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ANISOTROPY OF NICKEL-BASE
SUPERALLOY SINGLE CRYSTALS

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ANISOTROPY OF NICKEL-BASE
SUPERALLOY SINGLE CRYSTALS

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The influence of orientation on the tensile and stress rupture behavior of 52 Mar-M247 single crystals was studied. Tensile tests were performed at temperatures between 23° and 1093° C; stress rupture behavior was examined between 760° and 1038° C.

The mechanical behavior of the single crystals was rationalized on the basis of the Schmid factor contours for the operative slip systems and the lattice rotations which the crystals underwent during deformation. The tensile properties correlated well with the appropriate Schmid factor contours. The stress rupture lives at lower testing temperatures were greatly influenced by the lattice rotations required to produce cross slip.

A unified analysis was attained for the stress rupture life data generated for the Mar-M247 single crystals at 760° and 774° C under a stress of 724 MPa and the data reported for Mar-M200 single crystals tested at 760° C under a stress of 689 MPa. Based on this analysis, the stereographic triangle was divided into several regions which were rank ordered according to stress rupture life for this temperature regime. This plot indicates the highest lives near the $[\bar{1}11]$, high lives near the $[001]$, and low lives near the $[011]$. Crystals within about 25° of the $[001]$ exhibited significantly longer stress rupture lives when oriented closer to the $[001] - [011]$ boundary than to the $[001] - [\bar{1}11]$ boundary.

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INTRODUCTION

Single crystal superalloys have been identified as an attractive approach for increasing allowable gas turbine blade temperatures. Among the requirements for successful application of single crystal airfoils is a fundamental understanding of the anisotropy of single crystals. The orientation and temperature dependence of Mar-M200 (Table 1) single crystals has been studied (1).* At 760° and 871° C, the longest stress rupture lives were found to occur for crystals oriented near the [001] and $[\bar{1}11]$; the shortest lives were exhibited by specimens oriented near the [011]. At 982° C, the crystallographic orientations exerted much less influence on the stress rupture life. Mechanistic studies (2-4) revealed that during primary creep at 760° C $(a/2)\langle 112 \rangle$ dislocations were generated and then dissociated into $(a/6)\langle 112 \rangle$ and $(a/3)\langle 112 \rangle$ partials. These $(a/3)\langle 112 \rangle$ partial dislocations then controlled primary creep by shearing the γ' precipitates by a diffusion-assisted process. Second-stage creep begins only after sufficient strain hardening occurs because of the intersection of $\{111\}\langle 112 \rangle$ slip systems. Second-stage creep deformation is controlled by the shearing of the γ' by $(a/2)\langle 110 \rangle$ dislocation pairs. In contrast at 857° C, pairs of $(a/2)\langle 110 \rangle$ dislocations shear the γ' in both primary and second-stage creep.

The purpose of the present work was to attain an improved understanding of the orientation dependence of the mechanical properties of Mar-M247 single crystals. This study evaluates the tensile and stress rupture properties generated for Mar-M247 single crystals and provides a unified analysis of this stress rupture data and that reported for Mar-M200.

MATERIAL AND EXPERIMENTAL PROCEDURE

Fifty-two single crystals of Mar-M247 (Table 1) were solution treated at 1232° C for 2 hours, argon quenched, aged at 816° C for 24 hours to promote precipitation, and air cooled. Tensile and stress rupture specimens, 0.63 cm diameter by 3.5 cm gage length, were prepared.

The initial orientations of the specimens, as well as the final orientations of selected crystals after mechanical testing, were determined by the Laue back-reflection X-ray method. Tensile tests were performed at 23°, 649°, 760°, 871°, 982°,

* () references are listed at the end of the text.

and 1093° C according to ASTM E21. Stress rupture tests between 760° and 1038° C were performed according to ASTM E-139-70.

RESULTS AND DISCUSSION

The orientations and tensile properties of eighteen single crystals tested are summarized in Table 2. The tensile behavior was rationalized on the basis of Schmid's Law which states that:

$$\tau = \frac{P}{A} \cos \phi \cos \lambda$$

where τ is the critical resolved shear stress (CRSS), P/A is the yield strength, ϕ is the angle between the normal to the slip plane and the tensile axis, λ is the angle between the slip direction and the tensile axis, and $\cos \phi \cos \lambda$ is the Schmid factor.

The operative slip system for tensile testing up to 760° C is the (111)[$\bar{1}01$] slip system (2); the Schmid factor contours for this slip system are presented in Fig. 1. With the aid of this plot and the data in Table 2, the CRSS was determined to be essentially constant and equal to 400 MPa for Mar-M247 single crystals tested from 23° to 760° C. Because of this fact, the tensile data for 23°, 649°, and 760° C could be grouped together and examined to determine the influence of orientation on the tensile properties. The 0.02% yield strengths and percent elongations for Mar-M247 single crystals tested at these temperatures are presented as a function of initial orientation in Figs. 2(a) and (b), respectively. Comparison of these figures with the Schmid factor contours shown in Fig. 1 demonstrates that single crystals with high Schmid factors were favorably oriented for slip and therefore exhibit lower strengths and higher ductilities; those with low Schmid factors exhibited higher strengths and lower ductilities. At testing temperatures higher than 760° C, additional slip systems became operative and higher ductilities and lower strengths resulted.

Thirty-four Mar-M247 single crystals were stress rupture tested between 760° and 1038° C; the results are summarized in Table 3. Comparison of the stress rupture data in Table 3 with the data reported in Ref. 1 shows that Mar-M200 and Mar-M247 single crystals have similar stress rupture strengths. The stress rupture lives and crystallographic orientations

for selected Mar-M247 specimens tested at 774° and 982° C are presented in Figs. 3(a) and (b), respectively. These figures and Table 3 demonstrate that the effect of initial orientation is much more pronounced at lower temperatures. This decrease in the anisotropy of the stress rupture behavior with increasing temperature is attributed to the increase in the number of operative slip systems which occurs with increasing temperature (1,5). Consequently, this work was directed primarily at studying the stress rupture behavior at about 760° C, where the anisotropy is prominent. The data obtained for Mar-M247 single crystals stress rupture tested at 760° and 774° C under a stress of 724 MPa and the data reported (1) for Mar-M200 single crystals, tested at 760° C under a stress of 689 MPa, were considered in this analysis. The Mar-M200 stress rupture data is presented in Fig. 4. In contrast to the analysis of the tensile data, comparison of the stress rupture data with the Schmid factor contours did not reveal a simple relationship. The primary factor which influenced the stress rupture life was determined to be the amount of lattice rotation required to produce cross slip.

The mechanisms involved during stress rupture testing are somewhat more complex than those for tensile testing. The $\{111\}\langle 112 \rangle$ slip system rather than the $(111)[\bar{1}01]$ is operative during first-stage creep at 760° and 774° C (4). The Schmid factor contours for the most highly stressed $\{111\}\langle 112 \rangle$ slip systems are illustrated in Fig. 5. During plastic deformation, the single crystals rotate toward their slip direction. The rotations for the $\{111\}\langle 112 \rangle$ and $(111)[\bar{1}01]$ slip systems are shown in Figs. 6(a) and (b), respectively. The rotations determined by X-ray analysis for specimens stress rupture tested at 774° C are illustrated in Fig. 7. Clearly, the $\{111\}\langle 112 \rangle$ slip system is operative. The transition from first-stage to second-stage creep occurs only after sufficient intersecting slip strain hardens the material (2). Intersecting slip occurs for the $\{111\}\langle 112 \rangle$ slip system along the $[001]$ -Y and X- $[\bar{1}11]$ boundaries. Thus, second-stage creep cannot begin until the crystal has rotated to, or nearly to, one of these boundaries. During second-stage creep, the $(111)[\bar{1}01]$ slip system becomes operative (4). The smaller the rotation required to initiate cross slip, the sooner second-stage creep will begin, and the longer the stress rupture life will be because second-stage creep proceeds much more slowly than primary creep. Thus, specimens oriented along directions of high symmetry exhibited the longest stress rupture lives because they were initially oriented for cross slip. Crystals which required large rotations to become oriented for cross slip had the shortest stress rupture

lives. Crystals oriented such that small elongations caused them to rotate into intersecting slip orientations exhibited intermediate lives.

For example, crystal 157 in Fig. 7 had an approximate $[\bar{1}11]$ orientation and exhibited the longest stress rupture life of 1242 hours. This behavior is attributed to the cross slip and to the minimum in Schmid factor for both first and second-stage creep that occur for this orientation. A stress rupture life of 179 hours was exhibited by specimen 1 which was oriented near the $[001]$, as shown in Fig. 7. Although this crystal was oriented for multiple slip, it was not located in a low Schmid factor region, and a life significantly lower than that of the $[\bar{1}11]$ crystal resulted. Specimen 158 was oriented near the $[011]$ and had a life of 1 hour. As shown in Fig. 7, this crystal rotated through regions of high Schmid factor toward its slip direction during first-stage creep and failed before reaching the X- $[\bar{1}11]$ boundary. This crystal exhibited an extremely short life because it did not benefit from the strengthening effects of cross slip.

The Larson-Miller parameter plot shown in Fig. 8 presents stress rupture data for single crystals of Mar-M247 and Mar-M200. The values for Mar-M247 were generated in this study; those for Mar-M200 were computed from the data reported in the literature (1). A dashed line was constructed using the minimum values for the alloys at each stress level, and a second dashed line was constructed using the maximum values for the alloys at each stress level. The solid line displayed represents conventionally cast Mar-M200 (6) and is presented for comparison. The substantial increase in Larson-Miller parameter of an approximate $[\bar{1}11]$ orientation over that of an approximate $[001]$ orientation is clearly evident. This increase in Larson-Miller parameter represents an increase of almost an order of magnitude in the stress rupture life of the $[\bar{1}11]$ crystal over that for the $[001]$ crystal and demonstrates that the $[\bar{1}11]$ orientation provides the best creep-resistance and the longest stress rupture lives. It is also apparent from Fig. 8 that unfavorably oriented single crystals, such as those with an $[011]$ orientation, exhibit stress rupture lives which are shorter than the stress rupture lives of conventionally cast Mar-M200. At lower stress levels and higher testing temperatures, the dependency of orientation is not as pronounced because multiple slip occurs at more elevated temperatures for Mar-M200 (1,5).

Based on a consideration of the lattice rotations and the Schmid factors for the stress rupture life data of Mar-M247 single crystals tested at 760° and 774° C and the

data reported for Mar-M200 single crystals tested at 760° C, the standard stereographic triangle was divided into several regions which were rank ordered according to stress rupture life for this temperature regime. This plot shown in Fig. 9 indicates the highest lives near the $[\bar{1}11]$, high lives near the $[001]$, and low lives near the $[011]$. Crystals within about 25° of the $[001]$ exhibited longer stress rupture lives when oriented closer to the $[001]$ - $[011]$ boundary than to the $[001]$ - $[\bar{1}11]$ boundary because crystals closer to the $[001]$ - $[011]$ boundary do not have to rotate as far before reaching intersecting slip regions during first-stage creep. This latter finding has commercial significance; although the $[\bar{1}11]$ orientation may be the most creep-resistant, crystals oriented near the $[001]$ are utilized for most turbine blade applications because their low elastic modulus (1) provides improved thermal fatigue resistance. Thus, this plot should assist in establishing standards for commercially acceptable orientations.

CONCLUSIONS

1. During tensile testing between 23° and 760° C, single crystals with high Schmid factors were favorably oriented for slip and exhibited lower strengths and higher ductilities; those with low Schmid factors exhibited higher strengths and lower ductilities.
2. During stress rupture testing at about 760° C, crystals which required large rotations to become oriented for cross slip had the shortest lives; those which required little or no rotations had the longest lives.
3. Although crystals near the $[001]$ and $[\bar{1}11]$ were both favorably oriented for cross slip, the $[\bar{1}11]$ orientation provided much longer stress rupture lives because of lower Schmid factors.
4. Crystals oriented within about 25° of the $[001]$ exhibit longer stress rupture lives when oriented closer to the $[001]$ - $[011]$ boundary than to the $[001]$ - $[\bar{1}11]$ boundary for stress rupture testing at 760° and 774° C.

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Table 1. - Compositions of Selected Nickel-Base Superalloys (wt.%)

<u>Alloy</u>	<u>C</u>	<u>Cr</u>	<u>Co</u>	<u>Ti</u>	<u>Al</u>	<u>W</u>	<u>Zr</u>	<u>B</u>	<u>Fe</u>	<u>Mo</u>	<u>Ta</u>	<u>Hf</u>	<u>Ni</u>
Mar-M247	0.15	8.4	10.3	1.0	5.5	9.9	0.07	0.013	0.05	0.75	3.1	1.5	bal
Mar-M200	.15	9.0	10.0	2.0	5.0	12.5	.05	.015	1.5 max	----	----	----	bal

Table 2. - Tensile Testing of Mar-M247 Single Crystals

Spec. no.	Temp., °C	UTS, MPa	0.02% Y.S., MPa		0.2% Y.S., MPa		Elong., %	R.A., %	E, MPa	Orientation degrees from:	
			MPa	MPa	MPa	MPa				[001]	[011]
40	23	965	860	934	7	11	136	10	35		
49	23	951	836	904	11	14	140	7.5	38		
54	23	935	859	912	9	14	142	12.5	33		
55	649	848	788	806	13	15	130	18	27.5		
58	649	915	800	849	11	14	112	14	31		
60	649	1025	923	941	6	9	112	6.5	39		
64	760	1093	876	902	8	8	104	6.5	39.5		
76	760	969	829	863	9	5	185	35	26.5		
79	760	1054	855	867	8	10	111	12.5	34.5		
82	871	920	693	798	9	9	125	18	28.5		
119	871	885	718	812	6	10	131	25	20.5		
120	871	938	643	783	8	9	92	6	39.5		
121	982	586	400	440	16	23	83	23	25.5		
122	982	541	407	502	20	29	163	45	16.5		
124	982	603	342	432	20	21	178	42	28		
125	1093	310	216	259	16	37	67	21.5	30		
129	1093	274	158	208	17	51	85	13.5	31		
130	1093	281	---	---	28	37	---	44	21.5		

Table 3. - Stress Rupture Testing of Mar-M247 Single Crystals

Spec. no.	Temp., °C	Stress, MPa	Life, hr	Elong., %	R.A., %	Orientation degrees from:			
						[001]	[011]		
35	760	724	131	13	8	4.5	41.5		
161	760	724	231	15	16	5	40		
143	760	689	1005+	3	--	45.5	31.5		
1	774	724	179	16	15	3	42		
72	↓	↓	26	9	12	7	38.5		
74			21	11	13	10	36		
123			37	12	15	8	37.5		
128			20	8	12	28	17		
147			138	8	15	45	28		
157			1242	11	12	52.5	34.5		
158			1	24	28	39	7		
23			816	448	1889	30	31	5	41
20			843	379	2005	6	7	41.5	27.5
24			843	345	2183	32	41	9	39
19	871	310	561	15	33	35	16.5		
28	↓	↓	229	30	37	18	29.5		
37			377	30	43	6	39		
71			247	28	30	4	42.5		
132			414	28	42	5	40		
152			414	8	13	34	30		
162			414	12	14	50.5	25.5		
135			448	8	10	31	23		
17			982	172	256	43	55	24.5	21
6			↓	↓	70	36	60	10	35.5
27					99	34	56	7.5	39
53	91	33			59	4	41.5		
133	190	33			40	32	28		
156	83	22			36	40	6.5		
136	221	26			33	30	24.5		
163	221	56			36	57	6	42.5	
2	1010	138			192	21	34	19	29.5
25	1010	172			68	31	36	38	14
16	1038	138			82	36	62	10	37.5

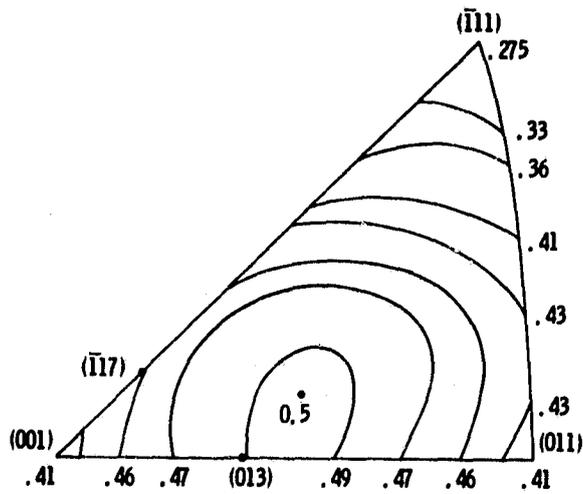


Figure 1. - Schmid factor contours for the (111) $[101]$ slip system (1).

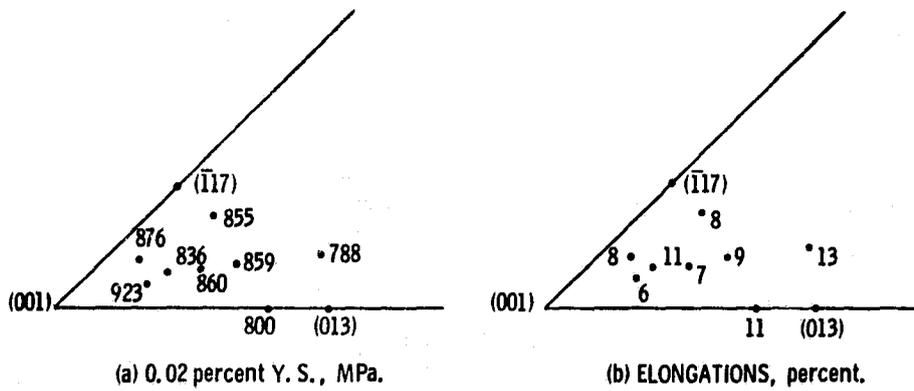


Figure 2. - Stereographic triangles showing yield strength and elongation of Mar-M247 single crystals tensile tested at 23° , 649° , and 760° C.

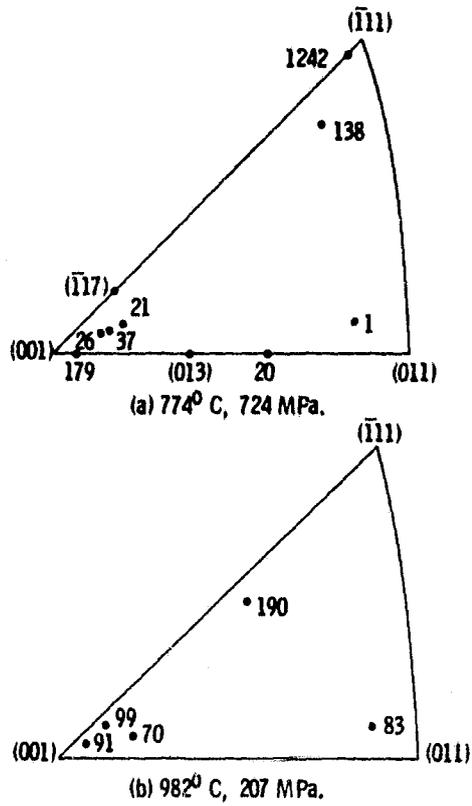


Figure 3. - Stress rupture lives as a function of orientation for Mar-M247 single crystals.

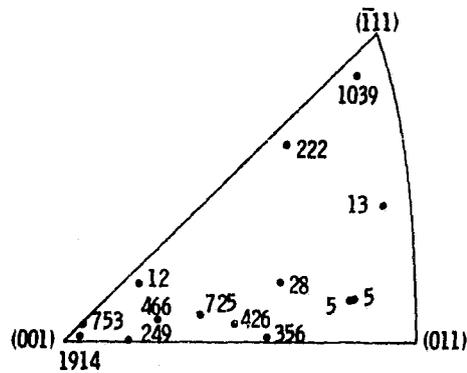


Figure 4. - Stress rupture lives as a function of orientation for Mar-M200 single crystals at 760°C and 689 MPa (1).

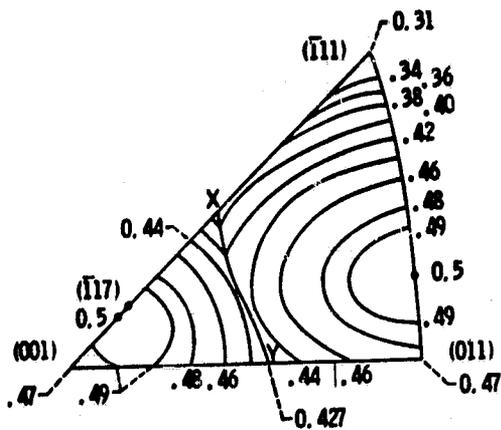


Figure 5. - Schmid factor contours for the most highly stressed $\{111\} \langle 112 \rangle$ slip system (2).

.49

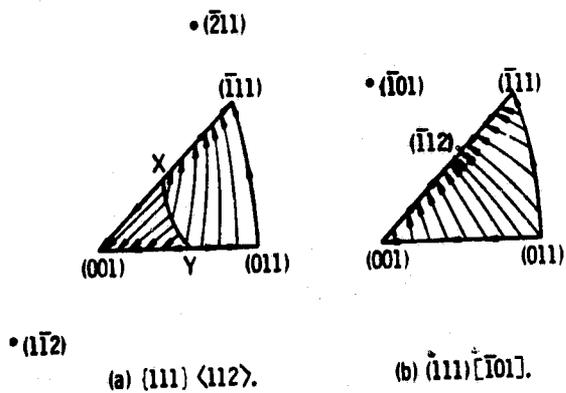


Figure 6. - Rotations of crystals under slip.

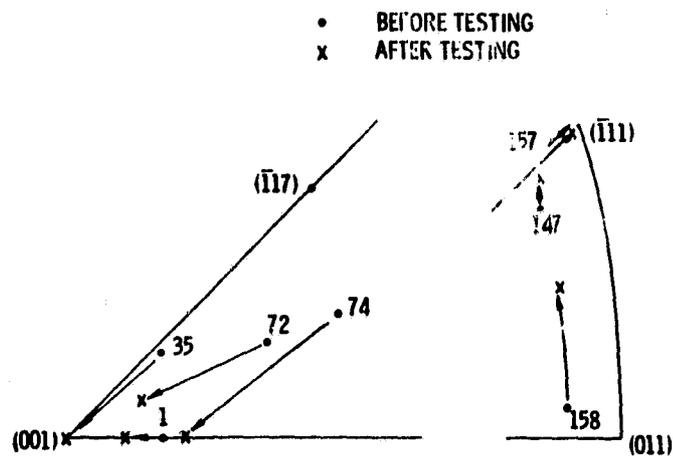


Figure 7. - Selected rotations of Mar-M247 single crystals.

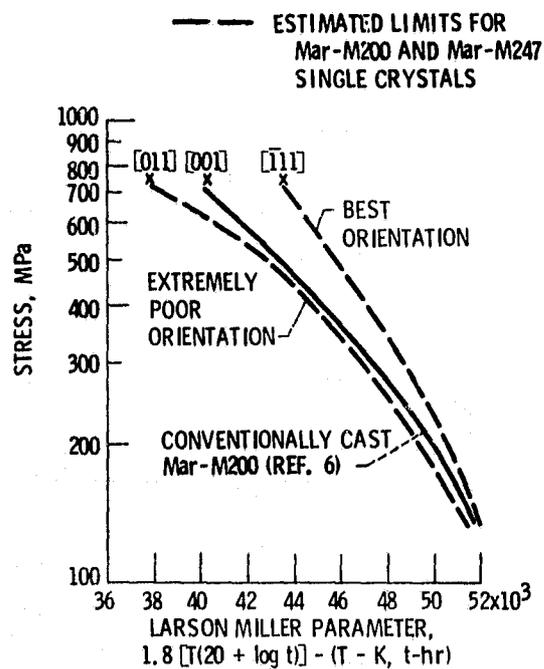


Figure 8. - Effect of crystallographic orientation on stress rupture life for Mar-M200 and Mar-M247.

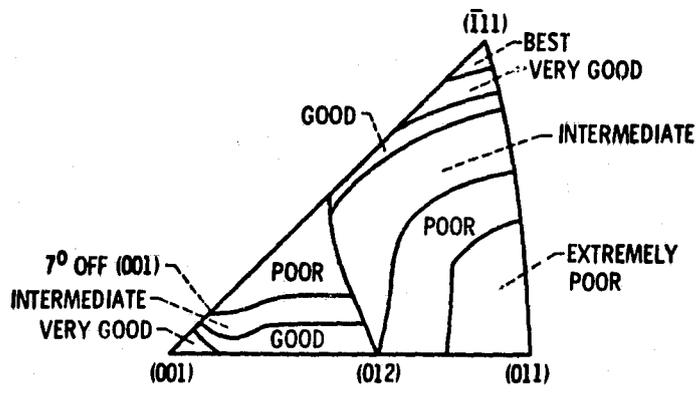


Figure 9. - Suggested regimes of stress rupture lives for Mar-M247 single crystals at about 760° C.

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