NOTICE

THIS DOCUMENT HAS BEEN REPRODUCED FROM MICROFICHE. ALTHOUGH IT IS RECOGNIZED THAT CERTAIN PORTIONS ARE ILLEGIBLE, IT IS BEING RELEASED IN THE INTEREST OF MAKING AVAILABLE AS MUCH INFORMATION AS POSSIBLE.
SOLAR HOT WATER SYSTEM INSTALLED AT LAS VEGAS, NEVADA - FINAL REPORT

Prepared from documents furnished by

LaQuinta Motor Inns, Inc.
Post Office Box 32064
San Antonio, Texas 78216

Under DOE Contract 77-G-01-1654

Monitored by

National Aeronautics and Space Administration
George C. Marshall Space Flight Center, Alabama 35812

For the U. S. Department of Energy
# TABLE OF CONTENTS

I. Key Word Abstract ...................................... 1

II. Introduction ........................................... 1

III. Design Philosophy .................................... 1

A. Collectors .......................................... 2

B. Storage System ..................................... 2

C. Heat Exchangers .................................... 2

D. Pump and Controls .................................. 2

IV. Operation of the System ............................. 2

V. Problems Encountered and Solutions .................. 3

VI. Pictures of Final Installation ....................... 4

Appendix A - Roof Plan/Solar ............................ A-1

Appendix B - Operator's Instructions ................... B-1

Appendix C - Manufacturer's Literature ............... C-1

Appendix D - Verification ............................... D-1
APPENDIX A

ROOF PLAN/SOLAR

FOR

LA QUINTA MOTOR INNS, INC.

LAS VEGAS, NEVADA
A. Collectors

The collectors chosen for this project were single glazed Model SG-18, manufactured by Raypak, Inc. A total of 36 collectors were used. The collectors were supplied with Model PR-18 Solar Panel Rack Kit. (See attached sheets on Raypak collectors.) All the collectors were orientated due south at a 46° tilt to maximize for winter solar collection.

B. Storage System

A 2,500 gallon insulated vertical steel storage tank was located outdoors next to the Inn's cooling tower. A temperature sensor was installed in the storage tank for control function. To improve heat transfer between the heat exchangers and stored water, a 1/12 HP Grundfos recirculating pump was installed.

C. Heat Exchangers

Two heat exchanger tube bundles were mounted into the storage tank. The upper heat exchanger which served to extract heat from the storage tank to the domestic hot water system was sized for 100 gpm at 10°F temperature rise. The lower heat exchanger which served to transfer heat from the solar collectors to the storage tank was sized for 51 gpm at 10°F temperature drop.

A solution of ethylene glycol was used as heat transfer fluid between the solar collectors and the lower heat exchanger. With the use of the upper heat exchanger for the domestic hot water system, a double wall separation was achieved between the domestic hot water system and the ethylene glycol.

D. Pump and Controls

Two solar loop pumps, each sized for 100% of the solar system requirements were installed. The pumps are controlled by a temperature differential controller with an alternator for equal usage of the pumps.

IV. OPERATION OF THE SYSTEM

The system was put into operation in the summer of 1979. During the high temperature and pressure test of the system, 18 collectors developed leaks at solder joints at the waterway and internal header. After investigation, the manufacturer replaced all absorbers in the system. The system has been operating satisfactorily since then.
V. PROBLEMS ENCOUNTERED AND SOLUTIONS

The system has been operating without any trouble since its completion. At the time of final inspection, it was noted that some modifications can be made which would improve the efficiency of the system. (Please see attached report in APPENDIX D - VERIFICATION.)
VI. PICTURES OF FINAL INSTALLATION

Solar Panels

Solar Panels on roof with 2,500 gallon storage tank on ground.
APPENDIX A

ROOF PLAN/SOLAR

FOR

LA QUINTA MOTOR INNS, INC.

LAS VEGAS, NEVADA
COLLECTOR/PARTIAL ROOF PLAN

SCALE 3/16" = 1'-0"

FOLDOUT FRAME
NOTES

1. COLLECTOR INFORMATION
   - LOCATION: ROOF
   - SIZE: 20 FT x 20 FT
   - MATERIAL: GALVANIZED STEEL
   - CONNECTOR: PVC FITTINGS

2. ANODE CABLE LENGTH: 50 FT
   - INSTALLATION: BETWEEN COLLECTOR AND INVERTER

3. WATER INLET: 1" PIPE
   - LOCATION: WALL

4. WATER OUTLET: 1" PIPE
   - LOCATION: WALL

5. WATER TANK: 500 GALLONS
   - LOCATION: ROOF

6. COLLECTOR UNEQUALITY TO BE DONE WITH 3/4" DURABLE COPPER TUBING

7. REFER TO MARKET PLAN FOR LOCATION OF MOUNTING CURVES
   AND COLLECTOR SPACED.
APPENDIX B

OPERATOR'S INSTRUCTIONS

AND

MAINTENANCE MANUAL
GENERAL DISCUSSION

This is a closed solar system utilizing two heat exchangers to transfer heat from the solar collectors to the domestic hot water system. Please refer to attached schematic drawing of the solar system.

P-1 and P-2 are solar loop pumps that circulate a 50-50 solution of ethylene glycol and water between the solar collectors and the heat exchanger, HX-1. Only one solar loop pump is needed for the system operation, the other solar loop pump serves as 100% standby. The solar loop pumps are controlled by a temperature differential controller which starts the pump when the temperature at the solar collectors is 20°F higher than the temperature in the 2,500 gallon storage tank. The temperature differential controller will de-activate the solar loop pump when the temperature at the solar collectors is not more than 3°F higher than the temperature in the 2,500 gallon storage tank. An alternator alternates the operation of P-1 and P-2 for equal usage.

P-3 is a recirculating pump to improve the heat transfer between the heat exchangers and the stored water in the 2,500 gallon storage tank. P-3 is interlocked with P-1 and P-2 so that if either P-1 or P-2 is activated, so will P-3. In addition, P-3 will activate when the ambient temperature is 32°F or lower.

Domestic cold water will enter heat exchanger, HX-2, to be preheated before entering the 750 gallon water heater. When the temperature in the 2,500 gallon storage tank reached a minimum of 8°F higher than the temperature of the water in the 750 gallon water heater, the temperature differential controller will activate pump P-4 to transfer the heat from the 2,500 gallon storage tank to the 750 gallon water heater. Pump P-4 will be de-activated when the temperature in the 2,500 gallon storage tank is only 4°F higher than the temperature of the 750 gallon water heater.

P-5 is the usual hot water recirculating pump of the buildings hot water system.

Mixing valve, V-1 is set to prevent the temperature of the hot water supplied to the building from exceeding 140°F.
II

MAINTENANCE REQUIREMENTS

1. Once a Week:
   a. Check fluid level in the solar system expansion tank. If low, add a 50-50 mixture of ethylene glycol and water to the system. CAUTION: NEVER ADD PLAIN WATER TO THE SYSTEM.

2. Once a Month:
   a. Wash glass surfaces of the solar collectors using a mild detergent solution and a soft brush. Thoroughly rinse with clean water.
   b. Check temperature differential controllers and alternator for proper operation.
   c. Check for fluid leaks from collectors and piping.

3. Once a Year:
   a. Check pump seals for leakage.
   b. Draw a sample of heat transfer fluid from the solar system for analysis and determination of any action needed to provide maximum corrosion inhibition.
MOTOR MOUNT
Centrifugal Pumps

SERIES 4260 for small capacities
SERIES 4280 single mechanical seal
SERIES 4285 packing gland arrangement
SERIES 4290 double mechanical seal
ARMSTRONG MOTOR MOUNT CENTRIFUGAL PUMPS

The motor-mount concept of pump design has a number of inherent advantages - compact arrangement, ease of installation, elimination of alignment problems and simplification of foundations. In addition, Armstrong Series 4280, 4280, 4290 and 4290 pumps offer an extensive range of outputs, optional materials of construction and a choice of important design features. A comprehensive, integrated line with wide acceptance for a variety of applications.

EXTENSIVE INTERCHANGEABILITY OF PARTS

MANUFACTURED AND INSPECTED TO RIGID STANDARDS

ALL PUMPS FACTORY TESTED PRIOR TO SHIPPING

SERIES 4280

1. VOLUTE. Radially-split volute can be left in the line while servicing the pump, eliminating needless disconnection of pipes. Tapped openings are provided for venting, draining and gauge connections. Wearing Rings optional.

2. IMPELLER. Balancing chamber and pressure relief holes in the impeller reduce axial thrusts to a minimum, ensuring smooth performance and long life.

3. MOTOR. The motor is equipped with heavy-duty grease-lubricated ball bearings adequately rated to accommodate impeller radial loads and residual hydraulic thrusts.

4. MECHANICAL SEAL. Self-lubricating "ARMSEAL" prevents liquid seepage. A carbon face rotating against a stationary ceramic seat provides positive sealing up to full design pressure.

5. BRACKET. A heavy cylindrical bracket with 360-degree register on both flanges provides a rigid union of pump and motor and establishes perfect alignment.

6. SHAFT. The impeller is mounted on an extension of the motor shaft with minimum overhang. A suitable shaft sleeve affords protection in the wetted area.

BACK PULL-OUT DESIGN. This feature eliminates the need to break piping connections when servicing the pump. The motor, with bracket and impeller attached, can be easily withdrawn from the volute after removing the volute cap screws.
SERIES 4260

Small capacity pump with mechanical seal. Stub shaft arrangement permits the use of standard "C" flange motors.

SERIES 4285

Packing gland arrangement...for use when pumping contaminated liquids and/or higher temperatures where gland leakage can be tolerated. Stuffing box can be lubricated either by liquid pumped or by separate clean water supply.

SERIES 4290

Double mechanical seal arrangement...for use when pumping contaminated liquids and/or higher temperatures without loss of system liquid. Sealing water can be taken from pump discharge...through a heat exchanger if necessary...or from city supply mains. Raw sealing water does not enter system.

### DESIGN DATA

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<th>SERIES 4280</th>
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<td>1¼&quot; through 6&quot;</td>
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ALL PERFORMANCE CURVES ARE BASED ON PUMPING CLEAN COLD FRESH WATER AT A TEMPERATURE NOT EXCEEDING 85°F (SPECIFIC GRAVITY 1.0).
ARMSTRONG MOTOR MOUNT CENTRIFUGAL PUMPS

DIMENSIONAL DATA
SERIES 4280
SERIES 4285
SERIES 4290

PUMP

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<td>1½</td>
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<tr>
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<td>1½</td>
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<tr>
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Pump sizes 2½ and larger have 125 lb. standard ASA flanges. Smaller pump sizes have NPT screwed connections. All pumps are rated for 175 psig maximum working pressure.

THREE-PHASE MOTOR

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<th>Motor Frame Size</th>
<th>Series 4280</th>
<th>Series 4285/4290</th>
<th>HP @ 1750 RPM</th>
<th>HP @ 3600 RPM</th>
<th>F</th>
<th>G</th>
<th>H</th>
<th>J</th>
<th>K</th>
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SINGLE-PHASE MOTOR

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<th>HP @ 3600 RPM</th>
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*For exact installation data, please contact factory for certified dimensions.
ARMSTRONG MOTOR MOUNT CENTRIFUGAL PUMPS

DIMENSIONAL DATA
SERIES 4260

ALL PUMP SIZES ARE PROVIDED WITH NPT SCREWED CONNECTIONS

PUMP

MOTOR

ALL DIMENSIONS IN INCHES*

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<th>%</th>
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<td>1½</td>
<td>2½</td>
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<tr>
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<td>2½</td>
<td>2½</td>
<td>3½</td>
<td>3½</td>
<td>3½</td>
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</tbody>
</table>

*For exact installation data, please write factors for certified dimensions.

TYPICAL SPECIFICATIONS

Furnish and install, as illustrated on the plans and specifications, an Armstrong End Suction Motor Mount Centrifugal Pump...

...SERIES 4260  ...SERIES 4280  ...SERIES 4285  ...SERIES 4290

equipped with a water-tight, long-life, self-lubricating "ARMSEAL."
equipped with a water-tight, long-life, self-lubricating "ARMSEAL."
equipped with a deep stuffing box, split gland, gland packing and full-length shaft sleeve.
equipped with double mechanical seal, seal plate and tagged connections for cooling water supply. (Auxiliary features specified separately.)

The pump shall be of the radially split casing type with back pull-out feature permitting removal of the pump internals without disturbing pipe connections. Pump construction shall be (all-iron) (all-bronze) suitable for a maximum working pressure of 175 psig.

The driving motor shall be of the horizontal shaft, foot-mounted, squirrel cage induction type with NEMA "C" flange, enclosure, and suitable for operation on a single volt cycle phase supply.

The complete unit shall be suitable for the following service (as shown in the pump schedule) and the pump manufacturer shall conduct running tests to verify the conditions of head and capacity specified.

SERVICE  LIQUID  PUMP SIZE
CAPACITY  USGPM  TEMPERATURE  "F.
TOTAL HEAD FEET  VISCOSITY  SSU  SPEED  RPM  MOTOR RATING  HP

Form no. 6185A 4M 7-76 HWA

C-13
SG18-DG18
for Domestic Water Heating, Space Heating and Air Conditioning

FEATURES
Heavy Duty Construction
Floated Absorber
All Copper Waterways
Fully Insulated
Low Iron Glass
Baked Enamel Exterior
Easy Field Access To All Components

Raypak has applied 30 years of leadership in the commercial boiler/heater industry to the development of a flat plate solar heating collector for residential, commercial and industrial applications. This advance design features all copper waterways for direct application to potable water, eliminating the need for a heat exchanger. Raypak's extensive experience in the boiler/heater industry means you get a product that meets codes and will function efficiently in your application year after year.
SG18-P-M-A/DG18-P-M-A
SG18-P-M-C/DG18-P-M-C

Technical Description - Sample Specification
Raypak's solar panels can be used for direct system application using water, for building heating or domestic water heating, or indirect application using a water/glycol solution (11% more panel required).

The Raypak solar panel consists of a non-ferrous heat transfer surface (absorber) and a container constructed to maximize absorptivity and minimize heat emissivity. The absorber is an all copper grid design with minimal pressure drop. The copper tubing is mechanically bonded between two sheets of copper or aluminum for maximum heat transfer. The top surface of the copper or aluminum is covered with durable semi-selective black coating.

The container is constructed of galvanized sheet steel with a baked enamel finish. The container is insulated with a rigid polyurethane foam which is sag-resistant, foil-faced on both sides, dimensionally stable and non-moisture absorbent. Insulating value is R10 and R8 respectively for bottom and sides. Glazing is 1/8" double strength tempered low iron glass to provide maximum resistance to wind load, hail impact, snow load and vandalism.

The absorber portion of the collector is designed to withstand 150 PSI and will meet building code piping standards. The collector is capable of withstanding temperatures up to 400°F with no flow of circulating media. Consult Catalog No. SP 3001-E for details on control systems.
SERIES 60

the extra quiet

in-line pump for general services

BELL & GOSSETT ITT
FLUID HANDLING DIVISION
Discharge Gage Tapping (on side opposite)

Rear Bearing

Coupler Assembly

Shaft

Motor Bracket Assembly

Bearing Bracket Assembly

Front Bearing

Suction Gage Tapping

Volute

Seal Assembly

Impeller (Enclosed)

Companion Flange (included)

1AA, 1¼ AA, 1½ AA and 2 AA construction details

Discharge Gage Tapping (on side opposite)

Rear Bearing

Coupler Assembly

Shaft

Motor Bracket Assembly

Bearing Bracket Assembly

Front Bearing

Suction Gage Tapping

Volute

Seal Assembly

Impeller (Enclosed)

Companion Flange (included)

1½ A and 2 A construction details

ORIGINAL PAGE IS OF POOR QUALITY

1AA, 1¼ AA, 1½ AA and 2 AA construction details

1½ A and 2 A construction details
Series 60 Pumps can be furnished in bronze-fitted, all iron, or all bronze construction to suit your application.

Curves based upon shop test using clear cold water at a temperature of not over 85°F.

Horsepower curves do not include motor service factor.
### Dimensions

**Fig. 1 AA Sizes**

**Fig. 2 A Sizes**

**Standard Voltages**

1/4 HP, 1 PH, 115 Volts. 1/2 to 1 1/2 HP, 1 PH, 115/230 Volts. 3 HP, 200-230/480 Volts. 1 to 2 HP, 208 or 230/460 Volts.

All single phase motors have built-in overload protection.

**Construction Flanges Furnished for Suction and Discharge**

### Construction Materials

**For Parts in Contact with Fluid Pumped**

<table>
<thead>
<tr>
<th>Description</th>
<th>Bronze Fitted Pump</th>
<th>All Iron Pump</th>
<th>All Bronze Pump</th>
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<tbody>
<tr>
<td>Volute</td>
<td>Cast Iron</td>
<td>Cast Iron</td>
<td>Bronze with Brass Face Plate</td>
</tr>
<tr>
<td>Bearing Bracket</td>
<td>Cast Iron</td>
<td>Cast Iron</td>
<td>Iron with Brass Face Plate</td>
</tr>
<tr>
<td>Impeller</td>
<td>Brass</td>
<td>Steel (AA)/Cast Iron (A)</td>
<td>Brass</td>
</tr>
<tr>
<td>Impeller Key</td>
<td>Steel</td>
<td>Steel</td>
<td>Brass</td>
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<tr>
<td>Impeller Lock Washer</td>
<td>Steel</td>
<td>Steel</td>
<td>Brass</td>
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<tr>
<td>Impeller Lock Nut</td>
<td>Brass (AA)/Steel (A)</td>
<td>Plated Steel</td>
<td>Brass</td>
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<tr>
<td>Pump Shaft</td>
<td>Steel</td>
<td>Steel</td>
<td>Brass</td>
</tr>
<tr>
<td>Shaft Sleeve</td>
<td>Copper</td>
<td>Stainless Steel</td>
<td>Copper</td>
</tr>
<tr>
<td>Seal Assembly</td>
<td>Carbon Seal Ring, Ceramic Seat, Synthetic Rubber Bellows and Stainless Steel Spring</td>
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</tbody>
</table>
APPENDIX D

VERIFICATION
VERIFICATIONS

1. Final Field Inspection

A team consisting of Jay Forester, Ronald Wang (Owner's Representative), Douglas Westrope, Jr., Houston M. Hammac, and W.T. Powers (Department of Energy Representatives) met for final inspection on April 23, 1980 through April 25, 1980.

The installation was found to be complete and operating as called for in the plans. The control system was checked out and confirmed to be performing as designed.

2. Data Obtained During Final Field Inspection

Please see attached sheets.

3. Acceptance

The installation is considered complete and accepted.

Ronald K. Wang
Mechanical/Electrical Engineer
Development Division
LA QUINTA MOTOR INNS, INC.

RW:cs
1. Operation Logic:

Collector-to-Storage $\Delta T = 20^\circ F$ - Flow on, P6 or P7
plus Storage Recirculation Pump P5
Collector-to-Storage $\Delta T = 3^\circ F$ - Flow Off
Storage-to-Load $\Delta T = 8^\circ F$ - Flow On, P4 plus
Storage Recirculation Pump P5
Storage-to-Load $\Delta T = 4^\circ F$ - Flow Off

2. Collector Loop @ 50 gpm nominal 5$^\circ F$ rise
   @ 25 gpm nominal 10$^\circ F$ rise
Load Loop @ 48 gpm nominal 2$^\circ F$ rise

During periods of high flow usage when washing machines are calling for water, the $\Delta T$ rise is approximately 10$^\circ F$. The load HX inlet will be approximately 70$^\circ F$ and the outlet will be approximately 80$^\circ F$ when solar storage at mid-tank is about 105$^\circ F$.

Flow in the collector loop was reduced from 50 gpm to 25 gpm, but flow in the load loop could not be reduced from the current 48 gpm with pump P4 on because current plumbing requires all CWS makeup to pass through pump P4 prior to entering the motel DHW supply. The motel usage may demand greater than 25 gpm at periodic intervals.

3. The supplementary DHW tank heating elements were noted to be operational during very brief intervals, and operation was only during the period of heavy laundry usage. Even then, no more than two element pairs were ever noted as activated.

4. Load loop HX piping in mechanical room is not insulated permitting unnecessary loss of energy.

5. Load loop HX piping connections to DHW tank are both at about one-quarter height of tank. The inlet to the HX is approximately 1 1/2 inches above the outlet from the HX. There is no baffle and both are open at the same penetration into the tank.

During the course of an operating day, there are periodic intervals that energy is removed from the DHW tank and passed back to the solar storage tank.

This can be attributable to the inlet and outlet HX plumbing connection as it now exists at the 750 gallon DHW tank. It is also influenced by an apparent insulated affect of the load loop temperature control sensor installed in the DHW tank. This sensor never exceeded 110$^\circ F$ even when other measurements indicated the temperature in the bottom of the tank exceeded 118$^\circ F$. 

D-3
1. On April 24, 1980, at 7:16 a.m., the insolation was measured as being 60 BTUH per square foot and at 4:16 p.m., it was measured as being 70 BTUH per square foot. The insolation peaked between 11 a.m. and 1 p.m. at 265 BTUH per square foot. During the 9-hour period of measurement, approximately 3,423,600 BTU's were available for collection. There were approximately 957,000 BTU's collected. During the period between 11 a.m. and 1 p.m., approximately 636,000 BTU's were available for collecting and about 212,600 BTU's were collected. This translates into a collector loop system efficiency of about 33 percent during conditions which rate the collector efficiency at about 34 percent.

2. In the load loop between the hours of 11 a.m. and 1 p.m. at a flow of 48 gpm with a nominal temperature rise of 2°F, approximately 96,000 BTU's were transferred to the DHW tank. This converts to about 28 kWh. Pumps P4, P5 and P6 used about 2 kWh yielding approximately 26 kWh gained.

3. During a period from 8:50 a.m. to 9 a.m., a 5 gpm flow to washer produced a 10°F rise across the HX. The inlet was 70°F and the outlet was 80°F. The solar storage at mid-tank was about 105°F. The BTU gained from solar storage was about 4,170 BTU's which translates into 1.2 kWh.

4. Based upon the measurements recorded during the April 23, 1980, to April 25, 1980, period, on days that insolation achieves at least 265 BTUH per square foot between the hours of 11 a.m. and 1 p.m., 900,000 BTU to 1,000,000 BTU will be deposited into solar storage during the total collection period. Usage will occur simultaneously with collection throughout the day. Solar energy collected exceeded the requirements for heating DHW usage during the day. Therefore, the excess collected remained in storage raising the solar storage tank by 21°F from about 106°F to approximately 127°F. This translates into approximately 437,000 BTU to be given up by solar storage during evening, night and early morning usage prior to reactivation of solar collection. This appears that about 54 percent of the energy collected is used during the day and the other 46 percent is available during the non-collection hours. By conservative estimates, 90 percent of the energy given up by solar storage will be transferred to motel usage through the DHW tank during daytime usage. Converting 90 percent of the BTU into kWh yields 135.3 kWh. Subtracting the parasitic energy consumed by pumps P4, P5 and P6 during this period leaves approximately (135.3 - 17.3) 118 kWh. During the designated nighttime operation in which the remaining 46 percent is available, 85 percent of the energy will be transferred for motel usage through the DHW tank. Converting 85 percent of the BTU into kWh yields approximately 103.8 kWh. Modifying this quantity by the parasitic energy consumed by pumps P4 and P5 leaves approximately (103.5 - 8.8) 95 kWh. Therefore, for each day approximately 213 kWh will be gained from solar. At current electric rates of $0.0485 per kWh in Las Vegas, NV, this trans-
lates into about $10.30 per day contributed to the motel by solar.

Houston M. Hammar
Site Equipment and Assessment Group
May 6, 1980
265 BTU/FT² peak for the day

Collected: 950,000 BTU
Usage: 513,000 BTU from 8 a.m. to 5 p.m. (Day)
437,000 BTU from 5 p.m. to 8 a.m. (Night)

Useful Recovery: Day @ 90%
Night @ 85%

Pump Wattage Consumption Rates: P4 @ 660 wh
P5 @ 185 wh
P6 or P7 @ 1100 wh

P4 & P5 between 5 p.m. and 11 p.m. @ 99% runtime
(660 + 185) * 6 * .99 = 5 kWh

P4 & P5 between 11 p.m. and 8 a.m. @ 50% runtime
(660 + 185) * 9 * .99 = 3.8 kWh

P4 & P5 & P6 between 8 a.m. and 5 p.m. @ 99% runtime
(660 + 185 + 1100) * 9 * .99 = 17.3 kWh

Day (from 8 a.m. to 5 p.m.)
513,000 BTU * .9 + 3413 = 135.3 kWh
less parasitic losses = 17.3 kWh
yields effective energy contribution = 118 kWh

Night (from 5 p.m. to 8 a.m.)
416,700 BTU * .85 + 3413 = 103.8 kWh
less parasitic losses = 8.8 kWh
yields effective energy contribution = 95 kWh

Total per day energy contribution:
118 kWh + 95 kWh = 213 kWh

@ $0.0485 per kWh electric rates:
213 kWh * 0.0485 = $10.30 per day.
1. Ensure that the modification to add two gas-fired DHW tanks is installed in a manner not detrimental to the solar contribution. The additional recirculation pump should not run when the load circulation pump P4 is operating. This is accomplishable in a manner similar to the attached Figure 1 enclosure.

2. The load HX piping in the mechanical room should be insulated to minimize losses to the room space.

3. Ensure baffles or some diverting scheme is installed in the 750 gallon DHW tank between the inlet and outlet to the load HX. Return from load HX connection point to the 750 gallon DHW tank should be at the higher level relative to the supply to the load HX connection point from the DHW tank.

4. Ensure the load loop temperature control sensor in the DHW tank is performing properly by responding to actual temperatures correctly and that it remains exposed to dynamic fluid conditions.

Incorporation of recommendations 3 and 4 should preclude the tendency to remove energy from the DHW tank to solar storage during transition periods.

5. The solar storage recirculation pump P5 should not operate except when pump P6 or P7 is operating, permitting maximum advantage of statification in the solar storage during non-collection periods.

6. Ensure the functionality of the expansion tank in the solar loop.

7. Modify the CWS makeup for the motel usage to the outlet of load circulation pump P4 permitting the flow to be reduced to 25 gpm. This will accomplish a higher temperature rise across the heat exchanger. The increase in sensible heat will effect greater energy transfer with less quantity of fluid decreasing pump P4 runtime.

8. The thermostat for the gas-fired DHW tanks should be set to come ON at 110° F and go OFF at 120° F. The recirculation line must be insulated to minimize losses and on time of the gas heat.

9. The collector loop should remain at 25 gpm to effect a greater temperature drop than will occur at 50 gpm. This will permit inlet temperature to the collectors to remain lower thus collector efficiency will be greater.

10. For any future installations, the pumps should be sized for required fluid flow to minimize parasitic energy consumption.

Houston M. Hammac
Site Equipment and Assessment Group
May 6, 1980
6. The collector loop expansion tank appears fully charged with no expansion functionality permitted in the tank.

7. On days when insolation reaches at least 265 BTU\(^\text{H}\) per square foot between 11 a.m. and 1 p.m., the solar storage will be raised to approximately 127\(^\circ\) F at mid-tank.

   Overnight usage will not drop the solar storage tank below approximately 106\(^\circ\) F at mid-tank.

8. Between the hours of 6 a.m. and 11 p.m., the load loop HX circulation pump P4 and the solar storage recirculation pump P5 operate about 99 percent of the time and between the hours of 11 p.m. and 6 a.m., operation is about 50 percent of the time.

Houston M. Hammac
Site Equipment and Assessment Group
May 6, 1980