG, TPKT, TPKF
COMMON/MLS003/FL10AE(4,2), FL10(4), DELTAT(2), XO(9,2), YO(4,2)
COMMON/MLS004/BMLS, BBB, MTIMES, MSET, MORE
20 C GENERAL SIMULATION: OPTIMIZATION OF MLS RECEIVERS FOR
C MULTIPATH ENVIRONMENTS
C DIMENSION X1(9), INDEX(2), Y(4), X(9)
C EQUIVALENCE (THAMAX, Y(1)), (ALFA, X(1))
C
25 C FOLG BEGINS EXECUTABLE STATEMENTS
C
C PI2=2.*PI
C SQ22=SQRT(.5)
C
30 C FOLG INITIALIZES THE DIAGONAL OF F(8,8)
C
C DO 10 I=1,9
C F(I,I)=1.
10 C CONTINUE
35 C CALL CONTRL(1)
C SSQ2=SIGMA*SQRT(2.)
C
C FOLLOWING COMPLETES INITIALIZATION AND COMPUTES SECONDARY
C PARAMETERS.
40 C
C DO 15 I=1,4
C FL10(I)=FL10AE(I,IAE)
15 C CONTINUE
C DO 20 I=1,4
C Y(I)=YO(I,IAE)
45 C CONTINUE
20 C OMEGA=(THAMAX-THAMIN)/TS
C SECPD=1./OMEGA
C TF=TS+TR-2.*THAMIN*SECPD
50 C
C FOLG ARE CONSTANT PARAMETERS USED BY P
C
C BBB=2.4/BMLS
C DUM=GAUSS(1.0)
55 C ALPHA=10.*(DSNRDB/20.)
C XO(1,IAE)=ALPHA
C ALPHAR=RHD*ALPHA

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```

        XG(4,IAE)=ALPHAR
        XU(7,IAE)=PI*BETA/180.
60      XU(8,IAE)=PI2*FSC
        TSAMP=1./FSAMP
        DELT=DELTAT(IAE)
        F(2,3)=DELT
        F(5,6)=DELT
65      F(7,8)=DELT
        F(7,9)=0.5*DELT**2
        F(8,9)=DELT
        JM1=JM+1
        JM2=JM/2
70      TWW2=0.5*TSAMP*(JM2+1)
        DO 30 I=1,9
        X(I)=XG(I,IAE)
        30      CONTINUE
        CALL CONTRL(2)
75      C
        C FOLG CALLS RECEIVER FOR INITIALIZATION
        C
        K=0
        CALL RCVR
80      C
        C FOLLOWING BEGINS SIMULATION PER SE, LGMAX RUNS OF KM SCANS EACH
        C
        CALL CONTRL(5)
        DO 77 MSET=1,MTIMES
85      MSET=MSET
        C
        CALL CONTRL(6)
        DO 1 LGG=1,LGMAX
        LG=LGG
90      CALL CONTRL(7)
        DO 2 KK=1,KH
        K=KK
        C
        CALL CONTRL(8)
95      IF (K.EQ. 1) GO TO 122
        C
        C FOLLOWING ADVANCES THE TRUE STATE AND SAVE PRIOR VALUE
        C
        DO 100 I=1,9
100     X1(I)=X(I)
        X(I)=0.
        CONTINUE
        DO 120 I=1,9
        DO 110 J=1,9
105     X(I)=X(I)+F(I,J)*X1(J)
        110     CONTINUE
        120     CONTINUE
        B=PVALUE(B,PI,0.)
        C
110     C FOLG SETS THES PRIOR TO COMPUTING SAMPLE TIMES
        THES=XG(2)+DELT*XG(3)
        IF(.NOT.TETHRD) GO TO 124
        CONTINUE
122     DO 123 I=1,9

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115..... XS1(I)=X(I)-ED(I)
      123 CONTINUE
      THES=XS1(2)
      124 CONTINUE
      C
120..... C FOLG BEGINS COMPUTATION OF SIGNALS AND RELATED QUANTITIES
      C FIRST, CALCULATION OF CONSTANTS ON THE PRESENT SCAN
      C
      AL2=ALFA**2
      AR2=ALFAR**2
125..... AA2=2.*ALFA*ALFAR
      TPST=(THES-THAMAX)*SECPD
      TPSF=TF+(THAMIN-THES)*SECPD
      TZT=TPST-TWW2
      TZF=TPSF+TWW2
130..... C FOLG COMPUTES FOR THIS KTH SCAN THE SIGNAL PEAK TIMES TPKT, TPKF AND
      C THE COMPOSITE SIGNAL-TO-NOISE RATIO CSNR(K)
      TPKT=(X(2)-THAMAX)*SECPD
      TPKF=TF+(THAMIN-X(2))*SECPD
      C
135..... C THAJ=THA(TPKT)=X(2), BY DEFINITION
      C PJ=PMLS(THA-THA(TPKT))=1.0, BY DEFINITION
      C AND SIMILARLY FOR TPKF
      C
      PRJ=PMLS(X(5)-X(2))
140..... BT=PVALUE(B+(WSC+0.5*WSCDOT*TPKT)*TPKT,PI,0.)
      BF=PVALUE(B+(WSC+0.5*WSCDOT*TPKT)*TPKT,PI,0.)
      QJT=AL2+AA2*PRJ*COS(BT)+AR2*(PRJ**2)
      QJF=AL2+AA2*PRJ*COS(BF)+AR2*(PRJ**2)
145..... CSNRT=SQRT(QJT)
      CSNRF=SQRT(QJF)
      CSNRMN=AMIN1(CSNRT,CSNRF)
      CSNRHX=AMAX1(CSNRT,CSNRF)
      CSNR=CSNRMN
      DCSNR=CSNRHX-CSNRMN.
150..... C
      C FOLG INITIATES A J-LOOP TO COMPUTE SAMPLE TIMES AND (LINEAR)
      C ENVELOPE SAMPLE VALUES
      C
      DO 130 J=1,JH2
155..... TINCR=J*TSAMP
      JFR=JM1-J
      INDEX (1)=J
      INDEX (2)=JFR
      C FOLG COMPUTES SAMPLE TIMES
160..... TJ=TZI+TINCR
      T(J)=TJ
      T(JFR)=TZF-TINCR
      THAJ=THA(TJ)
      PJ=PMLS(THA-THAJ)
165..... PRJ=PMLS(THR-THAJ)
      C FOLG COMPUTES ENVELOPE SAMPLES
      DO 127 I=1,2
      JVAL=INDEX(I)
      TJVAL=T(JVAL)
170..... XNC=SQ22*GAUSS(0.)
      XNS=SQ22*GAUSS(0.)

```

C-14

```

..... BLOCAL=PVALUE(B+(WSC+0.5*WSCDOT*TJVAL)*TJVAL,PI,0.)
..... QJ=AL2*(PJ**2)+AA2*PJ*PRJ*PCOS(BLOCAL)+AR2*(PRJ**2)
..... QJ=AMAX1(QJ,0.0)
175 ..... SORTQ2=2.*SORT(QJ)
..... UJ=QJ+SORTQ2*XNC+XNC**2+XNS**2
..... V(TJVAL)=SSQ2*SORT(UJ)
..... 127 CONTINUE
..... 130 CONTINUE
..... 180 C
..... C FOLLOWING COMPUTES RECEIVER RESPONSES
..... C CALL RCVR
..... 185 C
..... C FOLLOWING ASSIMILATES DATA FROM THIS SCAN FOR FUTURE EVALUATION
..... C CALL CONTRL(9)
..... Z CONTINUE
..... C
..... 190 C FOLLOWING ASSIMILATES DATA FROM THIS LG-TH SET OF SCANS
..... C CALL CONTRL(10)
..... C CONTINUE
..... 195 C FOLLOWING ASSIMILATES DATA FROM THIS MSET-TH SERIES OF LGMAX SETS OF KH SCANS
..... C CALL CONTRL(11)
..... 777 CONTINUE
..... C
..... 200 C FOLLOWING CLOSES THE SIMULATION RUN
..... C CALL CONTRL(12)
..... RETURN
..... END
..... 510008_CH_STORAGE USED .....1.465,SECONDS

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C-15

```

      FUNCTION THA(T)
      C
      C THIS COMPUTES THE ANTENNA SCAN ANGLE AT LOCAL SCAN TIME T.
      C THE PARAMETERS OF THE SCAN WAVEFORM, HENCE THE IDENTITY OF
      C THE ANGLE FUNCTION, ARE PASSED THROUGH COMMON AND ARE DEFINED
      C AS FOLLOWS:
      C TR=TIME BETWEEN TRAVERSAL OF ZERO DEGREES IN A TO-FRO SCAN
      C TS=DURATION OF THE TO SCAN
      C TF=DURATION OF THE TO SCAN+INTERSCAN REST INTERVAL
      C THAMAX=ANTENNA ANGLE AT BEGINNING OF TO SCAN
      C THAMIN=ANTENNA ANGLE AT END OF TO SCAN
      C OMEGA=ANTENNA ANGULAR SCAN RATE, DEG/SEC, DURING TO SCAN
      C
      COMMON/RCVROO/THAMAX,THAMIN,TS,TR,OMEGA,TF
      C
      C 15 T1=TS+TF
      C IF(T.GE.0.0) GO TO 50
      C THA=THAMAX
      C RETURN
      C 20 IF(T.GT.TS) GO TO 100
      C THA=THAMAX+OMEGA*T
      C RETURN
      C 100 IF(T.GE.TF) GO TO 200
      C THA=THAMIN
      C RETURN
      C 25 IF(T.GT.T1) GO TO 250
      C THA=THAMIN-OMEGA*(T-TF)
      C RETURN
      C 250 THA=THAMAX
      C RETURN
      C 30 END
      C
      41000B CM STORAGE USED .114 SECONDS

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```
SUBROUTINE DFLTR1(X,Y,C)
DIMENSION C(4)
S=X-C(3)*C(4)
Y=C(1)*S+C(2)*C(4)
C(4)=S
RETURN
END
```

41000B CM STORAGE USED .046 SECONDS

G-17

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BLOCK DATA MLS
REAL LAMDA
LOGICAL NOKLMN,NOLDE,NOAC,KALMAN,LOE,TETHRD,MORE
COMMON/IDDATA/IDNRS(6)
5. COMMON/RCVRO1/NGMIN,NGMAX,DELBL,NGH,IR,IAE
COMMON/RCVRO2/RHOMAX,DTHO,TORO,BO,WSCD,NSO(6),NGO(6)
COMMON/RCVRO3/PI,F(9,9),FL25(4),FSAMP,K,KH,TETHRD,NG,NS,JM
COMMON/RCVRO4/DELT,EO(9),GQGT(9,9),H(6,9),ICOUNT,SIGMA
10 COMMON/RCVRO5/NOLDE,NOKLMN,NOAC,GAMES(6),RDIAG(6),PMDIAG(9)
COMMON/RCVRO6/PPDIAG(9),RHAT(6,6),PHI(6,6),PA(9,9),LAMDA(6)
COMMON/RCVRO9/BRCVR,BB,PDCRIT,CC
COMMON/MLS001/CSNRT,CSNRF,DSNRDB,RHO,BETA,FSC,LGMAX
COMMON/MLS003/FL10AE(4,2),FL10(4),DELTAT(2),XD(9,2),YD(4,2)
COMMON/MLS004/BMLS,BBB,MTIMES,MSET,MORE
15. DATA PI/3.1415927/,F/81*0./,DSNRDB/20./,RHO/.5/
DATA DELTAT/.074074074/,024691358/,SIGMA/.7071/
DATA XD/0.,30.,35,0.,32.75,-.35,0.,0.,0.,
* 0.,10.,0.,0.,12.,-.9,0.,2.,0./
DATA YD/62.666667,-62.,6.233333E-3,6.6E-3,
20 *30.666667,0.,1.533333E-3,0.4E-3/
DATA FL10AE/.5,0.,-.5,0.,.25,0.,-.75,0./
DATA FL25/.34831,.34831,-.30336,0./
DATA JM/130/,TETHRD/.FALSE./,KM/100/,FSAMP/1.6E5/
DATA H/1.,6*0.,1.,12*0.,1.,6*0.,1.,12*0.,1.,12*0.,1./
25 DATA NSO/2,8,6,3,8,9/,NGO/2,5,4,2,6,6/
DATA DELBL/.01/,EO/9*0./
DATA GQGT/81*0./,PA/81*0./
DATA RHOMAX/.8/,DTHO/2.75/,TORO/0.0/,BO/0.0/,WSCD/0.0/
30 DATA NOLDE/.TRUE./,NOKLMN/.FALSE./,NOAC/.TRUE./
DATA IAE/1/,FSC/51.30/,BETA/-168.0/,LGMAX/1/
DATA BMLS/1.0/,BRCVR/1.0/,MTIMES/1/,MORE/.TRUE./
DATA IDNRS(5)/1/
END
41000B CH STORAGE USED . . . . .219 SECONDS . . . . .

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SUBROUTINE RCVR
REAL LAMDA,MJM2
LOGICAL NOKLMN,NOLOE,NOAC,KALMAN,LOE,TETHRD
COMMON/RCVRO0/THAMAX,THAMIN,TS,TR,OMEGA,TF
5 COMMON/RCVRO1/NGMIN,NGMAX,DELBL,NGM,IR,IAE
COMMON/RCVRO2/RHOMAX,DTHO,TDRO,BD,WSCD,NSO(6),NGO(6)
COMMON/RCVRO3/PI,F(9,9),FL25(4),FSAMP,K,KH,TETHRD,NG,NS,JM
COMMON/RCVRO4/DELT,ED(9),GQGT(9,9),H(6,9),ICOUNT,SIGMA
10 COMMON/RCVRO5/NOLOE,NOKLMN,NOAC,GAMES(6),ROIAG(6),PHDIAG(9)
COMMON/RCVRO6/PPDIAG(9),RMAT(6,6),PHI(6,6),PA(9,9),LAMDA(6)
COMMON/RCVRO7/T(130),V(130)
COMMON/RCVRO8/XSLOE(9),ESLDE(9),ES(9)
COMMON/RCVRO9/BRCVR,BB,PDCRIT,CC
COMMON/RCVR10/XS1(9),XS(9)
15 DIMENSION TPA1(9,9),PHT(9,6),TPA2(9,9),IVING(6)
DIMENSION RVNG(6),GAIN(9,6)
C
IF (K.GT. 0) GO TO 40
C FOLG IS INITIALIZATION
20 P12=2.*PI
SS2=.5/(SIGMA**2)
CALL PHILM
NS=NSO(IR)
NG=NGO(IR)
25 NCMIN=2
NGMAX=NGO(IR)
GQGT33=.01*DELT
GQGT(3,3)=GQGT33
GQGT(6,6)=GQGT33
30 GQGT(8,8)=.04/(DELT**2)
DO 20 I=1,NS
DO 10 J=1,NS
PA(I,J)=0.
10 CONTINUE
35 20 CONTINUE
CALL CONTRL(3)
BB=2.4/BRCVR
PDCRIT=PI*BB/8.
CC=PI*PDCRIT
40 IF(IR.GT.0) GO TO 30
NS=NSO(4)
NG=NGO(4)
30 CONTINUE
NGM=NGMIN
45 IF(NOAC) NGM=NG
KALMAN=.NOT. NOKLMN
LOE=.NOT. NOLOE
CALL CONTRL(4)
RETURN
50 40 CONTINUE
IF(K.GT.1) GO TO 50
C
C DIAGNOSTIC OUTPUT OF INPUT DATA FOR K=1 GOES HERE
C
55 50 GO TO 90
CONTINUE
C FOLG EXTRAPOLATES STATE ESTIMATE, AS REQ'D

```

C-19

C-4

```

      IF(1ETHRD) GO TO 80
      DO 70 I=1,NS
60      XS1(I)=0.
      DO 60 J=1,NS
      XS1(I)=XS1(I)+F(I,J)*XS(J)
      60      CONTINUE
      70      CONTINUE
85      80      CONTINUE
      90      CONTINUE
      C
      GQGT11=AMAX1(.25,.01*(XS1(1)**2))
      GQGT(1,1)=GQGT11
70      GQGT(4,4)=GQGT11
      C
      C FOLLOWING COMPUTES VECTORS Q(JM),HW(JM),LAMDA(NG),AND MATRICES DT(JM,
      C NG),PHI(NG,NS) ALSO SQUARED AMPLITUDE ENVELOPE VECTOR U(JM),AND
      C INDOVATION'S PROCESS VECTOR W(JM)
75      C
      CALL PHLM
      IF (NOLDE) GO TO 120
      C
      C FOLG COMPUTES RHAT=PHI-INVERSE AND THE LOE
80      CALL MATINV(RMAT,6,NG,IVNG,RVNG)
      DO 100 I=1,NG
      RDIAG (I)=RHAT (I,I)
      100      CONTINUE
      CALL MATMUL (6,NG,NG,6,NG,1,6,1,RMAT,LAMDA,GAMAES,1)
85      CALL MATMUL (6,NG,NS,6,NG,1,9,1,H,GAMAES,ESLOE,2)
      DO 110 I=1,NS
      XSLDE(I)=XS1(I)+ESLOE(I)
      IF (NOKLMN) XS(I)=XSLDE(I)
      110      CONTINUE
90      120      CONTINUE
      IF (NOKLHN) GO TO 170
      C
      C FOLLOWING EXTRAPOLATES STATE ESTIMATES,ERROR
      C COVARIANCE MATRIX PA(NS,NS)
95      C
      CALL MATMUL(9,NS,NS,9,NS,NS,9,9,PA,F,TPA1,3)
      CALL MATMUL(9,NS,NS,9,NS,NS,9,9,F,TPA1,PA,1)
      CALL MATSM(PA,PA,GQGT,1,9,9,9,NS,NS,9,NS,NS,0)
      DO 130 I=1,NS
      PMDIAG (I)=PA(I,I)
100      130      CONTINUE
      C
      C FOLLOWING COMPUTES MODIFIED-KALMAN GAIN MATRIX GAIN(NS,NG)
      C
105      CALL MATMUL(9,NS,NS,6,NG,NS,9,6,PA,H,PHT,3)
      CALL MATMUL(6,NG,NG,6,NG,NS,9,9,PHI,H,TPA1,1)
      CALL MATMUL(9,NG,NS,9,NS,NG,9,9,TPA1,PHT,TPA2,1)
      DO 140 I=1,NG
      TPA2(I,I)=TPA2(I,I)+1.
110      140      CONTINUE
      CALL MATINV(TPA2,9,NG,IVNG,RVNG)
      CALL MATMUL(9,NS,NG,9,NG,NG,9,6,PHT,TPA2,GAIN,1)
      C
      C FOLLOWING UPDATES STATE ESTIMATE

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```

115 CALL MATMUL (9,NS,NG,6,NG,1,9,1,GAIN,LAMDA,ES,1)
    CALL MATSM (XS,XS1,ES,1,9,1,9,NS,1,9,NS,1,0)
    C
    C FOLLOWING UPDATES STATE ESTIMATE ,ERROR COVARIANCE MATRIX
    C P(NS,NS)
120 C
    CALL MATMUL (9,NS,NG,9,NG,NS,9,9,GAIN,TPA1,TPA2,1)
    DO 150 I=1,NS
    TPA2(I,I)=TPA2(I,I)-1.
150 CONTINUE
125 CALL MATMUL (9,NS,NS,9,NS,NS,9,9,PA,TPA2,TPA1,3)
    CALL MATMUL (9,NS,NS,9,NS,NS,9,9,TPA2,TPA1,PA,1)
    CALL MATMUL (6,NG,NG,9,NS,NG,9,9,PHI,GAIN,TPA1,3)
    CALL MATMUL (9,NS,NG,9,NG,NS,9,9,GAIN,TPA1,TPA2,1)
    CALL MATSM (PA,PA,TPA2,1,9,9,9,NS,NS,9,NS,NS,0)
130 DO 160 I=1,NS
    PPOIAG (I)=PA(I,I)
160 CONTINUE
170 CONTINUE
135 XS(1)=ABS(XS(1))
    AN=(THAMAX+THAMIN)/2.
    XS(2)=SATU(XS(2)-AN,(THAMAX-THAMIN)/2.)+AN
    IF(NS.GE.3) XS(3)=SATU(XS(3),1.)
    IF(NS.GE.4) XS(4)=SATU(ABS(XS(4)),2*XS(1))
    HJM2=FLOAT(-(JM/2+1))
140 THWW2=HJM2*OMEGA/(2.+FSAMP)
    AMX=XS(2)+THWW2
    AMN=XS(2)-THWW2
    AN2=(AMX+AMN)/2.
    IF(NS.GE.5) XS(5)=SATU(XS(5)-AN2,(AMX-AMN)/2.)+AN2
    IF(NS.GE.6) XS(6)=SATU(XS(6),1.)
    IF(NS.GE.7) XS(7)=PVALUE(XS(7),PI,0.)
    IF(NG.EQ.5) XS(8)=PVALUE(XS(8),PI/DELT,0.)
    RSMAX=8000.
150 IF(NS.GE.9) XS(9)=SATU(XS(9),RSMAX)
    RETURN
    END

```

41000B CM STORAGE USED 1.412 SECONDS

BLOCKDATA ORVRID 73/172 TS

FTN 4.6+452

05/17/79 15.08.35

PAGE 1

BLOCK DATA ORVRID  
COMMON/IODATA/IDNRS(6)  
DATA IDNRS(4)/2/  
END

41000B CH STORAGE USED .012 SECONDS

C-22

## SUBROUTINE PHILM

C THIS OPTIMAL VERSION OF PHILM IS FOR ALL SCALLOPING RATES  
 C AND PROVIDES A CRUDE SEARCH-AND-ACQUISITION FUNCTION

5 C ACCESSED AS FOLLOWS:

C SEARCH MODE: NGH=NGMIN  
 C ACQUISITION MODE: NGMIN,LT,NGM,LT,NGMAX  
 C FULL TRACK MODE: NGH=NGMAX

10

C THIS\_NEEDS NGMIN.LE.NGH (.LE.NG) .LE.NGMAX.

15

C REAL LAMDA  
 C LOGICAL NOKLMN,NOLOE,NOAC,KALMAN,LOE,TETHRD  
 C COMMON/RCVRO1/NGMIN,NGMAX,DELBL,NGM,IR,IAE  
 C COMMON/RCVRO2/RHOMAX,DTHO,TDRD,BD,WSCO,NSO(6),NGO(6)  
 C COMMON/RCVRO3/PI,F(9,9),FL25(4),FSAMP,K,KM,TETHRD,NG,NS,JM  
 C COMMON/RCVRO4/DELT,EO(9),GGGT(9,9),H(6,9),ICOUNT,SIGMA  
 C COMMON/RCVRO5/NOLOE,NOKLMN,NOAC,GAMES(6),RDIAG(6),PHDIAG(9)  
 C COMMON/RCVRO6/PPDIAG(9),RMAT(6,6),PHI(6,6),PA(9,9),LAMDA(6)  
 C COMMON/RCVRO7/T(130),V(130)

20

C COMMON/RCVRO8/XSLOE(9),ESLOE(9),ES(9)  
 C COMMON/RCVRO9/BRCVR,BB,PDCRIT,CC  
 C COMMON/RCV10/ALFA,THES,THESDT,ALFAR,THRS,THRSDT,B,WSC,  
 C WSCDOT,XS(9)  
 C DIMENSION INDEX(2),DT(130,6),HW(130),W(130)

25

C FOLLOWING EFFECTS INITIALIZATION

30

C IF(K.GT.0) GO TO 10  
 C JM2=JM/2  
 C JM1=JM+1  
 C SS2=.5/(SIGMA\*\*2)  
 C RETURN  
 C 10 CONTINUE

35

C FOLLOWING PROGRAMS THE SEARCH

40

C IF (NGM.GT.NGMIN) GO TO 30.  
 C ALFAR=ALFA\*RHOMAX  
 C THRSDT=TDRD  
 C B=BD  
 C WSC=WSCO  
 C THRS=THES-DTHO

45

C FOLG TETHERS WSCDOT  
 C WSCDOT=0.  
 C 30 CONTINUE

50

C FOLLOWING COMPUTES CONSTANTS FOR PRESENT SCAN

55

C AL2=2.\*ALFA  
 C AL22=AL2\*ALFA  
 C AR2=2.\*ALFAR  
 C AR22=AR2\*ALFAR  
 C AA2=AL2\*ALFAR

C FOLLOWING\_INITIATES\_LOOP\_AND\_COMPUTES\_FUNCTIONS

```

C     FOR EACH J
C
60     DD 60 JI=1,JM2
        INDEX(1)=JI
        INDEX(2)=JM1-JI
        THAJ=THA(T(JI))
        THEE=THEE-THAJ
65     PJ=P(THEE)
        PDJ=PDOT(THEE)
        P2J=PJ**2
        THER=THRS-THAJ
        PRJ=P(THER)
70     PDRJ=PDOT(THER)
        PR2J=PRJ**2
        PPRJ=PJ*PRJ
        QNRJ=.5*AL22*P2J
        CRJ=QNRJ+.5*AR22*PR2J
75     DINET=AL2*P2J
        C1=AR2*PPRJ
        D2NET=AL22*PJ*PDJ
        C2=AA2*PDJ*PRJ
        D3J=AR2*PR2J
80     C3=AL2*PPRJ
        D4J=AR22*PDRJ*PRJ
        C4=AA2*PJ*PDRJ
        D5J=-AA2*PPPJ
C     FOLG COMPLETES CALCULATIONS FOR TD,FRO SCANS, RESP.
85     DD 50 I=1,2
        J=INDEX(I)
        TJ=T(J)
        BLOCAL=PVALUE(B+(WSC+0.5*WSCDOT*TJ)*TJ,3.1415927,DELBL)
90     SB=SIN(BLOCAL)
        CB=COS(BLOCAL)
        QJ=QNRJ
        QRJALL=QRJ-D5J*CB
        D1J=DINET
        D2J=D2NET
95     IF (NGM.LT.NGMAX) GO TO 40
        QJ=QRJALL
        D1J=D1J+C1*CB
        D2J=D2J+C2*CB
100    40     CONTINUE
        DT(J,1)=D1J
        DT(J,2)=D2J
        DT(J,3)=D3J+C3*CB
        DT(J,4)=D4J+C4*CB
105    DT(J,5)=DTJ5
C     FOLG IS FOR A 6D LOE DESIGN
        DT(J,6)=DTJ5*TJ
C     FOLLOWING COMPUTES VECTOR HW(JM),AND INNOVATIONS PROCESS VECTOR W(JM)
C
110    HW(J)=1./(1.+2.*QJ)
        UJ=V(J)
        UJ=SS2*(UJ**2)
        W(J)=(UJ/SQRT(1.+QJ*UJ))-1.
50     CONTINUE

```

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```

115 ..... 60 ... CONTINUE
      C
      C   FOLLOWING COMPUTES VECTOR LAMDA(NG) AND MATRICE PHI(NG,NG)
      C
..... 120 ..... 70
      DO 110 I=1,NG..
      LAMDA(I)=0.0
      DO 70 J=1,JM
      LAMDA(I)=LAMDA(I)+DT(J,I)*W(J)
..... 125 ..... 80
      CONTINUE
      DO 100 L=1,I
      PHILI=0.
      DO 80 J=1,JM
      PHILI=PHILI+HW(J)*DT(J,I)*DT(J,L)
      CONTINUE
      PHI(L,I)=PHILI
130 ..... 90
      PHI(I,L)=PHILI
      IF (NLOE) GO TO 90
      RMAT(L,I)=PHILI
      RMAT(I,L)=PHILI
..... 135 ..... 100
      CONTINUE
      CONTINUE
      RETURN
      END

```

410008 CM STORAGE USED      .823 SECONDS

```
BLOCK DATA PLOPID  
COMMON /IDDATA/IDNRS(6)  
COMMON/RCVRO1/NGMIN,NGMAX,DELBL,NGM,IR,IAE  
DATA IDNRS(3)/2/  
DATA IR/6/  
END
```

410008 CH STORAGE USED .019 SECONDS

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