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Progress Report 17
for the Period September 1980 to February 1981

and Proceedings of the
17th Project Integration Meeting

Prepared for
U.S. Department of Energy
Through an agreement with
National Aeronautics and Space Administration
by
Jet Propulsion Laboratory
California Institute of Technology
Pasadena, California

(JPL PUBLICATION 81-35)
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ABSTRACT

This report describes progress made by the Low-Cost Solar Array Project during the period September 1980 to February 1981. It includes reports on project analysis and integration; technology development in silicon material, large-area silicon sheet and encapsulation; production process and equipment development; engineering, and operations. It includes a report on, and copies of visual presentations made at, the Project Integration Meeting held at Pasadena, Calif, on February 4 and 5, 1981.
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<th>Description</th>
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<tbody>
<tr>
<td>A</td>
<td>Angström(s)</td>
</tr>
<tr>
<td>AM</td>
<td>Air Mass (e.g., AM1 = unit air mass)</td>
</tr>
<tr>
<td>AR</td>
<td>Antireflective</td>
</tr>
<tr>
<td>BCS</td>
<td>Balance of System (non-array elements of a PV system)</td>
</tr>
<tr>
<td>B-T</td>
<td>Bias/temperature</td>
</tr>
<tr>
<td>B-T-H</td>
<td>Bias/temperature/humidity</td>
</tr>
<tr>
<td>CFP</td>
<td>Continuous-flow pyrolyzer</td>
</tr>
<tr>
<td>CVD</td>
<td>Chemical vapor deposition</td>
</tr>
<tr>
<td>Cz</td>
<td>Czochralski (classical silicon crystal growth method)</td>
</tr>
<tr>
<td>DCF</td>
<td>Discounted cash flow</td>
</tr>
<tr>
<td>DLTS</td>
<td>Deep-level transient spectroscopy</td>
</tr>
<tr>
<td>DoE</td>
<td>Department of Energy</td>
</tr>
<tr>
<td>DS/RMS</td>
<td>Directionally solidified/refined metallurgical-grade silicon</td>
</tr>
<tr>
<td>EB</td>
<td>Electron beam</td>
</tr>
<tr>
<td>EFG</td>
<td>Edge-defined film-fed growth (silicon ribbon growth method)</td>
</tr>
<tr>
<td>EPR</td>
<td>Ethylene propylene rubber</td>
</tr>
<tr>
<td>EPSh</td>
<td>Experimental Process System Development Unit</td>
</tr>
<tr>
<td>ESB</td>
<td>Electrostatic bonding</td>
</tr>
<tr>
<td>ESGU</td>
<td>Experimental Sheet Growth Unit</td>
</tr>
<tr>
<td>EVA</td>
<td>Ethylene vinyl acetate</td>
</tr>
<tr>
<td>FAST</td>
<td>Fixed abrasive slicing technique</td>
</tr>
<tr>
<td>FBR</td>
<td>Fluidized-bed reactor</td>
</tr>
<tr>
<td>FPUP</td>
<td>Federal Photovoltaics Utilization Program</td>
</tr>
<tr>
<td>GRC</td>
<td>Glass-reinforced concrete</td>
</tr>
<tr>
<td>HCl</td>
<td>Hydrochloric acid</td>
</tr>
<tr>
<td>HEM</td>
<td>Heat exchanger method (silicon crystal ingot growth method)</td>
</tr>
</tbody>
</table>
HF  Hydrofluoric acid
HNO₃  Nitric acid
ID  Inner diameter
ILC  Intermediate-load center
IPEG  Interim Price Estimation Guidelines
IPEG4  Improved Price Estimation Guidelines
Iₜₜ  Short-circuit current
I-V  Current-voltage
LAPSS  Large-area pulsed solar simulator
LAR  Low-angle ribbon (silicon growth method)
LAS  Large-Area Silicon Sheet Task
LCP  Lifetime cost and performance
LeRC  Lewis Research Center
LSA  Low-Cost Solar Array
mgSi  Metallurgical-grade silicon
MIT-LL  Massachusetts Institute of Technology Lincoln Laboratory
MBS  Multiblade sawing
MEPSDU  Module experimental process system development unit
MWS  Multiwire sawing
NASA  National Aeronautics and Space Administration
NBNM  Natural Bridges National Monument
NDE  Nondestructive evaluation
NOCT  Nominal operating cell temperature
NTCR  Near-Term Cost Reduction
OTC  Optimal test conditions
P  Individual module output power
PA&I  Project Analysis and Integration Area
<table>
<thead>
<tr>
<th>Abbreviation</th>
<th>Full Form</th>
</tr>
</thead>
<tbody>
<tr>
<td>Pavg</td>
<td>Module rated power at SOC, Vno</td>
</tr>
<tr>
<td>PDU</td>
<td>Process Development Unit</td>
</tr>
<tr>
<td>PEBA</td>
<td>Pulsed electron beam annealing</td>
</tr>
<tr>
<td>P/FR</td>
<td>Problem-failure report</td>
</tr>
<tr>
<td>PIM</td>
<td>Project Integration Meeting</td>
</tr>
<tr>
<td>Pmax</td>
<td>Maximum power</td>
</tr>
<tr>
<td>PMMA</td>
<td>Polymethyl methacrylate</td>
</tr>
<tr>
<td>PnBA</td>
<td>Poly-n-butyl acrylate</td>
</tr>
<tr>
<td>POCl₃</td>
<td>Phosphorus oxychloride</td>
</tr>
<tr>
<td>PP&amp;E</td>
<td>Production Process and Equipment Area</td>
</tr>
<tr>
<td>ppba</td>
<td>Parts per billion atomic</td>
</tr>
<tr>
<td>ppma</td>
<td>Parts per million atomic</td>
</tr>
<tr>
<td>PRDA</td>
<td>Program Research and Development Announcement</td>
</tr>
<tr>
<td>PV</td>
<td>Photovoltaic(s)</td>
</tr>
<tr>
<td>PVB</td>
<td>Polyvinyl butyral</td>
</tr>
<tr>
<td>PVC</td>
<td>Polyvinyl chloride</td>
</tr>
<tr>
<td>RFP</td>
<td>Request for proposal</td>
</tr>
<tr>
<td>RFQ</td>
<td>Request for quotation</td>
</tr>
<tr>
<td>RMS</td>
<td>Refined metallurgical-grade silicon</td>
</tr>
<tr>
<td>RNHT</td>
<td>Relative normal hemispherical transmittance</td>
</tr>
<tr>
<td>RDI</td>
<td>Return on investment</td>
</tr>
<tr>
<td>RTR</td>
<td>Ribbon-to-ribbon (silicon crystal growth method)</td>
</tr>
<tr>
<td>SAMICS</td>
<td>Solar Array Manufacturing Industry Costing Standards</td>
</tr>
<tr>
<td>SAMIS</td>
<td>Standard Assembly-Line Manufacturing Industry Simulation</td>
</tr>
<tr>
<td>SCIM</td>
<td>Silicon coating by inverted meniscus</td>
</tr>
<tr>
<td>SEM</td>
<td>Scanning electron microscope</td>
</tr>
<tr>
<td>SEMI</td>
<td>Semiconductor Equipment Manufacturers Institute</td>
</tr>
<tr>
<td>Acronym</td>
<td>Description</td>
</tr>
<tr>
<td>---------</td>
<td>-------------</td>
</tr>
<tr>
<td>SERI</td>
<td>Solar Energy Research Institute</td>
</tr>
<tr>
<td>SiCl₄</td>
<td>Silicon tetrachloride</td>
</tr>
<tr>
<td>SiF₄</td>
<td>Silicon tetrafluoride</td>
</tr>
<tr>
<td>SiHCl₃</td>
<td>Trichlorosilane</td>
</tr>
<tr>
<td>SOC</td>
<td>Silicon on ceramic (crystal growth method)</td>
</tr>
<tr>
<td>SOC</td>
<td>Standard operating conditions (module performance)</td>
</tr>
<tr>
<td>SOLMET</td>
<td>Solar-meteorological</td>
</tr>
<tr>
<td>SPG</td>
<td>Silicon particle growth</td>
</tr>
<tr>
<td>SSMS</td>
<td>Spark-source mass spectrometry</td>
</tr>
<tr>
<td>STC</td>
<td>Standard test conditions (cell performance)</td>
</tr>
<tr>
<td>TR</td>
<td>Technical Readiness</td>
</tr>
<tr>
<td>UV</td>
<td>Ultraviolet radiation</td>
</tr>
<tr>
<td>V_{no}</td>
<td>Nominal operating voltage</td>
</tr>
<tr>
<td>V_{oc}</td>
<td>Open-circuit voltage</td>
</tr>
<tr>
<td>ZnCl₂</td>
<td>Zinc chloride</td>
</tr>
</tbody>
</table>
PROGRESS REPORT

Project Summary

Construction of the Union Carbide Corp. silane-to-silicon Experimental Process System Development Unit (EPSDU) (100 MT/yr), which was started in September 1980, is progressing well. Concrete and steel are being emplaced and the large distillation column is ready for installation. Union Carbide has initiated plans for the construction of a 1000 MT/yr silicon (Si) production plant that would start commercial operation in 1985.

The experimental reactor at Massachusetts Institute of Technology has the potential of reducing the cost of Si, if incorporated into a Siemens production plant, by enabling the recycling of silicon tetrachloride (STC) in the production of trichlorosilane (TCS).

The Hamco advanced Czochralski ingot grower with melt replenishment will be completed in February 1981, except for the automatic controls, which will be added in July 1981. Capacity will be five 30-kg ingots (15-cm dia) per run.

Efforts continue to increase the throughput rates of wafering machines: internal-diameter (ID) at Silicon Technology Corp. and multiwire (FAST) at Crystal Systems. The goals are 17 wafers/cm for 15-cm-dia wafers and 25 wafers/cm for 10-cm square wafers, which have been demonstrated at 85% and 90% yields, respectively, but with low slicing rates of 0.25 wafers/min.

The design of the web ribbon experimental sheet growth unit (ESGU) by Westinghouse continues to make good progress.

Mobil Tyco has reached its growth-rate goal of 4 cm/min for a single 10-cm-wide edge-defined film-fed-growth (EFG) ribbon and has grown three 10-cm-wide ribbons at 3.3 cm/min. Cells fabricated from 10-cm-wide ribbons grown at 3.5 cm/min, with CO2 ambient atmosphere, show efficiencies of 11.2% AM1 (AR coated, 28°C, 13-cm^2 area).

Module encapsulation technology progress, as summarized at the PIM, included:

- Material and process candidates under development and evaluation meet cost goals ($14/m^2) and have 20-year life potential.
- Encapsulation material requirements, specifications, and characterizations continue to evolve.
- Trade-offs for various module encapsulation designs and materials are being analyzed and will be verified by test.
- Durability testing of materials and modules (experimental and contemporary) is continuing in both accelerated and real time.

Ethylene vinyl acetate (EVA) developed as a module pottant is used in five of the Block IV modules.
PROJECT SUMMARY

Major material suppliers (DuPont Co., Rohm & Haas Co., 3M Co., Corning Glass Works, Schott, Masonite Corp., U.S. Gypsum Co., etc.), stimulated by the Low-Cost Solar Array Project (LSA), are participating voluntarily in encapsulation activities.

Automated solar cell and module manufacturing processes contracts were awarded (November 1980) to Solarex Corp. and Westinghouse Electric Corp. Module Experimental Process System Development Unit (MEPSDU) efforts are to demonstrate low-cost manufacturing technology:

The Solarex process uses 10 x 10-cm Semix polycrystalline wafers with spray-on front-junction formation, back-surface junction, spray-on AR coating, and electroless Ni contacts dipped in solder. The modules will be an EVA laminated glass superstrate design.

The Westinghouse process uses 2.5 x 10-cm dendritic web ribbons with diffused front junction, diffused back-surface junction, dip AR coating, and evaporated Ti/Pd/Cu-plated Cu contacts. Aluminum electrical interconnections will be ultrasonically welded to the cells. The modules will be an EVA-laminated glass superstrate design.

Analysis of non-mass-analyzed ion implantation indicates that it can be cost competitive with gaseous diffused-junction formation.

Block IV module observations and conclusions:

Manufacturers had some difficulties in evolving new designs that incorporated new technology, as evidenced by schedule slips, module problems during tests, and some retreats to conventional technology.

Price and performance progress of LSA module block purchases continues; prices are down, but the rate of decrease has slowed; efficiencies are up and reliability and durability are better, especially hail protection, moisture protection, and fault-tolerance capabilities.

Large-scale producibility will not be verified with limited purchase quantities.

Block IV module activities were critiqued by seven module manufacturers under contract in the four solicited topics listed below. The comments and ensuing discussions were well thought out, worthwhile, and mature. They will be incorporated into the Block V activities as appropriate. Major points are:

Design specifications: Module design is compromised and made more difficult by specifying both terminal voltage and module length. The module design specifications should be generalized whenever possible because they are used by many other buyers.

Environmental tests: Some believe that temperature range is excessive and humidity durations are not adequate. All would not voluntarily do as complete testing as the LSA tests.

SAMIS-SAMICS: Expensive operation and lack of confidence in results were two critical comments resulting from the inability to generate
accurate inputs with the small quantities involved. The less-complex IPEG4 is more useful to the contractors as an estimation tool. Most contractors also have costing methods of their own.

General: Industry working relationship with the Jet Propulsion Laboratory (JPL) is good. Feedback and consultation by JPL specialists is helpful. Block IV module requirements are not well matched to today's market, which is primarily for stand-alone applications. The Block IV activities were a valuable learning experience.

A flat-module and array safety design workshop, held February 3 and attended by more than 100 people, was based upon an Interim Standard for Safety written primarily by Underwriters Laboratories. The two-part document draft, consisting of construction requirements and performance requirements, will be updated based upon workshop comments and discussions.
Area Reports

PROJECT ANALYSIS AND INTEGRATION AREA

The objective of the Project Analysis and Integration (PA&I) Area is to support the planning, integration and decision-making activities of the Project. This is executed by providing coordinated assessments of Project goals and of progress toward the achievement of the goals by the various activities of the Project, the solar array manufacturing industry, and suppliers; by contributing to the generation and development of alternative Project plans through the assessment of possible achievements and economic consequences; by establishing the standards for economic comparisons of items under Project study; by supporting the integration of the tasks within the Project and between the Project and Program elements through development of procedures, and by developing analytical capabilities and performing or participating in the studies of required trade-offs.

The metallization-grid-pattern optimization effort, in cooperation with the PP&E Area, has made significant progress. The equations for the two-bus-bar design have been written and entered into the APL optimizing program.

Two different designs have been identified. The first is the present conventional design in that it is optimized using only two variables. The second is an improved design using four variables in the optimization. These designs, plus a third that uses less metal, will be used by PP&E in a large (about 50 each) sampling of solar cells. The actual output power produced from the cells will be compared with the results computed in the program.

Evaluation of the results of the near-term cost-reduction contracts has been completed. This was done in cooperation with the PP&E area; the results are presented in the Proceedings section of this document (see pp. 55-58).

A review of the SAMICS methodology is in progress. It covers the environmental requirements in SAMIS and a major update of the cost-account catalog, including labor rates, inflation rates, commodity prices and financial-organizational parameters. The user interface with SAMIS is also being reviewed to attempt to reduce the trauma experienced by first-time or occasional users. Formats A and C, the users' guide and other documentation are being reviewed. Planning is under way for a users' workshop.

The initial design was completed for the year-by-year financial reports (balance sheet, income statement, etc.) for SAMIS. Coding will start soon, after completion of a revision of the way the cost account catalog is handled in SAMIS. This will save about half the cost of that part of the computation (the savings will be about $15/run).

Sensitivity analyses were performed on the $2.70/Wp PV manufacturing plant. This was the first application of IPEG4 in the LSA Project. In addition, the calibration of IPEG4 to SAMIS has been completed and IPEG4 capabilities have been expanded to include RACI (Rapid Amortization of Capital Investment) price estimates.
TECHNOLOGY DEVELOPMENT AREA

Silicon Material Task

INTRODUCTION

The objective of the Silicon Material Task is to establish the practicality of processes capable of producing silicon (Si) suitable for use in the manufacture of solar cells at a rate equivalent to 500 MWp/yr of solar arrays at a price less than $14/kg (1980 $) by 1986. The program formulated to meet this objective provides for development of processes for producing either semiconductor-grade Si or a less pure, but utilizable (i.e., a solar-cell grade) Si material.

TECHNICAL GOALS, ORGANIZATION AND COORDINATION

Solar cells are now fabricated from semiconductor-grade Si, which has a market price of about $65/kg. A drastic reduction in cost of material is necessary to meet the economic objectives of the LSA Project. Efforts are now under way to develop processes that will meet the Task objectives in producing semiconductor-grade Si. Another means of meeting this requirement is to devise a process for producing so-called solar-cell-grade Si material, which is less pure than semiconductor-grade Si. However, the allowance for the cost of Si material in the overall economics of the solar arrays for LSA is dependent on optimization trade-offs, which concomitantly treat the price of Si material and the effects of material properties on the performance of solar cells. Accordingly, the program of the Silicon Material Task is structured to provide information for optimization tradeoffs concurrently with the development of high-volume, low-cost processes for producing Si. This structure has been described in detail in previous LSA Progress Reports. Besides the process development mentioned above, the program includes economic analyses of silicon-producing processes and supporting efforts, both contracted and in-house at JPL, to respond to problem-solving needs.

Thirteen contracts are in progress; these are listed in the table below.
## SILICON MATERIAL TASK

### Silicon Material Task Contractors

<table>
<thead>
<tr>
<th>Contractor</th>
<th>Technology Area</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>Semiconductor-Grade Silicon Processes</strong></td>
<td></td>
</tr>
<tr>
<td>Battelle Columbus Laboratories</td>
<td>Reduction of SiCl$_4$ by Zn in fluidized-bed reactor</td>
</tr>
<tr>
<td>Columbus, Ohio</td>
<td></td>
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<tr>
<td>JPL Contract No. 954339</td>
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<tr>
<td>Energy Materials Corp.</td>
<td>Gaseous melt replenishment system</td>
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<tr>
<td>Harvard, Massachusetts</td>
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<tr>
<td>JPL Contract No. 955269 (Near-Term Cost-Reduction Contract)</td>
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<tr>
<td>Hemlock Semiconductor Corp.</td>
<td>Dichlorosilane CVD process</td>
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<td>Hemlock, Michigan</td>
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<td>JPL Contract No. 955533</td>
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<tr>
<td>Union Carbide Corp.</td>
<td>Silane-Si process</td>
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<td>Tonawanda, New York</td>
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<tr>
<td>JPL Contract No. 954334</td>
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<tr>
<td><strong>Solar-Cell-Grade Silicon Processes</strong></td>
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<tr>
<td>Dow Corning Corp.</td>
<td>Electric-arc furnace process</td>
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<tr>
<td>SRI International</td>
<td>Na reduction of SiF$_4$</td>
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<td>Menlo Park, California</td>
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<tr>
<td>JPL Contract No. 954771</td>
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<td>Westinghouse Electric Corp.</td>
<td>Reduction of SiCl$_4$ by Na in arc heater reactor</td>
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## Silicon Material Task Contractors

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<tr>
<th>Contractor</th>
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<tr>
<td><strong>Impurity Studies</strong></td>
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<tr>
<td>Lawrence Livermore Laboratories</td>
<td>Impurity concentration measurements by neutron activation analysis</td>
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<tr>
<td>Livermore, California</td>
<td>NASA Defense Purchase Request No. WO-8626</td>
</tr>
<tr>
<td>Sah, C. T., Associates</td>
<td>Effects of impurities on solar cell performance</td>
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<tr>
<td>Urbana, Illinois</td>
<td>JPL Contract No. 954685</td>
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<tr>
<td>Westinghouse R&amp;D Center</td>
<td>Definition of purity requirements</td>
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<td>Pittsburgh, Pennsylvania</td>
<td>JPL Contract No. 954331</td>
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<tr>
<td><strong>Supporting Studies</strong></td>
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</tr>
<tr>
<td>AeroChem Research Laboratories</td>
<td>Formation and growth of Si particles from SiH₄ at high temperatures</td>
</tr>
<tr>
<td>Princeton, New Jersey</td>
<td>JPL Contract No. 955491</td>
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<tr>
<td>Lamar University</td>
<td>Technology and economic analyses</td>
</tr>
<tr>
<td>Beaumont, Texas</td>
<td>JPL Contract No. 954343</td>
</tr>
<tr>
<td>Massachusetts Institute of Technology</td>
<td>Hydrochlorination of metallurgical-grade silicon and SiCl₄</td>
</tr>
<tr>
<td>Cambridge, Massachusetts</td>
<td>JPL Contract No. 955382</td>
</tr>
</tbody>
</table>
SUMMARY OF PROGRESS

Development of Processes for Producing Semiconductor-Grade Silicon

Four processes for producing semiconductor-grade Si were under development in this period by Battelle Columbus Laboratories, Energy Materials Corporation, Hemlock Semiconductor Corporation and Union Carbide Corporation.

Battelle Columbus Laboratories concluded the experimental phase of their effort to develop a process for producing Si based on the reduction of silicon tetrachloride (SiCl₄) by zinc (Zn). Battelle was given a four-month contract extension, covering October 1980 through January 1981, for the purpose of continuing shakedown and testing operations aimed at accomplishing eight-hour operation of the process development unit (PDU). Numerous modifications and repairs were made to the apparatus. However, all attempts at sustained operation failed due to system malfunctions, primarily corrosion effects, plugging with zinc-zinc chloride mixtures, and breakage of equipment during operation.

Energy Materials Corp. completed its experimental effort on an Si melt-replenishment system for Czochralski crystal growth using trichlorosilane (SiHCl₃), under a near-term cost-reduction contract. The concept of in situ deposition of Si in a reactor and its subsequent removal and collection by melting was demonstrated. However, Technical Feasibility as a continuous process was not accomplished. The final report is being prepared.

Hemlock Semiconductor Corp. continued development of a process for producing Si approaching semiconductor-grade quality from dichlorosilane (SiH₂Cl₂) using Siemens-type C-reactors. Construction of the Process Development Unit (PDU), which will be used to investigate the scaled-up redistribution of SiHCl₃ and to produce SiH₂Cl₂ for reactor testing, was begun in November, with completion scheduled in May 1981. All concrete and structural steel work was completed, and all of the major pieces of equipment were ordered.

To assess the purity of redistributed chlorosilanes, samples of SiHCl₃ from various sources were passed through Dowex catalyst of the type that is expected to be used in the PDU, and the resulting mixtures, containing about 11 mole % of SiH₂Cl₂, were fed to a Siemens-type reactor. Analysis of the Si product indicated that it was of high quality and that the Dowex catalyst does not contribute contamination by electrically active species.

Union Carbide Corp. continued with the construction of a 100-MT-Si/yr experimental process system development unit (EPSDU) at East Chicago, Indiana. The process consists of the hydrochlorination of metallurgical-grade Si and SiCl₄ to SiHCl₃ and rearrangement of the latter to silane (SiH₄), which is then pyrolyzed to Si. All foundations for equipment and structures were completed and the structural steel for the process gantry was erected. All underground utilities and services lines were installed and the civil-structural subcontracts were completed with installation of two pre-engineered structures, the control room and the Si powder melter building. Fabrication of process and
auxiliary equipment for the EPSDU is progressing well. Equipment items started to arrive at the site.

In the UCC R&D program, the free-space reactor (FSR) PDU program was successfully completed after demonstrating long-term operability of the reactor. Three 12-hour tests and several shorter ones were completed according to plan. Fabrication of an alternative silane pyrolysis PDU, using a fluidized-bed reactor, was completed and installation is under way. Melters subcontract work by Kayex Corp. is about two months behind schedule. Most of the major components were procured and assembled. System checkout and preliminary melting tests using chunk Si will start soon.

Development of Processes for Producing Solar-Cell-Grade Silicon

Three contracts fall into this category; final reports are being prepared on each of them. SRI International's final report on the process for producing Si by the sodium reduction of SiF4 was delayed for additional changes and is expected to be issued early in March. Dow Corning Corp. issued its final report on the direct arc-reactor process, in which silica is reduced by carbon. Westinghouse Electric Corp. is about to publish the final report on its arc heater process, involving the reduction of SiCl4 by sodium.

Impurity Studies

C. T. Sah Associates is conducting a program to determine the maximum concentration of the metallic impurities -- titanium (Ti), molybdenum (Mo), Zn, and others -- that can be tolerated in the base of Si solar cells to maintain a given efficiency. To accomplish this, a computer model based on the fundamental parameters of solar cells for the determination of the effects of impurities and defects on cell performance is being developed. Three steps are employed in this study: (1) obtain the recombination rates of electrons and holes at impurity centers in Si; (2) compute the Si solar cell performance using the data obtained in (1), and (3) compare computed and measured cell performances. The voltage-stimulated capacitance transient spectroscopy and the diode reverse-switching current transient methods are employed to measure the thermal capture rates of electrons and holes at these impurity energy levels. The exact transmission line model is employed to compute the solar cell performances of n+/p/p+ and p+/n/n+ cells.

Measurements of the electron and hole capture rates at the lower Ti donor level and upper Ti acceptor level were made and compared with those published in the literature. Some of the published data are not accurate, due to the presence of large series resistance in both the Schottky barrier and diffused p/n junction diodes used. Large series resistance gives large resistance-times-capacitance time constants and seriously affects the filling rate measurements from which the majority carrier capture rates were determined. In addition to large series resistance, space-charge-limited current has also been observed in p-base Ti-doped n+/p diffused diodes at low temperatures (about 200K), and this current seriously affects the accuracy of the capture-rate measurements.
In the program by Westinghouse R&D Center to determine the effects of impurities on the performance of solar cells, spectral response measurements made in single-crystal and polycrystalline solar cells containing Mo, Ti, vanadium (V), or chromium (Cr) correlated well with cell I-V data. Both grain boundaries and impurities in polycrystalline devices were found to reduce carrier lifetime, resulting in decreased red response and cell efficiency. Deep-level transient spectroscopy (DLTS) and spectral response data taken together suggest interaction of Cr, a fast-diffusing species in Si, with grain boundaries to form precipitates.

Accelerated aging tests were completed for copper (Cu)- and nickel (Ni)-doped solar cells at 400°C, 600°C and 800°C. For Ni the data fit a model for thermally activated behavior with an activation energy of 0.673 eV. The "time to failure" (time to reduce cell efficiency to 90% of initial value) projected for cell operation at normal temperatures would be in excess of 20 years. In contrast to Ni, the time-temperature behavior of the Cu-doped devices does not fit a simple Arrhenius model.

Chromium-doped wafers were subjected to POCl₃ gettering at 600°C or 825°C and subsequently were step etched to reveal any variations in Cr activity with depth from the gettered surface. No activity was determined by DLTS to depths up to two mils below the junction, implying very rapid Cr outdiffusion or some form of thermal deactivation.

Supporting Studies

In a study of the formation and growth of Si particles from the decomposition of SiH₄ at high temperatures, AeroChem Research Laboratories used a high-temperature fast-flow reactor to make particle-growth measurements as functions of temperature (600°C to 1200°C), pressure (50 to 550 torr), and residence time (0.5 to 30 ms). Optical diagnostics consisting of attenuation and Mie scattering of laser light are being used to obtain information on formation, growth rates, and sizes of the particles. The extent of SiH₄ decomposition is being measured by infrared absorption spectroscopy. Particles are collected in the observation zone to check the particle concentrations and sizes, measured optically. Some of the results are presented in the Proceedings of the 17th PIM (see p. 103).

Lamar University prepared the draft final report on their process feasibility study, covering all efforts since contract inception in 1975. The report was reviewed by JPL personnel and is to be published soon.

In support of the Union Carbide program, the Massachusetts Institute of Technology is studying the production of SiHCl₃ by the hydrochlorination of metallurgical-grade Si and SiCl₄. Experiments were carried out with the objective of studying the life of the Si bed in the fluidized-bed reactor. After 238 hours of reaction, no significant change in the reaction rate was observed. The longevity of the Si bed shows that the hydrochlorination process can be operated continuously for long periods without interruption. A material balance of 92% was made on the Si. This result confirms the stoichiometry of the hydrochlorination reaction.
SILICON MATERIAL TASK

In a corrosion study made on Incoloy 800H, the selected material for the hydrochlorination reactor in the Union Carbide EPSDU, no measurable amount of corrosion was observed when a test sample was exposed to the hydrochlorination reaction for 238 hours at 500°C and 300 psig. A stable silicide protective film of approximately 20 µm thickness appears to form on the Incoloy 800H surface. This protective film is readily destroyed by air and moisture when it is exposed to the atmosphere but appears to be stable in the reactor environment. The study indicates that the Incoloy alloy is a good choice for this reactor.

The JPL in-house program included effort on the FBR, the conversion of SiH₄ to molten Si, consolidation of sub-µm Si powder produced by FSRs, and impurity studies.

The 2-in.-dia FBR was modified to improve instrumentation and to facilitate experiments. A series of experiments was then performed to determine how bed clogging would be affected by gas velocity. The results showed that the reactor could be operated without clogging at velocities as low as four times the minimum fluidization velocity (i.e., U/Uₘₚ = 4) at 700°C and 10 mole % SiH₄ in hydrogen, but the velocity during the initial period of the test must be higher (U/Uₘₚ > 7) to prevent clogging.

The silane-to-molten-silicon (SMS) conversion reactor was brought to temperatures above 1600°C on four occasions with no damage to the graphite heater or to the graphite reaction crucible. Lumps of Si obtained by melting sub-µm powder separate cleanly from the reactor walls.

Thermally stimulated capacitance measurements are being performed to determine electrically active impurity concentrations and energy levels of traps introduced by the impurities. Measurements were made on n-type substrate samples with aluminum contacts forming Schottky barrier diodes. The diode characteristics showed too much leakage to allow satisfactory measurements to be made; consequently, the diode fabrication process is being improved.

A method of consolidating sub-µm Si powder is being investigated. The top of a pedestal of Si is melted using a high-frequency generator. The sub-µm powder is extruded through a quartz tube, and partially compacted Si powder is fed into the molten Si surface and solidified by lowering the pedestal. It was shown that the surface of the pedestal can be melted successfully.
Large-Area Silicon Sheet Task

Present solar cell technology is based on the use of silicon wafers obtained by slicing Czochralski (Cz) or float-zone ingots (up to 10 cm in diameter), using single-blade inner-diameter (ID) diamond saws. This method of obtaining single-crystal silicon wafers is tailored to the needs of large-volume semiconductor device production (e.g., integrated circuits, discrete power and control devices other than solar cells). The small market offered by present solar cell users does not justify industry's development of the high-volume silicon production techniques that would result in low-cost photovoltaic electrical energy.

The improvement of the standard Czochralski ingot growth process by reduction of expendable material costs and improvement of ingot growth rate together with improved slicing techniques will produce large areas of silicon at costs meeting the goals of the LSA Project. Growth of large ingots by casting techniques, such as Heat Exchanger Method (HEM) growth, can further reduce sheet costs.

The objective of the Large-Area Silicon Sheet Task is to develop and demonstrate the feasibility of several processes for producing large areas of silicon-sheet material suitable for low-cost, high-efficiency solar photovoltaic energy conversion. To meet the objective of the LSA Project, sufficient research and development must be performed on a number of processes to determine the capability of each of producing on a number of processes to determine the capability of each of producing large areas of crystallized silicon at a low cost. The final sheet growth configurations must be suitable for direct incorporation into an automated solar array processing scheme.

Growth of crystalline silicon material in a geometry that does not require cutting to achieve proper thickness is an obvious way to eliminate costly processing and material waste. Growth techniques such as edge-defined film-fed growth (EFG), dendritic growth (web), silicon-on-ceramic (SOC), etc., are possible candidates for the growing of solar cell material.

Research and development on ribbon, sheet, and ingot growth plus multiple-blade, multiple-wire, and inner-diameter (ID) blade cutting, initiated in 1975-76, are in progress.

ORGANIZATION AND COORDINATION

When the LSA Project was initiated (January 1975) a number of methods potentially suitable for growing silicon crystals for solar cell manufacture were known. Some of these were under development; others existed only in concept. Development work on the most promising methods is now continuing. After a period of accelerated development, these methods will be evaluated and the best will be selected for advanced development. As the growth methods are refined, integrated process schemes will be developed by which the most cost-effective solar cells can be manufactured.

The Large-Area Silicon Sheet Task effort is organized into four phases: research and development of sheet growth methods (1975-77); advanced development of selected growth methods (1977-80); prototype development...
LARGE-AREA SILICON SHEET TASK

(1981-82); development, fabrication, and operation of pilot production growth plants (1983-86).

Large-Area Silicon Sheet Contracts

Research and development contracts awarded for growing crystalline silicon material for solar cell production are listed below. Preferred growth methods for further development have been selected.

Large-Area Silicon Sheet Task Contractors

<table>
<thead>
<tr>
<th>Contractor</th>
<th>Technology Area</th>
</tr>
</thead>
<tbody>
<tr>
<td>Crystal Systems, Inc.</td>
<td>Heat exchanger method (HEM)</td>
</tr>
<tr>
<td>Salem, Massachusetts</td>
<td>ingot growth; fixed-abrasive slicing technique (FAST)</td>
</tr>
<tr>
<td>JPL Contract No. 954373</td>
<td></td>
</tr>
<tr>
<td>Kayex Corp.</td>
<td>Advanced Cz growth (Adv. Cz)</td>
</tr>
<tr>
<td>Rochester, New York</td>
<td></td>
</tr>
<tr>
<td>JPL Contract No. 955733</td>
<td></td>
</tr>
<tr>
<td>P.R. Hoffman Co.</td>
<td>Multiblade slurry slicing technique (MBS)</td>
</tr>
<tr>
<td>Carlisle, Pennsylvania</td>
<td></td>
</tr>
<tr>
<td>JPL Contract No. 955563</td>
<td></td>
</tr>
<tr>
<td>Siltec Corp.</td>
<td>Inner diameter (ID)</td>
</tr>
<tr>
<td>Menlo Park, California</td>
<td>wafering</td>
</tr>
<tr>
<td>JPL Contract No. 955282</td>
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<tr>
<td>Siltec Corp.</td>
<td>Advanced Cz growth (Adv. Cz)</td>
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<tr>
<td>Menlo Park, California</td>
<td></td>
</tr>
<tr>
<td>JPL Contract No. 954886</td>
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</tr>
<tr>
<td>Silicon Technology Corp.</td>
<td>Internal diameter (ID)</td>
</tr>
<tr>
<td>Oakland, New Jersey</td>
<td>slicing</td>
</tr>
<tr>
<td>JPL Contract No. 955131</td>
<td></td>
</tr>
<tr>
<td>Semix Corp.</td>
<td>Ubiquitous crystallization process (UCP)</td>
</tr>
<tr>
<td>Gaithersburg, Maryland</td>
<td></td>
</tr>
<tr>
<td>DOE Contract No. DE-F101-80ET 23197</td>
<td></td>
</tr>
</tbody>
</table>

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## LARGE-AREA SILICON SHEET TASK

### Shaped Sheet Technology

<table>
<thead>
<tr>
<th>Contractor</th>
<th>Technology</th>
<th>JPL Contract No.</th>
</tr>
</thead>
<tbody>
<tr>
<td>Mobil Tyco Solar Energy Corp.</td>
<td>Edge-defined film-fed growth (EFC)</td>
<td>955843</td>
</tr>
<tr>
<td>Waltham, Massachusetts</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Westinghouse Research</td>
<td>Dendritic WEB growth (WEB)</td>
<td>955843</td>
</tr>
<tr>
<td>Pittsburgh, Pennsylvania</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Honeywell Corp.</td>
<td>Silicon-on-ceramic (SOC)</td>
<td>954356</td>
</tr>
<tr>
<td>Bloomington, Minnesota</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

### Material Evaluation

<table>
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<tr>
<th>Contractor</th>
<th>Description</th>
<th>JPL Contract No.</th>
</tr>
</thead>
<tbody>
<tr>
<td>Applied Solar Energy Corp.</td>
<td>Cell fabrication and evaluation</td>
<td>955089</td>
</tr>
<tr>
<td>City of Industry, California</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Cornell University</td>
<td>Characterization - Si properties</td>
<td>954852</td>
</tr>
<tr>
<td>Ithaca, New York</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Charles Evans and Associates</td>
<td>Technique for impurity and surface analysis</td>
<td>LX-694028</td>
</tr>
<tr>
<td>San Mateo, California</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Spectrolab, Inc.</td>
<td>Cell fabrication and evaluation</td>
<td>955055</td>
</tr>
<tr>
<td>Sylma, California</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Materials Research, Inc.</td>
<td>Partial pressures of reactant gases</td>
<td>955414</td>
</tr>
<tr>
<td>Centerville, Utah</td>
<td></td>
<td></td>
</tr>
<tr>
<td>University of Missouri, Rolla</td>
<td>Quantitative analysis of defects and impurity evaluation technique</td>
<td>955055</td>
</tr>
<tr>
<td>Columbia, Missouri</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

### INGOT TECHNOLOGY

**Crystal Systems:** The Schmid-Viechnicki technique (heat-exchanger method or HEM) was developed to grow large single-crystal sapphire. Heat is removed from the crystal by means of a high-temperature heat exchanger. The heat removal is controlled by the flow of helium gas (the cooling medium) through the heat exchanger. This obviates motion of the crystal, crucible, or heat zone. In essence, this method involves directional solidification from the melt where the temperature gradient in the solid is controlled by the heat.
exchanger and the gradient in the liquid is controlled by the furnace temperature. The overall goal of this program is to determine whether the heat-exchanger ingot casting method can be applied to the growth of large shaped-silicon crystals of 30-cm-cube dimensions of a quality suitable for the fabrication of solar cells. This goal is to be accomplished by the transfer of sapphire-growth technology (50-lb ingots have already been grown), and theoretical considerations of seeding, crystallization kinetics, fluid dynamics, and heat flow for silicon.

Siltec and Kayex: In the advanced Cz contracts, efforts are geared to developing equipment and a process to achieve the cost goals and demonstrate the feasibility of continuous-Cz solar-grade crystal production. Siltec's approach is to develop a furnace with continuous liquid replenishment of the growth crucible accomplished by a melt-down system and a liquid-transfer mechanism with associated automatic feedback controls. Kayex has already demonstrated the growth of 150 kg of single-crystal material, using only one crucible, by periodic melt replenishment.

Semix: The semicrystalline casting process is a Semix proprietary process yielding a polycrystalline silicon "brick" capable of being processed into cells of up to 16% efficiency at AM1.

Crystal Systems, P. R. HOFFMAN, Silicon Technology and Siltec: Today most silicon is sliced into wafers with an inner-diameter saw, one wafer at a time. Advanced efforts in this area are continuing. The multiwire slicing operation uses reciprocating blade-head motion with a workpiece fed from below. Multiwire slicing uses 5-mil steel wires surrounded by a 1.5-mil copper sheath that is impregnated with diamond as an abrasive.

The multiblade slurry technique is similar to the multiwire slicing technique, except that low carbon steel blades (typically 1 cm in height and 6 to 8 mils thick) are used in conjunction with an abrasive slurry mixture of SiC and oil.

MATERIAL EVALUATION

Applied Solar Energy Corp. (ASEC): Proper assessment of potential low-cost silicon sheet materials requires the fabrication and testing of solar cells using reproducible and reliable processes and standardized measurement techniques. Wide variations exist, however, in the capability of sheet-growth organizations to fabricate and evaluate photovoltaic devices. It therefore is logical and essential that the various forms of low-cost silicon sheet be evaluated impartially in solar cell manufacturing environments with well-established techniques and standards. ASEC has been retained to meet this need.

University of Missouri, Rolla (UMR): UMR is investigating the effects of partial atmospheric pressures of oxygen on the reaction at the contact interface between molten silicon and fused silica in several of the ingot and shaped-sheet growth techniques.

Materials Research, Inc.: The current MRI sheet defect structure assessment effort includes a correlation of impurity distributions with defect
LARGE-AREA SILICON SHEET TASK

Structures in various sheet materials obtained from the ingot and shaped-sheet manufacturers.

Charles Evans and Associates and Cornell University are doing silicon-sheet impurity analysis and structure characterization, respectively, by electron beam techniques.

SHAPED-SHEET TECHNOLOGY

Mobil Tyco Solar Energy Corp.: The EFG technique is based on feeding molten silicon through a slotted die. In this technique, the shape of the ribbon is determined by the contact of molten silicon with the outer edge of the die. The die is constructed from material that is wetted by molten silicon (e.g., graphite). Efforts under this contract are directed toward extending the capacity of the EFG process to a speed of 4.5 cm/min and a width of 10.0 cm. In addition to the development of EFG machines and the growing of ribbons, the program includes economic and theoretical analysis of ribbon thermal and stress conditions.

Westinghouse: Dendritic web is a thin, wide ribbon form of single-crystal silicon produced directly from the silicon melt. "Dendritic" refers to the two wirelike dendrites on each side of the ribbon, and "web" refers to the silicon sheet that results from the freezing of the liquid film supported by the bounding dendrites. Dendritic web is particularly suited for fabrication into solar cells for a number of reasons, including the high efficiency of the cells in arrays and the cost-effective conversion of raw silicon into substrates.

Honeywell: The purpose of this program is to investigate the technical and economic feasibility of producing solar-cell-quality sheet silicon by coating inexpensive ceramic substrates with a thin layer of polycrystalline silicon. The method to be developed is directed toward a minimum-cost process for producing solar cells with a terrestrial conversion efficiency of 12% or greater. The method consists of applying a graphite coating to one face of a ceramic substrate, and dipping that substrate in molten silicon. The silicon wets only the graphite-coated face and thus produces uniform thin layers of large-grain polycrystalline silicon. A minimal quantity of silicon is consumed.
Encapsulation Task

INTRODUCTION

The objective of the Encapsulation Task is to develop and qualify one or more solar array module encapsulation systems that have demonstrated high reliabilities and 20-year lifetime expectancies in terrestrial environments, and that are compatible with the low-cost objectives of the Project.

The scope of the Encapsulation Task includes developing the total system required to protect the optically and electrically active elements of the array from the degrading effects of terrestrial environments. The most difficult technical problem has been the development of high-transparency materials on the sunlit side that also meet the LSA Project low-cost and 20-year-life objectives. In addition, technical problems have occurred at interfaces between elements of the encapsulation system, between the encapsulation system and the active array elements, and at points where the encapsulation system is penetrated for external electrical connections.

The encapsulation system also serves other functions in addition to providing the essential environmental protection: e.g., structural integrity, electrical resistance to high voltage, and dissipation of thermal energy.

The approach being used to achieve the overall objective of the Encapsulation Task includes an appropriate combination of contractor and JPL in-house efforts. These efforts can be divided into two technical areas:

(1) Materials and Process Development. This effort includes all of the work necessary to develop, demonstrate, and qualify one or more encapsulation systems to meet the LSA Project cost and performance goals. It includes the testing of off-the-shelf materials, formulation and testing of new and modified materials, development of automated processes to handle these materials during formulation and fabrication of modules, and systems analysis and testing to develop optimal module designs.

(2) Life Prediction and Material Degradation. This work is directed toward the attainment of the LSA Project 20-year-minimum life requirement for modules in 1986. It includes the development of a life-prediction method applicable to terrestrial photovoltaic modules and verification by application of the method to specific photovoltaic demonstration sites. Material degradation studies are being conducted to determine failure modes and mechanisms. This effort supports both the materials and processes development work and the life-prediction method development.
ENCAPSULATION TASK

SUMMARY OF PROGRESS

Materials and Process Development

Pottant Materials

Candidate pottants for development and evaluation over the next two years at Springborn Laboratories have been identified in anticipation of LSA Technology Readiness. These are divided by process. The lamination-process pottants are ethylene vinyl acetate (EVA), ethylene methyl acrylate (EMA), and a recently identified all-acrylic thermoplastic laminating film from 3M Co. The casting-process pottants are poly-n-butyl acrylate (PnBA), a polyurethane and General Electric Co.'s low-cost TRV silicon rubber. The 3M acrylic laminating film and the GE TRV silicone-rubber casting liquid will be given preliminary evaluations at Springborn, with actual development and fine tuning to be carried out by the respective material manufacturers. Future work will reduce emphasis on identifying new encapsulation material candidates and will increase emphasis on improving existing material candidates. This will be carried out by fabrication and testing of modules to improve materials in those areas of specific weaknesses that limit or affect module reliability and durability.

UV Absorbers

Dr. Otto Vogl of the University of Massachusetts is continuing work on UV absorbers by grafting reactions of 4-vinyl 2(-hydroxyphenyl) benzotriazole with various polymers. Reactions are carried out with carefully prepared and purified absorber samples. Preparation of 3-propenyl-phenol by pyrolysis is also being worked on for use in condensation of diazotized o-nitroaniline in an attempt to make 5-propenyl-IV directly. Preparation of the 5-propenyl derivative has been concentrated on the preparation of p-propenyl phenol by pyrolysis of bisphenol A. Condensation of a diazonium salt, possibly with a disubstituted bisphenol A to produce a product that can be pyrolyzed to obtain unsubstituted benzotriazole and propenyl-substituted benzotriazole, has been studied. All products (derived from bisphenol A and pyrolyzed) of this path are potential UV absorbers. A crude condensation product has been prepared and will be characterized. If identified, the sample will be sent to JPL for further evaluation.

A modified technique using vacuum-sealed tubes (allowing reactions to be carried out at about 200°C higher) instead of an open-flask system has been successful in grafting 4-vinyl tinuvin to polypropylene. Careful evaluation will be made of this method using fractionation and gel-permeation chromatography analysis. Additional grafting experiments will be carried out using other polymers (polymethyl methacrylate, PnBA), EVA copolymers, polycarbonate, and polyamides.

Technology transfer of the vinyl tinuvin process from the University of Massachusetts to Springborn Laboratories has been accomplished.

Laboratory-scale production of vinyl tinuvin (approximately 250 grams) was accomplished at Springborn. The next effort with the chemically
ENCAPSULATION TASK

attachable UV screening agent will be to demonstrate chemical incorporation into EVA and other candidate pottants.

Electrostatic Bonding

Ten electrostatically bonded (ESB) minimodule assemblies were received from Spire as required by contract. These are being distributed to outdoor weathering sites at JPL, Point Vicente, and Goldstone, and for JPL qualification testing and other scheduled tests. Five minimodule assemblies with mesh interconnects are scheduled to be received from Spire before completion of contract, about February 1981.

Module Design

Phase I module analysis work has been completed and Phase II certification testing has begun at Spectrolab-Hughes. A day-long technical presentation on Phase I work was presented at JPL on September 11, 1980, which was summarized at both the Module Durability and Life Testing Workshop on September 23, 1980, and at the 16th PIM on September 25, 1980. The Phase I computer analysis has identified nine encapsulation design principles useful to module designers. The principles involve design features relating to thermal, optical, structural, and electrical properties, all of which were highlighted at the PIM, and will be reported in the Spectrolab-Hughes Phase I report.

Illinois Tool Works has identified three areas of difficulty in producing a state-of-the-art performing solar cell: (1) ion-plated metallization will readily form an ohmic contact on phosphorus-enriched Si surfaces but not on boron-enriched surfaces; (2) RF heating of junctions leads to junction deterioration or promotion of metal diffusion to the junction (it is believed that RF junction heating can be stopped with the use of a Faraday cage), and (3) improper packaging for shipment of diffused but unmetallized wafers results in mechanical damage to the fragile and very thin active surfaces. All of these problem areas are being worked on.

Bonding and Primers

Springborn has supplied samples of essentially all of the candidate encapsulation materials to Dr. Edward Plueddemann for identification of appropriate primers and adhesion systems, including EMA and PnBA. A primer for EVA has already been worked out and is performing satisfactorily. Efforts have also been started to identify primers for coupling candidate antisoiling coatings to outer-cover films and glasses.

Material Degradation and Life Prediction

Photodegradation Model for EVA:

A new approach to polymer photodegradation modeling by the University of Toronto that has as its basis the prediction of chemical change occurring
ENCAPSULATION TASK

within the polymer system as a function of outdoor exposure time was
initiated. A preliminary photooxidation mechanism has been formulated and a
literature search of available rate data has been carried out.

A computer simulation package necessary to generate concentration-time
profiles from the mechanical model as well as a preliminary experimental
design of alkane photooxidation studies has been completed.

A new gas-chromatography photolysis diagnostic technique using a
continuous-wave Hg-Cd laser to irradiate weathered polyurethane samples and to
monitor carbon monoxide evolved has been developed and assembled at Toronto.
Preliminary studies on the development of an automatic sequential sampling
system for the 50 to 100 solid samples have also been carried out. The
development of this instrument would permit early detection of early
weathering damage in solid plastic samples and give data necessary to test
computer models.

An automatic viscometer has been demonstrated by sequential routine
measurements of both solvents and polymer solutions. Preliminary measurements
of weathered samples of EVA (clear and white) supplied to Toronto by
Springborn indicate that there is an increase in the viscosity of solutions of
the polymers (exposed outdoors in Toronto, April-October) compared with the
unweathered samples. Viscosity tests are continuing.

Initial experiments on the photooxidation of n-decane as a model for
polyethylene are being done. The gas-chromatograph conditions for effective
product separation to afford quantitative data for validation of the computer
model are being optimized.

Corrosion Diagnostics and Modeling:

A new method of rapid computer-aided analysis for ac impedance response
of solar arrays has been developed at Rockwell Science Center. This analysis
is being implemented to characterize mechanical damage efforts, corrosive
aging mechanisms and consequent performance degradation.

Three analysis methods have been developed for nondestructive evaluation
of impedance measurements of solar cells and solar arrays. These methods
include: (1) a current-voltage (I-V) response model, (2) a model for
distribution of impedance parameters, and (3) an analysis of frequency
dependence of ac impedance response.

These models can now be combined to provide a computer-based
interpretation of solar array performance in terms of ac impedance.

A particular cell-failure mode of cracking was analyzed by Rockwell
Science Center using Auger electron spectroscopic profiling. Although
cracking may or may not be induced by corrosive mechanisms, the void produced
by a crack is a potential region for concentration of electrolytic impurities
that aggravate the failure. Work at JPL has indicated that corrosion couples
with the cracking process.
ENCAPSULATION TASK

In order to investigate this possibility, an Auger profile of a fracture surface adjacent to the metallization was made on a sample supplied by JPL. The cell was cracked and exposed to light with intermittent soaks in distilled water. The front-surface metallization of the solar cell consisted of a Pb/Sn solder whose major components were Pb, Sn and Fe with observable quantities of S, Cl, K, O, Cr, Ni, and C. The substrate (back-surface) electrode is a Ni/Pb alloy.

After a 200-sec sputter of superficial organic contamination, the fracture surface of the Si shows primarily Fe, Ni, and Cr. The distribution suggests a migration of Cr and Fe species from the upper electrode, possibly as a result of a corrosive mechanism. Some migration of Ni is also indicated. The metals that have apparently migrated are expected to be the most active from a thermodynamic point of view since the thermodynamic tendency to electrochemical oxidation takes the order C Fe-Ni Pb Sn.

A full year's corrosion-monitor recordings have been accumulated at Mead, Nebraska; these experiments are being interrupted to return the corrosion monitors to the Science Center for calibration and analysis.

Fracture and Crack Modeling:

The TEXGAP program, a FORTRAN-coded finite-element computer program, is being procured from the University of Texas. The main feature of the program, not available in existing commercial programs, is the availability of a finite-element code that has been developed for the analysis of cracks in structures due to differential temperature loading. The program will be used to predict the stress-intensity factor at the tip of a crack or at the interface between two dissimilar materials of a solar array. The results of this analysis will be used for solar array life prediction.

The mechanical modeling of modules has continued in house as follows:

(1) A series of computer analyses with various material properties and thicknesses of encapsulants has been completed. The data are being compiled and analyzed.

(2) A study investigating the stresses in cells bonded directly to the support frame (minimum thickness of adhesive) has been completed.

(3) An extension of (2) is in progress to study the effect of thickness of adhesive on the stresses in cells.

Module Life Testing:

Validation of the Battelle accelerated-test plan* continued in house through 40 days of accumulated test time. Fatigue cracks appeared in some of

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ENCAPSULATION TASK

the interconnects. One module exhibited an electrical open at +950°C. Electrical power output curves, however, were normal for all modules at ambient temperature.

Nine types of minimodules being weathered at the JPL site have endured six months of weathering with no visual degradation and no significant reduction in electrical output except that two of three Springborn-Solar Power minimodules with EVA potting and Super Dorlux (a wood product) substrates showed reductions of maximum power output of 67% and 33%. Failure analysis showed the cause to be cracked cells (three and one, respectively). It is assumed that the cell cracks were caused by humidity expansion of the Super Dorlux substrate. It is not known whether the cells were cracked during manufacture with humidity expansion widening the cracks, or cracks were initiated by the humidity expansion. An in-house program is under way to determine the temperature and moisture characteristics of Super Dorlux.

Two Controlled Environment Reactors (CER) have been constructed and tested in house. They were shipped to Springborn Laboratories (October 29, 1980) for accelerated weathering of sample modules. The CER provides acceleration of UV radiation up to 30 suns while maintaining temperature (+10°C) on the absorbing surface between 30°C and 60°C. It is equipped with rain and fog nozzles.

It was discovered that ventilation is extremely important during accelerated weathering. Springborn was instructed to purge the system continuously during testing using air, N₂, or any other gas mixture. The CER testing temperature range can be expanded to 100°C by installing a heating unit. Installation instructions were given to Springborn. An inspection of available accelerated testing facilities (RSA sun lamp) was also made and advantages of CER over RSA sun lamp were discussed.
PRODUCTION PROCESS AND EQUIPMENT AREA

AREA OBJECTIVES

The Production Process and Equipment Area is chartered to work with the Large-Area Sheet Task, the Encapsulation Task and the Engineering Task by selecting and developing manufacturing processes and by developing trade-offs designed to minimize the cost per watt of assembled solar modules. This work is divided into the phases shown in the figure below. At present PP&E is on schedule with Phase III, the design and development of equipment leading to demonstrations of 1982 Technical Readiness.

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Production Process and Equipment Area Phase Schedule

SUMMARY OF PROGRESS

The main Phase II efforts, the MEPSDU contracts with Solarex and Westinghouse, are under way and are approaching preliminary design reviews. Major milestones have involved approval of program plans and work breakdown structures.
Light-Trapping Concept

- USE OF HIGH INDEX OF REFRACTION MATERIALS
- DIFFUSELY REFLECTING INTERCELL AREA

Light Trapping by Diffuse Reflection in Thick Film

DIFFUSE LIGHT TRAPPING IS ACCOMPLISHED WHEN AN INCIDENT RAY ENTERS A HIGHER INDEX TRANSPARENT LAYER AND IS SCATTERED.

AN EXAMPLE RELATED TO PHOTOVOLTAIC MODULES IS SHOWN BELOW:
Process Sequence Development

An evaluation of approximately 500 advanced-Cz wafer samples indicated that excessive saw damage and microcracking result in a loss in electrical and mechanical yields.

Both Phase III contracts (Solarex and Westinghouse) were signed on November 26, 1980. These are two-year contracts culminating in the demonstration of Technical Readiness by 1982.

A contract was started with Motorola to investigate problems associated with processing non-Cz Si material into solar cells. The processes developed under Contract No. 954847 will be applied to this material. The contractor has agreed to investigate these processes on several non-Cz substrates, e.g., RTR and web.

Westinghouse has characterized its ultrasonic bonding of 0.001 aluminum foil with regard to the sintering of the cell metallization, the bonding pressure and power setting, and the resulting bond pull strength. The ultrasonic seam bonder was moved from Kulicke and Soffa (K&S) to their AESD Division. The seam-bonding test will be conducted at AESD by Westinghouse personnel.

Junction Formation

Spire Corp. has progressed through the construction phase of the PEBA (Pulsed Electron Beam Annealer). This machine is designed to anneal ion-implanted junctions at a rate of 10 MW/yr. Preliminary testing has been encouraging and final adjustment work has begun.

The effects of non-mass-analyzed beam parameters have been established. Sixty 2 x 2-cm samples were ion implanted without mass analysis in August and were sent to Applied Solar Energy Corp. for processing and testing. These cells were AR coated but have no back-surface field. In addition, data indicated a lack of sensitivity to implant energy over a range of 5 to 15 KeV. A reduction in dose increased the sheet resistance linearly. ASEC says that the metallization system could be optimized to achieve a fill factor of 0.76 without losing active area, up to a sheet resistance of about 500 ohms per square. This corresponds to a dose level of about 2 x 10^{14} atoms/cm^2.

Lockheed has successfully laser annealed back-surface fields, as well as front cell junctions, using their quartz 90° light-pipe homogenizer on the neodymium glass laser.

Metallization

The Solarex development effort to plate nickel directly on silicon has ended. PP&E is concerned about the marginal results of temperature cycling of sample cells. Efforts to verify this process in the PP&E laboratory have failed to obtain good adherence to cell p⁺ (Al BSF) surfaces. More work is necessary to ready this process for production.
Spectrolab has modified its previous process sequence to remedy problems with the Midfilm process. The junction cleanup step (laser scribing) is now being performed after the metallization step instead of after the junction formation step. This alleviates problems with the metal shunting the edge of the junction. The Ag powder (four types)-resin (three types) matrix has been completed with the best results obtained using 95% Thick Film Systems (TSF) spherical powder with 5% 3347D TFS frit and the newly formulated Ferro RG4933 resin, which is less humidity-sensitive. Early results gave unacceptable high series resistance ($R_s$) readings. The probable cause was insufficient removal of the resin from under the collector grid. Experiments involving time, temperature, pre-baking and oxygen content have produced $R_s$ of 31 m$\Omega$, down from the unacceptable 80 m$\Omega$ range.

Bernd Ross Associates has terminated AVX as a subcontractor for ink formulations. In order to provide more insight into the process variables and their tolerances, a more detailed study of the fabrication of the pastes is being carried out. A facility that will allow complete control of material and processes by contract scientific personnel is being developed. Since silver fluoride is the most problem-prone component of the present base-metal paste, and since it was one of three SiO etching agents during the initial Contract No. 955164, it is of interest to examine some of the other materials in combination with base-metal pastes. The first such material is Teflon powder. This is a deviation from the original program plan.

Assembly

Kulicke & Soffa has requested and received permission to exhibit the solar module assembly-line machine, developed under PP&E near-term cost-reduction contract, to prospective buyers at their Horsham facilities, and at the IEEE PV Conference in Florida. K&S will pay all transportation costs.

ARCO Solar is continuing work to debug the automated soldering machine. The ribbon-feed mechanism is being reworked at Albuquerque Laboratories to achieve more uniform cell-to-cell spacing. Final cell-to-interconnect alignment adjustments will follow after the spacing problem has been solved. The contractor hopes for a verification demonstration run in February 1981.

JPL has stressed that Science Applications Task I, the Optical Design Rules task, should receive relatively more emphasis than Task II. During November the Task I work studied more cases of minimum-design-change modules. Work on the Task II cost-analysis area was continued. Based on preliminary test data, the optimum packing fraction for modules was calculated as a function of time. Results indicate that by using white diffuser optical concentration, the 1979 cost of field-installed arrays can be reduced by a factor of 0.63. These calculations are based upon present array costs of $5.68/W, structure costs of $8.00/m$^2$, and land cost of $5.40/m$^2$.

The final report from ASEC on the high-efficiency p/n cell and module assembly contract has been approved. Tooling developed on this contract is deliverable. This tooling was used for fabrication of modules for the JPL Block IV purchase and was shipped to PP&E when no longer required.
Tracor MBA is continuing development of its automated laminating station. This station has three major components: (1) the vacuum-platen end effector used for robotic transfer of cell arrays and sheet materials, (2) the lamination preparation station, and (3) an automated lamination chamber. The vacuum platen has been built and tested. The platen can pick up, by means of its 35 vacuum cups, a 1 x 4-ft array of interconnected cells, glass and finished modules. All detail components of the automated lamination station are on order or are being fabricated in house at Tracor MBA.
INTRODUCTION

During the reporting period, activities within the Engineering Area emphasized array requirements generation, array subsystem development, array component engineering, module specification and test requirements development, and performance criteria and test standards development. A summary of Engineering Area in-house and contracted efforts in these areas of activity is presented in the Proceedings section of this document. An expanded description of the status of each of the Engineering Area contracts was included in the 17th PIM handout. Active contracts are listed on pp. 35-36 below.

ARRAY REQUIREMENTS

A in-house investigation of array maximum power point fluctuation during the normal range of operating conditions has been initiated. Selection of the optimum input voltage window for power conditioning is influenced by the array voltage fluctuations due to site weather conditions. SOLMET Typical Year data tapes are now being used to generate yearly array power output for 26 sites as a function of irradiance level and cell temperature. Since the voltage at maximum power of an I-V curve is a function of temperature and since the maximum power output is a function of both temperature and irradiance level, the fraction of yearly power generated for a given voltage range can be determined. The optimum voltage range (expressed as $\Delta V/V$) for a power conditioner is the minimum $\Delta V/V$ for which a desired fraction of available power is actually within the operating range (input voltage range) of the power conditioner. These data will be developed for both fixed-voltage and maximum tracking arrays.

In conjunction with the 17th PIM, an industry workshop on Module and Array Safety was conducted jointly by LSA Engineering and Underwriters Laboratories at JPL on February 3, 1981. A broad spectrum of module manufacturers, systems designers and PV users were represented by 100 workshop participants. The presentations and discussions centered on a draft version of an interim safety requirement document that had been jointly prepared by JPL and UL and forwarded in advance to workshop pre-registrants. Proposed requirements and test methods were described in detail. A significant result of the workshop was a clarification of the roles of UL and the NEC and the positive influence of early development of safety requirements on user acceptance of PV systems, especially for residential and ILC applications.

Also in support of the development of module safety requirements, JPL has recently completed an assessment of requirements concerning the ability of the capacitance of a photovoltaic module to hold a hazardous charge after extraction of the module from a high-voltage array. Results to be presented in the workshop indicate permissible capacitance levels from cell string to module ground. Current modules easily meet the requirements.

Carnegie-Mellon University, which had an LSA contract to perform an exploratory study, "Safety and Product Liability Considerations for
ENGINEERING AREA

Photovoltaic Modules and Panels," released the final report, DOE/JPL 955846-81/1, in January. The report addressed legal issues as they apply to module design, manufacture and application and suggested a methodology to be used during design of a photovoltaic module or array to eliminate or minimize perceived hazards.

Burt Hill Kosar Rittelmann Associates completed work on the study of commercial-industrial PV module and array code requirements. Preparation of the final report was initiated, with release scheduled March 30, 1981.

Results from the second part of the wind-tunnel tests have been received by the Boeing Co. The increased end-loading problem described in the September report can be reduced 50% to 70% by putting end plates on the arrays. The dynamic pressure data are being analyzed by Boeing. The Phase IV effort was initiated and the dynamic modes of two possible configurations have been determined as well as the seismic loads for those configurations. A draft of the Phase III report was received in January and is scheduled for release in March, 1981.

ARRAY SUBSYSTEM DEVELOPMENT

A design data package describing the large ground-mounted array displayed at the 16th PIM was completed including detailed panel and array structure design drawings. JPL Drawings 10097880, 10097881, and 10097882 provide sufficient detail to permit adaptation to a variety of module configurations. Copies are available from the LSA Engineering Area. A task report documenting the overall structure design effort is in press. In addition, a descriptive brochure, JPL No. 400-104, "JPL Low-cost Solar Array Structure," January 1981, was prepared for release and general distribution by DOE to interested photovoltaic-industry participants.

Contracts for the integrated residential photovoltaic array development effort have been signed with the AIA Research Corp. (JPL Contract No. 955893) and the General Electric Co. (JPL Contract No. 955894). The effort addresses the optimization of the PV array subsystem-roof interface and delivery of a prototypical section.

AIARC sponsored an eight-hour workshop on January 12, 1981, for the subcontractors performing the conceptual design work associated with the Integrated Residential PV Array Development effort. The objective of the workshop was to provide a consistent basis for the design effort and to answer questions and concerns with respect to the design boundary conditions and assumptions relative to cost.

General Electric Co. has completed a preliminary evaluation matrix of 19 residential array concepts, which were combined into 14 distinctively different module/array types. Thirty-nine evaluation criteria were grouped into seven broad categories and used to rank the concepts. Results of a preliminary assessment indicate that direct-mounted, overlapped shingle-type installation ranked highest.
ENGINEERING AREA

ARRAY COMPONENT ENGINEERING

The module soiling studies report was published and distributed during this reporting period. The report, JPL Publication No. 5101-131 (DOE/JPL 1012-41), Photovoltaic Module Soiling Studies May 1978-October 1980, November 1, 1980, describes the results to date of the in-house experimental study to characterize and understand the effects of outdoor contaminants on sensitive optical surfaces of flat-plate photovoltaic modules and cover materials. This report is available through the LSA Data Center and NTIS.

A task report (JPL Publication No. 5101-163), Determining Terrestrial Solar Cell Reliability, which documents the proceedings of the solar cell reliability workshop held May 1-2, 1980 at Clemson University, Clemson, South Carolina, was published during this reporting period. Included in the report are reproductions of graphic presentation materials and highlights of discussions related to solar cell reliability test methods. The report is available from the Data Center or from NTIS as Report No. DOE/JPL 954929-81/8. In the follow-on phase of cell reliability testing at Clemson there will be a strong focus on those cell types and metallization systems that will be used in modules designed for residential application demonstrations. This activity will be coordinated through MIT-LL.

During this reporting period, the series-parallel effort concentrated on the development of a hot-spot qualification test and, in turn, a better understanding of the operation of cells under back bias conditions. Several problems in connection with the analytical prediction of hot-spot problems and subsequent correlation of these results with tests are under investigation. These include the significance of power dissipation in a cell relative to the cell area, uniformity of power generation loci, and the uniformity of the light beam over the surface of the cell under test. The infrared camera equipment is being used to determine the temperature gradients over the surface of test cells. A hot-spot qualification test has been included in the Block V procurement package and test results were presented at the 12th PIM.

The solar cell fracture-mechanics effort continued during this reporting period. Optical microscopy and SEM examination of solar cells from Applied Solar Energy Corp. that were fracture-mechanics tested indicated that the fracture-initiating flaws for these cells are edge chips and cracks, some of which were not observed before the fracture testing. These cracks were sometimes covered by metallization and AR coating and were not obvious. A quantitative correlation of fracture strength and flaw size is under way.

A major effort in examining the mechanical fatigue life of cell interconnects is also continuing. The predictive model presented at the last PIM correlated well with interconnect failures experienced at Schuchuli, Arizona. Applying this failure prediction technique to similar modules at the Mead, Nebraska, site indicates that interconnect-fatigue problems should be expected there within two years. During the reporting period, an interconnect-fatigue cycling apparatus was fabricated and large numbers of interconnects tested to failure. Several additional configurations will be tested in the future. In the meantime a formal cost-optimal-design algorithm has been developed and its practicality demonstrated. The algorithm yields 20-year array power reduction and required interconnect redundancy to achieve
minimum life-cycle energy cost. Future work includes refining the algorithm (based upon additional interconnect tests) and developing charts and nomographs from which to compute interconnect strain levels (without the substantial cost impact of using a finite element computer code). An expanded predictive module based on observed probabilistic failure statistics together with the test data was presented at the 17th PIM.

In the area of PV/thermal module development, tests were completed on an unglazed PV/T module configuration to verify the feasibility of a PV/T test method proposed as part of the IPC. Preliminary indications are that the test method will be applicable to a variety of collector types and configurations. Work has been initiated on a joint task report with Arizona State University to document the background and rationale for the electrical and thermal performance test methods being developed for flat-plate PV/T and concentrator modules.

In the area of environmental test development, evaluation of the use of a "greenhouse" effect accelerated aging environmental exposure technique is continuing. After 75 days of exposure, minimodules from the outdoor hot box test have been taken down, inspected, flashed and tested for voltage breakdown. There has been some cosmetic degradation of several of the modules, but no electrical degradation. The post-exposure voltage breakdown test results are being studied. The modules are back in the hot box for further exposure.

In the Voltage Isolation Task a variety of activities continued. The low-voltage film breakdown apparatus fabrication is in progress. Sheldahl delivered the test samples on February 3, 1981. The order was placed for the Biddle Partial Discharge Test apparatus, with delivery scheduled for October 1981. Cell-string flaw-characterization test fixture fabrication was completed and initial air-gap and film-breakdown tests will begin after the 17th PIM. Several material test samples were received for electrical isolation capability testing including hardcoat anodized aluminum plates (intended for PV/T collector substrates) and laminate sections representing the Motorola Block IV design back surface composite. Humidity sensors and monitors were received and mounted in modules that will be installed at the JPL Field Site No. 1 High Voltage Facility. The decision was made to expand the test voltage capability to 3000 Vdc and to add a second test rack at this facility. Work on the facility modification is in progress.

IIT Research Institute released the first quarterly report on LSA Engineering Area Support Contract No. DOE/JPL 955720-80/1, on development of elements of a reliability design guidebook for flat-plate photovoltaic modules and arrays. This report documents work performed and completed by IITRI through September 1980 on two subtasks. It is available upon request from the LSA Data Center.

The DSET Laboratories Spectral Measurement contract, which is gathering data on relative global vs direct vs diffuse irradiance for the New River, Arizona, site, demonstrated fully automatic solar spectrum data acquisition, reduction and curve plotting using their NOVA-30 computer. Solar spectrum measurements at resolutions ranging from 1 nanometer to 5 nanometers, depending on the portion of the spectrum being measured, have been initiated at regular monthly intervals and will continue over the next two-year period.
ENGINEERING AREA

MODULE SPECIFICATIONS

As part of developing design test and qualifications criteria for the Block V Module Production RFP, drafts were completed of both residential and intermediate-load specifications. The drafts, along with the new interim safety standard, were forwarded to approximately 80 PV industry participants on January 21, 1981, with a request for review and comments by February 10th. Release of the two specifications, JPL Publication No. 5101-161 for intermediate-load requirements and JPL Publication No. 5101-162 for residential requirements, was scheduled for February 20, 1981. Work was initiated on a preliminary draft of a Central-Station Application Preliminary Specification.

PERFORMANCE CRITERIA AND TEST STANDARDS

The Array Subsystem Task Group met in Huntsville, Alabama, on November 19 and 20, 1980. The Electrical Performance Subgroup of the Array Subsystem Task Group met in October and November 1980, and January 1981. Test methods for actively and passively cooled concentrator modules were reviewed. Principal issues were: (1) the appropriateness of using reference cells for the I-V characterization of concentrator modules; (2) the advantages and disadvantages of several different formats for presenting electrical and thermal performance data; (3) new criteria in safety and durability and test methods for salt spray and SO₂.

The PV/Thermal Subgroup of the Array Subsystem task group met in Huntsville on November 18, 1980 at Wyle Laboratories. The subgroup discussed a draft of the Operating Cell Temperature Determination Test for Flat Plate Actively Cooled Modules and several performance criteria statements. A final version of the test method was prepared for the Task Group. Several of the criteria statements were also prepared for final review by the Task Group.

In support of the SERI-funded JPL standards efforts, Wyle Laboratories was awarded a contract to identify and document corrosion sensitivities and failures associated with outdoor exposure of photovoltaic modules and components and to document performance criteria and candidate test methods for inclusion in TPC-2. A data package on the corrosion observations at JPL field site prepared by LSA Quality Assurance was delivered to Wyle.

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Engineering Area Contractors

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OPERATIONS AREA

MODULE PRODUCTION TASK

Block IV Design and Qualification

Applied Solar Energy Corp., Motorola, Inc., Solar Power Corp., and Spire Corp. have completed work on the design and qualification phase of this task. ARCO has delivered intermediate-load modules for testing, but has not yet completed an approved set of drawings for the residential module; hence, residential modules have not yet been fabricated for test. Photowatt has delivered intermediate-load modules that are now in the environmental test sequence. Solarex Corp. has provided both residential and intermediate-load modules for testing but a completely satisfactory lamination sequence has not yet been demonstrated.

The physical features, encapsulation systems, cell features and electrical characteristics of these modules are tabulated in the Proceedings of the 17th PIM and are to be considered a part of this Progress Report (see pp. 71-74). A summary of the problems encountered in the course of the qualification testing and a brief summary of price analysis also appears in the Proceedings (see pp. 75-81).

Generally, the following observations and conclusions hold:

-- New design and technology were assimilated, but with some difficulty. Schedules slipped, tests were failed, and there were a few retreats to conventional approaches.

-- Large-scale production was not tested.

-- Prices are down; efficiencies have risen; reliability and durability appear to have improved because of better hail protection, improved moisture protection and fault-tolerant cell-circuit arrangement.

-- Most designs are to be offered commercially.

Block IV Production

Although purchase orders have been issued to six of the eight participants in the Block IV design phase, modules have been received from only two contractors. Motorola has delivered all but 10 modules ordered and will be the first contractor to complete the order. Solar Power has provided seven modules of a commercial configuration to be tested in lieu of the module designed under Block IV. ASEC, GE and Spire are in the fabrication mode. Solarex has not yet been given the go-ahead, since the drawing packages are not approved. ARCO Solar and Photowatt purchase orders have not yet been issued, and await qualification testing of the modules under Phase I.
Block V

The Block V RFP was prepared and made ready for issue, but was held back because of rebudgeting.

MODULE TEST AND EVALUATION

Environmental Testing

Two special series of tests were run in this period, both related to the Block V specifications. One of these was an extended sequence of thermal cycling tests of various modules to determine susceptibility to interconnect-fatigue cracks. This test was initiated after interconnect failures of Block II and III modules (Y type) in the field in less than two years. In the long-term temperature-cycling tests, opens occurred in Y-type modules in less than 100 cycles and in V-type Block III modules in less than 200 cycles. The proposed Block V 200-cycle temperature test should effectively uncover field interconnect problems that might occur in the first two to four years.

The other special test was the proposed Block V humidity cycling test. Results were reported by John Griffith at the 17th PIM (see p. 373). This single test is more effective than the Block IV temperature and humidity tests combined, both in severity and in the variety of degradation observed.

Tests have been completed on World Bank modules and results were also reported at the PIM (see p. 373).

Other environmental test results are summarized in the following tables. Modules tested include Block IV MIT-LL Residential Experiment Station (RES), and two commercial types (one with CdS cells).
## Recent Qualification Test Results

<table>
<thead>
<tr>
<th>VENDOR CODE</th>
<th>Construction</th>
<th>Prinicipal Problems</th>
</tr>
</thead>
<tbody>
<tr>
<td>RS</td>
<td>Glass, PVB, Tedlar/Al/Tedlar; Modified edge sealant includes glass tape and a butyl tape between laminate and SS frame</td>
<td>This latest version passed all hi-pot tests; backing material delaminated at J-box area</td>
</tr>
<tr>
<td>US</td>
<td>Glass, PVB, Tedlar/steel/Tedlar; steel backing now grounded to frame</td>
<td>Earlier ungrounded back surface modules failed hi-pot but this latest version passed; edge sealant extruded from ends of modules during temperature cycling</td>
</tr>
<tr>
<td>VS</td>
<td>Glass, PVB, Tedlar/Al/Tedlar, Al frame</td>
<td>Modules were electrically unstable with variations to +4%; many cracked cells found in the first to be received; after temperature cycling, there was frame separation at the corner of one, terminal covers loosened and fell off, some delamination at frame seal, 2 cell cracks</td>
</tr>
<tr>
<td>YR, YS</td>
<td>Glass, EVA, Tedlar</td>
<td>Latest set of two modules each have completed temperature and humidity cycling; in temperature cycling, frame seal delamination and Tedlar delamination and blistering occurred; all four modules degraded electrically in humidity cycling--10, 14, 16, and 45%, respectively; internal shorting was discovered in one; some cells moved closer and are touching</td>
</tr>
</tbody>
</table>
**OPERATIONS AREA**

Recent Qualification Test Results (Continued)

<table>
<thead>
<tr>
<th>MIT-LL Res Program/ Application Area</th>
<th>Construction</th>
<th>Principal Problems</th>
</tr>
</thead>
<tbody>
<tr>
<td>MB/NE</td>
<td>Glass, PVB, Tedlar</td>
<td>J-Boxes came loose, warped; terminal strip loosened; backside Tedlar delamination</td>
</tr>
<tr>
<td>YB/NE</td>
<td>Glass, EVA, Tedlar</td>
<td>Tedlar delamination and blistering, encapsulant air bubbles in temperature</td>
</tr>
</tbody>
</table>

Recent Commercial Module Test Results; Temperature and Humidity Cycling Only

<table>
<thead>
<tr>
<th>Vendor Code</th>
<th>Construction</th>
<th>Results</th>
</tr>
</thead>
<tbody>
<tr>
<td>BN</td>
<td>Glass, encapsulant, Al substrate and frame</td>
<td>Satisfactory after temperature cycling</td>
</tr>
<tr>
<td>BV</td>
<td>Clear acrylic, silicone gel encapsulant, white acrylic substrate, Al side rails</td>
<td>Catastrophic failure in temperature cycling; acrylic substrate corners broken, one cover sheet broken, delamination and bubbles over cells, electrical failures (18%, 29%, 50% and 52% loss, respectively)</td>
</tr>
<tr>
<td>EB</td>
<td>Glass, PVB, CdS cells, plastic screen, copper pan, paint; hermetically sealed</td>
<td>In temperature cycling, encapsulant bubbles developed at ends of cells; voltage-regulator plastic covers melted; one module has 25% power loss after humidity cycling; electrical measurements made in natural sunlight because of slow response time of CdS; power increased at low ambient temperatures after tests but stayed nearly the same at about 60°C</td>
</tr>
</tbody>
</table>
Performance Measurements

The spectral response of cells presently used for Block IV modules manufactured by ASEC, GE, and Photowatt do not match that of the reference cells now in use. New reference cells are being selected, fabricated and calibrated. Reference cells are also being selected, fabricated and calibrated for MIT Lincoln Laboratory to be used for testing ASEC, ARCO Solar, Inc., Solec International, Inc., Solarex, Motorola and Spire (photovoltaic/thermal) modules.

LAPSS 2 is functioning properly and is being used for module evaluation. Four types of modules with a maximum power of from 20 to 60 watts were measured using LAPSS 1 and LAPSS 2. Results indicate that LAPSS 1 $P_{\text{max}}$ measurements average 1.2% higher than LAPSS 2 $P_{\text{max}}$ measurements. Most of this difference is attributed to a similar difference in the measurement of module current ($I_{\text{sc}}$ and $I_{\text{mp}}$). This difference is considered to be within the normal measurement error of the system.

Field Tests

A draft of the annual report for the year ending August 31, 1980, is in press and is expected to be distributed by mid-February. The key conclusion from analysis of the data covered in the report is that no fundamental life-limiting mechanisms have been identified that could prevent the 20-year life goal being met.

Preparation began for deployment of the Block IV modules. To accommodate these modules a reorganization of the test site network is underway:

-- Eight of the Continental Remote sites -- Canal Zone, Key West, New Orleans, Houghton, New London, Albuquerque, Fort Greely (Alaska), and Mines Peak -- will double in size from four to eight 4 x 8-ft test stands. Most of the Block II modules will be removed and replaced with Block IV intermediate load modules; approximately four of each type will be deployed.

-- The operating mode at the Continental Remote sites at Seattle, Crane, San Nicolas Island, and Dugway will be changed to one of reduced activity. No Block IV modules will be deployed and the scheduled yearly acquisition of performance data on the remaining Block II modules will occur as time is available.

-- At the local remote sites, Goldstone, Point Vicente, and Table Mountain, all of the Block I modules and about half of the Block II and III modules will be removed and replaced with the same quantity and type of intermediate-load modules as deployed at the Continental Remote sites. In addition, small arrays composed of Block IV residential modules will be deployed.

-- At the JPL site, approximately 85% of the Block I modules and 70% of the Block II modules will be removed. The quantity of Block IV modules to be deployed will be two to three times the number at the
Operations Area

Local remote sites. The residential modules will be mounted as roof-section arrays on the large support in the northeast corner of the field.

On December 22, 1980 a diffuse-sky shadowing experiment was conducted at the JPL test site to confirm results obtained the previous year by the Performance Measurement Group. The purpose of the experiment was to determine the difference in insolation from the top to the bottom of a test subarray that is located behind (north of) another subarray. The difference is attributable to the shadowing of a portion of the sky by the forward subarray. All data were taken within 15 minutes of solar noon. The sky was hazy with high cirrus cloud formations. Insolation varied between 80 to 90 mw/cm² during the test period. A Li-Cor pyranometer was placed at the top of the array while a reference cell was moved down the subarray face in 6-in. increments. Readings from both instruments were recorded simultaneously. The subarrays were tilted 50° during the test period. The results, shown graphically in the following figure, indicate that the insolation at the bottom of the subarray could be as much as 13% less than at the top for the conditions stated and that the loss of insolation is almost linear as a function of the fraction of the sky below the sun that is shadowed or blocked out. This experiment will be repeated for other sky conditions.
OPERATIONS AREA

Failure Analysis

Analysis of a number of modules returned from Mead, Schuchuli, and Mount Laguna from one Block II and III manufacturer were found to have broken cell interconnects and opens due to cracked cells. The interconnect was found to have failed because of improper interconnect stress-relief loop forming, short active length for flexing, and thermal mismatch between the polyester glass substrate, the cell, and the copper interconnect. MIT Lincoln Labs also returned 20 modules from the Natural Bridges National Monument Application for analysis. Sixteen of the module failures involved shorts to ground, which were caused by the interconnect foil contacting ground, generally between the edges of the foil and the metal substrate or in the terminal area. The 17th PIM presentation on shorts to ground covered this problem in detail (see pp. 399-410). Three laminated-design modules with broken cover glasses were found to have edge chips, which initiated fractures during diurnal temperature cycling. One module failed due to a cracked cell, which fractured both main current collectors on the front surface of the cell. There was also a notable amount of discoloration at cell edges and where cell cracks existed in this PVB-encapsulated module.

The Mount Laguna Solar array was visited in January 1981. The number of 30W modules in the bypass mode (open-circuited) has increased from 128 in August 1980 to 160 in January 1981. The 20W module bypass increased from 14 to 20 during the same period. The next on-site evaluation is planned for July-August of 1981. It is expected that the latter module bypass rate will show a further increase at that time, since the predominant failure mode (fractured interconnects) tends to show open circuits at elevated temperatures.

Applications Interface

Test and Applications Project support provided:

-- Attendance and follow-up support to 22 reviews (Quarterly and Critical) at both Sandia for PRDA applications and Lincoln Laboratory for residential applications.

-- Coordination and follow-up support of module failure analysis activity as associated with field failures at various MIT-LL and Lewis Research Center installations.

-- Coordination of field survey of the PV installation at Mount Laguna.

-- Received modules from PRDA and residential applications for qualification testing.

-- Received and processed requests from Lincoln Laboratory for 10 reference cells to support the current residential applications. Number of required cells will probably increase as more experiments are undertaken. Sandia’s request for 40 reference cells (to support concentrator PRDAs) has been received and is being discussed with Sandia.
Proceedings Summary

Highlights of the 17th Project Integration Meeting held February 4 and 5, 1981, at the Pasadena Center, Pasadena, California:

The first day of the meeting consisted of a summary of a panel discussion on the Role of Government in Photovoltaics by invited industry executives and JPL management at The California Institute of Technology on the previous day. Highlighted were consensus items such as the need for emphasis on central-power-station demonstration work, continued underwriting of high-risk research and technology development, and the agreement that while $0.70/W modules will be produced, debate persists on whether that will be the common selling price in 1986.

In addition, the first day's session presented a summary of Union Carbide Corp. Si refinement activities. Also presented was a summary of the hydrogenation work on silicon tetrachloride being done by MIT and the significance of that work on the potential improvements in conventional Siemens deposition processes.

A summary was also presented on the results of approximately two and a half years' work in near-term cost-reduction activities. Numerous predicted cost reductions were realized through the contract actions that were completed.

A comprehensive discussion was held on encapsulation materials and design principles for photovoltaic module encapsulation packaging. Various aspects of material characteristics, compatibility with module requirements, lifetime potential and costs were presented.

The results of a Safety Design Workshop held the previous day were presented, highlighting the many safety considerations under study by LSA and its principal safety contractor, Underwriters Laboratories. Specific engineering procedures have been developed as a result of this work, which is still under way.

Block IV module procurement results were presented regarding physical and performance characteristics and attention was invited to the definite improvements over previous module purchases by LSA.

Presentations were made by both Westinghouse and Solarex on their MEPSDU contracts. Considerable interest was shown by the audience in both contract efforts, then just starting.

The computerized price estimation technique, IPEG4, was demonstrated to illustrate the flexibility of this new analytical tool. Example analyses were manipulated by audience request in real time.
Participants were privileged to hear two notable speakers. Eddie Mlavsky, for many years directly involved in the U.S. Photovoltaics Program, discussed some international perspectives on photovoltaics that were of interest in view of his work in Israel during the past two years. Paul MacCready presented an exciting film and a talk on his adventures and successes with the Gossamer Penguin and with the Solar Challenger photovoltaics-powered light aircraft.
Union Carbide reported on the status of development of the silane (SiH₄)-to-silicon (Si) process. An experimental process system development unit (EPSDU) with a Si capacity of 100 MT/yr is being constructed at East Chicago, Indiana. All foundations were completed, the structural steel for the process gantry was erected, and all underground utilities and service lines were installed. Process equipment is being fabricated, with delivery of some items already taking place.

The free-space reactor process development unit (PDU) effort was successfully completed, with demonstration of long-term operability of the reactor.

Hydrochlorination of mgSi and SiCl₄ for Si Processes (MIT)

Development of a process for producing low-cost trichlorosilane (SiHCl₃), which is used to make SiH₄ in the Union Carbide process and from which Si is deposited in the conventional (Siemens) process for producing semiconductor-grade Si, was described by MIT. The study has shown the conditions under which the hydrochlorination reaction should be carried out. Copper was shown to be an effective catalyst.

Significance of the Hydrochlorination Results (JPL)

The MIT hydrochlorination process, which converts metallurgical-grade Si (mgSi) and SiCl₄ to SiHCl₃ in a low-cost operation, has wider potential commercial application than only to the Union Carbide silane-to-silicon process. Relatively large amounts of SiCl₄ are produced as a byproduct in the conventional (Siemens) process for making semiconductor-grade Si and also in other processes using chlorosilanes as intermediates. Economic advantage could accrue from conversion of this SiCl₄ to SiHCl₃, thereby eliminating SiCl₄ disposal costs and attaining nearly complete Si utilization. It was recommended that trade-off studies be conducted to evaluate the potential savings.
# Status of Union Carbide EPSDU

## Union Carbide Corp.
Hiroshi Morihara

<table>
<thead>
<tr>
<th>TECHNOLOGY</th>
<th>REPORT DATE</th>
<th>STATUS</th>
</tr>
</thead>
<tbody>
<tr>
<td>Polycrystalline Silicon</td>
<td>02/04/31</td>
<td>- Design &amp; engineering work on the EPSDU</td>
</tr>
<tr>
<td></td>
<td></td>
<td>- Process and auxiliary equipment started to arrive at the job site.</td>
</tr>
<tr>
<td></td>
<td></td>
<td>- Detailed installation drawings for mechanical and electrical subcontracts to be completed within two months.</td>
</tr>
</tbody>
</table>

## Approach
- High-purity silane production from metallurgical-grade silicon; and silane pyrolysis and consolidation to form semiconductor-grade polycrystalline silicon

## Contractor
Union Carbide Corporation

## Goals
- Demonstrate process feasibility and engineering practicality.
- Establish technology readiness using EPSDU sized to 100 M/yr.
- Silicon price of less than $14/kg for high volume process.
- Define process economics.
**EPSDU PROGRAM MAJOR MILESTONES**

<table>
<thead>
<tr>
<th>ACTIVITY DESCRIPTION</th>
<th>CY 1981</th>
<th>CY 1982</th>
<th>CY 1983</th>
</tr>
</thead>
<tbody>
<tr>
<td>JPL EPSDU PROJECT</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>1.1 DESIGN</td>
<td>1</td>
<td>2</td>
<td>3</td>
</tr>
<tr>
<td>1.2 EQUIPMENT</td>
<td>4 5 6</td>
<td>7 8</td>
<td></td>
</tr>
<tr>
<td>1.3 INSTALLATION/</td>
<td>9</td>
<td>10 11</td>
<td>12 13</td>
</tr>
<tr>
<td>CHECKOUT</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>1.4 OPERATION</td>
<td></td>
<td>9</td>
<td>10 11</td>
</tr>
<tr>
<td>1.5 COMMERCIAL</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>ECONOMICS</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>1.6 SUPPORTING R&amp;D</td>
<td>14 15</td>
<td></td>
<td></td>
</tr>
<tr>
<td>1.7 MANAGEMENT</td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

1. BID PACKAGE READY FOR MECHANICAL & ELECTRICAL INSTALLATION.
2. MOST EQUIPMENT FOR SILICON TO SILANE DELIVERED TO SITE.
3. EQUIPMENT FOR SILANE PYROLYSIS DELIVERED TO SITE.
4. SUBCONTRACT AWARD FOR MECHANICAL INSTALLATION AND OFF SITE SUBASSEMBLY STARTED.
5. START OF ON-SITE INSTALLATION.
6. START OF ON-SITE ELECTRICAL INSTALLATION.
7. END OF INSTALLATION & START OF CHECKOUT.
8. END OF CHECKOUT.
9. OPERATING MANUAL COMPLETE & START OF OPERATOR TRAINING.
10. START OF STARTUP.
11. STARTUP COMPLETE AND START OF DATA ACQUISITION.
12. END OF DATA ACQUISITION AND START OF DURABILITY ASSESSMENT.
13. END OF TEST PROGRAM.
14. START OF FLUID-BED PDU TESTING.
15. END OF FLUID-BED TESTING.
PLENARY SESSION: SILICON MATERIAL TASK

What Is the Hydrochlorination Reactor?

UNION CARBIDE SILANE-TO-SILICON PROCESS

I HYDROCHLORINATION: \( 3 \text{ SiCl}_4 + 2 \text{ H}_2 + \text{ S}i \rightarrow 4 \text{ SiHCl}_3 \)

II REDISTRIBUTION: \( 2 \text{ SiHCl}_3 \rightarrow \text{ SiCl}_4 + \text{ SiH}_2\text{Cl}_2 \)
\( \text{ SiH}_2\text{Cl}_2 \rightarrow \text{ SiHCl}_3, \text{ SiH}_2\text{Cl}_2, \text{ SiHCl}_2, \text{ SiH}_4 \)

III PYROLYSIS: \( \text{ SiH}_4 \rightarrow 2 \text{ H}_2 + \text{ S}i \)

- HYDROCHLORINATION STEP ENABLES A CLOSED LOOP PROCESS BY RECYCLING BY-PRODUCT \( \text{ SiCl}_4 \)
- REACTOR PROCESSES ABOUT 65 LBS OF \( \text{ SiCl}_4 \) FOR ONE POUND OF S\( i \) METAL PRODUCED
- COST SAVING ON THIS STEP HAS A LARGE IMPACT ON THE ECONOMICS OF THE OVERALL PROCESS

What Has Been Done

HYDROCHLORINATION REACTOR DEVELOPMENT AT THE MASSACHUSETTS INSTITUTE OF TECHNOLOGY

I ENGINEERING DATA
- REACTION KINETICS, YIELD, CONVERSION
- CATALYST, IMPURITIES
- SILICON PARTICLE SIZE, MASS LIFE
- CORROSION STUDY

II CONCLUSIONS
- EFFICIENT REACTION, HIGH YIELD AND CONVERSION
- COPPER CATALYST DOUBLES REACTION RATE
- LONG PERIODS OF CONTINUOUS OPERATION
- CONVENTIONAL METAL ALLOYS FOR REACTOR

III RECOMMENDATION
- MAXIMIZE REACTOR PRESSURE 500 PSIG
- ADD COPPER CATALYST TO INCREASE RATE
- INCOLOY 800 AS MATERIAL OF CONSTRUCTION FOR THE REACTOR
PLENARY SESSION: SILICON MATERIAL TASK

What Remains to Be Done

I REFINE ENGINEERING DATA FOR SCALE-UP

- OPTIMIZE PROCESS PARAMETER, FLUIDIZED-BED, PACKED-BED DESIGN
- MAXIMIZE RAW MATERIAL UTILIZATION, RECYCLE BY-PRODUCT WASTE STREAM
- QUALITY CONTROL, ORGANIC AND INORGANIC IMPURITIES IN CHLOROSILANE PRODUCTS

II CORROSION STUDY

- MECHANISM OF CORROSION
- SCREEN MATERIAL OF CONSTRUCTION FOR THE HYDROCHLORINATION REACTOR

Potential Application to Polycrystalline Silicon Technology

I THE CURRENT SIEMENS TECHNOLOGY FOR POLY SILICON

\[ \text{SiHCl}_3 + \text{H}_2 \xrightarrow{1000\,^\circ\text{C}} \text{Si}, \text{SiCl}_4, \text{HCl}, \text{LITES}, \text{HEAVIES} \]

II THE HYDROCHLORINATION OF SiCl4

\[ 3 \text{SiCl}_4 + 2 \text{H}_2 + \text{Si} \xrightarrow{} 4 \text{SiHCl}_3 \]

- IT PRODUCES THE STARTING SiHCl3 FOR THE SIEMENS TYPE REACTOR AT ESSENTIALLY 100% EFFICIENCY
- IT CONSUMES THE BY-PRODUCT SiCl4
- IT CAN ALSO CONVERT HCl AND OTHER BY-PRODUCTS TO SiHCl3
- IT FITS PERFECTLY INTO THE SIEMENS PRODUCTION SCHEME TO FORM A CLOSED LOOP PROCESS
- SUBSTANTIAL SAVINGS ON RAW MATERIAL COST CAN BE REALIZED
SIGNIFICANCE OF HYDROCHLORINATION RESULTS

JET PROPULSION LABORATORY
Ralph Lutwack

- STC - A BY-PRODUCT OF CHLOROSILANE PROCESSES
  - SIEMENS PROCESS
  - UNION CARBIDE PROCESS
  - FLUIDIZED BED REACTOR PROCESSES

- PRESENT STC UTILIZATION
  - PRODUCTION OF SILICA
  - EPITAXIAL DEPOSITION

- ADVANTAGES OF HR USE
  - STC DISPOSAL COSTS ELIMINATED
  - COMPLETE SI UTILIZATION
  - COMPARATIVE PRODUCT VALUES
    - STC
    - SEMICONDUCTOR GRADE SI

- CONCLUSION AND RECOMMENDATION
  - ECONOMIC ADVANTAGES
  - TRADEOFF STUDIES
NEAR-TERM COST-REDUCTION RESULTS

JET PROPULSION LABORATORY

D.W. Boyd

Near-Term Activity Evolution

LEGISLATION

PUBLIC LAW 95-238, SECT. 208(b) (FEB., 1978); SUPPLEMENTAL APPROPRIATIONS BILL (PAUL TSONGAS, MA.)

$6.0M AUTHORIZED FOR NEAR-TERM TECHNOLOGY DEVELOPMENT OF PHOTOVOLTAIC SYSTEMS (ESPECIALLY COST REDUCING PRODUCTION TECHNOLOGIES)

GOALS

- ACCELERATE REDUCTION IN FLAT-PLATE PHOTOVOLTAIC MODULE MANUFACTURING COSTS (1979-1981)
- DEMONSTRATE NEAR-TERM COST REDUCTION IMPACT OF ADVANCED PROCESSING APPROACHES
- TRANSLATE COST-REDUCING MANUFACTURING TECHNIQUES INTO COMMERCIAL PRACTICE
- PROVIDE FOR MAXIMUM TECHNOLOGY TRANSFER TO INDUSTRY TO ENSURE COMMON BENEFIT

PROGRAM

- LSA PROJECT ADD-ON

- $4.5M FOR DEVELOPMENT OF COST REDUCTIONS IN MATERIAL, EQUIPMENT, MODULE DESIGN, PROCESSES AND AUTOMATION
PLENARY SESSION: PRODUCTION PROCESS AND EQUIPMENT AREA

Contract Selection and Evaluation Process

- PROPOSAL RECEIPT
- PROPOSAL EVALUATION
  - CRITERIA
    - PROBABILITY OF SUCCESS
    - COST EFFECTIVENESS
    - JPL BASELINE vs PROPOSED EFFORT
- CONTRACT AWARD
  - 14 CONTRACTS ($4.5M)
    - WAFER PREPARATION – 4
    - CELL SEQUENCES – 4
    - METALLIZATION – 2
    - MODULE PROCESSES – 4

- RFP
  - SCOPE
    - COST REDUCING IMPROVEMENTS (1979-1981)
    - STEPS OR SEQUENCES
  - COST REDUCTION DETERMINATION
    - REVIEW BOARD
    - SAMICS METHODOLOGY
    - COST EVALUATION
      - JPL BASELINE vs CONTRACTOR ACHIEVEMENT
    - BOARD CONSENSUS
    - REPORT

LSA Baseline Process Sequence

- GROW INGOT
- CROP AND GRIND
- ID SAW
- TEXTURIZE
- SPIN-ON DOPANT
- DIFFUSION
- BACK SURFACE ETCH
- SCREEN PRINT BACK
- SCREEN PRINT FRONT
- EDGE GRIND
- AR COAT
- ELECTRICAL TEST
- ASSEMBLE INTERCONNECTS IN PVB
- SOLDER CELLS/INTERCONNECTS
- INSPECT SOLDER
- LAMINATE
- INSPECT LAMINATION
- ASSEMBLE TERMINALS
- TEST MODULE
# Near-Term Contract Cost-Reduction Results

<table>
<thead>
<tr>
<th>COMPANY</th>
<th>TECHNOLOGY</th>
<th>PREDICTED COST REDUCTION ($/Wp)*</th>
<th>ACTUAL COST REDUCTION ($/Wp)*</th>
</tr>
</thead>
<tbody>
<tr>
<td>1. KULICKE &amp; SOFFA</td>
<td>MODULE ASSEMBLY</td>
<td>2.32</td>
<td>0.77</td>
</tr>
<tr>
<td>2. ARCO SOLAR</td>
<td>NON-CZ SHEET</td>
<td>2.16</td>
<td>-</td>
</tr>
<tr>
<td>3. SILTEC</td>
<td>CRYSTAL SLICING</td>
<td>1.46</td>
<td>0.33</td>
</tr>
<tr>
<td>4. ARCO SOLAR</td>
<td>MODULE ASSEMBLY</td>
<td>1.43</td>
<td>1.76</td>
</tr>
<tr>
<td>5. ENERGY MATT CORP.</td>
<td>PHOTOVOLTAIC MATERIAL</td>
<td>1.40</td>
<td>0</td>
</tr>
<tr>
<td>6. SENSOR TECHNOLOGY</td>
<td>CELL PROCESS SEQUENCE</td>
<td>0.74</td>
<td>0</td>
</tr>
<tr>
<td>7. KAYEX</td>
<td>CZ GROWTH</td>
<td>0.43</td>
<td>0.62</td>
</tr>
<tr>
<td>8. MOTOROLA</td>
<td>METALLIZATION PATTERNING</td>
<td>0.38</td>
<td>0</td>
</tr>
<tr>
<td>9. MOTOROLA</td>
<td>CELL PROCESS SEQUENCE</td>
<td>0.37</td>
<td>0.68</td>
</tr>
<tr>
<td>10. MOTOROLA</td>
<td>ENCAPSULATION</td>
<td>0.26</td>
<td>0.11</td>
</tr>
<tr>
<td>11. SENSOR TECHNOLOGY</td>
<td>ETCHING</td>
<td>0.21</td>
<td>0.23</td>
</tr>
<tr>
<td>12. SOLLOS</td>
<td>METALLIZATION DEPOSITION</td>
<td>0.10</td>
<td>0.09</td>
</tr>
<tr>
<td>13. NIB ASSOCIATES</td>
<td>ENCAPSULATION</td>
<td>0.08</td>
<td>0</td>
</tr>
<tr>
<td>14. RCA</td>
<td>MEGASONIC CLEANING</td>
<td>0.07</td>
<td>-</td>
</tr>
</tbody>
</table>

*1975 DOLLARS

## Project Baseline/Near-Term Composite Common Parameters

- **CELL SIZE**: 3 in. dia
- **NO CELLS/MOD**: 316
- **MODULE SIZE**: 4 ft x 4 ft
- **HARDWARE PERFORMANCE**: 100 W_p
- **MODULE EFFICIENCY**: 6.7%
- **CELL EFFICIENCY**: 10%
## Process Sequence Using Near-Term Contracts

<table>
<thead>
<tr>
<th>PROCESS STEP</th>
<th>PROJECT BASELINE</th>
<th>NEAR-TERM COMPOSITE</th>
<th>COMPOSITE COMPONENTS (NEAR-TERM)</th>
</tr>
</thead>
<tbody>
<tr>
<td>VALUE ADDED</td>
<td>YIELD %</td>
<td>ALTERNATE STEP</td>
<td>VALUE ADDED</td>
</tr>
<tr>
<td>NAME</td>
<td>$/Vpp</td>
<td></td>
<td>NAME</td>
</tr>
<tr>
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<td>KAYEX-MOLY SHIELD</td>
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<td>TEXTURIZE</td>
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<td>SILTEC - DYNAMIC FILTER CONTROL</td>
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<td>SOL/KOS-MOLY TIN METALLIZATION</td>
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<td>K&amp;S - AUTOMATED ASSEMBLY</td>
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<td>AGSPB</td>
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<td>Motorola - AR GLASS</td>
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<tr>
<td>2 HOSPF</td>
<td>0.700</td>
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<td>2 GRINDIN</td>
<td>0.041</td>
<td>98</td>
<td>-</td>
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<td>3 ARCONTI</td>
<td>0.030</td>
<td>98</td>
<td>-</td>
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<td>2 TEST</td>
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<td>INTASSY - INTERCEPTOR</td>
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<td>CELLASI</td>
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<tr>
<td>SOLONSI</td>
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<tr>
<td>LAN</td>
<td>0.203</td>
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<td>LAMINSI</td>
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<td>TERASSY</td>
<td>0.076</td>
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<td>2$/1000 Vpp</td>
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<td>2$/975 Vpp</td>
<td>7.064</td>
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<td>5.913</td>
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### Conclusions

**NEAR-TERM CONTRACT ACTIVITY WAS BENEFICIAL**

- LOW FUNDS EXPENDITURE
- SHORT TIME PERIOD
- FOCUS ON SPECIFIC TECHNOLOGY

**RESULTED IN**

- TIMELY IDENTIFICATION OF PROMISING AND LESS-CERTAIN PRODUCTION PROCESS IMPROVEMENTS

**NEAR-TERM PAYBACK IS FEASIBLE**
PLENARY SESSION: ENCAPSULATION TASK

STATUS OF ENCAPSULATION MATERIALS AND OF ENCAPSULATION DESIGN PRINCIPLES

JET PROPULSION LABORATORY

E.F. Cuddihy

LSA Encapsulation Task

(17th PIM Meetings)

1) WOOD SUBSTRATE WORKSHOP
2) GENERAL PRESENTATION ON STATUS OF ENCAPSULATION MATERIALS AND DESIGN PRINCIPLES
3) CONTRACTOR PRESENTATIONS
4) FORUM ON ENCAPSULATION MATERIALS AND DESIGN PRINCIPLES FOR IN-DEPTH QUESTIONS AND DETAILS

Post-PIM Publication

1) ENCAPSULATION HANDBOOK

Program Divisions

- MATERIALS, PROCESSES, AND MODULE DESIGNS
  - MATERIAL IDENTIFICATION AND DEVELOPMENT, MODULE FABRICATION PROCESSES, MODULE DESIGNS, ENGINEERING SPECIFICATIONS FOR MATERIALS AND MODULES

- MODULE LIFE AND RELIABILITY
  - ACCELERATED, ABBREVIATED, AND OUTDOOR TESTING; CHEMICAL AND DESIGN REQUIREMENTS FOR MATERIALS AND MODULES TO ASSURE LONG-TERM SERVICE LIFE, PERFORMANCE, DURABILITY, AND RELIABILITY
### ENCAPSULATION MATERIALS
Module Construction Elements

<table>
<thead>
<tr>
<th>Module Sunside</th>
<th>Layer Designation</th>
<th>Function</th>
</tr>
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<tbody>
<tr>
<td></td>
<td>Surface</td>
<td>• Low soiling</td>
</tr>
<tr>
<td></td>
<td>1) Material</td>
<td>• Easy cleanability</td>
</tr>
<tr>
<td></td>
<td>2) Modification</td>
<td>• Abrasion resistant</td>
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<tr>
<td></td>
<td>Front Cover</td>
<td>• Anti-reflective</td>
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<tr>
<td></td>
<td>Pottant</td>
<td>• UV screening</td>
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<tr>
<td></td>
<td>Porous Spacer</td>
<td>• Structural superstrate</td>
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<tr>
<td></td>
<td>Dielectric</td>
<td>• Solar cell encapsulation</td>
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<tr>
<td></td>
<td>Substrate</td>
<td>• Air release</td>
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<tr>
<td></td>
<td>Back Cover</td>
<td>• Mechanical separation</td>
</tr>
<tr>
<td></td>
<td></td>
<td>• Electrical isolation</td>
</tr>
<tr>
<td></td>
<td></td>
<td>• Structural support</td>
</tr>
<tr>
<td></td>
<td></td>
<td>• Mechanical protection</td>
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<tr>
<td></td>
<td></td>
<td>• Weathering barrier</td>
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<tr>
<td></td>
<td></td>
<td>• Infra-red emitter</td>
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Plus necessary primers/adhesives

---

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PLENARY SESSION: ENCAPSULATION TASK

Cost Distribution*

**SUPERSTRATE DESIGN**

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<thead>
<tr>
<th>Material</th>
<th>Projected Cost</th>
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<tr>
<td>Glass (Low Iron)</td>
<td>$0.90 - 8.90</td>
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<td>Spacer</td>
<td>$0.10 - 0.10</td>
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<td>Pottant</td>
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</tr>
<tr>
<td>Silicon Cells</td>
<td>$0.10 - 0.10</td>
<td></td>
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<tr>
<td>Spacer</td>
<td>$0.10 - 0.10</td>
<td></td>
</tr>
<tr>
<td>Pottant</td>
<td>$0.70 - 1.00</td>
<td></td>
</tr>
<tr>
<td>Spacer</td>
<td>$0.10 - 0.10</td>
<td></td>
</tr>
<tr>
<td>Back Cover</td>
<td>$1.00 - 2.00</td>
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<tr>
<td><strong>subtotal</strong></td>
<td>$7.00 - 12.00</td>
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<tr>
<td>Edge Seal &amp; Gasket</td>
<td>$1.10 - 2.00</td>
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<td>Module Total</td>
<td>$9.10 - 15.00</td>
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**SUBSTRATE DESIGN**

<table>
<thead>
<tr>
<th>Material</th>
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<tbody>
<tr>
<td>UV Cover Film</td>
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<td></td>
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<tr>
<td>Pottants</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Substrate (Wood or Steel)</td>
<td></td>
<td></td>
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<tr>
<td>Edge Seal &amp; Gasket</td>
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<tr>
<td><strong>Module Total</strong></td>
<td>$9.00 - 13.00</td>
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*In 1980 dollars for large volume purchases

Lamination Pottants

<table>
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<tr>
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<th>Status</th>
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<tbody>
<tr>
<td>1) Ethylene Vinyl Acetate</td>
<td>$0.95/ Pound</td>
<td>Available (Springborn)</td>
</tr>
<tr>
<td>2) Ethylene Methyl Acrylate</td>
<td>$0.95/ Pound</td>
<td>Being Developed (Springborn)</td>
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<tr>
<td>3) Acrylic Elastomer</td>
<td>$1.50/ Pound</td>
<td>Imminent Availability (3M)</td>
</tr>
<tr>
<td>4) Poly Vinyl Butyral</td>
<td>$3.00/ Pound</td>
<td>Commercial</td>
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**PLENARY SESSION: ENCAPSULATION TASK**

Formulation of Industrial-Ready EVA

<table>
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<th>INGREDIENT</th>
<th>FUNCTION</th>
<th>SPRINGBORN FORMULATION IDENTIFICATION NUMBER</th>
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<tr>
<td></td>
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<td>A-9918 CLEAR (phr)*</td>
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<tr>
<td>ELVAX 190</td>
<td>BASE EVA</td>
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<tr>
<td>LUPERSOL 101</td>
<td>CURING AGENT</td>
<td>1.5</td>
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<tr>
<td>NAUGARD-P</td>
<td>ANTIOXIDANT</td>
<td>0.2</td>
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<tr>
<td>TINUVIN 770</td>
<td>UV STABILIZERS</td>
<td>0.3</td>
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<tr>
<td>CYASORB UV-531</td>
<td></td>
<td></td>
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<tr>
<td>TiO₂</td>
<td>WHITE PIGMENTS</td>
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<tr>
<td>ZnO₂</td>
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<tr>
<td>FERRO AM-105</td>
<td>UV STABILIZER</td>
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*COMPOSITION - PARTS PER HUNDRED OF RUBBER

**Castable Pottants**

<table>
<thead>
<tr>
<th>MATERIAL</th>
<th>PROJECTED COST</th>
<th>STATUS</th>
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<tbody>
<tr>
<td>POLY-n-BUTYL ACRYLATE</td>
<td>≈$0.85/POUND</td>
<td>BEING DEVELOPED (JPL/SPRINGBORN)</td>
</tr>
<tr>
<td>ACRYLIC LIQUID</td>
<td>?</td>
<td>DEVELOPMENT BEING CONSIDERED (RICHARDSON)</td>
</tr>
<tr>
<td>ALIPHATIC POLYETHER URETHANE</td>
<td>≈$1.30/POUND</td>
<td>BEING DEVELOPED (SPRINGBORN)</td>
</tr>
<tr>
<td>SILICONES</td>
<td>≈$10.00/POUND</td>
<td>COMMERCIAL</td>
</tr>
<tr>
<td>GE SILICONES</td>
<td>≈$3.00/POUND</td>
<td>EXPERIMENTAL</td>
</tr>
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</table>
PLENARY SESSION: ENCAPSULATION TASK

Pottants: Evolving Specifications and Requirements

- Glass Transition Temperature < ~40°C
- Mechanical Creep Resistance at 90°C
- Tensile Modulus < 2000 PSI at 25°C
- Optical Transmission (0.4 to 1.1 μm), > 90%
- Hydrolysis Resistance (to be defined)
- Ultraviolet Reaction Sensitivity (Wavelength cut-off)
- Thermal Oxidation Resistance at 60°C
- Peak Service Temperature Call-out
- Chemical Inertness (copper, nickel, solder, etc)
- Others

Front Covers for Substrate Designs
UV-Screening Plastic Films

<table>
<thead>
<tr>
<th>MATERIAL</th>
<th>COMMERCIAl COST</th>
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<tr>
<td>ACRYLIC</td>
<td></td>
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<tr>
<td>a) X-22416, 2 MILS</td>
<td>4.8$/FT²</td>
<td>AVAILABLE, 3M</td>
</tr>
<tr>
<td>b) X-22417, 3 MILS</td>
<td>6.70$/FT²</td>
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<tr>
<td>FLUOROCARBON</td>
<td></td>
<td></td>
</tr>
<tr>
<td>a) TEDLAR 100 BG 30 UT, 1 MIL</td>
<td>6$/FT²</td>
<td>AVAILABLE, DUpONT</td>
</tr>
<tr>
<td>b) TEDLAR 200 XRB 160 SE, 2 MIL</td>
<td>12$/FT²</td>
<td>BEING DEVELOPED, DUPONT</td>
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<tr>
<td>ACRYLIC/FLUOROCARBON ALLOYS</td>
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<tr>
<td>BLENDS OF POLY VINYLIDENE FLUORIDE AND POLY METHYL METHACRYLATE</td>
<td></td>
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<tr>
<td>a) FLUOREX-A, 1.8 MILS</td>
<td>?</td>
<td>BEING DEVELOPED, REXHAM</td>
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PLENARY SESSION: ENCAPSULATION TASK

**Edge Gasket Materials Survey**
(Elastomeric Molding)

**CANDIDATES**
- ETHYLENE/PROPYLENE (EPDM)
- ETHYLENE VINYL ACETATE (EVA)
- NEOPRENE
- SILICONE

**NOT CANDIDATES**
- NATURAL RUBBER
- STYRENE/BUTADIENE
- BUTYL/HALOGENATED BUTYL RUBBERS
- NITRILE/BUTADIENE
- POLYSULFIDE
- HYPALON
- FLUOROELASTOMERS

**Edge-Seal Materials Survey**
(Tacky Filler)

- BUTYLS
- POLYSULFIDES
- POLYURETHANES
- SILICONES
- HYPALONS
- NEOPRENES
- POLYAMIDES
- ACRYLICS

**Edge Gaskets**
Evolving Specifications and Requirements

- GLASS TRANSITION TEMPERATURE, < -40°C
- WEATHER STABLE
- NON-STAINING
- UNPLASTICIZED
- LOW COMPRESSION SET AT 60°C
- CHEMICAL INERTNESS
- ACCOMMODATE MODULE EXPANSION/CONTRACTION
- FABRICABLE AS SEAMLESS, ONE-PIECE UNIT
Dimensional Change of Masonite Under Vacuum-Bag Lamination Processing Condition

- Heating under vacuum for 20 min.
- Equilibration to atmosphere pressure.
- Cooling down at 1 atm N₂.

TEMP °C

LENGTH (10^-3 in)

20 40 60 80 100 120 140 160

305

304.5

PLENARY SESSION: ENCAPSULATION TASK

Commercial Corrosion-Prevention Coatings for Mild Steel

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<thead>
<tr>
<th>COATINGS</th>
<th>COST, BOTH SIDES</th>
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<tr>
<td>• POLYVINYLIDENE FLUORIDE (PRIMER + ENAMEL)</td>
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<td>PPG INDUSTRIES, 10 YEARS OUTDOOR TO DATE</td>
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<tr>
<td>• SILICONE/POLYESTER</td>
<td>5.4</td>
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<tr>
<td>DEXTER - MIDLAND, PROTOTYPES TO 20 YEARS</td>
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<tr>
<td>• POLYESTER</td>
<td>4.0</td>
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<td>DEXTER - MIDLAND, 5-10 YEARS OUTDOORS</td>
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<tr>
<td>• ACRYLIC COATING</td>
<td>4.0</td>
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<tr>
<td>PPG INDUSTRIES, 5 YEARS OUTDOORS</td>
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<tr>
<td>• POLYESTER (COMPLIANCE COAT)</td>
<td>4.0</td>
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<tr>
<td>DEXTER - MIDLAND, 5 YEARS OUTDOORS</td>
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<tr>
<td>• ACRYLIC EMULSION COATING</td>
<td>5.2</td>
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<tr>
<td>DEXTER - MIDLAND, 5 YEARS (EXTRAPOLATED)</td>
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<tr>
<td>• POLYESTER POWDER COATING</td>
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<td>DEXTER - MIDLAND</td>
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<tr>
<td>• &quot;BONDERITE&quot; PRIMER TREATED CONVERSION; TO BE APPLIED PRIOR TO COATING</td>
<td>0.2</td>
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Back Covers for Glass Superstrate Designs

• WHITE PIGMENTED POTTANTS (SPRINGBORN)

• SCOTCHPAR 10-CP-WHITE POLYESTER FILM (3M)
  a) 1 MIL STANDARD ≈ 2¢/FT²
  b) 2 MIL STANDARD ≈ 4¢/FT²
  c) 2 MIL H1-FILLED ≈ 5¢/FT²

• WHITE PIGMENTED VERSIONS OF X-22416 AND X-22417 UV SCREENING ACRYLIC FILMS, BEING DEVELOPED BY 3M

• PLASTIC FILM/METAL FOIL LAMINATES
  • MYLAR
  • TEDLAR
Candidate Anti-Soiling Coatings
Or Surface Treatments

1) FLUORINATED SILANE, L-1668 (3M)
2) FC-721 AND FC-723, FLUORINATED ACRYLIC POLYMER (3M)
3) PERFLUORODECANOIC ACID WITH CHEMICAL COUPLING PRIMER
4) GLASS RESIN 650 (OWENS-ILLINOIS)
5) WL-81 ACRYLIC (ROHM AND HAAS)
6) SANTICIZER 141 SURFACTANT (MONSANTO) WITH CHEMICAL COUPLING PRIMER Q3-6060 (DOW CORNING)
7) SHC-1000 ANTI-ABRASION COATING (GENERAL ELECTRIC)
8) MAGNESIUM FLUORIDE ANTI-REFLECTIVE COATING (DEPOSITED ON GLASS BY ION-PLATING, ITW)

Solar Cell Temperature
Illustrative Trend as Function of Thermal Resistivities and Backside Emissivity
PLENARY SESSION: ENCAPSULATION TASK

Deflection Analysis
(Glass Superstrate Design)

WIND LOAD \pm 50 \text{ psf}
0.125 \text{ in. thick, tempered glass}

(E = POTTANT MODULUS, PSI)

Thermal Stress Analysis (\Delta T = 100^{\circ}C)
(Glass Superstrate Design)

1/8 INCH THICK, TEMPERED GLASS
(E = POTTANT MODULUS, PSI)

DOTTED LINE - ALLOWABLE CELL STRESS IN TENSION
PLENARY SESSION: ENCAPSULATION TASK

Engineering Design: Trends and Guidelines

1) TEMPERATURE CONTROLLED PRIMARILY BY EMISSIVITY, AIR CIRCULATION, NOT BULK THERMAL CONDUCTION
2) AR COATING ON CELL A MUST
3) RIBS ARE NECESSARY ON SUBSTRATE MODULES
4) AL SUBSTRATE NOT COST EFFECTIVE FOR LARGE CELLS
5) ENCAPSULANT SHOULD BE ELASTOMERIC
6) LOW IRON TEMPERED GLASS COST EFFECTIVE
7) CRANE GLASS MATS ABOVE CELLS OKAY
8) FRAME DESIGN: 3/8" BITE, 1/16" GASKET
9) MINIMUM POTTANT THICKNESS HAS STRUCTURAL DEPENDENCE
PLENARY SESSION: OPERATIONS AREA

BLOCK IV MODULE RESULTS

JET PROPULSION LABORATORY
Larry Dumas

Outline

• CONTRACT OVERVIEW
  • OBJECTIVES
  • APPROACH
  • SCHEDULE

• MODULE CHARACTERIZATION
  • MECHANICAL
  • ELECTRICAL

• ENVIRONMENTAL TEST EXPERIENCE

• PRICE ANALYSES

• SUMMARY AND CONCLUSIONS

Contract Objectives

• STIMULATE USE OF LATEST IMPROVEMENTS IN PRODUCTION TECHNOLOGY

• PROVIDE PROVEN, STATE-OF-THE-ART RESIDENTIAL & INTERMEDIATE-LOAD MODULE DESIGNS FOR DOE PROCUREMENTS

• ASSESS PROGRESS IN MEETING INTERIM PRICE AND PERFORMANCE GOALS

• PROVIDE INDUSTRY WITH PRODUCT PERFORMANCE DATA
PLENARY SESSION: OPERATIONS AREA

Third-Generation Designs

- Improved specification of power output
- Fault tolerance for increased reliability (improved yield)
- Mechanical and electrical configurations are addressed to generally larger applications
- Improved array efficiency is encouraged
- Environmental qualification procedures and levels are consistent with and responsive to application factors
- Process-control-related QA programs are emphasized
- Innovative design approaches demonstrating technology readiness (cells, materials, processes)

Schedule

<table>
<thead>
<tr>
<th>BLOCK IV</th>
<th>ORIGINAL PLAN</th>
<th>1979</th>
<th>1980</th>
<th>1981</th>
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⇒ CONTRACT START

○ FINAL DESIGN REVIEW

□ PRELIM DESIGN REVIEW

△ FINAL REPORT

◦ MOD. TO JPL FOR TEST
### Physical Features

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<th>MANUFACTURER</th>
<th>MODEL NO</th>
<th>SIZE</th>
<th>Mass</th>
<th>ELECTRICAL TERMINATION</th>
<th>CELL CONFIGURATION</th>
<th>CELL PACKING FACTOR</th>
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### Encapsulation

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<th>POTTANT</th>
<th>SPACER</th>
<th>SUBSTRATE OR BACK COVER</th>
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<td>TEDLAR</td>
<td>EVA</td>
<td>RTV</td>
<td>POLYETHYLENE FOAM</td>
<td>BATTEN-SEAM</td>
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<td>EVA</td>
<td>CRANEGlass</td>
<td>WEATHERPROOF PAPER</td>
<td>NONE</td>
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<td>GASKET</td>
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<td>ARCO SOLAR R</td>
<td>1/8 in. GLASS</td>
<td>PVB</td>
<td></td>
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<td>ALUMINUM</td>
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<td>PVB</td>
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<td>TELTAR</td>
<td>ALUMINUM</td>
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<td>1/8 in. GLASS</td>
<td>PVB</td>
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<td>TELTAR-AI-TELAR</td>
<td>STAINLESS STEEL</td>
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<td>EVA</td>
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<td>ALUMINUM</td>
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<td>SPIRE</td>
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<td>EVA</td>
<td>PELLON</td>
<td>MYLAR-AI-COAT</td>
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### Cell Features

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<th></th>
<th>SIZE (cm)</th>
<th>BASE MATERIAL</th>
<th>JUNCTION</th>
<th>FRONT METALLIZATION</th>
<th>BACK METALLIZATION</th>
<th>ENCAPSULATED CELL % AT SOC</th>
<th>ENCAPSULATED CELL % AT 28°C</th>
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<tr>
<td>ARCO SOLAR</td>
<td>10 (DIA)</td>
<td>Cz</td>
<td>n/p</td>
<td>PRINTED-Ag</td>
<td>Ti-Pd-Ag</td>
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<td>12.3</td>
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<td>Cz</td>
<td>n/p</td>
<td>PRINTED-Ag</td>
<td>Ti-Pd-Ag</td>
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<td>12.5</td>
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<tr>
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<td>n/p p*</td>
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<td>Ti-Pd-Ag</td>
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<td>p/n</td>
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### Electrical Characteristics

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<th>RATED VOLTAGE AT SOC (volts)</th>
<th>RATED POWER AT SOC (watts)</th>
<th>NOMINAL OPERATING CELL TEMPERATURE (NOCT) (°C)</th>
<th>MODULE % AT SOC</th>
<th>MODULE % AT 28°C</th>
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# Qualification Tests for Flat-Plate Modules

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<th>TESTS</th>
<th>MODULES</th>
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<th>BLK IV/RES</th>
<th>TEST LEVELS</th>
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<td>BLK II</td>
<td>BLK III</td>
<td>PRDA-38</td>
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<td>THERMAL CYCLE</td>
<td>X</td>
<td>X</td>
<td>X</td>
<td>X</td>
<td></td>
<td>-40°C, +60°C</td>
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<tr>
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<td></td>
<td></td>
<td></td>
<td>50 CYCLES</td>
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<tr>
<td>HUMIDITY CYCLE</td>
<td>X</td>
<td>X</td>
<td>X</td>
<td>X</td>
<td></td>
<td>5 CYCLES, 95%, +40°C, +26°C</td>
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<td>X</td>
<td>(100)</td>
<td>X</td>
<td>(100)</td>
<td>X</td>
<td>2.4 kPa, 10,000 CYCLES</td>
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<td></td>
<td></td>
<td></td>
<td>UL 997</td>
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<tr>
<td>TWIST</td>
<td>X</td>
<td>X</td>
<td>X</td>
<td>X</td>
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<td>±2 cm/m</td>
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<td>HAIL IMPACT</td>
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<td>20 mm HAIL/25 mm HAIL</td>
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<td>X</td>
<td>X</td>
<td>X</td>
<td>X</td>
<td></td>
<td>2 X SYSTEM VOLTAGE PLUS 1000 VDC</td>
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<td>GROUND CONTINUITY</td>
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<td></td>
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<td>50 milliohm TEST</td>
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<td>HOT-SPOT ENDURANCE</td>
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<td></td>
<td>X</td>
<td>100 h SHORT-CIRCUITED AT SOC</td>
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### Qualification Test Sequence

#### ENVIRONMENTAL TESTS

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<th>PASS-FAIL CRITERIA</th>
<th>THERMAL CYCLING</th>
<th>HUMIDITY CYCLING</th>
<th>MECHANICAL LOAD OR WIND RESISTANCE</th>
<th>TWIST</th>
<th>HAIL IMPACT</th>
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<tr>
<td>GROUND CONTINUITY (R &lt; 50 mΩ)</td>
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<td>ELECTRICAL ISOLATION (1 &lt; 50 μA)</td>
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<tr>
<td>POWER DEGRADATION (ΔP &lt; 5%)</td>
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<td>✓</td>
<td>✓</td>
<td>✓</td>
<td>✓</td>
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<tr>
<td>PHYSICAL DEGRADATION (PER 1SPI)</td>
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<td>✓</td>
<td>✓</td>
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### Summary of Qualification Test Results

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<th>NUMBER OF PASS-FAIL CHECKS</th>
<th>NUMBER OF PROBLEMS</th>
<th>TOTAL PROBLEMS</th>
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<tr>
<td>THERMAL CYCLING</td>
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<td>HUMIDITY CYCLING</td>
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<td>132</td>
<td>9</td>
<td>6.8</td>
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<tr>
<td>TWIST</td>
<td>128</td>
<td>4</td>
<td>3.1</td>
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<td>TOTAL</td>
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### Nature of Test Problems

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<th>NUMBER OF PROBLEMS</th>
<th>% PROBLEMS</th>
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<tr>
<td>Electrical Isolation (I&lt;50μA)</td>
<td>135</td>
<td>3</td>
<td>2.2</td>
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<tr>
<td>Power Degradation (ΔP&lt;5%)</td>
<td>279</td>
<td>7</td>
<td>2.5</td>
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<tr>
<td>Physical Degradation (Per ISP)</td>
<td>174</td>
<td>58</td>
<td>33.3</td>
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<tr>
<td><strong>Total</strong></td>
<td><strong>588</strong></td>
<td><strong>68</strong></td>
<td><strong>11.6</strong></td>
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### Electrical Isolation Problems

- 1 of 6 manufacturers
- 3 of 40 modules

- Capacitive coupling of cell string to floating back foil; breakdown between foil and frame

- Corrected by improving isolation between foil and frame
PLENARY SESSION: OPERATIONS AREA

**Power Degradation**

- 3 OF 6 MANUFACTURERS
  4 OF 40 MODULES

- CRACKED CELLS (2 MODULES)

- UNDETERMINED (2 MODULES)

- LAMINATION PROBLEMS LIKELY CONTRIBUTOR IN ALL CASES
  - CRACKED CELLS
  - UNCURED EVA

**Physical Degradation**

6 OF 6 MANUFACTURERS
37 OF 40 MODULES

<table>
<thead>
<tr>
<th>CONDITION</th>
<th>#MFRS</th>
<th>#MODULES</th>
<th>PROBABLE CAUSE</th>
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<td>ENCAPSULANT DELAMINATION</td>
<td>6</td>
<td>21</td>
<td>PROCESS SEQUENCE; WORKMANSHIP</td>
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<td>CRACKED CELLS</td>
<td>5</td>
<td>14</td>
<td>LAMINATION DAMAGE; ENVIRONMENTAL STRESS</td>
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<tr>
<td>METALLIZATION DISCOLORATION</td>
<td>2</td>
<td>3</td>
<td>FLUX RESIDUE</td>
</tr>
<tr>
<td>J-BOX THREADS STRIPPED</td>
<td>1</td>
<td>3</td>
<td>DESIGN/WORKMANSHIP</td>
</tr>
<tr>
<td>SEALANT EXTRUDED</td>
<td>1</td>
<td>6</td>
<td>MATERIAL SELECTION</td>
</tr>
<tr>
<td>BROKEN FRAME CORNER</td>
<td>2</td>
<td>1</td>
<td>DESIGN/WORKMANSHIP</td>
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PLENARY SESSION: OPERATIONS AREA

SAMIS/SAMICS Results for 1 MW/yr (1980 $)

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<tr>
<th>MANUFACTURER</th>
<th>MODULE ($/WATT)</th>
<th>CELL ($/WATT)</th>
<th>NON-CELL ($/WATT)</th>
<th>CELL MODULE (%)</th>
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<td>0.76</td>
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<td>12.35</td>
<td>3.03</td>
<td>80</td>
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<td>6.93</td>
<td>5.23</td>
<td>1.70</td>
<td>75</td>
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<tr>
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<td>1.96</td>
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<td>SOLAREX IL</td>
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<td>7.59</td>
<td>2.76</td>
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<td>20.20</td>
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<td>5.71</td>
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Module Efficiency, Block Procurements

\[ T_M = \frac{\text{MODULE POWER}}{\text{GROSS AREA OF MODULE} \times \text{SOLAR INSOLATION}} \quad 28^\circ C \quad 100 \text{ mW/cm}^2 \]

![Diagram showing module efficiency over years](image)
Module Price History

DOLLARS PER WATT FOR BLOCK PROCUREMENTS

1980 DOLLARS
280°C
100 mW/cm²

Quality Assurance Recommendations

- IMPLEMENT INSPECTION SYSTEM PLANS AS WRITTEN
- PROVIDE FOR TRAINING OF INSPECTORS AND PRODUCTION PERSONNEL
- FOCUS ON PROCESS CONTROL AT PIECE PART AND ASSEMBLY LEVELS
- PROVIDE FOR RAPID FEEDBACK OF INSPECTION DATA FOR CORRECTIVE ACTION IMPLEMENTATION
- GIVE MANAGEMENT ATTENTION TO THE APPLICATION AND EFFECTIVENESS OF QUALITY ASSURANCE ACTIVITIES
PLENARY SESSION: OPERATIONS AREA

Observations and Conclusions

- NEW DESIGNS AND TECHNOLOGIES WERE ASSIMILATED WITH SOME DIFFICULTY
  - SCHEDULE SLIPS
  - TEST PROBLEMS
  - RETREATS TO CONVENTIONAL APPROACHES
- LARGE-SCALE PRODUCIBILITY UNTESTED
- PRICE AND PERFORMANCE PROGRESS CONTINUES
  - PRICES ARE DOWN
  - EFFICIENCIES ARE UP
  - RELIABILITY AND DURABILITY BETTER
    - HAIL PROTECTION
    - MOISTURE PROTECTION
    - FAULT TOLERANCE
- MOST DESIGNS WILL BE OFFERED COMMERCIALLY
PLENARY SESSION: PRODUCTION PROCESS AND EQUIPMENT AREA

MODULE EXPERIMENTAL PRODUCTION SYSTEM DEVELOPMENT UNITS
JET PROPULSION LABORATORY

PLENARY SESSION D.B. Bickler, Chairman

The Module Experimental Production System Development Unit (MEPSDU) presentations for the Production Process and Equipment Development Area were intended to acquaint the industry with the purpose and extent of these new contracts. After the two companies made their presentations a panel of industry representatives discussed concerns that they had identified from their experiences. Comments were also taken from the audience. Several concerns were identified by PP&E to be discussed at the contractor preliminary design reviews.

PREVIEW OF SOLAREX’S MEPSDU PROGRAM

SOLAREX CORP.

John Wohlgemuth

Design Philosophy

- Use processes that have already been verified, in most cases by more than one contractor.
- Use commercially available equipment or modifications of such equipment.
- Use production equipment, not laboratory-scale equipment.
- No manual handling of cells.
General Process Description

INCOMING MATERIAL
SEMICRYSTALLINE
10 CM X 10 CM WAFER

SURFACE PREPARATION
NAOH ETCH

FRONT JUNCTION FORMATION
SPRAY-ON DOPANT
AND BELT DIFFUSION

BACK JUNCTION FORMATION
AL PASTE
BELT FIRE

AR COATING
SPRAY-ON

METALLIZATION
NEGATIVE SCREEN PRINT
ELECTROLESS Ni PLATE
SOLDER DIP

EDGING
LASERSCRIBE

CELL TEST

TAB AND STRING
SOLDER CONTACTS

ENCAPSULATE MODULE
LAMINATED EVA ON GLASS

MODULE TEST

SHIP
Module Design

72 10 cm x 10 cm SEMICRYSTALLINE CELLS
2 PARALLEL - 36 SERIES

APPROXIMATE ENVELOPE DIMENSIONS
66 cm x 125 cm
26" x 49.3"

DESIGN VOLTAGE - 14.5 V
GLASS SUPERSTRATE
ETHYLENE VINYL ACETATE ENCAPSULANT
POLYETHYLENE VAPOR BARRIER
GASKET FOR MOUNTING (NO FRAME)
AMP OUTPUT CONNECTORS
INTERNAL DIODE PROTECTION - 3 DIODES PER MODULE

Module Cross Section
Incoming Material

Semicrystalline 10 cm x 10 cm wafers

Chosen because:
- Available for use now.
- Closely related to other advanced sheet materials.
- Consistent with 70$/watt cost goal.
- Solarex has sufficient experience with its processing to understand its behavior through the proposed process steps.

Quality Assurance:
- Measure lifetime and bulk resistivity using microwave technique.
- Good correlation between the measurement and subsequent cell performance.
**Surface Preparation**
- Etch 37% NaOH 110-120°C
- Water Rinse
- Neutralize 50% HCL
- Water Rinse
- Dry
- Spot Check Sheet Resistance
- Spot Check Thickness

**Front Junction Formation**
- Spray on Dopant (Water Base)
- Dry Spray 100-150°C
- Diffuse 900°C Air
- Water Rinse
- Dry
- Spot Check Sheet Resistance
- All on Belts

**Back Junction Formation**
- Screen Print Al Paste
- Dry Paste 150 to 250°C (Belt)
- Fire Paste 950°C (Less Than 1 Min.) (Belt)
- Remove Residues (Either HCL or Abrasion)
- Oxide Removal HF Etch
- Water Rinse
- Dry

**Back Surface Formation**
- Screen Print Al Paste
- Dry Paste 150 to 250°C (Belt)
- Fire Paste 950°C (Less Than 1 Min.) (Belt)
- Remove Residues (Either HCL or Abrasion)
- Oxide Removal HF Etch
- Water Rinse
- Dry
AR Coating

SPRAY ON TITANIUM ISOPROPXIDE

SINTER 400°C (BELT)

SCREEN ON RESIST INK

ETCH OFF AR FROM GRID PATTERN

RINSE

Metallization

ELECTROLESS NI PLATE

REMOVE RESIST (VAPOR DEGREASER)

RINSE

SOLDER FLUX

SOLDER

RINSE

DRY

Edging

LASER Scribe

LINE WIDTH = 0.035" 
PENETRATION = 0.001"

LASER Scribe

CELL TEST

STORE IN CASSETTES
Tabbing and Stringing

Use K&S machine
Pulsed heat solder bonds
One piece stamped copper interconnect with solder plate for wraparound and series connection to next cell.
Two interconnects per cell with 4 bonds top and bottom.
Machine makes series strings of 12 cells.
Then places string in position and makes required parallel connections.
Produces layout of module ready for encapsulation

Encapsulate Module

- RINSE CELL STRING
- LAY-UP MODULE
  - LAMINATE 100°C-1/2hr.
- INSTALL CONNECTOR & GASKET
- TEST MODULE

PRIME GLASS
PLENARY SESSION: PRODUCTION PROCESS AND EQUIPMENT AREA

Cost Analysis

**Assumptions**

- 50 MW per year production rate.
- 15% Efficient Encapsulated Cells
  - AMI-100W/cm² - 25°C
- 93% Yield from Wafer to Module
- $0.306 per Watt Wafer Cost

**Results**

- IPEG - $0.691 per Watt
- Literature - $0.661 per Watt
  (Compilation of others' cost analysis for same process steps)

(All in 1980 dollars)

**Efficiency of Semicrystalline Material**

- **Small Area Samples (2 cm x 2 cm)**
  - Best - 17%
  - Best Lot Average - 16.5%

- **Large Area Samples (9.5 cm x 9.5 cm)**
  - Best - 13.5%
  - Best Lot Average - 12%

**Typical Production**

- 10 - 11% Lot Average

All efficiencies measured at 100W/cm² - AMI - 25°C.
Westinghouse MEPSDU Baseline Process Sequence

1. **Pre Diffusion Clean**
2. **Back Junction Formation**
3. **Front Junction Formation**
4. **AR/PR Deposition/Bake**
5. **Front Grid Delineation**
6. **Metallize - Front & Back (Ti/Pd)**
7. **Rejection Cu Plating**
8. **Cell Separation and Test**
9. **Cell Interconnect**
10. **Module Lamination**
11. **Module Test**
12. **Crate**
PLENARY SESSION: PRODUCTION PROCESS AND EQUIPMENT AREA

Pre-Diffusion Cleaning

PURPOSE: PREPARE WEB FOR DIFFUSION BY REMOVAL OF SURFACE CONTAMINANTS

PROCESS:

- HF/DI H₂O/DRY
- PLASMA CLEAN

INPUT: 17" LENGTHS OF AS-GROWN WEB

CONTROLS:

- 200 ±10 WATTS RF POWER
- 300 ±10 CC/MIN OF O₂
- 3 MINUTE HOLD AT T < 130°C

OUTPUT: 17" LENGTHS OF CLEANED WEB

VALUE ADDED: $0.041/PEAK WATT; 25 MW/yr PRODUCTION

ALTERNATE: EXTENSIVE AND LESS AUTOMATABLE CHEMICAL CLEANING PROCESSES

Back Junction Formation

PURPOSE: FORMATION OF P+ BACK JUNCTION INTO P-BASE WEB

PROCESS:

- COAT FRONT SURFACE OF WEB WITH SiO₂;
- BB₃ DIFFUSION IN STANDARD DIFFUSION FURNACE;
- ETCH WEB TO REMOVE OXIDE

- 1200 ± 200 Å THICK COATING OF SiO₂
- 6 ± 1 CC/MIN Ar THROUGH BB₃
- 90 ±9 CC/MIN O₂

CONTROLS:

- 2400 ± 240 CC/MIN Ar CARRIER GAS
- TEMPERATURE = 980 ±5 -10°C
- TIME = 20 ± 4 MIN
- COOLING RATE = 5 ± 3°C/MIN FROM T = 980°C TO T < 700°C

OUTPUT: BACK SURFACE DIFFUSED WEB WITH 60 ±5/-20 Ω/□ SHEET RESISTIVITY

VALUE ADDED: $0.023/PEAK WATT (1980 $, 25 MW/YEAR PRODUCTION)

ALTERNATIVES: 1. ALUMINUM BACK SURFACE FIELD
2. ION IMPLANTATION
PLENARY SESSION: PRODUCTION PROCESS AND EQUIPMENT AREA

Front Junction Formation

**PURPOSE:** FORMATION OF N+ FRONT JUNCTION INTO P-BASE WEB

- COAT BACK SURFACE OF WEB WITH SiO$_2$;
- POC$_3$ DIFFUSION IN STANDARD DIFFUSION FURNACE;
- ETCH WEB TO REMOVE OXIDE

**INPUT:**
- 17" LENGTHS OF WEB WITH FORMED BACK JUNCTIONS
- 1200 ± 200 Å THICK COATING OF SiO$_2$
- 200 ± 20 CC/MIN N$_2$ THROUGH POC$_3$
- 1550 ± 150 CC/MIN N$_2$ CARRIER GAS

**CONTROLS:**
- 62.5 ± 6.0 CC/MIN O$_2$ CARRIER GAS
- TEMPERATURE = 850 ± 50°C
- TIME = 35 ± 10 MIN
- COOLING RATE = 5 ± 1°C/MIN FROM T = 850°C TO T < 700°C

**OUTPUT:**
- N+P+ FORMED WEB WITH 50 ± 5 Ω/□ SHEET RESISTANCE

**VALUE ADDED:** $0.023/PEAK WATT (1980 $, 25 MW/YEAR PRODUCTION)

**ALTERNATIVE:** ION IMPLANTATION
Antireflective Coating Application

**PURPOSE:** APPLY AR COATING AND PLATING MASK TO SURFACE OF WEB

**PROCESS:**
- DIP AND WITHDRAW WEB FROM TiO₂/SiO₂ METAL/ORGANIC SOLUTION
- AIR BAKE TO FORM GLASS AR COATING

**INPUT:**
- 17” LENGTHS OF WEB WITH N + PP + STRUCTURE
- 3.5 ± 0.5% OXIDE MIXTURE IN ALCOHOL

**CONTROLS:**
- OXIDE MIXTURE – 88 ± 2% TiO₂/12 ± 2% SiO₂
- WITHDRAWAL RATE = 30 ± 3 CM/MIN
- HEAT IN AIR FOR 15 ± 1 MIN AT 400 ± 10°C

**OUTPUT:** WEB WITH 750 ± 30 Å AR COATED SURFACES

**VALUE ADDED:** $0.005/PEAK WATT, 25 MW/YR PRODUCTION

**ALTERNATIVE:** NONE AS COST EFFECTIVE

Photoresist Coating Application

**PURPOSE:** APPLY PR LAYER TO SURFACE OF WEB FOR GRID DELINEATION

**PROCESS:**
- DIP AND WITHDRAW WEB FROM POSITIVE PR SOLUTION
- AIR BAKE TO CURE PR

**INPUT:**
- 17” LENGTHS OF AR COATED WEB
- 50 ± 5% SOLUTION OF PR AND PR THINNER

**CONTROLS:**
- WITHDRAWAL RATE = 25 ± 5 CM/MIN
- HEAT IN AIR 90 ± 3°C FOR 25 ± 3 MIN

**OUTPUT:** WEB COATED WITH 1.0 ± 0.2 µM OF CURED POSITIVE PR

**VALUE ADDED:** $0.011/PEAK WATT, 25 MW/YR PRODUCTION

**ALTERNATIVE:** NONE IDENTIFIED COMPATIBLE WITH BASELINE SEQUENCE
Grid Delineation

PURPOSE: DEFINE GRID PATTERN ON FRONT SURFACE OF CELLS

PROCESS: EXPOSE PR; DEVELOP PR; ETCH EXPOSED AR

NEGATIVE MASK LOCATED BETWEEN DENDRITES, SUN SIDE
EXPOSE PHOTORESIST AT 55 ± 10 MJ/CM² (BOTH SIDES)
DEVELOP EXPOSED PR; 60 ± 5 SEC AT 20 ± 5°C

CONTROLS:
RINSE IN DI H₂O
AR ETCH: 3:1/H₂O:HF FOR 5 ± 1 SEC
RINSE IN DI H₂O AND DRY

OUTPUT: 17" LENGTHS OF WEB WITH SI EXPOSED GRID PATTERN HAVING LESS THAN 5% CELL AREA COVERAGE

VALUE ADDED: $0.020/PEAK WATT, 25 MW/YR PRODUCTION

Metallization

PURPOSE: APPLICATION OF BASE METAL SUB-STRATE CONTACTS

PROCESS: EVAPORATE Ti/Pd/Cu METALS ON FRONT AND REAR WEB SURFACES

INPUT: WEB WITH DELINEATED GRID (FRONT) AND EXPOSED SI BACK SURFACE

PRESSURE ≈ 10⁻⁶ TORR
E-BEAM METAL EVAPORATION

CONTROLS:
COMPUTER POWER CONTROL/CRYSTAL DEPOSITION RATE SENSOR

DEPOSITION RATES = 2-5 Å/SEC

OUTPUT: WEB WITH 300 ± 50 Å Ti/Pd/Cu FILMS ON FRONT AND BACK

VALUE ADDED: $0.032/PEAK WATT, 25 MW/YR PRODUCTION

ALTERNATIVE: OTHER METALLIZATION CONFIGURATIONS
PLENARY SESSION: PRODUCTION PROCESS AND EQUIPMENT AREA

Rejection of Excess Metal

PURPOSE: REMOVE EXCESS METALS FROM CELL FRONT SURFACES

PROCESS:
- DISSOLVE UNEXPOSED PR
- REMOVE METAL COATED ON PR

INPUT: 17" LENGTHS OF WEB WITH Ti/Pd FILMS DEPOSITED ON ENTIRE SURFACE

ACETONE IMMERSION OF WEB

CONTROLS:
- ULTRASONIC AGITATION
- MEOH/H₂O RINSE; DRY

OUTPUT: 17" LENGTHS OF WEB WITH Ti/Pd FILMS DEPOSITED ONLY ON SILICON

VALUE ADDED: $0.010/PEAK WATT, 25 MW/YR PRODUCTION

Copper Electroplating

PURPOSE: DEPOSIT CURRENT CARRYING CONTACTS ON CELLS

PROCESS: ELECTROPLATE COPPER OVER EXPOSED Cu SURFACES

INPUT: 17" LENGTHS OF WEB WITH DEPOSITED Ti/Pd/Cu SUB-STRATE

ACIDIC COPPER PLATING SOLUTION

CONTROLS:
- CURRENT DENSITY = 15 ± 5 MA/CM² FOR 10 ± 1 MIN
- RINSE IN DI H₂O/DRY

OUTPUT: 17" LENGTHS OF WEB WITH 6-8 µM THICK COPPER PLATING

VALUE ADDED: $0.031/PEAK WATT, 25 MW/YR PRODUCTION

ALTERNATIVE: SILVER ELECTROPLATING
Cell Separation

PURPOSE: SEPARATE CELLS FROM DENDRITE/WEB MATRIX

OPTICALLY ALIGN WEB IN LASER Scribe

PROCESS: LASER Scribe CELL PATTERN ON SCRIBE

MECHANICALLY FRACTURE/SEPARATE CELLS FROM MATRIX

INPUT: 17" LENGTH OF COPPER PLATED WEB

SCRIBE DEPTH = 50 ± 5 µM (REAR SCRIBE)

CONTROLS: MECHANICAL FRACTURE/SEPARATION

OUTPUT: FOUR 2.5 x 10 CM FINISHED CELLS

VALUE ADDED: $0.015/PEAK WATT (INCLUDING CELL TEST); 25 MW/YR PRODUCTION

Interconnect

PURPOSE: INTERCONNECT INDIVIDUAL CELLS IN SERIES/PARALLEL MODULE MATRIX

PROCESS: ULTRASONICALLY BOND ELECTRICAL INTERCONNECT TAGS TO ADJACENT CELLS

POSITION INDIVIDUAL CELLS IN REQUIRED MODULE MATRIX

INPUT: 0.015" ALUMINUM INTERCONNECT TABS

180 PROCESSED CELLS LOADED INTO CASSETTES

CONTROLS: MICROPROCESSOR CONTROLLED ULTRASONIC BONDING PARAMETERS (POWER, FORCE, AND SPEED) AND CELL HANDLING STATION

OUTPUT: FOUR SERIES CONNECTED STRINGS OF 45 CELLS POSITIONED FOR LAMINATION

VALUE ADDED: $0.018/PEAK WATT, 25 MW/YR PRODUCTION

ALTERNATIVES: 1. ULTRASONIC SPOT BONDING OF INTERCONNECTS

2. SOLDER REFLOW BONDING
Module Lamination and Assembly

**PURPOSE:**

ENCAPSULATE INTERCONNECTED CELLS INTO LAMINATED MODULE ASSEMBLY

**PROCESS**

- LAMINATE MODULE LAYUP
- INSTALL LAMINATED ASSEMBLY INTO FRAME
- TEMPERED FLOAT GLASS, INTERCONNECTED CELL ASSEMBLY,

**INPUT:**

- EVA, CRANE GLASS, KORAD, RUBBER GASKETS, AND FRAME COMPONENTS

**CONTROLS:**

- LAMINATION TEMPERATURE = 200 ± 4°C
- LAMINATE VACUUM = (1 ± .5) x 10⁻² TORR

**OUTPUT:**

16" x 48" SOLAR MODULE MEETING JPL 5101-138 ENVIRONMENTAL SPECIFICATION

**VALUE ADDED:**

$0.205/PEAK WATT (INCLUDING TEST AND CRATING), 25 MW/YR PRODUCTION

**Process Sequence Status**

- BASELINE MEPSDU PROCESS SEQUENCE SELECTED
- ALL BASELINE PROCESS SEQUENCE STEPS SUCCESSFULLY DEMONSTRATED
- COMPATIBILITY OF STEPS WITHIN SEQUENCE DEMONSTRATED
- ALTERNATE STEPS UNDER INVESTIGATION
PLENARY SESSION: PRODUCTION PROCESS AND EQUIPMENT AREA

SAMICS Analysis: Conceptual Factory

- 25 MW/YR PRODUCTION, BALANCED LINE
- ALL AUTOMATED PROCESSES
- CELLS: 2.5 CM X 40 CM (NOM)
- MODULES: 40 CM X 120 CM
- 12% MODULE EFFICIENCY AT 28°C
- 345 DAYS/YR OPERATION (3 SHIFT)
- DENDRITIC WEB SHEET MATERIAL COST $0.24/WATT (1980 $)
- 86% OVERALL YIELD

MEPSDU Module Mechanical Design

- OVERALL SIZE OF 40 cm X 120 cm (OPEN APERTURE 38 cm X 118 cm)
- LAMINATED TEMPERED FLOAT GLASS SUPERSTRATE
- LAMINATION LAYUP: EVA, CRANE GLASS, MOISTURE BARRIER
- COR-TEN STEEL USED FOR FRAME AND MOUNTING
- DESIGNED TO PASS JPL 5101-138

MEPSDU Module Electrical Design

- 180 CELLS/MODULE; 2.5 cm X 10.0 cm CELLS
- 4 PARALLELED STRINGS OF 4.5 SERIES CONNECTED CELLS
- ALL CONNECTIONS INSIDE MODULE TO BE ULTRASONICALLY WELDED
- INTERCELL SPACING · 0.03 cm
- PACKING FACTOR · 92%
- TEN ELECTRICAL INTERCONNECTS/CELL
- CELL ASPECT RATIO IMPROVES RELIABILITY
MEPSDU Module Operation

- THERMAL ANALYSIS UNDERWAY
- ASSUMING NOCT OF 40°C MODULE OUTPUT AT 80 MW/cm²:

  \[
  \begin{align*}
  \text{VOLTAGE} & \quad - \quad 19.1 \text{ V} \\
  \text{CURRENT} & \quad - \quad 2.39 \text{ A} \\
  \text{POWER} & \quad - \quad 45.6 \text{ WATTS} \\
  \text{MODULE EFFICIENCY} & \quad - \quad 19.9\% 
  \end{align*}
  \]

- ASSUMING AT 25°C AND 100 MW/cm²:

  \[
  \begin{align*}
  \text{VOLTAGE} & \quad - \quad 20.4 \text{ V} \\
  \text{CURRENT} & \quad - \quad 2.95 \text{ A} \\
  \text{POWER} & \quad - \quad 61 \text{ WATTS} \\
  \text{MODULE EFFICIENCY} & \quad - \quad 12.7\% 
  \end{align*}
  \]
Measured Yield Required to Demonstrate 0.95 Confidence That Large Production Yield Will Be 86%
PLENARY SESSION: PRODUCTION PROCESS AND EQUIPMENT AREA

Data Collection During Technical Readiness Demo Runs

- OVERALL INPUT
- OVERALL OUTPUT
- OPERATIONAL COST FACTORS
  - OPERATOR TIME
  - EXPENDABLE CONSUMPTION RATES
  - ENERGY CONSUMPTION RATE

Approach to Demonstration of Technical Readiness

- DESIGN, BUILD AND OPERATE A BALANCED 1 MW/YR MEPSDU LINE
- EXPLOIT ADVANTAGES OF DENDRITIC WEB SILICON
- EMPHASIS PLACED ON MAXIMIZING EFFICIENCY
- INCORPORATE ONLY QUALIFIED PROCESS STEPS
- INCORPORATE ONLY AUTOMATABLE PROCESS STEPS
- UPDATE SAMICS CONTINUALLY TO VERIFY THAT PROCESS SEQUENCE WILL MEET COST GOALS OF $.70/WATT IN 1986 (1980 $)
- SPECIFY MEPSDU EQUIPMENT WITH DEMONSTRATED RELIABILITY RECORD
Seven contractors reported on progress in developing Si production processes and in supporting activities.

Having summarized the status of their programs at the plenary session, Union Carbide Corp. and the Massachusetts Institute of Technology reviewed progress in more detail. The free-space reactor R&D program was successfully completed by UCC. Design and procurement of the Si powder melting and consolidation equipment were completed, and installation and checkout are in progress. In MIT's study of the hydrochlorination of metallurgical-grade Si and SiCl₄ to SiHCl₃, a prolonged test (238-hour duration) was carried out to study the life of the Si bed in the fluidized-bed reactor. No significant change in the reaction rate was observed, indicating good bed life.

Hemlock Semiconductor Corp. started construction of the dichlorosilane (SiH₂Cl₂) PDU, after making changes in its design and location as a result of finding that SiH₂Cl₂ is more hazardous to handle than previously thought. The PDU will be used to study the preparation of SiH₂Cl₂, and to make feedstock for Siemens-type reactors to investigate the Si deposition process. Hemlock described the safety-related tests that were conducted on SiH₂Cl₂ and its mixtures with hydrogen and air.

Battelle Columbus Laboratories reported on efforts to operate a PDU consisting of the critical components required for their process (zinc reduction of SiCl₄). Battelle described the numerous modifications that were made to the PDU to improve operability and stated that in 10 tests made after the modifications, Si deposition was achieved in seven. Efforts to operate for eight hours failed; the longest test was 41 minutes. The experimental phase of the Battelle contract was completed at the end of January.

In the area of impurity studies, Westinghouse reported on its spectral response measurements made on polycrystalline solar cells, indicating that both impurities and grain boundaries reduce carrier lifetime, causing decreased red response and cell efficiency. Information was also presented on accelerated aging tests and other studies. Progress was reported by C. T. Sah Associates on the program to determine the maximum concentrations of certain metallic impurities that can be allowed in Si solar cells to maintain a given efficiency.

Experimental results were reported by AeroChem Research Laboratories in a study on the formation and growth of Si particles produced by the decomposition of silane at high temperatures. Representative data indicate that: (1) particles formed from silane decomposition have a narrow size distribution and are spherical in shape at a given time in the
decomposition-growth process; (2) the decomposition-growth process is dominated by heterogeneous gas-particle interactions for sizes greater than 0.05 \( \mu \)m radius; (3) rates of particle growth and silane decomposition are consistent with diffusion-limited kinetics in the 50 to 550 torr pressure range studies; (4) tentatively, particles larger than 0.05 \( \mu \)m radius do not grow by agglomeration; and (5) particles larger than 0.05 \( \mu \)m radius have a cellular structure.

Material presented by the contractors is summarized in the following pages.
### Particle Formation and Growth Studies

- **LIGHT SCATTERING DATA**
- **SIZE CALIBRATION**
- **PARTICLE GROWTH RATES**
- **PARTICLE SEEDING**
- **PARTICLE COLLECTION**
SILICON MATERIAL TASK

Apparatus Construction

- HTFFR
- LIGHT SCATTERING DIAGNOSTICS
- LONG PATH IR CELL
- FLUIDIZED BED
SILICON MATERIAL TASK

1 \mu m 
(4300)

0.25 \mu m 
(100)

HETEROGENEOUS GROWTH

0.05 \mu m

HOMOGENEOUS GROWTH

0.01 \mu m >
Problems and Concerns

MORE WORK NEEDED

- PARTICLE CONCENTRATION
  BY FORWARD SCATTERING
- EXPERIMENTS CLOSE TO PROCESS CONDITIONS
- ADDITIONAL COMPUTER WORK
- IMPROVE Si, SiH, SiH₂ MEASUREMENTS

SILANE-TO-SILICON PROCESS
UNION CARBIDE CORP.

ASSUMPTIONS:

PLANT SIZE: 1000 MT/YR SEMICONDUCTOR-GRADE Liquid Silicon Product

TOTAL PLANT COST: $9.66 M
START-UP COST: $1.74 M
WORKING CAPITAL: $0.72 M
ANNUAL OPERATING COST: $5.88 M
FEDERAL INCOME TAX: 46%
CONSTRUCTION TIME: 2.5 - 3 YRS
DEPRECIATION: 10 YEARS SUM OF YEARS DIGITS
PROJECT LIFE: 15 YEARS

PROJECTION

ROI RATE (%) | PRODUCT PRICE, $/KG
--- | ---
10 | 8.77
15 | 9.77
20 | 10.90

* Incremental product price increase going from liquid silicon to polycrystalline silicon shot has not been determined. One to two dollar/kg increase is anticipated.
Problems and Concerns

EPSDU Engineering & Installation

- A safety review meeting was held in November 1980, and possible problems were identified. Design changes are being made which address these potential problems.
- A portion of the waste treatment system design is relatively novel, and some field adjustment may be needed for proper operation.

SILANE Pyrolysis R & D

- A successful operation of the silicon powder melting/shotting system must be demonstrated.
- A reliable silicon powder transfer system from the free-space reactor to the melter/shotter must be designed.

Engineering Summary

A. M. G. Silicon - to - Silane

- Process design complete
- Facility design complete
- All major equipment ordered
- Installation design -- complete in April
- Installation subcontracts -- ongoing thru 1981
- Shakedown/startup -- early 1982

B. Silane - to - Polysilicon

- Process design -- complete in May
- Installation design -- complete in 1981
- Shakedown/startup -- mid 1982
Free-Space Reactor Summary

- THREE 12-HR. RUNS & SEVERAL SHORT DURATION RUNS CONFIRMED REACTOR OPERATILIRY.

- POLYCRYSTALLINE BOULE PULLED FROM MELTED POWDER SHOWED RESISTIVITY OF 55 nCM, P TYPE.

- PDU OPERATION WAS SUCCESSFULLY COMPLETED AND ALL ITS OBJECTIVES WERE MET.

- EPSDU PYROLYSIS REACTOR DESIGN WAS INITIATED.

Fluid-Bed Reactor Summary

- PDU DESIGN & FABRICATION COMPLETED.

- INSTALLATION & CHECKOUT IN PROGRESS.

- OPERATING PROCEDURES PREPARED.

- STARTUP WITH HYDROGEN PLANNED FOR APRIL.
SILICON MATERIAL TASK

Quality-Control Activities Summary

- Phosphine dopant profile completed in epitaxy reactor.
  - Provides confirmation of analytical method and calibration for rapid go/no go spot evaluation of silane.

- Polysilicon rods grown with controlled diborane or phosphine dopant level in silane feed gas.
  - Provides confirmation of analytical method and calibration for on-line silane quality monitoring.

- Diborane/silane vapor-liquid equilibrium measured at EPSDU operating conditions.
  - Near ideal behavior confirms EPSDU design basis.

- EPSDU A/C laboratory facility ordered.

- On-line sampling devices designed.

Melting and Consolidation Summary

- Silicon shutter design & procurement completed.

- Installation & checkout in progress.

- Preliminary tests using chunk silicon to start soon.
CONTRACTOR: BATTELL COLUMBUS LABORATORIES (BCL)

PRICE PROJECTION (1980$, 1000-MT/YR, 20% ROI)

ASSUMPTIONS:
FLUIDIZED-BED REACTORS: TWO 29-INCH DIAMETER OR ONE 41-INCH DIAMETER
ELECTROLYSIS CELLS FOR ZINC AND CHLORINE RECYCLE: ONE, TWO, SIX, OR TWELVE

<table>
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<tr>
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<th>2 REACTORS</th>
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Progress Since 16th PIM

- PDU OPERATING EXPERIENCE REVIEWED TO DEFINE NEEDS FOR IMPROVEMENT OF DESIGN AND PROCEDURE
- MODIFICATIONS OF DESIGN AND PROCEDURE MADE, RESULTING IN IMPROVED PDU OPERATION
- OUTGASSING OF RESIDUAL ZINC FROM 400μm-DIA MINIPLANT PRODUCT GRANULES MODELLED TO PERMIT EXTRAPOLATION TO EXPECTED 800μm PRODUCT
PDU Activities Since 16th PIM: Overview

• REVIEW OF OPERATING EXPERIENCE TO IDENTIFY NEEDED SYSTEM IMPROVEMENTS
• UPGRADING OF PDU SYSTEM
• RESUMPTION OF PDU OPERATION
• SUMMARY OF EXPERIENCE

PDU Improvements

• REDESIGNED REACTOR INLET AND OUTLET CONNECTIONS
• CORRECTED REACTOR SHELL WARPAGE
• MODIFIED QUARTZ DELIVERY TABLE
• IMPROVED ZnCl₂ RECIRCULATION IN CONDENSER
• IMPROVED ZINC FEED SYSTEM
• MODIFIED REACTOR DISTRIBUTOR PLATE

PDU Operation

• TEN RUNS CONDUCTED
• SILICON PRODUCTION ACHIEVED IN SEVEN RUNS

Summary of PDU Experience

• SYSTEM OPERABILITY IMPROVED
• PRESENT GRAPHITE-LINED STAINLESS STEEL REACTOR REQUIRES BASIC REDESIGN TO BE COMMERCIALLY PRACTICAL
• ZINC REDUCTION PROCESS STILL TECHNICALLY AND ECONOMICALLY VIABLE WITH APPROPRIATE DESIGN OF FLUIDIZED-BED REACTOR
Zinc Removal

OBJECTIVE

• TO STUDY THE REMOVAL OF AN EXPECTED ~100 ppmw RESIDUAL ZINC FROM THE GRANULAR PRODUCT OF THE ZINC VAPOR REDUCTION OF SiCI, IN A FLUIDIZED BED OF SEED PARTICLES.

APPROACH

1. CONSIDER OPTIONS.
2. STUDY VACUUM OUTGASSING OF MINIPLANT PRODUCTS CONTAINING ~160 ppmw AND ~2300 ppmw ZINC.
3. DEVELOP MODEL FOR EXTRAPOLATION OF MINIPLANT-PRODUCT RESULTS TO LARGER SIZE.
4. REVIEW OPTIONS AND DATA, AND RECOMMEND PROCEDURE.

OPTIONS

1. POST-PROCESS FUSION OF ZINC GRANULES (REJECTED BECAUSE OF LOSS OF CONVENIENT FREE-FLOWING PRODUCT FORM).
2. POST-PROCESS HEAT TREATMENT OF GRANULES IN VACUUM OR INERT GAS, AT E.G., 1100 C (TEMPERATURE LIMITED BY SINTERING AND LOSS OF FREE-FLOWING FORM).
3. POSTPONE ZINC REMOVAL UNTIL FUSION IN INGOT FORMATION OR SHEET FORMING PROCESS.

Conclusions From Outgassing Data

(1) MODEL A (DIFFUSION OF ZINC THROUGH SOLID SILICON SPHERE) IS INCONSISTENT WITH DATA AT DIFFERENT CONCENTRATION LEVELS.
(2) MODEL C (ZINC VAPOR PERMEATION OF MICROPORES ORIGINALLY OCCUPIED BY ZINC) RESOLVES BEHAVIOR AT DIFFERENT CONCENTRATIONS, BUT RATIO OF INITIAL TO LATER OUTGASSING RATE IS TOO LOW FOR SPHERICAL PARTICLES (ALSO TRUE FOR MODEL A).
(3) MODEL B (DIFFUSION OF ZINC THROUGH SOLID SILICON TO CONNECTED ZERO-IMPEDANCE MICROPORES) RESOLVES DATA WITH ASSUMPTION THAT PORE SIZE OR DEGREE OF POROSITY IS A FUNCTION OF ZINC CONCENTRATION. RATIO OF INITIAL TO LATER OUTGASSING RATE IS TOO HIGH FOR UNIFORM POROSITY. CAN BE RESOLVED BY ASSUMING RANGE OF PORE SIZES.
(4) NO CORRELATION IS COMPLETELY SATISFACTORY, BUT EFFORT TO RESOLVE IS NOT JUSTIFIABLE.
(5) WORST-CASE SCENARIO (MODEL C) PREDICTS HUNDREDS OF HOURS OUTGASSING TIME FOR 800-μm-DIAMETER GRANULES AT 1100 C. IF CONNECTED POROSITY IS CONFIRMED (MODEL B) ONLY TENS OF HOURS MAY BE NEEDED.
(6) AS OUTGASSING ADDS TO COST, IMPLICATIONS OF REMOVING ZINC IN INGOT- OR SHEET-GROWTH PROCESS SHOULD BE SERIOUSLY CONSIDERED.
SILICON MATERIAL TASK

Volumetric Ratio of Zn Condensate to SiO Condensate in Cz Ingot Growth

- RATE OF ATTACK OF SiO₂ BY Si(I) = 1 x 10⁻⁵ cm min⁻¹ [CHANÉY & VARKER, J. CRYSTAL GROWTH 33, 188 (1976)]
- Si(I) SATURATED WITH O AT 30 ppmw

\[
\frac{V_{Zn}}{V_{SiO}} = \frac{0.0074 \, w}{0.335t \left( \frac{1}{h} + \frac{4}{d} \right) + 1}
\]

\( V_{Zn} \) = Zn CONDENSATE VOLUME, cm³
\( V_{SiO} \) = SiO CONDENSATE VOLUME, cm³
\( w \) = ZINC CONCENTRATION, ppmw
\( t \) = Si/SiO₂ EXPOSURE TIME, minutes
\( h \) = INITIAL SILICON DEPTH, cm
\( d \) = CRUCIBLE DIAMETER, cm

PREDICTION FOR \( d = 18 \) cm, \( h = 19 \) cm and \( t = 180 \) min:

<table>
<thead>
<tr>
<th>( w ), ppmw</th>
<th>( \frac{V_{Zn}}{V_{SiO}} )</th>
</tr>
</thead>
<tbody>
<tr>
<td>10</td>
<td>0.005</td>
</tr>
<tr>
<td>50</td>
<td>0.024</td>
</tr>
<tr>
<td>100</td>
<td>0.048</td>
</tr>
<tr>
<td>500</td>
<td>0.238</td>
</tr>
<tr>
<td>1000</td>
<td>0.475</td>
</tr>
</tbody>
</table>

CONCLUSION

AT ≤ 100 ppmw ZINC IN SILICON, ZINC CONDENSATE SHOULD NOT BE NOTICED IN SiO CONDENSATE.

Project Summary

- TECHNICAL AND ECONOMIC FEASIBILITY OF THE ZINC REDUCTION PROCESS REMAINS PROMISING
- 13%-EFFICIENT CELLS (WITH AR COATING) ATTEST TO UTILITY OF THE PRODUCT
- UNDERSTANDING OF PROCESS ENHANCED BY PDU OPERATION
- BASICALLY NEW FLUIDIZED-BED REACTOR DESIGN NEEDED FOR COMMERCIAL OPERATION
SILICON MATERIAL TASK

HYDROCHLORINATION PROCESS
MASSACHUSETTS INSTITUTE OF TECHNOLOGY

<table>
<thead>
<tr>
<th>TECHNOLOGY</th>
<th>REPORT DATE</th>
</tr>
</thead>
<tbody>
<tr>
<td>POLYCRYSTALLINE SILICON</td>
<td>FEBRUARY 4, 1981 17th P.M</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>APPROACH</th>
<th>STATUS</th>
</tr>
</thead>
</table>
| HYDROCHLORINATION OF METALLURGICAL GRADE SILICON TOGETHER WITH SILICON TETRACHLORIDE AND HYDROGEN TO FORM TRICHLOROSILANE FOR PRODUCING SILICON | 1. REACTION KINETICS MEASUREMENT
|                    | • TEMPERATURE              |
|                    | • PRESSURE                 |
|                    | • \(\text{H}_2/\text{SiCl}_4\) FEED RATIO |
|                    | • COPPER CATALYST CONCENTRATION |
|                    | • PARTICLE SIZE DISTRIBUTION |
|                    | • EFFECT OF IMPURITIES IN SILICON |

<table>
<thead>
<tr>
<th>CONTRACTOR</th>
<th>GOALS</th>
</tr>
</thead>
</table>
| MASSACHUSETTS INSTITUTE OF TECHNOLOGY | TO SUPPORT THE UNION CARBIDE SILANE-TO-SILICON PROCESS BY CONDUCTING EXPERIMENTAL AND THEORETICAL STUDIES,

- ESTABLISH FUNDAMENTAL UNDERSTANDING OF HYDROCHLORINATION OF METALLURGICAL GRADE SILICON IN TERMS OF REACTION KINETICS AND ROLE OF CATALYST
- OPTIMIZE THE REACTION CONDITION FOR THE HYDROCHLORINATION STEP

<table>
<thead>
<tr>
<th></th>
<th>II MASS LIFE STUDY</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>• NO CHANGE IN REACTION RATE AFTER 238 HOURS - LONG MASS LIFE</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th></th>
<th>III CORROSION STUDY</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>• NO CORROSION OF THE METAL REACTOR MADE OF INCOLOY 800</td>
</tr>
<tr>
<td></td>
<td>• STABLE SILICIDE PROTECTIVE FILM ON REACTOR WALL</td>
</tr>
</tbody>
</table>

Summary of Progress

- REACTION RATE AT 500 PSIG, 500°C REINFORCES THE UNION CARBIDE ENGINEERING DESIGN
- COPPER CATALYST INCREASES REACTION RATE BY 100%
- REACTION RATE INDEPENDENT OF Si PARTICLE SIZE
- IMPURITIES IN M.G. SILICON INCREASE REACTION RATE
- LONG MASS LIFE MEANS REACTION CAN BE RUN FOR LONG Periods OF TIME WITH NO INTERRUPTION
- CORROSION OF THE METAL REACTOR IS NOT A PROBLEM
- INCOLOY 800 IS A GOOD CHOICE AS THE MATERIAL OF CONSTRUCTION OF THE HYDROCHLORINATION REACTOR
What Has Been Done

HYDROCHLORINATION REACTOR DEVELOPMENT AT
THE MASSACHUSETTS INSTITUTE OF TECHNOLOGY

I ENGINEERING DATA
• REACTION KINETICS, YIELD, CONVERSION
• CATALYST, IMPURITIES
• SILICON PARTICLE SIZE, MASS LIFE
• CORROSION STUDY

II CONCLUSIONS
• EFFICIENT REACTION, HIGH YIELD AND CONVERSION
• COPPER CATALYST DOUBLES REACTION RATE
• LONG PERIODS OF CONTINUOUS OPERATION
• CONVENTIONAL METAL ALLOYS FOR REACTOR

III RECOMMENDATION
• MAXIMIZE REACTOR PRESSURE 500 PSIG
• ADD COPPER CATALYST TO INCREASE RATE
• INCOLOY 800 AS MATERIAL OF CONSTRUCTION FOR THE REACTOR

Potential Application to Polycrystalline Silicon Technology

I THE CURRENT SIEMENS TECHNOLOGY FOR POLY SILICON

\[
\text{SiHCl}_3 + \text{H}_2 \xrightarrow{1000^\circ\text{C}} \text{Si}, \text{SiCl}_4, \text{HCl}, \text{LITES, HEAVIES}
\]

II THE HYDROCHLORINATION OF SiCl_4

\[
3 \text{SiCl}_4 + 2 \text{H}_2 + \text{Si} \rightleftharpoons 4 \text{SiHCl}_3
\]

• IT PRODUCES THE STARTING SiHCl_3 FOR THE SIEMENS TYPE REACTOR AT ESSENTIALLY 100% EFFICIENCY
• IT CONSUMES THE BY-PRODUCT SiCl_4
• IT CAN ALSO CONVERT HCl AND OTHER BY-PRODUCTS TO SiHCl_3
• IT FITS PERFECTLY INTO THE SIEMENS PRODUCTION SCHEME TO FORM A CLOSED LOOP PROCESS
• SUBSTANTIAL SAVINGS ON RAW MATERIAL COST CAN BE REALIZED
SILICON MATERIAL TASK

DICHLOROSILANE CVD PROCESS
HEMLOCK SEMICONDUCTOR CORP.

<table>
<thead>
<tr>
<th>TECHNOLOGY</th>
<th>REPORT DATE</th>
</tr>
</thead>
<tbody>
<tr>
<td>POLYCRYSTALLINE SILICON</td>
<td>FEBRUARY, 1981</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>APPROACH</th>
<th>STATUS</th>
</tr>
</thead>
<tbody>
<tr>
<td>CHEMICAL VAPOR DEPOSITION OF SILICON FROM DICHLOROSILANE (DCS)</td>
<td>SAFETY RELATED REDESIGN OF PDU, INTERMEDIATE REACTOR FEED PROGRAMS COMPLETE</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>CONTRACTOR</th>
<th></th>
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<tbody>
<tr>
<td>HEMLOCK SEMICONDUCTOR CORPORATION</td>
<td></td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>GOALS</th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>• DEMONSTRATE PROCESS FEASIBILITY</td>
<td></td>
</tr>
<tr>
<td>• ESTABLISH TECHNICAL READINESS BY OPERATION OF EPICLUSIZED TO ABOUT 1525 MT/yr</td>
<td></td>
</tr>
<tr>
<td>• SILICON PRICE OF LESS THAN $2.1/KG (1980$ $0.700/mt, 22% ROI) IN LOW-RISK PROGRAM</td>
<td></td>
</tr>
<tr>
<td>• DEFINE PROCESS ECONOMICS</td>
<td></td>
</tr>
</tbody>
</table>
SILICON MATERIAL TASK

Autoignition Temperature

<table>
<thead>
<tr>
<th>Conc.</th>
<th>Temp. (°C ± 5°C)</th>
</tr>
</thead>
<tbody>
<tr>
<td>DCS</td>
<td>58</td>
</tr>
<tr>
<td>DCS/H₂</td>
<td>255</td>
</tr>
<tr>
<td>10/90</td>
<td></td>
</tr>
<tr>
<td>EQUILIBRATED TCS</td>
<td>130</td>
</tr>
<tr>
<td>DCS/TCS/STC 10/86/10</td>
<td></td>
</tr>
<tr>
<td>TCS</td>
<td>215</td>
</tr>
</tbody>
</table>

LITERATURE
Explosion Severity

- PRESSURE - TIME BEHAVIOR CHARACTERISTIC OF COMBUSTION IN A CLOSED VESSEL

![Graph of Experimental Pressure vs. Time](image)

**CH₄/AIR**
- AVERAGE = 900 PSI/SEC
- MAXIMUM = 2700 PSI/SEC

<table>
<thead>
<tr>
<th>SYSTEM COMPOSITION</th>
<th>AVG. PSI/SEC</th>
<th>MAX. PSI/SEC</th>
</tr>
</thead>
<tbody>
<tr>
<td>DCS</td>
<td>6. x 10⁴</td>
<td>1 x 10⁶</td>
</tr>
<tr>
<td>DCS/H₂ 10/90</td>
<td>3.2 x 10⁴</td>
<td>5.4 x 10⁴</td>
</tr>
<tr>
<td>H₂ (LITERATURE)</td>
<td></td>
<td>2.4 x 10⁴</td>
</tr>
<tr>
<td>EQUILIBRATED TCS</td>
<td></td>
<td>2.4 x 10⁴</td>
</tr>
<tr>
<td>DCS/TCS/STC 10/80/10</td>
<td></td>
<td></td>
</tr>
<tr>
<td>TCS (17%, 23% IN AIR)</td>
<td></td>
<td>1.2 x 10³</td>
</tr>
</tbody>
</table>
SILICON MATERIAL TASK

DCS Hazards Summary

- LOW AIT FOR DCS
  $$\Rightarrow$$ IGNITION OF DCS IS EXTREMELY FACILE, AND CAN BE UNPREDICTABLE

- HYDROLYSIS PRODUCTS ARE COMBUSTIBLE

- DCS/AIR MIXTURES HAVE HIGH EXPLOSION SEVERITY POTENTIAL
  $$\Rightarrow$$ REMOTE OR PROTECTED LOCATION FOR EQUIPMENT SHOULD BE USED

- EXPLOSIVE OUTPUT TRIALS INDICATED DEFLAGRATION RATHER THAN DETONATION

- DILUTION OF DCS WITH H₂ ATTENUATES HAZARDS

PDU Revised Design Features

- REMOTE LOCATION

- NO DCS STORAGE

- MINIMAL DCS HOLDUP IN EQUIPMENT

- DCS DILUTED WITH H₂ BEFORE TRANSPORT

- REMOTE OPERATION
SILICON MATERIAL TASK

Purity of Si Grown From Laboratory Rearranger-Supplied Chlorosilanes

<table>
<thead>
<tr>
<th>TCS SOURCE</th>
<th>CATALYST</th>
<th>BORON (PPBA)</th>
<th>DONOR (PPBA)</th>
<th>AL (PPBA)</th>
<th>CARBON (PPMA)</th>
</tr>
</thead>
<tbody>
<tr>
<td>CONTROL</td>
<td>---</td>
<td>0.19</td>
<td>1.1</td>
<td>0.30</td>
<td>0.5</td>
</tr>
<tr>
<td>A</td>
<td>DOWEX (24 °C)</td>
<td>0.48</td>
<td>1.4</td>
<td>0.09</td>
<td>0.5</td>
</tr>
<tr>
<td>CONTROL</td>
<td>---</td>
<td>0.15</td>
<td>1.7</td>
<td>0.18</td>
<td>0.3</td>
</tr>
<tr>
<td>A</td>
<td>DOWEX (77 °C)</td>
<td>0.69</td>
<td>1.2</td>
<td>0.06</td>
<td>0.4</td>
</tr>
<tr>
<td>CONTROL</td>
<td>---</td>
<td>0.11</td>
<td>0.84</td>
<td>0.26</td>
<td></td>
</tr>
<tr>
<td>B</td>
<td>DOWEX (77 °C)</td>
<td>0.24</td>
<td>1.0</td>
<td>0.17</td>
<td></td>
</tr>
<tr>
<td>A</td>
<td>DOWEX (77 °C)</td>
<td>0.41</td>
<td>1.7</td>
<td>0.51</td>
<td></td>
</tr>
</tbody>
</table>

CONCLUSIONS:
- Silicion purity greatly exceeds solar requirements
- Dowex resin is not a direct source of impurities
- Dowex resin may serve as indirect source of boron in some situations

Intermediate Reactor Task

OBJECTIVES

- Demonstrate safe and efficient production of silicon from commercial DCS in an intermediate sized reactor
- Focus on system operability, especially at large rod diameters

STATUS

- Project delayed for safety reasons
- Feed system completely redesigned
- Construction underway
- Startup scheduled for March, 1981
HSC Low-Cost Si Process Cost-Capital Summary

For a 1000 metric tonne plant:

\[ \text{(1980) $/kg Silicon} \]

<p>| | |</p>
<table>
<thead>
<tr>
<th></th>
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</tr>
</thead>
<tbody>
<tr>
<td>Manufacturing Cost</td>
<td>15.47</td>
</tr>
<tr>
<td>Profit (20% ROI)</td>
<td>4.38</td>
</tr>
<tr>
<td>Product Cost</td>
<td>19.85</td>
</tr>
</tbody>
</table>

Manufacturing Capital: $21.9 M

*Note: In PIM handout, price of Si product was erroneously given as $18.95/kg.

Problems and Concerns

- Project delay due to safety considerations
## DEFINITION OF PURITY REQUIREMENTS

WESTINGHOUSE ELECTRIC CORP.

<table>
<thead>
<tr>
<th>Technology</th>
<th>Report Date</th>
</tr>
</thead>
<tbody>
<tr>
<td>Impurity effects in silicon</td>
<td>2/4/81</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Approach</th>
<th>Status</th>
</tr>
</thead>
<tbody>
<tr>
<td>Analysis of silicon material and solar cells with controlled impurity additions</td>
<td>Phase IV experimental program approximately 70% completed</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Contractor</th>
<th>Recent Results:</th>
</tr>
</thead>
<tbody>
<tr>
<td>Westinghouse Electric Corp., R&amp;D Center</td>
<td>- Spectral response data indicate both impurities and grain boundaries reduce carrier lifetime in polycrystal cells.</td>
</tr>
<tr>
<td></td>
<td>- Accelerated aging of Ni-doped cells projects time to failure over 20 years</td>
</tr>
<tr>
<td></td>
<td>- Combined electrical bias/temperature stress show no effect for seven impurities up to 205°C</td>
</tr>
<tr>
<td></td>
<td>- Impurity model for narrow base, BSF and wide base, ohmic contact high efficiency devices completed.</td>
</tr>
</tbody>
</table>

### Phase IV

**Goals**

- Evaluate impurity effects in:
  - Polycrystalline silicon
  - High efficiency cells
  - Experimental silicon material
  - Cells subjected to processing e.g. gettering
  - Cells treated to simulate long term behavior

### Graph

- **Uncontaminated Single Crystal**
- **Uncontaminated (76) Poly Crystal**
- **Poly Crystal (216)** with $10^{15}$ cm$^{-3}$ Cr
- **Single Crystal (004)** with $10^{15}$ cm$^{-3}$ Cr

---

125
SILICON MATERIAL TASK

STD. CELL \( \eta = 14\% \)
- Efficiency Projected by Impurity Model
- Efficiency Calculated by Finite Element Model

WIDE BASE CELL \( \eta = 15.5\% \), \( W_b = 76.5 \mu m \)
- Impurity Model Curve Projected from Standard Design Cell Behavior
- Finite Element Model Curve
SILICON MATERIAL TASK

1. Efficiency Projected by Impurity Model
2. Efficiency Calculated by Finite Element Model

BSF CELL ($\% = 15.4\%, W_e = 150 \mu m$)

○ Efficiency Projected by Impurity Model
▲ Efficiency Calculated by Finite Element Model
SILICON MATERIAL TASK

EFFECTS OF IMPURIETIES
ON SOLAR CELL PERFORMANCE
C.T. SAH ASSOCIATES

<table>
<thead>
<tr>
<th>TECHNOLOGY IMPURITY EFFECTS IN SILICON SOLAR CELLS</th>
<th>REPORT DATE 81/02/05</th>
</tr>
</thead>
<tbody>
<tr>
<td>APPROACH CAPACITANCE TRANSIENT SPECTROSCOPY AND P/N JUNCTION DIODE REVERSE SWITCHING CURRENT TRANSIENT ARE USED TO DETERMINE THE THERMAL CAPTURE RATES OF ELECTRONS AND Holes AT THE IMPURITY RECOMBINATION LEVELS IN SILICON.</td>
<td>STATUS LARGE SERIES RESISTANCE HAVE BEEN OBSERVED FROM LOW TEMPERATURE D.C. CURRENT-VOLTAGE CHARACTERISTICS OF BOTH SCHOTTKY AND P/N JUNCTION DIODES DOPED WITH Ti, V, Cr AND Mo. THE LARGE RC TIME CONSTANT MAKES THE PUBLISHED ELECTRON CAPTURE RATE AT THE $E_C$-228 mV Ti LEVEL UNRELIABLE DUE TO THE VERY SHORT ELECTRON FILLING TIME ($&lt; 10$ ns). A 30-60 ohm-cm n-Si doped with Ti IS GROWN TO GIVE LARGER ELECTRON CAPTURE TIME AT THE Ti LEVEL.</td>
</tr>
<tr>
<td>CONTRACTOR C. T. SAH ASSOCIATES</td>
<td>GOALS TO DETERMINE THE CAPTURE RATES ACCURATELY SO THAT THE MAXIMUM ALLOWABLE RECOMBINATION IMPURITY CONCENTRATION AT A GIVEN AM1 EFFICIENCY CAN BE PREDICTED.</td>
</tr>
</tbody>
</table>
TECHNOLOGY DEVELOPMENT AREA
Large-Area Silicon Sheet Task

TECHNOLOGY SESSION
J. Liu, Chairman

Shaped-Sheet Technology

Mobil Tyco Solar Energy Corp. (EFG)

Several temperature profiles of cartridges #2 and #3 (the two cartridges furthest away from the melt replenishment port) in the multiple-ribbon-growth machine (Machine 16) have been made. The data indicate a temperature variation of about 20 to 30° across the die tops. This cannot be corrected with adjustments of the present cartridge end heaters and is attributable to undue influence of the main furnace heaters. It is apparent that this condition is adversely affecting the optimum growth throughput of the EFG ribbons in the multiple-ribbon machine. Five to six different modifications of the main furnace heaters were made to assess a proper direction toward solving this poor thermal symmetry. Several subsequent multiple-ribbon growth runs were attempted.

One hour and 49 minutes of simultaneous three-ribbon growth was demonstrated as part of a 5-hour, 20-minute run. The run was terminated due to a shortage of starting material in the necessary rod form. A total of 19 meters of 10-cm-wide ribbon was grown from the three cartridges at an average rate of 3.3 cm/min.

Several high-growth-rate runs were made in Machine 17 using CO₂ ambient and a new die-shield configuration.

Runs made in Machine 18 with CO and CO₂ ambient and improved gas purging in the vicinity of the die top resulted in production of 7 to 8 meters of 10-cm-wide ribbon material.

Westinghouse Electric Corp. (Web)

Westinghouse is now in the design phase of a web ESGU. This includes some redesign of the present web grower configuration.

Engineering drawings of the dendritic web ESGU mechanical system were received at JPL for review and a preliminary design review was held with Westinghouse at JPL.

Work continues on the design of the low-cost modifications of the web-growth system. Electronic developments include: redesign of the closed-loop melt-level controller; a re-specified custom temperature controller for a reduction in the component cost; installation for testing of the start-up programmer, and identification of a supplier for the web-thickness.
LARGE-AREA SILICON SHEET TASK

Sensor-controller. Mechanical design developments include: identification of a lower-cost stainless-steel pipe for the furnace chamber wall and design of an inexpensive web take-up reel.

Advanced web throughput runs have begun and faster growth rates have been achieved while maintaining thickness (Westinghouse relates stress to ribbon thickness, not pull speed or width). This development, like the planned web width-control study, depends upon passive heat-shield design development.

Honeywell Corp. (SOC)

Both the SCIM II and dip-coat machines were operated during this period; 10-cm-wide slotted substrates were coated by SCIM II at speeds of 3 to 5 cm/min. Areas of uniform thickness, 100 µm, were deposited on the substrate.

Problems encountered and overcome included the continuous formation of dendrites along the center of the sheet, the freezing of silicon between the crucible and the coating trough, mullite substrate cracking and non-uniformity of temperature along the furnace tunnel. The best SCIM-coated cell showed an efficiency of 7.5% AM1.

SOC material dip-coated at speeds of 3 to 5 cm/min continues to provide cells of 10-10.5% AM1 efficiencies.

The latest contract expired December, 1980. Further work in this technology will be funded by SERI, and will be managed jointly by JPL and SERI.

Ingot Technology

Kayex Corp. (Advanced Cz)

A design review of the Advanced Cz ESGU was held at JPL in October. The ESGU will be a prototype of equipment suitable for high-volume silicon ingot production (150 kg of ingots from a single crucible, 2.5 kg/h throughput, 90% yield). The review consisted of presentation and discussion of design and assembly drawings, system diagrams and machine and process specifications together with appropriate technical justifications.

Kayex has commenced modification of a CG 2000 (to be called CG 6000) for the Cz ESGU. All of the long-lead-time items are in, and the chamber, framework, and crucible-lift mechanism are assembled; 15-in-dia crucibles are in and are being analyzed for impurities. Testing and debugging has begun on the console electronics. Growth-parameter sensors and microprocessor test and definition continue for automated growth.

Siltec Corp. (Advanced Cz)

Siltec's Advanced Cz contract expired in September, 1980; negotiations are under way for continuation of the program into the next phase, ESGU development. Siltec presently is working with in-house funding on two major problem areas. These center mainly on the transfer-tube heater system and the
LARGE-AREA SILICON SHEET TASK

automatic ingot-diameter control. Using a new modified diameter controller, Siltec has successfully demonstrated the growth of a large ingot (weighing approximately 60 kg) from the CLF furnace with a uniform 13.8-cm diameter along the entire length.

Crystal Systems, Inc. (HEM)

A redirection of program goals for the HEM casting technology was made during this reporting period. The new goal calls for the growth of HEM ingots to yield 35 kg (30 x 30 x 15 cm) in a 56-hour cycle time. The other goals of the original contract remain the same.

Several growth runs aimed at improving the quality of the ingot material have been completed. These are tests with various growth parameters; such runs will continue in coming months.

Successful growth of several 35-kg ingots was reported by CSI. A growth rate of 28 hours per 35-kg ingot with a total cycle time of 56 hours has been achieved. No further attempt to improve the cycle time was made in this period. Emphasis at this point is on optimization of the growth process to improve material quality. CSI has noted a substantial increase in the amount of single-crystal material across the bottom of the ingots for these runs.

Preliminary results from a material analysis of the HEM material showed a large amount of precipitates, presumably the source of carbon impurities in the material. These precipitates are also the source of the high concentration of dislocations in this material. The impurities observed in this material are undoubtedly due to the graphite heaters in the HEM furnace.

Semix Inc. (Semicrystalline Casting)

Terms of a confidentiality agreement have been established and the first meaningful technical review took place during this reporting period. Technical and economic data that were received at and after the PIM are now being analyzed to ascertain the validity of Semix's process claims.

Hardware design and fabrication continues on the casting, wafering and test subsystems. In the wafering area, Semix is planning to evaluate high-speed multi-blade slicing and ID wafering by various manufacturers. Data collection for a SAMICS analysis report has been completed. A review draft of this report, entitled "Definition of Present Technology and Economic Considerations," has been received by DOE/JPL; a final version illustrating 1982 and 1986 sheet costs will be made based on comments and suggestions from JPL and DOE.
LARGE-AREA SILICON SHEET TASK

Silicon Technology Corp. (Advanced ID Sawing)

STC has replaced the hollow spindle of the prototype R&D slicing machine with a solid ball-bearing spindle. This successfully reduced the excessive blade vibrations observed with the hollow spindle. Some feed-column-related vibration remains. Nevertheless, 15-cm-dia wafers are now being successfully plunge-cut at rates up to 4.5 cm/min with slice and kerf thickness (d and k) each equal to 12.5 mils at >90% yield. Edge chipping remains the major fault with rotary slicing, but slow rates (3.8 cm/hr) and high slice thickness (d = 20 mils, k = 11 mils) are also problems.

For the 10 x 10-cm ingot wafering, both single-crystal material from Crystal Systems, Inc., and polycrystalline material were used. The minimum thickness of the poly wafers was 6.5 mils and the kerf loss was 11 mils. (The d + k value for the desired goal of 25 wafers/cm is 16 mils.) The average yield for these runs was greater than 90%, the material being sliced at an average rate of 2.5 cm/min (0.25 wafer/min). One observation made by STC was that polycrystalline material was easier to slice than single-crystal and had greater yields. Also, STC noted that the 6.5-mil wafers were very difficult to handle.

The use of thin core material for the saw blades (4.8 mil or 120 µm thick) resulted in some blade deflection causing a blade-rubbing problem with the wafers. This problem does not occur with the thicker (6-mil) core material. More 4.8-mil core material of different steel composition has been ordered and will be used in subsequent experiments.

Siltec Corp. (Enhanced ID Slicing)

Slicing experiments with the 42-cm (16 5/8-in.) blade head have resulted in the production of 250-µm (10-mil)-thick wafers with 200-µm (8-mil) kerf thickness from 10-cm-dia silicon ingots. These experiments were done with ingot rotation and yields of 85-90% have been achieved. Blade life, however, has been much less than expected (about 200 cuts as opposed to 800-1000 expected). Wafer throughput in these demonstrations averaged 0.25 wafers/min.

Crystal Systems, Inc. (FAST)

An attempt at slicing a 10-cm dia ingot at 25 wafers/cm was successfully completed at CSI during this period. The yield was <30%. The slicing rate was a moderate 2.9 mils/min; slice and kerf thickness, d + k, was 7 mils + 9 mils. CSI also tried to slice a 15-cm-dia ingot but aborted the run after approximately 13 cm. The reason for the failure was given as a combination of wire and roller degradation.

One significant achievement during this period was that one wire pack electroplated in house was able to slice through three ingots with yield of 85%, 80% and 38%, respectively. The last run might have also had an 80% yield, but the epoxy holding the ingot in place loosened and the ingot shifted during the last 20% of slicing.
Material Evaluation

Applied Solar Energy Corp. (Cell Fabrication)

Cells fabricated on vertically sliced HEM wafers (Ingot No. 41-41C) show that the material in some places is as good as Cz material. An average taken over one entire slice indicates that the HEM efficiency is 92% of that of the Cz controls (HEM average: 10.2% AM1, Cz average: 11.1% AM1). No definite pattern of cell efficiency was obtained over the cross-section of the ingot although there is a trend toward lower efficiency for cells from the seed area. Horizontal sections of the same ingot (41-41C) have been fabricated into cells and tested. The results will be correlated with the results for the vertical sections. Material from the same ingot will also be tested for dislocation densities and oxygen and carbon concentrations.

Gettering experiments on HEM ingot material were also performed during this period. The results are similar to those in earlier gettering experiments, i.e., cells made from material at the top of the ingot improve substantially with gettering whereas those from material at the bottom of the ingot showed little improvement. DLTS measurements reveal a wide band of trapping levels in this material indicating a large number of impurities.

Data from dislocation-etch experiments on the HEM and EFG material revealed that dislocations are evenly distributed throughout the HEM ingot, while the EFG ribbons showed a significant drop in dislocation density on ribbon grown in a CO atmosphere.

A two-step diffusion process on polycrystalline EFG, Wacker and Hamco Cz materials did not improve the Wacker or Hamco Cz cell performances and degraded the performance of the EFG cell. A 9-hour, 750°C pre-diffusion step has shown a 10% improvement in the short-circuit current on Wacker Silso material.

University of Missouri, Rolla (Reactant Gas Studies)

UMR visited three Task II sheet growth contractors to measure oxygen partial pressures in their silicon growth systems during this reporting period. The three contractors are Westinghouse, Hon-Well and Crystal Systems, Inc.

At Westinghouse, the web growth system proved to be very stable, with little change in the partial pressure of oxygen with varying gas flow rates. There also was no evidence of back diffusion of oxygen into the system. These findings were of particular interest to Westinghouse in that they indicate that some cost savings can be made by reducing gas flow rates.

Cornell University (Silicon Sheet Characterization)

HEM samples were investigated by a combination of EBIC and optical microscopy-etching. It is found that high-angle grain boundaries in HEM are only weakly electrically active. Centers of electrical activity are due to
BOUNDARY DISLOCATIONS. Many grain boundaries that appear macroscopically to be high-angle boundaries are really made up of alternating sections of coherent twin or low-angle boundaries, or both.

Materials Research, Inc. (Silicon Microstructure)

MRI is currently characterizing the defect structure of both the surface and cross-section areas of web material from Westinghouse. The through-the-thickness defect density may or may not be similar to the surface density; this is to be investigated. Two web samples have been mounted edge-on and are presently being prepared for defects and image characterization.

Honeywell's SOC material has been difficult to section. The entire width of the mullite substrate has had to be bonded to an aluminum support plate during cutting.

In-House Activities

MBS Slurry Tests: Four additional types of corrosion inhibitors for a water-based slurry to be used in MBS wafering were evaluated. The evaluations consisted of fatigue testing of the 1095 carbon steel MBS blades in a water solution of the corrosion inhibitors. The fatigue lives of blades tested in three of the four types of inhibitors evaluated were greater than the fatigue lives of such blades tested in the standard PC oil used in MBS slurries. These water-based corrosion inhibitors would provide a large cost savings for MBS wafering.

MBS Blade Tests: Lateral deflection and twist tests were made on 1095 high-carbon steel and three types of metallic glass (Metglas) ribbons for the MBS wafering technology. The lateral deflection tests are used to compare flexibility of metallic glass ribbon with that of 1095 carbon blades under equivalent tensile forces in MBS wafering and the lateral twist test results indicate that a very small force can produce an appreciable twisting of the metallic glass ribbons.

Crystal Growth: Two runs were made with the in-house Czochralski crystal growth system using a new flexible seed holder in attempts to grow and evaluate crystals from Battelle-produced polysilicon starting material. In the first effort, melting as-received poly resulted in clouds of vapor that obscured the operator's view and made growth difficult. For the second run the poly was leached for 20 minutes in HF, rinsed and dried before melting. It produced much less vapor. In both cases, small single crystals were grown and are being evaluated.

Characterization: A preliminary measurement of oxygen content in HEM material using an IR spectrophotometer on material adjacent to that used for the solar cells indicate a correlation between cell efficiency and oxygen content in the material. The lower-efficiency cells were made from material that exhibited high oxygen content.
Preliminary experiments on silicon grain boundaries using a light-induced deep-level transient spectroscopy (DLTS) method has shown some signals from the minority carrier trapping levels. More investigations are under way to improve the resolution of this technique. This technique can provide information concerning minority carrier trapping levels at the grain boundaries that a conventional DLTS measurement cannot give.

Economic Analysis: A Monte-Carlo simulation model program has been improved to include the consideration of ingot technology alternatives. Several runs were made with current data and the results indicate that there is need for further improvement of the model for an equitable comparison of results from different sheet technologies. A program to examine the sensitivity of various parameters has been developed for the EFG, HEM and SOC processes. This will compute the add-on price of silicon as a function of sheet thicknesses, throughput rates and other parameters of the processes.

Other: A Cameca IMS-3f ion microanalysis probe was delivered and installed in JPL. This instrument provides the capabilities of elemental analysis with coherent spatial resolutions of less than 1 µm depth resolutions of 100Å, and detection limits of $10^{13}$ to $10^{16}$ atoms/cm$^2$ (depending on element) and will greatly enhance the capability of the Task in evaluating silicon-sheet material.
## LARGE-AREA SILICON SHEET TASK

### SILICON WEB PROCESS DEVELOPMENT

WESTINGHOUSE ELECTRIC CORP.

<table>
<thead>
<tr>
<th>Technology</th>
<th>Completion Date</th>
<th>Report Date</th>
</tr>
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<tbody>
<tr>
<td>Single crystal ribbon growth</td>
<td>10/30/80</td>
<td>2/4/81</td>
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<table>
<thead>
<tr>
<th>Approach</th>
<th>Status</th>
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<tbody>
<tr>
<td>Silicon dendritic web growth</td>
<td>• 27 Square centimeters per minute growth demonstrated</td>
</tr>
<tr>
<td>Contractor</td>
<td>• One-day manually-controlled melt replenished growth cycle demonstrated</td>
</tr>
<tr>
<td>Westinghouse Electric Corp.</td>
<td>• Solar cell efficiency of 15.5% AM1 demonstrated. Average efficiency = 13.5% AM1</td>
</tr>
<tr>
<td>Research &amp; Development Center</td>
<td>• Semi-automated growth demonstrated - 8 hours</td>
</tr>
<tr>
<td>JPL Contract 954654</td>
<td>• Thickness routinely 100-200 µm</td>
</tr>
<tr>
<td></td>
<td>• Dislocation density routinely &lt; 10^4/cm^2</td>
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</tbody>
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<table>
<thead>
<tr>
<th>Goals</th>
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<tbody>
<tr>
<td>• Area rate of growth</td>
<td>• 25 cm^2/minute</td>
</tr>
<tr>
<td>• Continuous melt replenishment</td>
<td>• Cell efficiency &gt; 15% AM1</td>
</tr>
<tr>
<td>• Cell efficiency &gt; 15% AM1</td>
<td>• Semi-automatic growth cycle</td>
</tr>
<tr>
<td>• Semi-automatic growth cycle</td>
<td>• Thickness routinely 100-200 µm</td>
</tr>
<tr>
<td>• Thickness 100-200 µm</td>
<td>• Dislocation density routinely &lt; 10^4/cm^2</td>
</tr>
<tr>
<td>• Dislocation density &lt; 10^4/cm^2</td>
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LARGE-AREA SILICON SHEET TASK

ADVANCED DENDRITIC WEB GROWTH DEVELOPMENT

WESTINGHOUSE ELECTRIC CORP.

<table>
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<table>
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<th>Approach</th>
<th>Status</th>
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<tbody>
<tr>
<td>Silicon dendritic web growth Contractor</td>
<td>• Advanced throughput development in progress</td>
</tr>
<tr>
<td>Westinghouse Electric Corp. Research &amp; Development Center JPL Contract 955843</td>
<td>• Design of prototype web growth machine in progress on schedule</td>
</tr>
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</table>

<table>
<thead>
<tr>
<th>Goals</th>
<th>Verification of automation concepts in progress</th>
</tr>
</thead>
<tbody>
<tr>
<td>Demonstrate Technology Readiness</td>
<td>Preliminary design review at JPL 11/16/80</td>
</tr>
<tr>
<td>• Automated melt-replenished growth period to 65 hours</td>
<td></td>
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<tr>
<td>• Area rate of growth 25 cm$^2$/min</td>
<td></td>
</tr>
<tr>
<td>• Length of web crystal &gt;10 meters</td>
<td></td>
</tr>
<tr>
<td>• Dislocation density &lt;10$^4$/cm$^2$</td>
<td></td>
</tr>
<tr>
<td>• Resistivity 1 to 3 ohm-cm p-type</td>
<td></td>
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<tr>
<td>• Terrestrial solar cell efficiency &gt;15%</td>
<td></td>
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<tr>
<td>Demonstrate Advanced Throughput</td>
<td></td>
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<tr>
<td>• 30-35 cm$^2$/min area growth rate</td>
<td></td>
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</tbody>
</table>

Chronology of Key Development Goals

<table>
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<tr>
<th>Process Development</th>
<th>Technology Readiness</th>
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<tr>
<td>954654</td>
<td>955843</td>
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<table>
<thead>
<tr>
<th>Area Throughput Rate, cm$^2$/min</th>
<th>Demonstrate 25</th>
<th>Routinely 25</th>
</tr>
</thead>
<tbody>
<tr>
<td>Cell Efficiency, AM1%</td>
<td>Demonstrate 15</td>
<td>Average 15</td>
</tr>
<tr>
<td>Continuous Melt Replenishment</td>
<td>1 Day Cycle</td>
<td>3 Day Cycle</td>
</tr>
<tr>
<td>Growth Mode</td>
<td>Semi-Automatic</td>
<td>Automatic</td>
</tr>
</tbody>
</table>

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1986 Cost Projection per SAMICS/IPEG (1980 $)

**Assumptions:**

Area throughput rate 25 cm$^2$/minute  
Terrestrial Cell efficiency 15%  
Continuously melt-replenished 3 day growth cycle  
Automated growth  
Solar grade polysilicon price $14/kg  
Thickness 150 μm

<table>
<thead>
<tr>
<th>Value-Added Sheet Cost</th>
<th>$0.134</th>
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<tbody>
<tr>
<td>Polysilicon Cost</td>
<td>$0.039</td>
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<tr>
<td>Total Sheet Cost</td>
<td>$0.173</td>
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<tr>
<td>DOE/JPL 1986 Goal</td>
<td>$0.224</td>
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**Overview of Approach**

- Overall objective is to achieve the Low Cost Solar Array Project technology readiness goal for silicon sheet growth
- Program combines the demonstrated key elements of silicon web growth shown by economic analysis to be capable of satisfying the DOE/JPL 1986 cost goal
- Major program tasks to achieve technology readiness are:
  - Design and build prototype web growth machine having features to satisfy 1986 goal
  - Operate prototype machine to demonstrate technology readiness
  - Provide full information for transfer of technology
- Develop advanced web growth techniques and demonstrate higher area throughput rates
**Milestone Chart**

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<tr>
<td></td>
<td>O</td>
<td>N</td>
<td>D</td>
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<tr>
<td>1. Design and Fabricate a Prototype Web Growth Machine</td>
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<tr>
<td>2. Investigate Form of Feedstock Silicon</td>
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<td>3. Operate the Prototype Machine</td>
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<tr>
<td>4. Evaluate Prototype Machine for Technology Readiness</td>
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<tr>
<td>5. Develop Advanced Web Growth Techniques</td>
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<tr>
<td>6. 30 cm²/min throughput</td>
<td>△</td>
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<tr>
<td>7. 35 cm²/min throughput</td>
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<td>8. Update Economic Analysis</td>
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<tr>
<td>9. Evaluate Effect of Process Variations on Quality of Silicon Web</td>
<td>△</td>
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<tr>
<td>10. Provide Web Samples</td>
<td>△</td>
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<tr>
<td>11. 9. Evaluate Energy Utilization of the Prototype Machine</td>
<td>△</td>
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<tr>
<td>10. Provide Technology Transfer Information in Form of:</td>
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</tr>
<tr>
<td>A) Equipment capable of producing silicon equivalent</td>
<td>△</td>
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<tr>
<td>to that demonstrated during program</td>
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<tr>
<td>B) Written procedures applicable to the equipment in (A) above</td>
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<tr>
<td>11. Support Preliminary and Final Design and Performance Reviews</td>
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<tr>
<td>Preliminary</td>
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<tr>
<td>Final</td>
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<td>12. Support Meetings</td>
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<td>13. Provide Documentation</td>
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**LARGE-AREA SILICON SHEET TASK**
Work in Progress

- Design of prototype web growth machine
- Development of advanced web growth techniques for high throughput

Development Plan: Advanced Web Growth Techniques for High Throughput

High Speed Growth  Increase dissipation of latent heat. Maximize coefficients in equation $V = C + D/ \sqrt{t}$
- Modify lid design*
- Modify shield configuration*
- Control melt height (continuous melt replenishment)*
- Manage gas flow

Wide Web Growth  Management of melt profile and thermal stress
- Growth slot/susceptor shield design to control melt profile
- Control of thermal stress (elastic)
  - Develop criterion for critical buckling stress*
  - Identify required thermal profile in web
  - Design lid/shield system to generate required profile

Combine Speed and Width Designs
* Current Activity
LARGE-AREA SILICON SHEET TASK

Design Status: Prototype Web Growth Machine

Mechanical Design

- Functional design completed
- Design refinement for equipment cost reduction in progress

Electronic Design

- Functional design near completion
- Unverified control circuits undergoing evaluation
- Design refinement for equipment cost reduction in progress

Closed-Loop Circuit for Melt-Level Control
CURRENT PROBLEMS

- Long delivery time for electronic components
- Availability of low-cost pellet-form polysilicon

SUMMARY

All Tasks On Schedule Per Contract Requirement

- Prototype design
- Development of techniques for higher throughput

MULTIPLE SILICON RIBBON GROWTH BY EFG

MOBIL TYCO SOLAR ENERGY CORP.

1980 GOALS

1. Demonstrate on a small cell (minimum 4 cm²) that 13% efficiency can be obtained from any ribbon grown in resistance-heated equipment: Achieved.

2. Show ribbon growth at 10 cm width to be possible at 4 cm/minute: Achieved.

3. Demonstrate cell efficiencies of 10% on cells of 50 cm² area prepared from 10 cm wide ribbon grown at -4 cm/minute: Achieved.

4. Technical features demonstration, multiple ribbon growth: Three ribbons, 10 cm wide at 4 cm/minute for eight hours under continuous melt replenishment; mean cell efficiency on a 10% sample = 10.2%: First scheduled for July 1980; not achieved. Rescheduled for December 1980; not achieved.

### Run 16-248

**Cart. #3**  | Seeding trials (seed fracture problems)
---|---
**Cart. #2**  | Growth unstable (ribbon dimensions unacceptable, reseeded)
**Cart. #1**  | Seeding trials (unstable growth)

- **o** = "Freeze" to the die (restart necessary).
- **-** = Stable growth under automatic control from one cartridge.
- **N** = Periods of simultaneous growth of three acceptable 10 cm wide ribbons.
Run 16-250

12/31/80
TIME: 8:00 9:00 10:00 11:00 12:00 1:00 2:00 3:00 4:00 5:00 6:00 7:00 8:00 9:00 10:00 11:00

CART. #1
Seeding trials (seed fracture problems)

Ribbon left frozen while working on cartridges #2 and #3

CART. #2
Seeding trials (unstable growth)

Melting back broken ribbon into the die, reseeding (seed fracture problems)

CART. #3
Seeding trials (fracture problems)

X Trying to repair wiring errors in the automatic width control system

Ribbon growth unstable due to control problems

6 HR 47 MIN

15 MIN

1 HR 15 MIN

40 MIN

• = "Freeze" to the die (restart necessary).

- = Stable Growth under automatic control from one cartridge.

§ = Periods of simultaneous growth of three acceptable 10 cm wide ribbons.
LARGE-AREA SILICON SHEET TASK

1. THE HOT-ZONE TEMPERATURE PROFILE PROBLEMS WHICH PREVIOUSLY PREVENTED SATISFACTORY GROWTH IN CARTRIDGE POSITIONS 2 AND 3 HAVE BEEN SOLVED.

2. THE AUTOMATIC WIDTH CONTROL SYSTEM HAS BEEN SHOWN TO FUNCTION WELL TO SUSTAIN GROWTH FOR LONG PERIODS WITHOUT ATTENTION. CARTRIDGE POSITION 2 OPERATED FOR 54 HOURS IN RUN 249 AND 6 3/4 HOURS IN RUN 250. IN BOTH THESE CASES, STEADY-STATE GROWTH APPEARED LIKELY TO CONTINUE MUCH LONGER, BUT THE RUNS HAD TO BE ENDED AT THE END OF THE WORKDAY.

3. THE AUTOMATIC CONTROL SYSTEM CANNOT RELIABLY COMPENSATE FOR THE LARGE TEMPERATURE EXCURSIONS INDUCED IN THE LEFT SIDE OF CARTRIDGE 1 BY THE LOWERING OF SILICON RODS INTO THE MELT REPLACEMENT UNIT. THIS PROBLEM MAY BE PARTIALLY SOLVED BY OPERATING THE RIBBON-EDGE CONTROL LOOP AT HIGHER GAIN, BUT WILL BE MORE COMPLETELY SOLVED BY THE INCLUSION, IN FUTURE FURNACE HOT ZONE DESIGNS, OF SOMEWHAT GREATER SEPARATION BETWEEN THE MELT REPLACEMENT UNIT AND THE GROWTH CARTRIDGES.

4. THE COOLING PROFILE IN THE CARTRIDGE NEEDS TO BE CHANGED TO REDUCE THE MAGNITUDE OF THERMAL STRESSES IMPOSED ON THE RIBBON. THE CARTRIDGE/PULLER MOUNTING HARDWARE ALSO NEEDS TO BE REDESIGNED TO ENSURE A MORE PRECISE ALIGNMENT BETWEEN THESE TWO UNITS.

5. THE EXISTING MELT REPLACEMENT SYSTEM CANNOT SUPPLY SILICON AT A RATE SUFFICIENT TO SUSTAIN THE GROWTH OF THREE RELATIVELY THICK 11-cm WIDE RIBBONS. A NEW REPLACEMENT UNIT IS BEING DESIGNED WHICH USES SILICON IN THE FORM OF CHUNKS AND WHICH, WHEN BUILT, WILL BE DEVELOPED TO OBTAIN AN ADEQUATE MELTING RATE TO FEED THE FOUR CARTRIDGES OF FUTURE MULTIPLE RIBBON FURNACES.

6. DESIGN MODIFICATIONS NEED TO BE MADE TO THE CARTRIDGE AND HOT ZONE SO THAT GAS FLOWS AND COMPOSITIONS IN THE MULTIPLE FURNACE CAN BE MORE PRECISELY CONTROLLED. IT WILL THEN BE POSSIBLE TO DETERMINE THE CONDITIONS NECESSARY FOR LOW-CARBIDE RIBBON AS IS PRODUCED BY FURNACES 17 AND 18.

7. THE CARTRIDGE POWER SUPPLIES NEED TO BE REVISED TO PROVIDE GREATER IMMUNITY TO FALSE TRIGGERING AND POWER SURGES CAUSED BY POWER-LINE TRANSIENTS. THE USE OF POWER CONTROLLERS WITH PROPERLY APPLIED SCR'S RATHER THAN TRIACS, AND CAREFUL SELECTION OF THE OUTPUT VOLTAGE OF THE STEP-DOWN TRANSFORMERS, APPEAR LIKELY TO SOLVE THIS PROBLEM.

*THIS IS DESIGN WORK UNDERTAKEN FOR OUR INTERNAL MULTIPLE GROWTH PROGRAM."
LARGE-AREA SILICON SHEET TASK

Ambient Studies in Furnace 17

• USE OF HOLLOW DIE SHIELD HAS IMPROVED GAS DISTRIBUTION AT INTERFACE.

• AMBIENT MANIPULATION SHOWN TO HAVE INFLUENCE ON QUALITY OF RIBBON GROWN WITH COLD SHOE SYSTEM.

• SOLAR CELLS OF 10 TO 11% EFFICIENCY PRODUCED AT SPEEDS OF 3.5 TO 4 CM/MINUTE.

• OPTIMIZATION STUDIES IN PROGRESS TO INVESTIGATE AMBIENT/SPEED/COOLING PROFILE/COLD SHOE EFFECTS.
### Machine 17

<table>
<thead>
<tr>
<th>Date</th>
<th>Run No.</th>
<th>Growth</th>
<th>Thickness (cm)</th>
<th>Speed (cm/minute)</th>
<th>Process</th>
<th>Average Resistivity (Ω-cm)</th>
<th>J_sc</th>
<th>V_oc</th>
<th>FF</th>
<th>n</th>
<th>Notes</th>
</tr>
</thead>
<tbody>
<tr>
<td>02/30/80</td>
<td>17-139</td>
<td>CO₂ off CO₂ on</td>
<td>0.019 - 0.033</td>
<td>3.5</td>
<td>PH₃, 1&quot; x 2&quot;, no AR</td>
<td>5</td>
<td>15.5</td>
<td>0.470</td>
<td>0.734</td>
<td>5.35</td>
<td></td>
</tr>
<tr>
<td>12/16/80</td>
<td>17-136</td>
<td>CO₂ off CO₂ on</td>
<td>0.030</td>
<td>3.1</td>
<td>PH₃, 2&quot; x 4&quot;, no AR</td>
<td>5.9</td>
<td>13.8</td>
<td>0.472</td>
<td>0.681</td>
<td>5.03</td>
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<tr>
<td>12/16/80</td>
<td>17-134</td>
<td>CO₂ off CO₂ on</td>
<td>0.027</td>
<td>3.1</td>
<td>PH₃, 2&quot; x 4&quot;, no AR</td>
<td>6.2</td>
<td>14.1</td>
<td>0.459</td>
<td>0.680</td>
<td>4.40</td>
<td>furnace problem</td>
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<tr>
<td>11/05/80</td>
<td>17-131</td>
<td>reduced ambient, SOP</td>
<td>0.029</td>
<td>3.6</td>
<td>PH₃, 2&quot; x 4&quot;, no AR</td>
<td>5</td>
<td>16.7</td>
<td>0.483</td>
<td>0.621</td>
<td>5.0</td>
<td>graphite-like</td>
</tr>
<tr>
<td>10/26/80</td>
<td>17-126</td>
<td>reduced ambient, SOP</td>
<td>0.025</td>
<td>3.4</td>
<td>PH₃, 2&quot; x 4&quot;, no AR</td>
<td>5.2</td>
<td>15.7</td>
<td>0.476</td>
<td>0.708</td>
<td>5.29</td>
<td>graphite-like</td>
</tr>
</tbody>
</table>
LARGE-AREA SILICON SHEET TASK

Evaluation

SOLAR CELL EVALUATION OF MATERIAL GROWN
IN JPL GROWTH MACHINE NO. 1.
ALL CELLS WERE FABRICATED WITH THE PH3, DIFFUSION PROCESS.

FLH LIGHT, 100 mW/cm², 28°C, AR COATED, CELL AREA = 13 cm²

<table>
<thead>
<tr>
<th>Run No.</th>
<th>Growth Conditions</th>
<th>Jsc (mA/cm²)</th>
<th>Voc (V)</th>
<th>FF</th>
<th>n (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>17-139</td>
<td>CO2 &quot;off&quot;</td>
<td>22.6</td>
<td>0.483</td>
<td>0.71</td>
<td>7.8</td>
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<tr>
<td></td>
<td></td>
<td>21.6</td>
<td>0.476</td>
<td>0.73</td>
<td>7.5</td>
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<tr>
<td></td>
<td></td>
<td>22.2</td>
<td>0.478</td>
<td>0.74</td>
<td>7.8</td>
</tr>
<tr>
<td></td>
<td></td>
<td>24.2</td>
<td>0.502</td>
<td>0.72</td>
<td>8.3</td>
</tr>
<tr>
<td>p = 5 Ω·cm</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>3.5 cm/min</td>
<td>CO2 &quot;on&quot;</td>
<td>26.6</td>
<td>0.521</td>
<td>0.75</td>
<td>10.4</td>
</tr>
<tr>
<td></td>
<td></td>
<td>26.0</td>
<td>0.514</td>
<td>0.74</td>
<td>9.9</td>
</tr>
<tr>
<td></td>
<td></td>
<td>28.0</td>
<td>0.528</td>
<td>0.76</td>
<td>11.2</td>
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<tr>
<td></td>
<td></td>
<td>27.7</td>
<td>0.533</td>
<td>0.72</td>
<td>10.6</td>
</tr>
<tr>
<td></td>
<td></td>
<td>27.9</td>
<td>0.527</td>
<td>0.75</td>
<td>11.1</td>
</tr>
</tbody>
</table>
LARGE-AREA SILICON SHEET TASK

Run 17-139

\[ L_n (\mu m) = \begin{cases} 40 & \text{for } CO_2^{ON}\, \text{(a)} \\ 30 & \text{for } CO_2^{OFF}\, \text{(a)} \end{cases} \]

\[ NO (Cm^{-2} Sec^{-1}) = \begin{cases} 10^{15} & \text{for } CO_2^{ON}\, \text{(a)} \\ 10^{16} & \text{for } CO_2^{OFF}\, \text{(a)} \end{cases} \]
LARGE-AREA SILICON SHEET TASK

Cartridge-Furnace Interaction in JPL No. 1

- INCREASED POWER DEMAND OF 10 CM CARTRIDGE HAS NECESSITATED COMPLETE REBUILDING OF FURNACE POWER SUPPLIES:

MAIN ZONE
- INSULATION RECONFIGURED.
- HEATER POSTS REDESIGNED FROM POLYBEDIUM TO GRAPHITE TO IMPROVE HANDLING OF HIGHER CURRENTS.

AFTERHEATER
- POWER DEMAND COUPLED TO MAIN ZONE INSULATION EFFECTIVENESS.
- AVAILABLE TRANSFORMER POWER INADEQUATE FOR HEATING LARGER CROSS SECTION LINEAR COOLING PLATES.

FACE HEATER
- POWER DEMAND COUPLED TO COLD SHOE/AFTERHEATER CONFIGURATION.
- HEAVY DUTY CONTROLLERS INSTALLED.

- GROWTH CONDITIONS CLOSELY RELATED TO BALANCE OF MAIN ZONE, AFTERHEATER, FACE HEATER POWER LEVELS.
**LARGE-AREA SILICON SHEET TASK**

**SILICON ON CERAMIC**

**HONEYWELL CORP.**

<table>
<thead>
<tr>
<th>TECHNOLOGY</th>
<th>REPORT DATE</th>
</tr>
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<tbody>
<tr>
<td>SILICON ON CERAMIC</td>
<td>FEBRUARY 4, 1981</td>
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<table>
<thead>
<tr>
<th>APPROACH</th>
<th>STATUS</th>
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<tbody>
<tr>
<td>SCIM-COATED SOC</td>
<td>• SCIM-COATING 10 cm x 100 cm FULLY SLOTTED</td>
</tr>
<tr>
<td>12 x 100 cm SLOTTED CERAMIC</td>
<td>SUBSTRATES ROUTINELY</td>
</tr>
<tr>
<td></td>
<td>• 15 cm/min DEMONSTRATED (DIPCOATING)</td>
</tr>
<tr>
<td></td>
<td>• 30 cm/min THIN LAYERS SCIM-COATED.</td>
</tr>
<tr>
<td></td>
<td>• 10.54% CELL EFFICIENCY (DIPCOATED)</td>
</tr>
<tr>
<td></td>
<td>• 7.64% ON SCIM-COATED SOC</td>
</tr>
<tr>
<td></td>
<td>• 9.6 ± .5% AVERAGE EFFICIENCY FOR 74 RECENT</td>
</tr>
<tr>
<td></td>
<td>DIP-COATED CELLS.</td>
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</table>

<table>
<thead>
<tr>
<th>CONTRACTOR</th>
<th>12 cm WIDE x 100 cm LONG</th>
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<tbody>
<tr>
<td>HONEYWELL INC.</td>
<td>15 cm/min PULL SPEED</td>
</tr>
<tr>
<td></td>
<td>350 cm²/min THROUGHPUT</td>
</tr>
<tr>
<td></td>
<td>11% CELL EFFICIENCY</td>
</tr>
<tr>
<td></td>
<td>9.8% AVERAGE EFFICIENCY</td>
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</table>

<table>
<thead>
<tr>
<th>GOALS</th>
<th>350 cm²/min THROUGHPUT</th>
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</thead>
<tbody>
<tr>
<td></td>
<td>11% CELL EFFICIENCY</td>
</tr>
<tr>
<td></td>
<td>9.8% AVERAGE EFFICIENCY</td>
</tr>
</tbody>
</table>
Growth Activities and Status

- All SCIM-II runs now use 10 cm x 100 cm substrates fully slotted.
- Manual melt replenishment used with each run.
- Heavy boron doping routinely used if desired.
- Longitudinal temp. profile has been specified.
- Transverse trough temperature gradients significantly improved.
- Effects of changes in crucible, trough, preheater, temperatures investigated.
- Effects of liquid-solid interface position investigated.
- Effects of gas blowing, gas purity investigated.
- SCIM-III design complete, construction begun.
- Material production based on dipcoating.
- SCIM-I not in operation.
LARGE-AREA SILICON SHEET TASK

SCIM Sample 45-3 (1-8-81)

Distance Across Sample in CM

Silicon Thickness (Åm)

Locus of Liquid Solid Interface

RAISED Substrate

NORMAL Substrate

Trough Meniscus

Back Meniscus

Inverted Meniscus

TILTED TROUGH

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Liquid-Solid Interface (LSI) Effects

- LSI CLEARLY VISIBLE BECAUSE OF NON-ZERO CONTACT ANGLE.
- WHEN DENDRITES FORM, LSI ROUGHENS; SOLID POINTS PROJECT INTO LIQUID, AS VIEWED FROM BACK.
- COATING OCCURS OVER A WIDE RANGE OF MENISCUS PressURES, BUT THICKNESS VARIES.
- LSI POSITION ALONG HORIZONTAL AXIS CONTROLLED BY MENISCUS Pressure; SUBSTRATE ANGLE AND HEIGHT HAVE MUCH LESS EFFECT.
- FOR GIVEN THERMAL CONDITIONS, THERE IS A PREFERRED LSI POSITION ALONG HORIZONTAL AXIS. TOO CLOSE PRODUCES THIN LAYERS, TOO FAR PRODUCES DENDRITES.
- BLOWING ARGON ON MENISCUS MOVES LSI AWAY FROM TROUGH, NON-DENDRITIC GROWTH CAN BE OBTAINED WITH HIGHER MENISCUS PressURES.
TYPES OF DENDRITES IN SOC GROWTH

A. LARGE, THICK REGIONS
B. SMALL, ISOLATED REGIONS
C. SINGLE ISOLATED PEAKS
D. THIN, FINE STRUCTURE; LARGE REGIONS
E. FINE STRUCTURE, LONG NARROW REGIONS (SCIM-II ONLY)

KNOWN CAUSES OF DENDRITES

1. MELT TOO COOL
2. SPEED TOO FAST
3. CARBON, SILICON IN SLOTS

POSSIBLE CAUSES OF DENDRITES

1. IMPURITIES IN MELT - CONSTITUTION SUPERCOOLING
2. SURFACE ROUGHNESS OF CERAMIC
3. SiO ON CARBON SURFACE
4. VIBRATION OF MELT
5. THICKNESS TEMPERATURE GRADIENT (PREHEATER LOCATION)
6. MENISCUS GEOMETRY AND PRESSURE
Slotted SOC Cell

No: 485-4-211

Total Area: 5.0 cm²
Metal Coverage: 8.0%

Before AR | After AR
---|---
Voc | 0.568 | 0.573
Jsc | 17.44 | 25.16
FF | 0.754 | 0.731
η | 7.47 | 10.54

Isc = 125.8 mA

Isc = 87.2 mA
LARGE-AREA SILICON SHEET TASK

SCIM-Coated Slotted SOC Cell

No: 38-4-35-111

<table>
<thead>
<tr>
<th>Before AR</th>
<th>After AR</th>
</tr>
</thead>
<tbody>
<tr>
<td>Voc</td>
<td>0.539</td>
</tr>
<tr>
<td>Jsc</td>
<td>14.32 mA</td>
</tr>
<tr>
<td>FF</td>
<td>0.697</td>
</tr>
<tr>
<td>#%</td>
<td>5.38</td>
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</tbody>
</table>

Total Area: 5.0 cm²
Metal Coverage: 8.0%
LARGE-AREA SILICON SHEET TASK

![Graphs showing voltage, fill factor, short-circuit current density, and conversion efficiency for different conditions.](image-url)
LARGE-AREA SILICON SHEET TASK

![Graphs showing fill factor, conversion efficiency, open-circuit voltage, and short-circuit current as a function of diffusion length.]

- Fill Factor
  - X-axis: Diffusion Length (μm)
  - Y-axis: Fill Factor
- Conversion Efficiency
  - X-axis: Diffusion Length (μm)
  - Y-axis: Conversion Efficiency (%)
- Open-Circuit Voltage (V)
  - X-axis: Diffusion Length (μm)
  - Y-axis: Open-Circuit Voltage (V)
- Short-Circuit Current (mA/cm²)
  - X-axis: Diffusion Length (μm)
  - Y-axis: Short-Circuit Current (mA/cm²)
LARGE-AREA SILICON SHEET TASK

Summary of JPL Cell Results

- **BEST DIP-COATED CELL:** 10.54%
- **BEST SCiM-COATED CELL:** 7.64%
- **1980 BASELINE CELLS:**

  \[
  \begin{align*}
  \eta & = 9.6\% \pm 0.5 \\
  \text{Jsc} & = 23.6 \text{ mA/cm}^2 \pm 0.7 \\
  \text{Voc} & = 0.57 \text{ V} \pm 0.01 \\
  \text{FF} & = 0.72 \pm 0.03 \\
  \text{A} & = 5 \text{ cm}^2 \text{ FOR ALL CELLS AM1 WITH AR COATING}
  \end{align*}
  \]

  TOTAL AREA

Major Assumptions

- 2.5 MILLION m² PRODUCTION
- 0.25-cm/sec PULL SPEED.
- TWO 12.5-cm TRACKS PER COATING MACHINE
- $50,800 COST FOR SILICON COATING MACHINE
- 1/12 OPERATOR PER COATING MACHINE: 4.7 SHIFTS
- OPERATOR LABOR $13.150/YEAR WITHOUT FRINGE BENEFITS
- COATING MACHINES STACKED SIX HIGH (24 ft² PROPRATED FLOOR SPACE PER MACHINE)
- $5.78/m² CERAMIC COST
- 85% PLANT EFFICIENCY
- 92% PROCESS YIELD
### Projected Technology Costs by IPEG2 ($/m²)

<table>
<thead>
<tr>
<th>TASK</th>
<th>EQPT</th>
<th>SQFT</th>
<th>DLAB</th>
<th>MATS</th>
<th>UTIL</th>
<th>TOTAL</th>
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</thead>
<tbody>
<tr>
<td>CARBON COATING</td>
<td>0.0078</td>
<td>0.0283</td>
<td>0.0692</td>
<td>0.330&lt;sup&gt;(a)&lt;/sup&gt;</td>
<td>0.00678</td>
<td>7.981</td>
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<td></td>
<td>7.539&lt;sup&gt;(b)&lt;/sup&gt;</td>
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<tr>
<td>SILICON COATING</td>
<td>1.917</td>
<td>0.1731</td>
<td>0.954</td>
<td>0.662&lt;sup&gt;(c)&lt;/sup&gt;</td>
<td>0.12154</td>
<td>3.828&lt;sup&gt;(e)&lt;/sup&gt;</td>
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<td></td>
<td>4.263&lt;sup&gt;(d)&lt;/sup&gt;</td>
<td></td>
<td>8.091&lt;sup&gt;(f)&lt;/sup&gt;</td>
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<tr>
<td>INSPECT</td>
<td>0.104</td>
<td>0.1045</td>
<td>0.966</td>
<td>---</td>
<td>0.00352</td>
<td>1.178</td>
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<tr>
<td>TOTALS</td>
<td>2.029</td>
<td>0.306</td>
<td>1.98</td>
<td>8.531&lt;sup&gt;(e)&lt;/sup&gt;</td>
<td>0.132</td>
<td>12.987&lt;sup&gt;(e)&lt;/sup&gt;</td>
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<td>12.791&lt;sup&gt;(f)&lt;/sup&gt;</td>
<td></td>
<td>17.250&lt;sup&gt;(f)&lt;/sup&gt;</td>
</tr>
</tbody>
</table>

(a) CARBON, (b) SUBSTRATES, (c) ARGON, CRUCIBLES, FURNACES, INSULATION, (d) POLYSILICON, (e) EXCLUDING SILICON, (f) INCLUDING SILICON
IPEG2 Projected Cost Breakdown

**Added Value**: $12.99/㎡

**Including SE**: $17.25/㎡

- **CarBoat**: 0.6%
- **CNSpect**: 4.6%
- **Silcoat**: 29.3%
- **Substrate**: 43.7%
- **Other Materials**: 3.8%

*Processing Costs Excluding Materials*

**Problems and Concerns**

- **Adequate Silicon Thickness at High Speeds Not Demonstrated**
- **Dendritic Growth in SCIM-II**
- **Cell Efficiency of SOC Grown at High Speeds Not Demonstrated**
LARGE-AREA SILICON SHEET TASK

OXYGEN ANALYSIS

UNIVERSITY OF MISSOURI, ROLLA

P.D. Ownby
H.V. Romero

Introduction

At oxygen partial pressure maintained higher than 10^{-19} atm. in the presence of molten silicon is observed to enhance the interaction between the silicon and the container material. Thus it is desirable to know the $P_{O_2}$ over molten silicon in actual production facilities.

$P_{O_2}$ measurements were made in:
- Westinghouse Silicon Web Furnaces
- Honeywell SCM Coater Furnace
- Honeywell Dip Coater Furnace

To determine:
- $P_{O_2}$ of purge gas
- $P_{O_2}$ of furnace atmosphere at operating temperature
LARGE-AREA SILICON SHEET TASK

Conditions for Westinghouse Runs

— THORIA-YTTRIA OXYGEN CELL USED WITH A CO/CO₂ REFERENCE GAS HAVING A P₀₂ OF 10⁻¹⁴ ATM.

— LONG SAMPLE LINE FROM FURNACE TO CELL

— SLOW SAMPLE RATE (14 CC/MIN) DRAWN THROUGH CELL WITH HOUSE VACUUM—GAS FLOW PATH(1)

— THORIA TUBE DESTROYED BY THERMAL SHOCK ON INITIAL HEAT-UP—CELL REBUILT WITH NEW THORIA TUBE

— LESS THAN 1.5 VARIATION IN LOG P₀₂ OVER DURATION OF RUNS EXCEPT WHEN AIR WAS INTRODUCED INTO THE SAMPLE LINE

— HOUSE ARGON P₀₂ = 10⁻¹² ATM.

Gas Flow in Oxygen Cell

![Diagram of Gas Flow in Oxygen Cell]

1. Gas Flow 14 CC/min
2. Gas Flow 640 CC/min Max

Alumina Tube — Thermocouple — Alumina Tube

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LARGE-AREA SILICON SHEET TASK

Gas Supply to Oxygen Cell

House Argon Supply
from RE furnace

Air
from WA furnace

Flow meter

Oxygen Cell

Flow meter

House Vacuum

Log $pO_2$ vs Time for Westinghouse Web Furnace

Log $pO_2$

Time (hours)

0 1 2 3 4 5 6 7

0 -2 -4 -6 -8 -10 -12 -14 -16
LARGE-AREA SILICON SHEET TASK

Response of Oxygen Cell to Introduction of Air
(While Monitoring House Argon)

Conditions for Honeywell Runs

- ZIRCONIA-YTTRIA OXYGEN CELL WITH 1 ATM. OF OXYGEN FOR REFERENCE

- HIGH SAMPLE RATE (200 CC/MIN)--GAS FLOW PATH

- $p_{O_2}$ OF HOUSE ARGON FOR DIP FURNACE WAS $10^{-4.8}$ ATM.

- $p_{O_2}$ OF HOUSE ARGON FOR SCIM FURNACE WAS $10^{-5.0}$ ATM.

- $p_{O_2}$ OF SCIM FURNACE ATMOSPHERE VARIED BETWEEN $10^{-16.0}$ AND $10^{-14.3}$ ATM DURING COATING

- $p_{O_2}$ OF DIP FURNACE ATMOSPHERE VARIED BETWEEN $10^{-14.8}$ AND $10^{-13.0}$ ATM DURING COATING

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LARGE-AREA SILICON SHEET TASK

Summary of Results

BASELINE OXYGEN PARTIAL PRESSURE AS MEASURED AT 1000°C WITH SOLID ELECTROLYTE CELL

1. FROM WESTINGHOUSE WEB FURNACE:
   \[ P_{O_2} = 10^{-12.5} \text{ ATM} \]

2. FROM HONEYWELL SOC FURNACES:
   A) SCIM COATER:
   \[ P_{O_2} = 10^{-16.0} \text{ ATM} \]
   B) DIP COATER:
   \[ P_{O_2} = 10^{-15.5} \text{ ATM} \]

3. FROM MOBIL-TYCO EFG FURNACE:
   \[ P_{O_2} = 10^{-12.1} \text{ ATM} \]
LARGE-AREA SILICON SHEET TASK

ADVANCED CZOCHRALSKI INGOT GROWTH

KAYEX CORP.

Design Program Requirements

<table>
<thead>
<tr>
<th>TECHNOLOGY - INGOT GROWTH</th>
<th>REPORT DATE: DECEMBER 31, 1980</th>
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<tbody>
<tr>
<td>APPROACH.</td>
<td>START DATE: JULY 1, 1980</td>
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<tr>
<td>DESIGN OF A MODIFIED CG 2000 RC CRYSTAL GROWER FOR ADVANCED CZOCHRALSki GROWTH FOR TECHNICAL READINESS.</td>
<td></td>
</tr>
<tr>
<td>GOALS.</td>
<td>MODIFICATIONS.</td>
</tr>
<tr>
<td>EQUIPMENT TO BE CAPABLE OF PULLING FIVE CRYSTALS, EACH OF 30 KG WEIGHT, 150 MMS DIAMETER FROM A SINGLE 16&quot; DIAMETER CRUCIBLE.</td>
<td>A. OVERALL EQUIPMENT DESIGN.</td>
</tr>
<tr>
<td></td>
<td>B. PROCESS AUTOMATION WITH M.P.U.</td>
</tr>
<tr>
<td></td>
<td>C. SENSOR DEVELOPMENT: MELT LEVEL, MELT TEMPERATURE; CRYSTAL DIAMETER.</td>
</tr>
<tr>
<td></td>
<td>D. RADIATION SHIELD TO ACCELERATE GROWTH.</td>
</tr>
<tr>
<td></td>
<td>E. RECHARGE MELTING RATE OF 25 KG/HR USING SILICON CHUNKS OF GRANULAR SILICON UTILIZING A RECHARGE HOPPER.</td>
</tr>
<tr>
<td></td>
<td>F. MODIFIED GROWTH CHAMBER SUITABLE FOR USE AS A PRODUCTION FACILITY.</td>
</tr>
<tr>
<td></td>
<td>G. THROUGHPUT CAPABILITY OF 2.5 KG/HR.</td>
</tr>
</tbody>
</table>
**Equipment Design CG 6000 RC**

<table>
<thead>
<tr>
<th>GOALS</th>
<th>IMPLEMENTATION</th>
</tr>
</thead>
<tbody>
<tr>
<td>1. OVERALL EQUIPMENT DESIGN.</td>
<td>A). 2000 RC AS BASIC CONCEPT</td>
</tr>
<tr>
<td></td>
<td>B). INCREASED CHAMBER SIZE.</td>
</tr>
<tr>
<td></td>
<td>C). IMPROVED RELIABILITY: - SEALS, WELDS, VIEWPORTS, ARGON SUPPLY, GRAPHITE.</td>
</tr>
<tr>
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<td>D). INCREASED CAPACITY: - 15&quot; x 12&quot; AND 16&quot; x 12&quot; HOT ZONES, SEED MOTION MECHANISM.</td>
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# Equipment and Process Goals

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<td>1. CONTINUOUS GROWTH OF 150 KG OR MORE OF MULTIPLE INGOTS FROM ONE CRUCIBLE USING MELT REPLENISHMENT.</td>
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<td>7. PROTOTYPE EQUIPMENT SUITABLE FOR HIGH VOLUME SILICON PRODUCTION TRANSFERABLE DIRECTLY TO INDUSTRY.</td>
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# Overall Program

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**PROGRAM.**

1. **EQUIPMENT CONSTRUCTION AND TEST.**
   
2. **PROCESS DEVELOPMENT.**
   
3. **AUTOMATION AND CONTROLS.**
   
4. **ANALYTICAL STUDY.**
   
5. **DOCUMENTATION**

**PROGRAM GOAL.**

1. **CONSTRUCT/DEBUG/TEST CG 6000 RC CRYSTAL PULLER.**
   
2. **A. ACCELERATED RECHARGE.**
   
3. **B. ACCELERATED GROWTH.**
   
4. **C. YIELD AND COST IMPROVEMENT.**
   
5. **MPU INCORPORATING MELT LEVEL, MELT TEMPERATURE, DIAMETER CONTROL SENSORS.**
   
6. **A. PURITY ANALYSIS.**
   
7. **B. SOLAR CELL FABRICATION.**
   
8. **C. TECHNICAL REPORTS.**
   
9. **D. ECONOMIC ANALYSIS.**
   
10. **C. PRODUCTION/PROCESS EQUIPMENT SPEC. FOR TECHNOLOGY READINESS.**
   
11. **D. FINAL REPORT.**

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175
### Large-Area Silicon Sheet Task

#### Project Plan

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**LARGE-AREA SILICON SHEET TASK**

*Original page is of poor quality*
### Project Title:
Advanced Czochralski Growth for Technology Readiness

### Program Plan Revision No. 1

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LARGE-AREA SILICON SHEET TASK

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Overall View of Kayex CG 6000 RC Crystal Puller (JPL's LASS Task ESGU)
LARGE-AREA SILICON SHEET TASK

Cz Growth Parameters, Low-Cost Cz
(Poly Lump Feed)

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<td>60</td>
<td>60</td>
</tr>
</tbody>
</table>

Process Time Cycle

<table>
<thead>
<tr>
<th>OPERATION</th>
<th>LOW COST CZ</th>
<th>LOW COST CZ</th>
</tr>
</thead>
<tbody>
<tr>
<td>1. PREPARATION</td>
<td>150 MINS</td>
<td>165 MINS</td>
</tr>
<tr>
<td>LOAD POLY</td>
<td>20</td>
<td>25</td>
</tr>
<tr>
<td>CLOSE FURNACE</td>
<td>5</td>
<td>5</td>
</tr>
<tr>
<td>PUMP DOWN</td>
<td>20</td>
<td>10</td>
</tr>
<tr>
<td>MELT</td>
<td>105</td>
<td>125</td>
</tr>
<tr>
<td>2. GROWTH CYCLE (INITIAL)</td>
<td>508 MINS</td>
<td>962 MINS</td>
</tr>
<tr>
<td>LOWER SEED *</td>
<td>15°</td>
<td>15°</td>
</tr>
<tr>
<td>STABILIZE TEMP.</td>
<td>30</td>
<td>30</td>
</tr>
<tr>
<td>SEED GROWTH</td>
<td>20</td>
<td>20</td>
</tr>
<tr>
<td>CROWN GROWTH</td>
<td>55</td>
<td>55</td>
</tr>
<tr>
<td>STRAIGHT GROWTH</td>
<td>343</td>
<td>797</td>
</tr>
<tr>
<td>TAPER END</td>
<td>60</td>
<td>60</td>
</tr>
<tr>
<td>3. RECHARGE/GROWTH CYCLE</td>
<td>2792 MINS</td>
<td>2324 MINS</td>
</tr>
<tr>
<td>COOL CRYSTAL</td>
<td>30 (4 CYCLES)</td>
<td>30 (2 CYCLES)</td>
</tr>
<tr>
<td>REMOVE CRYSTAL</td>
<td>10</td>
<td>10</td>
</tr>
<tr>
<td>LOAD HOPPER &amp; VAC DOWN (2)</td>
<td>60</td>
<td>60</td>
</tr>
<tr>
<td>LOWER HOPPER (2)</td>
<td>10</td>
<td>10</td>
</tr>
<tr>
<td>MELT POLY LUMP</td>
<td>80</td>
<td>90</td>
</tr>
<tr>
<td>LOWER SEED *</td>
<td>15°</td>
<td>15°</td>
</tr>
<tr>
<td>STABILIZE TEMP.</td>
<td>30</td>
<td>30</td>
</tr>
<tr>
<td>SEED GROWTH</td>
<td>20</td>
<td>20</td>
</tr>
<tr>
<td>CROWN GROWTH</td>
<td>55</td>
<td>55</td>
</tr>
<tr>
<td>STRAIGHT GROWTH</td>
<td>343</td>
<td>797</td>
</tr>
<tr>
<td>TAPER END</td>
<td>60</td>
<td>60</td>
</tr>
</tbody>
</table>

* COMPLETED DURING STABILIZATION OF MELT TEMPERATURE.
LARGE-AREA SILICON SHEET TASK

<table>
<thead>
<tr>
<th>OPERATION</th>
<th>LOW COST CZ</th>
<th>LOW COST CZ</th>
</tr>
</thead>
<tbody>
<tr>
<td>SHUT DOWN CYCLE</td>
<td>140 MINS</td>
<td>140 MINS</td>
</tr>
<tr>
<td>COOL FURNACE</td>
<td>80</td>
<td>80</td>
</tr>
<tr>
<td>REMOVE CRYSTAL **</td>
<td>10**</td>
<td>10**</td>
</tr>
<tr>
<td>CLEAN, SET UP</td>
<td>60</td>
<td>60</td>
</tr>
</tbody>
</table>

** COMPLETED DURING FURNACE COOLING TIME

TOTAL TIME = 60 HRS

GROWTH RATE CALCULATION:

AVERAGE STRAIGHT GROWTH FOR 27 KG

343 MINS = 4.72 KG/HR
AT 1050 GMS/INCH: = 4.49"/HR GROWTH RATE

AVERAGE STRAIGHT GROWTH FOR 47 KG

797 MINS = 3.54 KG/HR
= 3.37"/HR GROWTH RATE

SAMICS-IPEG Input Data and Cost Calculation

<table>
<thead>
<tr>
<th>CONDITIONS (PER CYCLE)</th>
<th></th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>TOTAL Si MELTED (KG)</td>
<td>160</td>
<td>160</td>
</tr>
<tr>
<td>CRYSTAL WT (KG)</td>
<td>30</td>
<td>50</td>
</tr>
<tr>
<td>NO CRYSTALS/CRUCIBLE</td>
<td>5</td>
<td>3</td>
</tr>
<tr>
<td>DIAMETER OF CRYSTAL (CMS)</td>
<td>15</td>
<td>15</td>
</tr>
<tr>
<td>AVG. STR. GROWTH RATE (CMS/HR)</td>
<td>11.4</td>
<td>8.56</td>
</tr>
<tr>
<td>CYCLE TIME (HRS)</td>
<td>60</td>
<td>60</td>
</tr>
<tr>
<td>CRUCIBLE SIZE (INS)</td>
<td>16 x 12</td>
<td>16 x 12</td>
</tr>
</tbody>
</table>

INPUT DATA ($1980)

| CAPITAL EQUIP COST (EQPT)      | $266900    | 266900     |
| MANUFACTURING FLOOR SPACE (SQFT) | 100        | 100        |
| ANNUAL DIRECT SALARIES         |            |            |
| PROD. OPERATOR (0.65 PERSONS/YR)$ | 8554      | 8554       |
| ELECT. TECHNICIAN (0.3 PERSONS/YR)$ | 5082      | 5082       |
| INSPECTOR (0.1 PERSONS/YR)     | $1155      | 1155       |
| TOTAL D/LAB                    | $14791     | 14791      |
# LARGE-AREA SILICON SHEET TASK

## DIRECT USED MATERIALS & SUPPLIES

<table>
<thead>
<tr>
<th>Description</th>
<th>Cost (Low Cost CZ)</th>
<th>Cost (Low Cost CZ)</th>
</tr>
</thead>
<tbody>
<tr>
<td>85% USAGE PER YEAR</td>
<td></td>
<td></td>
</tr>
<tr>
<td>CYCLES/YR HRS/CYCLE</td>
<td>138/60</td>
<td>138/60</td>
</tr>
<tr>
<td>POLY KG/YR CHARGED</td>
<td>22080</td>
<td>22080</td>
</tr>
<tr>
<td>SEED ($20 EA)</td>
<td>1380</td>
<td>1380</td>
</tr>
<tr>
<td>DOPANT (NOT COSTED)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>ARGON (150 FT³/CYCLE HR a $0.02/FT³)</td>
<td>24840</td>
<td>24940</td>
</tr>
<tr>
<td>CRUCIBLES (16&quot; x 12&quot; = $375 EA.)</td>
<td>51750</td>
<td>51750</td>
</tr>
<tr>
<td>MISCELLANEOUS (4 SETS OF 16&quot; GRAPHITE/YR AT $8889 PER SET)</td>
<td>35556</td>
<td>35556</td>
</tr>
<tr>
<td>MATERIALS TOTAL (MATS)</td>
<td>$113526</td>
<td>$113526</td>
</tr>
</tbody>
</table>

## UTILITIES (PROCESS)

<table>
<thead>
<tr>
<th>Description</th>
<th>Cost (Low Cost CZ)</th>
<th>Cost (Low Cost CZ)</th>
</tr>
</thead>
<tbody>
<tr>
<td>ELECTRICITY</td>
<td></td>
<td></td>
</tr>
<tr>
<td>(90 KW a $0.035/KW) (CYCLE TIME - 3 HRS) (# OF CYCLES)</td>
<td>$24778</td>
<td>$24778</td>
</tr>
<tr>
<td>COOLING WATER</td>
<td></td>
<td></td>
</tr>
<tr>
<td>(90 KW a $0.0074/KW) (CYCLE TIME - 2 HRS) (# OF CYCLES)</td>
<td>$5331</td>
<td>$5331</td>
</tr>
<tr>
<td>UTILITIES TOTAL (UTIL)</td>
<td>$30109</td>
<td>$30109</td>
</tr>
</tbody>
</table>

## IPEG PRICE

<table>
<thead>
<tr>
<th>Description</th>
<th>Cost (Low Cost CZ)</th>
<th>Cost (Low Cost CZ)</th>
</tr>
</thead>
<tbody>
<tr>
<td>C1 EQPT = $0.57/YR = $ EQPT</td>
<td>152133</td>
<td>152133</td>
</tr>
<tr>
<td>C2 SOFT = $1.09/YR = $ SOFT</td>
<td>10900</td>
<td>10900</td>
</tr>
<tr>
<td>C3 DLAB = $2.1/YR = $ DLAB</td>
<td>31061</td>
<td>31061</td>
</tr>
<tr>
<td>C4 MATS = $1.2/YR = $ MATS</td>
<td>136231</td>
<td>136231</td>
</tr>
<tr>
<td>C5 UTIL = $1.2/YR = $ UTIL</td>
<td>36131</td>
<td>36131</td>
</tr>
<tr>
<td>ANNUAL COST</td>
<td>$366456</td>
<td>$366456</td>
</tr>
</tbody>
</table>

## QUAN. (TOTAL CHARGE x % YIELD) (KG)=

<table>
<thead>
<tr>
<th>Description</th>
<th>Cost (Low Cost CZ)</th>
<th>Cost (Low Cost CZ)</th>
</tr>
</thead>
<tbody>
<tr>
<td>THROUGHPUT</td>
<td>18216 KG</td>
<td>19044</td>
</tr>
<tr>
<td>ADD ON COST ($KG OR $M²) (ASSUME 1 KG = 1M²)</td>
<td>$20.12</td>
<td>$19.24</td>
</tr>
<tr>
<td>PEXC WATT CALCULATION =</td>
<td>14.19$/PEAK WATT</td>
<td>13.57$/PEAK WATT</td>
</tr>
</tbody>
</table>

\[
\text{PEAK WATT CALCULATION} = \frac{10000\text{W/M}^2 \times \text{CELL EFF.} \times \text{CELL YIELD} \times \text{MANUF. YIELD}}{(15\%) \times (35\%) \times (99.5\%)}
\]
LARGE-AREA SILICON SHEET TASK

<table>
<thead>
<tr>
<th>CONDITIONS</th>
<th>3 x 50 KG CRYSTAL GROWTH</th>
</tr>
</thead>
<tbody>
<tr>
<td>CRUCIBLE SIZE (INS)</td>
<td>16&quot; x 12&quot;</td>
</tr>
<tr>
<td>CRYSTAL DIAMETER (CMS)</td>
<td>15</td>
</tr>
<tr>
<td>GROWTH RATE (CMS/HR)</td>
<td>11.40</td>
</tr>
<tr>
<td>TOTAL POLY MELTED (KG)</td>
<td>160</td>
</tr>
<tr>
<td>TOTAL CRYSTAL PULLED (KG)</td>
<td>150</td>
</tr>
<tr>
<td>PULLED YIELD (%)</td>
<td>93.75</td>
</tr>
<tr>
<td>YIELD AFTER CG (%)</td>
<td>86.25</td>
</tr>
<tr>
<td>NO OF CRYSTALS/CRUCIBLE</td>
<td>3</td>
</tr>
<tr>
<td>CYCLE TIME (HRS)</td>
<td>49.85</td>
</tr>
</tbody>
</table>

Process Time Cycle

<table>
<thead>
<tr>
<th>OPERATION</th>
<th>MINS</th>
</tr>
</thead>
<tbody>
<tr>
<td>1. PREPARATION</td>
<td>165 MINS</td>
</tr>
<tr>
<td>LOAD POLY</td>
<td>25</td>
</tr>
<tr>
<td>CLOSE FURNACE</td>
<td>5</td>
</tr>
<tr>
<td>PUMP DOWN</td>
<td>10</td>
</tr>
<tr>
<td>MELT</td>
<td>125</td>
</tr>
<tr>
<td>2. GROWTH CYCLE (INITIAL)</td>
<td>762 MINS</td>
</tr>
<tr>
<td>LOWER SEED *</td>
<td>15*</td>
</tr>
<tr>
<td>STABILIZE TEMPERATURE</td>
<td>30</td>
</tr>
<tr>
<td>SEED GROWTH</td>
<td>20</td>
</tr>
<tr>
<td>CROWN GROWTH</td>
<td>55</td>
</tr>
<tr>
<td>STRAIGHT GROWTH</td>
<td>597 (SEE CALCULATION)</td>
</tr>
<tr>
<td>TAPER END</td>
<td>60</td>
</tr>
<tr>
<td>3. RECHARGE/GROWTH CYCLE</td>
<td>1924 MINS (2 CYCLES)</td>
</tr>
<tr>
<td>COOL CRYSTAL</td>
<td>30</td>
</tr>
<tr>
<td>REMOVE CRYSTAL</td>
<td>10</td>
</tr>
<tr>
<td>LOAD HOPPER &amp; VAC DOWN (2)</td>
<td>60</td>
</tr>
<tr>
<td>LOWER HOPPER (2)</td>
<td>10</td>
</tr>
<tr>
<td>MELT POLY LUMP</td>
<td>90</td>
</tr>
<tr>
<td>LOWER SEED *</td>
<td>15*</td>
</tr>
<tr>
<td>STABILIZE TEM.</td>
<td>30</td>
</tr>
<tr>
<td>SEED GROWTH</td>
<td>20</td>
</tr>
<tr>
<td>CROWN GROWTH</td>
<td>55</td>
</tr>
<tr>
<td>STRAIGHT GROWTH</td>
<td>597</td>
</tr>
<tr>
<td>TAPER END</td>
<td>60</td>
</tr>
</tbody>
</table>

* COMPLETED DURING STABILIZATION OF MELT TEMPERATURE
LARGE-AREA SILICON SHEET TASK

OPERATION

4. SHUT DOWN CYCLE 140 MINS
   COOL FURNACE 80
   REMOVE CRYSTAL ** 10**
   CLEAN, SET UP 60
   TOTAL TIME (HRS) 49.85

** COMPLETED DURING FURNACE COOLING TIME

AVERAGE STRAIGHT GROWTH FOR 47 KG

597 MINS = 4.72 KG/HR
AT 1050 GMS/INCH = 4.49*/HR AV. GROWTH RATE REQUIRED

SAMICS-IPEG Input Data and Cost Calculation
For 3 x 50-kg Crystal Growth

CONDITIONS (PER CYCLE)
TOTAL SI MELTED (KG) 160
CRYSTAL WEIGHT (KG) 50
NO CRYSTALS/Crucible 3
DIAMETER OF CRYSTAL (CMS) 15
GROWTH RATE (CMS/HR) 11.40
CYCLE TIME (HRS) 49.85
CRUCIBLE SIZE (INS) 16" x 12"

INPUT DATA ($1980)
CAPITAL EQUIP COST (EQPT) $266900
MANUFACTURING FLOOR SPACE (SOFT) 100
ANNUAL DIRECT SALARIES
   PROD. OPERATOR (0.65 PERSONS/YR) $8554
   ELECT. TECH. (0.3 PERSONS/YR) $5082
   INSPECTOR (0.1 PERSONS/YR) $1155

TOTAL D/LAB $14791
## LARGE-AREA SILICON SHEET TASK

### DIRECT USED MATERIALS & SUPPLIES

85% USAGE PER YEAR

<table>
<thead>
<tr>
<th>CYCLES/yr</th>
<th>HRS/CYCLE</th>
<th>166/49.85</th>
</tr>
</thead>
<tbody>
<tr>
<td>POLY Kg/yr CHARGED</td>
<td>26560</td>
<td></td>
</tr>
<tr>
<td>SEED ($20 EA)</td>
<td>$1660</td>
<td></td>
</tr>
<tr>
<td>DOPANT (NOT COSTED)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>ARGON 150 FT³/CYCLE HR @ $0.02/FT³</td>
<td>$24825</td>
<td></td>
</tr>
<tr>
<td>CRUCIBLES (16&quot; x 12&quot; – $375 EA.)</td>
<td>$62250</td>
<td></td>
</tr>
<tr>
<td>MISCELLANEOUS (4 SETS OF 16&quot; GRAPHITE/yr @ $8889 PER SET)</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

MATERIALS TOTAL (MATS) $124291

### UTILITIES (PROCESS)

| ELECTRICITY | (90 KW @ $0.035/KW)(CYCLE TIME 3 HRS)(# OF CYCLES) | 24498 |
| COOLING WATER | (90 KW @ 0.0074/KW)(CYCLE TIME 2 HRS)(# OF CYCLES) | 5290 |

UTILITIES TOTAL (UTIL) 29788

### LOW COST CZ

IPEG PRICE

| C1 EQPT = $0.57/YR = $EQPT | 152133 |
| C2 SOFT = $1.09/YR = $SOFT | 10900 |
| C3 DLAB = $2.1/YR = $DLAB | 31061 |
| C4 MATS = $1.2/YR = $MATS | 149149 |
| C5 UTIL = $1.2/YR = $UTIL | 35746 |

ANNUAL COST $378989

QUAN. (TOTAL CHARGE x % YIELDING)(KG) 22908 KG

THROUGHPUT = 2.77 KG/HR

ADD ON COST ($KG OR $M²) = $16.54

(ASSUME 1 KG - 1M²) = 11.66¢/PEAK WATT
Recent efforts centered on identification and control of process variables to achieve optimum monocrystalline yields.

Automatic diameter control of ingots of 125 dia can now hold diameter variations to 380 µm. Ingots of 75 kg (150 µm dia.) have been grown. Better control of thermal convection currents in melt resulted in significant increases in monocrystalline yield.

The melt transfer system was simplified, with improved insulation and better temperature control of the replenishing melt stream.

Preliminary material analysis shows greater consistency in impurity levels (i.e. carbon, oxygen and others) in ingot material grown from the CLF furnace.

An overall design for a production prototype CLF-Cz furnace has been begun, incorporating Siltec’s new microprocessor-controlled AG660-Cz growth furnace.

Schematic of Silicon "Rock" Feeder for the Continuous Liquid-Feed Furnace

Constructed Hopper Chamber for Si Particles (50 kg Capacity)
Bench Test of Silicon Particle Feeder

150-mm-dia Si Ingot

Effect of Crystal Size on CLF-Cz Add-On Cost

Artist's Conception of CLF Cz ESGU

Original page is of poor quality
LARGE-AREA SILICON SHEET TASK

Siltec's AG660 Cz Furnace

Control Panel for Microprocessor-Controlled AG660
LARGE-AREA SILICON SHEET TASK

SEMICRYSTALLINE CASTING PROCESS
SEMIX INC.

Basic Terms of Cooperative Agreement

• ESTABLISHED AGREEMENT FORMAT - INTEGRATED INTO JPL/LSA PROJECT

• 3 YEAR PROGRAM

• FINANCIAL COST SHARING AGREEMENT - 77.6% D.O.E. - $7.7M
  22.2% SEMIX - $2.2M
  PAYBACK - 1% OF NET SALES AFTER PROGRAM SUCCESSFULLY COMPLETED

• PATENT AND TECHNICAL DATA RIGHTS
  GOVERNMENT WAIVES PATENT RIGHTS
  RESTRICTION OF PROPRIETARY INFORMATION

Agreement Objectives

• DEVELOP AND DEMONSTRATE THE KEY ELEMENTS OF SI SHEET TECHNOLOGY NEEDED BY SEMIX TO ACHIEVE COMMERCIAL READINESS TO MEET 1982 PRICE GOALS AT 10MW/YEAR OUTPUT
  $1.66/WP* (SHEET) • $56/KG SILICON COSTS FOR $2.80/WP (MODULE)

• DEVELOP AND DEMONSTRATE TECHNOLOGY READINESS TO MEET 1986 PRICE GOALS
  $0.37/WP* (SHEET) • $14/KG SILICON COSTS FOR $0.70/WP (MODULE)

• SEMIX INTENDS TO FULLY COMMERCIALIZE TECHNOLOGY WITH PRIVATE FUNDS, TO MEET OR EXCEED PHOTOVOLTAIC PROGRAM GOALS

• SEMIX INTENDS TO SELL SHEET TO PHOTOVOLTAIC INDUSTRY AT PRICE GOALS IF PROJECT IS SUCCESSFUL (PROJECTED BY FY 83)

* ALLATION BASED UPON JPL PRICE GUIDELINES
LARGE-AREA SILICON SHEET TASK

Program Status

PHASE I — JUNE 1980 — JUNE 1981

% COMPLETE

TASK 1 — ECONOMIC AND TECHNICAL PERFORMANCE ANALYSIS OF CURRENT SEMICRYSTALLINE PROCESS 80%

TASK 2 — DEMONSTRATE PROOF OF CONCEPT 25%

TASK 3 — PRELIMINARY DESIGN, ANALYSIS AND Prototype EVALUATION 60%

TASK 4 — CRITICAL SUBSYSTEM DESIGN, ASSEMBLY AND TEST 50%

"X3K 5 — PRELIMINARY TECHNICAL AND ECONOMIC EVALUATION FOR 1985 GOALS 90%

• 2 REVIEW MEETINGS — DOE/JPL/SEMIX

• DELIVERABLES ON SCHEDULE — SEVERAL CELLS DELIVERED AHEAD OF SCHEDULE FOR EARLY VERIFICATION

Summary of Ubiquitous Crystallization Process (UCP) SAMICS Analyses
(1980 $/Wp)

<table>
<thead>
<tr>
<th>PROCESS</th>
<th>CASE 1 1982 TECHNOLOGY SILICON PRICE $5/14/KILOGRAM</th>
<th>CASE 2 1982 TECHNOLOGY SILICON PRICE $14/KILOGRAM</th>
<th>CASE 3 1986 TECHNOLOGY SILICON PRICE $14/KILOGRAM</th>
</tr>
</thead>
<tbody>
<tr>
<td>CASTING</td>
<td>0.41</td>
<td>0.20</td>
<td>0.065</td>
</tr>
<tr>
<td>SIZING</td>
<td>0.04</td>
<td>0.032</td>
<td>0.003</td>
</tr>
<tr>
<td>WAFFERING</td>
<td>0.39</td>
<td>0.31</td>
<td>0.127</td>
</tr>
<tr>
<td>CLEANING</td>
<td>0.006</td>
<td>0.005</td>
<td>N/A</td>
</tr>
<tr>
<td>QUALITY CONTROL</td>
<td>0.014</td>
<td>0.011</td>
<td>0.001</td>
</tr>
<tr>
<td>TOTAL VALUE ADDED FOR PROCESSES</td>
<td>0.86</td>
<td>0.558</td>
<td>0.196</td>
</tr>
<tr>
<td>JPL PRICE ALLOCATION</td>
<td>1.00</td>
<td>N/A</td>
<td>0.26</td>
</tr>
<tr>
<td>FEEDSTOCK SILICON COST</td>
<td>0.789</td>
<td>0.158</td>
<td>0.130</td>
</tr>
<tr>
<td>TOTAL SHEET COST</td>
<td>1.649</td>
<td>0.716</td>
<td>0.326</td>
</tr>
<tr>
<td>CELL EFFICIENCY</td>
<td>12%</td>
<td>15%</td>
<td>15%</td>
</tr>
</tbody>
</table>
LARGE-AREA SILICON SHEET TASK

UCP SAMICS Analyses
(Not Including Cost of Si Feedstock)
(1980 $/Wp)

CASE 1
Q.C. 1.6% CLEANING 0.7%
WAFERING 45.3%
CASTING 47.7%
SIZING 4.7%
TOTAL VALUE ADDED ADDED = $0.86

CASE 2
Q.C. 2.0% CLEANING 0.8%
WAFERING 54.9%
CASTING 36.6%
SIZING 5.7%
TOTAL VALUE ADDED ADDED = $0.558

CASE 3
Q.C. 0.5% CASTING 33.3%
WAFERING 64.8%
SIZING 1.4%
TOTAL VALUE ADDED ADDED = $0.196

UCP Semicrystalline Cell Measurements

• 11% AM1 AVERAGE 10 X 10 CM CELL EFFICIENCY —
  MEASURED BY SEMIX

• >12% AM1 AVERAGE 2 X 2 CM CELL EFFICIENCY —
  MEASURED BY SEMIX
**IPEG Analysis Assumptions for HEM Casting**

<table>
<thead>
<tr>
<th>Equipment cost per unit, $</th>
<th>35,000</th>
</tr>
</thead>
<tbody>
<tr>
<td>Floor space per unit, sq.ft.</td>
<td>60</td>
</tr>
<tr>
<td>Labor, units/operator</td>
<td>10</td>
</tr>
<tr>
<td>Cycle time, hrs.</td>
<td>48</td>
</tr>
<tr>
<td>Expendables/run, $</td>
<td>135</td>
</tr>
<tr>
<td>Conversion ratio, m²/kg</td>
<td>1</td>
</tr>
</tbody>
</table>

Ingots are cast by HEM and sectioned into nine bars of 10 cm x 10 cm x 30 cm size.

<table>
<thead>
<tr>
<th>Value added price</th>
<th>$8.65/m²</th>
</tr>
</thead>
<tbody>
<tr>
<td>Goal</td>
<td>$18.15/m²</td>
</tr>
</tbody>
</table>
LARGE-AREA SILICON SHEET TASK

![Graph showing the relationship between equipment cost and value added price per square meter. The goal line is set at 18 units on the value added price axis. The equipment cost is measured in thousands of dollars, ranging from 0 to 80, while the value added price ranges from 0 to 18 units. The graph shows a linear increase in value added price with increasing equipment cost.](image-url)
LARGE-AREA SILICON SHEET TASK

![Graph showing relationship between expendables per run and value added price per m^2.](image)
LARGE-AREA SILICON SHEET TASK

GOAL

VALUE ADDED PRICE, $/m^2

CYCLE TIME, HRS.
GOAL

VALUE ADDED PRICE, $/m^2

FINISHED INGOT SIZE, kg
LARGE-AREA SILICON SHEET TASK

Revised IPEG Analysis Assumptions
For HEM Casting

<p>| | |</p>
<table>
<thead>
<tr>
<th></th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>EQUIPMENT COST PER UNIT, $</td>
<td>35,000</td>
</tr>
<tr>
<td>FLOOR SPACE PER UNIT, SQ.FT.</td>
<td>60</td>
</tr>
<tr>
<td>LABOR, UNITS/OPERATOR</td>
<td>10</td>
</tr>
<tr>
<td>CYCLE TIME, HRS.</td>
<td>48</td>
</tr>
<tr>
<td>EXPENDABLES/RUN, $</td>
<td>135</td>
</tr>
<tr>
<td>CONVERSION RATIO, M²/KG</td>
<td>1</td>
</tr>
</tbody>
</table>

INGOTS ARE CAST BY HEM AND SECTIONED INTO
NINE BARS OF 10 CM X 10 CM X 15 CM SIZE.

<table>
<thead>
<tr>
<th>Value Added Price</th>
<th>$15.59/M²</th>
</tr>
</thead>
<tbody>
<tr>
<td>Goal</td>
<td>$18.15/M²</td>
</tr>
</tbody>
</table>
### Heat Exchanger and Furnace Temperatures

<table>
<thead>
<tr>
<th>RUN</th>
<th>PURPOSE</th>
<th>SEEDING</th>
<th>GROWTH CYCLE</th>
<th>REMARKS</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>FURN. TEMP.</td>
<td>DECREASE OF</td>
<td>GROWTH TIME IN HRS.</td>
</tr>
<tr>
<td></td>
<td></td>
<td>ABOVE M.P. °C</td>
<td>FURN. TEMP. °C</td>
<td></td>
</tr>
<tr>
<td>41-37</td>
<td>Improve crystallinity</td>
<td>-</td>
<td>-</td>
<td>Run aborted during meltdown due to problem at heat exchanger fitting</td>
</tr>
<tr>
<td>41-38</td>
<td>Improve crystallinity</td>
<td>24</td>
<td>42</td>
<td>25</td>
</tr>
<tr>
<td>41-39</td>
<td>Improve crystallinity</td>
<td>8</td>
<td>24</td>
<td>25</td>
</tr>
<tr>
<td>41-40</td>
<td>Improve crystallinity</td>
<td>6</td>
<td>22</td>
<td>27</td>
</tr>
<tr>
<td>41-41</td>
<td>Cast 32 x 32 cm$^2$ 35 kg ingot</td>
<td>15</td>
<td>33</td>
<td>40</td>
</tr>
<tr>
<td>41-42</td>
<td>Improve crystallinity at bottom</td>
<td>37</td>
<td>29</td>
<td>24</td>
</tr>
<tr>
<td>41-43</td>
<td>Improve crystallinity at bottom</td>
<td>48</td>
<td>48</td>
<td>32</td>
</tr>
<tr>
<td>41-44</td>
<td>Improve crystallinity at bottom</td>
<td>62</td>
<td>64</td>
<td>31.5</td>
</tr>
<tr>
<td>RUN</td>
<td>PURPOSE</td>
<td>SEEDING FURN. TEMP. ABOVE M.P. °C</td>
<td>GROWTH CYCLE</td>
<td>REMARKS</td>
</tr>
<tr>
<td>------</td>
<td>-----------------------------</td>
<td>----------------------------------</td>
<td>---------------</td>
<td>--------------------------------</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>DECREASE OF FURN. TEMP. °C</td>
<td>GROWTH TIME IN HRS.</td>
</tr>
<tr>
<td>41-45</td>
<td>Improve crystallinity at bottom</td>
<td>39</td>
<td>29</td>
<td>23</td>
</tr>
<tr>
<td>41-46</td>
<td>Cast 32 x 32 cm² 35 kg ingot</td>
<td>-</td>
<td>-</td>
<td>-</td>
</tr>
<tr>
<td>41-47</td>
<td>Study heat flow</td>
<td>33</td>
<td>33</td>
<td>22</td>
</tr>
<tr>
<td>41-48</td>
<td>Cast 32 x 32 cm² 35 kg ingot</td>
<td>14</td>
<td>14</td>
<td>28.5</td>
</tr>
<tr>
<td>41-49</td>
<td>Study heat flow</td>
<td>33</td>
<td>33</td>
<td>14</td>
</tr>
<tr>
<td>41-50</td>
<td>Study heat flow</td>
<td>20</td>
<td>20</td>
<td>21</td>
</tr>
</tbody>
</table>
Grid Pattern on Cross Section of Ingot Cast in Run 41-41, Corresponding to Positions for Resistivity Values Shown Below

<table>
<thead>
<tr>
<th></th>
<th>(a)</th>
<th>(b)</th>
<th>(c)</th>
<th>(d)</th>
<th>(e)</th>
<th>(f)</th>
<th>(g)</th>
<th>(h)</th>
<th>(i)</th>
<th>(j)</th>
<th>(k)</th>
</tr>
</thead>
<tbody>
<tr>
<td>(a)</td>
<td></td>
<td>1.31</td>
<td>1.17</td>
<td>1.18</td>
<td>1.28</td>
<td>1.27</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>(b)</td>
<td>1.66</td>
<td>1.20</td>
<td>1.19</td>
<td>1.17</td>
<td>1.34</td>
<td>1.23</td>
<td>1.25</td>
<td>1.24</td>
<td>1.20</td>
<td>1.40</td>
<td></td>
</tr>
<tr>
<td>(c)</td>
<td>1.36</td>
<td>1.29</td>
<td>1.34</td>
<td>1.40</td>
<td>1.39</td>
<td>1.46</td>
<td>1.49</td>
<td>1.38</td>
<td>1.29</td>
<td>1.38</td>
<td>1.25</td>
</tr>
<tr>
<td>(d)</td>
<td>1.45</td>
<td>1.44</td>
<td>1.45</td>
<td>1.47</td>
<td>1.48</td>
<td>1.58</td>
<td>1.53</td>
<td>1.40</td>
<td>1.48</td>
<td>1.44</td>
<td>1.37</td>
</tr>
<tr>
<td>(e)</td>
<td>1.60</td>
<td>1.44</td>
<td>1.49</td>
<td>1.53</td>
<td>1.58</td>
<td>1.57</td>
<td>1.60</td>
<td>1.52</td>
<td>1.62</td>
<td>1.44</td>
<td>1.55</td>
</tr>
<tr>
<td>(f)</td>
<td>1.55</td>
<td>1.47</td>
<td>1.55</td>
<td>1.59</td>
<td>1.50</td>
<td>1.52</td>
<td>1.51</td>
<td>1.58</td>
<td>1.59</td>
<td>1.56</td>
<td>1.63</td>
</tr>
<tr>
<td>(g)</td>
<td>1.45</td>
<td>1.58</td>
<td>1.47</td>
<td>1.55</td>
<td>8.55</td>
<td>1.66</td>
<td>1.69</td>
<td>1.75</td>
<td>1.57</td>
<td>1.55</td>
<td></td>
</tr>
</tbody>
</table>

Resistivity data in $\Omega$-cm
Cross Section of Ingot Cast in Run 41-48
**LARGE-AREA SILICON SHEET TASK**

**FIXED-ABRASIVE SLICING TECHNIQUE (FAST)**

**CRYSTAL SYSTEMS, INC.**

F. Schmid  
C.P. Khattak

**Silicon Slicing Summary**

<table>
<thead>
<tr>
<th>RUN</th>
<th>PURPOSE</th>
<th>FEED FORCE/BLADE</th>
<th>AVERAGE CUTTING RATE</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>lb</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>gm</td>
<td>mil/min, mm/min</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>WIRE TYPE</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>REMARKS</td>
</tr>
<tr>
<td>441-SX</td>
<td>Test codeposited bladepack</td>
<td>0.068</td>
<td>31.60</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>3.7</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>0.092</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>5 mil, 0.125 mm W wire, codeposited with 45, 30 ( \mu )m diamonds</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>48% yield. Diamond pull-out caused blade wander.</td>
</tr>
<tr>
<td>442-SX</td>
<td>Test codeposited bladepack</td>
<td>0.066</td>
<td>30.01</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>3.4</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>0.085</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>5 mil, 0.125 mm W wire, codeposited with 45, 30 ( \mu )m diamonds</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>55% yield. Loss of wafers during last inch of cut.</td>
</tr>
<tr>
<td>443-SX</td>
<td>Test codeposited bladepack</td>
<td>0.070</td>
<td>32.14</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>3.5</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>0.087</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>5 mil, 0.125 mm W wire, codeposited with 45, 30 ( \mu )m diamonds</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>38% yield.</td>
</tr>
<tr>
<td>444-SX</td>
<td>Test codeposited bladepack</td>
<td>0.044</td>
<td>19.9</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>-</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>-</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>5 mil, 0.125 mm stainless steel core; 0.1 mil, 2.5 ( \mu )m Cu wire; codeposited with 45, 30 ( \mu )m diamonds</td>
</tr>
<tr>
<td></td>
<td>(25/cm)</td>
<td></td>
<td>Run aborted due to wire jumping from the grooves of support rollers and diamond pullout</td>
</tr>
<tr>
<td>445-SX</td>
<td>Test codeposited bladepack</td>
<td>0.072</td>
<td>32.2</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>2.9</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>0.074</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>5 mil, 0.125 mm W core, codeposited with 45, 30 ( \mu )m diamonds</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>48% yield; diamond pullout reduced cutting effectiveness</td>
</tr>
<tr>
<td>446-SX</td>
<td>Test CSI codeposited bladepack</td>
<td>0.070</td>
<td>31.6</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>3.8</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>0.098</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>5 mil, 0.125 mm W wire, codeposited on one side with 45 ( \mu )m diamonds</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>49% yield.</td>
</tr>
<tr>
<td>447-SX</td>
<td>Test CSI codeposited bladepack</td>
<td>0.072</td>
<td>32.5</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>2.6</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>0.066</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>5 mil, 0.125 mm W wire, codeposited on both sides with 45 ( \mu )m diamonds</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>91% yield.</td>
</tr>
<tr>
<td>448-SX</td>
<td>Test CSI codeposited bladepack</td>
<td>0.072</td>
<td>32.5</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>3.7</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>0.094</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>5 mil, 0.125 mm W wire, codeposited on both sides with 45 ( \mu )m diamonds</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>80% yield.</td>
</tr>
<tr>
<td>449-SX</td>
<td>Life test (2nd run)</td>
<td>0.079</td>
<td>35.8</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>2.8</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>0.071</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>5 mil, 0.125 mm W wire, codeposited on both sides with 45 ( \mu )m diamonds</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>74% yield.</td>
</tr>
<tr>
<td>450-SX</td>
<td>Life test (3rd run)</td>
<td>0.082</td>
<td>37.0</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>2.4</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>0.061</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>5 mil, 0.125 mm W wire, codeposited on both sides with 45 ( \mu )m diamonds</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>38% yield. Sudden breakage of wafers due to loosening of workpiece.</td>
</tr>
<tr>
<td>451-SX</td>
<td>Test CSI codeposited bladepack</td>
<td>0.063</td>
<td>28.5</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>2.15</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>0.055</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>5 mil, 0.125 mm W wire, codeposited on both sides with 45 ( \mu )m diamonds</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>Run aborted due to loss of water coolant system which caused wafer breakage.</td>
</tr>
<tr>
<td>452-SX</td>
<td>Life test (2nd run)</td>
<td>0.062</td>
<td>28.3</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>2.9</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>0.087</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>5 mil, 0.125 mm W wire, codeposited on both sides with 45 ( \mu )m diamonds</td>
</tr>
<tr>
<td></td>
<td>(25/cm)</td>
<td></td>
<td>18% yield. Some breakage during handling.</td>
</tr>
<tr>
<td>453-SX</td>
<td>Slice 15 cm diameter crystal</td>
<td>0.071</td>
<td>32.4</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>1.9</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>0.048</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>5 mil, 0.125 mm W wire, codeposited on both sides with 45 ( \mu )m diamonds</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>Run aborted after 4.5 inch of cut.</td>
</tr>
</tbody>
</table>
SEM Photograph of Electroplated Wire Before Use in Runs 437-SX and 438-SX, Showing Diamonds Buried in Nickel

SEM Photograph of Wire Used in Run 437-SX, Showing High Diamond Concentration and Even Diamond Distribution
SEM Photos of Electroplated Wires Showing No Diamonds on the Sides
SEM Photograph of Wire After Use
In Runs 433–8X Through 435–8X

Wire Shown Above, Before Use
Sample No. 1. CSI Electroplated Wire, with Diamond on One Side
LARGE-AREA SILICON SHEET TASK

RUN NUMBER 453-SX
15 cm diameter ingot
LARGE-AREA SILICON SHEET TASK

RUN NUMBER 452 SX
25/cm Wirepack

DEPTH OF CUT (INCHES)

CUTTING TIME (HOURS)
Sample No. 2. CSI Electroforming Technique to Produce Predetermined Kerf
1. Contract Goals

The contract goals are aimed at demonstrating the state-of-the-art capability of ID slicing for producing wafers suitable for solar cells.

This contract is aimed at demonstrating reduced-kerf slicing of silicon, and slicing throughput is of secondary consideration.

The two slicing methods used for slicing 6-in. dia silicon are aimed at producing wafers with thickness greater than 10 mils with a total material usage at 17 to 18 wafers/cm. This translates to approximately 23 mils for slice thickness plus kerf.

Plunge cutting of 4-in.-dia round and 4-in. square ingots and rotational cutting of 4-in.-dia round ingots are aimed at producing 25 wafers/cm, which translates to about 16 mils for slice thickness plus kerf.

2. Equipment and Blades.

The plunge cutting of 6-in.-dia ingots is being done exclusively on the RD-140 prototypes machine due to its large capacity. The RD-140 saw has a 32-in.-dia blade mount that can slice ingots up to 8-in diameter.

The design of the RD-140 is different from the pivot arm concept. The blade mount and spindle are kept stationary while the ingot is moved vertically by linear air bearing pads on a granite block.

There were three spindles used for the saw. They are:

1) Air-bearing spindle.
2) Hollow conventional-bearing spindle.
3) Solid conventional-bearing spindle.

The solid mechanical spindle has provided the best results. Chief advantages of the mechanical spindle are low vibration, trueness of the rotational plane and high reliability.

The air bearing pads on the granite block were the cause of some vibration which affected the quality of the wafers during the cutting stroke. By adjusting air pressure, the problem has been resolved and the air bearing surface provides an accuracy of 1 μm over a 10-in cutting stroke. The smooth action of the air pads evidences itself by exceptionally good surface quality of wafers cut on the RD-140 saw.

The blade mount used on the RD-140 is a hydraulic Dyna-Head design which does not permit the fine tuning of the ID runout. Typically, the ID of a 32-in. blade had a 2- to 3-mil runout. We are in the process of building a mechanical mount that will allow a much truer ID, thereby allowing faster cutting rates and thinner wafers.
The 32-in.-dia blades had 6-mil cores, which provided good results. We are able to slice satisfactorily with about 13 mils of kerf. We plan to experiment with 4- and 5-in. cores which will reduce kerf by 1 or 2 mils; however, the thinner cores may be more successful on smaller-diameter blades. Since we do not need the full capacity of the 32-inch blade, we plan to make a 27-inch blade mount that will amply accommodate 6-in.-dia crystals.

Rotational slicing of 6-in. and 4-in. round crystals and plunge slicing of 4-in. square crystals were done on a standard 22-inch STC saw equipped with crystal rotation and programmed feed rate. The programmable feed is of a new design that allows feed rates up to 6 in./min. Programming is done through a cam that moves a linear potentiometer.

All slicing was programmed for the rotational slicing and slicing of 4-in.-square wafers.

The 22-inch blades had 6-mil cores, which gave kerf losses from 11 to 12 mils. We tried some 22-inch blades with 5-mil cores, but they were not very successful. We think that the problem was with the material and we have ordered some new 5-mil sheet material. We also plan to test 4-mil cores, which will reduce kerf below 10 mils.


3.1 Six-in-Dia Plunge Cutting

Average kerf for the 32-in.-dia blades was 13 mils. We were able to cut wafers down to 12 mils thick with yield greater than 85%. Throughout the 6-in. plunge runs, we were able to maintain cutting speeds at 1.5 in./min. The kerf plus slice thickness yielded about 16 wafers/cm; our goal is 17 wafers per cm.

The greatest area for improving wafers/cm will come from reduction of kerf losses. A 27-inch OD can amply accommodate 6-in.-dia wafers. Kerf should be reduced to 11.5 mils for the 27-in.-dia blades. With the present slice thickness of 12 mils, we should achieve 17 wafers per cm.

3.2 Six-in-Dia Rotational Slicing

Rotational slicing of 6-in.-dia wafers was less successful than plunge cutting. Although kerf was reduced to 11.5 mils on the 22-inch blade, it was difficult to get whole wafers less than 18 mils thick. Even at 20 mils, yield was only about 50%. Cutting rates were about .3 in./min. It was much more difficult to slice 6-in. dia ingots rotationally than 4-dia.-dia ingots. The problem may be due to alignment of the rotational axis and larger deviations at the larger diameter.

3.3 Rotational Slicing of 4-in.-Dia Ingots

We were able to cut wafers down to 9 mils thick with about 9.5 mils kerf. Rotational slicing of 4-in.-dia wafers yielded the lowest kerf due to
the use of smaller 16-in blades. Average cutting rates were about 0.4 in./min for plunge cutting. The feed was programmed from 0.080 to 0.600 in./min and the rotation from 9 to 20 rpm.

3.4 Plunge Cutting of 4-in. Squares

We achieved best results on 4-in. square polycrystalline silicon with a fine-grain structure (1 to 5-mm grain sizes.) With 11 mils kerf, we were able consistently to cut 5 to 6-mil wafers at 1 in./minute. Yield was better than 90%. When the thickness was doubled to 10 or 12 mils we were able to increase cutting rates to 2.5/min with the same yield. This type of material seems to slice much better than single-crystal or larger-grain polycrystalline silicon.

We tested other 4-in.-square material but were not able to reduce slice thickness below 10 mils with the same yields.

4. Conclusions

The best results are achieved by plunge cutting 6-in.-dia single-crystal silicon and 4-in.-square fine-grain polycrystalline silicon. Although rotational slicing allows for use of smaller blades, ease of set-up, lower equipment cost and faster cutting rates seem to favor conventional plunge cutting. Of course, square ingots must be plunge cut.

We still intend to pursue rotational slicing of 6-in.-dia silicon because the problems we are encountering may be due to the equipment being used rather than inherent deficiencies in rotational slicing. The biggest problem we are seeing is the difficulty in aligning the rotational axis, which may be resolved by better equipment and techniques.

In terms of achieving the stated goals of material usage, we have already demonstrated 25 wafers/cm with 4-in.-square material and we should be able to demonstrate 17 to 18 wafers/cm with 6-in. material within a short time with the 27-inch blade mount.

Production capability with desired add-on costs is very easily attainable with some more development in terms of automation using present state-of-the-art ID technology.

5. Recommendations for Future Work

We plan to continue plunge cutting and rotational cutting of 6- and 4-in. ingots.

The RD-140 and the STC 22-inch machines will be modified to improve results. Both machines will be changed to mechanical blade mounts to allow less run-out of the ID.

The blade mount enclosure on the RD-140 will be modified to reduce turbulence, which will allow thinner wafers.
A 27-inch blade mount will be used to slice 6-in. material. We will experiment with 4-mil and 5-mil core material on the 22- and 27-inch blade mounts to reduce kerf losses.
LARGE-AREA SILICON SHEET TASK

Contract Goals

<table>
<thead>
<tr>
<th>6-inch Diameter</th>
<th>17-18 wafers/cm (23 mils T + K)</th>
</tr>
</thead>
<tbody>
<tr>
<td>4-inch Square</td>
<td>25 wafers/cm (16 mils T + K)</td>
</tr>
<tr>
<td>4-inch Round</td>
<td></td>
</tr>
</tbody>
</table>

Slicing Methods

Plunge Cutting

<table>
<thead>
<tr>
<th>6&quot; Ø Round</th>
</tr>
</thead>
<tbody>
<tr>
<td>4&quot; Ø Round</td>
</tr>
<tr>
<td>4&quot; Square</td>
</tr>
</tbody>
</table>

Rotational Cutting

<table>
<thead>
<tr>
<th>6&quot; Ø Round</th>
</tr>
</thead>
<tbody>
<tr>
<td>4&quot; Ø Round</td>
</tr>
</tbody>
</table>
LARGE-AREA SILICON SHEET TASK

Equipment

- RD-140 Prototype 32-inch Saw
- Standard STC 22-inch Saw

Modifications:

- Programmable Feed Rate
- Crystal Rotation
- Monitoring Devices

- Blades
  32-inch - 13 mils kerf
  22-inch - 11 mils kerf
  22-inch - 10 mils kerf
  16-inch - 9 mils kerf

Slicing Results

<table>
<thead>
<tr>
<th>Kerf</th>
<th>Slice Thickness</th>
<th>Wafers/ cm</th>
<th>Cutting Speed</th>
<th>Yield</th>
</tr>
</thead>
<tbody>
<tr>
<td>6&quot; Ø Plunge</td>
<td>13 mils</td>
<td>12 mils</td>
<td>16</td>
<td>1.5 in/min</td>
</tr>
<tr>
<td>6&quot; Ø Rotary</td>
<td>11.5 mils</td>
<td>18 mils</td>
<td>13</td>
<td>.6 in/min</td>
</tr>
<tr>
<td>4&quot; Ø Rotary</td>
<td>9.5 mils</td>
<td>9 mils</td>
<td>21</td>
<td>.8 in/min</td>
</tr>
<tr>
<td>4&quot; Plunge</td>
<td>11 mils</td>
<td>5 mils</td>
<td>25</td>
<td>1 in/min</td>
</tr>
</tbody>
</table>
Side View of Silicon Technology Corp. RD-140 Prototype 32-in. ID Saw
(Note Fixed Saw Head and Movable Ingot Feed Fixtures)
Close-Up View of Ingot Rotating Fixture as Mounted in Standard STC 22-in. ID Saw
12-inch ID Blade for STC RD-140 Prototype ID Saw in Background

ORIGINAL PAGE IS OF POOR QUALITY
## LARGE-AREA SILICON SHEET TASK

### IPEG Assumptions With Present Technology (1980 $)

<table>
<thead>
<tr>
<th></th>
<th>6 in-round</th>
<th>4 in-square</th>
<th>4 in-square</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>Ingot Size</strong></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td>6 in-round</td>
<td>4 in-square</td>
<td>4 in-square</td>
</tr>
<tr>
<td><strong>Wafer Thickness</strong></td>
<td>12 mils</td>
<td>6 mils</td>
<td>12 mils</td>
</tr>
<tr>
<td><strong>Cutting Speed</strong></td>
<td>1.5&quot;/min.</td>
<td>1&quot;/min.</td>
<td>2.5&quot;/min.</td>
</tr>
<tr>
<td><strong>Equipment Cost</strong></td>
<td>$45,000.00</td>
<td>$40,000.00</td>
<td>$40,000.00</td>
</tr>
<tr>
<td><strong>Machine Area</strong></td>
<td>84 ft.(^2)</td>
<td>80 ft.(^2)</td>
<td>80 ft.(^2)</td>
</tr>
<tr>
<td><strong>No. of Machines/Operator</strong></td>
<td>10</td>
<td>10</td>
<td>10</td>
</tr>
<tr>
<td><strong>Blade life</strong></td>
<td>4,000 slices</td>
<td>4000 slices</td>
<td>4000 slices</td>
</tr>
<tr>
<td><strong>Blade Cost</strong></td>
<td>100</td>
<td>80</td>
<td>80</td>
</tr>
<tr>
<td><strong>Other Materials/Year</strong></td>
<td>1800</td>
<td>1800</td>
<td>1800</td>
</tr>
<tr>
<td><strong>Power Consumption</strong></td>
<td>2000 watts</td>
<td>2000 watts</td>
<td>2000 watts</td>
</tr>
<tr>
<td><strong>Add-on Cost/Meter(^2)</strong></td>
<td>25.79</td>
<td>42.50</td>
<td>17.02</td>
</tr>
</tbody>
</table>

### Sheet Cost Comparison: 4-in. Square Wafers ($/m\(^2\))

![Graph showing sheet cost comparison for 4-in. square wafers](image-url)

- **6 mil wafers**
- **12 mil wafers**

---

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LARGE-AREA SILICON SHEET TASK

Plans for ID Technology

Near Term -
27-inch Blade Mount
Mechanical Blade Mount
Redesigned Wheel Guard
Thinner core 22- and 27-inch Blades
Programs for Feed Rates

Long Term -
Equipment Design
  - Higher Throughput
  - Automation
Blade Design
Systems Approach to Factory Design
SUMMARY OF WORK AND RESULTS:

Severe limitations were experienced in slicing thin wafers with ID rotation because of anisotropic material characteristics of single-crystal silicon.

Reduction of ingot feed eliminated fracturing problems but resulted in less than cost-effective wafer-throughput levels.

Best results achieved consistently with ID rotation are 250 µm-thick, 100-µm-dia wafers with kerfs of 200 µm sliced at a feed rate of 15 µm/min.

Results were improved by increasing cutting head size, thereby reducing high-frequency vibrations during slicing.

Cutting-edge position control was effective in all experiments, particularly when cutting with low-kerf (152-200 µm) blades.

Prefabricated blade inserts for ID blade show great potential but require further work in bonding of insert to core to become an effective production tool.

Alternative solution of etched blade core construction has shown good results.

Comparison of ID plunge and rotation cutting results indicate that a multiple-ingot ID plunge technique will improve slicing production significantly.

Oriented Fractures due to ID Rotation Slicing

Closed-Loop Blade Position Control System
LARGE-AREA SILICON SHEET TASK

Close-Up of Blade Position Control System With Ingot in Position for Wafering

Perspective View of Prefabricated Insert Blade

ID Blade With Core Ingot

Close-Up View of Insert-Core Bone Showing Distortion at Weld

ID Blade Construction With Etched Core

Conceptual Drawing of Multiple Ingot Feed for ID Wafering
LARGE-AREA SILICON SHEET TASK

150-mm-dia Wafers Trimmed to Show Packing Improvement With Hexagonal Shape

Meyer & Burger TS-23 ID Saw

Close View of Meyer & Burger TS-23 27-in. Blade Head
LARGE-AREA SILICON SHEET TASK

CHARACTERIZATION
APPLIED SOLAR ENERGY CORP.

Material Evaluation

1. EFG (MOBIL - TYCO):
   
   A. COMPARISON OF EFG MATERIALS WITH AND WITHOUT A CO ENVIRONMENT IN THE SAME FURNACE.
   
   B. LOW TEMPERATURE ANNEALING (600°C, 30 hr.)
   
   C. GRAIN BOUNDARIES PASSIVATION WITH TWO STEP DIFFUSION (ALSO INCLUDE POLY HAMCO CZ AND SILSO)

2. DENDRITIC WEB (WESTINGHOUSE)
   
   A. BASELINE PROCESS
   
   B. ADVANCE PROCESSES

3. HEM (CRYSTAL SYSTEM) - MAPPING OF A CRYSTAL:
   
   HEM I.D. 41-41C

EFG Materials With and Without CO In Ambient of Same Furnace

<table>
<thead>
<tr>
<th></th>
<th>$V_{oc}, \text{mV}$</th>
<th>$J_{SC}, \text{mA/cm}^2$</th>
<th>$CFF %$</th>
<th>$\eta %$</th>
</tr>
</thead>
<tbody>
<tr>
<td>Without CO</td>
<td>540</td>
<td>22.9</td>
<td>70</td>
<td>8.6</td>
</tr>
<tr>
<td>With CO</td>
<td>567</td>
<td>25.1</td>
<td>76</td>
<td>10.7</td>
</tr>
<tr>
<td>CZ Control</td>
<td>582</td>
<td>28.2</td>
<td>78</td>
<td>12.7</td>
</tr>
</tbody>
</table>

*SELINEL PROCESS ON 2 x 2 CELLS WITH $I_{ILL}$ MEASURED AT 280°C AM1.*
LARGE-AREA SILICON SHEET TASK

EFG Material With Low-Temperature Annealing
(600°C, 30 h)

<table>
<thead>
<tr>
<th></th>
<th>Voc, mV</th>
<th>Jsc mA/cm²</th>
<th>CFF %</th>
<th>η %</th>
</tr>
</thead>
<tbody>
<tr>
<td>Not Annealed</td>
<td>493</td>
<td>13.2</td>
<td>74</td>
<td>4.8</td>
</tr>
<tr>
<td>Annealed</td>
<td>493</td>
<td>13.3</td>
<td>73</td>
<td>4.7</td>
</tr>
<tr>
<td>Cz Control</td>
<td>568</td>
<td>20.1</td>
<td>74</td>
<td>8.5</td>
</tr>
</tbody>
</table>

BASELINE PROCESS ON 2x2 CELLS WITHOUT AR MEASURED AT AM1 AT 28°C. (EFG MATERIAL WITHOUT CO IN THEIR GROWTH)

Average Short-Circuit Current Density (Jsc mA/cm²) for Two-Step Diffusion Process (750°C, 9 h in POCl₃)

<table>
<thead>
<tr>
<th></th>
<th>EFG</th>
<th>Poly</th>
<th>Silso</th>
</tr>
</thead>
<tbody>
<tr>
<td>No 2 Step Diffusion</td>
<td>17.9</td>
<td>22.1</td>
<td>22.4</td>
</tr>
<tr>
<td>2 Step Diffusion</td>
<td>15.3</td>
<td>22.1</td>
<td>22.3</td>
</tr>
</tbody>
</table>

Jsc of Control : 23.4 mA/cm²

Baseline Process on 2 x 2 cells without AR, measured at AM1, 28°C. (EFG Material without CO in growth)
### Dendritic Web Solar Cell from Baseline Process

<table>
<thead>
<tr>
<th>WEB ID. NO.</th>
<th>17-1373 p=8.5/cm²</th>
<th>17-1377 p=3.4/cm²</th>
<th>17-1390 p=9.4/cm²</th>
<th>CZ CONTROL</th>
</tr>
</thead>
<tbody>
<tr>
<td>Voc (mV)</td>
<td></td>
<td></td>
<td></td>
<td>588</td>
</tr>
<tr>
<td>AV.</td>
<td>532</td>
<td>534</td>
<td>515</td>
<td></td>
</tr>
<tr>
<td>S.D.</td>
<td>530-534</td>
<td>532-536</td>
<td>512-513</td>
<td></td>
</tr>
<tr>
<td>R</td>
<td>2</td>
<td>2</td>
<td>3</td>
<td></td>
</tr>
<tr>
<td>Jsc (mA/cm²)</td>
<td></td>
<td></td>
<td></td>
<td>29.8</td>
</tr>
<tr>
<td>AV.</td>
<td>28.8</td>
<td>28.1</td>
<td>28.6</td>
<td></td>
</tr>
<tr>
<td>S.D.</td>
<td>0.5</td>
<td>0.3</td>
<td>0.5</td>
<td>0.5</td>
</tr>
<tr>
<td>R</td>
<td>28.3-28.4</td>
<td>27.8-28.4</td>
<td>27.4-29.0</td>
<td>29.3-30.0</td>
</tr>
<tr>
<td>CFF (%)</td>
<td></td>
<td></td>
<td></td>
<td>74</td>
</tr>
<tr>
<td>AV.</td>
<td>76</td>
<td>76</td>
<td>75</td>
<td></td>
</tr>
<tr>
<td>S.D.</td>
<td>1</td>
<td>1</td>
<td>1</td>
<td>3</td>
</tr>
<tr>
<td>R</td>
<td>75-76</td>
<td>75-76</td>
<td>74-77</td>
<td>70-77</td>
</tr>
<tr>
<td>η (%)</td>
<td></td>
<td></td>
<td></td>
<td>13.0</td>
</tr>
<tr>
<td>AV.</td>
<td>11.6</td>
<td>11.4</td>
<td>11.0</td>
<td></td>
</tr>
<tr>
<td>S.D.</td>
<td>0.1</td>
<td>0.1</td>
<td>0.2</td>
<td>0.6</td>
</tr>
<tr>
<td>R</td>
<td>11.4-11.7</td>
<td>11.3-11.5</td>
<td>10.6-11.3</td>
<td>12.2-13.5</td>
</tr>
</tbody>
</table>

**NOTE.** 1) 2x2 cm cells under AM1 measured at 28°C test block temperature.
### Dendritic Web Solar Cells From Advanced Process

<table>
<thead>
<tr>
<th></th>
<th>WEB</th>
<th>WEB</th>
<th>CZ</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>Voc (mV)</strong></td>
<td>545</td>
<td>531</td>
<td>581</td>
</tr>
<tr>
<td><strong>Jsc (mA/cm²)</strong></td>
<td>29.2</td>
<td>28.1</td>
<td>29.9</td>
</tr>
<tr>
<td><strong>CFF (%)</strong></td>
<td>79</td>
<td>78</td>
<td>78</td>
</tr>
<tr>
<td><strong>η (%)</strong></td>
<td>12.5</td>
<td>11.7</td>
<td>13.5</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th></th>
<th>14</th>
<th>11</th>
<th>-</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>526-558</td>
<td>514-546</td>
<td>570-582</td>
</tr>
<tr>
<td></td>
<td>0.6</td>
<td>0.5</td>
<td>-</td>
</tr>
<tr>
<td></td>
<td>28.5-29.8</td>
<td>27.4-28.8</td>
<td>29.3-30.4</td>
</tr>
<tr>
<td></td>
<td>1</td>
<td>2</td>
<td>-</td>
</tr>
<tr>
<td></td>
<td>78-80</td>
<td>75-79</td>
<td>77-79</td>
</tr>
<tr>
<td></td>
<td>11.8-13.0</td>
<td>10.9-12.2</td>
<td>13.2-13.7</td>
</tr>
</tbody>
</table>

**NOTE:**
1) Measured under AM1 at 28°C test block temperature.
2) Advanced process: SJ+BSF+MLAR

**HEM ID 41-41C**

- **SIZE:** 12" x 12" x 6"
- **WT.:** ~ 35 kg
**LARGE-AREA SILICON SHEET TASK**

**Summary of Results for HEM (ID 41-41C)**

Average Parameters for Horizontally Cut Layers
(Values Normalized to Control are in Parenthesis)

<table>
<thead>
<tr>
<th></th>
<th>Voc, mV</th>
<th>Jsc, mA/cm²</th>
<th>CFF %</th>
<th>η %</th>
</tr>
</thead>
<tbody>
<tr>
<td>Top</td>
<td>557 (.97)</td>
<td>26.1 (.93)</td>
<td>69 (.91)</td>
<td>10 (.82)</td>
</tr>
<tr>
<td>Middle</td>
<td>566 (.98)</td>
<td>27.0 (.96)</td>
<td>73 (.96)</td>
<td>11.1 (.90)</td>
</tr>
<tr>
<td>Bottom</td>
<td>550 (.95)</td>
<td>25.1 (.89)</td>
<td>73 (.96)</td>
<td>10.0 (.81)</td>
</tr>
<tr>
<td>Cz Control</td>
<td>577</td>
<td>28.2</td>
<td>76</td>
<td>12.3</td>
</tr>
</tbody>
</table>

Average Parameters for Vertically Cut Layer
(Values Normalized to Control are in Parenthesis)

<table>
<thead>
<tr>
<th></th>
<th>Voc, mV</th>
<th>Jsc, mA/cm²</th>
<th>CFF %</th>
<th>η %</th>
</tr>
</thead>
<tbody>
<tr>
<td>CENTRAL</td>
<td>559 (.97)</td>
<td>25.8 (.95)</td>
<td>72 (.93)</td>
<td>10.4 (.85)</td>
</tr>
<tr>
<td>Cz Control</td>
<td>577</td>
<td>27.3</td>
<td>77</td>
<td>12.2</td>
</tr>
</tbody>
</table>

All values were measured in AM1, 28°C. Cells were fabricated by baseline process with SiO AR coating.

Cell Size: 2x2cm
LARGE-AREA SILICON SHEET TASK

HORIZONTALLY CUT HEM ID 41-41C

$J_{sc}(mA/cm^2)$ for Bottom Layer

\[
\begin{array}{cccccccc}
25.8 & 26.3 & 25.8 & - & 19.8 & 23.3 & 24.3 & 19.3 \\
- & - & 25.8 & 26.3 & 21.2 & 21.2 & 22.2 & 25.4 \\
25.4 & 26.3 & 25.9 & 26.9 & 26.4 & 26.2 & 26.9 & 25.2 \\
24.9 & 25.4 & 25.9 & 24.9 & 26.8 & 25.8 & 23.8 & 25.7 \\
\end{array}
\]

Ave 25.1 (892)
Control Ave 28.2

CFF (%) for Top Layer

\[
\begin{array}{cccccccc}
78 & 72 & 45 & 77 & 35 & 37 & 62 & 59 & 76 \\
75 & 76 & 73 & 79 & 52 & 74 & 75 & 75 & 61 \\
74 & 73 & 74 & 51 & 77 & 76 & 62 & 76 & 77 \\
- & - & 74 & 72 & 73 & 74 & 74 & - & - \\
\end{array}
\]

Ave 68% (90%)
Control Ave 71%
LARGE-AREA SILICON SHEET TASK

VERTICALLY CUT HEM ID 41-41C

Resistivity Distribution

CFF (%)

AVE: 72% (93%)
CONTROL AVE: 76%
LARGE-AREA SILICON SHEET TASK

HEM ID 41-41C

Represented by top layer → 25%
Represented by middle layer → 60%
Represented by bottom layer → 15%

Average for the whole crystal: 10.7% AM1
Normalized to Cz control: 87% (in usable area)
Encapsulation Task progress and status were reported in three major PIM sessions. A general overview and summary of module encapsulation technology and design guidelines was presented by Ed Cuddihy in the Wednesday-morning plenary session, with a follow-up discussion session on Thursday afternoon. Individual contractor reports were presented during contract reviews on Wednesday afternoon and Thursday morning.

A major goal of the Encapsulation Task is to compile and publish this year an encapsulation-design report that will document the encapsulant material system performance requirements and the status and characteristics of available encapsulant materials and fabrication processes. The report is being organized to be of maximum usefulness to module manufacturers and to the material-supply industry. This is being achieved through discussions at the PIMs and continuing technical contracts between LSA and industry. It is expected that this encapsulation-design report will be updated in subsequent years. Ed Cuddihy presented at this PIM the current technology status and the general content of the evolving encapsulant material specifications and performance requirements. Selected figures from the presentation are included in these Proceedings (see p. 59).

The following highlights are summarized from the LSA contract review session, which also covered JPL in-house efforts on module-life assessment and photothermal aging. Selected figures from the presentations are included.

Springborn Laboratories: EVA formulated specifically for PV module lamination is now being made available to module manufacturers for module production evaluation. Alternative potant materials being intensively developed and evaluated include EMA for lamination and PnBA for a casting potant. One low-cost edge-gasket material, under evaluation for module mounting, that appears to meet the LSA goals is EPDM (ethylene propylene diene monomer) rubber, which comes in a variety of compositions and molded forms. The EPDM edge gasket may be supplied either as a continuous extruded shape and cut to fit the module edges or as a complete molded one-piece "picture frame."

Spire Corp.: Small solar modules with cells electrostatically bonded (ESB) to a borosilicate glass superstrate and encapsulated on the back side with a conventional potant and cover film have been produced routinely, and these modules are currently undergoing durability testing. These modules have also been produced with preformed mesh front metallization applied during the ESB process.
ENCAPSULATION TASK

The ESB process has also been demonstrated as a lower-temperature approach to bonding Si wafers to larger glass sheets and processing the cells with interdigitated back-contact metallization.

Illinois Tool Works: Ion plating of front metallization has been used on 4-in.-dia wafers with boron-doped junctions in n-type base Si to produce cells as good as production cells. Low-cost materials and high deposition rates are the potential advantages of this approach.

Rockwell Science Center: The measurement of module or cell ac impedance has been demonstrated as a potentially sensitive non-destructive field or laboratory evaluation technique for assessing changes in solar cell series and shunt resistance. The technique will be applied to a set of Block II modules now undergoing accelerated life testing at JPL.

JPL In-House: Photothermal degradation rates and mechanisms and ultraviolet absorption characteristics of polymeric encapsulants are being measured as a function of polymer composition and test exposure conditions. Data are being obtained for silicones, EVA, PnBA, polyurethane, and acrylic films. Additional materials will be characterized during the coming year. Failure mechanisms and critical temperature limits associated with module hot-cell experience are being identified for use in establishing module circuit design and diode protection criteria.

Modeling of the photodegradation of UV screening acrylic outer cover films has yielded rates of degradation of the material constituents and of the total system. These data have been used to provide material composition criteria for the achievement of optimum low-cost long-life cover films.

Encapsulation Task Highlights Summary: Candidate encapsulant material systems and configurations that meet the LSA cost and performance goals and have the potential for meeting the life and durability goals have been identified and demonstrated. Recognizing that module manufacturers may prefer different module assembly methods (e.g., casting vs laminating pottants), candidate pottants for each process have been identified. Furthermore, it is expected that future module designs will be optimized for specific applications and for specific geographic or climatic areas. In consideration of these different requirements, candidate design approaches within the cost guidelines include both the glass superstrate designs and the steel or wood hardboard substrate panel designs. Each design approach has its advantages and disadvantages, depending on application and deployment site. The lowest potential cost resides with the hardboard substrate design.

Validation of the 20-year module life potential is still the focus of intensive LSA studies on photothermal degradation at JPL with contracted support from organizations that include Case Western Reserve University, University of Toronto, Colorado State University, Rockwell Science Center and the California Institute of Technology.

Specific life-limiting module failure modes that have been observed and related to the characteristics of the encapsulation material systems include cell cracking due to gas evolution under hot-spot cells and cell cracking and interconnect fatigue due to expansion and contraction of organic substrate panels with varying humidity and temperature. Candidate solutions to these
ENCAPSULATION TASK

Failure modes have been identified and are in the process of evaluation. Solution approaches include optimizing the module circuit design to limit hot-spot temperatures, controlling the substrate expansion stresses by material selection and packaging design and by ranking and selecting encapsulants for the greatest photothermal stability.

Encapsulation Task Technical Readiness

I. ENCAPSULANT MATERIALS, PROCESSES, & DESIGNS WHICH MEET THE LSA COST, PERFORMANCE, & LIFE GOALS
   - Fabrication of prototype modules with selected materials and production methods
   - Pass JPL qualification tests
   - A Design Specification Handbook for industry (material suppliers and module builders)
   - Optimize designs for minimum life cycle energy cost

II. ASSESS 20-YEAR LIFE POTENTIAL BY ACCELERATED AND OUTDOOR TESTING
   - Identify and eliminate or minimize long term material degradation modes
   - Accumulate maximum operating experience
   - Provide life prediction relationships based on models and accelerated tests
ENCAPSULATION TASK

LOW-COST ENCAPSULATION SYSTEMS

SPRINGBORN LABORATORIES, INC.

Ethylene Vinyl Acetate (EVA) Pottant

NOW PRODUCED BY SPRINGBORN LABORATORIES—“CRANEGLASS” SPACER

ADVANTAGES:
- Glass mat available in roll form
- Effective anti-blocking surface
- Positive spacer for module components
- Aids degassing in lamination
- Provides insulation resistance
- Total integrated transmission 91% *
- Add on cost, $0.78/ft²

* Product improvement with no loss of power

Candidate Pottant Under Development
Ethylene Methyl Acrylate*

- Cost, $0.59 / lb
- Very high thermal stability
- Excellent adhesion properties
- Non-hydrophilic
- Available with anti-blocking additive
- Vacuum bag lamination demonstrated
- Total integrated transmission: 91.5 %
- Extrudable in thin films

* Gulf Oil Chemicals
ENCAPSULATION TASK

ETHYLENE/METHYL ACRYLATE

FORMULA NO. A11877

<table>
<thead>
<tr>
<th>Ingredient</th>
<th>Parts</th>
</tr>
</thead>
<tbody>
<tr>
<td>EMA TD 938 BASE RESIN</td>
<td>100.0</td>
</tr>
<tr>
<td>LUPERSOL 231 (CURING AGENT)</td>
<td>3.0</td>
</tr>
<tr>
<td>CYASORB UV-531 (STABILIZER)</td>
<td>0.3</td>
</tr>
<tr>
<td>TINUVIN 770</td>
<td>0.1</td>
</tr>
<tr>
<td>NAUGARD - P (ANTIOXIDANT)</td>
<td>0.2</td>
</tr>
</tbody>
</table>

INGREDIENTS TUMBLE BLENDED PRIOR TO EXTRUSION - NO SEPARATE COMPOUNDING STEP REQUIRED

NO RELEASE PAPER REQUIRED DURING ROLL WINDUP

SAME CURE REQUIREMENTS AS EVA POTTANT

SAMPLES AVAILABLE FOR INDUSTRIAL EVALUATION BY MARCH, 1981
ENCAPSULATION TASK

Butyl Acrylate Casting Syrup

CURRENT FORMULATION:

- BUTYL ACRYLATE POLYMER 35%
- BUTYL ACRYLATE MONOMER 60%
- HEXANEDIOLDIACRYLATE (CROSSLINKING AGENT) 5%

CURE CHARACTERISTICS:

- APPX. 5 MINUTES AT 45°C
- INITIATOR: LUPERSOL - 11, 0.5% BY WEIGHT
- POT LIFE APPX. 8 HOURS AT ROOM TEMPERATURE

SAMPLES WILL BE AVAILABLE FOR INDUSTRIAL EVALUATION BY MAY, 1981

PROPERTIES:

SYRUP: WATER WHITE, CLEAR
VISCOSITY APPX. 10,000 CENTIPOISE
SPECIFIC GRAVITY APPX. 0.94

CURED PROPERTIES:

TENSILE STRENGTH (D538) 200 PSI
100% MODULUS (D-638) 300 PSI
ULTIMATE ELONGATION (D638) 100 %
HARDNESS (SHORE A) 44
GEL CONTENT 84 %
ODOR: ACCEPTABLE LOW

MAY BECOME ACCEPTABLE REPLACEMENT FOR RTV SILICONES
ENCAPSULATION TASK

BUTYL ACRYLATE CASTING SYRUP

NEW METHOD OF PRODUCTION:

- SOLVENT
- MONOMER
- INITIATOR
- POLYMERIZATION VESSEL
- CROSSLINKING AGENT
- WIPED FILM VACUUM STRIPPER

SOLVENT RETURN LOOP

COMPLETED SYRUP

ELIMINATES THE RECOVERY OF DRY POLYMER AND PROCEEDS DIRECTLY TO SYRUP FORMULATION
## Gasket Compounds

<table>
<thead>
<tr>
<th>Elastomer</th>
<th>Cost/Lb</th>
<th>Compression Set Recovery</th>
<th>Cost/Set Recovery</th>
</tr>
</thead>
<tbody>
<tr>
<td>Silicone</td>
<td>$2.53</td>
<td>65 - 90%</td>
<td>2.81 - 3.89</td>
</tr>
<tr>
<td>Ethylene/Vinyl Acetate</td>
<td>$0.85</td>
<td>65 - 80%</td>
<td>1.06 - 1.31</td>
</tr>
<tr>
<td>Neoprene</td>
<td>$0.87</td>
<td>75 - 85%</td>
<td>1.02 - 1.16</td>
</tr>
<tr>
<td>EPDM</td>
<td>$0.58</td>
<td>70 - 90%</td>
<td>0.64 - 0.83</td>
</tr>
</tbody>
</table>

EPDM compounds, advantages:
- **Best Compression Set/Cost Ratio**
- **Low Cost**
- **Easy Extrusion - Complex Profiles**
- **Demonstrated Weatherability**
- **History of Successful Use in Related Applications (Automotive Windshields)**

A. For comparative purposes only
### ENCAPSULATION TASK

#### RS/4 Sunlamp Exposure

<table>
<thead>
<tr>
<th>MATERIAL</th>
<th>HOURS</th>
<th>PROPERTY RETAINED (ASTM D-638)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>TENSILE</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Material</th>
<th>HOURS</th>
<th>TENSILE</th>
<th>ELONGATION</th>
</tr>
</thead>
<tbody>
<tr>
<td>3M ACRYLIC FILM X-22417</td>
<td>3,000</td>
<td>54%</td>
<td>100%</td>
</tr>
<tr>
<td>EMA BASE RESIN (UNCOMPONDED)</td>
<td>5,000</td>
<td>10%</td>
<td>10%</td>
</tr>
<tr>
<td>EMA A11877 (COMPOUNDED)</td>
<td>5,000</td>
<td>100%</td>
<td>100%</td>
</tr>
<tr>
<td>DUPONT TEDLAR 100 BG 30 UT</td>
<td>3,000</td>
<td>100%</td>
<td>100%</td>
</tr>
<tr>
<td>BUTYL ACRYLATE BASE FORMULATION</td>
<td>4,099</td>
<td>N/A</td>
<td>N/A</td>
</tr>
</tbody>
</table>

EVA POTTANT (NO COVER FILM)

CLEAR STABILIZED EVA EXPOSED 17,600 HOURS
NO OBSERVABLE CHANGE

<table>
<thead>
<tr>
<th>TOTAL INTEGRATED TRANSMISSION (%)</th>
<th>ULTIMATE* ELONGATION (%)</th>
<th>TENSILE* STRENGTH (PSI)</th>
</tr>
</thead>
<tbody>
<tr>
<td>CONTROL</td>
<td>91</td>
<td>510</td>
</tr>
<tr>
<td>EXPOSED</td>
<td>90</td>
<td>560</td>
</tr>
</tbody>
</table>

UNSTABILIZED ELVAX 150 (EVA) BECOMES SOFT, Tacky
AND LOSES PHYSICAL PROPERTIES IN LESS THAN 1,000 HOURS

* ASTM D-638

241
ENCAPSULATION TASK

ELECTROSTATIC BONDING
SPIRE CORP.

Phase III Summary

• INTEGRAL FRONT MODULE FABRICATION IS ROUTINE
  --- Efficiency to 13%
  --- Yield in Non-Production Bonder > 90%

• PREFORMED CONTACT BONDING
  --- Process Routine with Skilled Operators
  --- Efficiency Nearly as Good as Conventional Cells

• LOW TEMPERATURE MODULE FABRICATION
  --- 12'' x 16'' Modules Fabricated on Hot Plate
  --- Good Results with Proper Glass Surface
  --- Continue Work to Lower Bond Temperature

• LARGE AREA BONDER ENGINEERING
  --- Conceptual Design Complete
ENCAPSULATION TASK

Low-Temperature Preformed Contact Process

1. Press Preform into Glass at High Temperature

2. Electrostatically Bond Bare Cell to Glass/Wire Structure at Low Temperature
ENCAPSULATION TASK

SEM Photo of Cu Wire Hot Pressed Into Glass Cover Slip (350x)

SEM Photo of Cu Wire Hot Pressed Into Glass Cover Slip (100x)
ENCAPSULATION TASK

ION PLATING

ILLINOIS TOOL WORKS

ITW-Endurex Cell No. 101
Front: Ni, Sn With Bus Bars and Solder Dip
Back: Ti, Cu

ION-PLATED CELL MADE IN JANUARY 1981

SOLAR POWER
4-INCH CELLS

CONTROL GROUP

2.5

2.0

1.5

1.0

0.5

0.0

0

0.1

0.2

0.3

0.4

0.5

0.6

V (VOLTS)

I (AMPS)
ENCAPSULATION TASK

**Proposed Low-Cost Metallization Systems**
For p on n and n on p Solar Cells

<table>
<thead>
<tr>
<th></th>
<th>P on N Type Wafers</th>
<th>N on P Type Wafers</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>Front</strong></td>
<td></td>
<td></td>
</tr>
<tr>
<td>1st Layer</td>
<td>Nickel, Chromium</td>
<td>Nickel, Chromium, Titanium</td>
</tr>
<tr>
<td>2nd Layer</td>
<td>Copper</td>
<td>Copper</td>
</tr>
<tr>
<td><strong>Back</strong></td>
<td></td>
<td></td>
</tr>
<tr>
<td>1st Layer</td>
<td>Titanium</td>
<td>Titanium-Aluminum Alloy</td>
</tr>
<tr>
<td>2nd Layer</td>
<td>Copper (.124 Ω·cm²)</td>
<td>Copper (.091 Ω·cm²)</td>
</tr>
</tbody>
</table>

---Copper is used for ease of connecting
---Additional layers for corrosion protection, etc. may be used

**MATERIAL DEGRADATION AND LIFE PREDICTION**

**JET PROPULSION LABORATORY**

Diagram showing the testing of materials and designs under real and accelerated environments, including outdoor exposure, design development, photothermal studies, degradation modeling, and monitoring techniques.

- **Testing of Materials and Designs**
  - Under real and accelerated environments
  - Outdoor exposure
  - Design development of accelerated test chambers
  - Photothermal studies
  - Degradation mechanism modeling

- **Monitoring of Environment**
  - Radiometers
  - Sun sensors
  - Conductivity
  - Soil measurements
  - AC impedance
  - Pyrolysis GC
  - Dielectric measurements

- **Diagnostic Techniques**
  - Flash photolysis
  - Laser thermal lens
ENCAPSULATION TASK

Long-Term Degradation Modeling

EVA: UNIVERSITY OF TORONTO
STATUS: DEVELOPED COMPUTER MODEL OF PHOTODEGRADATION
PNBA: CASE WESTERN RESERVE U.
STATUS: DEVELOPED MECHANISM OF PHOTODEGRADATION OF UNCROSS-LINKED PNBA
UV SCREENING: IN-HOUSE
COVERS
STATUS: DEVELOPED PHOTODEGRADATION MODEL AND ACCELERATED TESTING CRITERIA

PHOTOTHERMAL DEGRADATION OF EVA FILMS

LOADS AND STRESSES

• UV LEVEL: 6-10 SUNS/DARK
• TEMPERATURE: 25°C, 70°C, 85°C, 105°C
• OXYGEN LEVEL: FULL ACCESS, NO EDGE SEAL, CLOSED OVEN

PROPERTIES MEASURED

• WEIGHT LOSS
• CHANGE IN ABSORBANCE: UV/VISIBLE/IR
• STRESS-STRAIN
• EXTRACTION/GPC/SWELLING STUDIES

OBJECTIVE

• DETERMINE DEGRADATION RATES
ENCAPSULATION TASK

WEIGHT LOSS DATA

70°C
GRADUAL WEIGHT LOSS UP TO 0.5 WT% AFTER 500 HRS OF AGING

85°C
GRADUAL WEIGHT LOSS UP TO 1% AFTER 800 HRS OF AGING

105°C

UV-VISIBLE TRANSMISSION ANALYSIS OF EVA FILMS

- TESTS CARRIED OUT AT 70°C, 85°C, 105°C. SIMILAR FEATURES AT ALL TEMPERATURES RATES DIFFERENT

105°C
a: CLOSED OVEN; b: NO EDGE SEAL, UV; c: UV/AIR
ENCAPSULATION TASK

TRANSMISSION ANALYSIS ON EVA FILMS

RESULTS

• LOSS OF ADDITIVES (800 HR TEST)

<table>
<thead>
<tr>
<th></th>
<th>CLOSED</th>
<th>NO EDGE SEAL</th>
<th>OPEN</th>
</tr>
</thead>
<tbody>
<tr>
<td>85°C</td>
<td>0</td>
<td>11%</td>
<td>19%</td>
</tr>
<tr>
<td>105°C</td>
<td>0</td>
<td>14%</td>
<td>24%</td>
</tr>
</tbody>
</table>

• YELLLOWING: (Δ ABSORBANCE AT 400 nm)

<table>
<thead>
<tr>
<th></th>
<th>CLOSED, NO UV</th>
<th>UV+ NO EDGE SEAL</th>
<th>UV+ AIR</th>
</tr>
</thead>
<tbody>
<tr>
<td>85°C</td>
<td>0.01</td>
<td>0.005</td>
<td>0.005</td>
</tr>
<tr>
<td>105°C</td>
<td>0.02</td>
<td>0.01</td>
<td>0.01</td>
</tr>
</tbody>
</table>

FT — IR ANALYSIS OF EVA FILMS

• 25°C
  SLOW PHOTOOXIDATION INDICATED BY HYDROXYLS FORMATION (OLD DATA)

• 105°C
  FASTER PHOTOOXIDATIVE FORMATION OF HYDROXYLS IN PRESENCE OF UV AND O₂
  BUILD UP OF ACETIC ACID IN CLOSED OVEN

250
ENCAPSULATION TASK

EXTRACTION OF IRRADIATED EVA FILMS

- PERCENT EXTRACTIBLE ~30% UNDER ALL EXPERIMENTAL CONDITIONS AFTER 800 HRS

- MOLECULAR WEIGHT ANALYSIS OF EXTRACTIBLES

\[
105^\circ\text{C}, 800 \text{ HRS}
\]

<table>
<thead>
<tr>
<th>SAMPLE</th>
<th>(\overline{M_n})</th>
</tr>
</thead>
<tbody>
<tr>
<td>CONTROL</td>
<td>200,000</td>
</tr>
<tr>
<td>OVEN (CLOSED)</td>
<td>170,000</td>
</tr>
<tr>
<td>UV/AIR</td>
<td>91,000</td>
</tr>
<tr>
<td>UV/NO EDGE SEAL</td>
<td>44,000</td>
</tr>
</tbody>
</table>

- SWELLING STUDIES: IN PROGRESS

PHOTOTHERMAL TESTING OF PVB FILMS

LOADS AND STRESSES

- TEMP 55°C, 70°C

- O\(_2\) LEVELS: CLOSED OVEN, AMBIENT AIR
  NO EDGE SEAL (3" X 1/2")

- UV LEVELS: 6-10 SUNS, DARK

PROPERTIES MEASURED

- WEIGHT LOSS

- EXTRACTION, MOL. WT.

- TRANSMISSION
ENCAPSULATION TASK

RESULTS

WEIGHT LOSS AT 70°C

<table>
<thead>
<tr>
<th>Condition</th>
<th>WT. Loss</th>
<th>Activation Energy 55-70°C</th>
</tr>
</thead>
<tbody>
<tr>
<td>CLOSED OVEN</td>
<td>&lt;0.5%</td>
<td>~10K CAL/MOLE</td>
</tr>
<tr>
<td>UV/AIR</td>
<td>6%</td>
<td>~10K CAL/MOLE</td>
</tr>
<tr>
<td>NO EDGE SEAL</td>
<td>9%</td>
<td>~10K CAL/MOLE</td>
</tr>
</tbody>
</table>

EXTRACTION AT 70°C

<table>
<thead>
<tr>
<th>Condition</th>
<th>% Soluble</th>
</tr>
</thead>
<tbody>
<tr>
<td>CONTROL</td>
<td>100</td>
</tr>
<tr>
<td>CLOSED OVEN</td>
<td>100</td>
</tr>
<tr>
<td>UV/AIR</td>
<td>54</td>
</tr>
<tr>
<td>NO EDGE SEAL</td>
<td>59</td>
</tr>
</tbody>
</table>
ENCAPSULATION TASK

RESULTS

FT-IR SPECTROSCOPIC ANALYSIS

• CLOSED OVEN, 105°C: Si—H STRETCH DISAPPEARING, NO CARBONYL FORMATION, TRACE HYDROXYL

• UV/AIR AT 105°C, 800 HRS: LOSS OF Si—H LARGE HYDROXYL PEAK, FORMATION OF CARBONYL

EXTRACTION

• PERCENT EXTRACTIBLES UNCHANGED = 0.4%

• NO CHANGE IN MOL. WT. OF EXTRACTIBLES

WEIGHT LOSS DATA

• CLOSED OVEN AT 105°C: 0.3% AT 800 HRS

• UV/AIR AT 105°C: 0.5% AT 800 HRS

TRANSMISSION CHANGE

• YELLOWING IN CLOSED OVEN, ACCELERATED UNDER UV/AIR E (ACTIVATION)

85° — 105° = 20K cal/MOLE
ENCAPSULATION TASK

Photodegradation of PnBA

RATE OF ABSORBANCE CHANGE OF P-NBA AS A FUNCTION OF IRRADIATING TIME

Development of Accelerated Test Chambers

- TESTS CONDUCTED ON WOOD SUBSTRATE MODULES: PREDICTED CELL CRACKING WITH CURRENT DESIGN

- IDENTIFIED NEW FAILURE MODE: CORROSION AT CRACK SITES: MAY BE RADIATION DRIVEN

- TWO TEST CHAMBERS CONSTRUCTED, TESTED, SHIPPED AND INSTALLED AT SPRINGBORN LABS
ENCAPSULATION TASK

Photothermal and Photodegradation
Of UV-Stabilized Front-Cover Films

PHOTOTHERMAL STUDIES OF 3M — ACRYLIC FILM

• AT ROOM TEMP STRAIN AT YIELD POINT WAS MEASURED TO BE 4.5 — 10%
  DEPENDING ON ORIENTATION

• AFTER 800 HRS. AT 85°C, SLIGHT TRANSMISSION GAIN (< 1%) AT 400 nm

Loss of UV Absorber From Korad at 85°C

![Graph showing absorption over time and wavelength](image-url)
ENCAPSULATION TASK

Material Modification Concepts

- CUT DOWN SYNERGISM (SENSITIZATION) THRU MORE RAPID DEACTIVATION OF UV ENERGY

- ATTACH UV ABSORBERS CHEMICALLY ON POLYMER CHAIN

NEW CANDIDATE

COPOLYMER OF MMA AND 5 VINYL TINUVIN

\[
\begin{align*}
\text{5 Vinyl TINUVIN}
\end{align*}
\]
MEPSDU planned activities presented by Solarex and Westinghouse (contracts awarded November, 1980) were critiqued by senior industry representatives. MEPSDU efforts are to demonstrate technology capable of manufacturing modules for $0.70/Wp.

The Solarex process uses 10 x 10-cm Semix polycrystalline wafers with spray-on front-junction formation, back-surface junction, spray-on AR coating, and electroless Ni contacts dipped in solder. The modules will be an EVA-laminated glass superstrate design.

Westinghouse process uses 2.5 x 10-cm dendritic-web ribbons with diffused front junction, diffused back-surface junction, dip AR coating, and evaporated Ti/Pd/Cu-plated Cu contacts. Aluminum electrical interconnections will be ultrasonically welded to the cells. The modules will be an EVA-laminated glass superstrate design.

Critiques indicated that backup activities should be implemented to offset potential problem areas when any are identified.

The near-term cost-reduction contracts resulted in the timely identification and demonstration of cost-effective process improvements, especially in automated cell interconnections and module assembly.

A computer program for cell metallization grid trade-off analyses is available. The program calculates cell power losses from series resistance and shading effects for various cell grid designs.

Analysis of non-mass-analyzed ion implantation indicates that it can be cost-competitive with gaseous diffused junction formation.
MEPSDU STATUS

JET PROPULSION LABORATORY

D.B. Bickler

- Open minded approach using processes from several sources
- Both using cassettes with rectangular wafers
- Both reasonably well balanced production
- Demonstration at relatively small rates (1 MW & 5 MW)
- Both have experience with proposed processes, mostly low volume
- Preliminary design reviews due in March 1981

Near-Term Cost-Reduction Contracts

- Timely identification of cost effective process improvements
- Automated cell interconnecting most cost effective
- Some promising technologies identified which are not yet fully developed

Junction Formation

- Pulsed electron beam annealing machine constructed and ready for testing
- Laser annealing data indicates that with development it can be equivalent to pulsed electron annealing.
- Non-mass analyzed ion implantation not only feasible but practical
PRODUCTION PROCESS AND EQUIPMENT AREA

Metallization

- MIDFILM PROCESSES DEVELOPED USING Ag; SAMPLES BEING PREPARED FOR ENVIRONMENTAL TEST

- BERND ROSS ASSOCIATES Cu BASED PRINTED METALLIZATION SHIFTING EMPHASIS FROM AgF FLUX TO TEFLON

- JPL COMPUTER PROGRAM FOR PARALLEL GRID TRADE OFFS IS AVAILABLE

- MOTOROLA GRID PATTERN ANALYSES USE "ACTUAL" METAL CROSS SECTION

Assembly

- MB ASSOCIATES LAMINATION STATION IN FINAL STAGES OF ASSEMBLY

- JPL IN-HOUSE ASSESSING MEPSDU’s FOR AUTOMATED MECHANICAL HANDLING

- SCIENCE APPLICATIONS DIFFUSE REFLECTION ANALYSIS INDICATES APPROXIMATELY 6% GAIN USING WHITE BACKGROUND ON STATE-OF-THE-ART MODULES
SOLAR CELL JUNCTION PROCESSING SYSTEM
SPIRE CORP.

Solar Cell Junction Processor

- $P_{31}$ Implant @ $2.5 \times 10^{15}$
- 1200 4" Wafers/Hour
- Pulse Anneal - Liquid Phase Epitaxy
- Cassette-to-Cassette
PRODUCTION PROCESS AND EQUIPMENT AREA

SPI-PULSE 7000 Pulse Annealer

- Fluence - 2 Joule/cm² (max.)
- Beam Area - 100 cm²
- Rep Rate - 1 Pulse/Second (Max)
- Transport Rate - 1200 Wafers/Hour
PRODUCTION PROCESS AND EQUIPMENT AREA

SPI-PULSE 7000 Block Diagram

SPI-PULSE 7000 BLOCK DIAGRAM

VIN SUPPLY ——— H V STORAGE LINE ——— H V TRIGGER ——— D IODE ——— CALORIMETER

VIN CONTROL

DATA ACQUISITION SYSTEM

19-POINT CALORIMETER

VACUUM SYSTEMS

CONTROL COMPUTER

ROCKWELL 6502

VACUUM CONTROL

ENTRY LOCK & WAFER POSITION SENSORS

PROCESS CHAMBER & WAFER POSITION SENSORS

EXIT LOCK & WAFER POSITION SENSORS

DATA ACQUISITION COMPUTER

HP 9825

DATA ACQUISITION SYSTEM

19-POINT CALORIMETER

MAPNET CONTROL

BEAM FOCUS MAGNET

N Layout of High-Speed Vacuum Transport

ION BEAM FOOTPRINTS

ION IMPLANTER

ION BEAM

OUTPUT LOCKS

ELECTRON BEAM

PULSE ANNEALER

TRACK SPEED: 1100"/min

TRACK SPEED: 3' /min

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PRODUCTION PROCESS AND EQUIPMENT AREA

Process Chamber: Top View
Y Track Cassette Input Locks

- Outer Lock Door Housing
- Elevator Drive
- External Cassette Valve
- Wafer Transfer Arm
- Internal Elevator Cassette
- Pumping Port
- TO IMPLANT REGION
Junction Processor: Hardware Status

1. ELECTRON BEAM PULSER
   - All Hardware Fabricated
   - Assembly Almost Completed
   - Control/Transport System Operational
   - HV Checkout Next Week
   - Anneal Development in March

2. WAFER TRANSPORT SYSTEM
   - Pulser Portion Completed
   - Ion Implanter Track Being Designed
   - Cassette Elevators Design Complete

3. ION IMPLANTER
   - Concept Determined
   - Design to Begin in 1-2 Months
# Development of Junction Processing Equipment

<table>
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<tr>
<th>PROGRAM TASKS</th>
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<th>1981</th>
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|                  | 17th PIM |
## PRODUCTION PROCESS AND EQUIPMENT AREA

### LASER ANNEALING FOR ION-IMPLANTED JUNCTIONS

**LOCKHEED MISSILES & SPACE CO. INC.**

2 x 4 cm Cell Processing Variations and Results

<table>
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<tr>
<th>WAFER SURFACE CONDITIONS</th>
<th>ION IMPLANTATION LEVELS</th>
<th>SCREEN CONDITIONS</th>
<th>LASER ENERGY DENSITY (J/cm²)</th>
<th>QTY CELLS</th>
<th>MEAN VALUES</th>
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<td>Voc(mV)</td>
<td>Iac(mA)</td>
<td>CFF(%)</td>
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**WITH BF₂:**

- **CHEM-POLISHED PO-5**
  - 5 KEV, 2.5 x 10ⁱ⁸
  - 25 KEV, 5 x 10¹⁵
  - 1.2
  - PEA 5
  - 497 265 71.3 11.8

- **CHEM-POLISHED PO-10**
  - 10 KEV, 2.5 x 10¹⁸
  - 25 KEV, 5 x 10¹⁵
  - 1.2
  - PEA 5
  - 541 255 76.6 12.2

- **TEXTURE ETCHED TE 10**
  - 10 KEV, 4 x 10¹⁵
  - 1.2
  - 6
  - 463 257 70.7 9.0

**WITH BF₂:**

- **CHEM-POLISHED PO-5**
  - 5 KEV, 2.5 x 10¹⁸
  - 5 KEV, 2.5 x 10¹⁸
  - 25 KEV, 5 x 10¹⁵
  - 1.5
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- **TEXTURE ETCHED TE 10**
  - 10 KEV, 4 x 10¹⁵
  - 1.2
  - 6
  - 463 257 70.7 9.0
## PRODUCTION PROCESS AND EQUIPMENT AREA

### 2 x 4 cm Cells Ranked by Conversion Efficiencies

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<td>Text Etch, 10 KeV, LA @ 1.5J, No BSF</td>
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* Laser Annealed
Pulsed Laser Annealed 1.2 J/cm²

As Implanted, 31P

ORIGINAL PAGE IS
OF POOR QUALITY
SIMS Profile of Phosphorus in Texture-Etched Silicon

- **Laser Annealed (1.5J/cm²)**
- **As Implanted**

**Concentration (atoms/cc)**

**Depth (microns)**
SIMS Profile of Boron in Chem-Polished Silicon

CONCENTRATION (atoms/cc)

0 0.30 0.60 0.90 1.20 1.50

DEPTH (microns)

AS IMPLANTED
ELECTRON BEAM ANNEALED
LASER ANNEALED (1.5J/CM²)
ELECTRON BEAM PLUS
LASER ANNEALED (1.5J/CM²)
SIMS Profile of Boron in Flash-Etched Silicon

- As Implanted
- Electron Beam Annealed
- Laser Annealed (1.5 J/cm²)
- Electron Beam Plus Laser Annealed (1.5 J/cm²)

CONCENTRATION (atoms/cc)

DEPTH (microns)
PRODUCTION PROCESS AND EQUIPMENT AREA

Scan Pattern for Annealing 3-in.-dia Wafer
## Process Verification: 2 x 2 cm Cells

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<td>Flash Etched, 10 KeV, 2.5 x 10¹⁵/cm²</td>
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<td>10 KeV, 2.5 x 10¹⁵/cm²</td>
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<td>582</td>
<td>137</td>
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Nd: Glass Laser for 1-PPS Application
Conclusions

- Texture etched silicon surfaces are not compatible with pulsed laser annealing processing.

- Implantation/pulse annealing parameters for a back surface field formation require further development to optimize performance.

- Screened and fired aluminum paste for a back surface field formation yield acceptable performance in combination with front implant/laser annealed devices.

- A high throughput pulsed laser system to accommodate single pulse annealing of three (3) inch diameter wafers at a rate of one (1) per second appears feasible.
PRODUCTION PROCESS AND EQUIPMENT AREA

NON-MASS-ANALYZED ION IMPLANTS

CALIFORNIA INSTITUTE OF TECHNOLOGY
JET PROPULSION LABORATORY

D.J. Fitzgerald

PURPOSE

- INCREASE THROUGHPUT (BEAM CURRENT)
- REDUCE COMPLEXITY (COST)
- IMPROVE PRODUCTION EFFICIENCY (POWER/MASS FLOW)

APPROACH

- STUDY MOLECULAR PHOSPHORS/CONTAMINANT EFFECTS WITH MASS ANALYSIS (CALTECH)
- PERFORM DIRECT IMPLANTS WITHOUT MASS ANALYSIS (JPL)

Mass Spectrum From Solid Red Phosphorus Source

![Mass Spectrum Diagram](image-url)
I-V Characteristics

IMPLANT PARAMETERS:
DOSE: $1 \times 10^{15}$ P-ATOMS/cm$^2$
ENERGY: 10 KeV AT 10°
SPECIES: PHOSPHOROUS
(NO MASS ANALYSIS)
CELL SIZE: 2 cm x 2 cm x 12 mils
Effect of Implant Energy and Molecular Species on Power Output

![Graph showing the relationship between implant energy and power output. The graph includes data points for 'AMO-ILLUMINATION (140 mW/cm²)', 'CAMPUS DATA', 'JPL DATA', and 'PHOSPHOPOUS WITHOUT MASS ANALYSIS'. The x-axis represents implant energy in KeV/P-ATOM, and the y-axis represents current density at 400 mV in mA/cm². The graph includes symbols for different molecular species and dosages.]
Effect of Dose on Sheet Resistance

- JPL (CORRECTED) DATA (15 KeV)
- CAMPUS DATA (20 KeV/P-ATOM)
Effect of Dose on Power Output

- CAMPUS DATA - $P_2^+$ AT 40 KV (20 KeV/ P-ATOM)
- JPL (CORRECTED) DATA - RED PHOSPHOROUS SOURCE WITHOUT MASS ANALYSIS AT 15 KeV
- AMO ILLUMINATION (140 mW/cm²)

CURRENT DENSITY AT 400 mV, mA/cm²

DOSE, P-ATOMS/cm²
PRODUCTION PROCESS AND EQUIPMENT AREA

Results

• SOLAR CELL JUNCTIONS MADE WITH PHOSPHOROUS W/O MASS ANALYSIS

• NON-MASS-ANALYZED IMPLANT HAVE COMPARABLE PERFORMANCE

• POWER OUTPUT INSENSITIVE TO DOSE >2.5 (10^15) ATOMS/CM^2

• SMALL INCREASE IN POWER OUTPUT AT LOWER IMPLANT ENERGY

Conclusions

• ION IMPLANTED JUNCTIONS W/O MASS ANALYSIS IS FEASIBLE

• DOSE UNIFORMITY REQUIREMENTS MAY BE RELAXED ABOVE 2.5 (10^15) ATOMS/CM^2

• RELATIVELY LOW VOLTAGE IMPLANTS DESIRABLE < 5 KV

• ION THRUSTER/MILLING TECHNOLOGY USEABLE FOR CELL IMPLANTS
PRODUCTION PROCESS AND EQUIPMENT AREA

HIGH-RESOLUTION, LOW-COST CONTACT DEVELOPMENT (MIDFILM)

SPECTROLAB INC.
Alec Garcia

Program Tasks

I. Establish MIDFILM Process at Spectrolab

II. Fabrication of Modules

III. Environmental Test

IV. Alternate Materials
**PRODUCTION PROCESS AND EQUIPMENT AREA**

**Midfilm Process Sequence**

1. **SURFACE PREPARATION**
   - 30% NaOH

2. **JUNCTION FORMATION**
   - SPIN-ON DIFF. SOURCE

3. **PRINT & FIRE Al**

4. **CLEAN Al BACK**
   - HF + BRUSH CLEAN

5. **SPIN-ON RESIN**

6. **EXPOSE RESIN**

7. **APPLY SILVER**

8. **FIRE CONTACT**

9. **JUNCTION CLEAN**
   - LASER SCRIBE

10. **TEST**

11. **AR COAT**

12. **TEST**

*These steps are the MIDFILM photolithographic technique for producing front contacts.

**Exposure System:**

- **Mercury Vapor Lamp ~ 1000 Watts**

- **Collimating Lens**

- **10 Seconds Exposure**
PRODUCTION PROCESS AND EQUIPMENT AREA

Powder Firing Parameters

- **No Dry**

- **Pre-Fire at 575°C, 24"/Min., 18"**
  -- Remove Organics

- **Fire at 675°C, 36"/Min., 18"**
  -- Sinter Silver

24 in. per min., No AR Coating

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<td>9.7</td>
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<tr>
<td>35</td>
<td>600</td>
<td>661</td>
<td>570</td>
<td>10.2</td>
</tr>
<tr>
<td>28</td>
<td>598</td>
<td>660</td>
<td>581</td>
<td>10.4</td>
</tr>
</tbody>
</table>

Average 596 642.6 549.6 9.8

Standard Deviation 1.7 15.5 20.9

Yield: 23 of 25 - 92%
Soldering Results: 45° Pull Test

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Average Pull Strength</th>
<th>Notes</th>
</tr>
</thead>
<tbody>
<tr>
<td>1 Sec., 340°C</td>
<td>283 Grams</td>
<td>One Cell Tab Had No Strength</td>
</tr>
<tr>
<td>1 Sec., 370°C</td>
<td>643 Grams</td>
<td>All Cells at Least 500 Grams</td>
</tr>
<tr>
<td>1 Sec., 400°C</td>
<td>531 Grams</td>
<td>All Cells at Least 375 Grams</td>
</tr>
</tbody>
</table>

5 Cells Were Tested in Each Group.
NEW SOURCE OF ELECTRONIC PASTES IDENTIFIED. SOLAR CELL EXPERIMENT COMPLETED AND ANALYZED. ANALYSIS INDICATES SOME POTENTIAL SOURCES OF PROBLEM. FRONT CONTACT EXPERIMENT UNSUCCESSFUL DUE TO ADHESION PROBLEMS OF RECENT PASTE BATCHES.

MACROSCOPIC COMPARISON OF SUCCESSFUL AND UNSUCCESSFUL BATCHES OF S080. THE FIRED PRINT (LEFT) SPONTANEOUSLY SEPARATED FROM THE SOLAR CELL. DARK BROWN APPEARANCE IS PROBABLY DUE TO OXIDATION DURING REMOVAL FROM FURNACE TUBE WHILE PASSING THROUGH FLAME CURTAIN. THE FRAGMENT LABELED CONTROL TO THE RIGHT IS BRIGHT COPPERY IN APPEARANCE, HAS GOOD ADHERENCE AND ELECTRICAL CHARACTERISTICS.
Optical micrographs of S080 successful and S079 unsuccessful screened prints with experimental copper pastes.

Left side, top: Silicon substrate under good S080 print (electrode removed by etching in concentrated nitric acid).
Bottom: Silicon substrate of S079 print (electrode peeled spontaneously).
Right side, top: S080 successful electrode print.
Bottom: S079 unsuccessful electrode print.

Magnification 400x
SEM MICROGRAPHS OF SO80, UNSUCCESSFUL ELECTRODING EXPERIMENT.
LEFT SIDE: SUBSTRATE. RIGHT SIDE: ELECTRODE.
Energy dispersive xray spectrum of original S080 screened print with log ordinate
ENERGY DISPERSIVE XRAY SPECTRUM OF RECENT ATTEMPT TO REPRODUCE S080 (LINEAR ORDINATE)
ENERGY DISPERSIVE XRAY SPECTRUM OF SILICON SUBSTRATE FROM WHICH UNSUCCESSFUL S080 ELECTRODE WAS REMOVED BY PEELING (LINEAR ORDINATE)
Energy dispersive x-ray spectrum of S079 screened print with log ordinate
Conclusions and Problems

1. Paste manufacture of experimental pastes reinitiated.

2. Special analysis shows essential compositional components but potentially inadequate SiO₂ removal by decomposing silver fluoride.

3. Inadequate adhesion of previously manufactured pastes prevented electrical evaluation of front contact experiments.

4. Escalating cost of silver fluoride (AgF) makes substitute scavenging agent desirable.
AUTOMATED SOLAR MODULE ASSEMBLY (ASMA)

TRACOR MBASSOCIATES

1. PHASE ONE — IMPROVE EXISTING LAYUP AND INTERCONNECT SYSTEM. PROGRESS SINCE LAST PIM:

- PHASE COMPLETED AS PER CONTRACTUAL REQUIREMENTS
- PREPARATION CYCLE TIME REDUCED 40% (15 Sec to 8½ Sec)
- MANIFOLD TYPE DISPENSER FOR IMPROVED SOLDER PASTE DISPENSING
- IMPROVE LAYDOWN ACCURACY TO ROBOT MAXIMUM (± 0.050"")
- SOLDERING TIME REDUCED ON ORDER OF MAGNITUDE (30 Sec to 3 Sec)
- NEW SOLDER TECHNIQUE TO ELIMINATE SOLDER AND FLUX SMEAR
- SYSTEM INSTALLED IN NEW ENCLOSURE
II. PHASE THREE — AUTOMATED MODULE ENCAPSULATION.

PROGRESS SINCE LAST PIM:

- DETAILED LAYOUT DRAWINGS COMPLETED
- FRAME FABRICATED
- COMPONENT DRAWINGS 75% COMPLETE
- COMPONENT FABRICATION 50% COMPLETE
- COMPONENT ASSEMBLY (ONTO FRAME) 30% COMPLETE
IN-HOUSE ROBOTICS

JET PROPULSION LABORATORY

R. Cunningham
E. Saund
D. Varney
C. Ruoff

Objective

APPLICATION OF ADVANCED ROBOTICS
AND MACHINE PERCEPTION TECHNIQUES
TO SOLAR CELL MODULE PRODUCTION.

Plan

- AUTOMATION EVALUATION STUDY TO IDENTIFY POTENTIAL APPLICATIONS
  OF MACHINE INTELLIGENCE
  - INITIAL STRAWMAN BASED ON 1978 JPL PROCESS SEQUENCE
  - MEPSDU BASED STRAWMEN (IN PROCESS)
  - LAB DEMONSTRATION OF SELECTED DEVELOPMENT TASK(S)

Automation Issues

- WHAT IS THE PROCESS SEQUENCE?
- CONTINUOUS VS. BATCH PROCESSING
- INTER-STEP TRANSFER
- BUFFERING
- MODULE FABRICATION
- INSPECTION AND TESTING FOR QUALITY CONTROL FEEDBACK
- PROCESS CONTROL
- COMPUTERIZATION
PRODUCTION PROCESS AND EQUIPMENT AREA

Process Sequence

• THE MEPSDU PROPOSALS FROM SOLAREX AND WESTINGHOUSE ARE CURRENTLY BEING EVALUATED
• A PRODUCTION STRAWMAN WILL BE PROPOSED FOR EACH MEPSDU

Continuous vs Batch Processing

CONTINUOUS

• CONVEYOR BELT OPERATIONS
  FURNACES, SPRAY-ON COATINGS, DIFFUSION, SILK SCREEN
• K & S CELL STRINGING MACHINE
• CELL TEST
• LASER SCRIBING

BATCH

• DIP COATING
• CLEANING/ETCHING
• METAL PLATING

Interstep Transfer

• BETWEEN FIXTURES (CASSETTES, ETC.)
• CELL ORIENTATION
• INVERTING CELLS
• CONVERGENT/DIVERGENT PROCESSES
PRODUCTION PROCESS AND EQUIPMENT AREA

Buffering

- LINE BALANCING
- MACHINE DOWN TIME
- MORE FLEXIBLE WHEN DONE ON INDIVIDUAL CELL BASIS

Inspection and Testing

- INSPECTION FOR BROKEN CELLS
- VERIFICATION THAT CELL IS PRESENT
- ELECTRICAL TESTS
- CELL ORIENTATION

Process Control

- MAINTAIN PROCESS PARAMETER SUCH AS CHEMICAL CONCENTRATIONS, TEMPERATURE, AND PROCESSING TIME
- COULD POSSIBLY ADJUST ONE PARAMETER ON THE BASIS OF DEVIATIONS OF ONE OF THE OTHERS
- STATUS MONITORED BY CENTRAL COMPUTER

Computerization

- DISTRIBUTION OF CONTROL
- INTER-STEP COMMUNICATION
- HUMAN INTERFACE
Candidate Development Tasks

1. CELL HANDLING
   - INTERSTEP TRANSFER
   - BUFFERING
   - INSPECTION

2. MODULE FABRICATION
   - BUS BARS
   - PARALLEL INTERCONNECTIONS
   - BYPASS DIODES
   - TERMINALS

Development Task Selection Considerations

- SHOW COST BENEFIT USING SAMICS METHODOLOGY
- ALTHOUGH A PUMA ROBOT WILL BE USED FOR DEMONSTRATION PURPOSES, IT IS RECOGNIZED THAT A SOMEWHAT SIMPLER DEVICE MAY ALSO BE SUITED TO THE TASK.
Westinghouse Process Sequence

1. PRE-DIFFUSION CLEAN - PLASMA ETCH
2. POCl₃ DIFFUSION - DIFFUSION FURNACE
3. OXIDE ETCH
4. BSF FORMATION - PLASMA SPRAY, DRIVE FURNACE
5. AR COATING - DIP TANKS, FURNACES
6. PHOTORESIST COATING - DIP TANKS, FURNACES
7. EXPOSE/DEVELOP/ETCH - LIGHT SOURCE, DIP TANKS
8. METALLIZATION - BOX COATER
9. REJECTION/PLATING - PLATING LINE
10. CELL SEPARATION - LASER Scribe
11. CELL TEST
12. INTERCONNECT - ULTRASONIC WELDER
13. LAMINATION/ASSEMBLY
14. MODULE TEST
PRODUCTION PROCESS AND EQUIPMENT AREA

Solarex Process Sequence

1. SURFACE PREPARATION - NaOH ETCH
2. FRONT JUNCTION FORMATION - SPRAY-ON DOPANT, BELT DIFFUSION
3. BACK JUNCTION FORMATION - Al PASTE, BELT FIRE
4. AR COATING - SPRAY-ON, BELT DRY
5. METALLIZATION - NEGATIVE SCREEN PRINT, ELECTROLESS Ni PLATE, SOLDER DIP
6. EDGING - LASER SCRIBE
7. CELL TEST
8. TAB AND STRING - SOLDER CONTACTS
9. ENCAPSULATE MODULE
10. MODULE TEST

Computer Vision Demonstration

- INSPECTION AND VERIFICATION IN THE CONTEXT OF A SIMULATED CELL STRINGING OPERATION
- ESTIMATE POSITION ERRORS
- CORRECTLY IDENTIFY SITUATIONS WHERE TWO OR THREE CELLS OVERLAP
- DETECT BROKEN CELLS, MISSING CELLS

Other Applications

- INTERSTEP TRANSFER
  - MISSING CELLS
  - BROKEN CELLS
- CONVEYOR BELTS
  - OVERLAPPING CELLS
- LASER SCRIBING
  - BROKEN CELLS
  - VERIFY SIZE
PRODUCTION PROCESS AND EQUIPMENT AREA

**Vision System Features**

- Adapts to changes in the absolute location of the task
- Absolute cell position is determined to avoid propagation of errors
- Easily programmed to handle different cell sizes and layup patterns

**Improvements**

- Increased image resolution
- Hardware image feature extraction for increased speed
- Extend image analysis to handle interconnects
- Modify to handle different cell shapes
PRODUCTION PROCESS AND EQUIPMENT AREA

PROCESSING EXPERIMENTS ON
NON-CZOCHRALSKI SI SHEET

MOTOROLA, INC.

Major Areas of Investigation

1. PROCESS TECHNOLOGY
   SUBSTRATE SURFACE PREPARATION
   SURFACE ETCHING
   SURFACE TEXTURING
   SURFACE CLEANING
   PROCESS UNIFORMITY CONSIDERATIONS
   HANDLING RECTANGULAR SHAPES

2. CELL DESIGN
   METALLIZATION PATTERN OPTIMIZATION FOR RECTANGULAR CELLS

3. METALLIZATION
   PLATED METALLIZATION ADVANCEMENTS

4. COST ANALYSIS
   DOCUMENTATION OF MOTOROLA APPROACH AND COMPARISON WITH SAMIS

Process Technology: Baseline Process Sequence

1. BLANKET PHOSPHORUS DIFFUSION, PH₃ AT 900°C.
2. MESA JUNCTION ETCH, PHOTORESIST WITH A PLASMA ETCH FOR SILICON.
3. SILICON NITRIDE COAT, LPCVD Si₃N₄ AT 780°C.
4. OHMIC PATTERN, PLASMA ETCH NITRIDE.
5. METAL PLATE, NICKEL-COPPER OR PALLADIUM-NICKEL-COPPER.
Process Technology: Surface Preparation Experiment

1. DESIRED STRUCTURE: SIDE-BY-SIDE COMPARISON OF TEXTURED AND NON-TEXTURED (FRONT SURFACE) CELLS.

2. PROCEDURE: USE SILICON NITRIDE COATING TO MASK TEXTURED SURFACE PREPARATION ON ENTIRE BACK SIDE AND HALF OF FRONT SIDE (LENGTHWISE) FOR 10 RIBBON SAMPLES.

3. SOLAR CELL STRUCTURE: FORM PAIRS OF SIDE-BY-SIDE 1 cm BY 2 cm SOLAR CELLS, ONE CELL OF THE PAIR ON TEXTURED SIDE AND THE OTHER ON SMOOTH SIDE OF THE RIBBON. (USE BASELINE PROCESS.)

Substrates Used for Texture-Etch And Surface-Etch Studies

[Diagram showing textured and non-textured cells and substrates]
PRODUCTION PROCESS AND EQUIPMENT AREA

Process Technology: Surface Preparation Experiments

RESULTS

1. 10 RIBBONS PROCESSED, UP TO 11 CELL PAIRS PER RIBBON.

2. 48 PAIRS USED FOR ANALYSIS.

3. 32 PAIRS INDICATED IMPROVEMENT IN SHORT CIRCUIT CURRENT, \( I_{SC} \) WITH TEXTURING.
   AVERAGE \( I_{SC} \) INCREASE 2.1 mA OR 4.3%.

4. 15 PAIRS INDICATED DECREASE IN \( I_{SC} \) WITH TEXTURING.
   AVERAGE \( I_{SC} \) DECREASE 1.6 mA OR 3.2%.

5. TOTAL AVERAGE INCREASE WITH TEXTURING (FOR ALL 48) WAS 0.9 mA OR 1.9%.

Cell Design: Metal Pattern Optimization Procedure

EXPRESSION FOR EFFICIENCY:
\[
\eta = \eta^0 T (1 - F) - (P\Omega / P_i)
\]
\[
= \eta^0 T - \Delta \eta
\]

WHERE
\( \eta \) = OVERALL EFFICIENCY
\( \eta^0 \) = INHERENT SUBSTRATE CONVERSION EFFICIENCY
\( T \) = OPTICAL TRANSMISSION COEFFICIENT OF EXPOSED FRONT SURFACE
\( F \) = METAL SHADOWING FRACTION
\( P\Omega \) = OHMIC POWER LOSS
\( P_i \) = TOTAL INPUT POWER OVER USEFUL SPECTRUM

NOTE: \( \Delta \eta = \eta^0 T F + P\Omega / P_i \)
\[= \Delta \eta_{\text{SHADOW}} + \Delta \eta_{\text{OHMIC}} \]
PRODUCTION PROCESS AND EQUIPMENT AREA

CELL DESIGN - METAL PATTERN OPTIMIZATION PROCEDURE

NECESSARY OPTIMIZATION CONDITION

\[ \frac{\partial \Delta \eta}{\partial F} = 0 \]

HENCE \[ \frac{\partial \Delta \eta}{\partial F} \left( P \Omega \right) = -\eta_{T} \]

THIS CONDITION, ALONG WITH OTHER SPECIFIC CONSTRAINTS RELATED TO THE DESIRED CELL DESIGN, RESULTS IN EQUATIONS TO DETERMINE OPTIMUM LINE WIDTHS, SPACING, ETC.

Surface Current and Potential Distributions
At a Zone Element

Optimized Performance vs Line Width
(Spacing Variable) for 1 x 2-in. Cell With Side Buses
PRODUCTION PROCESS AND EQUIPMENT AREA

Performance vs Line Width
(Fixed Spacings) for 4-in.-Square Cell With 3 Buses

Metallization: Electroless Nickel Plating

FORMULA CURRENTLY BEING INVESTIGATED:

<table>
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<tr>
<th>REAGENT</th>
<th>CONCENTRATION</th>
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<tbody>
<tr>
<td>NICKEL SULFATE NiSO₄·6H₂O</td>
<td>25 g/l</td>
</tr>
<tr>
<td>SODIUM PYROPHOSPHATE Na₄P₂O₇·10H₂O</td>
<td>50 g/l</td>
</tr>
<tr>
<td>AMMONIUM HYDROXIDE 58% NH₄OH</td>
<td>66 ml/l</td>
</tr>
<tr>
<td>SODIUM HYPOPHOSPHITE NaH₂PO₂·H₂O</td>
<td>25 g/l</td>
</tr>
</tbody>
</table>

PRODUCTION PROCESS AND EQUIPMENT AREA

Cost Analysis: Motorola Costing Program

REQUIRED INPUT FILES:

1. PROCESS NAME FILE
2. CELL DIMENSION FILE
3. PROCESS DATA FILE
4. VARIABLE DATA

Cost Analysis: Input File Contents

1. PROCESS NAME FILE
   PROCESS NAME
   NUMBER OF PROCESS STEPS
   PROCESS SEQUENCE
   PROCESS CATEGORIES

2. CELL DIMENSION FILE
   DIMENSION IDENTIFYING NAME
   CELL AREA
   DIMENSION FILE NAME
   SILICON CONSUMPTION
### Cost Analysis - Input File Contents

#### 3. Process Data File
- **Process Yield (%)**
- **Machine Efficiency**
- **Machine Capacity**
- **Machine Cost**
- **Direct Labor**
- **Floor Space**
- **Electrical Power**
- **Ventilation**
- **De-Ionized Water**
- **Process Expenses**
- **Machine Expenses (Constant)**
- **Machine Expenses (Variable)**
- **Process Materials**
- **Facility Requirement Code**
- **Equipment Maintenance Personnel**

#### 4. Variable Data
- **Annual Production Volume (MW)**
- **Cell Efficiency (%)**
- **Solar Concentration (Suns)**
- **Silicon Cost ($/kg)**
- **Factory Life (Months)**
- **Interest Rate (%)**
- **Electrical Power Rate ($/kWh)**
- **Direct Labor Rate ($/Hour)**
- **Silicon Thickness (Microns)**
PRODUCTION PROCESS AND EQUIPMENT AREA

Motorola Costing Program

SIMPLIFIED BLOCK DIAGRAM OF MOTOROLA COSTING PROGRAM

START

PROCESS NAME FILE

CELL DIMENSION FILE

PROCESS DATA FILE

PROCESS DESCRIPTION FILE

SINGLE

ANALYSIS TYPE

SENSITIVITY

VARIABLE DATA FROM TERMINAL

VARIABLE DATA FROM FILE

COSTING CALCULATIONS

NO

ANALYSIS TYPE?

SENSITIVITY

SINGLE

END OF DATA

YES

STOP

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Organization of Design Guide

- **BACKGROUND** - Material to familiarize audience with basic physical concepts, goals and purposes of this Guide
- **SIMPLIFIED DESIGN TECHNIQUES** - To allow a design engineer to develop effective options and study trade-offs
- **EXAMPLES** - To illustrate the techniques presented
- **CONCLUSIONS AND REFERENCES** - For follow up in more detail on facts presented here

Acknowledgments

- Science Applications, Inc. appreciates the assistance of the low cost solar array project of the Jet Propulsion Laboratory, particularly Don Bickler and Paul Alexander of PPE and Ed Cuddihy of the encapsulation task.

- The design guide was prepared by C.N. Bain, Bruce Gordon, Bob Malinowski, and T. Michael Knasel (Project Manager) of SAI McLean, Virginia.
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CONCLUSIONS
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• GOALS OF DESIGN GUIDE
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**Contract Details**

**TITLE:** ANALYSIS OF COST-EFFECTIVE PHOTOVOLTAIC PANEL DESIGN CONCEPTS USING LIGHT TRAPPING

**SPONSOR:** JET PROPULSION LABORATORY

**CONTRACT NO:** 955787

**OBJECTIVES:**

1. DEVELOP OPTICAL DESIGN RULES FOR EFFICIENT USE OF LIGHT TRAPPING IN FLAT PANEL PHOTOVOLTAIC MODULES

2. PERFORM A COST BENEFIT STUDY OF OPTIMUM DESIGNS TO DETERMINE ECONOMIC VALUE OF LIGHT TRAPPING

**Goals of Design Guide**

**Taking the point of view that a photovoltaic module is a optical thick film - three dimensional optical system in which trapping of light can and does take place:**

- Develop graphical relationships between cell/module efficiencies and optical variables
- Variables shall include:
  - Cell spacing
  - Cover plate materials
  - Encapsulation thickness
  - Index of refraction of all optical materials
  - Reflectivity (angular pattern) of back layer
- Modeling effort shall address single and multiple trapping layers
- Simplified equations shall be developed as approximations to fully detailed calculations
- Pictorial displays and cross-sectioning of optical materials shall be used as appropriate

The design guide will enable the engineer to use light trapping effectively in PV panel design.
Definitions

- **Thin Film Optical Systems** - Two dimensional structures that reflect, refract or transmit light dependent on the wavelength and the optical properties of the materials - optical radiation goes forward or backward only.

- **Thick Film Optical Systems** - Three dimensional structures that reflect and transmit optical radiation forward or backward, with propagation possible transverse to layer structure.

- **Light Trapping** refers to propagation in thick films where light is trapped in high index materials by total internal reflection. Light is not normally trapped unless it is scattered in a diffuse (i.e., non-specular) manner.

Optical Principles

- Refraction, reflection in thick films
- Light Trapping concept
- Thick films for optical concentration
- Closed form approximate solution
- Computer modeling
- Simplified design equations
Refraction, Reflection in Thick Films

REFRACTION AND REFLECTION ARE THE PRINCIPAL OPTICAL INTERACTIONS IN THICK FILMS:

- **REFRACTION**: BENDING OF OBLIQUE RAYS AS THEY PASS FROM ONE MEDIUM TO ANOTHER HAVING A DIFFERENT REFRACTIVE INDEX

- **REFLECTION**: THE RETURN OF RADIATION BY A SURFACE WITHOUT CHANGE IN WAVELENGTH
  - **SPECULAR** - FROM A SMOOTH SURFACE
    - ANGLE OF INCIDENCE (θ₁) EQUAL ANGLE OF REFLECTION (θ₂)
  - **DIFFUSE** - FROM A ROUGH SURFACE
    - INTO MANY (SOMETIMES ALL) DIRECTIONS OF A HEMISPHERE

- MOST SURFACES CONTRIBUTE SPECULAR AND DIFFUSE COMPONENTS.

Thick Films as Optical Concentrators

THE ABILITY OF THICK FILMS TO PROPAGATE OPTICAL RADIATION IN A TRANSVERSE DIRECTION RAISES THE POSSIBILITY THAT OPTICAL CONCENTRATION (CALLED GAIN) CAN BE ACHIEVED. SUCH SYSTEMS WOULD HAVE THE FOLLOWING PROPERTIES:

- **MAXIMUM THEORETICAL GAIN FOR ANY RECEIVING ELEMENT WOULD BE LIMITED TO THE SQUARE OF THE RATIO OF INDICES, \( \left( \frac{n_{\text{HIGH}}}{n_{\text{LOW}}} \right)^2 \)**

- **MAXIMUM GAIN FOR AN ARRAY OF ELEMENTS THAT TRAP WOULD BE LIMITED TO THE RATIO OF THE TOTAL AREA TO AREA OF RECEIVER, \( \frac{A_{\text{TOTAL}}}{A_{\text{RCVR}}} \)**

- **THE GAIN WILL BE LIMITED ALSO BY THE ABSORPTION OF THE THICK FILM**
Light Trapping by Diffuse Reflection in Thick Film

Diffuse light trapping is accomplished when an incident ray enters a higher index transparent layer and is scattered.

An example related to photovoltaic modules is shown below:
Closed-Form Approximate Solution

**ASSUMPTIONS:**
- Single trapping layer, index \( n_2 \), placed in air, index \( n_1 \).
- No absorption in layer.
- No Fresnel reflections.
- Homogeneous mixture of diffusing layer and cells.
- Perfect diffuse (Lambertian) reflection between cells.

**METHOD—SERIES SOLUTION TO RAY PROPAGATION**

\[
G_0(N_1) = \frac{1}{(C+L-LC)}
\]

\[
N_1 = \frac{n_2}{n_1}
\]

\( C \) = Cell packing factor.

\( L \) = Loss due to less than critical angle reflection.

\[
L = \sin^2 \theta = \left( \frac{n_2}{n_1} \right)^2 = (N_1)^2
\]

For the case where the packing factor is small, the expression reaches the optical limit for gain.

\[
G_0(N_1) = \frac{1}{(N_1)^2} \quad C \to 0
\]

\[
= (\frac{n_2}{n_1})^2
\]

**Derivation of Closed-Form Solution**

\[
G = \left[ 1 + \frac{(1-C)(1-L) + (1-C)^2(1-L)^2 \cdot \cdot \cdot}{1-C-L+LC} \right]
\]

\[
G = \sum_{n=0}^{\infty} (1-C-L+LC)^n = \sum_{n=0}^{\infty} x^n = \frac{1}{1-x} \quad C+L-LC
\]

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Simplified Design Equations

1) GAIN WITH NO FRESNEL REFLECTIONS
\[ G_0 = \frac{1}{C+L-LC} \]

2) GAIN WITH FRESNEL REFLECTION AT TOP LAYER
\[ G_0 = \frac{1}{C+L-LC-LF+LCF} \]

3) GAIN WITH FINITE REFLECTIVITY \( R \leq 1.0 \)
\[ G(R) = \frac{1}{1-R(1-C-L+LC+LF-LCF)} \]

4) GAIN FOR LESS THAN OPTIMUM THICKNESS \( T/A < 0.3 \)
\[ G(T) = 1 + \left[ G_0 - 1 \right] \left( 1-(1-3.33/tA)^3 \right) \]

5) EFFECTS OF ADDITIONAL LAYERS ARE MULTIPLICATIVE
\[ G(N_1, N_2, \ldots) = 1 + G(N_1) G(N_2) \ldots - 1 \]

6) EFFECTS OF \( R, T \) CAN BE ALSO INCLUDED
\[ G(N_1, N_2, \ldots, R_1, \ldots, T_1, \ldots) = 1 + G(N_1, R_1, T_1) G(N_2, R_2, T_2) \ldots - 1 \]

Computer Model for Simulation of Light Propagation And Diffusion by Monte Carlo Methods

In order to check the closed form solution and to provide more design detail a computer code was written with these features:

- Propagation of light in three dimensions includes Fresnel losses, absorption losses, and diffusion losses.
- Diffused rays given angles which effectively sample the real distribution of diffused light - a Monte Carlo technique is used.
- Various diffusion patterns including Lambertian distribution are available as input.
- A twenty by twenty box matrix is used to define cell and diffusing areas.

The accurate computer predictions were then compared to the closed form solutions.
Closed-Form Equation vs Computer Calculation Comparison Format

LABELS
- CELL DIAMETER (INCHES)
  OR SIDE IF SQUARE
- REFLECTIVITY OF WHITE DIFFUSING LAYER, R
- TOTAL THICKNESS ABOVE CELL, T
- INDEX OF REFRACTION ABOVE CELL, N

AXES
- Y AXIS, GAIN ON CELL, G
- X AXIS, PACKING FACTOR, PF

LINE
- CLOSED FORM EQUATION
- POINTS, MONTE-CARLO MEAN (X) AND ERROR (BAR)

Closed-Form Equation vs Computer Calculation
PRODUCTION PROCESS AND EQUIPMENT AREA

4 INCH CELLS  P = 0.85  T = 0.5  N = 1.5

GAIN

4 INCH CELLS  P = 0.85  T = 0.125  N = 1.5

GAIN

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PRODUCTION PROCESS AND EQUIPMENT AREA

GAIN

1 INCH CELLS  P=0.85  T=0.25  N=1.5

GAIN

1 INCH CELLS  P=0.85  T=0.25  N=1.5

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PRODUCTION PROCESS AND EQUIPMENT AREA

Baseline Module Design

- MODULE LAYOUT, CELL SPACING GEOMETRY
- BASELINE PERFORMANCE ESTIMATES
- EXPERIMENTAL CONFIRMATION

Light-Trapping Concentration for PV: Concept Description

- Light trapped by diffuse back reflection from the region between cells can contribute to system performance.
- System trade-off is between cell spacing, cover thickness, and index of refraction.
- Light trapping works over the entire hemisphere, thus providing concentration of solar diffuse radiation as well as direct.

Module Layout; Cell-Spacing Geometry
PRODUCTION PROCESS AND EQUIPMENT AREA

Definition of Layers in Baseline Module Cross Section*

<table>
<thead>
<tr>
<th>OPTICALLY IMPORTANT MODULE LAYERS FROM SUN SIDE DOWN</th>
<th>PREFERRED MATERIAL CHOICES AND NOMINAL THICKNESS</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>LAMINATION</td>
</tr>
<tr>
<td></td>
<td>CASTING</td>
</tr>
</tbody>
</table>

SUPERSTRATE DESIGN:

| TOP COVER                                      | LOW IRON, TEMPERED SODA-LIME GLASS, 125 MIL MINIMUM |
| POTTANT                                         | ETHYLENE VINYL ACETATE (EVA) OR ETHYLENE METHYLACRYLATE (EMA), 5 MIL MINIMUM |
| SPACER                                          | NON-WOVEN GLASS MAT TO ACHIEVE MINIMUM POTTANT THICKNESS - CRANEGLAS |

SUBSTRATE DESIGN:

| TOP COVER                                      | BIAXILALLY ORIENTED POLYMETHYLACRYLATE (PMMA) OR TEDLAR, 3 MIL |
| POTTANT                                        | NONE REQUIRED ON SUN SIDE |

FOR EITHER MODULE:

| CELLS                                           | FOUR INCH ROUND OR FOUR BY ONE INCH RECTANGULAR, PACKING FACTOR 0.6 TO 0.85 |

*SOURCE: JPL LETTER TO SAI OCTOBER 1, 1980.

Variation in Module Thickness

- The thickness of a photovoltaic module is a function of module size, materials used, wind and environmental loads on the module and the array structure.

- In modules where the encapsulating materials provide most of the module strength, superstrate layer thicknesses may increase optical performance and strength.

- In light trapping PV modules, the important design parameters are:
  - material index and transmission
  - length of transmission paths
  - number of reflections, energy absorbed
  - trapping layer material heat capacitance

- Material(s), thickness of trapping layer(s), cell size and PF can be controlled to maximize gain, or to minimize module cost per watt.

- These parameters and costs can be traded off against land, structure, and operation and maintenance costs to minimize system cost per watt.
PRODUCTION PROCESS AND EQUIPMENT AREA

Experimental Confirmation

Design Rules

- VARIATION IN MODULE THICKNESS/MATERIAL INDEX OF REFRACTION

- TRAPPING GAIN AS A FUNCTION OF PACKING FACTOR AND LAYER THICKNESS
Design Equations for Various Indexes of Encapsulant, Thickness and Packing Factor

PRODUCTION PROCESS AND EQUIPMENT AREA
PRODUCTION PROCESS AND EQUIPMENT AREA

Typical Gains for Block III Modules Using Simplified Design Equations

<table>
<thead>
<tr>
<th>SUPPLIER</th>
<th>AS CONFIGURED</th>
<th>WITH r = 1/2&quot;</th>
</tr>
</thead>
<tbody>
<tr>
<td>ARCO</td>
<td>1.08</td>
<td>1.17</td>
</tr>
<tr>
<td>MOTOROLA</td>
<td>1.10</td>
<td>1.20</td>
</tr>
<tr>
<td>SENSOR TECHNOLOGY</td>
<td>1.12</td>
<td>1.24</td>
</tr>
<tr>
<td>SOLAR POWER</td>
<td>1.06</td>
<td>1.13</td>
</tr>
<tr>
<td>SOLAREX</td>
<td>1.13</td>
<td>1.26</td>
</tr>
</tbody>
</table>

Module Design

- MODIFICATIONS FOR LIGHT TRAPPING
- MAXIMIZING GAIN IN A DENSELY PACKED MODULE
- MULTIPLE LAYERS
- INTER-CELL/INTRA-CELL TRAPPING

Maximizing Gain in Densely Packed Module

These steps will produce an optically efficient PV module:

- AR COATING
- ADD DIFFUSE REFLECTOR
- OPTIMIZE SUPERSTRATE THICKNESS BASED ON CELL SIZE
- UTILIZE TWO OR MORE TRAPPING LAYERS
- USE DIFFUSING LAYER ON CELL GRIDS
- ADD REFLECTORS TO SUPER- AND SUB-STRATE EDGES
- OPTIMIZE LOAD
Production Process and Equipment Area

Modifications for Light Trapping

Design Options to be Considered

<table>
<thead>
<tr>
<th>MATRIX OF STUDY CASES</th>
<th>PANEL PERFORMANCE IMPROVEMENT DUE TO TRAPPING FROM</th>
</tr>
</thead>
<tbody>
<tr>
<td>COMPLEXITY OF TRAPPING LAYER</td>
<td>INTER-CELL REGION</td>
</tr>
<tr>
<td>Single Layer</td>
<td>(BASELINE CASE)</td>
</tr>
<tr>
<td>• Existing Design</td>
<td>Use Commercial Module Design</td>
</tr>
<tr>
<td>• Optimal Design</td>
<td>Design is a function of time as cell costs decline with time</td>
</tr>
<tr>
<td>Multiple Layers</td>
<td>Use Commercial Module Design</td>
</tr>
<tr>
<td>• Existing Design</td>
<td>Design is a function of time as cell costs decline with time</td>
</tr>
<tr>
<td>• Optimal Design</td>
<td></td>
</tr>
</tbody>
</table>

Intercell-Intracell Trapping

- **Intercell Trapping** traps light by diffuse back reflection from the regions between cells.

- **Intracell Trapping** uses a diffusing layer on the cell grid itself to recover a large part of grid blockage losses.

- In both cases light trapping works over the entire hemisphere thus providing concentration of the sky diffused component of solar radiation.

System Concepts That Exploit Light Trapping

- **GROWTH SYSTEM**

- **WALL INTEGRATED SYSTEMS**
Growth System

- Designing a photovoltaic system to allow for the optimum packing factor with today's prices, can also allow a more effective system when the DOE cost goals are met or exceeded, since the inflation sensitive material and labor items are produced early.

**Economic Model**

**Required Area of Solar Cells**

\[ A_s = \frac{P_{out}}{\eta 16} \]

**Required Total Area**

\[ A_T = \frac{A_s}{P.F.} \]

**Total Cost**

\[ C_T = A_s C_s + A_T (C_c + C_f + C_L) \]

Cost/m² of:
- Solar Cells
- Trapping Structure
- Land

\[ C_T = \frac{P_{out}}{\eta 16} \left[ C_s + \frac{1}{P.F.} (C_c + C_f + C_L) \right] \]
Example: 1980 Cell Prices, Three Encapsulant Thickness

PRODUCTION PROCESS AND EQUIPMENT AREA

FALL IN CIRCULAR CELLS

SYstem COST ($/kW)

PACKING FACTOR

1/1
1/8
1/2
1/4
Future Prospect

- GOALS OF COST/BENEFIT STUDY
- INFORMATION NEEDED

Goals of Cost-Benefit Study

As a follow-up to the design guide a cost/benefit study was performed:

- Uses simplified design equation for PV module performance.
- Simplified costing equations to relate cost of cells, encapsulant, array structures and land at a constant power level, were developed.
- The goal is to determine the optimum cost/benefit point for optical design of photovoltaic panels.
Information Required

IN ORDER TO PERFORM THE COST/BENEFIT STUDY THE FOLLOWING DATA IS REQUIRED:

- **MODULE**
  - OPTICAL MATERIALS, INDEX, ABSORPTION,
  - VOLUMETRIC COST OF MATERIALS, COST OF LABOR FOR MANUFACTURER
  - COST OF CELLS, AND EFFICIENCY

- **ARRAY**
  - AREA RELATED COST OF ARRAY STRUCTURE,
  - COST OF LAND

PROCEDURE IS TO TRADE-OFF PACKING FACTOR, AND/OR MODULE THICKNESS VERSUS COST FOR THE SAME LEVEL OF DELIVERED ELECTRICAL POWER.

Conclusions

- OPTICAL DESIGNS OF PV PANELS USING LIGHT TRAPPING INTRODUCE A HOST OF NEW PARAMETERS THAT MUST BE CONSIDERED IN PV MODULE DESIGN AND NEW RESEARCH AND DEVELOPMENT AVENUES THAT PROMISE TO PROVIDE EARLY DIVIDENDS.

- LIGHT TRAPPING CAN BE USED TO:
  - IMPROVE EFFICIENCY IN STANDARD PV MODULES
  - OPTIMIZE PV MODULE DESIGNS BASED ON COST USING CURRENT AND PROJECTED MATERIAL, LABOR, MONEY AND REAL ESTATE
  - IMPROVE THE EFFICIENCY OF SOLAR SYSTEMS ARCHITECTURALLY INTEGRATED INTO BUILDINGS TO PROVIDE PV ELECTRIC POWER GENERATION, SPACE HEATING AND DIFFUSE LIGHTING.

- LIGHT TRAPPING PV MODULES USING TRAPPING LAYERS MADE OF CURRENTLY AVAILABLE MATERIALS IS ALREADY A VIABLE PROPOSITION. THE DEVELOPMENT OF HIGHER INDEX MATERIALS CAN IMPROVE THIS SITUATION EVEN AS CELL COSTS DECLINE.
PRODUCTION PROCESS AND EQUIPMENT AREA

Design Method

- Familiarization with concepts - examples
- Obtain data on materials: optical properties and costs to augment data on module
- Use design nomographs or simplified design equation to obtain gain as a function of packing factor and thickness of encapsulant above cell
- Use costing nomograph or simplified costing equations to determine gain for various packing factor and thickness values, find a cost minimum
- Estimate cost savings obtained at minimum and compare with standard design
- Repeat with other material choices

Recommended Applications

Based on this study it is recommended that designers consider light trapping designs in situations where

- Round cells (full or partial) are to be utilized
- Silicon is costly and/or in short supply
- Cells are roof and/or wall integrated (residential)
- Module thickness is important - (hail areas is an example)
- Rapid power requirement growth is anticipated at site
- Thin or sharp shadows fall on array
- Array area costs are low
References


2. UNITED STATES PATENT NO. 4,162,928, "SOLAR CELL MODULE", NEAL F. SHEPARD, JR., JULY 31, 1979, (ASSIGNED TO NASA).


6. UNITED STATES PATENT APPLICATION "FIXED SOLAR ENERGY CONCENTRATOR" (ASSIGNED TO Science Applications, Inc.).
Design Rules for Front Metallization
Of Large-Area Solar Cells

1. Observe: Careless metallization design is costly.

2. Select conductor metal of the highest practical conductivity.

3. Select deposition processes which approach bulk conductivity as closely as practical.

4. Each higher level in the hierarchy of conductors needs a much lower sheet resistance than the preceding level. This leads to the "sky scraper rule" for the bus lines: Build high rather than wide.

5. If the bus lines cannot have a sheet resistance small compared to the grid lines, omit the bus lines. Proceed directly to 10.

6. Select the bus line spacing, for bus lines of round wire, according to:

   \[ 2W = \left( \frac{3}{\pi^2} \frac{n_{BL}}{R_{sh, GL}} \frac{2}{3} \frac{v_{mp}}{j_{mp}} \right)^{1/8} L_1^{1/2} \]

7. Select bus line wire diameter according to:

   \[ T_{BL} = \left( \frac{32}{3\pi} \frac{|j_{mp}| n_{BL}}{v_{mp}} L_1^2 W^2 \right)^{1/3} \]

8. For rectangular bus wires of height-to-width ratio \( k \), multiply each \( \pi \) by \( 4k/\pi \).
PRODUCTION PROCESS AND EQUIPMENT AREA

9. For bus lines of constant sheet resistance \( R_{sh, BL} \) rather than thickness directly proportional to width, as in round or rectangular wires, the relationship:

\[
\frac{T_{BL}}{2W} = L_1 \left( \frac{|j_{mp}|}{3 V_{mp}} R_{sh, BL} \right) \frac{1}{2}
\]

applies, instead of 6.) and 7.). Choose \( W \) then as small as practical, considering 13.) and 14.).

10. Arrange grid lines normal to bus lines, and parallel to each other.

11. Select grid line width as small as practical, commensurate with acceptable production costs and yields and solar cell value differences resulting from the consequent efficiency differences.

12. Select grid line spacing \( S \) according to:

\[
S = \left( \frac{6 V_{mp} T_{GL}}{|j_{mp}| R_{sh, FL}} \right)^{1/3} - \frac{2}{3} \frac{R_{sh, GL} \delta_{GL} W^2}{R_{sh, FL} T_{GL}}
\]

13. Check that

\[
\frac{T_{GL}}{S} = \left( \frac{1}{3} R_{sh, GL} \delta_{GL} \frac{|j_{mp}|}{V_{mp}} \right)^{1/2} W
\]

14. Check that

\[
S \leq 2 \cdot \left[ \left( \frac{R_{sh, GL} \delta_{GL}}{R_{sh, FL}} \right)^{1/2} \left( \frac{3 V_{mp}}{|j_{mp}|} \right)^{1/2} W \right]^{1/2}
\]

15. If checks 13.) and 14.) are negative, select \( S \) as small as possible in view of 11.), but not significantly larger than given by 14.). If \( T_{GL}/S \) is large compared to right hand side of 13.), use the smallest practical value for \( T_{GL} \), if pattern resolution is limiting. If grid line width-to-thickness ratio is limiting, reduce thickness (increase \( R_{sh, GL} \)), to find \( T_{GL} \) and \( R_{sh, GL} \) values for least power loss.

16. The "shape factor" \( \delta \) varies from 0.75 for fully tapered grid lines to unity for uniform width lines of equal shading.
PRODUCTION PROCESS AND EQUIPMENT AREA

Back Metallization

3 LAYERS IN PARALLEL:

\[ R_{SH,P} = \frac{1 \text{ cm}}{2 \times 10^{-2} \text{ cm thick}} = 50 \ \Omega \]

\[ R_{SH,P+} = \frac{0.02 \text{ cm}}{2 \times 10^{-3} \text{ cm thick}} = 10 \ \Omega ; \quad n_A = 2 \times 10^{18} \text{ cm}^{-3} ; \]

\[ u_p = 160 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1} \]

\[ R_{SH,Cu} = \frac{1.7 \times 10^{-6} \text{ cm}}{1 \times 10^{-4} \text{ cm thick}} = 1.7 \times 10^{-2} \ \Omega \]

COMPOSITE SHEET RESISTANCE:

\[ R_{SH,COMP} = R_{SH,P} \cdot R_{SH,P+} \cdot R_{SH,Cu} \]

\[ = \frac{50 \times 10^{-2} \cdot 1.7 \times 10^{-2}}{1.7 \times 10^{-1} + 8.5 \times 10^{-1} + 50 \times 10^{-2}} = 1.7 \times 10^{-2} \ (\text{0.2\%}) \]

CONCLUSIONS:

1. Metal dominates sheet flow, even in 0.1 \text{ cm thickness.}
2. Current flow through semiconducting base (P and P+) is normal.
3. Bus wires on back permit layer-metal savings for equal performance. (Important for TF AG with Cu bus wires.)

GENERAL:

4. Grid structure on back does not provide metal saving, requires proportionally greater thickness for equal performance.
Optimization Constraints

1. Where sheet resistance (or conductor thickness) is fixed, an optimization of individual dimensions is not possible. Optimum would be spacing \( \cdot 0 \). However, the shading ratios \( \frac{t_{GL}}{S} \) and \( \frac{t_{BL}}{2W} \) can be optimized. (Design Rules 9 and 13.)

2. Where conductor thickness is proportional to width, individual dimensions can be optimized. (Design Rules 6 and 7.)

3. When technological constraints determine the line width, an optimum spacing can be determined. (Design Rule 12.)

4. Reducing line spacing, while keeping the line width to spacing ratio constant, reduces the voltage drop in the next lower level of conductor \( (V_{FL} \cdot 0, \text{ when } S \cdot 0) \). However, it does not make sense to reduce the spacing further, when the next lower level voltage drop is already negligible compared to the higher level conductor voltage drop and shading loss. (Design Rules 14 and 15.)
PRODUCTION PROCESS AND EQUIPMENT AREA

Tapered Grid Lines

\[ V(W) = \frac{R_{MH} S h^2}{2 TGL} \cdot G(f) ; \]
\[ P = J_{MP} S W V_{EFF}(f) ; \]
\[ V_{EFF} = V(W) \cdot \frac{1}{2} \cdot H(f) ; \]

\[ S = \text{CLEAR SPACING BETWEEN GRID LINES} \]

<table>
<thead>
<tr>
<th>Width</th>
<th>( f )</th>
<th>( G(f) )</th>
<th>( V_{EFF} )</th>
</tr>
</thead>
<tbody>
<tr>
<td>Uniform Width</td>
<td>( 1 )</td>
<td>( 1 )</td>
<td>( \frac{2}{3} V(W) )</td>
</tr>
<tr>
<td>Fully Tapered</td>
<td>( 0 )</td>
<td>( 1 )</td>
<td>( \frac{1}{2} V(W) )</td>
</tr>
</tbody>
</table>

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Oblique Grid Lines

\[ V_{\text{OBL}}(\alpha) = \frac{V_{\text{NORM}}(\alpha)}{\cos \alpha}; \]

- \( \alpha = 30^\circ : V_{\text{OBL}}(4) = 1.33 V_{\text{NORM}}(4) \);
- OR: \( T_{\text{GL,OBL}} = 1.33 T_{\text{GL,NORM}} \);

To obtain \( V_{\text{OBL}}(\alpha) = V_{\text{NORM}}(\alpha) \)

<table>
<thead>
<tr>
<th>( \alpha = 0^\circ )</th>
<th>( \alpha = 30^\circ )</th>
</tr>
</thead>
<tbody>
<tr>
<td>Grid Shading</td>
<td>0.3 cm²</td>
</tr>
<tr>
<td>Bus Shading</td>
<td>0.36 cm²</td>
</tr>
<tr>
<td>Add'l Connections</td>
<td>-</td>
</tr>
<tr>
<td>Total Shading</td>
<td>1.16 cm²</td>
</tr>
<tr>
<td>Rel. Power Loss</td>
<td>0</td>
</tr>
<tr>
<td>( \alpha )</td>
<td>0</td>
</tr>
</tbody>
</table>

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PRODUCTION PROCESS AND EQUIPMENT AREA

Hierarchy of Conductors: Decreasing Sheet Resistance

SEMI-CONDUCTING FRONT LAYER:
- \( R_{SH,FL} = 35 \, \Omega \)
- \( R_{SH,FL} = 1.7 \times 10^{-3} \, \Omega \)

GRID LINES (10 \, \mu m \, \text{THICK Cu}): \( R_{SH,GL} = 1.7 \times 10^{-3} \, \Omega \)

BUS LINES (30 Ga Cu wire, 0.255 \, \text{mm DIA.}): \( R_{SH,BL\, (\text{equiv.})} = 8.5 \times 10^{-5} \, \Omega \)

**IF \( R_{SH,BL} = R_{SH,GL} \): DO NOT USE BUS LINES!**

MINIMUM LOSS WITH GRID LINES ONLY, S-0, 10 cm x 10 cm CELL:
- \( P_{\text{FRONT}} = 11.7\% \)

EXAMPLES FOR 10 cm x 10 cm CELLS:

A.) 65 GRID LINES, 10 \, \mu m \, \text{THICK Cu}, 85 \, \mu m \, \text{WIDE}
- \( P_{\text{FRONT}} = 12.0\% \)

B.) 65 GRID LINES, 10 \, \mu m \, \text{THICK Cu}, 25 \, \mu m \, \text{WIDE}
7 BUS LINES, 10 \, \mu m \, \text{THICK Cu}, 750 \, \mu m \, \text{WIDE}
- \( P_{\text{FRONT}} = 12.1\% \)

C.) 65 GRID LINES, 10 \, \mu m \, \text{THICK Cu}, 25 \, \mu m \, \text{WIDE}
7 BUS LINES, 255 \, \text{\mu m DIA Cu WIRE}
- \( P_{\text{FRONT}} = 4.9\% \)

**Effect of Metal Mass on Cell and Its Price**

<table>
<thead>
<tr>
<th>METALLIZATION</th>
<th>GRID LINES</th>
<th>BUS LINES</th>
<th>BACK METAL</th>
<th>TOTAL</th>
<th>METAL COST</th>
<th>POWER LOSS</th>
</tr>
</thead>
<tbody>
<tr>
<td>OPTION</td>
<td>NO. ( n_G )</td>
<td>THICK MASS</td>
<td>NO. ( n_B )</td>
<td>THICK MASS</td>
<td>THICKNESS</td>
<td>MASS</td>
</tr>
<tr>
<td>TF Ag</td>
<td>40 ( 20 )</td>
<td>52.5</td>
<td>4 ( 20 )</td>
<td>10.6</td>
<td>0 ( 20 )</td>
<td>1060</td>
</tr>
<tr>
<td>TF Ag</td>
<td>65 ( DTO )</td>
<td>25</td>
<td>7 ( DTO )</td>
<td>324</td>
<td>0</td>
<td>990</td>
</tr>
<tr>
<td>BULK Cu</td>
<td>65 ( 10 )</td>
<td>146</td>
<td>7</td>
<td>324</td>
<td>0</td>
<td>990</td>
</tr>
</tbody>
</table>

1) PER 10 cm x 20 cm CELL
2) 50% OF VOLUME IS Ag
At the Wednesday-afternoon session of the PIM devoted to Block IV Module Production, contractors commented on the efficacy of that initiative by addressing design and performance requirements, environments, SAMICS-SAMIS, and general topics. Discussion was candid and, not surprisingly, there were both positive and negative comments on the contract content. A summary of these comments is given below.

Under the topic Design and Performance Requirements, these remarks stand out as subjects for consideration and concern:

1. Standardizing on a module terminal voltage is not necessary, and when coupled with dimensional constraints and the requirement to specify power at NOCT, becomes an important cost driver.

2. Redundant terminals serve no crucial purpose and raise the cost, but redundant interconnects are of significant value.

3. Efficiency was characterized both as being of critical importance and of secondary importance.

4. The need for shunt diode protection when arrays are used with maximum power tracking electronics in highly paralleled arrays was challenged. The case for diodes located external to the modules was advocated. The hot-spot endurance of modules should be verified (as planned for Block V).

5. The focus on residential and intermediate-load modules was said to be out of step with the market, which now is oriented toward remote applications.

6. The documentation required by JPL in support of a design program is unreasonable.

7. The quality assurance program demanded by JPL is too rigorous, given recent improvements in module yield and reliability. QA imposed is not what contractors use for commercial product line.
"Environmental Requirements" also elicited a wide range of comments:

1. Thermal and humidity testing was characterized both as valid and as inadequate. Recommendations were received both for more severe and less severity testing. Constant, longer-term humidity testing at lower temperature rather than cycling was suggested. Thermal cycling both before and after humidity testing was proposed. Less-severe thermal cycling but with increased number and rate of cycles was recommended.

2. Environmental design and testing should be site specific.

3. Tests such as hail and twist should be deleted when prior testing or analysis shows that design is satisfactory.

4. Wind loading should be a panel requirement, not a module requirement. That is, structural capability of modules should be evaluated as installed (rack or roof, as applicable).

5. Pass-fail should be determined on a performance basis, not on cosmetic criteria; a 5% performance degradation limit is too small.

6. In qualifying modules there is no need to run tests by both the contractor and JPL. Substantial costs to contractors for duplicate tests were identified.

7. Environmental testing is not a substitute for life testing.

8. Increased emphasis should be placed on reliability and durability requirement.

The use of SAMICS-SAMIS elicited considerable spirited discussion; comments ran the gamut from favorable to unfavorable, as follows:

1. Program is easy to use; program is difficult to use. The consensus was that it is difficult to use, particularly for new users who lack computer experience.

2. The high cost of running the program is a nearly universal objection.

3. Their usefulness is generally held to be dubious, primarily because of the imprecision of the Block IV input data, but there were also complaints that SAMIS overhead is too high and that some catalog prices are not correct.

4. Some contractors preferred to omit SAMIS (Solar Power) or do their own cost projection (Motorola).

5. Since the results can be manipulated, the program is valuable only in a relative sense; however, there was fairly good agreement between SAMIS results and prior contractor bids in several cases.
ENGINEERING AND OPERATIONS AREAS

In the area of general comments, the need for more rapid feedback from JPL was mentioned, and the desirability of having large prototype runs was also expressed.

In the open discussion that followed the contractors' presentations, cognizant JPL personnel responded to these comments. It is expected that some -- but not all -- of the recommendations can be incorporated in the Block V contracts.

In the Thursday-morning session, John Griffith, LSA Environmental Test Director, presented the results of comparative environmental testing of candidate foreign and domestic modules for water-pumping applications. The U.S. modules compared favorably with their foreign competitors. In exploratory testing of 11 modules in the proposed new Block V humidity-freeze cycle, this was seen to be more effective than the Block IV sequence in inducing corrosion, delamination, and some forms of power degradation.

Steve Forman of MIT-LL gave an update of applications experiments experience and a status report on residential experiments under development. Residential sites in the Northeast are nearing completion, and the Southwest Residential Experiment station (RES) is approaching the hardware phase. Array performance at the various MIT-LL sites continues to be excellent, with some concern about the increasing frequency of interconnect failures and discoloration of PVB-encapsulated cells.

Charles Cox of MIT-LL reported on their recently developed I-V meter for field use. The meter uses a capacitor-charging method of I-V curve tracing and is capable of handling high-power (multiple-module) measurements.

Steve Sollock and Alex Shuska of the JPL Failure Analysis Laboratory gave a joint presentation on module cell string shorts to ground. Sollock presented a historical overview that showed the problem to be prevalent and persistent, and he characterized the various types of shorts that have been encountered. Shuska detailed the causes of each type, and described the experimental tools available for analysis. It was concluded that the problems seen to date can be prevented through attention to design and workmanship.

R.G. Ross, Jr., Engineering Area manager, presented a summary of Engineering Area activities since the 16th PIM. Recently published reports by Engineering Area contractors include the Phase I report on Product Liability Assessment by Carnegie-Mellon University and the Third Annual Report of the Clemson University cell-reliability testing contract.

In the area of requirements development, two new module design and test specification drafts prepared by LSA Engineering were distributed to the PV industry for review and comment, along with a preliminary draft of a module and array safety requirements document, jointly developed by JPL and Underwriters Laboratories.

An industry workshop on module and array safety was conducted in conjunction with the 17th PIM on February 3, 1981.

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As part of the Array Subsystem Development activities, a design data package for the LSA-developed Low-Cost Array Structure was made available to industry participants.

Contract awards were made during this reporting period to General Electric Co. and the American Institute of Architects Research Corp. for integrated residential PV array development. In the area of Module Engineering and Reliability, reports were issued covering in-house soiling studies and the proceedings of the Cell Reliability Workshop that was sponsored jointly by JPL and Clemson University. A number of ongoing tasks were described briefly in the areas of requirement development, array subsystem development, module engineering and reliability studies, and standards activities. The status of a number of these activities was described in a technical session held jointly with the Operations Area.

Due to a schedule conflict, Dr. Weinstein of Carnegie-Mellon University was unable to present his discussion of Module Product Liability as planned during the joint session; however, participants in the Safety Workshop did hear his presentation covering methodology for assessment of product safety and liability.

A presentation by J. Oster and R. Rittelmann of Burt Hill Kosar Rittelmann Associates described the results of their study of commercial and industrial PV module and array requirements based on a review of building codes and regulations. Important findings were related to module sizing and modularity, material selection restrictions, and wiring and interconnection concerns, especially with regard to the National Electric Code.

A defect diagnosis approach to sizing terrestrial photovoltaic electrical insulation systems was presented by C. R. Mon. The approach consists of gathering quantitative data characterizing voltage breakdown statistics of thin insulating films. For a designated failure density the number of layers of film of a particular thickness can be selected. Typical flaws that can enhance the likelihood of breakdown were discussed and design procedures to minimize their effects presented.

The method realizes its full power when failure rate data is available. This technique was discussed and preliminary results were presented.

Clemson University offered a presentation covering exploratory testing of several different types of photovoltaic cells for the purpose of investigating possible correlation between cell electrical characteristic degradation and losses and/or removal of antireflective (AR) coating. The initial impetus to study this problem came from reports on field observations made by MIT-LL on modules taken from photovoltaic field application sites. When MIT-LL personnel learned of the availability of special equipment at Clemson University, i.e. an IBM 7400 Spectrophotometer, it was suggested to the JPL Engineering Area that quantitative tests using color spectrum analyses might provide useful reliability data.

From the tests performed, plots were generated of percentage decrease in electrical output vs percentage missing AR coating from the cell. The color-spectrum analysis data gathered was taken using strict controls on
ENGINEERING AND OPERATIONS AREAS

orientation and alignment, observation angle and spectral reflectance. Data derived from use of IBM 7400 spectral reflectance measurements included chromaticity tristimulus, etc.

Module hot-spot endurance test development was addressed in presentations prepared jointly by J. Arnett and C. Gonzales. Details of the new Block V Hot-Spot Endurance Test Procedure and its rationale for development were presented at the Safety Workshop on February 3. As a follow-up, specific testing results and preliminary design information were presented at the joint technology session.

In presentations by R. Whitaker and E. Zerlaut of DSET Laboratories, Phoenix, Arizona, the current status of two LSA Engineering Area contracts was described. The results of a total of $1.7 \times 10^6$ langley's of exposure of Block III Modules (approximately equivalent to 8.5 years of weathering) during the preceding 18 months was described along with examples of typical before-and-after I-V measurements. Completion of the computer software and instrument calibration for the DSET Scanning Spectroradiometer was reported along with sample solar spectral curves as part of the Natural Sunlight Measurements contract.
ENGINEERING AND OPERATIONS AREAS

BLOCK IV CONTRACTOR EXPERIENCE

APPLIED SOLAR ENERGY CORP.
Bill Sampson

Design and Performance Requirements

- REQUIRED OUTPUT VOLTAGE WITHIN A RANGE (15V-60V) NOT FIXED.
- REDUNDANT CIRCUIT THROUGHOUT NOT ONLY AT TERMINATION
- BYPASS DIODES EXTERNAL TO MODULE.
- MODULE INTERCHANGEABILITY SHOULD END WITH PHYSICAL DIMENSIONS ONLY NOT ELECTRICAL PERFORMANCE

Effect of Design Requirement

- FIXED VOLTAGE REQUIREMENT
  1. NONSTANDARD CELL SIZE (3.05" DIAMETER)
  2. LOWER PACKING FACTOR
  3. ADDITIONAL ENGINEERING TIME
  4. INCREASED COSTS

- FIXED ENVELOPE DIMENSIONS AND INCREMENTAL DIMENSION RESTRICTIONS
  1. LOWER PACKING FACTOR
  2. DETERMINED CELL SIZE AND QUANTITY
  3. DOES NOT FIT ANY COMMERCIAL OR ARCHITECTURAL STANDARD
Module Efficiency

- Efficiency should not be a factor if it is not economical.

Knowledge Gained During This Contract

- Tempered glass
- Reduction of hot spots
- Low cost frame assembly
- Bypass diodes
- Tedlar substrate
- Samics program

Environmental Test Requirements

- Severity
  1. Covers extreme environmental condition
  2. Cycle time faster than actual in many cases

- Results
  1. Pass/failure based on electrical performance and safety.
  2. 5% power degradation seems extreme when compared to other 20 year lifetime products

- Test data
  1. Data is very helpful in isolating problem areas

- In-house testing
  1. Without JPL testing we would conduct our own selected tests on a random sample basis.
ENGINEERING AND OPERATIONS AREAS

SAMICS and SAMIS

- THE PROGRAM
  1. VERY WELL DONE
  2. EASY TO USE AND ACCURATE
  3. EXPERT HELP FROM JPL STAFF
  4. COSTS TOO MUCH TO RUN

- TEST RESULTS
  1. ACCURACY IS DOUBTFUL
     a. INPUT DATA ACCURACY
     b. INTENT OF OUTPUT
     c. CONSIDERED TO BE TODAY'S COST - NOT PILOT PLANT COST

Suggestions

- CHECK LIST IN USERS GUIDE
- TROUBLE SHOOTING SECTION IN USERS GUIDE
- EXPLAIN IMPORTANT FUNCTIONS (SAVE/STOP)
- ADD COST SAVING SECTION (TEXT EDITOR, IPEG, STACKING, ETC.)
- SPECIFY EXACT REPORTS REQUIRED BY NAME AND NUMBER
- REVIEW ALL INPUT (FORMAT A,B,C, AND CURRENT TECHNOLOGY)
- SPECIFY IF "PROOF COPY" IS REQUIRED

General Comments

FEEDBACK:
- ADEQUATE
- HELPFUL
- SUFFICIENT

DESIGN AND PRODUCTION NEEDS:
- QUOTE HIGH EFFICIENCY/HIGH TECHNOLOGY MODULES
- QUOTE LOW COST MODULES
- LARGER PROTOTYPE RUNS
Introduction

At this time, as PV technology faces new markets, the primary general concerns are the balance of cost reduction versus reliability requirements and the need to meet immediate and near-term market demands while developing technology for the long term. ARCO Solar's involvement in Block IV is with two designs for two applications: (1) an intermediate-load module, and (2) a residential module. Module (1) is related to our mainline product and the Block III product, while module (2) is a new departure. Our goal in these developments, like JPL's in Block IV, has been to go for higher quality and cost reduction in that order. The tendency in Block IV to emphasize reliability is certainly an advantage for long-term market development, even where it increases cost in the near term.

A. Design and Performance Requirements

To a certain extent we found the Block IV design requirements incompatible with commercial market requirements. The specification of both voltage and module dimensions (especially the 1.2 meter dimension) potentially required a costly redesign and a more costly product, without any improvement in reliability.

For the present world market, with a large number of different applications, module dimensions need not and should not be standardized, and voltage is not standardizable for all applications. Therefore, Block IV designs may not be compatible with customer requirements. These concerns apply to Module (1) not Module (2). Further, at a time when the majority of sales are for applications of 1-10 modules for battery charging, array dimensioning is not critical for efficiency. We are on the threshold of penetrating some markets where areas and area-related costs become important and module efficiency more critical to the buyer.

ARCO Solar has improved the design of both module types more rapidly than might have happened otherwise, as a result of these requirements and our interaction with JPL. The intermediate-load module is based on a commercial product that had previously been modified to incorporate a metal-foil back as a moisture barrier to meet world market requirements for hermeticity. This had to be grounded when Block IV hi-pot testing revealed capacitive coupling from the circuit to the foil, which discharged to the frame.

The residential module was developed at this time partly because of the stimulus of Block IV. Improvements in termination and diode design resulted from interaction with JPL and the design requirements. More important, our choice of EVA instead of PVB for this module resulted from these requirements.
ENGINEERING AND OPERATIONS AREAS

As shown in the table, we found sample modules using EVA to be clearly superior in maintaining performance parameters after 15-year simulated exposure at DSET Laboratories in Phoenix.

<table>
<thead>
<tr>
<th>POTANT</th>
<th>COVER</th>
<th>Voc</th>
<th>Vpm</th>
<th>Isc</th>
<th>Ipm</th>
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<tbody>
<tr>
<td>EVA</td>
<td>TEDLAR</td>
<td>1.00 +.02</td>
<td>1.02 +.05</td>
<td>1.02 +.03</td>
<td>1.00 +.05</td>
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<tr>
<td>EVA</td>
<td>KORAD</td>
<td>1.01 +.01</td>
<td>.999 +.05</td>
<td>1.01 +.05</td>
<td>1.00 +.08</td>
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<tr>
<td>PVB</td>
<td>TEDLAR</td>
<td>0.72 +.22</td>
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<td>0.99 +.03</td>
<td>1.11 +.08</td>
<td>0.86 +.12</td>
<td>0.79 +.15</td>
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</table>

B. Environmental Test Requirements

These requirements are about right for this stage of development. A key to JPL's success in assisting development is the coupling of progressively stiffer requirements in the successive Block procurements with experience in accelerated testing and in the field. The common experimental data base for lifetime testing and evaluation is a key benefit from JPL's program to the developing PV industry.

The test results are meaningful as indicators of what we should be doing in design. However, the relationship of these test requirements to probable module lifetime remains to be established. European environmental specifications are much stiffer. JPL and industry need to balance carefully the roles of cost and reliability in design and to determine what environmental requirements are needed to achieve optimally balanced designs.

C. SAMICS-SAMIS

The investment of engineering time for estimating cost elements for this rather complex program is high, considering the reliability of input data that can be obtained before production starts. For near-term production, current operational data are much more useful for estimating cost. For far-off production, back-of-envelope calculation is adequate for development program justification until economic analysis methods of the type required for internal planning may be used. These methods of analysis are very company-specific and depend on company strategic goals. Thus SAMICS is not useful to the individual contractor for estimating future costs. This is not to say that SAMICS may not be very useful at the program level, comparing processes or technologies across the industry, if some imprecision can be tolerated in the estimated input data.
ENGINEERING AND OPERATIONS AREAS

D. GENERAL

Data feedback from JPL is good; we found the personnel very cooperative, and the failure analysis work is excellent.

Technology development activities should focus on such things as developing environmental and life-history performance data, and not so much on defining voltage and dimensional characteristics, which are market-directed.

GENERAL ELECTRIC CO.
Neal Shepard

Topics of Concern

• PROCUREMENT DURATION
• DESIGN CHANGES
• ENVIRONMENTAL TESTING

Procurement Duration

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<tr>
<td>PROPOSAL SUBMITTED</td>
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<tr>
<td>CONTRACT START</td>
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<tr>
<td>MODULE DELIVERY COMPLETE</td>
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<td>FINAL DESIGN REVIEW</td>
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<td>FOLLOW-ON PROPOSAL SUBMITTED</td>
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<td>FOLLOW-ON CONTRACT START</td>
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<tr>
<td>FOLLOW-ON MODULE DELIVERY</td>
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<td>PROPOSAL EVALUATION</td>
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<tr>
<td>CONTRACT PERFORMANCE</td>
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</tbody>
</table>

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ENGINEERING AND OPERATIONS AREAS

Scheduling Implications

- 26 MONTHS FROM BLOCK IV DESIGN INCEPTION UNTIL COMPLETION OF STAGED PROCUREMENT

- TOO LONG TO "FREEZE" DESIGN

- SHORTENED SCHEDULE POSSIBLE WITH ONE CONTRACT FOR ENTIRE BLOCK IV PROCUREMENT

Design Changes

<table>
<thead>
<tr>
<th>Solar Cell Supplier</th>
<th>Block IV</th>
<th>Block IV-A</th>
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</thead>
<tbody>
<tr>
<td>Module-to-Module Interconnection</td>
<td>Arco Solar</td>
<td>Solec International</td>
</tr>
<tr>
<td>Integral Wiring With Screw/Washer</td>
<td>Integral Amp Inc. Under Carpet FCC With Crimp Connections</td>
<td></td>
</tr>
</tbody>
</table>

Environmental Testing

- DUPLICATE TESTING (BY JPL AND THE CONTRACTOR) IS EXPENSIVE

- 50 CYCLE THERMAL CYCLING TEST $3500.00
- 7 DAY HUMIDITY TEMPERATURE TEST $2050.00
JPL Solar Module Development Effort

STRUCTURE: GOOD
- Emphasis on solid technology
- Third-party input
- Evaluation support

INTENT:
- Reliable, low-cost residential and intermediate load modules
- Somewhat out-of-step with present commercial markets, i.e., low-voltage, remote systems

APPROACH:
- Iterative
- Industry and user feedback
- Desire to identify appropriate solutions
ENGINEERING AND OPERATIONS AREAS

Solar Module Design and Test Specifications

TEST SPECIFICATIONS:

- QUALIFICATION - GOOD, COMPLETE, NECESSARY
- LIFE TESTING - LACK OF LIFE TESTING TENDS TO SKEW MODULE DESIGNS TOWARDS PASSING QUAL REQUIREMENTS WITH POTENTIALLY REDUCED LIFE AS A CONSEQUENCE, E.G., METALLIC BACKSKIN OF LAMINATED MODULES
- SUGGEST: BALANCE OF QUAL AND LIFE TEST REQUIREMENTS WHICH SHOULD BRING ABOUT BALANCE PRODUCT DESIGNS

DESIGN CRITERIA:

- ORIENTATION TOWARDS RESIDENTIAL/INTERMEDIATE LOAD APPLICATIONS OUT-OF-STEP WITH TODAY'S COMMERCIAL MARKETS, I.E., LOW VOLTAGE, REMOTE SYSTEMS

SAMICS

VALUE

- COMPARE PROCESSES WITHIN FRAMEWORK OF FIXED BURDEN COMPANY
- ALL LABOR SUPPLIES AND COMPONENTS ARE AT SAME PRICE FOR EVERYONE
- PROGRAM IS "UPDATEABLE" FOR NEW ITEMS

DRAWBACKS

- CAN BE INTERPRETED AS TRUE COSTS WHICH IS NOT NECESSARILY SO
- CAN BE MANIPULATED
- DOES NOT ALLOW FOR MANAGEMENT INFLUENCE
- HAS LOADING IN INDIRECTS THAT ARE NOT NECESSARILY VALID

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Design and Performance Requirements

Is the design and performance specification responsive to your perception of the need for modules?

By placing a limitation on size and requirement for an integral voltage, JPL has restricted the module design in regard to cell size.

This restriction becomes more severe as the cell size increases.

What has been the effect of the design requirements on your design?

Forced Solarex to use a 9.5 cm x 9.5 cm cell instead of a 10 cm x 10 cm cell. This had a significant impact on module cost since a 9.5 cm x 9.5 cm cell costs the same as a 10 cm x 10 cm cell.

How critical is module efficiency?

People should not buy modules by efficiency but by average power knowing the module size and the measurement conditions.

The importance of module efficiency depends on conditions of the use including:

- Land availability and cost
- Support structure and interarray wiring costs
- Maintenance requirements and cost

Only after this systems analysis can one determine if a lower-cost-per-watt, lower efficiency module is a better value than a higher-cost-per-watt, higher efficiency module.
IN THE PROCESS OF DESIGNING TO COMPLY WITH THE SPECIFICATION, DID YOU LEARN ANYTHING USEFUL ABOUT MODULE DESIGN?

No more so than designing a module to any specification for a customer.

**Environmental Test Requirements**

ARE THE TESTS TOO STIFF OR TOO LENIENT?

WE PREFER A HIGHER TEMPERATURE HUMIDITY TEST WITH NO CYCLING 70°C AND 90% RELATIVE HUMIDITY. PROBLEMS SHOW UP FASTER.

SHOULD DO THERMAL CYCLE TESTS BOTH BEFORE AND AFTER HUMIDITY.

50 THERMAL CYCLES TOO SHORT TO REALLY INDICATE EXPECTED FIELD PERFORMANCE.

+90°C TO -40°C IS TOO SEVERE TO ACTUALLY SIMULATE PERFORMANCE.

RECOMMEND LESS SEVERE CYCLE, MUCH SHORTER CYCLE, BUT MANY MORE CYCLES.

ARE THE RESULTS OF THE TESTS MEANINGFUL?

IN GENERAL THERMAL CYCLE AND HUMIDITY ARE VERY USEFUL.

DON'T REALLY UNDERSTAND THE RESULTS OF THE HAIL TEST AND WHY SOME MODULES ARE TESTED TO FAILURE.

AS MORE MODULES ARE PROVIDED WITHOUT FRAMES A REDEFINITION OF THE MECHANICAL LOADING TEST MAY BE REQUIRED.

TWIST TEST APPEARS MEANINGLESS ESPECIALLY AFTER THE MECHANICAL LOADING TEST.
ENGINEERING AND OPERATIONS AREAS

Would you perform the testing if JPL did not require it?

We do thermal cycle and humidity testing routinely.

Probably would not do the mechanical loading and twist tests since these properties are well known for glass.

SAMICS and SAMIS

Do you believe the results of this analysis?

Our quote for small quantities (100 kW) was actually less than SAMICS results due to the high overhead rate in SAMICS. We believe that the high overhead is due to an artificial environment where the factory only makes modules. An integrated cell-module line better distributes overhead and yields a lower cost.

We identified a number of areas where materials cost was either much higher or much lower than we now pay.

How could the system be improved?

The formal SAMICS procedure doesn’t provide a format that is easy to use for identification of cost components and cost drivers.

Would rather JPL stress a less complicated technique that the contractor can use to understand the cost components and cost drivers.
ENGINEERING AND OPERATIONS AREAS

General

Is the feedback of data from JPL adequate for our needs?

Generally, the feedback is very good but slow.

In what ways could the technology development activities of the project be better focused on your module design and production needs?

I believe that the JPL procurement group needs more support and interaction with the encapsulation and PP&E groups to better incorporate results from other JPL programs.

Other

Why does JPL put out a specification entitled “Design and Test Specification for Intermediate Load Modules” and limit the size and voltages of the module? Such decision should be left up to the module manufacturer and the system designer.
Design and Performance Requirements

- SPECIFICATIONS
  --- Cost Drivers
    - Redundant output terminations
    - Dimensional tolerances
    - High voltage isolation

- PERFORMANCE REQUIREMENTS
  --- Generally Well Stated
  --- Referenced to NOCT
    - Difficult to establish

- DESIGN REQUIREMENTS
  --- Obvious Interpretation Is To Design A
    High Reliability Module

- MODULE EFFICIENCY
  --- Critical

- MEETING OF SPECIFICATIONS
  --- Useful Learning Process
  --- Thanks To Engineering Area Personnel
ENGINEERING AND OPERATIONS AREAS

Environmental Test Requirements

- Level of requirements is appropriate
- Need for continuous update
  --- e.g. Hot Spot Test
- For consistency JPL should do all testing and report in detail
- Ultimately requirements should be site specific

SAMICS and SAMIS

- SAMIS is expensive
- Results are representative but interpretation difficult for the uninitiated
- Use IPEG for working system
- Reserve SAMICS for final determination
ENGINEERING AND OPERATIONS AREAS

General

- **JPL DATA FEEDBACK**
  - Information Available Informally
  - Formal Structure Inadequate

- **PROJECT ACTIVITIES**
  - Establish Independent Certification of Modules
  - JPL Specifications Often Quoted
    - Only comprehensive documents
    - Not always representative of customer needs

- **BLOCK PROCUREMENT PROGRAM**
  - Represents and Demonstrates Technology Advancement
  - Should Insure Establishment of Reliable Industry Standards
  - It is Difficult to Make Significant Technological Advancements and Cost Reductions Simultaneously and at Low Volume
ENGLISH TESTING
JET PROPULSION LABORATORY
John S. Griffith

Contents

• RESULTS OF TESTING WORLD BANK MODULES

• NEW BLOCK V HUMIDITY TEST - TRIAL RUN ON 11 DIFFERENT TYPES OF MODULES

WORLD BANK MODULES
UNDP Project GLO/78/004

• TITLE: TESTING AND DEMONSTRATION OF SMALL SCALE SOLAR POWERED PUMPING SYSTEMS

• PURPOSE: DEVELOPMENT AND DEMONSTRATION OF IRRIGATION PUMPING IN DEVELOPING COUNTRIES

• FINANCED BY: UNITED NATIONS DEVELOPMENT PROGRAMME

• EXECUTED BY: WORLD BANK

• A&E: SIR WILLIAM HALCROW AND PARTNERS, CONSULTING ENGINEERS AND ARCHITECTS, LONDON, IN ASSOCIATION WITH THE INTERMEDIATE TECHNOLOGY DEVELOPMENT GROUP LTD

• LOCATIONS: SUDAN, MALI (AFRICA), PHILIPPINES

Test Requirements

• U.V. IRRADIATION: AT ROYAL AIRCRAFT ESTABLISHMENT, FARNBOROUGH, ENGLAND, 2 MODULES

• BLOCK IV TEST: (JPL5101-16A) AT JPL, 4 MODULES
ENGINEERING AND OPERATIONS AREAS

Test Results for F1 Modules

- **CONSTRUCTION**
  GLASS TOP COVER, 0.13 mm AIRSPACE, CELLS IN SILICONE RUBBER ENCAPSULANT, ANODIZED ALUMINUM SUBSTRATE

- **TEST RESULTS**
  - **UV**
    AMBER DISCOLORATION OF ENCAPSULANT NEAR EDGE SEAL
  - **HIPOT**
    FAILED PRETEST AND POSTTEST HIPOT
  - **TEMPERATURE CYCLING**
    ONE OF FOUR MODULES OPEN CIRCUITED DUE TO MULTIPLE FRACTURED INTERCONNECTS. DIFFUSION OF EDGE SEALANT INTO ENCAPSULANT (1 MODULE)
  - **HUMIDITY CYCLING**
    THE TWO UV IRRADIATED MODULES SHOWED FURTHER DISCOLORATION. DELAMINATION NEAR TERMINALS ON ONE. MILKY ENCAPSULANT IN THE OTHER
  - **WIND**
    NOT DONE. NO MOUNTING PROVISIONS.
  - **TWIST**
    ONE MODULE SHORTED TO FRAME

- **COMMENTS**
  DESIGN DEFICIENCIES INCLUDE AIRGAP UNDER GLASS, NO STRESS RELIEF LOOPS, SINGLE (NON-REDUNDANT) INTERCONNECTS, INADEQUATE ENCAPSULANT UNDER CELLS (0.03 TO 0.15 mm).

Test Results for F2 Modules

- **CONSTRUCTION**
  GLASS TOP, ENCAPSULATED CELLS, GLASS

- **TEST RESULTS**
  - **HIPOT**
    ALL FOUR MODULES FAILED PRETEST HIPOT, PASSED POSTTEST HIPOT
  - **WIND**
    ONE MODULE HAD INTERMITTENT OPEN DURING TEST. A LOOSE TERMINAL SCREW WAS FOUND

- **COMMENTS**
  RESULTS ARE SOMEWHAT AMBIGUOUS SINCE ISOLATION WAS RESTORED AND THE LOOSE SCREW PROBABLY CAUSED THE INTERMITTENT OPEN
ENGINEERING AND OPERATIONS AREAS

Test Results for U1 Modules

• CONSTRUCTION
  GLASS TOP, CELLS IN PVB, TEDLAR, PVB, KORAD/STEEL BACK SURFACE. BUTYL EDGE SEALANT

• TEST RESULTS
  • HIPOT
    TWO MODULES FAILED PRETEST, 3 FAILED POSTTEST
  • TEMPERATURE CYCLING
    FRAME SEALANT EXTRUDED OUT OF FRAMES, (4 MODULES) AND IN TOWARD CELLS (2 MODULES)
  • HUMIDITY CYCLING
    ONE MODULE HAD BACK SURFACE DELAMINATION (BLISTER)

• COMMENTS
  SOME REDESIGN AND PROCESSING IMPROVEMENTS NEEDED

Test Results for U2 Modules

• CONSTRUCTION
  GLASS TOP, ENCAPSULATED CELLS, FIBERGLASS/POLYESTER SUBSTRATE

• TEST RESULTS (5 MODULES)
  • HIPOT
    UV IRRADIATED MODULES FAILED PRETEST HIPOT, PASSED POSTTEST HIPOT
  • HUMIDITY CYCLING
    ONE CELL CRACKED; NO ELECTRICAL DEGRADATION
  • TWIST
    INCREASE IN SERIES RESISTANCE OBSERVED, ONE MODULE

• COMMENTS
  RESULTS GENERALLY VERY GOOD. CAUSES OF HIPOT AND TWIST TEST PROBLEMS UNKNOWN
ENGINEERING AND OPERATIONS AREAS

Conclusions

• ONE U.S. AND ONE FOREIGN MODULE APPEAR TO BE SATISFACTORY AFTER CORRECTING SOME MINOR DEFICIENCIES

• ANOTHER U.S. MODULE REQUIRES MORE EXTENSIVE IMPROVEMENTS

• THE SECOND FOREIGN MODULE IS UNSATISFACTORY ON SEVERAL COUNTS

PROPOSED NEW ENVIRONMENTAL TESTS FOR BLOCK V MODULES

• QUALIFICATION TESTS HAVE NOT BEEN EFFECTIVE IN REVEALING SOME MODULE WEAKNESSES

• EXAMPLES
  • BROKEN INTERCONNECTS IN < 2 yrs AT SCHUCHULI, UPPER VOLTA
  • HOT CELL PROBLEM AT MT. LAGUNA AND OTHER SITES
  • DELAMINATION, DISCOLORATION, CORROSION, ELECTRICAL DEGRADATION

• NEW TESTS PROPOSED
  • INTERCONNECT FATIGUE - 200 TEMPERATURE CYCLES
  • HOT CELLS - BACK BIAS SEVERAL CELLS TO WORST CONDITIONS
  • DELAMINATION, ETC - MORE SEVERE HUMIDITY TEST WITH FREEZING

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New Humidity-Freezing Cycle Test
(To Follow 50 Temperature Cycles)

ENGINEERING AND OPERATIONS AREAS

- Condition:
  - 85% ± 2.5% RH

- Freezing:
  - 85% ± 2.5% RH
  - 100°C/h Maximum
  - 200°C/h Maximum
  - 0.5h Minimum
  - 20 Minimum
  - 4 Maximum

CONTINUE FOR 10 CYCLES

END OF CYCLE

START OF CYCLE

TIME (h)

MODULE TEMPERATURE (°C)
## Results of 85° - 85% Test

<table>
<thead>
<tr>
<th>VENDOR/ BLOCK</th>
<th>PRE-85/85 TEST HISTORY</th>
<th>CONSTRUCTION</th>
<th>RESULTS</th>
</tr>
</thead>
<tbody>
<tr>
<td>YII</td>
<td>NONE</td>
<td>RTV, F/P*</td>
<td>J-BOX CORROSION</td>
</tr>
<tr>
<td>YIII</td>
<td>NONE</td>
<td>RTV, F/P</td>
<td>J-BOX CORROSION</td>
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<tr>
<td>ZIII</td>
<td>NONE</td>
<td>SILICONE, F/P</td>
<td>6% ELECT. DEGRAD, YELLOWED ENCAP, DELAM AT ICs, CELLS, FRAME SEAL, 1 CELL CRACK</td>
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<tr>
<td>VIII</td>
<td>NONE</td>
<td>RTV, PVC SCREEN, ALUM PAN</td>
<td>YELLOWED ENCAP, GRAY METALLIZATION</td>
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<tr>
<td>VIII</td>
<td>NONE</td>
<td>GLASS, RTV, SCREEN ALUM PAN</td>
<td>GROUND TERM. RUST, FRAME SEAL DELAM</td>
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<tr>
<td>UII</td>
<td>NONE</td>
<td>GLASS, PVB, TEDLAR, ALUM FRAME</td>
<td>19% ELECT. DEGRAD, 98% FRAME SEAL DELAM, END CAPS DISTORTED</td>
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<td>*F/P, FIBERGLASS POLYESTER SUBSTRATE</td>
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<td>ZPRDA</td>
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<td>GLASS, RTV, MYLAR, ALUM FRAME</td>
<td>FRAME SEAL DELAM, CELL DELAM</td>
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<td>RIV</td>
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<td>GLASS, PVB, TEDLAR/ALUM/TEDLAR BACK, SS FRAME</td>
<td>(2) CELLS CR., FRAME SEALANT EXTRUDED</td>
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<td>SIIV</td>
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<td>GLASS, EVA, RIPSTOP, MYLAR/ALUM, BACKSPRAY</td>
<td>CORROSION OF RIVETS AND GROUND CLIP</td>
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<tr>
<td>GIV</td>
<td>QUAL</td>
<td>SHINGLE - GLASS, SILICONE, CARDBOARD</td>
<td>29% ELECT. DEGRAD, CORROSION OF ICs, COLLECTORS</td>
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<td>MIV</td>
<td>QUAL</td>
<td>GLASS, PVB, TEDLAR, ALUM FRAME</td>
<td>60% FRAME SEAL DELAMINATION, GRAY ICs, RUSTED RIVETS</td>
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</table>
### Comparison: Earlier Qualification Tests vs New 85° - 85%

#### RESULTS

<table>
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<tr>
<th>VENDOR/ BLOCK</th>
<th>PRE-85/ 85 TEST HISTORY</th>
<th>ELECT. DEGRAD</th>
<th>CELL CRACKS</th>
<th>DELAMINATION</th>
<th>BACK SEALANT</th>
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<td>•</td>
<td>•</td>
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<td>•</td>
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<td>NIZ NONE</td>
<td>•</td>
<td>•</td>
<td>•</td>
<td>O</td>
<td>•</td>
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<td>MIZ QUAL</td>
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</table>

○ EARLIER QUAL TESTS - TEMP AND HUMIDITY CYCLING  
● RECENT 85/85 TEST

SIZE OF CIRCLE INDICATES DEGREE OF DEGRADATION
CONCLUSIONS

- WORLD BANK MODULES
  - TWO FOREIGN AND TWO U.S. TYPES OF MODULES WERE TESTED FOR APPLICATION TO PUMPING SYSTEMS IN DEVELOPING COUNTRIES
  - TWO MODULES WERE SATISFACTORY, 1 FOREIGN AND 1 U.S.; 1 U.S. WAS MARGINAL; ONE FOREIGN WAS UNSATISFACTORY

- PROPOSED NEW HUMIDITY-FREEZE TEST
  - THE NEW TEST IS 85°C, 85% R.H. FOR 10 days EXCEPT FOR 10 SHORT EXCURSIONS TO ~40°C
  - A TRIAL RUN WAS MADE ON 11 TYPES OF MODULES
  - RESULTS SHOW THE NEW TEST TO BE MORE EFFECTIVE IN REVEALING PROBLEMS WITH CORROSION, DELAMINATION, AND SOME FORMS OF POWER DEGRADATION
MIT-LL Residential PV Test Facilities

1. NE RESIDENTIAL TEST STATION
   5 PROTOTYPES IN CONCORD, MA
   1 ISEE IN CARLISLE, MA

2. SW RESIDENTIAL TEST STATION
   8 PROTOTYPES IN LAS CRUCES, NM

3. INNOVATIVE PV APPLICATIONS FOR RESIDENCES
   ARIZONA, FLORIDA, HAWAII (3)

4. SE RESIDENTIAL TEST STATION
   RFQ FOR SITE OPERATOR ISSUED 19 DECEMBER 1981

Northeast Residential Test Station, Concord MA

SITE OPERATOR: MIT LL

<table>
<thead>
<tr>
<th>PRIME CONTRACTOR</th>
<th>NO. OF MODULES</th>
<th>PV ARRAY DETAILS</th>
<th>TILT ANGLE</th>
<th>PEAK POWER - kW</th>
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</thead>
<tbody>
<tr>
<td>TRISOLAR</td>
<td>36 ASEC</td>
<td>47.6</td>
<td>45°</td>
<td>4.8</td>
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<tr>
<td></td>
<td>INTEGRAL</td>
<td></td>
<td></td>
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<tr>
<td>GENERAL ELECTRIC</td>
<td>375 6E</td>
<td>73.7</td>
<td>33.7°</td>
<td>5.6</td>
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<td></td>
<td>SHINGLE</td>
<td></td>
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<tr>
<td>SOLAREX</td>
<td>80 SX</td>
<td>74.3</td>
<td>40°</td>
<td>6.2</td>
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<td>STANDOFF</td>
<td></td>
<td></td>
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<tr>
<td>WESTINGHOUSE</td>
<td>160 ARCO</td>
<td>59.5</td>
<td>45°</td>
<td>5.4</td>
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<td></td>
<td>INTEGRAL</td>
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<td></td>
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<tr>
<td>MIT LL</td>
<td>120 SX</td>
<td>93.6</td>
<td>45°</td>
<td>7</td>
</tr>
<tr>
<td></td>
<td>STANDOFF</td>
<td></td>
<td></td>
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</table>
ENGINEERING AND OPERATIONS AREAS

PEAK POWER DISTRIBUTION FOR 120 BLOCK-IV RESIDENTIAL SOLAR MODULES USED IN THE MIT/LL PROTOTYPE AT THE NORTHEAST RESIDENTIAL EXPERIMENT STATION

PEAK POWER DISTRIBUTION FOR 36 RESIDENTIAL APPLIED SOLAR ENERGY MODULES USED IN THE TRIANGULAR PROTOTYPE AT THE NORTHEAST RESIDENTIAL EXPERIMENT STATION

ORIGINAL PAGE IS OF POOR QUALITY
ENGINEERING AND OPERATIONS AREAS

PEAK POWER DISTRIBUTION FOR 40 QUADS OF ARCO RESIDENTIAL MODULES
USED IN THE WESTINGHOUSE PROTOTYPE AT THE NORTHEAST RESIDENTIAL EXPERIMENT STATION

PEAK POWER DISTRIBUTION FOR 132 BLOCK IV RESIDENTIAL
SOLAREX MODULES TO BE USED FOR THE CARLISLE HOUSE
PROJECT

383
## Engineering and Operations Areas

### Southwest Residential Test Station, Las Cruces NM

**Site Operator:** NMSEI

### PV Array Details

<table>
<thead>
<tr>
<th>Prime Contractor</th>
<th>No. of Modules</th>
<th>Size - m²</th>
<th>Tilt Angle</th>
<th>Peak Power - kW</th>
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<tbody>
<tr>
<td>BDM</td>
<td>117 MOT STANDOFF</td>
<td>49.9</td>
<td>35°</td>
<td>4.7</td>
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<tr>
<td>TEA</td>
<td>112 MOT RACK MOUNTED</td>
<td>49.6</td>
<td>29.7°</td>
<td>4.5</td>
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<td>80 SX STANDOFF</td>
<td>70.6</td>
<td>26°</td>
<td>5.2</td>
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<tr>
<td>TRISOLAR</td>
<td>44 ASEC INTEGRAL</td>
<td>58.1</td>
<td>30°</td>
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<td>ARTU</td>
<td>168 ARCO STANDOFF</td>
<td>62.5</td>
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<tr>
<td>ARCO</td>
<td>126 ARCO BATTEN-SEAM</td>
<td>80</td>
<td>26°</td>
<td>6.6</td>
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<td>GE</td>
<td>375 GE SHINGLE</td>
<td>73.3</td>
<td>26.6°</td>
<td>5.6</td>
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<tr>
<td>WESTINGHOUSE</td>
<td>160 ARCO INTEGRAL</td>
<td>59.5</td>
<td>30.2°</td>
<td>5.8</td>
</tr>
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</table>

### Innovative PV Applications for Residences

1. **J. F. Long House - Phoenix, Arizona**
   - 120 ARCO Batten-Seam Modules, 4.6 kW

2. **Florida Solar Energy Center, Cape Canaveral, Florida**
   - 152 ARCO Standoff Modules, 5 kW

3. **Hawaii Natural Energy Institute, Honolulu, Hawaii**
   - Three Sites: Kalihi, Pearl City, Molokai
   - All Sites Use ARCO Modules
ENGINEERING AND OPERATIONS AREAS

PV Module Performance at Various MIT-LL Test Sites

I. SYSTEM TEST FACILITIES
   - HBPL, UTAH 100 kW
   - READ, NEBRASKA 25 kW
   - RESIDENTIAL TEST BED, MASSACHUSETTS 25 kW
   - AM RADIO STATION, BRYAN, OHIO 25 kW
   - ROOFTOP TEST BED, MASSACHUSETTS 10 kW
   - UNIVERSITY OF TEXAS, ARLINGTON 7.5 kW
   - CHICAGO MUSEUM 1.5 kW

II. ENVIRONMENTAL TEST SITES
   - NEW YORK UNIVERSITY - (23 MODULES)
   - COLUMBIA UNIVERSITY - (10 MODULES)
   - MASSACHUSETTS INSTITUTE OF TECHNOLOGY - (18 MODULES)
   - MT. WASHINGTON, NEW HAMPSHIRE WEATHER STATION - (5 MODULES)

PV Module Failures at MIT-LL Test Sites

DATA UP TO 1/81

<table>
<thead>
<tr>
<th>Fig.</th>
<th>NEB</th>
<th>RES STF</th>
<th>ROOF STF</th>
<th>UTA</th>
<th>CHIC</th>
<th>NBNO</th>
<th>NBMV</th>
<th>TOTALS</th>
</tr>
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<tbody>
<tr>
<td></td>
<td>(7/77)</td>
<td>(11/79)</td>
<td>(5/77)</td>
<td>(0/78)</td>
<td>(7/77)</td>
<td>(0/79)</td>
<td>(1/80)</td>
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<tr>
<td>A (I)</td>
<td>-</td>
<td>-</td>
<td>15/945</td>
<td>-</td>
<td>6/290</td>
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<td>-</td>
<td>15/1235</td>
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<td>A (II)</td>
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<td>5/64</td>
<td>65/240</td>
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<td>70/2240</td>
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<tr>
<td>B (II)</td>
<td>35/728</td>
<td>-</td>
<td>8/372</td>
<td>5/640*</td>
<td>-</td>
<td>-</td>
<td>-</td>
<td>5/726</td>
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<tr>
<td>C (III)</td>
<td>15/700</td>
<td>0/38</td>
<td>0/36</td>
<td>-</td>
<td>-</td>
<td>-</td>
<td>-</td>
<td>13/1012</td>
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<td>D (III)</td>
<td>5/194</td>
<td>1/74</td>
<td>-</td>
<td>-</td>
<td>-</td>
<td>4/200</td>
<td>-</td>
<td>9/1000</td>
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<tr>
<td>E (III)</td>
<td>-</td>
<td>-</td>
<td>-</td>
<td>-</td>
<td>-</td>
<td>-</td>
<td>1/1740</td>
<td>1/1740</td>
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<tr>
<td>F (III)</td>
<td>-</td>
<td>-</td>
<td>-</td>
<td>-</td>
<td>-</td>
<td>3/2004</td>
<td>31/2004</td>
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4.2%  2.21%  1.9%  27%  0%  0.5%  0.7%  250/11117
0.8%  2.2%  2.2%

* Array Start Date 5/60
** 52 Modules have been found with cracked glass cover sheets

ORIGINAL PAGE IS OF POOR QUALITY
## PV Module Failures at MIT LL Test Sites

**Data Up To 01/81**

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<tr>
<th>Site</th>
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<td>RES STF</td>
<td>11/78</td>
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<td>15/700</td>
<td>13/556</td>
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<td>ROOF STF</td>
<td>5/77</td>
<td>15/945</td>
<td>5/100</td>
<td>1/74</td>
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<tr>
<td>UTA</td>
<td>8/78-4/80</td>
<td>--</td>
<td>65/240</td>
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<tr>
<td>UTA</td>
<td>4/80</td>
<td>--</td>
<td>--</td>
<td>5/640</td>
</tr>
<tr>
<td>CHIC</td>
<td>8/79</td>
<td>0/288</td>
<td>--</td>
<td>--</td>
</tr>
<tr>
<td>WBNO</td>
<td>8/70</td>
<td>--</td>
<td>5/640</td>
<td>--</td>
</tr>
<tr>
<td>NBNM</td>
<td>1/80</td>
<td>--</td>
<td>0/720**</td>
<td>32/3804</td>
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</table>

**Totals** 15/1233 180/4000 55/5884

(1.22%)  (4.50%)  (0.95%)

**Note:** 52 modules have been found with cracked glass cover sheets.

### Principal Causes of Module Failures

1. **Cells cracked due to weathering or internal module stresses.**
2. **Failed solder joints.**
3. **Interconnects not soldered to rear sides of cells at assembly.**
4. **Cell string shorted to substrate.**
5. **Broken or split interconnects.**
In-Service Performance of Nebraska PV Modules

![Diagram showing cumulative failed modules percentage over operating time in months]

- **2240 Modules**
- **Hail**

**Operating Time, Months:**

**Cumulative Failed Modules, Percent:**

C - S
Module Failures at Mead Test Site

FRONT ROW = 728 MODULES
BACK ROW = 1512 MODULES

STARTING DATE = JULY 1977

<table>
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<th>DATE OF SEARCH</th>
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<tr>
<td>OCTOBER 1977</td>
<td>0</td>
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<tr>
<td>NOVEMBER 1977</td>
<td>1</td>
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<tr>
<td>FEBRUARY 1978</td>
<td>0</td>
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<td>MARCH 1978</td>
<td>0</td>
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<td>JULY 1978</td>
<td>6</td>
</tr>
<tr>
<td>SEPTEMBER 1978</td>
<td>3</td>
</tr>
<tr>
<td>FEBRUARY 1979</td>
<td>2</td>
</tr>
<tr>
<td>MARCH 1979</td>
<td>1</td>
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<td>JULY 1980</td>
<td>11</td>
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<td>OCTOBER 1980</td>
<td>4</td>
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<tr>
<td><strong>TOTALS</strong></td>
<td><strong>35</strong></td>
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</table>

Failed Modules With Broken Interconnects

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<tr>
<th>SITE (MFG)</th>
<th>TOTAL NO. OF MODULES</th>
<th>TOTAL NO. OF FAILURES</th>
<th>FAILURES WITH BROKEN INTERCONNECTS</th>
<th>TIME</th>
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<tr>
<td>NEB (D-II)</td>
<td>728</td>
<td>35</td>
<td>4</td>
<td>3-1/4 YRS.</td>
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<tr>
<td>OHIO (D-III)</td>
<td>800</td>
<td>4</td>
<td>2</td>
<td>9 MOS.</td>
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<td>RES STF (D-III)</td>
<td>194</td>
<td>5</td>
<td>5</td>
<td>2 YRS.</td>
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<tr>
<td>ROOF STF (D-III)</td>
<td>74</td>
<td>1</td>
<td>1</td>
<td>2 YRS.</td>
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<td>(B-II)</td>
<td>64</td>
<td>5</td>
<td>1</td>
<td>3-1/4 YRS.</td>
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ENGINEERING AND OPERATIONS AREAS

1-V CURVE TRACER EMPLOYING A CAPACITIVE LOAD

MASSACHUSETTS INSTITUTE OF TECHNOLOGY
LINCOLN LABORATORY

C.H. Cox III
T.H. Warner

Functions and Requirements

Operations
  Display
  Analysis
  Storage

Interface
  IEEE Bus

Packaging
  Portable
  AC Available

Basic Capacitive-Charging Method

Resultant I-V Curve

\[ v(t) = \frac{1}{C} \int_{0}^{t} i(\tau) d\tau \]
ENGINEERING AND OPERATIONS AREAS

\[ C = 1000 \, \mu F \]

CURRENT SOURCE APPROXIMATION

Increasing charging interval (seconds)

\( V_{OC} - \text{Final capacitor voltage (volts)} \)
ENGINEERING AND OPERATIONS AREAS

I-V Curve Tracer

SEQUENCE CONTROL LOGIC

VOLTAGE SENSE

CURRENT SENSE

DATA AQUISITION

MEMORY

DISPLAY

DATA PROCESSING

USER CONTROL

ENERGY DISSIPATION

ARRAY

TAPE STORAGE

HP-85

391
Comparison of 10-kW Curve Tracers

BRANCH # AP1-1
AMB T = -1.8 DEG C
CEL T = 4.80 DEG C
INSO = 98.0 MW/SQ CM
VOC = 283 VOLTS
ISC = 10.4 AMPS
PMAX = 1935 WATTS
= 210 V & 8.83 A
## ENGINEERING AND OPERATIONS AREAS

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<th>Resistor Load</th>
<th>Capacitor Load</th>
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<td>Power HP</td>
<td>Total</td>
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<td>Weight (lbs)</td>
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<td>13 20</td>
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<td>Size (cu ft)</td>
<td>4.3</td>
<td>0.5 1.08</td>
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<td>Cost ($)</td>
<td>10,000</td>
<td>2500 3200</td>
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<tr>
<td>Power Consumption (W)</td>
<td>240</td>
<td>20 30</td>
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ENGINEERING AND OPERATIONS AREAS

PROBLEM-FAILURE ANALYSIS

JET PROPULSION LABORATORY
Steve Sollock

Problem-Failure Reporting System
Short-to-Ground History

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<thead>
<tr>
<th>VENDOR</th>
<th>PROCUREMENT</th>
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<td></td>
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<td>V</td>
<td>1</td>
</tr>
<tr>
<td>W</td>
<td>2</td>
</tr>
<tr>
<td>Y</td>
<td>2</td>
</tr>
<tr>
<td>Z</td>
<td>2</td>
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<tr>
<td>U</td>
<td></td>
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</tr>
<tr>
<td>K</td>
<td></td>
</tr>
<tr>
<td>M</td>
<td></td>
</tr>
<tr>
<td>COM AND DEVEL</td>
<td></td>
</tr>
</tbody>
</table>

Short to Ground

- PROBLEM CLASSIFICATION

- DESIGN
  - PROBLEMS RELATING TO PROCESS AND MATERIALS

- WORKMANSHP
  - PROBLEMS RELATING TO PROCEDURE AND ASSEMBLY
Sample Module Laminate

Shorts Due to a Conductive Sealant
Substrate Burnthrough Caused by Interconnect Foil Short to Substrate Pan Assembly

Sample Module Laminate
ENGINEERING AND OPERATIONS AREAS

Electrical Hazards Resulting From Shorts

- TO EQUIPMENT
- PERSONNEL

Short to Ground
ENGINEERING AND OPERATIONS AF: EAS

PROBLEM-FAILURE ANALYSIS

JET PROPULSION LABORATORY
Alex Shumka

Objective

• PRESENT FAILURE ANALYSIS RESULTS ON SHORTS TO GROUND

• DISCUSS PROBABLE FAILURE CAUSE

• DESCRIBE MEASUREMENT TECHNIQUES ON DIELECTRIC MATERIALS USEFUL FOR DESIGN EVALUATION, QUALITY CONTROL AND FAILURE ANALYSIS

Shorts to Ground

• MODULE FRAME TO CELL STRING

• MODULE FRAME TO MODULE TERMINALS

• ARRAY STRUCTURE/MODULE FRAME TO MODULE INTERCONNECT WIRES

• FRAME TO FLOATING METALLIC MOISTURE BARRIER

• CELL STRING TO FLOATING/GROUNDED METALLIC MOISTURE BARRIER

General Construction
Improperly Etched Margin; Poor Dielectric Coating Application
Misaligned Scrim Cloth; Dielectric Coating Cut Through
Pressure-Induced Kapton Failure

CLAMPING FORCE

GLASS
INTERCONNECT

S.S. PAN

FAILURE

SIDE VIEW

KAPTON FILM
PRESSURE SPLIT

BOTTOM VIEW

KAPTON
CU

CU FOIL

ENGINEERING AND OPERATIONS AREAS
Burr-Induced Insulation Failure; Power Overstress at Solder Joint

ORIGINAL PAGE IS OF POOR QUALITY
Insufficient Spacing Between Cells and Frame
Partial Discharge Tester

Discharges Due to Voids

Point-to-Plane Discharges

Surface Discharges

Contact Resistance Discharges

LOOSE OR NOISY CONTACT
ENGINEERING AND OPERATIONS AREAS

![Graph showing partial discharge (corona) in picocoulombs (peak) vs. test voltage in kV (AC RMS 60 Hz).]

- **Y-axis**: Partial discharge (corona) in picocoulombs (peak)
- **X-axis**: Test voltage in kV (AC RMS 60 Hz)

The graph indicates a calibration level at 20 and shows a sharp increase at around 1.6 kV.
ENGINEERING AND OPERATIONS AREAS

Failure Analysis Module Dielectric Tests

<table>
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<tr>
<th>TEST</th>
<th>Q/C EVALUATION</th>
<th>DESIGN EVALUATION</th>
<th>DEGRADATION QUAL TEST</th>
<th>DEGRADATION FIELD</th>
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<td>CAPACITANCE</td>
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<td>✓ X</td>
<td>✓ X</td>
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<td>DC I_L OR I_R</td>
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NOTE: ✓ - TESTS PERFORMED BY JPLIFA  
X - TESTS RECOMMENDED BY JPLIFA

Summary

SOME FAILURE CAUSES

DESIGN: INADEQUATE INSULATION MARGIN; UNDESIRABLE DEFORMATION OF INSULATION DUE TO COMPRESSIVE FORCES; USE OF CONDUCTIVE SEALANT MATERIAL

WORKMANSHIP: METALLIC BURRS; SHARP POINTS ON INTERCONNECTS; MISALIGNMENT OF INSULATORS AND/OR CELLS

HANDLING: MECHANICAL DAMAGE OF TERMINALS AND FRAME

408
Discharges Due to Voids

Surface Discharges
Point-to-Point Discharges
Recent Accomplishments

- REQUIREMENT DEVELOPMENT
  - FLAT-PLATE MODULE SAFETY STANDARD (5101-164)
  - FLAT-PLATE ARRAY SAFETY WORKSHOP (FEB. 3)
  - BLOCK V MODULE DESIGN SPECIFICATIONS (5101-161, 5101-162)
  - PRODUCT LIABILITY PHASE 1 REPORT (CMU)

- ARRAY SUBSYSTEM DEVELOPMENT
  - GROUND-MOUNTED ARRAY STRUCTURE DESIGN PACKAGE
  - RESIDENTIAL ARRAY STRUCTURE CONTRACT INITIATION (GE, AIA/RC)

- MODULE ENGINEERING/RELIABILITY
  - MODULE SOILING REPORT (5101-131)
  - CELL RELIABILITY TESTING ANNUAL REPORT (Clemson)
  - CELL RELIABILITY WORKSHOP PROCEEDINGS (5101-163)
  - INTERCONNECT FATIGUE PROBABILITY ANALYSIS
  - HOT-SPOT ENDURANCE TEST PROCEDURE/RESULTS

- PERFORMANCE CRITERIA AND STANDARDS
  - FLAT-PLATE PV-T TEST METHOD
  - ACTIVELY COOLED CONCENTRATOR TEST METHOD
ENGINEERING AND OPERATIONS AREAS

Ongoing Activities

- REQUIREMENT DEVELOPMENT STUDIES
  - SAFETY DESIGN REQUIREMENTS (UL)
  - PRODUCT LIABILITY REQ. (CARNEGIE-MELLON)
  - COMMERCIAL BUILDING CODES (BURT-HILL)
  - WIND LOADING (BOEING/CSU)

- ARRAY SUBSYSTEM DEVELOPMENT
  - LARGE GROUND MOUNTED ARRAYS (JPL)
  - INTEGRATED RESIDENTIAL ARRAYS (GE AND AIA)

- MODULE ENGINEERING/RELIABILITY STUDIES
  - OVERALL RELIABILITY ANALYSIS (JPL/IITRI)
  - ELECTRICAL INSULATION (JPL)
  - GLASS BREAKAGE (JPL)
  - INTERCONNECT FATIGUE (JPL)
  - HOT-SPOT ENDURANCE (JPL)
  - CELL RELIABILITY TESTING (CLEMSON)
  - CELL FRACTURE MECHANICS (JPL)
  - ACCELERATED SUNLIGHT TESTING (DSET)
  - LONG-TERM HUMIDITY TESTING (WYLE)
  - CORROSION ENDURANCE (WYLE)
  - SOILING (JPL)

- STANDARDS ACTIVITIES
  - ARRAY TASK GROUP MANAGEMENT (FOR SERI)
  - PV-T PERFORMANCE TEST DEVELOPMENT (JPL)
  - CONCENTRATOR PERFORMANCE TEST DEVEL (ASU)
ENGINEERING AND OPERATIONS AREAS

Code Development and Usage

- **INDUSTRY**
- **PROFESSIONAL**
- **PUBLIC**

**CODE USERS**

**CODE NEEDS OR REQUIREMENTS**

**MODEL CODE GROUPS**

**RE-EVALUATION AND UPDATING**

**CODE CONGRESS**

**EXECUTIVE DIRECTOR**

**CODES**

**DAY TO DAY**

Southern Building Code Congress (SBCC)
ENGINEERING AND OPERATIONS AREAS

BOCA BASIC BUILDING CODE 1981 EDITION

SECTION 101.3: MATTERS NOT PROVIDED FOR:

Any requirement essential for structural, fire or sanitary safety of an existing or proposed building or structure, or essential for the safety of the occupants thereof, and which is not specifically covered by this Code, shall be determined by the Building Official.

SECTION 107.4: ALTERNATIVE MATERIALS AND EQUIPMENT

The provisions of this Code are not intended to prevent the use of any material or method of construction not specifically prescribed by this Code, provided any such alternative has been approved. The Building Official may approve any such alternative provided the Building Official finds that the proposed design is satisfactory and complies with the intent of the provisions of this Code, and that the material, method or work offered is, for the purpose intended, at least the equivalent of that prescribed in this Code in quality, strength, effectiveness, fire resistance, durability and safety.
## ENGINEERING AND OPERATIONS AREAS

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### Engineering and Operations Areas

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<th>Building Height</th>
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<th>Type 4</th>
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<tr>
<td>Stories and Feet</td>
<td>Exterior Masonry Walls</td>
<td>Frame</td>
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<td>Classification</td>
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<td>Non-Combustible</td>
<td>Timber</td>
<td>Ordinary</td>
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<td>Assembly School</td>
<td>5 ft</td>
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<td>Business Office</td>
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<td>Factory/Industry</td>
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<td>50</td>
<td>30</td>
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418
<table>
<thead>
<tr>
<th>ENGINEERING AND OPERATIONS AREAS</th>
</tr>
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<tbody>
<tr>
<td>POTENTIAL FOR PHOTOVOLTAIC APPLICATION</td>
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<td>CLASSIFICATION</td>
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<td>EXAMPLE CITED: DENTAL CLINIC</td>
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<td>A ASSEMBLY TYPE</td>
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<tr>
<td>R RESIDENTIAL NON-HOUSKEEPING</td>
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<td>S STORAGE</td>
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</tbody>
</table>

**KEY**
- PROBABLE
- POSSIBLE
- IMPROBABLE
- N.P.
- NOT PERMITTED

*ORIGINAL PAGE IS OF POOR QUALITY*
ENGINEERING AND OPERATIONS AREAS

Building Codes Reviewed

SOUTHERN BUILDING CODE CONFERENCE (SRCC)  
STANDARD BUILDING CODE

BUILDING OFFICIAL CONFERENCE OF AMERICA (BOMA)  
BASIC BUILDING CODE

INTERNATIONAL CONFERENCE OF BUILDING OFFICIALS (ICOB)  
UNIFORM BUILDING CODE

PITTSBURGH BUILDING CODE

LOS ANGELES BUILDING CODE

Standards and Testing Agencies Reviewed

AMERICAN SOCIETY OF TESTING AND MATERIALS (ASTM)

AMERICAN NATIONAL STANDARDS INSTITUTE (ANSI)

NATIONAL BUREAU OF STANDARDS (NBS)

FEDERAL STANDARDS AND SPECIFICATIONS

NATIONAL FIRE PROTECTION ASSOCIATES (NFPA)

UNDERWRITERS LABORATORIES (UL)
ENGINEERING AND OPERATIONS AREAS

Present Potential Barriers to the Development
Of Photovoltaic Arrays in Model Codes

- Roof covering materials must achieve a Class A or B rating for many applications when tested according to ASTM E108, The Standard Methods of Fire Tests of Roof Coverings.

- Plastic materials must achieve an approved status of C-1 or C-2 according to ASTM D635, Rate or Burning and/or Extent and Time of Burning of Self-Supporting Plastics in a Horizontal Position, to be utilized. Even then, restrictions can be severe.

### Plastic Roof Panels

<table>
<thead>
<tr>
<th>Classification</th>
<th>Max. Panel Area (Individual Unit)</th>
<th>Total Area of Plastic on Roof (% of Floor Area)</th>
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<tbody>
<tr>
<td>SBCC and BOCA</td>
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<tr>
<td>Class CC1</td>
<td>300 S.F.</td>
<td>30%</td>
</tr>
<tr>
<td>Class CC2</td>
<td>100 S.F.</td>
<td>25%</td>
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</table>

- Photovoltaic modules which become part of a bearing wall section or roof section must be rated according to ASTM E110 Standard Methods of Fire Tests of Building Construction and Materials for Hours of Fire Containment with Structural Retention.

### Construction Type

<table>
<thead>
<tr>
<th>Mounting Application</th>
<th>Fireproof Pro-</th>
<th>Non-Combustible Pro-</th>
<th>Timbers Pro-</th>
<th>Masonry Walls Ordinary</th>
<th>Frame Unpro-</th>
<th>Type 1</th>
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<th>Type 3</th>
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<td>2B</td>
<td>2C</td>
<td>3A</td>
<td>3B</td>
<td>3C</td>
<td>4A</td>
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<td>Non-Rear Wall</td>
<td>4A</td>
<td>4B</td>
<td>1A</td>
<td>1B</td>
<td>1C</td>
<td>4A</td>
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</table>

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ENGINEERING AND OPERATIONS AREAS

Rack

Standoff

Direct

Integral
PRELIMINARY CONCLUSIONS

- PV NOT ADDRESSED IN NEC
- POSSIBLE INCLUSION IN NEC 1984 EDITION - DRAFT REQUIRED BY MID - 1982
- PREMANUFACTURED WIRING SYSTEMS ADVANTAGEOUS
- VOLTAGE LEVEL 110 - 220 V (BASED ON COST OF WIRING)
- UL TESTING AND APPROVAL NECESSARY
- FURTHER WORK REQUIRED ON OPTIMUM SIZE
- NO MAJOR OR INSURMOUNTABLE PROBLEMS
- STANDARD INVESTIGATION IS ANTICIPATORY AND CURRENTLY UNDERWAY BY SERI
  AND ANSI
- CODE INVESTIGATION REQUIRED FOR EACH APPLICATION

NATIONAL ELECTRIC CODE SUMMARY

GENERAL

THE PURPOSE OF THE CODE IS PRACTICAL SAFEGUARDING OF PERSONS AND
PROPERTY.

SAFETY

LIVE PARTS OPERATING AT 50 VOLTS OR MORE SHALL BE GUARDED AGAINST
ACCIDENTAL CONTACT DURING INSTALLATION. THIS MAY BE NECESSARY AT ALL
VOLTAGE LEVELS.
ENGINEERING AND OPERATIONS AREAS

NATIONAL ELECTRICAL CODE SUMMARY

GROUNDING

NEC GROUNDING REQUIREMENTS FOR D.C. SYSTEMS DO NOT APPLY TO PV SYSTEMS IN GENERAL. THE AREAS OF NONAPPLICABILITY INCLUDE:

- QUALIFICATION FOR CIRCUIT AND SYSTEM GROUNDING BASED ON VOLTAGE LEVEL
- POINT OF GROUNDING CONNECTION FOR D.C. SYSTEMS
- GROUNDING OF CONDUCTOR ENCLOSURES
- GROUNDING OF SOME NONCURRENT-CARRYING METAL PARTS OF EQUIPMENT

PV GROUNDING SHOULD COMPLY WITH THE NEC IN CERTAIN AREAS:

- EFFECTIVE GROUNDING PATH
- GROUNDING ELECTRICAL CONDUCTOR REQUIREMENTS (E.G. SIZE AND MATERIAL)

PV SYSTEMS GROUNDING PHILOSOPHY SHOULD BE CHARACTERIZED BY:

- GROUNDING OF CONDUCTIVE ENCLOSURE OF ANY EQUIPMENT THAT IS INTERFACED WITH GROUNDED AC SYSTEM (DUE TO NEC REQUIREMENTS)
- GROUNDING OF ARRAY FRAME CONDUCTIVE MEMBERS
- METALLIC CONDUIT (IF USED) AND NON-UTILITY INTERFACING EQUIPMENT BE ISOLATED FROM GROUND
- UNGROUNDED CONDUIT ONLY ACCESSIBLE BY QUALIFIED PERSONNEL USING GROUND DETECTOR
- ISOLATION TRANSFORMER USED TO SEPARATE AC AND DC CIRCUITS
ENGINEERING AND OPERATIONS AREAS

NATIONAL ELECTRICAL CODE SUMMARY

WIRING

The major difference between residential and commercial/industrial sectors is the use of conductor protective enclosure, e.g., conduit. This is due to propensity for mechanical damage of unprotected conductors.

Factory installed internal wiring of equipment that is listed by an electrical testing laboratory is accepted for use by the NEC without needing to meet further NEC requirements. PV wiring design should consider this approach to accelerate acceptance, as the burden of interpretation is essentially removed from the code official.

Definite NEC requirements will apply if the wiring qualifies as a "service entrance conductor".

Conductor sizing should be based on individual system characteristics as well as related NEC requirements. This sizing criteria should include:

- Amperage of short-circuit "system" current & maximum insolation
- Number of conductors in a raceway or cable (NEC)
- Ambient temperature of conductor environment
- Material(s) of conductors
- Total system voltage drop (5% - NEC)
- Cost

Systems with voltages in excess of 600 volts will need to meet certain NEC requirements for:

- Service conductors entering a building (AWG No. 6 or No. 8 minimum)
- Limited access
ENGINEERING AND OPERATIONS AREAS

NATIONAL ELECTRICAL CODE SUMMARY

LIGHTNING

IN GENERAL THE NEED FOR LIGHTNING PROTECTION IS BASED ON THE FOLLOWING FACTORS:

- OCCUPANT SAFETY
- NATURE OF BUILDING AND CONTENTS
- RELATIVE EXPOSURE
- THUNDERSTORM FREQUENCY AND SEVERITY
- INDIRECT LOSSES
- AVAILABILITY OF FIREFIGHTING APPARATUS

TWO MAJOR CONSIDERATIONS FOR LIGHTNING PROTECTION FOR PV ARRAYS INVOLVE INDIRECT LOSSES RESULTING FROM VOLTAGE SURGES CAUSED EITHER BY DIRECT STROKE OR INDUCTION:

- FIRE RESULTING FROM ELECTRICAL EQUIPMENT OR CONDUCTOR INSULATION FAILURE
- SHOCK RESULTING FROM CONTACT WITH "HOT" EQUIPMENT ENCLOSURE OR UNINSULATED CONDUCTOR

THE TWO TECHNIQUES USED IN LIGHTNING PROTECTION SYSTEMS ARE "SHIELDING" AND "ARRESTING". THE SHIELDING METHOD INTERCEPTS THE STRIKE WHILE THE ARRESTING IS USED TO DRAIN DAMAGING HIGH POTENTIAL CURRENT TO GROUND. BOTH SHOULD BE USED ON PV SYSTEM.

SPACING OF THE PV SYSTEM FROM LIGHTNING TERMINALS DICTATES BONDING TO LIGHTNING SHIELD SYSTEM.

- NEC 250-46
- NFC SECTION 78 PARAGRAPH 3-24

LIGHTNING ROD CONDUCTORS CANNOT BE USED FOR PV SYSTEM GROUNDING

- NEC 250-86

NFC VOLUME 7 SECTION 78 ADDRESSES LIGHTNING PROTECTION SYSTEMS REQUIREMENTS.
ENGINEERING AND OPERATIONS AREAS

NATIONAL ELECTRICAL CODE SUMMARY

TERMINATION

WIRING TERMINATION REQUIREMENTS ARE NOT EXTENSIVELY ADDRESSED BY THE NEC.

CERTIFICATION BY A RECOGNIZED ELECTRICAL TESTING LABORATORY WOULD SUFFICE FOR ACCEPTANCE BY THE NEC. (IN MOST JURISDICTIONS)

FUNDAMENTAL TERMINATION REQUIREMENTS ARE:

- ADEQUATE CURRENT CAPACITY
- ADEQUATE ELECTRICAL INSULATION (VOLTAGE REQUIREMENT)
- LOW OMNIC CONTACT
- ADEQUATE WEATHERIZATION
- LOW LIFE-CYCLE COST

AT THIS POINT IN TIME, TESTING AND MAINTENANCE ACCESS IS IMPORTANT. WHEN RELIABILITY IS IMPROVED, AND IT IS FOUND THAT MEAN TIME BETWEEN FAILURE EXCEEDS MODULE LIFE, THEN THESE REQUIREMENTS SHOULD BE RECONSIDERED.

PERTINENT TEST STANDARDS PRESENTLY AVAILABLE FOR CONNECTORS:

- UL310 QUICK CONNECT TERMINALS
- UL486 WIRE CONNECTORS AND SOLDERING LUGS
- UL514 OUTLET BOXES AND FITTINGS
- MIL-STD-810-C ENVIRONMENTAL TEST METHODS
- MIL-STD-202, METHOD 107 ACCELERATED TEMPERATURE CYCLING
- ASTM D-1435-65 RECOMMENDED PRACTICE FOR OUTDOOR WEATHERING OF PLASTIC QUICK CONNECT TERMINALS. ALTHOUGH NOT SPECIFICALLY MENTIONED IN THE CODE, ARE A RECOGNIZED METHOD FOR MAKING ELECTRICAL CONNECTIONS. INDIVIDUAL QUICK CONNECTS MUST BE TESTED AND APPROVED BY A RECOGNIZED TESTING LAB. SOME MUNICIPALITY CODES DO NOT RECOGNIZE QUICK CONNECTS WHERE INSTALLATIONS ARE CONSIDERED TO BE PERMANENT.
<table>
<thead>
<tr>
<th>ENGINEERING AND OPERATIONS AREAS</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>DIMENSION (LENGTH) FT. IN.</strong></td>
</tr>
<tr>
<td><strong>MATERIAL</strong></td>
</tr>
<tr>
<td>PRECAST CONC.</td>
</tr>
<tr>
<td>GLASS REINFORCED CONC.</td>
</tr>
<tr>
<td>CONC. BLOCK</td>
</tr>
<tr>
<td>BRICK MASONRY</td>
</tr>
<tr>
<td>DOORS</td>
</tr>
<tr>
<td>WINDOWS</td>
</tr>
<tr>
<td>METAL PANELS</td>
</tr>
<tr>
<td>CORRUGATED IRON &amp; STEEL</td>
</tr>
<tr>
<td>PROTECTED METAL</td>
</tr>
<tr>
<td>ALUMINUM</td>
</tr>
<tr>
<td>CORRUGATED FIBERGLASS</td>
</tr>
<tr>
<td>COPPER</td>
</tr>
<tr>
<td>TITANIUM, COPPER, ZINC</td>
</tr>
<tr>
<td>STAINLESS STEEL</td>
</tr>
</tbody>
</table>

**Exterior Closure**

**Interior Construction**

**Roof Systems**

**Mechanical**

**Electrical**

(Absorbed by structural and roof systems)

(Absorbed by structural and flooring systems)

(Not a modular concern)
| Material                        | 5' | 6   | 8   | 9   | 10  | 12  | 14  | 16  | 18  | 20  | 22  | 24  | 25  | 28  | 30  | 35  | 40  | 45  | 50  | 60  | 80  | 100' |
|--------------------------------|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Exterior Closure (Walls)       |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Corrugated Iron & Steel        |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Protected Metal                |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Aluminum                       |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Asbestos                       |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Corrugated Fiberglass          |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Copper                         |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Lead                           |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Titanium, Copper, Zinc         |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Stainless Steel                |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Interior Construction          |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| 1st Conveying Systems          |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Precast Conc. Slabs            |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Metal Deck                     |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Short Span 1-1/2" Deep         |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Long Span 3 - 7-1/2" Deep     |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Steel Joists 12"               |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| 15"                            |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| 24"                            |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Conc. One Way Slabs            |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Conc. Beam & Slab              |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Flat Plate & Slab              |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Joist & Slab                   |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Waffle Slabs                   |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Conc. T'S (Single)             |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Conc. T'S (Double)             |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| 2nd Mechanical                 |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| Electrical                     |    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |

吸收于结构和屋顶系统。
LEAST LIFE-CYCLE ENERGY COST INTERCONNECT RELIABILITY DESIGN

JET PROPULSION LABORATORY
G.R. Mon

Overview

- **Problem:** Diurnal thermal cycles strain interconnects, which may lead to their eventual rupture and loss of array power output.

- **Goal:** Design module and interconnects not to exceed cost-optimal array power reduction after a specified number of years.

- **Approach:** Use design algorithm, presented here, incorporating:
  - Minimum life-cycle cost analysis
  - Interconnect structural analysis
  - Interconnect failure statistics

Cost-Optimal Interconnect Reliability Design Algorithm

[Diagram of the design algorithm]

432
Life-Cycle Energy Cost Analysis

EQUATION

\[
\text{ENERGY COST} \left( \frac{\$}{\text{kWh}} \right) = \frac{\text{BALANCE OF PLANT COST, } \$/\text{kw}}{\text{INITIAL ARRAY COST, } \$/\text{m}^2} + \frac{\text{ARRAY O&M COST, } \$/\text{m}^2}{\text{PLANT EFFICIENCY, } (100 \text{ mW/cm}^2, \text{ NOCT})}
\]

\[
\text{ANNUAL INSOLATION } \times \frac{\text{L-C ENERGY FRACTION}}{\text{kWh/m}^2/\text{yr}}
\]

METHOD

- DETERMINE ENERGY COSTS FOR VARIOUS 20-YEAR ARRAY POWER LOSS FRACTIONS AND INTERCONNECT REDUNDANCIES
- MINIMUM ENERGY COST DETERMINES DESIGN SELECTION

Strain Prediction Analysis

MODULE PROPERTIES:
- MATERIAL
- GEOMETRIC

CELL OPERATING TEMPERATURE ABOVE AMBENT \( \Delta T_{\text{OP}} \)

YEARLY AVERAGE CELL DIURNAL TEMPERATURE RANGE \( \Delta T \cdot \Delta T_{\text{OP}} \cdot \Delta T_D \)

YEARLY AVERAGE SITE DIURNAL TEMPERATURE RANGE \( \Delta T_D \)

CAP EXCURSION \( \Delta \)

FINITE ELEMENT COMPUTER CODE OR RELATED NOMOGRAPHS AND CHARTS

PREDICTED PEAK-TO-PEAK INTERCONNECT STRAIN \( \Delta e \)

- SEE D. MOORE'S PRESENTATION, THE "TIN CAN LID" PHENOMENON, AT THE 16th PIM
- CHARTS AND NOMOGRAPHS TO DETERMINE PREDICTED INTERCONNECT STRAIN ARE IN PREPARATION
ENGINEERING AND OPERATIONS AREAS

Allowable Strain Analysis

Array Power Loss

FROM 5101-167, SERIES/PARALLEL DESIGN WORKSHOP PROCEEDINGS
Cell Failure Probability Formula

\[ P_C = 1 - (1 - F_{SS})^{\frac{1}{n}} \]

- \( P_C \) \quad \text{CELL FAILURE PROBABILITY}
- \( F_{SS} \) \quad \text{SUBSTRING FAILURE PROBABILITY}
- \( n \) \quad \text{NUMBER OF PARALLEL INTERCONNECT GROUPS PER SUBSTRING (APPROXIMATELY EQUAL TO NUMBER OF CELLS PER SUBSTRING)}

EXAMPLE: 4 CELLS, \( n = 6 \)

Interconnect vs Cell Failure Probability
With Redundancy \( m \) as Parameter

\[ P_I = P_C^{1/m} \]

Graph showing \( P_I \) vs \( P_C \) with different levels of redundancy.
Interconnect Fatigue: Experimental Study

- OBJECTIVES
  - Understand interconnect failure probability behavior
  - Relate interconnect failure probabilities, strain levels, and array life

- APPROACH
  - Develop apparatus to mechanically simulate field thermal cycles (accelerated test)
  - Gather statistical failure data for several OFHC copper interconnect configurations
  - Develop strain-life (fatigue) curves for interconnects. Use strain prediction analysis to compute strain

Interconnect Strain-Cycle Apparatus
ENGINEERING AND OPERATIONS AREAS

Interconnect Configurations Tested to Date

Interconnect Strain-Cycle Test Data

![Graph showing failure probability vs. cycles for different configurations with parameters and symbols for S and T.]
ENGINEERING AND OPERATIONS AREAS

OFHC Copper Strain-Cycle (Fatigue) Curves

Manson's Empirical Curve: \( \Delta e = 1.33 \times 10^6 N^{-0.6} + 0.0070 N^{-0.12} \)

Reference: Manson, "Fatigue: A Complex Subject - Some Simple Approximations", EXPERIMENTAL MECHANICS, 7/65, pp. 193-213
ENGINEERING AND OPERATIONS AREAS

Superposition of Test Data Curves
And Failure Rate Determination

OBSERVATIONS

- WEAROUT FAILURE RATES EXHIBIT SMALL VARIABILITY; THEY ARE ESSENTIALLY THE SAME FOR ALL CASES TESTED.
- DEFECT-RELATED FAILURE RATES EXHIBIT LARGE VARIABILITY. A CONSERVATIVE ENVELOPE IS THEREFORE USED IN THIS REGION.
- INTERCONNECTS EXHIBITING EXTENDED REGIONS OF HIGH STRAIN (S-TYPE) ARE MORE PRONE TO DEFECT FAILURES.

WEAROUT FAILURES

\[ P_i = 0.3027 \cdot \log \left( \frac{N_p}{N} \right) + 0.5, \quad 0.03 < P_i < 0.5 \]

DEFECT FAILURES

\[ P_i = 1.4602 \cdot \log \left( \frac{N_p}{N} \right) + 0.5, \quad 0.5 < P_i < 1.0 \]
Interconnect Fatigue Curves With Failure Probability as Parameter

**CYCLES, N**

- **MANSON'S EMPIRICAL CURVE:** \( \Delta e = 1.3304 N^{-0.6} + 0.0070 N^{-0.12} \)

- CONSTANT PROBABILITY FATIGUE CURVES ARE DERIVED FROM MANSON'S CURVE USING FAILURE RATE FORMULAS OBTAINED IN THIS STUDY

- REALISTIC INTERCONNECT FAILURE PROBABILITIES \( (P_f < 0.30, \text{ SAY}) \) AT 20-YEAR ARRAY LIFE CONFINES THE DESIGN STRAIN TO VALUES AT OR NEAR THE "FATIGUE LIMIT" OF THE INTERCONNECT MATERIAL:
  \( \Delta e = 0.0025 \text{ TO } 0.005 \)

Interconnect Strain \( \Delta e \) vs Failure Probability \( P_f \) With Array Life (Years) as Parameter

- **YEARS**
  - 1
  - 2
  - 5
  - 10
  - 20
  - 25
  - 50
  - 100

**OPHC COPPER INTERCONNECTS**

440
Design Example: 1982 MTR Strawman

- ARRAY CONFIGURATION
  - OFHC COPPER INTERCONNECTS
  - 8 PARALLEL BY 11 SERIES CELLS PER SERIES BLOCK
  - 57 SERIES BLOCKS PER BRANCH CIRCUIT
  - 1 SERIES BLOCK PER DIODE
  - $V_{\text{ARRAY}} \cdot 250$ VOLTS

- DESIGN OBJECTIVES
  - 20-YEAR ARRAY POWER REDUCTION YIELDING MINIMUM LIFE-CYCLE ENERGY COSTS
  - REQUIRED INTERCONNECT REDUNDANCY

- ALLOWABLE STRAIN ANALYSIS

<table>
<thead>
<tr>
<th>20-YEAR ARRAY POWER REDUCTION $f$</th>
<th>SUBSTRING FAILURE PROBABILITY $F_{SS}$</th>
<th>CELL FAILURE PROBABILITY $P_C$</th>
<th>INTERCONNECT FAILURE PROBABILITY, $P_I$ FOR REDUNDANCY $m$</th>
<th>MAXIMUM ALLOWABLE STRAIN, $\Delta e$, FOR INTERCONNECT REDUNDANCY $m$</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.20</td>
<td>0.092</td>
<td>0.008735</td>
<td>0.0935</td>
<td>0.2059</td>
</tr>
<tr>
<td>0.10</td>
<td>0.055</td>
<td>0.005130</td>
<td>0.0716</td>
<td>0.1725</td>
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<tr>
<td>0.05</td>
<td>0.029</td>
<td>0.002672</td>
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<td>0.1388</td>
</tr>
<tr>
<td>0.01</td>
<td>0.0022</td>
<td>0.000200</td>
<td>0.0141</td>
<td>0.0585</td>
</tr>
<tr>
<td>0.001</td>
<td>0.00009</td>
<td>0.000008</td>
<td>0.0028</td>
<td>0.0200</td>
</tr>
</tbody>
</table>

- OBSERVATIONS
  - FOR A GIVEN INTERCONNECT REDUNDANCY, STRAIN LEVEL IS RELATIVELY INSENSITIVE TO ARRAY POWER REDUCTION, BUT SENSITIVITY INCREASES WITH INCREASING REDUNDANCY
  - FOR A GIVEN POWER REDUCTION, GREATER REDUNDANCY PERMITS HIGHER DESIGN STRAIN LEVELS; THE EFFECT IS MORE PRONOUNCED AT LARGER POWER REDUCTIONS, AT WHICH COST TRADE-OFFS BETWEEN STRAIN LEVEL AND REDUNDANCY CAN BE MADE
ENGINEERING AND OPERATIONS AREAS

- LIFE-CYCLE ENERGY COST ANALYSIS

\[
\text{ENERGY COST (\$/kWh)} = \frac{\text{BALANCE OF PLANT COST (\$/kWh)}}{\left(\frac{\text{INITIAL ARRAY COST, A} + \text{L-C O&M COST, } \epsilon_{\text{L}}}{\epsilon_{\text{LC}}} + \frac{\text{PLANT EFFICIENCY (100 mW/cm}^2, \text{ NOCT)}}{\text{ANNUAL INSOLATION (kWh/m}^2\text{yr)}}\right)}
\]

\[
(250) + \frac{0.092}{0.092} = \frac{(2000 \times \epsilon_{\text{LC}})}
\]


- ASSUMPTIONS

  △ 0% DISCOUNT RATE
  △ ARRAY COST LESS INTERCONNECTS: 113 \$/m²
  △ CONSTANT ARRAY POWER LOSS RATE: \( \epsilon_{\text{LC}} = \sum_{n=1}^{20} (1 - \frac{n}{20} \cdot f) \)

  \( f = 20\)-YEAR ARRAY POWER LOSS FRACTION

- CALCULATIONS

<table>
<thead>
<tr>
<th>20-YEAR ARRAY POWER REDUCTION f</th>
<th>INTERCONNECT REDUNDANCY m</th>
<th>ESTIMATED COSTS FOR INTERconnects $/m²</th>
<th>TOTAL INITIAL ARRAY COST $/m²</th>
<th>LIFE-CYCLE ENERGY COST $/kWh</th>
<th>LIFE-CYCLE ENERGY COST $/kWh</th>
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<tbody>
<tr>
<td>0.20</td>
<td>2</td>
<td>4.22</td>
<td>117.22</td>
<td>17.9000</td>
<td>0.043</td>
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<tr>
<td>0.10</td>
<td>2</td>
<td>4.22</td>
<td>117.22</td>
<td>18.9500</td>
<td>0.040</td>
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<tr>
<td>0.05</td>
<td>3</td>
<td>4.22</td>
<td>117.22</td>
<td>19.4750</td>
<td>0.039</td>
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<td>2</td>
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<td>118.05</td>
<td>19.8950</td>
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<td>0.0001</td>
<td>4</td>
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<td>0.039</td>
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<tr>
<td>0</td>
<td>∞</td>
<td>∞</td>
<td>∞</td>
<td>20.0000</td>
<td>∞</td>
</tr>
</tbody>
</table>

- COST-OPTIMAL DESIGN SELECTION

  - DESIGN FOR A POWER REDUCTION OF 1% AND AN INTERCONNECT REDUNDANCY OF 3
ENGINEERING AND OPERATIONS AREAS

PHOTOVOLTAIC MODULE CAPACITANCE AND PERSONAL SAFETY

JET PROPULSION LABORATORY
G.R. Mon

- OBJECTIVE
  - DETERMINE LIMITS ON MODULE CAPACITANCE TO GUARANTEE PERSONAL SAFETY DURING ROUTINE OPERATION AND MAINTENANCE FIELD REMOVALS AND REPLACEMENTS

- APPROACH
  - GATHER DATA ON HUMAN TOLERANCE TO ELECTRICAL SHOCK BY CAPACITIVE DISCHARGE
  - DETERMINE MAXIMUM ALLOWABLE MODULE UNIT CAPACITANCE AS A FUNCTION OF ARRAY OPERATING VOLTAGE
Factors Affecting Severity of Shock

- VOLTAGE
  - TYPE
    - AC
    - DC - CONTINUOUS OR INTERRUPTED
    - EXPONENTIAL DECAY
  - MAGNITUDE

- CURRENT
  - TYPE
  - MAGNITUDE
  - DURATION

- BODY IMPEDANCE
  - CURRENT PATH
  - PRESENCE OF MOISTURE

Human Physiological Response to Electric Shock

- AC - 60 Hz, 120 V (UL, USDL)

<table>
<thead>
<tr>
<th>I, mA</th>
<th>PHYSIOLOGICAL RESPONSE</th>
</tr>
</thead>
<tbody>
<tr>
<td>&lt; 0.5</td>
<td>NO SENSATION</td>
</tr>
<tr>
<td>0.5 - 2</td>
<td>THRESHOLD OF PERCEPTION</td>
</tr>
<tr>
<td>1 - 5</td>
<td>REACTION</td>
</tr>
<tr>
<td>2 - 10</td>
<td>MUSCULAR CONTRACTION</td>
</tr>
<tr>
<td>5 - 25</td>
<td>CAN'T LET GO</td>
</tr>
<tr>
<td>&gt; 15</td>
<td>STOPPAGE OF BREATHING</td>
</tr>
<tr>
<td>&gt; 25</td>
<td>SEVERE MUSCULAR CONTRACTION</td>
</tr>
<tr>
<td>30 - 200</td>
<td>VENTRICULAR FIBRILLATION</td>
</tr>
</tbody>
</table>

- DC

  DOES NOT PRODUCE SEVERE MUSCULAR CONTRACTIONS AS DOES AC.
  HIGHER DC LEVELS CAN BE TOLERATED
Electrical Impedance of the Human Body

- Measurement - 50 Hz, 125 V

![Diagram of the human body with electrical components]

- Suggested Working Values
  - DAMP: \( R_{\text{HUMAN}} = 500 \Omega \)
  - DRY: \( R_{\text{HUMAN}} = 1500 \Omega \)

Accepted and Suggested Human Tolerance Levels

- Voltage (1978 NEC)

<table>
<thead>
<tr>
<th>Wave Form</th>
<th>Dry</th>
<th>DamP</th>
</tr>
</thead>
<tbody>
<tr>
<td>AC</td>
<td>30 V RMS</td>
<td>15 V RMS</td>
</tr>
<tr>
<td>Interrupted DC</td>
<td>24.8 V PEAK</td>
<td>12.4 V PEAK</td>
</tr>
<tr>
<td>Continuous DC</td>
<td>60 V</td>
<td>30 V</td>
</tr>
</tbody>
</table>

- Current/Duration (UL)
  - Sinusoidal AC
    - 5 mA RMS is considered non-hazardous regardless of duration
    - From experiments on sheep and dogs,
      \[ I_{\text{MAX}} = 20t^{-0.7} \text{ mA RMS, } 0.00833 \text{ sec} < t < 7.25 \text{ sec} \]
      is safe
Minimum Fibrillating Current vs Shock Duration for Human Beings (After UL)

SHOCK DURATION TIME, sec

AC RMS CURRENT (mA)

I_{MAX SAFE} \cdot 201^{-0.7}

I_{MAX SAFE} \cdot 5 mA

SAFE

UNSAFE
ENGINEERING AND OPERATIONS AREAS

Accepted and Suggested Human Tolerance Levels (Cont.)

- **CAPACITANCE/VOLTAGE**
  - **CIRCUIT**
  
  ![Circuit Diagram]

- **EQUIVALENCE OF WAVE FORMS**
  It is assumed that the two wave forms shown produce the same effect upon the human heart.

- **MAXIMUM SAFE CAPACITANCE** \( R \cdot R_{HUMAN} = 500 \Omega \)
  
  \[ C_{SAFE}^{MAX} = \frac{0.0884}{V^{1.43} (\ln V - 1.26)}, \quad 3.5 \, V < V < 403.5 \, V \]

  \[ C_{SAFE}^{MAX} = 0.0353 \, V^{-1.536}, \quad 403.5 \, V < V < 40,000 \, V \]

- **VOLTAGES EXCEEDING 40,000 V ARE CONSIDERED UNSAFE REGARDLESS OF CAPACITANCE SIZE**
ENGINEERING AND OPERATIONS AREAS

Maximum Safe Capacitance at Voltage (UL)

- Voltage across capacitance before discharge (volts)
- Capacitance (C) in pF

Unsafe

Safe

Log-log scale with voltage on the y-axis and capacitance on the x-axis.
### Typical Measured Module Capacitance
And Insulation Resistance

<table>
<thead>
<tr>
<th>VENDOR - BLOCK</th>
<th>TYPE</th>
<th>( R_M ) (M( \Omega ))</th>
<th>( C_M ) (( \mu F ))</th>
<th>( C_M/A ) (( \mu F/m^2 ))</th>
<th>( \tau = 3 R_M C_M ) (sec)</th>
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<td>ST - II, III</td>
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- Module leakage resistance is so high that discharge currents will pass entirely through human.
- For some modules, charge bleed-off time can be quite large - several minutes.
Conclusions

- CHARGES STORED IN MODULES JUST EXTRACTED FROM AN ACTIVE ARRAY DO NOT POSE A SAFETY PROBLEM FOR PRESENT ARRAY DESIGNS (MODULE UNIT CAPACITANCES AND ARRAY VOLTAGE LEVELS)
Hot-Spot Study Objective

DEVELOP TEST PROCEDURES FOR EVALUATING HOT-SPOT ENDURANCE CAPABILITY OF A MODULE UNDER A SEVERE HOT-SPOT FIELD CONDITION:

- 100 mW/cm²
- 40 °C AIR
- MODULE AT SHORT CIRCUIT
- WORST-CASE CELL REVERSE I-V CHARACTERISTICS
- WORST-CASE CELL CURRENT MISMATCH
  - CRACKS
  - SHADOWING
  - INTERCONNECT FAILURE
  - SHORTED CELL

Secondary Study Objectives

- TO DETERMINE THE RELATIONSHIP OF $T_{\text{CELL}} - T_{\text{AIR}}$ vs HOT-SPOT POWER DISSIPATION (mW/cm²) FOR SEVERAL MODULE CONFIGURATIONS AND CELL SIZES

- TO CORRELATE ABILITY TO WITHSTAND HOT-SPOT HEATING WITH MODULE CONSTRUCTION AND CELL SIZE

- DEVELOP DESIGN GUIDELINES FOR MODULE AND CELL CONFIGURATIONS TO IMPROVE HOT-SPOT ENDURANCE
ENGINEERING AND OPERATIONS AREAS

Approach

• DETERMINE FACTORS AFFECTING HOT-SPOT HEATING LEVELS
• DEVELOP HOT-SPOT TEST PROCEDURES
• IDENTIFY AND/OR DEVELOP AND TEST REQUIRED EQUIPMENT AND INSTRUMENTATION
• INVESTIGATE CELL REVERSE VOLTAGE (2nd QUADRANT) I-V CHARACTERISTICS
• INVESTIGATE RESPONSE OF MODULES AND CELLS TO POWER DISSIPATION AND PERFORM SUPPORTIVE DIAGNOSTIC TESTS
• CORRELATE RESULTS AND DEVELOP RECOMMENDATIONS

Hot-Spot Test Considerations

FACTORs INFLUENCING HOT-SPOT HEATING LEVEL

• REVERSE VOLTAGE (2nd QUADRANT) CELL I-V CHARACTERISTICS
• MODULE SERIES-PARALLEL CONFIGURATION
• NUMBER OF CELLS PER DIODE STRING
• OVERALL MODULE CURRENT LEVEL
• AMOUNT OF CURRENT LIMITING IN AFFECTED CELL
• IRRADIANCE LEVEL

CRITICAL TEST CONSTRAINTS

• SELECTION OF CELLS WITH APPROPRIATE 2nd-QUADRANT I-V CHARACTERISTICS
• APPROPRIATE TEST VOLTAGE AND CURRENT SELECTION
• CONTROL DEGREE OF REVERSE BIASING BY MEANS OF ILLUMINATION LEVEL

• TEST CELL SELECTION AND INSTRUMENTATION
• DETERMINE CURRENT AND VOLTAGE TEST LEVELS
• ESTABLISH TEST THERMAL ENVIRONMENT
• EVALUATE PERFORMANCE

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Selection of Module Evaluation Criteria

- **SAFETY CRITERIA**
  - VISUAL INSPECTION: NO DETERIORATION THAT WOULD IMPAIR PERFORMANCE
  - HI-POI: SATISFY INITIAL ELECTRICAL ISOLATION REQUIREMENT

- **PERFORMANCE**
  - ELECTRICAL POWER $\geq 95\%$ OF PRETEST
Selection of Test Voltage and Current for Type A Cell

**Illumination Level Selected to Control Degree Of Reverse Biasing (Type A Cells)**

- **HIGH IRRADIANCE**
  - LOW POWER DISSIPATION

- **WORST-CASE IRRADIANCE**
  - MAXIMUM POWER DISSIPATION

- **LOW IRRADIANCE**
  - LOW POWER DISSIPATION
Selection of Test Voltage and Current for Type B Cell

Current

Selection of Test Thermal Environment
To Simulate 100 mW/cm², 40°C Field Condition

- Air Temperature - 20 °C, Still Air
- Irradiance -
  - Visible at selected level
  - IR to achieve pre-hot-spot cell and background temperature - NOCT

N - Number of Series Cells Per Diode

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ENGINEERING AND OPERATIONS AREAS

Selection of Test Sequence

SCHEDULE:

- POWER CYCLED ON-OFF
- 1 HOUR, POWER ON: HOT-SPOT HEATING
- POWER OFF: COOLING TO INITIAL THERMAL CONDITIONS (NOCT ± 5 °C)

DURATION:

- 100 HOURS ACCUMULATED HOT-SPOT POWER ON-TIME

Selection of Module Evaluation Criteria

- VISUAL INSPECTION:
  - MUST MEET PRODUCTION MODULE ACCEPTANCE REQUIREMENTS

- ELECTRICAL PERFORMANCE
  - ≥ 95% OF PRETEST POWER WITH ANY DISRUPTED INTERCONNECTS RECONNECTED

- ELECTRICAL ISOLATION
  - MUST MEET INITIAL HI-POT REQUIREMENT
ENGINEERING AND OPERATIONS AREAS

Hot-Spot Endurance Test Summary

- **TEST CURRENT** -
  - TYPE A: \( I_L \cdot I_{MP} \) OF AVERAGE CELL AT 100 mW/cm\(^2\), NOCT
  - TYPE B: \( I_L \cdot I_{SC} \) OF AVERAGE CELL AT 100 mW/cm\(^2\), NOCT

- **TEST VOLTAGE** -
  - \( V_T \leq V_L \cdot N \times V_{MP} \) (100 mW/cm\(^2\), NOCT) FOR N SERIES CELLS/DIODE

- **TEST CELLS** -
  - 3 SELECTED REPRESENTATIVE OF RANGE OF 2nd-QUADRANT I - V CURVES

- **THERMAL CONDITION** -
  - CELLS AT INITIAL TEMPERATURE - NOCT (IR SOURCE WITH LOW VISIBlE CONTENT)

- **ILLUMINATION** - (TYPE A ONLY)
  - UNIFORM SOURCE WITH LOW IR CONTENT (e.g., TYPE ELH)

- **LABORATORY AMBIENT** - 20 °C, NO AIR CURRENTS
Hot-Spot Endurance Test Equipment Arrangement
## Typical Hot-Spot Test Results

- Time to achieve equilibrium temperature
- Cell thermal gradients under test
- Measured cell temperature vs number of series cells per diode
- Hot-spot temperatures for field environment (predicted)
- Visual observations at increasing cell temperatures

### Characteristics of Modules Tested

<table>
<thead>
<tr>
<th>MODULE MFG</th>
<th>MODULE CHARACTERISTICS</th>
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<tr>
<td>SOLAREX</td>
<td>GLASS-FIBER-REINFORCED POLYESTER SUBSTRATE</td>
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<td>SYLGARD 184 ENCAPSULANT</td>
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<td>ALUMINUM FRAME</td>
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<td>CELL SIZE: 3 in.</td>
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<td>PHOTOWATT</td>
<td>ALUMINUM SUBSTRATE</td>
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<td>RTV 615 ENCAPSULANT</td>
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<td>ALUMINUM FINS</td>
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<td>PVB ENCAPSULANT</td>
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<td>SYLGARD 184 ENCAPSULANT</td>
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<td>CELL SIZE: 4 in.</td>
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<td>CELL SIZE: 2 in.</td>
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ENGINEERING AND OPERATIONS AREAS

Time to Reach Equilibrium Temperature

SOLAREX
CELL TYPE A

ARCO SOLAR
CELL TYPE B

SPECTROLAB
CELL TYPE B

Observed Module Response vs Cell Temperature

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<tr>
<th>MODULE MFR</th>
<th>100 °C</th>
<th>120 °C</th>
<th>140 °C</th>
<th>160 °C</th>
<th>180 °C</th>
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<td>SOLAREX</td>
<td>CELL BREAKDOWN</td>
<td>CRACKED CELL</td>
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<td>PHOTOWATT</td>
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<td>CELL BREAKDOWN</td>
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<tr>
<td>ARCO SOLAR</td>
<td>ONSET OF CARBONATION</td>
<td>CARBONATION OVER HALF OF CELL</td>
<td>ENCAPSULANT DISCOLORED AND SMOKING</td>
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<td>SOLAR POWER</td>
<td>MULTIPLE CELL CRACKS AND ENCAPSULANT DELAMINATION</td>
<td>ONE CELL SURVIVED TO 180 °C BEFORE CRACKING AND SMOKING</td>
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<td>SPECTROLAB</td>
<td>ONSET OF CARBONATION</td>
<td>CARBONATION OVER ENTIRE CELL AREA</td>
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Hot-Spot Temperature Above Ambient vs Power Into Cell (Field Environment)

![Graph showing Hot-Spot Temperature Above Ambient vs Power Into Cell (Field Environment)]
ENGINEERING AND OPERATIONS AREAS

Measured Hot-Spot Temperature vs Number of Series Cells per Diode

![Graph showing measured hot-spot temperature vs number of series cells per diode. The graph plots voltage (V) against cell temperature (°C) for different series cells/diode (N). Various manufacturers are labeled, including Solarex, Arco Solar, Solar Power, Spectrolab, and Photowatt.]
ENGINEERING AND OPERATIONS AREAS

Calculation of Expected Hot-Spot Temperature

- KEY MODULE AND CELL PARAMETERS
  4 in. cells, 103.2 cm² of area
  36 cells, 1 diode per module
  $V_{\text{MAXP(NOCT)}} = 0.42 \text{ V}$
  $I_{\text{SC}} = 2 \text{ A}$
  Type A cell
- $V_L = 15 \text{ V}$, $I_L = 2 \text{ A}$
- At 0 ILLUMINATION, CURRENT AT 15V IS 0.25 A

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<tr>
<th>CELL TEMPERATURE - LABORATORY ENVIRONMENT</th>
<th>20°C AIR TEMPERATURE</th>
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<td>$P_e$ (UNIT AREA)</td>
<td>30 W/103.2 cm² = 291 mW/cm²</td>
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<tr>
<td>$P_{ill} = I_L \times 100 \text{ mW/cm}² = 87.5 \text{ mW/cm}²$</td>
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<tr>
<td>$P_{ill}$</td>
<td>NOCT EQUIVALENT = 80 mW/cm²</td>
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<tr>
<td>$P_T = P_e + P_{ill}$</td>
<td>458.5 mW/cm²</td>
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<td>$T_{cell} = 120 \degree C$, $T_{cell} = 140 \degree C$</td>
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<th>CELL TEMPERATURE - FIELD ENVIRONMENT</th>
<th>40°C AIR TEMPERATURE</th>
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<td>$P_{ill}$</td>
<td>100 mW/cm² = 341 mW/cm²</td>
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<tr>
<td>$T_{cell} = 120 \degree C$, $T_{cell} = 140 \degree C$</td>
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Summary

- TEST PROCEDURES DEVELOPED
- EXPERIMENTAL VERIFICATION
- DETERMINATION OF MODULE AND CELL RESPONSE TO HOT-SPOT HEATING
- CRITICAL ASPECTS AND PROBLEM AREAS IDENTIFIED

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ENGINEERING AND OPERATIONS AREAS

Future Work

• CONTINUE INVESTIGATION OF CORRELATION OF MODULE AND CELL CONFIGURATION AND PHYSICAL PARAMETERS WITH HOT-SPOT HEATING ENDURANCE, AS NEW MODULES BECOME AVAILABLE

• REFINE TEST PROCEDURES AND ACCURACY BASED ON INDUSTRY RESPONSE AND FEEDBACK

• DEVELOP DESIGN GUIDELINES FOR HOT-SPOT ENDURANCE

• PREPARE TASK REPORT
PERCENT OF AR COATING MISSING

PERCENT DECREASE IN ELECTRICAL OUTPUT

Visually Estimated % of AR Coating Removed vs. Measured % Decrease in Isc and Pm for Lots G-14 and G-19 after 500 Hours Pressure Cooket
Spectral Distribution of Solar Radiation Received Outside the Atmosphere and at Sea Level

1976 CIE L*A*B Color Space
### Tristimulus Values

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<th>X (RED)</th>
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<td>1.5 - 10.5</td>
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ENG:NEERING AND OPERATIONS AREAS

New Cell Color Data

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<th>SPECTRAL DATA</th>
<th>WAVE</th>
<th>SAMPLE</th>
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SAMP: ILLUM=A OISUR=10
TRIST: X Y Z
SAMP 1.79 1.73 2.01
CHROMA: X Y
SAMP 0.3330 0.3133
COLOR COORD: L* A* B*
SAMP 14.04 -3.17 -25.29

Stressed Cell Color Data

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<th>WAVE</th>
<th>SAMPLE</th>
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<td>640</td>
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<tr>
<td>700</td>
<td>6.49</td>
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SAMP: ILLUM=A OISUR=10
TRIST: X Y Z
SAMP 8.08 7.30 3.03
CHROMA: X Y
SAMP 0.4370 0.3978
COLOR COORD: L* A* B*
SAMP 32.49 -0.75 -4.74

468
Data for Three Stress Levels X, Y, Z, and L Color Parameters vs. Percent Change in Isc.
### Stress Data - Group I Cells

**X, Y, Z, and L Color Parameters vs. Percent Change in Isc**

<table>
<thead>
<tr>
<th>Cell Number</th>
<th>0.1</th>
<th>0</th>
<th>2.5</th>
<th>5</th>
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<td>57</td>
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<td>58</td>
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</tr>
</tbody>
</table>

**Color Parameters**

- X
- Y
- Z
- L

**Percent Decrease in Isc**

470
ENGINEERING AND OPERATIONS AREAS

Conclusions (1 Cells)

- 3 - 7% DECREASE IN Isc (4 - 9% Pm)

- TOTAL % DECREASE IN Isc IS DUE TO MORE THAN JUST AR COATING LOSS

- POSSIBILITY OF RELATING FIELD RESULTS TO COLOR MEASUREMENTS
MINIMODULE ACCELERATED WEATHERING
DSET LABORATORIES, INC.
E. Zerlaut

Technical Approach

- **Real-Time Weathering**
- **Exposure of Micromodules on EMMA(QUA) Test Machines**
- **Long-term exposure of minimodules on SuperMag Test Machine (Equivalent to 10-20 years)**
- **Regular, periodic inspections and I-V measurements**

Objectives

- **Gain experience in the application of accelerated aging techniques to photovoltaic modules**
- **Accurately simulate encapsulation system designs of full-scale modules deployed in the field**
- **Provide a test bed for performing aging tests with samples which can be scaled to full size**
- **Obtain basis for correlation of accelerated degradation modes to real-time field experience**
ENGINEERING AND OPERATIONS AREAS

I-V Testing of Photovoltaics

- Reference cell preferred for measurement of $I_T$.
- If reference cell not same as test cell, global pyranometric measurement preferred.
- Direct normal "beam" measurement not desirable.
- DSET uses outdoor pulse method.
- IV data taken in 1 sec.

Pulse Testing in Direct Natural Sunlight

![Diagram of test setup](image)

SCAS = Solar Cell Array Scanner (Dynamic Load) ± 25 V/4Amps (100 watts)
SCAS Controller = Dynamic Load Ramp Generator
GP = Global Pyranometer
NIP = Normal Incidence Pyrheliometer

Houston (EG & G)
Digital X-Y Plotter
DATE: 07:20:29, SOLAR TIME: 09:50:00
DSET LABORATORIES, INC.
BOX 1850 BLACK CANYON STAGE
PHOENIX, ARIZONA 85029

DSET SP SYSTEM SOFTWARE VERSION 01A

NORMALIZED DATA

COMPANY: QUALITY CONTROL, INC
VOC: 4950.9 MV
INC: 365.9 MA
SERIAL #: SERIAL-001
V (OF MMD): 979.0 MV
T (OF MMD): 275.8 MA
T (AMB): 100.00 OF
P (SORI): 2950.0 MA

COMPUTER GENERATED
I-V PLOTS IN 3 QUAD
(QUAD I SCAN TIME ~ 1/2 SEC)
NORMALIZED TO 28°C
AND 1000 W/ M²
Degradation Modes That Have Correlated Well With Field Experience

- Cracked cells
- Delamination
- Encapsulant carbonation
- Glazing failure
- Contact corrosion
### Exposure Response History of Block II Modules to Super-MaQ Testing

<table>
<thead>
<tr>
<th>MODULE</th>
<th>SN</th>
<th>INITIAL</th>
<th>0.955</th>
<th>1.245</th>
<th>1.418</th>
<th>REMARKS</th>
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<tbody>
<tr>
<td>SILICONE RUBBER ENCAP., POLYESTER</td>
<td>021</td>
<td>1.43</td>
<td>1.34</td>
<td>1.28</td>
<td>1.27</td>
<td>YELLOWING OF INTERCONNECTS &amp; SUBSTRATE. MODERATE WATER SPOTTING</td>
</tr>
<tr>
<td>V&lt;sub&gt;oc&lt;/sub&gt;</td>
<td>6.71</td>
<td>6.93</td>
<td>6.59</td>
<td>6.53</td>
<td></td>
<td>SLIGHT DIRT RETENTION.</td>
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<tr>
<td>SUBSTRATE</td>
<td>024</td>
<td>1.48</td>
<td>1.37</td>
<td>1.31</td>
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<tr>
<td>V&lt;sub&gt;oc&lt;/sub&gt;</td>
<td>6.77</td>
<td>6.96</td>
<td>6.66</td>
<td>6.60</td>
<td></td>
<td></td>
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<tr>
<td>SILICONE RUBBER ENCAP., ALUMINUM</td>
<td>058</td>
<td>0.52</td>
<td>0.50</td>
<td>0.47</td>
<td>0.34</td>
<td>MODERATE DIRT RETENTION &amp; WATER SPOTTING. SLIGHT HAZE OF ENCAPSULANT.</td>
</tr>
<tr>
<td>V&lt;sub&gt;oc&lt;/sub&gt;</td>
<td>13.43</td>
<td>13.77</td>
<td>13.16</td>
<td>13.19</td>
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<td>TERMINAL DISCOLORATION.</td>
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<td>SUBSTRATE</td>
<td>13.44</td>
<td>13.42</td>
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<td>13.33</td>
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<tr>
<td>SILICONE RUBBER ENCAP., MOLDED POLYESTER SUBSTRATE</td>
<td>826</td>
<td>2.19</td>
<td>(TERMINATED 8/7/78)</td>
<td></td>
<td>EXTENSIVE DELAMINATION (SWELLING); CRACKED CELLS</td>
<td></td>
</tr>
<tr>
<td>V&lt;sub&gt;oc&lt;/sub&gt;</td>
<td>4.71</td>
<td>4.80</td>
<td>( &quot; &quot; )</td>
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<td></td>
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<tr>
<td>GLASS SUPERSTRATE, POLYMERIZED MOLDING</td>
<td>028</td>
<td>2.02</td>
<td>0.62</td>
<td>(TERMINATED 8/7/78)</td>
<td>SEVERE CARBONATION; CRACKED GLAZING, WHITE &amp; YELLOW HAZE EXTENSIVE</td>
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<tr>
<td>V&lt;sub&gt;oc&lt;/sub&gt;</td>
<td>5.04</td>
<td>4.80</td>
<td>( &quot; &quot; )</td>
<td></td>
<td>CARBONATION; SLIGHT WATER SPOTTING; YELLING OF INTERCONNECTS.</td>
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<tr>
<td>PVB/ MYLAR LAMINATE</td>
<td>042</td>
<td>2.03</td>
<td>1.81</td>
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<tr>
<td>V&lt;sub&gt;oc&lt;/sub&gt;</td>
<td>4.96</td>
<td>5.12</td>
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<td>EXP.</td>
<td>807</td>
<td>1,098</td>
<td>1,271</td>
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<td>EQUIVALENT YEARS =</td>
<td>.5</td>
<td>6-1/2</td>
<td>7-1/2</td>
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<td>YEARS</td>
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<tr>
<td>EXCEPT V =</td>
<td>4-1/4</td>
<td>5-3/4</td>
<td>6-3/4</td>
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<td>YEARS</td>
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</tbody>
</table>
I-V CHARACTERISTIC CURVE

DATE: 4-30-79
DSET #19260
MODULE: O58
EXPOSURE DATA: SUPER #3
FROM: 2-2-79 TO: 4-30-79
LANGLEY: 1,447,840
TEMP: 21.2°C
INTENSITY: 1074 W/m²
NORMALIZED Isc = 0.440 Voc = 13.33
I - V CHARACTERISTIC CURVE

DATE: 4-30-79
DSET # 19260

MODULE: 7.24

EXPOSURE DATA: SUPER MB
FROM: 1-2-79 TO: 4-30-79
LANGLEY: 1,459,960

TEMP: 28.1°C
INTENSITY: 1070 W/M²
NORMALIZED ISC = 1.365  VOC = 6.60
ENGINEERING AND OPERATIONS AREAS

DSEI LABORATORIES, INC.
BOX 1878 BLACK CANYON STAGE
PHOENIX, ARIZONA 85029

DATE: 01/09/81, SOLAR TIME: 10:34:00
DSEI SP SYSTEM SOFTWARE VERSION 01E

NORMALIZED DATA

<table>
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<tr>
<th>0.120</th>
<th>0.240</th>
<th>0.360</th>
<th>0.480</th>
<th>0.600</th>
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<tr>
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<td>8.00</td>
<td>12.00</td>
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ORIGINAL: $I_{sc} = 0.610$
$V_{oc} = 13.53$

AFTER 1,640,000 LANGLEYS
- CELL/ENCAPSULANT HAZE
- SLIGHT DARKENING OF METALLIZATION AND ENCAPSULANT

0.120
0.240
0.360
0.480
0.600

483
ENGINEERING AND OPERATIONS AREAS

DSET LABORATORIES, INC.
905 1850 BLACK CANYON STAGE
PHOENIX, ARIZONA 85029

DATE: 01/08/81, SOLAR TIME: 10:29:00
DSET SP SYSTEM SOFTWARE VERSION 01E

NORMALIZED DATA

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<tr>
<td>1/FCC</td>
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<td>VOC:</td>
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<td>1/FMT</td>
<td>20.9 °C</td>
<td>ISC:</td>
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<td>1/HP_MAX</td>
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<td>I (LP_MAX):</td>
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<td>1/MAX</td>
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<td>V (MAX):</td>
<td>5.170 V</td>
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ORIGINAL: I_sc = 0.619
V_oc = 13.46

AFTER 1,640,000 LANGLEYS
- SLIGHT CELL/ENCAPSULANT HAZE
- SLIGHT DARKENING OF ENCAPSULANT
  AND METALLIZATION
ORIGINAL: $I_{sc} = 1.37$
$V_{oc} = 6.43$

AFTER 1,640,000 LANGLEYS
- MODERATE CARBONATION
- SLIGHT HAZE
- DARKENING OF METALLIZATION

DSET LABORATORIES, INC.
BOX 1950 BLACK CANYON STAGE
PHOENIX, ARIZONA 85029

DATE: 01/08/81, SOLAR TIME: 10:44:00
DSET SP SYSTEM SOFTWARE VERSION 01E
ENGINEERING AND OPERATIONS AREAS

Conclusions

- Field failure modes have been duplicated
- Acceleration factors of 6x to 8x are attainable
- Test method is feasible as a predictive tool for PV lifetime durability assessment

SOLAR SPECTRAL MEASUREMENTS

DSET LABORATORIES, INC.

R. Whitaker

Scanning Spectroradiometer

- Materials Durability
- Energy Availability
- Site Specific Spectral Characteristics
- Efficient Data Acquisition, and Measurement Analysis
- Contract Essentials
ENGINEERING AND OPERATIONS AREAS

Capabilities

- Solar Spectrum 280 - 2500 nm

- Global Normal, Global Fixed, and Direct Normal
  Azimuth: ± 90°
  Elevation: Horizon to 90°

- Accuracy
  Intensity: Better than ± 5%
  Wavelength: Better than ± 1 nm

- Operation
  Measurement: 10 minutes
  Data Reduction: 30 minutes
  Outdoor/Indoor
  Transportable
DSET Spectroradiometer

Source Optics

SUN

D E

SUN

Slits, entrance

Leiss Double-Dispersion Monochromator

Slits, Exit

A Wavelength Encoder
B Chopper
C Detector Housing
D Pyrheliometer Comparison Tube
E Integrating Sphere

Analog Plotter

Synchro-Heterodyne Lock-in Amplifier

Line Printer

Nova 3D Computer

and/or

Micro-Nova Computer

A/D

Digital xy Plotter

Keyboard CRT
ENGINEERING AND OPERATIONS AREAS

Software

Read

Interface to and Control of Instrument Amplifier

Computational

Application of Calibration Values to Raw Signal Data

Formatting/Analysis

Data Scaling and Detector Data Combination, Band Irradiance Calculation

Presentation

Generation of Spectral Plots and Tabular Hardcopy

Magnetic Storage Archival

Calibration

- WAVELENGTH

5 LAMPS 185 - 1050 nm

ARGON
KRYPTON
NEON
XENON
MERCURY - ARGON

3 FILTERS

DIDYMUM - VIS/NEAR IR
HOLMIUM OXIDE - VIS/NEAR IR
TRICHLOROBENZENE - NEAR IR

- INTENSITY

NBS 1000 WATT QUARTZ IODINE LAMP
EPPLEY LABORATORIES (CAL./TRANS.)
250 - 2500 nm

214 DISCRETE CALIBRATIONS, 280 - 2500 nm
Solar Spectral Irradiance: New River, Arizona
(July 9, 1979)

Air Mass 1.05

A Global, normal incidence
B Direct beam, 6° fov
C Spectral bandpass
Hemispherical and Direct Spectral UV: New River, Arizona
(July 9, 1979)

(A) GLOBAL, NORMAL INCIDENCE
(B) DIRECT NORMAL (~ 6° FOV)

Air Mass: 1.05

WAVELENGTH, NM
ENGINEERING AND OPERATIONS AREAS

Spectroradiometer Total Spectrum Plot

DATE 11 IX 1980
MODE GLOBAL
TILT NORMAL
SOLAR TIME 13:54 - 14:04
GEOMETRIC AIR MASS CIRRUS
SLIT WIDTH 2 mm
SITE NEW RIVER
LATITUDE 30 DEG 50 MIN
LONGITUDE 112 DEG 10 W
ALTITUDE 2034 ft

ORIGIN OF POOR QUALITY
ENGINEERING AND OPERATIONS AREAS

Selected Band Energy Analysis

<table>
<thead>
<tr>
<th>DATE</th>
<th>11 IX 1980</th>
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<tbody>
<tr>
<td>NODE</td>
<td>GLOBAL</td>
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<tr>
<td>TILT</td>
<td>NORMAL</td>
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<tr>
<td>SOLAR TIME</td>
<td>13:54 - 14:04</td>
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<tr>
<td>GEOMETRIC AIR MASS</td>
<td>CIRROCUHULUS</td>
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<tr>
<td>SLIT WIDTH</td>
<td>.2 MM</td>
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<tr>
<td>SITE</td>
<td>NEW RIVER</td>
</tr>
<tr>
<td>LATITUDE</td>
<td>330 DEG 50 MIN</td>
</tr>
<tr>
<td>LONGITUDE</td>
<td>112 DEG 10' W</td>
</tr>
<tr>
<td>ALTITUDE</td>
<td>2034'</td>
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<table>
<thead>
<tr>
<th>WAVEBAND</th>
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<tbody>
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<td>TO</td>
</tr>
<tr>
<td>nm</td>
<td>W / cm²*²</td>
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<tr>
<td>280.000</td>
<td>315.000</td>
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<td>750.000</td>
</tr>
<tr>
<td>750.000</td>
<td>2500.000</td>
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Near-Term Future Capabilities

- **Increased Operational Efficiency**
  
  Measurement: 5 minutes
  Data Reduction: 15 minutes

- **Improved Accuracy**
  
  Increased intensity resolution, especially in ultraviolet
  Increased band