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Produced by the NASA Center for Aerospace Information (CASI)
DILUTION JET MIXING PROGRAM

PHASE I REPORT

by

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Garrett Turbine Engine Company
A Division of the Garrett Corporation

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The main objective of the NASA Dilution Jet Mixing Phase I Program was to quantify by means of parametric tests the effect of the following on the mixing of a row of jets with a confined cross-flow:

- Jet to mainstream density ratio
- Flow area convergence as encountered in transition sections.
- Non-uniform mainstream profile upstream of dilution orifices.

The general conclusions derived from Phase I work are:

- Jet spreading rate in transverse direction is increased with increasing J, H/D and with decreasing S/D.
- The density ratio has only a second order effect on the jet mixing characteristics for a constant momentum ratio.
- The temperature distributions in the jet mixing region are strongly influenced by the undisturbed mainstream profile. Therefore, a superposition of the mainstream profile on the correlations for isothermal mainstream conditions yields good agreement with data.
- Flow area convergence enhances mixing in radial and transverse directions. An asymmetric convergent duct with flat wall injection has the same jet mixing characteristics as a symmetric convergent duct. An asymmetric convergent duct with slant wall injection has a faster jet spreading rate in the transverse direction.
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<tr>
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<td>87</td>
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<tr>
<td>88</td>
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<td>147</td>
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<td>Title</td>
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1.0 SUMMARY

The main objective of the NASA Dilution Jet Mixing Phase I Program was to quantify by means of parametric tests the effect of the following on the mixing of a row of jets with a confined cross-flow.

- Jet to mainstream density ratio
- Flow area convergence as encountered in transition sections
- Non-uniform mainstream profile upstream of dilution orifices.

The general conclusions derived from Phase I work are:

- Jet spreading rate in transverse direction is increased with increasing J, H/D and with decreasing S/D.
- The density ratio has only a second order effect on the jet mixing characteristics for a constant momentum ratio.
- The temperature distributions in the jet mixing region are strongly influenced by the undisturbed mainstream profile. Therefore, a superposition of the mainstream profile on the correlations for isothermal mainstream conditions yields good agreement with data.
- Flow area convergence enhances mixing in radial and transverse directions. An asymmetric convergent duct with flat wall injection has the same jet mixing characteristics as a symmetric convergent duct. An asymmetric convergent duct with slant wall injection has a faster jet spreading rate in the transverse direction.
2.0 INTRODUCTION AND OBJECTIVES

Advanced aircraft propulsion gas turbine engines for civil and military applications must provide increased power density usually expressed in terms of thrust or horsepower per unit airflow. Higher cycle pressure ratio and turbine inlet temperature (TIT) offer the greatest potential for increasing engine performance and reducing engine weight and size. However, because of the higher average TIT, the gas temperature distribution must be closely tailored for acceptable radial temperature profile and minimal peak gas temperature.

The combustor discharge temperature quality is influenced by nearly all aspects of the combustor design and in particular by the dilution zone. Due to increasing burner inlet air temperature and fuel/air ratio, an increasingly higher fraction of the combustor through-flow air is needed for combustion and cooling with correspondingly reduced airflow available for dilution purposes.

An improved understanding of dilution jet mixing processes will result in effective utilization of the available dilution air. The present program has been undertaken to acquire a data base of dilution jet mixing characteristics to develop empirical jet mixing correlations and validate combustor analytical design models.

The penetration and mixing of air jets directed into a cross-stream have been investigated by many researchers. Jet trajectory and mixing models have been developed both empirically and analytically. In the majority of the studies, the models are not directly applicable to flows in gas turbine combustion systems due to either an inappropriate range of flow conditions or unrealistic test geometries. In almost all cases, correlations have been derived using single jets discharging into a uniform cross-flow in relatively large ducts. In gas turbine combustion systems, a
number of dilution orifices in single or multiple rows normally inject the cooler air into relatively small annular ducts with non-uniform flow fields, resulting in jet interaction with adjacent jets and the liner walls. The availability of experimental data to extend current jet mixing models to account for these factors is limited, which results in only qualitative application of the models by combustion engineers in actual design practice.

The work reported in References 1 through 4 for multiple-jet injection into a confined cross-stream provided the basis for the program reported here. The nominal cross-flow test conditions in those studies were: \( U_m = 15 \text{ m/sec} \); \( T_{\infty} = 600^\circ\text{K} \) with uniform temperature and velocity profiles. Dilution jet velocities \( (V_j) \) varied over the range of 25 m/sec to 35 m/sec with jets at an ambient temperature \( T_j = 300^\circ\text{K} \). The test conditions were established based primarily on jet to mainstream momentum ratio \( (J = \frac{\rho_j V_j^2}{\rho_m U_m^2}) \) variation from 6 to 60, with density-ratio \( (\rho_j/\rho_m) \) variation from 1.5 to 2.5.

Jet mixing correlations were developed (References 2 and 4) in terms of the momentum ratio and the following geometric variables:

\[ 2 \leq S/D \leq 6 \]  
\[ 4 \leq H_o/D \leq 16 \]  
\[ 0.25 \leq X/H_o \leq 2 \]  
\[ 0 \leq Z/S \leq 0.5 \]

- \( D \) = Dilution orifice diameter
- \( H_o \) = Channel height at injection plane
- \( X \) = Axial flow direction
- \( Z \) = Lateral flow direction
- \( S \) = Orifice spacing along the transverse direction
The main objective of the NASA Dilution Jet Mixing Phase I Program was to quantify the effect of the following factors on jet penetration and mixing:

- \( J, H_c/D, S/D, \rho_j/\rho_\infty \)
- Non-uniform cross-stream temperature and velocity main profiles upstream of dilution orifices
- Cold versus hot jet injection
- Cross-stream flow area convergence (accelerating cross-stream) as encountered in practical dilution-zone geometries.

The experimental effort was divided into four series of tests:

Series 1 test objectives were to evaluate current data in relation to previous data and correlations at comparable conditions for jet mixing in a uniform cross-stream and to compare mixing characteristics of a cold jet injected into a hot stream versus a hot jet injected into a cold stream.

The effects of mainstream velocity and temperature profiles on jet mixing processes were investigated in Series 2 test. Two types of cross-stream temperature profiles were studied. A profile generator was used to inject a cooler stream near the jet injector wall with an increasing temperature profile away from the injection wall. A decreasing radial temperature profile was used in the second set of investigations.

Dilution zone geometric details, including flow area convergence rate and shape (symmetric or asymmetric convergence),
affect jet penetration and downstream radial profiles. The effect of mainstream acceleration on jet mixing behavior was studied in Series 3 tests. Both symmetric and asymmetric converging test sections were used in this test series.

Practical dilution zone designs include both flow convergence and profiled cross-stream. A limited study was done in Series 4 tests on quantifying the effect of flow convergence as well as cross-stream profile on jet spreading.

In addition to the four test series described above, limited model validation and correlation were done based upon the extension of the correlations developed by Holdeman and Walker (Reference 2).
3.0 TEST RIG AND FACILITY DESCRIPTIONS

3.1 Test Rig

A schematic layout of the jet mixing test rig is presented in Figure 2 and a partially assembled rig in Figure 3. The mainstream airflow is ducted from the test cell main air supply through a 15.24-cm internal diameter pipe. A transition section connects the inlet pipe to a rectangular cross section of constant width (30.48 cm) and adjustable height.

A perforated plate with 25 holes of 1.43-cm diameter provides a relatively uniform airstream upstream of the profile generator plenum. The profile generator duct incorporates an adjustable bottom wall to match the test section inlet height, which can vary from 10.16 cm to 15.24 cm.

A separate air supply enables the profile generator to provide the desired radial profile of temperature and velocity upstream of the jet-injection plane.

A third air supply allows the dilution injection orifices to vary jet velocity and density. A number of interchangeable dilution orifice plates and test section geometries were used to study confined jet mixing with the mainstream. To minimize the rig heat losses, the rig walls were insulated with a 2.54-cm thick layer of Kaolite insulation.

In addition to a traversing $P_t/P_s/T$ rake, as shown in Figure 2, the rig instrumentation includes a number of wall static pressure taps and flow thermocouples.

A brief description of the profile generator, test sections, and dilution orifice plates is provided in the following paragraphs.
3.1.1 Profile Generator

A profile generator (Figure 4) provides a desired radial profile in the mainstream. This is achieved by varying independently the flow conditions of the approaching mainstream and the flow injected from the profile generator. As shown in Figure 2, a separate air supply is used to vary the temperature and velocity of the air supplied to the profile generator slot, which is 2.54-cm high and 29.2-cm wide. The slot is fed uniformly through an inclined perforated plate having 50 orifices of 1.47-cm diameter; these orifices can be seen in Figure 4. The supply-air duct dumps the air into a rectangular plenum (or settling chamber) of 30.48 x 16.75 x 12.7-cm dimensions.

Three wall static pressure taps and one thermocouple were used to control the plenum air pressure and temperature levels, which, along with the main supply flow condition, control the mainstream radial profile.

3.1.2 Test Sections

In the present study, jet mixing was characterized for four different test sections, as pictured in Figure 5; their important dimensional parameters are summarized in Table I. Both constant-height and variable-height test sections were investigated.

Test Section I has a constant channel height \( H_o = 10.16 \text{ cm} \) and slightly more than \( 2H_o \) length to allow radial profile measurements at \( X/H_o = 0.5, 0.75, 1.5, \) and \( 2.0 \).
<table>
<thead>
<tr>
<th>Test Section Number</th>
<th>Description</th>
<th>Test Section Height (cm)</th>
<th>Jet Injection Angle α (Degrees)</th>
<th>Test Section Convergence Rate $\frac{-dh}{dx}$</th>
</tr>
</thead>
<tbody>
<tr>
<td>I</td>
<td>Constant Height</td>
<td>10.16</td>
<td>90.0</td>
<td>0</td>
</tr>
<tr>
<td>II</td>
<td>Symmetric Convergence</td>
<td>10.16</td>
<td>97.1</td>
<td>0.25</td>
</tr>
<tr>
<td>III</td>
<td>Symmetric Convergence</td>
<td>10.16</td>
<td>97.1</td>
<td>0.25</td>
</tr>
<tr>
<td>IV</td>
<td>Symmetric Convergence</td>
<td>10.16</td>
<td>104.0</td>
<td>0.50</td>
</tr>
<tr>
<td>V</td>
<td>Asymmetric Flat-Wall Injection</td>
<td>10.16</td>
<td>90.0</td>
<td>0.50</td>
</tr>
<tr>
<td>VI</td>
<td>Asymmetric Inclined-Wall Injection</td>
<td>10.16</td>
<td>116.6</td>
<td>0.50</td>
</tr>
</tbody>
</table>

The same piece of hardware was used for Test Sections II and III, which are symmetrically converging with a wall inclination angle equal to 7.1 degrees. Consequently, the jet injection angle is 97.1 degrees. The test section flow area convergence rate (defined as $\frac{-dh}{dx}$) is 0.25. Test Section II exit-plane height is 5.08 cm at $X = 2 H_0$, and the corresponding injection to exit plane area ratio is 2.0. Test Section III is assumed to be 10.16-cm long with attendant exit-plane height of 7.62 cm and area ratio equal to 1.33.
Test Section IV is symmetrically converging with a convergence rate of 0.5; the corresponding inclination angle is 14.0 degrees for both top and bottom walls. Therefore, the jet injection angle is 104 degrees. The test section injection to exit plane area ratio is 2.0.

Test Sections V and VI are asymmetric with a convergence rate equal to that of Test Section IV. The bottom wall of Test Section V is horizontal and the top wall inclination is 26.6 degrees with an attendant jet injection angle of 116.6 degrees. By turning Test Section V, the top wall becomes flat (horizontal) and the jet injection angle becomes 90 degrees.

It should be noted that all test sections have a 10.16-cm channel height at the injection plane. Consequently, the inlet channel heights of the test sections range between 10.16 and 15.24 cm. To match the test section height, the profile generator section height was adjusted by means of a moveable wall.

To insure well-controlled boundary layer profile at the injection plane, a boundary-layer trip (0.41-cm high and 0.33-cm wide) was welded to all four walls of the test sections. The trip is located 15.24 cm upstream of the jet injection plane.

A number of static pressure taps are installed on all four walls of the test sections. As delineated in Figure 6 for Test Section I, a total of 32 wall statics are used to measure static pressure distribution. Four thermocouples (two thermocouples extending from the top wall and two through the bottom wall) are used for monitoring the mainstream gas temperature levels. These thermocouples are immersed 1.27 and 3.81 cm from the bottom and top walls, respectively.
3.1.3 Dilution Orifice Plate Geometry

Four circular orifice configurations, illustrated in Figure 7, were used on the present investigation. These plates are designated by 3-set numerals indicating aspect ratio, S/D, and H₀/D. The aspect ratio is unity for the circular orifices. Two orifice spacings (S/D = 2 and 4) were investigated. Similarly, two orifice sizes (D = 1.27 and 2.54 cm) were employed, producing H₀/D = 8 and 4, where H₀ (test section height at the injection plane) is equal to 10.16 cm. Table II gives important dimensions of the four dilution orifice plates used in the present study.

TABLE II. DESCRIPTION OF DILUTION ORIFICE PLATES

<table>
<thead>
<tr>
<th>Designation</th>
<th>Orifice Diameter, D (cm)</th>
<th>Number of Orifices</th>
<th>S/D</th>
<th>H₀/D</th>
<th>S/H₀</th>
</tr>
</thead>
<tbody>
<tr>
<td>01/02/04</td>
<td>2.54</td>
<td>6</td>
<td>2</td>
<td>4</td>
<td>0.50</td>
</tr>
<tr>
<td>01/04/04</td>
<td>2.54</td>
<td>3</td>
<td>4</td>
<td>4</td>
<td>1.00</td>
</tr>
<tr>
<td>01/02/08</td>
<td>1.27</td>
<td>12</td>
<td>2</td>
<td>8</td>
<td>0.25</td>
</tr>
<tr>
<td>01/04/08</td>
<td>1.27</td>
<td>6</td>
<td>4</td>
<td>8</td>
<td>0.50</td>
</tr>
</tbody>
</table>

3.2 Test Facilities

The test rig was installed in the combustion test cell, C-100. Three air supplies were used for setting up the required flow conditions for the mainstream, profile generator, and dilution jets. Nonvitiated air from the laboratory compressors and heaters was used throughout the present investigation.
The mainstream air temperature can be regulated from ambient to 725°K. A special preheater is used for obtaining air temperatures above 750°K. For the majority of the test cases the mainstream nominal temperature and flow rate were 644°K and 0.25 kg/sec, respectively. For the test cases involving hot jet injection the mainstream nominal temperature and flow rate were 310°K and 0.56 kg/sec, respectively. The mainstream temperature was measured by thermocouples located at the test section entrance. A standard ASME orifice section installed in a 15-cm inside diameter pipe was used for measuring the mainstream airflow rate.

A second, separately controlled air supply was used for the profile generator, which can be installed in either the top or bottom walls of the test rig. The mainstream profile was adjusted by varying the pressure drop across the profile generator and the attendant airflow rate. The airflow rate was measured by an ASME orifice in a 7.62-cm inside diameter pipe.

A third air supply was used for controlling the dilution jet flow conditions, including jet velocity and temperature. For a majority of test cases, the dilution jet air was at ambient temperature and therefore no external heater was required. For hot jet injection, an external heater supplied a nominal dilution air temperature of 450°K. The dilution airflow rate was measured by an orifice section in accordance with standard ASME airflow measurement procedures.
4.0 DATA ACQUISITION AND REDUCTION

4.1 Data Acquisition

The dilution jet mixing characteristics were determined by measuring temperature and pressure distribution within the test section at different axial stations. A traversing probe, shown in Figure 8, was used for this purpose.

The probe consists of a 20-element thermocouple rake surrounded by 20 total-pressure sensors on one side and 20 static-pressure rakes on the other side. The nominal transverse spacing between the thermocouple rake and the total pressure rake is 5.08 mm; similarly, the spacing between the thermocouple and the static pressure elements is 5.08 mm.

The center-to-center height of the probe is 9.35 cm. The first element is therefore located 4.05 mm from the top wall of the constant-height test section, i.e., 0.16 D for a 2.54-cm dilution jet diameter. All the elements are equally spaced in the vertical direction, providing a nominal spacing of 4.92 mm.

The total-pressure sensor elements are made of Inconel tubes with an outside diameter of 0.16 cm and a wall thickness of 0.023 cm. The internal conical design of the tube at the inlet provides a ±15 degree flow insensitivity angle. The static pressure tubes, similar to the total pressure sensors, are dead-ended with four bleeding holes of 0.03-cm diameter 90 degrees apart and 0.7 cm from the tip. The total temperature sensors are type K thermocouple wires with insulated junctions encased in 0.10-cm inside diameter tubes, supported by 0.21 cm inside diameter enveloping tubes. The insulated junction tubes exposed to the airstream are 0.76-cm long. All the sensing elements have a straight length of 1.52 cm or more before the first bend to the probe core.
where all tubes are inserted in a rectangular probe shield, 4.32 cm x 0.67 cm.

The probe is mounted on a traversing system (Figure 9) that allows travel in three directions. This system allows 30.48 cm traverse in the X-direction (mainstream flow direction) and 22.86 cm in the radial (Y) and lateral (Z) directions with an accuracy of ±0.015 percent. The flow field mapping in the Z direction is done over a distance equal to the hole spacing (S) for any given orifice plate. The measurements in the Z direction were made at the planes identified by Z/S = 0, 0.1, 0.2, 0.3, 0.4, 0.5, 0.6, 0.7, 0.8, 0.9, and 1.0, where Z/S = 0 denotes center of the orifice. The measurements in the X-direction were made at the planes X/H_o = 0.5, 0.75, 1.0, 1.5, and 2.0. The probe was traversed over a matrix of 11 x 5 survey locations.

The temperature and pressure values from the test rig instrumentation were recorded on magnetic tapes through a central computerized data acquisition system. An on-line data display system provided real-time information on selected raw data for monitoring the flow conditions. The raw data from the magnetic tape were later used for detail data reduction, analysis, and correlation.

4.2 Data Reduction

The rectangular grid network at which the measurements were made can be described with the aid of Figures 1 and 10. The X-axis is the axis along the length of the duct in the direction of the bulk flow. The X=0 station is located at the jet injection plane. The Y-axis (radial direction) is the direction along the jet injection direction. The Y=0 plane is located at the jet orifice exit plane. The Z-axis is in the cross-stream direction. The Z=0 plane is the vertical X, Y plane at a jet centerline. The
streamwise (X) and radial (Y) distances are nondimensionalized by \( H_o \), the channel height at the jet injection plane. The lateral distance, \( Z \), is nondimensionalized by \( S \), the dilution orifice spacing.

The measured gas temperature distributions are presented in a nondimensionalized form as:

\[
\theta(X, Y, Z) = \frac{T_m - T(X, Y, Z)}{T_m - T_j}
\]

where,

\( T_m \) or TMAIN = Mainstream stagnation temperature

\( T_j \) or TJET = Jet stagnation temperature

\( T(X, Y, Z) \) = Stagnation temperature at the point \((X, Y, Z)\) in the flow field.

\( \theta \) is a measure of the temperature change due to the jet at any point \((X, Y, Z)\) compared to the maximum possible temperature change. \( \theta \) can vary from 0.0 to 1.0. \( \theta = 0.0 \) when the local temperature equals the mainstream temperature and \( \theta = 1.0 \) when the local temperature equals the jet temperature. When the jet and the mainstream are perfectly mixed, the local temperature reaches ideal equilibrium temperature, \( T_{EB} \), given by

\[
T_{EB} = \left( \frac{\dot{m}_\infty T_\infty + \dot{m}_j T_j}{\dot{m}_\infty + \dot{m}_j} \right)
\]

The ideal equilibrium theta (\( \theta_{EB} \) or THEB) is defined as
This parameter, $\theta_{EB}$, provides a measure of the quality of the jet mixing. The arithmetic average temperature ($T_{av}$) at any X plane and the corresponding $\theta_{av} (\frac{T_m - T_{av}}{T_m - T_j})$ are also presented with the reduced data to provide the information on the average value of the temperature field at that plane.

The measured $\theta$ values are presented in three-dimensional (isometric) plots at each X-station. The measured $\theta$ values are also presented in the form of isopleths for each X-station for the purpose of detailed comparison with correlations. These plots are presented over a 2S span in the Z direction by assuming symmetry of the $\theta$ distribution with respect to the midplane between two orifices. This assumption was invoked only for the purpose of improving the clarity of visual presentation of the temperature distribution. The accuracy of this assumption depends upon the uniformity of flow distribution across the jet orifices. Preliminary tests were performed to ensure that the jet mass flow was uniformly distributed over the entire orifice plate configuration. The isometric plots provide a convenient means of presenting the jet trajectory and mixing. Furthermore, a comparison of the data and correlations is presented in a two-dimensional (2-D) plot of $\theta$ versus $Y/H_0$ along the jet centerplane at each of the $X/H_0$ stations.

The pressure recordings from the probe rake were used to compute the velocity $(V(X,Y,Z))$ at the point $(X,Y,Z)$. An interpolation scheme was used to compute the total pressure $(P_t)$ and static pressure $(P_s)$ values at the point where probe thermocouples are located. From these total and static pressures, a nondimensionalized velocity, $V(X,Y,Z)/V_j$, was computed. $V(X,Y,Z)$ is obtained from
\[ V(X,Y,Z) = \left[ 2 \left( P_t(X,Y,Z) - P_s(X,Y,Z) \right) / \rho(X,Y,Z) \right]^{1/2} \]

The jet velocity, \( V_j \), is calculated from

\[ V_j = \frac{4 \cdot m_j}{\left( \rho_j \cdot \pi \cdot D^2 \cdot C_D \right)} \]

where \( D \) is the orifice diameter, \( N \) is the number of orifices, \( \rho_j \) is the jet density \( (P_j/RT_j) \), and \( C_D \) is the orifice discharge coefficient.

The orifice discharge coefficients were determined by measuring the pressure drop across the orifice plate (without cross-flow) for a range of mass flow rates. The discharge coefficient, \( C_D \), was obtained from the relation

\[ \frac{\Delta P}{P} = 1.99 \left[ \frac{\dot{w}_C}{A \cdot C_D} \right]^2 \]

where, \( \dot{w}_C \) is the corrected flow rate in \( \text{lbm/sec} \) and \( A \) is the geometric area of the orifices in square inches.

Note: \( \dot{w}_C = \dot{w}_a \frac{\sqrt{\beta}}{\delta} \), \( \beta = \frac{T(\text{oR})}{517} \), and \( \delta = \frac{P(\text{psi})}{14.896} \)

The velocity vector in the vicinity of the jet injection plane is predominantly in the radial direction. In such regions, the velocity values obtained from the rake probe are not expected to be accurate. For the sake of brevity, the measured velocity distributions are not presented in this report. However, tables of nondimensional velocity distribution, \( V(X,Y,Z)/V_j \), will be provided for each test case in the Comprehensive Data Report (CDR) on this program.

An important parameter relevant to the jet description is the jet momentum ratio, \( J \), defined as
\[ J = \frac{\rho_j v_j^2}{(\rho_m v_m^2)} \]

where

- \( \rho_j \) = Jet density
- \( \rho_m \) = Mainstream density = \( \frac{P_m}{RT_m} \)
- \( V_j \) or VJET = Jet velocity at the orifice Vena Contracta
- \( V_m \) or VMAIN = Mainstream Velocity = \( \frac{m_m}{P_m A_m} \)

Other flow parameters of interest are:

- Blowing rate, M or BLORAT = \( \frac{\rho_j v_j}{\rho_m v_m} \)
- Temperature ratio, TRATIO = \( \frac{T_j}{T_m} \)
- Density ratio, DENRATIO = \( \frac{\rho_j}{\rho_m} \)
- Velocity ratio = \( \frac{V_j}{V_m} \)

The geometric parameters of importance associated with the orifice configuration are: \( S/D_j \) and \( H_o/D_j \), where \( D_j \) is the effective jet diameter defined by

\[ D_j = D \sqrt{C_D} \]

The quantities defined in this section define the geometric and flow conditions of each test and are reported along with the reduced data.
5.0 EXPERIMENTAL DATA

5.1 Series 1 Tests

The purpose of this series was to investigate penetration, radial, and lateral mixing characteristics of cold and hot dilution jets with an isothermal, confined cross-flow in a constant channel height of 10.16 cm. The main objectives of this series were the following:

- Comparison with the NASA/Aerojet data
- Relative mixing characteristics of cold versus hot jet injection.

A total of 12 data sets were taken with the orifice geometrical description and nominal flow conditions listed in Table III. Tests 1 through 8 were repeats of the cases selected from the Aerojet study to demonstrate reproducibility of the jet mixing data from two different rigs. Typical comparison of data from Aerojet and the present investigation is presented in Figure 11 for the jet centerline plane at three axial stations.

TABLE III. SERIES 1 TEST CONFIGURATIONS AND FLOW CONDITIONS

<table>
<thead>
<tr>
<th>Test No.</th>
<th>Orifice Dia(D) (cm)</th>
<th>B/D</th>
<th>H/Ho</th>
<th>Mainstream Velocity (m/sec)</th>
<th>Temp (°C)</th>
<th>Jet Velocity (m/sec)</th>
<th>Temp (°C)</th>
<th>Momentum Ratio</th>
<th>Density Ratio</th>
<th>Equilibrium Temp (°C)</th>
<th>Region of Axial Direction (D/Ho)</th>
<th>Measurements In Transverse Direction (D/H)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>2.54</td>
<td>2.0</td>
<td>4.0</td>
<td>15.8</td>
<td>645</td>
<td>26.0</td>
<td>308</td>
<td>5.7</td>
<td>2.11</td>
<td>0.176</td>
<td>0.5 - 2.0</td>
<td>0.0 to 1.0</td>
</tr>
<tr>
<td>2</td>
<td>2.54</td>
<td>2.0</td>
<td>4.0</td>
<td>16.3</td>
<td>651</td>
<td>21.6</td>
<td>308</td>
<td>6.1</td>
<td>2.12</td>
<td>0.107</td>
<td>0.5 - 2.0</td>
<td>0.0 to 1.0</td>
</tr>
<tr>
<td>3</td>
<td>2.54</td>
<td>4.0</td>
<td>4.0</td>
<td>52.2</td>
<td>304</td>
<td>26.7</td>
<td>304</td>
<td>6.1</td>
<td>2.17</td>
<td>0.191</td>
<td>0.5 - 2.0</td>
<td>0.0 to 1.0</td>
</tr>
<tr>
<td>4</td>
<td>2.54</td>
<td>4.0</td>
<td>4.0</td>
<td>52.2</td>
<td>304</td>
<td>26.7</td>
<td>304</td>
<td>25.3</td>
<td>2.13</td>
<td>0.169</td>
<td>0.5 - 2.0</td>
<td>0.0 to 1.0</td>
</tr>
<tr>
<td>5</td>
<td>1.27</td>
<td>4.0</td>
<td>4.0</td>
<td>51.9</td>
<td>308</td>
<td>25.3</td>
<td>308</td>
<td>25.3</td>
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<td>649</td>
<td>101.6</td>
<td>299</td>
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<td>102.2</td>
<td>445</td>
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(X/H₀ = 0.5, 1.0, and 2.0) for two values of jet momentum ratios (J = 6.1 and 26.7) with S/D = 4 and H₀/D = 4. The comparison, as shown for Tests 3 and 4, of data from two different rigs is quite good. Also shown in Figure 11 is the predicted racial profiles, using the NASA/Aerojet correlations.

The measured distribution of the nondimensionalized temperature, θ, for a momentum ratio (J) of 5.74 and uniform mainstream temperature, using the orifice plate 01/02/04 (S/D = 2, H₀/D = 4) is presented in Figure 12. The top part of this figure shows the isometric plot of the θ profiles at five axial planes of X/H₀ = 0.5, 0.75, 1.0, 1.5, and 2.0. The geometrical and flow parameters of interest are provided at the top of this figure. The bottom part of the figure shows the measured θ contours for the corresponding axial planes. The contour values were selected to cover the range of θ values observed in the test. One of the contour values selected is also the value equal to θₑᵇ, which is 0.1759 in this case. The locations of jet centerline and jet direction are indicated by the arrows at the top of each contour plot and in the isometric plots.

The mixing performance for any given configuration can be estimated from the deviation of θ distribution about θₑᵇ. A small deviation from θₑᵇ characterizes nearly complete mixing of the jet and the mainstream. The θₑᵇ value for Test 1 is 0.1759, which corresponds to Contour 3. θₑᵇ contours are deformed by the penetration of the jets. This deformation is gradually smoothed out farther downstream. The location of the jet centerline can be identified from the location of the largest contour value. For Test 1, at X/H = 0.5, the jet centerline is inside Contour 9, which is at Y/H = 0.34.

The spreading of the jets in the transverse direction can be determined from the smoothness of the contour shapes. For this test, the presence of the individual jets can be seen at X/H = 0.5
and the jets quickly merge beyond $X/H = 0.75$. The locations of the theta contour in the radial direction are not significantly different as $X/H_o$ increases beyond 1.0. From the $\theta$ profiles at $X/H_o = 2.0$ it can be seen that approximately the top half of the test section has an air temperature less than the equilibrium temperature, $T_{EB}$, whereas the bottom half has hotter gases. This indicates the jets have not penetrated the test section to the bottom wall.

The predicted theta distributions for Test 1 ($J = 5.74$, $S/D = 2$, $H_o/D = 4$) are presented in Figure 13. The predictions are obtained using NASA/Aerojet correlations. The top part of this figure shows the predicted theta contours while the bottom part provides a comparison between measured and predicted radial profiles of theta along the jet centerplane. Details of the NASA/Aerojet correlations are presented in Paragraph 6.1.

Although the predicted radial profiles are in good agreement with the measured theta profiles, significant differences in the theta contours can be observed. The predicted theta distributions for this test case underestimate the transverse spreading of the jets.

The measured theta distributions for Test 2 ($J = 21.59$, $S/D = 2$, $H_o/D = 4$) with uniform mainstream temperature ($T_m$) are presented in Figure 14. In this case, $\theta_{EB}$ is equal to 0.2705. The measurements show that for $J = 21.59$, the jet centerline at $X/H_o = 0.5$ is located at about $Y/H = 0.6$ compared to 0.34 for $J = 5.7$ (Figure 12). At $X/H_o = 0.5$, the two jets can be separately identified and they merge gradually as $X/H_o$ increases. The variation in the radial penetration of the jets with increasing downstream distance is insignificant. As in Test 1, there is a top cold and bottom-hot profile distribution.
The predicted theta distributions for Test 2 are portrayed in Figure 15. The agreement between the correlations and the data is good up to X/H₀ = 1.0. Beyond this station, some differences in the profiles are seen.

The measured data for Test 3, with uniform Tₘ, J = 6.14, S/D = 4 and H₀/D = 4, are presented in Figure 16. In this test case, the jets are located farther apart than the first two tests and θₑₑ = 0.1074. For a constant value of J, H₀/D, the effect of S/D on the jet mixing characteristics can be inferred by comparing Figures 12 and 16. For S/D = 4, the data clearly shows the presence of two separate jets at all the axial stations. If the half-width values (from the contours) are used, it can be seen that the jets begin to merge only at X/H₀ = 2.0, whereas Figure 12 shows that the merging is essentially complete at X/H₀ = 1.0. Spreading of the contours in the radial direction is significantly higher in Test 3 than in Tests 1 and 2. This demonstrates that an increase in S/D results in improving the radial mixing and decreasing the lateral spreading rate.

The predicted theta values for Test 3 are portrayed in Figure 17. The NASA/Aerojet correlations slightly underpredict the jet penetration and overpredict the θ_max for this configuration.

The measured results for Test 4 with uniform Tₘ, J = 26.7, S/D = 4, and H₀/D = 4 are provided in Figure 18. For this test condition with θₑₑ = 0.1915, data reveals the jets are impinging on the opposing test section wall. The mixing in both the radial and transverse directions is substantially enhanced farther downstream as compared to Test 2 with S/D = 2 (Figure 14).

An optimum dilution orifice spacing is quite important to achieving the desired radial profiles. The profiles from Test 2
(Figure 14) and Test 4 (Figure 18) clearly illustrate this importance. The amount of dilution air in Test 2 is approximately twice that of Test 4. At the same values of orifice diameter and J, Test 2 provided a hub-peak (hot near the bottom wall) profile, whereas in Test 4 a tip-peak profile was achieved.

The predicted results for Test 4 are presented in Figure 19. Initially the correlations underpredict jet penetration, but farther down, jet impingement is predicted to occur between 1.0 and 1.5 \( H_0 \). The predicted radial profiles are in good agreement with the data at \( X/H = 2.0 \).

In the next four tests, the effects of \( H_0/D \) parameters on the mixing characteristics were studied. In these tests, the jet orifice diameter was reduced to 1.27 cm and the channel height was unchanged. The resultant value of \( H_0/D \) was 8.

The measured theta distributions for Test 5 with uniform \( T_m' \), \( J = 25.32 \), \( S/D = 2 \), and \( H_0/D = 8 \) are presented in Figure 20. This orifice plate (01/02/08) is characterized by 12 closely spaced, small holes \( (D = 1.27 \text{ cm}) \) and a large duct height to diameter ratio. For this plate at a momentum ratio of 25.32, the data shows the jets have spread quickly in the transverse direction and no individual jet shapes can be identified even at \( X = 0.75 H_0 \). The gradual radial spreading of the contours demonstrates the slow radial jet spreading rate.

The predicted results for Test 5 are included in Figure 21. The predicted profiles are in good agreement with the data. The theta contour lines in both predicted and measured data are essentially horizontal, indicating the completeness of the mixing in the transverse direction. The predicted radial profiles are in very good agreement with the data in the entire mixing region of interest.
The data for Test 6 with uniform $T_m$, $J = 107.8$, $S/D = 2$, and $H_o/D = 8$ are depicted in Figure 22. As observed in the results for Test 5, the jet spreading in the transverse direction is nearly complete, even at $X/H_o = 0.5$ compared to 0.75 in the previous test with $J = 25$. The data shows that even for the high momentum ratio of 107.8, the jets do not impinge on the opposing wall. This results in bottom-hot profiles at all axial planes.

The predicted results for Test 6 are presented in Figure 23. The predicted profiles are in good agreement with the data up to $X/H = 1.0$. Beyond this station, the predictions show different trends compared to the data.

The measured data for Test 7 with uniform $T_m$, $J = 26.3$, $S/D = 4$, and $H_o/D = 8$ are portrayed in Figure 24. In this test, an orifice plate with six holes of 1.27-cm diameter was used. For this test condition, the data shows that at $X/H = 0.5$, the two jets are separately identifiable. The two jets spread in the transverse direction gradually as $X/H_o$ increases. The gradual spreading of the contours in the radial direction with increasing $X/H_o$ describes the radial mixing characteristics. The mixing characteristics for this orifice plate (01/04/08) are similar to that of orifice plate 01/02/04 (compare Figures 14 and 24) at the same momentum ratio, $J$.

The predicted results for Test 7 are presented in Figure 25. The predicted profiles are in good agreement with the data. With increasing hole spacing ($S$), the jet penetration is increased, as was shown previously for the 2.54-cm orifice diameter.

Figure 26 portrays the measured data for Test 8 with uniform $T_m$, $J = 109.0$, $S/D = 4$, and $H_o/D = 8$. For this momentum ratio, the data reveals that the jets impinge on the opposite wall at $X/H_o = 0.5$. The contour plots show significantly enhanced radial and transverse directions at stations farther downstream. It may be
recalled that for a comparable J value no impingement was observed with orifice plate 01/02/08, again indicating an increase in penetration with increasing S/D. The predicted results for Test 8 are presented in Figure 27. The predictions underestimate the jet penetration at X/Ho = 0.5 and 0.75. Jet impingement is predicted at X/Ho = 1.0, while the data shows jet impingement at X/Ho = 0.5. A similar trend was also observed for orifice plate 01/04/04.

The next four tests demonstrate the effect of density ratio. In these tests, a cold mainstream and hot jets were used. Tests were conducted with all four orifice plates and uniform mainstream temperature distribution.

Figure 28 portrays the measured data for Test 9 with heated jets at J = 31.0, S/D = 2, and H_o/D = 4. Comparison of these data with the results for cold jets at a comparable momentum ratio, J, and the same S/D and H_o/D (Figure 14) reveals very similar θ distributions.

The predicted results for Test 9 are presented in Figure 29. It is emphasized that the NASA/Aerojet correlations do not explicitly include the effects of density ratio since it was considered to be of second order in magnitude. However, the density ratio is taken into account in determining the nondimensional equilibrium temperature, θ_EB, which is used for predicting the theta distribution. Comparison between Figures 29 and 15 shows very nearly the same type of profiles. These comparisons reveal the effect of density ratio on the jet mixing characteristics is relatively weak.

Test 10 was performed with heated jets at J = 30.64, using orifice plate 01/04/04 (S/D = 4, H_o/D = 4). The measured theta distributions for Test 10 are depicted in Figure 30. For this case, jet impingement is observed at X/Ho = 1.0. At X/Ho = 0.5 and 0.75, the jets are separate. Beyond the point of impingement, an
enhanced mixing in radial as well as transverse direction is evident.

The predicted results for Test 10 are provided in Figure 31. The predicted profiles are in good agreement with the data. Comparison of this figure with Figure 19 shows that for a comparable momentum ratio, jet impingement on the opposite wall is observed with cold jets even at \( X/H_o = 0.5 \). However, the \( \theta \) profiles for hot and cold jet cases are very similar.

Figure 32 shows the data for Test 11 with hot jets, \( J = 30.19, S/D = 2, \) and \( H_o/D = 8 \). The jet spreading in transverse direction is faster compared to that in the radial direction.

The predicted results for Test 11 are presented in Figure 33. The predicted \( \theta \) profiles are in good agreement with the data although the predicted \( \theta \) values are slightly higher than the measured values. Notwithstanding this difference, which is of second-order magnitude, the correlations show the same nature of jet mixing characteristics as the data. The data for this case are very similar to the characteristics for cold jet injection (Figure 20).

The measured theta distributions for Test 12 with heated jets, \( J = 30.53, S/D = 4, \) and \( H_o/D = 8 \) are presented in Figure 34. The data shows the presence of two individual jets at \( X/H_o = 0.5 \). The two jets mix well with each other rapidly, and at \( X/H_o = 1.5 \), the mixing is nearly complete, as indicated by nearly horizontal contour lines. The radial jet spreading rate is slower compared to that in the transverse direction.

The predicted results for Test 12 are presented in Figure 35. The predicted profiles have the same shape as the data, and the predicted \( \theta \) values are slightly higher than the measured values. The \( \theta \) distributions for heated jets are quite similar to that for
cold jets, indicating a weak influence of density ratio on jet mixing characteristics.

The first 12 tests presented thus far cover the Series 1 tests. In analyzing these tests, the parameter, orifice spacing (S) to duct height (H) ratio, S/H, was considered only implicitly. For the orifice plate 01/02/08, S/H = 0.25, while S/H = 0.5 for orifice plates 01/02/04 and 01/04/08 and S/H = 1.0 for orifice plate 01/04/04. From the results presented in this paragraph (5.1), it is seen that the transverse or lateral mixing is enhanced as S/H decreases. Furthermore, the jet penetration is increased with increasing value of S/H. As reported in Reference 2, the coupling of J and S/H parameters is thus an important criterion for describing the jet penetration and mixing characteristics.

5.1.1 Conclusions for Series 1 Tests

The Series 1 tests were conducted with constant duct height and uniform cross-flow temperature distribution. Four different orifice plate geometries were used to study the jet mixing characteristics. From these test data, the following conclusions are made:

- A good agreement between the present data and previous data and correlations (References 1 through 4) has been obtained.

- The jet penetration distance ($Y_c/H_o$) increases with increasing momentum ratio (J) and orifice diameter (D).

- For a given duct height to diameter ratio ($H_o/D$), the lateral mixing, that is, the jet spreading rate in the transverse direction, is enhanced with increasing
momentum ratio, J, and decreasing spacing to diameter ratio, S/D.

- For a given S/D, the lateral mixing is increased with increasing J and H_o/D.

- The radial mixing, that is, the jet spreading rate in the vertical direction, is enhanced with increased jet penetration. This is highlighted in the case of jet impingement on the opposite wall.

- The penetration of a hot jet in a cold cross-flow is very similar to that of a cold jet in a hot cross-flow at constant J. Although the hot jet penetration is slightly smaller (less than 5 percent) than the cold jet penetration at X/H_o = 0.5, the differences are minimal farther downstream. The density ratio effects are, at best, of second-order magnitude and can be neglected for a first-order approximation, provided the momentum ratio values, J, are the same.

- The NASA/Aerojet correlations are accurate to first order and provide a useful tool for predicting the jet thermal centerline trajectory and temperature profiles. The temperature profiles are well described by the correlations except very close to the jet injection plane, especially when jet impingement occurs.

5.2 Series 2 Tests

The objective of this series of tests was to investigate the interaction of the jets with a non-uniform cross-flow temperature distribution in a constant area duct. A non-uniform mainstream temperature profile is generated by using the profile generator as
described in Section 3.0. Six tests were conducted in Series 2 with orifice geometries and nominal flow conditions as listed in Table IV.

**Table IV. Series 2 Test Configurations and Flow Conditions**

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Tests 13 through 16 were conducted with the mainstream temperature profile cold near the jet exit plane (top) and hot at the bottom of the duct. These test conditions are referred to as "top cold".

Tests 17 and 18 were conducted with an inverted temperature profile: hot at the top and cold at the bottom. These two test conditions are identified as "top hot".

The temperature profiles used for these six tests are depicted in Figure 36, in a nondimensionalized form, \( \theta_p \):

\[
\theta_p(y) = \frac{T_{max} - T_p(y)}{T_{max} - T_j}
\]

where

- \( T_{max} \) = Maximum value of the profiled mainstream stagnation temperature
- \( T_p(y) \) = Local value of the mainstream stagnation temperature upstream of the jet injector plane.
\[ T_j = \text{Jet stagnation temperature.} \]

The nondimensionalized temperature variable, \( \theta \), represents the ratio of the actual temperature change due to the dilution jets to the maximum possible temperature change for any given flow condition. Consequently, the value of \( \theta \) will always be between 0 and 1. For Series 2 tests, the maximum possible temperature change is \( (T_{\text{max}} - T_j) \). Thus, the definition of \( \theta \) is modified for the tests with profiled mainstream as

\[
\theta = \frac{(T_{\text{max}} - T)}{(T_{\text{max}} - T_j)}
\]

where \( T \) is the local temperature in the mixing region. To be consistent with this definition of theta, the NASA/Aerojet correlations were also modified. Details of the modifications are included in Paragraph 6.1.

The measured theta distributions for Test 13 with top cold profile, \( J = 22.63, \xi/D = 2, \) and \( H_o/D = 4 \) are presented in Figure 37. An extent of the radial and lateral jet spreading rates can be obtained from the distortion and spreading of the contours.

For Test 13, at \( X/H_o = 0.5 \), two distinct jets can be associated with the dip in the contours around the jet injection locations. However, at \( X/H_o = 1.0 \) and farther downstream, the contour lines tend towards a horizontal line, indicating a tendency towards complete lateral mixing. It is also interesting to note that once the contour lines become nearly horizontal, the spreading in the radial direction is enhanced.

Figure 36 portrays the predicted theta distributions for Test 13. The predicted results were obtained by superposing the mainstream theta profile, \( \theta_p(Y) \), on the NASA/Aerojet correlations.
for uniform mainstream temperature. Detailed descriptions of these correlations are provided in Paragraph 6.1. The predicted theta profiles are not in good agreement with the data, although they show the same qualitative profiles. This suggests that the superposition method is perhaps valid if a suitable scaling parameter is employed for the profiled mainstream theta, \( \theta_p(Y) \).

The measured theta distributions for Test 14 with top cold profile, \( J = 7.5 \), \( S/D = 4 \), and \( H/D = 4 \) are presented in Figure 39. In these figures, the modulation of the \( \theta \) contours around the location of the jets is evident. Comparison of these figures with those in Figure 37 shows a substantial reduction in both lateral and radial mixing. This is largely due to the lower \( J \) value and a higher \( S/H_o \) ratio.

The predicted theta distributions for Test 14 are presented in Figure 40. The predicted profiles seem to overestimate the lateral mixing, while the jet centerplane radial profiles are in qualitative agreement with the measured profiles. It is also interesting to note that the major part of the differences between the data and correlations is in the region where the profiled mainstream temperature is cold (near the top for this test case).

The data for Test 15 are depicted in Figure 41. This test was conducted with top cold profile, \( J = 109.9 \), \( S/D = 2 \), and \( H_o/D = 8 \). The \( \theta \) contours are nearly flat, even at \( X/H_o = 0.5 \), indicating a high lateral mixing. The gradual movement of the contour locations toward the top wall provides an idea of the relatively slow jet spreading rate in the radial direction. The dominance of the mainstream profile is clearly seen in the isometric plots.

The predicted results for Test 15 are portrayed in Figure 42. The predicted contours are horizontal lines, indicating the high lateral mixing rate. The radial profiles between the data and correlations are again in qualitative agreement.
Figure 43 depicts the measured theta distributions for Test 16, with top cold profile, $J = 22.55$, $S/D = 4$, and $H_o/D = 8$. At $X/H_o = 0.5$, the $\theta$ contours are modulated by the jet and these distortions are gradually smoothed out farther downstream. The spread of the contours in the radial direction is gradual, indicating a slow radial mixing rate.

The predicted results for Test 16 are presented in Figure 44. The radial profiles are in good agreement near the bottom and in qualitative agreement near the top. This trend was also noted in Tests 13 through 15.

The next two tests were conducted with an inverted mainstream temperature profile, namely, hot at the top and cold at the bottom. Figure 45 portrays the measured results for Test 17 with top hot mainstream temperature profile, $J = 22.14$, $S/D = 2$, and $H_o/D = 4$. The isometric plots show the dominance of the profiled mainstream. At $X/H_o = 0.5$, the distortion of the $\theta$ contours around the jet injection indicates the extent of jet penetration. These distortions are smoothed out at $X/H_o = 1.5$. The radial mixing characteristics are seen from the relatively rapid changes in the contour locations in the radial direction.

Figure 46 portrays the predicted theta distributions for Test 17. The predicted profiles are in good agreement with the data, especially at $X/H_o = 0.5$. It is also interesting to note that the differences in the profiles between data and correlations are more pronounced in the colder part of the duct (near the bottom in this test case).

The measured theta distributions for Test 18 with top hot mainstream temperature profile, $J = 27.69$, $S/D = 4$, and $H_o/D = 8$ are presented in Figure 47. As observed in the previous test case,
the lateral mixing appears to be rapid. The dominance of the profiled mainstream on the theta distribution throughout the mixing region is seen clearly in the isometric plots.

Figure 48 presents the predicted theta distributions for Test 18. The predicted profiles are in good agreement with the measurements, especially at stations closer to the jet injection plane \((X/H_o = 0.5 - 1.0)\).

5.2.1 Conclusions for Series 2 Tests

Series 2 tests consisted of six tests with constant height duct and profiled mainstream temperature distribution. The mainstream temperature profiles employed included both top cold and top hot profiles. Four orifice plate configurations were used to study the jet mixing characteristics. The following conclusions are made from these tests:

- A new definition for nondimensional temperature, \(\theta\), is needed for analyzing the jet mixing characteristics.
- The jet spreading characteristics with profiled mainstream are very similar to those with uniform mainstream temperature profile.
- The radial temperature profiles in the mixing region are strongly influenced by the mainstream profiles upstream of the jet injection plane.
- The superposition procedure used for modifying the NASA/Aerojet correlations is reasonably good. This is seen from the good qualitative agreement between the data and correlations. Some of the differences in the
agreements may be due to the distortion of the mainstream temperature profile downstream of the jet injection plane. These differences between correlations and data can be reduced by using an appropriate scaling parameter on the superposition scheme employed.

5.3 Series 3 Tests

The objective of the Series 3 tests was to investigate the penetration and mixing characteristics of cold dilution jets injected into an isothermal cross-flow in a converging duct. These tests can be divided into two segments based upon the geometry of the convergent ducts:

- Symmetric convergence (Test Sections II and IV)
- Asymmetric convergence (Test Sections V and VI)

For each of the test sections, two orifice plates (01/02/04 and 01/04/08) were used, and two momentum ratios were selected for each orifice plate. A total of 16 tests were performed in Series 3 with orifice geometrical description and nominal flow conditions as listed in Table V. Tests 19 through 26 were conducted with symmetrical convergence, and Tests 27 through 34 were conducted with an asymmetrically convergent test section. All the convergent test sections used in these tests (shown in Figure 5) have the same area ratio, $A_o/A_{\text{min}} = 2$, where $A_o$ is the duct area at the jet injection plane and $A_{\text{min}}$ is the minimum area of the duct. The results for symmetric convergence are presented in Paragraph 5.3.1 and for asymmetric convergence in Paragraph 5.3.2.

5.3.1 Symmetric Convergence Test Sections

The two symmetric convergence test sections used in these tests were Test Sections II and IV. (See Figure 5.) Uniform
mainstream temperature and velocity profiles were generated at the jet injection plane. All these test sections have a duct height ($H_0$) of 10.16 cm at the jet injection plane.

Test Section II is a symmetrically convergent duct with channel height reduction from 10.16 cm (4 in.) to 5.08 cm (2 in.) over a length of 20.32 cm (8 in.). Test Section IV has a channel height reduction from 10.16 cm (4 in.) to 5.08 cm (2 in.) over a length of 10.16 cm (4 in.).

Since the Series 3 tests were performed with uniform mainstream temperature profiles, the definition of theta needed for analyzing these data is identical to those used in Series 1, namely,

$$\theta = \frac{T_m - T}{T_m - T_j}$$
The measured theta distributions for Test 19 with Test Section II, $J = 27.09$, $S/D = 4$, and $H_o/D = 8$ are portrayed in Figure 49. For Test Section II, the jet injection angle is 97.1 degrees and measurements were made at four axial planes. For orifice plate 01/04/08, the measurements were taken at $X/H_o = 0.25, 0.5, 1.0$, and 2.0. Figure 49 shows the presence of two distinct jets at $X/H_o = 0.25$ and 0.5. At $X/H_o = 1.0$, the two jets begin to diffuse with each other and at $X/H_o = 2$, the contour lines are almost horizontal, indicating nearly complete mixing in the lateral direction.

Comparison of Figures 49 and 24 reveals the effect of convergence on the jet mixing characteristics. These two figures correspond to the same orifice configuration at a comparable momentum ratio. For both cases, the jet centerline is located at about 50 percent of local channel height at $X/H_o = 0.5$ and 1.0. The jet spreading rate in the radial direction is significantly faster in the convergent duct than in the constant area duct. The jet spreading rates in the transverse direction for the two cases are nearly the same.

The predicted theta distributions for Test 19 were obtained by modifying the NASA/Aerojet correlations for a convergent duct. In a convergent duct, the local mainstream velocity, $V_m(X)$, increases with $X$ according to the relation

$$\frac{V_m(X)}{V_o} = \frac{A_o}{A(X)}$$
where $A_o$ is the duct cross-sectional area at the jet injection plane, $A(X)$ is the local duct cross-sectional area, and $V_o$ is the mainstream velocity at the jet injection plane. For low Mach numbers, the density variation with $X$ can be neglected. Thus, the equivalent momentum ratio at any axial station can be expressed as:

$$J_{eq} = \frac{P}{J_0} = \frac{\rho_j V_j^2}{\rho_m V_m^2(X)} = \frac{\rho_j V_j^2}{\rho_m V_o^2} \frac{V_o^2}{V_m^2(X)}$$

Thus,

$$J_{eq} = J_0 \left( \frac{A(X)}{A_o} \right)^2$$

where $J_0$ is the momentum ratio at the jet injection plane. Predictions for convergent ducts were obtained by using the equivalent momentum ratio, $J_{eq}$, in the NASA/Aerojet correlations. These results are presented in Figure 50 for Test 19. The predicted radial theta profiles are in very good agreement with the data at $X/H_o = 0.25$ and 0.5. The agreement between data and correlations is qualitatively good at $X/H_o = 1.0$ and $X/H_o = 2.0$. The accelerating flow in the convergent duct enhances mixing in radial and transverse directions. Although the correlations correctly predict the jet penetrations, the enhanced mixing due to convergence is not properly taken into account.

Figure 51 illustrates the measured theta distributions for Test 20 with Test Section II, $J = 102.5$, $S/D = 4$, and $H_o/D = 8$. For this condition, the jets impinge on the opposite wall even at $X/H_o = 0.25$, followed by a rapid mixing in the transverse direction. The theta distributions for this case are similar in characteristics to those with constant area duct. (See Figure 26.)

The predicted results for Test 20 are presented in Figure 52. The predicted profiles are in very good agreement with the data at
X/H₀ = 1.0 and 2.0. In regions closer to the jet injection plane, the jet penetration is underpredicted. It is recalled that even in Series 1 test cases, the NASA/Aerojet correlations underpredicted the jet penetrations for high momentum ratios.

The measured theta distributions for Test 21 are shown in Figure 53. Test 21 was performed with Test Section II, J = 6.7, S/D = 2, and H₀/D = 4. For this orifice plate, measurements were taken at X/H₀ = 0.5, 0.75, 1.0, and 2.0. At the momentum ratio of 6.76, the jets penetrate to about Y/H = 0.4 at X/H₀ = 0.5 and gradually diffuse in radial and transverse directions. The radial mixing rates in this case are slightly faster than that with uniform duct height at the same momentum ratio. (See Figure 12.)

The predicted results for Test 21 are presented in Figure 54. The predicted theta profiles are in good agreement with the data at X/H₀ = 0.5. Beyond this station, the predicted theta values are slightly larger, but the shapes of the θ profiles are correctly predicted.

The measured theta distributions for Test 22 with Test Section II, J = 26.07, S/D = 2, and H₀/D = 4 are illustrated in Figure 55. For this momentum ratio, the jet penetration is about 60 percent of the local duct height at X/H₀ = 0.5, the jets gradually diffuse deeper, and at X/H₀ = 2.0, the jet centerline is located near Y/H = 1.0.

The predicted theta values for Test 22 are portrayed in Figure 56. The predicted radial profiles are in good agreement with the data, especially in regions close to the jet injection plane. The predicted theta values are slightly higher than the measured values although the profile shapes are correctly predicted.

The next four test cases correspond to the measurements taken with Test Section IV. The measured theta distribution with Test
Section IV, $J = 21.07$, $S/D = 4$, and $H_o/D = 8$ are presented in Figure 57. At $X = 0.25$, two separate jets are observed which rapidly diffuse in the lateral direction. For Test Section IV, the jets are injected at an angle of 104 degrees. The upstream component of the jet momentum tends to enhance the mixing in both radial and transverse directions.

Comparison of Figures 57 and 49 shows the effects of different convergence rates. For Test Section IV, at $X/H_o = 1$, the area ratio, $A_o/A$, is 2.0. For Test Section II, at $X/H_o = 1$, the area ratio, $A_o/A$, is 1.33. With increasing convergence rate (area ratio), jet penetration is also increased. Furthermore, the lateral jet spreading rate is increased with increasing area ratio.

The predicted results for Test 23 are presented in Figure 58. The predicted distributions are at best in qualitative agreement with the data. The correlations underpredict the jet penetration. Some of these differences are due to the effects of jet injection angle, which are neglected in the correlations. Furthermore, the predicted theta values are slightly higher than the measured values.

The measured theta distributions for Test 24 with Test Section IV, $J = 85.84$, $S/D = 4$, and $H_o/D = 8$ are presented in Figure 59. For this momentum ratio, the jets impinge on the opposite wall, followed by an enhanced lateral mixing. Figure 60 illustrates the predicted theta profiles for Test 24. The predicted profiles are in poor agreement with the data. The correlations underpredict the jet penetration.

The measured theta values for Test 25 with Test Section IV, $J = 6.73$, $S/D = 2$, and $H_o/D = 4$ are shown in Figure 61. For the low momentum ratio of 6.73, the jets penetrate up to about 40 percent of the local channel height. The mixing in the transverse direction...
is very slow, as evidenced by the contour shapes. The predicted results for Test 25 are portrayed in Figure 62. For this case, the correlations overpredict the penetration and the predicted theta values are significantly higher than the measured values.

Comparison of Figures 61 and 53 shows that the mixing characteristics for Test Section IV are very similar to that of Test Section II.

The data for Test 26 with Test Section IV, J = 26.73, S/D = 2, and H₀/D = 4 are illustrated in Figure 63. In this case, the jets penetrate up to about 65 percent of the channel height at X/H₀ = 0.5 and gradually reach the bottom wall at X/H₀ = 1.0. The individual jet contours are clearly seen until the jet centerline reaches the opposing wall. The predicted results for Test 26 are presented in Figure 64. The predicted profiles are in good qualitative agreement with the data. The predicted theta values are higher in magnitude compared to the measured theta values. The jet mixing characteristics for this case are very similar to those with Test Section II. (See Figure 55.)

5.3.2 Asymmetric Convergence Test Sections

The following eight tests (Tests 27 through 34) were performed with asymmetric Test Sections V and VI. Test Section V is a duct with rectangular cross-section with a flat wall on one side and a slant wall on the opposite side, such that the channel height reduces from 10.16 cm (4 in.) to 5.08 cm (2 in.) over a length of 10.16 cm (4 in.). The jets are injected from the flat wall (jet injection angle is 90 degrees).

Test Section VI has the same geometry as Test Section V, but the jets are injected from the slant wall. The geometry of the test sections is illustrated in Figure 5.
The tests with asymmetric converging ducts were performed with orifice plates 01/02/04 and 01/04/08, with two momentum ratios for each orifice plate as listed in Table V. Measurements were made at X/H_o = 0.25, 0.5, and 1.0 with orifice plate 01/04/08 and at X/H_o = 0.5, 0.75, and 1.0 with orifice plate 01/02/04.

The measured theta distributions with Test Section V, J = 27.18, S/D = 4, and H_o/D = 8 are portrayed in Figure 65. At X/H_o = 0.25, the jet centerline penetration is at about Y/H = 0.5 and the jet gradually penetrates farther with increasing X/H_o, but does not reach the opposite wall.

Figures 57 and 65 provide a comparison between the jet mixing characteristics for symmetric convergence and asymmetric convergence with flat wall injection. These two figures show nearly the same theta distribution at all X/H_o locations. This suggests that the jet mixing characteristics for flat wall injection are almost identical to that in a symmetrically convergent duct at the same orifice and flow conditions.

The predicted results for Test 27 are presented in Figure 66. The predicted profiles are in very good agreement with the data except at X/H_o = 1.0. The theta values predicted are slightly higher than the measured values at most of the axial stations.

The measured theta values for Test 28 with Test Section V, J = 106.7, S/D = 4, and H_o/D = 8 are presented in Figure 67. For this momentum ratio, the jets impinge on the opposite wall at X/H_o = 0.25. The jets mix rapidly in both radial and transverse directions. The jets merge with each other at X/H_o = 0.5. The predicted results for Test 28 are shown in Figure 68. The predicted theta radial profiles are in good agreement with the data.

In this test case, measurements were made only up to Y/H = 0.75 at X/H_o = 0.25. However, the contour plots for these cases were obtained by using extrapolated values beyond that region. The extrapolated values were obtained by using a cubic spline
curve fit. This was done only for the purpose of clarity in presenting the data.

Comparison of Figures 67 and 59 shows that the asymmetric convergence with flat wall injection has the same theta distribution as the symmetric convergence with the same area reduction.

The test results for Test 29 with Test Section V, J = 7.07, S/D = 2, and H_o/D = 4 are illustrated in Figure 69. At this low momentum ratio, the jets remain separate as far downstream as X/H_o = 1.0. The radial and lateral mixing rates are quite slow as evidenced by the shape and size of the contours. The predicted results for Test 29 are presented in Figure 70. The predicted radial profiles are in qualitative agreement with the data, and the predicted theta values are significantly higher than the measured values. This trend has been observed for most of the Series 3 tests. Furthermore, the predicted jet penetrations are slightly deeper than that seen from the test data for this case. The theta distributions for this test case are very similar to those with symmetric convergence. (See Figures 61 and 69.)

The measured theta values for Test 30 with Test Section V, J = 27.31, S/D = 2, and H_o/D = 4 are presented in Figure 71. At X/H_o = 0.5, the jets penetrate up to about 65 percent of local channel height and they gradually reach the opposite (slant) wall at X/H_o = 1. The jet spreading rate in the radial direction appears to be faster than that in the transverse direction. The predicted theta distributions for Test 30 are portrayed in Figure 72. For this test condition, the predicted and the measured radial profiles are in good agreement at X/H_o = 0.5 and are in only qualitative agreement farther downstream. As observed in the other test cases in Series 3, the predicted theta values are slightly higher than the measured values. Figures 71 and 72 show distributions very similar to those in Figures 63 and 64. This re-emphasizes the similarity in the jet mixing characteristics of Test Sections IV and V.
The following four test cases were taken with Test Section VI, where the dilution jets were injected from the slant test section wall. The jet injection angle for these cases is 106.6 degrees. The jets are injected in the upstream direction, and are expected to alter the mixing characteristics compared to the 90-degree injection case associated with Test Section V. Comparison of the data for these two test sections provides information about the mixing characteristics at two different injection angles with asymmetric convergence.

The measured theta distributions for Test 31 with Test Section VI, J = 26.59, S/D = 4, and H₀/D = 8 are given in Figure 73. At X/H₀ = 0.25, the jet penetration is at about 60 percent of local duct height and the penetration gradually increases farther downstream. The lateral mixing is significantly higher for this test section compared to that with Test Section V. (See Figure 65.) This is primarily due to the upstream injection.

The predicted theta distributions for Test 31 are portrayed in Figure 74. The correlations underpredict the jet penetration and overestimate the theta values compared to the measurements. The correlations do not properly account for the effects of the jet injection angle, which is primarily responsible for the poor agreement with the data.

Comparison of Figures 74 and 66 reveals that the correlations predict the profiles more accurately for flat wall injection than for slant side injection. Furthermore, it is seen that the jet penetration with slant side injection is deeper than that with flat wall injection.

The measured data for Test 32 with Test Section VI, J = 107.8, S/D = 4, and H₀/D = 8 are illustrated in Figure 75. For this momentum ratio, the jets impinge on the opposite (flat) wall. A comparison of Figure 75 with Figure 67 for flat wall injection
at a comparable momentum ratio shows that with the slant wall injection, the jet spreading rate in the transverse direction is significantly faster, while the radial jet spreading rates are nearly the same. The predicted results for Test 32 are illustrated in Figure 76. The correlations underpredict the penetration at $X/H_o = 0.25$ and 0.5, and the agreement between data and correlations is poor. At $X/H_o = 1.0$, the agreement between the two centerplane profiles is very good.

Figure 77 illustrates the data for Test 33, with Test Section VI, $J = 7.05$, $S/D = 2$, and $H_o/D = 4$. The jets penetrate to about 40 percent of the duct height at $X/H_o = 0.5$ and the jet centerline and gradually return to the injection wall. Comparison of this figure with Figure 69 shows that for slant wall injection at $J = 7.05$, the lateral jet spreading rate is slightly faster than that for flat wall injection. The radial jet spreading rates are not significantly different between these two cases. The predicted results for Test 33 are portrayed in Figure 78. The predicted jet penetrations are slightly deeper than the measured ones and the predicted theta values are higher than the measured values. The correlations are, however, in good qualitative agreement with the data.

The data for Test 34, with Test Section VI, $J = 26.4$, $S/D = 2$, and $H_o/D = 4$ are illustrated in Figure 79. At $X/H_o = 0.5$, the jets penetrate up to about 70 percent of the local duct height and reach the opposite (flat) wall at $X/H_o = 0.75$. Comparing this test case with Test 30 (Figure 71) shows that the lateral mixing is enhanced with slant wall injection. The mixing in the radial direction is accelerated after the jet centerline reaches the opposite wall. The predicted theta values for Test 34 are portrayed in Figure 80. The correlations slightly underpredict the jet penetration and overpredict the theta values. The higher theta values are a result of underestimating the mixing rate in the correlations.
5.3.3 Conclusions for Series 3 Tests

Interactions between a row of jets with cross-flow in a convergent duct were studied. Two geometric orifice configurations and two flow conditions for each convergent duct were considered. Symmetric and asymmetric convergent test sections with uniform mainstream temperature and velocity profiles were used in Series 3 tests. The following conclusions are drawn from these tests:

- Mixing is generally enhanced by flow area convergence. The jet spreading in radial and transverse directions occurs within a shorter distance from the jet injection plane than in the case with a constant area duct.

- The jet penetration is slightly reduced in symmetric convergence Test Section II compared to those in a constant cross-sectional area duct. For Test Section IV, the jets are injected upstream at a higher angle toward a region of higher cross-sectional area, where the mainstream velocities are lower. Regions of lower mainstream velocities can be associated with a higher apparent jet momentum ratio and hence the jet penetration in those regions is deeper.

- For asymmetric Test Section V with flat wall injection, the jet mixing characteristics are the same as those of the symmetric convergent Test Section IV.

- In the asymmetric Test Section VI with slant wall injection (jet injection angle of 116.6 degrees), the mixing in the transverse direction is significantly enhanced while the radial mixing is very similar to that with flat wall injection.
The modified NASA/Aerojet correlations with equivalent momentum ratio ($J_{eq}$) yield qualitatively good comparison with the data. However, the predicted theta values are higher than the measured values. The differences between the two results are larger with increasing jet injection angle. Further refinements in the correlations are needed to improve the agreement between data and correlations.

5.4 Series 4 Tests

The objective of these tests was to study the combined effects of flow area convergence and profiled mainstream temperature. These tests were taken with Test Section V (flat wall injection) and with orifice plate 01/04/08. Both top cold and top hot profiles were employed with two momentum ratios for each profile. The test configuration and flow conditions employed in this series are listed in Table VI. Measurements were taken at two axial stations, $X/H_o = 0.25$ and 1.0.

As stated in Paragraph 5.2 for the Series 2 tests, the definition of theta used to analyze these data is

$$\theta = \frac{T_{max} - T}{T_{max} - T_j}$$
where:

\[ T_{\text{max}} \] = Maximum temperature of the profiled mainstream.

\[ T \] = Local stagnation temperature in the mixing region.

\[ T_j \] = Jet stagnation temperature.

The measured theta distributions for Test 35 with top cold profile, \( J = 26.82 \), \( S/D = 4 \), and \( H_o/D = 8 \) are depicted in Figure 81. The jet penetration in this case is about 40 percent of the channel height at \( X/H_o = 0.25 \). The jets retain their individual shapes at both \( X/H_o = 0.25 \) and 1.0. The mainstream temperature (top cold) profile seems to inhibit the lateral and radial mixing. This is evident by comparing Figure 81 with the data for uniform mainstream profile (Figure 65). The predicted theta values for Test 35 are portrayed in Figure 82. The predictions are obtained by superposing the mainstream theta profile \( \theta_p(y) \) on the NASA/Aerojet correlations with equivalent momentum ratio, \( J_{eq} \), in a manner similar to the one described in Paragraph 5.2. The predicted radial profiles along the jet centerplanes are in qualitative agreement with the data at \( X/H_o = 0.25 \) and in poor agreement with the data at \( X/H_o = 1.0 \).

The data for Test 36 with top cold profile, \( J = 109.8 \), \( S/D = 4 \), and \( H_o/D = 8 \) are illustrated in Figure 83. At \( X/H_o = 0.25 \), the jet centerlines are located at about 60 percent of local channel height. The mixing in the transverse direction is much slower than in the corresponding test case with uniform mainstream temperature profile (Figure 67). The predicted theta distributions for Test 36 are presented in Figure 84. The comparison of predicted and measured radial profiles is poor.

The measured theta distributions with Test Section V, top hot mainstream temperature profile, \( J = 8.51 \), \( S/D = 4 \), and \( H_o/D = 8 \) are...
are depicted in Figure 85. At $X/H_0 = 0.25$, the jets retain their individual shapes and mix rapidly in the transverse direction. This characteristic is contrary to the trend observed with the top cold mainstream profile. The predicted theta values for Test 37 are portrayed in Figure 86. At $X/H_0 = 0.25$, the agreement between data and correlations is good. At $X/H_0 = 1$, the agreement is poor.

The measured theta values for Test 38 with top hot profile, $J = 30.24$, $S/D = 4$, and $H_0/D = 8$ are presented in Figure 87. At $X/H_0 = 0.25$, the jets penetrate to about 50 percent of the channel height and gradually penetrate to the opposite wall at $X/H_0 = 1.0$. The shape and location of the contours indicate enhanced mixing in both radial and transverse directions in comparison with those with top cold profiles (Figure 81). The predicted theta distributions for Test 38 are presented in Figure 88. The correlations and data are in good agreement at $X/H_0 = 0.25$, while the agreement is poor at $X/H_0 = 1.0$.

5.4.1 Conclusions for Series 4 Tests

Confined jet mixing characteristics were studied with flow area convergence and profiled mainstream temperature. Four tests were performed with orifice plate 01/04/08, including top cold and top hot mainstream temperature profiles.

The following conclusions are drawn from the data:

- Mixing of the jets in radial and transverse directions is inhibited with top cold mainstream temperature profile and is not significantly affected with top hot profile when compared to tests with isothermal mainstream conditions.
o The mainstream temperature profile has a dominant influence on the temperature distribution throughout the mixing region.

o The superposition scheme used in the correlations is inadequate for predicting the temperature distribution with flow area convergence and profiled mainstream.
6.0 JET MIXING CORRELATIONS DEVELOPMENT

A number of empirical and semiempirical methods have been developed by various researchers for predicting jet interaction with a cross-flow. These models were mostly concerned with jet blockage, entrainment, and mixing in the wake region (References 5, 6, and 7). Empirical models have been proposed for jet trajectory, jet spread, and mixing rate. The main differences between the various models were in the postulated mechanisms for jet entrainment and trajectory.

Most of the popular approximate predictive techniques (References 8 through 12) employ integral methods with simplifying assumptions introduced for mathematical simplicity.

One of the unknowns in integral mixing field prediction methods is usually the shape of the jet cross section. The complex jet cross-section geometries are often approximated by rectangles, circles, or ellipses for satisfying the conservation of mass, momentum, and energy. The second unknown is a velocity profile parameter, which is usually modeled by an appropriate similarity assumption. These models are invalid for curved jets.

The jet deflection is treated in two ways: The first approach treats the jet as a solid body and uses discharge coefficients for the cylinders or ellipses, together with a pressure differential across the jet in the mainstream direction to compute the jet deflection. The second approach deals with mass and momentum entrained from the mainstream into the jet through empirical models and this approach is generally considered to be more accurate. The correlations used in this study are the NASA/Aerojet correlations, which are described in the following paragraph.
6.1 NASA/Aerojet Correlations

The correlations developed by Holdeman and Walker (Reference 2) are based upon experimental data involving a row of jets injected into a confined cross-flow. The jet centerline trajectory is given as:

Correlations for Predicting the Centerplane Temperature Profiles

Thermal Trajectory (Centerline):

\[
\frac{Y_{C,0}}{D_j} = 0.539 J^{0.25} \left( \frac{S}{D_j} \right)^{0.14} \left( \frac{H}{D_j} \right)^{0.38} \left( \frac{X}{D_j} \right)^{0.17} e^{-b} (5.1)
\]

where

\[
b = 0.091 \left( \frac{X}{H} \right)^2 \left( \frac{H}{S} - \frac{\sqrt{J}}{3.5} \right)
\]

The results for temperature field are presented in nondimensional form by using

\[
\theta = \frac{(T_m - T)}{(T_m - T_j)}
\]

where \(T_m\) is the undisturbed mainstream stagnation temperature, \(T\) is the local stagnation temperature in the mixing region, and \(T_j\) is the stagnation temperature of the jet. The variable \(\theta\) represents the ratio of actual temperature change to the maximum possible temperature change due to the dilution jets. The centerline temperature is correlated by the following expression:

Centerline Temperature Difference Ratio:

\[
\theta_{c,0} = \theta_{EB} + (1-\theta_{EB}) \left[ 1.452 J^{-0.35/\left( \frac{X}{D_j} \right)} \right] (5.2)
\]
The temperature difference ratio, $\theta$, at any point in the flow field is determined from:

$$\theta = \theta_{\text{min}}^+ + (\theta_c - \theta_{\text{min}}^-) \exp \left[\left(-\ln 2\right)\left(\frac{Y - Y_c}{W_{1/2}^+}\right)^2\right] \quad (5.3)$$

where $\theta_{\text{min}}^+$ and $W_{1/2}^+$ are defined as follows:

**Minimum Centerplane Temperature Difference Ratios:**

$$\frac{\theta_{\text{min},o}^+}{\theta_{c,o}} = 1 - e^{-c^+} \quad (5.4)$$

where

$$c^+ = 0.038 J^{1.62} \left(\frac{S}{D_j}\right)^{1.5} \left(\frac{H}{D_j}\right)^{-3.67} \left(\frac{X}{D_j}\right)^{1.1}$$

$$\frac{\theta_{\text{min},o}^-}{\theta_{c,o}} = 1 - e^{-c^-} \quad (5.5)$$

where

$$c^- = 1.57 J^{-0.3} \left(\frac{S}{D_j}\right)^{-1.4} \left(\frac{X}{D_j}\right)^{0.9}$$

**Centerplane Half-Widths:**

$$\frac{W_{1/2,o}^+}{D_j} = 0.162 J^{0.18} \left(\frac{S}{D_j}\right)^{-0.25} \left(\frac{H}{D_j}\right)^{0.5} \left(\frac{X}{D_j}\right)^{0.5} \quad (5.6)$$
The half-widths $W_{1/2}^\pm$ are the distance between the jet centerline and the location where $\theta = (\theta_c + \theta_{\min})/2$. 

Correlations for Predicting the Off-Centerplane Variation of the Temperature Profile Scaling Parameters

Off-Centerplane Penetration

$$\frac{Y_{c,z}}{Y_{c,o}} = 1 - \left(\frac{z}{S/2}\right)^2 e^{-g} \quad (5.8)$$

where

$$g = 0.227 J^{0.67} \left(\frac{S}{D_j}\right)^{-1} \left(\frac{X}{D_j}\right)^{0.54}$$

Off-Centerplane Maximum Temperature Difference Ratio

$$\frac{\theta_{c,z}}{\theta_{c,o}} = 1 - \left(\frac{z}{S/2}\right)^2 e^{-d} \quad (5.9)$$

where

$$d = 0.452 J^{0.53} \left(\frac{S}{D_j}\right)^{-1.53} \left(\frac{X}{D_j}\right)^{0.83}$$

Off-Centerplane Minimum Temperature Difference Ratios and Half-Widths

$$\frac{\theta_{\min,z}^\pm}{\theta_{c,z}^\pm} = \frac{\theta_{\min,o}^\pm}{\theta_{c,o}^\pm} \quad (5.10)$$
These correlations provide a useful and reasonably accurate prediction of the temperature profiles along the jet centerplanes. However, the predicted off centerplane temperature profiles are not very accurate and need refinement. Furthermore, the correlations are inaccurate for high momentum ratios when the jets penetrate to the opposite wall.

The NASA/Aerojet correlations described in this Paragraph (6.1) were derived for a uniform flow area and uniform mainstream conditions. When a non-uniform mainstream temperature profile exists, the NASA/Aerojet correlations for theta, $\theta_{NA}$, can be assumed to represent the changes in the local mainstream temperature distribution by dilution jets. In other words,

$$\theta_{NA} = \frac{(T_m(y) - T)}{(T_m(y) - T_j)}$$  \hspace{1cm} (5.11)

Here, $\theta_{NA}$ represents the results from equation (5.3).

For flows with non-uniform profiled mainstream, the ratio of actual temperature change to the maximum possible temperature change due to the jets is obtained from the following definition of nondimensionalized temperature difference ratio:

$$\theta = \frac{(T_{max} - T)}{(T_{max} - T_j)}$$  \hspace{1cm} (5.12)

where:

- $T_{max}$ = Maximum stagnation temperature of the undisturbed mainstream profile
- $T$ = Local stagnation temperature
- $T_j$ = Jet stagnation temperature.
Using equation (5.12), the profiled mainstream theta, \( \theta_m(y) \), can be defined as

\[
\theta_m(y) = \frac{T_{\text{max}} - T_m(y)}{T_{\text{max}} - T_j}
\]  
(5.13)

From equations (5.11), (5.12), and (5.13) it is seen that

\[
\theta = \theta_m(y) + [1 - \theta_m(y)] \theta_{\text{NA}}
\]  
(5.14)

Equation (5.14) is used to generate the predicted theta values for test cases in Series 2 and 4. It is important to note that the variation of the nondimensionalized temperature, \( \theta \), is conveniently scaled between 0.0 and 1.0. The nondimensional temperature distribution, \( \theta_{\text{NA}} \), is obtained from the NASA/Aerojet correlations (Equation 5.3).

For test cases with flow area convergence, the following modifications are used in obtaining predictions. For converging ducts at low Mach numbers, the average mainstream velocity increases by the relation

\[
V_m(x) = V_0 \left( \frac{A_0}{A(x)} \right)
\]  
(5.15)

where:

- \( V_m(x) \) = Average mainstream velocity in the duct at any given axial Station X
- \( V_0 \) = Average mainstream velocity at the jet injection plane (\( X = 0 \))
- \( A(x) \) = Cross-sectional area of the duct at the axial Station X
- \( A_0 \) = Cross-sectional area of the duct at the jet injection plane (\( X = 0 \))
Thus, \[ \rho_m(X) V_m^2(X) = \rho_o V_o^2 \left( \frac{A_o}{A(X)} \right)^2 \]

Due to the acceleration induced by the flow area convergence, the equivalent jet-to-mainstream momentum ratio is given by

\[ J_{eq} = \frac{\rho_j V_j^2}{\rho_m(X) V_m^2(X)} = \frac{\rho_j V_j^2}{\rho_o V_o^2} \left( \frac{A(X)}{A_o} \right)^2 \]

Thus,

\[ J_{eq} = J_o \left( \frac{A(X)}{A_o} \right)^2 \quad (5.16) \]

Where, \( J_o \) is the momentum ratio at the jet injection plane.

The correlations for convergent ducts are obtained by substituting the equivalent momentum ratio, \( J_{eq} \), wherever \( J \) is used in the NASA/Aerojet correlations. This approach was found to yield improved results compared to the results obtained from the original NASA/Aerojet correlations. However, the correlations do not account for the effects of jet injection angle, which have been observed to have significant effect on the jet spreading rates. Further work on the correlations is required to properly account for these effects.

For test cases with flow area convergence and profiled mainstream, the correlations were obtained by combining the procedures described for convergent ducts and profiled mainstream. The predictions obtained from these correlations are inadequate for correctly describing the jet mixing characteristics in Series 4 tests. This is partly due to the fact that the distortion of the mainstream temperature profile (without the jets) by the flow area convergence is ignored in the correlations.
The NASA/Aerojet correlations, along with the modifications suggested in this section, provide an excellent analytical design tool for predicting the jet mixing characteristics in the dilution zone of a combustor. These correlations were formed to yield excellent qualitative agreement (and good quantitative agreement in some of the test cases) with the measurements made in this program. Additional work is needed to improve the predictions obtained from the correlations.
7.0 CONCLUSIONS AND RECOMMENDATIONS

The tests made in Phase I of the NASA Dilution Jet Mixing Program were directed toward better understanding of the mixing processes of a row of jets injected into a ducted cross-flow. The following conclusions are drawn from these tests:

- The jet penetration distance increases with increasing the momentum ratio, J, and jet orifice diameter, D.
- The jet spreading rate in the transverse direction increases with increasing the momentum ratio, J, a duct height to hole diameter ratio, H_o/D, and decreasing the hole spacing to diameter ratio, S/D.
- The jet spreading in the radial direction is enhanced with increased jet penetration.
- The jet-to-mainstream density ratio, \( \rho_j/\rho_m \), has only a second-order effect on the mixing characteristics for a given momentum ratio.
- The temperature distribution in the jet mixing region is strongly influenced by the mainstream temperature profile. The jet spreading rates with profiled mainstream are similar to those with uniform mainstream. This suggests that a superposition principle could be applied to predict temperature profiles with profiled mainstream.
- Jet mixing is generally enhanced by flow area convergence. The jet penetration is increased with increasing upstream injection angle.

57
The jet mixing characteristics with asymmetric convergence and flat wall injection are similar to those in a symmetric convergent test section of the same area ratio.

The asymmetric test section with slant wall injection has a significantly faster jet spreading rate in the transverse direction.

The radial and lateral jet spreading rates with "top cold" mainstream profile and flow area convergence are significantly slower compared to those with uniform mainstream profile and flow area convergence. The jet spreading rates are not appreciably altered with a "top hot" mainstream temperature profile.

The NASA/Aerojet correlations adequately predict the theta profiles for constant area duct and uniform mainstream profile. For the case of constant area duct with profiled mainstream, the superposition of mainstream theta profiles on the correlations yield good qualitative results. An improved scaling parameter is needed to obtain a good quantitative agreement with data.

The modified NASA/Aerojet correlations with equivalent momentum ratio, $J_{eq}$, provide improved predictions of nondimensionalized temperature profiles. However, this model does not properly account for the effects of jet injection angles.

For situations involving flow area convergence and profiled mainstream, the superposition of mainstream temperature profile on the NASA/Aerojet correlations is
inadequate for predicting the temperature profiles in the mixing region. This is mainly due to the decay of the mainstream temperature profile due to flow area convergence. Further work on the correlations is needed to improve the predictions.

The correlations used in this program provide a very useful and simple analytical tool for designing the dilution zone of a combustor. However, additional work is needed to further refine the correlations for convergent ducts and non-uniform mainstream conditions.
Figure 1. Multiple Jet Study Coordinate System and Important Nomenclature.
Figure 2. Jet Mixing Rig Schematic.
Figure 3. Partially Assembled Dilution Jet Mixing Test Rig.
Figure 4. Profile Generator.
Figure 5. Jet Mixing Test Sections. $H_o = 10.16$ cm.
Figure 6. Test Section Wall Statics and Thermocouples.
Figure 7. Dilution Orifice Plate Configurations.
Figure 8. Total Pressure, Thermocouple, and Static Pressure Rake.
Figure 9. X-Y-Z Actuator with the Rake Mounted.
Figure 10. Jet Mixing Rig as Viewed from Rig Discharge End.
Figure 11. Typical Comparison Between Data From NASA/Aerojet and Present Investigation for S/D = 4 and H₀/D = 4.
S = 0.0608 METERS  S/DJ = 2.443  HO/DJ = 4.887  VMAIN = 15.8 M/SEC  VJET = 26.0 M/SEC  TRMAIN = 649.8 K

X/HO = 0.600  X/DJ = 2.44

X/HO = 0.750  X/DJ = 3.67

X/HO =  X/DJ =

MEASURED THETA PROFILES FOR TEST NO. 1, TEST SECTION 1, TRMAIN=CONST.

MEASURED THETA CONTOURS FOR TEST NO.1, TRMAIN=CONST.

CONTOUR  1  2  3  4  5  6
VALUE  0.0500  0.1000  0.1759  0.2000  0.2500  0.3000

ORIGINAL PAGE IS OF POOR QUALITY
W/SEC TMAIN = 649.8 K TJet = 308.1 K THEB = 0.1759 BLORAT = 3.243 DENRATIO = 2.113 TRATIO = 0.474

X/M0 = 1.000 X/DJ = 4.89

X/M0 = 1.600 X/DJ = 7.33

X/N0 = 2.000 X/DJ = 9.77

I, TMAIN=CONST., J = 5.74, S/D = 2.00, H/D = 4.00

5 6 7 8 9 10 11
0.2500 0.3000 0.3500 0.4000 0.5000 0.6000 0.7000

TRANSVERSE DIST. L/S

TRANSVERSE DIST. L/S

TRANSVERSE DIST. L/S

Figure 12

ORJINAL PAGE 19
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/ FOLDOUT FRAME
PREDICTED THETA CONTOURS FOR TEST NO. 1. TMAIN=CONST.

\[ \frac{T_{\text{MAIN}} - T}{T_{\text{MAIN}} - T_j} \]

CONTOUR 1 2 3 4 5 6 7
VALUE 0.0500 0.1000 0.1759 0.2000 0.2500 0.3000 0.3500

COMPARISON BETWEEN DATA AN. CORRELATIONS FOR TEST NO. 1. TEST SECTION I. TMAIN

S/DJ = 2.44  HO/DJ = 4.89  VRATIO = 1.65  TRATIO = 0.474  DENRATIO = 2.113

X/H = 0.50  X/DJ = 2.44

X/H = 0.75  X/DJ = 3.37

X/H = 1.00  X/DJ = 4.89

ORIGINAL PAGE IS OF POOR QUALITY
SECTION I. \( T_{\text{MAIN}} = \text{CONST.} \), \( J = 5.74 \), \( S/D = 2.0 \), \( H/D = 4.0 \)

\[
\begin{array}{cccccc}
6 & 7 & 8 & 9 & 10 & 11 \\
0.3000 & 0.3500 & 0.4000 & 0.5000 & 0.6000 & 0.7000 \\
\end{array}
\]

Figure 13

ORIGINAL PAGE IS OF POOR QUALITY
$S = 0.0508 \text{ Meters}$  $S/DJ = 2.582$  $HO/DJ = 5.164$  $V_{\text{MAIN}} = 16.3 \text{ M/SEC}$  $V_{\text{JET}} = 52.0 \text{ M/SEC}$  $T_{\text{MAIN}} = 651.2 \text{ K}$  $T_{\text{JET}}$

$X/HO = 0.500$  $X/DJ = 2.58$

$X/HO = 0.710$  $X/DJ = 3.87$

$X/HO = 1.000$  $X/DJ = 5.16$

**Measured Theta Profiles for Test No. 2, Test Section I, $T_{\text{MAIN}}=\text{Const.}$, $J=2$**

**Measured Theta Contours for Test No. 2, $T_{\text{MAIN}}=\text{Const.}$, $J=2$**

**Contour Value**

1  0.0600
2  0.1200
3  0.1800
4  0.2400
5  0.2705

*Original page is of poor quality*
1. TMAIN=CONST., J = 1.59, S/D = 2.00, H/D = 4.00

X/H0 = 1.000
X/DJ = 5.16

X/H0 = 1.500
X/DJ = 7.75

X/H0 = 2.000
X/DJ = 10.33

TRIMS ERSE OIS 7.16
TRANSVERSE DIST. US

Figure 14

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PREDICTED THETA CONTOURS FOR TEST NO. 2, TMAIN=CONST. J=21.59

S/DJ = 2.58  MD/DJ = 5.16  VRATIO = 3.18  TRATIO = 0.473  UENRATIO = 2.132  TMAIN = 651

X/H = 0.50  X/DJ = 2.58
X/H = 0.75  X/DJ = 3.87
X/H = 1.00  X/DJ = 5.16

COMPARISON BETWEEN DATA AND CORRELATION FOR TEST NO. 2, TEST SECTION I, UNIFORM TMAIN

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Figure 15

TEST SECTION 1, UNIFORM TMAIN, \( J = 21.59 \), S/D = 2.00, H/D = 4.00

\[ \text{ORIGINAL PAGE IS OF POOR QUALITY} \]
MEASURED THETA PROFILES FOR TEST NO. 3, TEST SECTION 1, TMAIN=CONST, J =

<table>
<thead>
<tr>
<th>CONTOUR</th>
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<th>2</th>
<th>3</th>
<th>4</th>
<th>5</th>
</tr>
</thead>
<tbody>
<tr>
<td>VALUE</td>
<td>0.025</td>
<td>0.075</td>
<td>0.1074</td>
<td>0.175</td>
<td>0.225</td>
</tr>
</tbody>
</table>

MEASURED THETA CONTOURS FOR TEST NO. 3, TMAIN=CONST.
M/SEC  TMAIN = 649.3 K  TJET = 306.9 K  THEB = 0.1074  BLORAT= 3.356  DENRATIO= 2.122  TRATIO=0.473

X/HO = 1.000  X/DJ = 4.68
X/HO = 1.500  X/DJ = 7.02
X/HO = 2.000  X/DJ = 9.36

I. TMAIN=CONST.  J = 6.14  S/D = 4.00  H/D = 4.00

3  4  5  6  7  8  9
0.1074  0.1750  0.2250  0.2750  0.3250  0.3750  0.4250


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Figure 16
PREDICTED THETA CONTOURS FOR TEST NO. 3, TMAIN=CONST, J=6

CONTOUR 1 2 3 4 5
VALUE 0.0250 0.0750 0.1074 0.1750 0.2250

TRANSVERSE DIST. Z/6

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S/DJ = 4.68  M0/D0 = 4.68  VRATIO = 1.70  TRATIO = 0.473  DENRATIO = 2.122  TMAIN
X/H = 0.50  X/DJ = 2.34
X/H = 0.75  X/DJ = 3.51
X/H = 1.00  X/DJ = 4.68

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 3, TEST SECTION I, UNIFORM

FOLDOUT FRAME
Figure 17

TEST SECTION I, UNIFORM TMAIN, J = 6.14, S/D = 4.00, H/D = 4.00

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OF POOR QUALITY

NO. 3, TMAIN=CONST, J=6.14, S/D=4.0, H/D=4.0
S = 0.1016 METERS  S/DJ = 4.869  HO/DJ = 4.869  VMAIN = 14.9 M/SEC  VJET = 52.2 M/SEC  TMAIN = 651

X/HO = 0.500  X/DJ = 2.43

X/HO = 0.750  X/DJ = 3.65

MEASURED THETA PROFILES FOR TEST NO. 4. TEST SECTION I. TMAIN=CONST

CONTOUR 1 2 3 4
VALUE 0.0500 0.1000 0.1500 0.1915

MEASURED THETA CONTOURS FOR TEST NO. 4. TMAIN=

ORIGINAL PAGE IS OF POOR QUALITY
TMAIN = 651.2 K  
TJET = 304.0 K  
THEB = 0.1915  
BLORAT = 7.148  
DENRATIO = 2.174  
TRATIO = 0.467  

4. TMAIN=CONST.  
J = 26.68  
S/D = 4.00  
H/D = 4.00  

4. TMAIN=CONST.  
J = 26.7  
S/D = 4.0  
H/D = 4.0
PREDICTED THETA CONTOURS FOR TEST NO. 4, TMAIN=CONST. J=26

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OF POOR QUALITY

S/DJ = 4.87  NO/DJ = 4.87  VRATIO = 3.50  TRATIO = 0.46°  DENRATIO=2.174  TMAIN

X/H = 0.50  X/DJ = 0.43

X/H = 0.75  X/DJ = 3.65

X/H = 1.00  X/DJ = 4.87

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 4, TEST SECTION 1, UNIFORM
TEST SECTION I, UNIFORM TMAIN, J = 26.68, S/D = 4.00, H/D = 4.00

Figure 19

ORIGINAL PAGE IS OF POOR QUALITY
\[
\text{CONTOUR} \begin{array}{cccc}
1 & 2 & 3 & 4 \\
V \text{VALUE} & 0.0500 & 0.1000 & 0.1687 & 0.2000 & 0.2 \\
\end{array}
\]

\[
\text{MEASURED THETA PROFILES FOR TEST NO. 5, TEST SECTION I, TMAIN=CONST.}
\]

\[
S = 0.0254 \text{ METERS} \quad S/DJ = 2.582 \quad H0/DJ = 10.328 \quad V\text{MAIN} = 15.0 \text{ M/SEC} \quad V\text{JET} = 51.9 \text{ M/SEC} \quad T\text{MAIN} = 648.7 \text{ K}
\]

\[
\text{X/H0} = 0.500 \quad \text{X/DJ} = 5.16 \quad \text{X/H0} = 0.750 \quad \text{X/DJ} = 7.75 \quad \text{X/H0} = \text{X/DJ} =
\]

\[
\text{MEASURED THETA CONTOURS FOR TEST NO. 5, TMAIN=CONST.}
\]

\[
\text{SOLDOUT FRAME}
\]

\[
\text{ORIGINAL PAGE IS OF POOR QUALITY}
\]
THRIN = 648.7 K  TJET = 308.3 K  THEB = 0.1687  BLOGAT = 6.890  DENRATIO = 2.128  TRATIO = 0.475

X/HO = 1.000  X/DJ = 10.33

X/HO = 1.500  X/DJ = 15.49

X/HO = 2.000  X/DJ = 20.66

TMAIN = CONST.  J = 25.32  S/D = 2.00  H/D = 0.00

NO. 5, TMAIN = CONST.  J = 25.32  S/D = 2.0  H/D = 0.0

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Figure 20
CONTOUR

VALUE

0.0500 0.1000 0.1687 0.2000 0.2500

PREDICTED THETA CONTOURS FOR TEST NO. 5, TMAIN=CONST. J=2

S/DJ = 2.58  
H0/DJ = 10.33  VRATIO = 3.45  TRATIO = 0.475  DENRATIO = 2.128  TMAIN

X/H = 0.50  X/DJ = 6.16

X/H = 0.75  X/DJ = 7.75

X/H = 1.00  X/DJ = 10.33

FOLDOUT FRAME

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 5, TEST SECTION I, UNIFORM

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TEST SECTION I, UNIFORM TMAIN, J = 25.32, S/D = 2.00, H/D = 8.0
$$S = 0.0254 \text{ METERS} \quad S/OJ = 2.571 \quad H0/DJ = 0.285 \quad VMAIN = 15.1 \text{ M/SEC} \quad VJET = 103.6 \text{ M/SEC} \quad TMAIN = 649.7 \text{ K}$$

$X/H0 = 0.500$
$X/DJ = 5.14$

$X/H0 = 0.750$
$X/DJ = 7.71$

$X/H0 = 1.000$
$X/DJ = 10.29$

MEASURED THETA PROFILES FOR TEST NO. 6, TEST SECTION I, TMAIN=CONST., J =

<table>
<thead>
<tr>
<th>CONTOUR</th>
<th>1</th>
<th>2</th>
<th>3</th>
<th>4</th>
<th>5</th>
<th>6</th>
<th>7</th>
</tr>
</thead>
<tbody>
<tr>
<td>VALUE</td>
<td>0.0500</td>
<td>0.1000</td>
<td>0.1500</td>
<td>0.2000</td>
<td>0.2500</td>
<td>0.3018</td>
<td>0.3500</td>
</tr>
</tbody>
</table>

MEASURED THETA CONTOURS FOR TEST NO. 6, TMAIN=CONST., J

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I= TMAIN=CONST. J= 107.78 S/D = 2.00 H/D = 8.00

Figure 22

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PREDICTED THETA CONTOURS FOR TEST NO. 6. TMAIN=CONST. J=10

<table>
<thead>
<tr>
<th>CONTOUR</th>
<th>1</th>
<th>2</th>
<th>3</th>
<th>4</th>
<th>5</th>
<th>6</th>
<th>7</th>
</tr>
</thead>
<tbody>
<tr>
<td>VALUE</td>
<td>0.0500</td>
<td>0.1000</td>
<td>0.1500</td>
<td>0.2000</td>
<td>0.2500</td>
<td>0.3018</td>
<td>0.3500</td>
</tr>
</tbody>
</table>

S/DJ = 2.57  H0/DJ = 10.29  VRATIO = 6.85  TRATIO = 0.460  DENRATIO=2.287  TMAIN

X/H = 0.50  X/DJ = 0.14
X/H = 0.75  X/DJ = 0.71
X/H = 1.00  X/DJ = 10.29

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COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 6. TEST SECTION I, UNIFORM...
MAIN = CONST, J = 107.8, S/D = 2.0, H/D = 8.0

\[ \frac{T_{\text{MAIN}} - T_{\text{JET}}}{T_{\text{MAIN}} - T_{\text{JD}}} = \frac{T_{\text{MINT}} - T_{\text{JA}}}{T_{\text{MAIN}} - T_{\text{J}}} \]

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S = 0.0508 METERS  S/OJ = 5.143  HO/OJ = 10.285  VMAIN = 15.2 M/SEC  VJET = 52.8 M/SEC  TMAIN = 651.4 K

MEASURED THETA PROFILES FOR TEST NO. 7, TEST SECTION I, TMAIN=CONST.

CONTOUR  1  2  3  4  5
VALUE  0.0500  0.0750  0.1048  0.1250  0.1500

MEASURED THETA CONTOURS FOR TEST NO. 7, TMAIN=CONST.
M/SEC | TMAIN = 651.4 K | TJet = 302.1 K | THEB = 0.1048 | BLORAT = 7.127 | DENRATIO = 2.192 | TRATIO = 0.464

X/Ho = 1.000  
X/DJ = 10.29

X/Ho = 1.500  
X/DJ = 15.43

X/Ho = 2.000  
X/DJ = 20.67

Figure 24

TMAIN=CONST., J = 26.34, S/D = 4.00, H/D = 8.00

Figure 24

ORIGINAL PAGE IS OF POOR QUALITY
PREDICTED THETA CONTOURS FOR TEST NO.7, TMAIN=CONST.

\[ \frac{(T_{\text{main}} - T)}{(T_{\text{main}} - T_{\text{j}})} \]

\begin{tabular}{|c|c|c|c|c|c|}
\hline
CONTOUR & 1 & 2 & 3 & 4 & 5 \\
\hline
VALUE & 0.0500 & 0.0750 & 0.1048 & 0.1250 & 0.1501 \\
\hline
\end{tabular}

\( S/DJ = 5.14 \quad H_0/DJ = 10.29 \quad VRATIO = 3.4 \quad TRATIO = 0.464 \quad \text{JENRATIO} = 2.192 \)

\( X/H = 0.50 \quad X/DJ = 5.14 \)

\( X/H = 0.76 \quad X/DJ = 7.71 \)

\( X/H = 1.00 \quad X/DJ = 10.29 \)

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO.7, TEST SECTION I, UNL.
TEST NO. 7. TMAIN = CONST. J = 26.34, S/D = 4.0, H/D = 8.0

\[
\begin{array}{cccccc}
3 & 4 & 5 & 6 & 7 & 8 \\
0.1048 & 0.1250 & 0.1500 & 0.1750 & 0.2000 & 0.2500 \\
\end{array}
\]

1.00 \quad X/OJ = 10.29 \quad X/H = 1.50 \quad X/OJ = 15.43 \quad X/H = 2.00 \quad X/OJ = 20.57

\[
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\]

\[
\frac{(T_{\text{MAIN}} - T)}{(T_{\text{MAIN}} - T_{\text{J}})} \quad \frac{(T_{\text{MAIN}} - T)}{(T_{\text{MAIN}} - T_{\text{J}})} \quad \frac{(T_{\text{MAIN}} - T)}{(T_{\text{MAIN}} - T_{\text{J}})}
\]

7. TEST SECTION I. UNIFORM TMAIN. J = 26.34, S/D = 4.00, H/D = 8.00

\frac{O}{O} \quad \text{FINITE FRAME}
S = 0.0608 METERS  S/DJ = 5.143  H0/DJ = 10.286  VMMAIN = 15.1 M/SEC  VJET = 104.1 M/SEC  TMAIN = 649.2 K  TJET = 1087 K

X/H0 = 0.600  X/DJ = 6.14
X/H0 = 0.750  X/DJ = 7.71
X/H0 = 1.000  X/DJ = 10.29

MEASURED THETA PROFILES FOR TEST NO. 8, TEST SECTION I, TMAIN=CONST.  J = 10

CONTOUR  VALUE
1  0.0500
2  0.0750
3  0.1000
4  0.1250
5  0.1809

MEASURED THETA CONTOURS FOR TEST NO. 8, TMAIN=CONST. J=

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FOLDOUT FRAME
I M/SEC  TMAIN = 649.2 K  TJet = 298.7 K  THEB = 0.1808  BLQRT= 14.866  DENRATI= 2.303  TRATIO= 0.460

ON I, TMAIN=CONST, J = 108.97, S/D = 4.00, H/D = 8.00

TEST NO. 8, TMAIN=CONST, J=109.0, S/D=4.0, H/D=8.0

Figure 26

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PREDICTED THETA CONTOURS FOR TEST NO. 8, TMAIN=CONST.

S/DJ = 5.14  H0/DJ = 10.29  VRATIO = 6.88  TRATIO = 0.460  DENRATIO = 2.303

X/H = 0.50  X/DJ = 5.14  X/H = 0.76  X/DJ = 7.71  X/H = 1.00  X/DJ = 10.29

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 8, TEST SECTION I, UNIF

ORIGINAL PAGE IS OF POOR QUALITY
FOR TEST NO. 8. TMAIN=CONST. J=109.0, S/D=4.0, H/D=8.0

TIO = 0.460 DENRATIO=2.303 TMAIN = 649.2 K TJET = 298.7 K THEB = 0.181

X/H = 1.00 X/DJ =10.29 X/H = 1.25 X/DJ =12.86 X/H = 2.00 X/DJ =20.67

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NO. 8. TEST SECTION I .UNIFORM TMAIN. J = 108.97 , S/D =4.00 , H/D =8.00

Figure 27
S = 0.0608 METERS  S/DJ = 2.561  H0/DJ = 5.121  VMAIN = 15.4 M/SEC  VJET = 109.4 M/SEC  TMAM = 3

MEASURED THETA CONTOURS FOR TEST NO. 9. TMRI

MEASURED THETA PROFILES FOR TEST NO. 9, TEST SECTION I. TMAIN=CON'

MEASURED THETA CONTOURS FOR TEST NO. 9, TMAI

CONTOUR 1 2 3 4 5 6
VALUE 0.0500 0.1000 0.1500 0.1830 0.2000 0.21

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OF POOR QUALITY

FOLDOUT FRAME
$T_{MAIN} = 305.8 \text{ K}$
$T_{JET} = 511.5 \text{ K}$
$THEB = 0.1830$
$ALORAT = 3.765$
$DENRATIO = 0.617$
$T_TRATIO = 1.673$

$X/H_0 = 1.000$
$X/DJ = 5.12$

$X/H_0 = 1.500$
$X/DJ = 7.68$

$X/H_0 = 2.000$
$X/DJ = 10.24$

$X/Y_0 = 5.12$

$T_{MAIN} = \text{CONST.}$
$J = 31.00$
$S/D = 2.00$
$H/D = 4.00$

$RATIO = 1.673$

$T_{MAIN} = \text{CONST.}$
$J = 31.0$
$S/D = 2.0$
$H/D = 4.0$

Figure 28
PREDICTED THETA CONTOURS FOR TEST NO. 9, TMAIN=CONST.

S/DJ = 2.56  \( \frac{H_0}{D_J} = 5.12 \)  VRATIO = 7.09  TRATIO = 1.673  DENRATIO = 0.617

\[
\begin{array}{c|c|c|c|c|c|c}
\text{CONTOUR} & 1 & 2 & 3 & 4 & 5 & 6 & 7 \\
\text{VALUE} & 0.0500 & 0.1000 & 0.1500 & 0.1830 & 0.2000 & 0.2500 & 0.3 \\
\end{array}
\]

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 9, TEST SECTION 1, UN..
Figure 29

ST SECTION I, UNIFORM TMAIN, J = 31.00, S/D = 2.00, H/D = 4.00

0.9, TMAIN = CONST, J = 31.0, S/D = 2.0, H/D = 4.0

DENRATIO = 0.617
TMAIN = 306.8 K
TJET = 511.5 K
THEB = 0.183

X/DJ = 6.12
X/H = 1.50
X/DJ = 7.68
X/H = 2.00
X/DJ = 10.24
MEASURED THETA PROFILES FOR TEST NO. 10, TEST SECTION I, TMAIN=CONST., J =:

CONTOUR 1 2 3 4 5 6 7
VALUE 0.0500 0.1024 0.1500 0.2000 0.2500 0.3018 0.3500

MEASURED THETA CONTOURS FOR TEST NO. 10, TMAIN=CONST., J:
$T_{\text{MAIN}} = 293.5 \text{ K}$

$T_{\text{JET}} = 406.1 \text{ K}$

$THEE = 0.1024$

$BLORAT = 3.673$

$DENRATIO = 0.663$

$TRATIO = 1.560$

$X/H_0 = 1.000$

$X/D_J = 6.17$

$X/H_0 = 1.500$

$X/D_J = 7.76$

$X/H_0 = 2.000$

$X/D_J = 10.33$

$I, T_{\text{MAIN}}=\text{CONST.}, J = 30.64, S/D = 4.00, H/D = 4.00$

$ST \text{ NO. 10, } T_{\text{MAIN}}=\text{CONST.}, J = 30.64, S/D = 4.0, H/D = 4.0$

**Figure 30**

*Original page is of poor quality*
PREDICTED THETA CONTOURS FOR TEST NO. 10. TMAIN=CONST. J=30

\[
\frac{(T\text{MAIN}-T)}{(T\text{MAIN}-T\text{J})} \quad \frac{(T\text{MAIN}-T)}{(T\text{MAIN}-U)} \quad \frac{(T\text{MAIN}-T)}{(T\text{MAIN}-T\text{J})}
\]

CONTORL VALUE

<table>
<thead>
<tr>
<th></th>
<th>1</th>
<th>2</th>
<th>3</th>
<th>4</th>
<th>5</th>
<th>6</th>
<th>7</th>
</tr>
</thead>
<tbody>
<tr>
<td>VALUE</td>
<td>0.0500</td>
<td>0.1024</td>
<td>0.1500</td>
<td>0.2000</td>
<td>0.2500</td>
<td>0.3018</td>
<td>0.3500</td>
</tr>
</tbody>
</table>

\[
\frac{S}{D\text{J}} = 5.17 \quad \frac{H_0}{D\text{J}} = 5.17 \quad \text{VRATIO} = 6.80 \quad \text{TRATIO} = 1.560 \quad \text{DENRATIO} = 0.663 \quad \text{TMAIN} = \]

| X/H = 0.60 | X/DJ = 2.58 |
| X/H = 0.75 | X/DJ = 0.87 |
| X/H = 1.00 | X/DJ = 5.17 |

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 10, TEST SECTION I, UNIFORM

ORIGINAL PAGE IS OF POOR QUALITY
TEST SECTION I. UNIFORM TMAIN. J = 30.64, S/D = 4.00, H/D = 4.00

ORIGINAL PAGE IS OF POOR QUALITY
MEASURED THETA PROFILES FOR TEST NO. 11, TEST SECTION I. TMAIN=CONST. J = 3

CONTOUR 1  2  3  4  5  6  7
VALUE 0.0500 0.1025 0.1500 0.2000 0.2500 0.3000 0.3500

MEASURED THETA CONTOURS FOR TEST NO.11, TMAIN=CONST. J=

SOLDOUT FRAME

ORIGINAL PAGE IS
OF POOR QUALITY
\text{TMAIN} = 290.3 \text{ K} \quad \text{TJET} = 444.8 \text{ K} \quad \text{THEB} = 0.1025 \quad \text{BLORAT} = 3.875 \quad \text{DENRAT} = 0.672 \quad \text{TRAT} = 1.532

\begin{align*}
\text{X/HD} & = 1.002 \\
\text{X/DJ} & = 10.35 \\
\text{X/HD} & = 1.502 \\
\text{X/DJ} & = 15.52 \\
\text{X/HD} & = 2.002 \\
\text{X/DJ} & = 20.60
\end{align*}

\text{TMAIN} = \text{CONST} \quad J = 30.19 \quad \text{S/D} = 2.00 \quad \text{H/D} = 8.00

\text{D} \quad 6 \quad 7 \quad 8 \quad 9 \quad 10 \quad 11
\begin{align*}
2500 & \quad 0.3000 \quad 0.3500 \\
0.4000 & \quad 0.5000 \quad 0.6000 \quad 0.7000
\end{align*}

\text{NO. 11, TMAIN=CONST, J=30.19, S/D=2.0, H/D=8.0}

\text{ORIGINAL PAGE IS OF POOR QUALITY}

\text{Figure 32}
PREDICTED THETA CONTOURS FOR TEST NO. 11. TMAIN=CUNST.

\[
\frac{(T_{\text{MAIN}}-T)}{(T_{\text{MAIN}}-U)}
\]

<table>
<thead>
<tr>
<th>CONTOUR</th>
<th>VALUE</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>0.3500</td>
</tr>
<tr>
<td>2</td>
<td>0.1025</td>
</tr>
<tr>
<td>3</td>
<td>0.1500</td>
</tr>
<tr>
<td>4</td>
<td>0.2000</td>
</tr>
<tr>
<td>5</td>
<td>0.2500</td>
</tr>
<tr>
<td>6</td>
<td>0.3000</td>
</tr>
<tr>
<td>7</td>
<td>0.3500</td>
</tr>
</tbody>
</table>

\[
S/DJ = 2.56 \quad H_0/DJ = 10.33 \quad VRATIO = 6.70 \quad TRATIO = 1.632 \quad DENRATIO= 0.672 \quad T_{\text{MAIN}}
\]

\[
X/H = 0.50 \quad X/DJ = 5.19 \\
X/H = 0.76 \quad X/DJ = 7.77 \\
X/H = 1.00 \quad X/DJ = 10.36
\]

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 11. TEST SECTION I. UNIFORM
<p>| | | | | | |</p>
<table>
<thead>
<tr>
<th></th>
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<th></th>
<th></th>
<th></th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>5</td>
<td>6</td>
<td>0.3000</td>
<td>7</td>
<td>8</td>
<td>0.4000</td>
</tr>
<tr>
<td>9</td>
<td>10</td>
<td>0.5000</td>
<td>11</td>
<td>0.6000</td>
<td></td>
</tr>
<tr>
<td>12</td>
<td>0.7000</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

**Test Section I, Uniform Tmain, J = 30.19, S/D = 2.0, H/D = 8.0**

**Figure 33**

---

No. 11, Tmain=Const. J=30.13, S/D=2.0 H/D=8.0

Denratio = 0.672

Tmain = 290.3 K

Tjet = 444.8 K

Theb = 0.102

X/DJ = 0.35

X/H = 1.50

X/DJ = 1.50

X/H = 2.00

X/DJ = 20.68

**Figure 33**

- **Foldout frame**
\[ S = 0.0508 \text{ Meters} \quad S/OJ = 4.961 \quad V\text{MAIN} = 15.3 \text{ M/SEC} \quad V\text{JET} = 97.6 \text{ M/SEC} \quad T\text{MAIN} = 293.0 \text{ K} \]

**Measured Theta Profiles for Test No. 12, Test Section I.**

- **Contour Values:**
  - Contour 1: Value 0.0250
  - Contour 2: Value 0.0500
  - Contour 3: Value 0.0617
  - Contour 4: Value 0.0750
  - Contour 5: Value 0.1000
  - Contour 6: Value 0.1250
  - Contour 7: Value 0.1500

**Measured Theta Contours for Test No. 12, TMAIN=CONST.**

*Original page is of poor quality.*
M/SEC $T_{MAIN} = 293.0$ K $T_{JET} = 457.2$ K $T_{THEB} = 0.0617$ $BLORAT = 4.117$ $DENRATIO = 0.747$ $TRATIO = 1.391$

$M \cdot W \cdot F_{1,1} \cdot Y_{r}$

ON I, $T_{MAIN}=\text{CONST.}$, $J = 30.53$, $S/D = 4.00$, $H/D = 8.00$

Figure 34

Figure 34
CONTOUR 1 2 3 4 5 6 7
VALUE 0.0250 0.0500 0.0617 0.0750 0.1000 0.1250 0.1500

PREDICTED THETA CONTOURS FOR TEST NO. 12, TMAIN=CONST. J=3

S/DJ = 4.96  NO/DJ = 9.32  VRATIO = 6.39  TRATIO = 1.391  DENRATIO=0.747  TMAIN
X/H = 0.50  X/DJ =4.96
X/H = 0.75  X/DJ =7.44
X/H = 1.00  X/DJ =9.82

COMPARISON BETWEEN ORTR AND CORRELATIONS FOR TEST NO. 12, TEST SECTION I, UNIFORM

ORIGINAL PAGE IS OF POOR QUALITY
FOLDOUT FRAME

Figure 35

ORIGINAL PAGE IS
OF POOR QUALITY
Figure 36. Profiled Mainstream Theta Distributions Used in Series 2 Test Cases.
$S = 0.0508$ Meters   $S/DJ = 2.561$   $H0/DJ = 5.122$   $VMAIN = 16.9$ M/SEC   $VJET = 59.7$ M/SEC   $TMAIN = 524.4$ K

$X/H0 = 0.500$   $X/DJ = 2.66$ 

$X/H0 = 0.750$   $X/DJ = 3.84$ 

$X/H0 = 1.000$   $X/DJ = 5.12$

MEASURED THETA PROFILES FOR TEST NO. 13, TEST SECTION II, TOP COLD  

CONTOUR  | 1  | 2  | 3  | 4  | 5  | 6  | 7  |
VALUE    | 0.0500 | 0.1000 | 0.1500 | 0.2000 | 0.2500 | 0.3120 | 0.3500 |

MEASURED THETA CONTOURS FOR TEST NO. 13, TOP COLD, J=22

FOLDOUT FRAME

ORIGINAL PAGE IS OF POOR QUALITY
\[ M/SEC \quad T\text{MAIN} = 524.4 \quad K \quad T\text{JET} = 293.5 \quad K \quad T\text{HEB} = 0.3120 \quad BLORAT = 7.626 \quad DENRATIO = 1.805 \quad TRATIO = 0.560 \]

\[ X/H\text{O} = 1.000 \quad X/DJ = 5.12 \]

\[ X/H\text{O} = 1.500 \quad X/DJ = 7.68 \]

\[ X/H\text{O} = 2.000 \quad X/DJ = 10.24 \]

\[ \text{ION II, TOP COLD} \quad J = 22.63 \quad S/D = 2.00 \quad H/D = 4.00 \]

\[ 5 \quad 6 \quad 7 \quad 8 \quad 9 \quad 10 \quad 11 \]

\[ 0.0 \quad 0.2500 \quad 0.3120 \quad 0.3500 \quad 0.4000 \quad 0.5000 \quad 0.6000 \quad 0.7000 \]

\[ \text{TEST NO. 13, TOP COLD, J=22.63, S/D=2.0, H/D=4.0} \]

\[ \text{FOLDOUT FRAME} \]
PREDICTED THETA CONTOURS FOR TEST NO. 13, TOP COLD. J=22

\[
\frac{(T_{MAX}-T)}{(T_{MAX}-T_{J})}
\]

<table>
<thead>
<tr>
<th>CONTOUR</th>
<th>1</th>
<th>2</th>
<th>3</th>
<th>4</th>
<th>5</th>
<th>6</th>
<th>7</th>
</tr>
</thead>
<tbody>
<tr>
<td>VALUE</td>
<td>0.0500</td>
<td>0.1000</td>
<td>0.1500</td>
<td>0.2000</td>
<td>0.2500</td>
<td>0.3120</td>
<td>0.3500</td>
</tr>
</tbody>
</table>

\[
\frac{(T_{MAX}-T)}{(T_{MAX}-T_{J})}
\]

S/DJ = 2.56  H0/DJ = 5.12  VRATIO = 3.54  TRATIO = 0.560  DENRATIO=1.805  TMAIN

\[
\begin{align*}
X/H & = 0.50 \quad X/DJ = 2.56 \\
X/H & = 0.76 \quad X/DJ = 3.84 \\
X/H & = 1.00 \quad X/DJ = 6.12
\end{align*}
\]

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 13, TEST SECTION II, TOP

FOLDOUT FRAME

ORIGINAL PAGE IS OF POOR QUALITY
13. TEST SECTION II. TOP COLD. J = 22.63, S/D = 2.00, H/D = 4.00

Figure 38

97

ORIGINAL PAGE IS OF POOR QUALITY
R = 0.1016 METERS  S/DJ = 4.845  X/HO = 0.500  X/DJ = 2.42
X/HO = 0.750  X/DJ = 3.63
X/HO = 1.000  X/DJ = 4.84

MEASURED THETA PROFILES FOR TEST NO. 14, TEST SECTION I, TOP COLD  \( J = 7 \)

CONTOUR 1 2 3 4 5 6 7
VALUE 0.0500 0.1140 0.1500 0.2000 0.2500 0.3000 0.3500

MEASURED THETA CONTOURS FOR TEST NO.14, TOP COLD. \( J=7.5 \)

Foldout Frame

Original page is of poor quality
\[ X/HO = 1.000 \]
\[ X/DJ = 4.84 \]
\[ X/HO = 1.500 \]
\[ X/DJ = 7.27 \]
\[ X/HO = 2.000 \]
\[ X/DJ = 9.68 \]

On I. TOP COLD, J = 7.50, S/D = 4.00, H/D = 4.00

<table>
<thead>
<tr>
<th></th>
<th>5</th>
<th>6</th>
<th>7</th>
<th>8</th>
<th>9</th>
<th>10</th>
<th>11</th>
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<tbody>
<tr>
<td></td>
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<td>0.3500</td>
<td>0.4000</td>
<td>0.5000</td>
<td>0.6000</td>
<td>0.7000</td>
</tr>
</tbody>
</table>

Original page is of poor quality

Figure 39

2 FOLDOUT FRAME
PREDICTED THETA CONTOURS FOR TEST NO. 14, TOP COLD, J=7

\[
\frac{T_{\text{MAX}} - T}{T_{\text{MRX}} - T_{\text{J}}} \quad \frac{T_{\text{MAX}} - T}{T_{\text{MAX}} - T_{\text{J}}}
\]

<table>
<thead>
<tr>
<th>CONTOUR</th>
<th>VALUE</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>0.0500</td>
</tr>
<tr>
<td>2</td>
<td>0.1140</td>
</tr>
<tr>
<td>3</td>
<td>0.1500</td>
</tr>
<tr>
<td>4</td>
<td>0.2000</td>
</tr>
<tr>
<td>5</td>
<td>0.2500</td>
</tr>
<tr>
<td>6</td>
<td>0.3000</td>
</tr>
<tr>
<td>7</td>
<td>0.3500</td>
</tr>
</tbody>
</table>

\[
0.0500 \quad 0.1140 \quad 0.1500 \quad 0.2000 \quad 0.2500 \quad 0.3000 \quad 0.3500
\]

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 14, TEST SECTION I, TOP

ORIGINAL PAGE IS OF POOR QUALITY

FOLDOUT FRAME
ST. NO. 14, TOP COLD, J = 7.50, S/D = 4.0, H/D = 4.0

DENRATIO = 2.210
TMAIN = 572.3 K
TJET = 304.7 K
THEB = 0.084

X/H = 1.50, X/D = 7.27
X/H = 2.00, X/D = 9.89

ORIGINAL PAGE IS OF POOR QUALITY
S = 0.0254 METERS  S/DJ = 2.688  H0/DJ = 10.353  VMAIN = 15.6 M/SEC  VJET = 109.3 M/SEC  TMAIN = 616.1 K  TJET =

MEASURED THETA PROFILES FOR TEST NO. 15, TEST SECTION I, TOP COLD  J =

<table>
<thead>
<tr>
<th>CONTOUR</th>
<th>VALUE</th>
</tr>
</thead>
<tbody>
<tr>
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</tr>
<tr>
<td>2</td>
<td>0.1000</td>
</tr>
<tr>
<td>3</td>
<td>0.1500</td>
</tr>
<tr>
<td>4</td>
<td>0.2000</td>
</tr>
<tr>
<td>5</td>
<td>0.2500</td>
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<tr>
<td>6</td>
<td>0.3029</td>
</tr>
<tr>
<td>7</td>
<td>0.3500</td>
</tr>
</tbody>
</table>

MEASURED THETA CONTOURS FOR TEST NO.15, TOP COLD, J=10

/ EOLDOUT, FRAME

ORIGINAL PAGE IS OF POOR QUALITY
SEC MAIN = 616.1 K   T JET = 297.2 K   THEB = 0.3029   BLORAT = 14.821   DENRATIO = 2.215   TRATIO = 0.482

X/HO = 1.000   X/DJ = 10.36
X/HO = 1.500   X/DJ = 15.63
X/HO = 2.000   X/DJ = 20.71

I. TOP COLD   J = 109.85   S/D = 2.00   H/D = 8.00

TRANVERSE DIST. z/s

NO. 15, TOP COLD, J = 109.85, S/D = 2.0, H/D = 8.0

Figure 41

ORIGINAL PAGE IS OF POOR QUALITY
PREDICTED THETA CONTOURS FOR TEST NO. 15, TOP COLD, J=109

CONTOUR VALUE

<table>
<thead>
<tr>
<th>1</th>
<th>2</th>
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<th>4</th>
<th>5</th>
<th>6</th>
<th>7</th>
</tr>
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<tbody>
<tr>
<td>0.0500</td>
<td>0.1000</td>
<td>0.1500</td>
<td>0.2000</td>
<td>0.2500</td>
<td>0.3029</td>
<td>0.3500</td>
</tr>
</tbody>
</table>

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 15, TEST SECTION I, TOP
15. TEST SECTION 1. TOP COLD, \( J = 109.85 \), \( S/D = 2.00 \), \( H/D = 8.00 \)

<table>
<thead>
<tr>
<th>( \text{DIMENSION} )</th>
<th>( \text{VALUE} )</th>
</tr>
</thead>
<tbody>
<tr>
<td>5</td>
<td>0.2500</td>
</tr>
<tr>
<td>6</td>
<td>0.3029</td>
</tr>
<tr>
<td>7</td>
<td>0.3500</td>
</tr>
<tr>
<td>8</td>
<td>0.4000</td>
</tr>
<tr>
<td>9</td>
<td>0.5000</td>
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<tr>
<td>10</td>
<td>0.6000</td>
</tr>
<tr>
<td>11</td>
<td>0.7000</td>
</tr>
</tbody>
</table>

\( \frac{T_{\text{max}} - T}{T_{\text{max}} - T_J} \)

**ORIGINAL PAGE IS OF POOR QUALITY**
S = 0.0608 Meters  S/DJ = 4.888  H0/DJ = 9.776  VMAIN = 18.1 M/SEC  VJET = 63.0 M/SEC  TMAIN = 567.1 K  TJE

MEASURED THETA PROFILES FOR TEST NO. 16, TEST SECTION I, TOP COLD  J = 1

CONTOUR  1  2  3  4  5  6  7
VALUE  0.0500  0.0996  0.1500  0.2000  0.2500  0.3000  0.3500

MEASURED THETA CONTOURS FOR TEST NO.16, TOP COLD, J=22

FOLDOUT FRAME
**Figure 43**

Test No. 16. Top Cold. J = 22.55, S/D = 4.0, H/D = 8.0

M/Sec Tmain = 567.1 K  Tjet = 310.6 K  Tmeb = 0.0996  Blorat = 6.908  Denratio = 1.856  Tratio = 0.548

X/HO = 1.000
X/DJ = 9.78

X/HO = 1.500
X/DJ = 14.66

X/HO = 2.000
X/DJ = 19.55

On I. Top Cold, J = 22.55, S/D = 4.0, H/D = 8.0

<table>
<thead>
<tr>
<th>5</th>
<th>6</th>
<th>7</th>
<th>8</th>
<th>9</th>
<th>10</th>
<th>11</th>
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<td>0</td>
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<td>0.3500</td>
<td>0.4000</td>
<td>0.5000</td>
<td>0.6000</td>
</tr>
</tbody>
</table>

PREDICTED THETA CONTOURS FOR TEST NO. 16, TOP COLD, J=2

S/DJ = 4.89  H0/DJ = 9.78  VRATIO = 3.49  TRATIO = 0.548  DENRATIO=1.856  TMAX

X/H = 0.50  X/DJ =4.89

X/H = 0.75  X/DJ =7.33

X/H = 1.00  X/DJ =9.78

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 16, TEST SECTION I, TOP

ORIGINAL PAGE IS OF POOR QUALITY
\( J = 22.55 \), \( S/D = 4.0 \) \( H/D = 8.0 \)

\[ \text{TOP COLD} \quad J = 22.55 \quad S/D = 4.00 \quad H/D = 8.00 \]
MEASURED THETA PROFILES FOR TEST NO. 17, TEST SECTION I, TOP HOT J.

CONTOUR 1 2 3 4 5 6 7
VALUE 0.0500 0.1000 0.1500 0.2000 0.2500 0.3052 0.35

MEASURED THETA CONTOURS FOR TEST NO. 17, TOP HOT J.
Figure 45

I. TOP HOT, J = 22.14, S/D = 2.00, H/D = 4.00

T NO. 17, TOP HOT, J = 22.14, S/D = 2.0, H/D = 4.0

ORIGINAL PAGE IS OF POOR QUALITY
PREDICTED THETA CONTOURS FOR TEST NO. 17, TOP HOT, J=22.1

S/DJ = 2.43  \( \Delta H/DJ = 4.87 \)  VRATIO = 3.51  TRATIO = 0.564  DENRATIO=1.798  TMAIN =

\[ X/H = 0.60 \quad X/DJ = 2.43 \]

\[ X/H = 0.76 \quad X/DJ = 3.86 \]

\[ X/H = 1.00 \quad X/DJ = 4.87 \]

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 17, TEST SECTION I, TOP
Figure 46

TEST SECTION I, TOP HOT, J = 22.14, S/D = 2.00, H/D = 4.00

NO. 17, TOP HOT, J = 22.14, S/D = 2.00, H/D = 4.00

DENRATIO = 1.798
TMAIN = 538.2 K
TJET = 303.3 K
TWEB = 0.153

X/DJ = 4.87
X/H = 1.60
X/DJ = 7.30
X/H = 2.00
X/DJ = 9.74

EOLDOUT FRAME

ORIGINAL PAGE IS OF Poor QUALITY
S = 0.0508 METERS  S/DJ = 4.869  H0/DJ = 9.737  VMAIN = 18.2 M/SEC  VJET = 72.2 M/SEC  TMAIN = 545.0 K  TJET

MEASURED THETA PROFILES FOR TEST NO. 18, TEST SECTION I, TOP HOT  J = 2

CONTOUR 1 2 3 4 5 6 7
VALUE 0.0500 0.1066 0.1500 0.2000 0.2500 0.3000 0.3500

MEASURED THETA CONTOURS FOR TEST NO. 18, TOP HOT, J=27

FOLDOUT FRAMES
ORIGINAL PAGE IS OF POOR QUALITY
M/SEC TMAIN = 545.0 K TJet = 316.8 K THEB = 0.1066 BDRAT = 7.207 DENRAT = 1.757 TRATIO = 0.581

1.000
X/HO = 1.000
X/D = 9.74

1.500
X/HO = 1.500
X/D = 14.61

2.000
X/HO = 2.000
X/D = 19.47

ON I, TOP HOT J = 27.69 S/D = 4.00 H/D = 8.00

5 6 7 8 9 10 11
0.2500 0.3000 0.3500 0.4000 0.5000 0.6000 0.7000

TEST NO. 18, TOP HOT J = 27.63 S/D = 4.00 H/D = 8.00

Figure 47
Predicted theta contours for test no. 18. Top hot. J=27.6

<table>
<thead>
<tr>
<th>CONTOUR</th>
<th>VALUE</th>
</tr>
</thead>
<tbody>
<tr>
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<tr>
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<td>0.1066</td>
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</tr>
<tr>
<td>4</td>
<td>0.2000</td>
</tr>
<tr>
<td>5</td>
<td>0.2500</td>
</tr>
<tr>
<td>6</td>
<td>0.3000</td>
</tr>
<tr>
<td>7</td>
<td>0.3500</td>
</tr>
</tbody>
</table>

S/DJ = 4.87  
H0/DJ = 9.74  
Vratio = 3.97  
TRATIO = 0.581  
DENRATIO = 1.757  
TMAIN =

X/H = 0.60  
X/DJ = 4.87

X/H = 0.75  
X/DJ = 7.30

X/H = 1.00  
X/DJ = 9.74

Comparison between data and correlations for test no. 18. Test section I, top hot.
TEST NO. 18. TOP HOT, J = 27.69, S/D = 4.0, H/D = 8.0

\[ \frac{T_{\text{MAX}} - T}{T_{\text{MAX}} - T_{\text{J}}} \]

\( X/OJ = 0.0 \)

\( X = 1.50 \) \( X/OJ = 14.61 \)

\( X = 2.00 \) \( X/OJ = 19.47 \)

**Figure 48**

18. TEST SECTION 1, TOP HOT, \( J = 27.69 \), S/D = 4.00, H/D = 8.00

ORIGINAL PAGE IS OF POOR QUALITY
\[ S = 0.0508 \text{ Meters} \quad S/DJ = 4.961 \quad HO/DJ = 9.821 \quad V\text{MAIN} = 15.9 \text{ M/SEC} \quad V\text{JET} = 58.1 \text{ M/SEC} \quad T\text{MAIN} = 656.2 \text{ K} \quad T\text{JET} = \ldots \]

**Measured Theta Profiles for Test No. 19, Test Section II, T\text{MAIN}=\text{Const.}, J = 27**

<table>
<thead>
<tr>
<th>Contour</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>0.050</td>
</tr>
<tr>
<td>2</td>
<td>0.105</td>
</tr>
<tr>
<td>3</td>
<td>0.150</td>
</tr>
<tr>
<td>4</td>
<td>0.200</td>
</tr>
<tr>
<td>5</td>
<td>0.250</td>
</tr>
<tr>
<td>6</td>
<td>0.300</td>
</tr>
</tbody>
</table>

**Measured Theta Contours for Test No. 19, T\text{MAIN}=\text{Const.}**

*Original page is of poor quality*
Figure 49

ORIGINAL PAGE IS OF POOR QUALITY
PREDICTED THETA CONTOURS FOR TEST NO. 19, TMAIN=CON

CONTOUR 1 2 3 4 5 6
VALUE 0.0500 0.1055 0.1500 0.2000 0.2500 0.3000

COMPARISON BETWEEN ORTR AND CORRELATIONS FOR TEST NO. 19, TEST SECTION II, UNIF0

ORIGINAL PAGE IS OF POOR QUALITY
For Test No. 19, TMAIN=CONST, J=27.09, S/D=4.0, H/D=8.0

\[ \text{DENRATIO}=2.020 \quad \text{TMAIN}=656.2 \text{ K} \quad \text{TJET}=330.4 \text{ K} \quad \text{THERB}=0.106 \]

\[ X/H = 1.00 \quad X/DJ =9.92 \]

\[ X/H = 2.00 \quad X/DJ =19.84 \]

Figure 50
S = 0.0508 METERS  S/OJ = 5.037  H0/OJ = 10.074  VMAIN = 15.5 M/SEC  VJET = 106.4 M/SEC  TMAIN = 644.6 K

X/H0 = 0.250  X/OJ = 2.52

X/H0 = 0.500  X/OJ = 5.04

MEASURED THETA PROFILES FOR TEST NO. 20, TEST SECTION II, TMAIN=CONST.

CONTOUR 1 2 3 4 5 6
VALUE 0.0050 0.1000 0.1500 0.1881 0.2000 0.2500

MEASURED THETA CONTOURS FOR TEST NO. 20, TMAIN=...
106.4 M/SEC TMAIN = 644.6 K TJet = 313.9 K THEB = 0.1881 BLOMAT = 15.278 DENRATIO = 2.185 TRATIO = 0.487

SECTION II, TMAIN = CONST., J = 102.50, S/D = 4.00, H/D = 8.00

TOURS FOR TEST NO. 20, TMAIN = CONST., J = 102.5, S/D = 4.0, H/D = 8.0

ORIGINAL PAGE IS OF POOR QUALITY

Figure 51
110

OLDOUT FRAME
PREDICTED THETA CONTOURS FOR TEST NO. 20, TMAIN=CON

S/DJ = 5.04  H0/DJ = 10.07  VRATIO = 6.85  TRATIO = 0.487  DEnRATIO = 2.185  TMAIN =

X/H = 0.25  X/DJ = 2.52  X/H = 0.50  X/DJ = 5.04  X/H = 1.00  X/DJ = 10.07

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 20, TEST SECTION II, UNIFORM

FOLDOUT FRAME

ORIGINAL PAGE IS OF POOR QUALITY
TEST NO. 20. TMAIN=CONST. J = 102.5, S/D = 4.0, H/D = 8.0

DENRATIO = 2.185

TMAIN = 644.6 K
TJET = 313.9 K
THEB = 0.188

X/H = 1.00  X/DJ = 10.07
X/H = 2.00  X/DJ = 20.15

Figure 52

TEST SECTION II. UNIFORM TMAIN. J = 102.50, S/D = 4.00, H/D = 8.00

Figure 52

ORIGINAL PAGE IS OF POOR QUALITY
MEASURED THETA PROFILES FOR TEST NO. 21, TEST SECTION II, TMAIN=CONST., J =

<table>
<thead>
<tr>
<th>CONTOUR</th>
<th>1</th>
<th>2</th>
<th>3</th>
<th>4</th>
<th>5</th>
<th>6</th>
</tr>
</thead>
<tbody>
<tr>
<td>VALUE</td>
<td>0.050</td>
<td>0.100</td>
<td>0.150</td>
<td>0.1973</td>
<td>0.200</td>
<td>0.250</td>
</tr>
</tbody>
</table>

MEASURED THETA CONTOURS FOR TEST NO. 21, TMAIN=CONST.

ORIGINAL PAGE IS OF POOR QUALITY
I, TMAIN = CONSTR. J = 6.76, S/D = 2.00, H/D = 4.00

FOR TEST NO. 21, TMAIN = CONSTR. J = 6.76, S/D = 2.0, H/D = 4.0

Figure 53
PREDICTED THETA CONTOURS FOR TEST NO. 21, TMAIN = CONSTANT

S/DJ = 2.46  HO/DJ = 4.92  VRATIO = 1.78  TRATIU = 0.471  DENRATIO = 2.129  TMAIN

X/H = 0.50  X/DJ = 2.46
X/H = 0.75  X/DJ = 3.69
X/H = 1.00  X/DJ = 4.92

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 21, TEST SECTION II. UNIFORM
RS FOR TEST NO. 21, TMAIN=CONST, J=6.76, S/D=2.0, H/D=4.0

\( \frac{T_{MAIN} - T}{T_{MAIN} - T_J} \)

4 5 6 7 8 9 10
0.1973 0.2000 0.2500 0.3000 0.3500 0.4000 0.4500

FOLDOUT FRAME 2

0.21, TEST SECTION II. UNIFORM TMAIN, J = 6.76, S/D = 2.00, H/D = 4.00

Figure 54

113

ORIGINAL PAGE IS OF POOR QUALITY
**Measured Theta Profiles for Test No. 22, Test Section II, \( T_{MAN}=\text{const.} \), \( J = \)**

- **Contour Values**: 0.0500, 0.1000, 0.1500, 0.2000, 0.2500, 0.3074

**Original Page is of Poor Quality**
SEC. TMAIN = 653.7 K T JET = 303.8 K THEB = 0.3074 BLOMAT = 7.538 DENRATIO = 2.179 TRATIO = 0.465

I. TMAIN = CONST., J = 26.07, S/D = 2.00, H/D = 4.00

X/H0 = 1.000
X/DJ = 5.16

X/H0 = 2.000
X/DJ = 10.33

FOR TEST NO.22. TMAIN = CONST. J = 26.07, S/D = 2.0, H/D = 4.0

ORIGINAL PAGE IS OF POOR QUALITY
CONTOUR 1  2  3  4  5  6
VALUE  0.0500  0.1000  0.1500  0.2000  0.2500  0.3074  0.

PREDICTED THETA CONTOURS FOR TEST NO. 22, TMAIN=CONST

S/DJ = 2.56
H0/DJ = 5.16
VRATIO = 3.46
TRATIO = 0.465
DENRATIO = 2.179
TMAIN =

X/H = 0.50  X/DJ = 2.56
X/H = 0.75  X/DJ = 3.87
X/H = 1.00  X/DJ = 5.16

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 22, TEST SECTION II, UNIFORM

ORIGINAL PAGE IS OF POOR QUALITY
TEST NO. 22, TMAIN = CONST, J = 26.07, S/D = 2.0, H/D = 4.0

DENRATIO = 2.179  TMAIN = 653.7 K  TJet = 303.8 K  THEB = 0.307
X/H = 1.00  X/DJ = 0.16
X/H = 2.00  X/DJ = 0.33

Figure 56

TEST SECTION II, UNIFORM TMAIN, J = 26.07, S/D = 2.0, H/D = 4.0

2 FOLDOUT FRAME


CONTOUR 1 2 3 4 5 6 7 8 9
VALUE 0.0500 0.0972 0.1500 0.2000 0.2500 0.3000 0.3500 0.4000 0.4500

ORIGINAL PAGE IS OF POOR QUALITY
TMAIN = CONST, J = 21.07, S/D = 4.0, H/D = 8.0

FOLDOUT FRAME

Figure 57
CONTOUR 1 2 3 4 5 6 7 8 9
VALUE 0.0500 0.0972 0.1500 0.2000 0.2500 0.3000 0.3500 0.4000 0.5000


S/DJ = 4.93  H0/DJ = 9.85  VRATIO = 3.17  TRATIO = 0.484  DENRATIO=2.102  TMAIN :
X/H = 0.26  X/DJ =2.46

X/H = 0.50  X/DJ =4.93

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 23, TEST SECTION IV, TMAIN:

ORIGINAL PAGE IS OF POOR QUALITY.

FOLDOUT FRAME
\[ \frac{Z_{\text{FMN}}}{Z_{\text{FMN}} - Z_{\text{J}}} \]

\[ \frac{T_{\text{MAIN}} - T_{\text{J}}} {T_{\text{MAIN}} - T_{\text{J}}} \]

\[ T_{\text{MAIN}} = \text{CONST.} \quad J = 21.07 \quad S/D = 4.0 \quad H/D = 8.0 \]

\[ D = 0.484 \quad \text{DENRATIO} = 2.102 \quad T_{\text{MAIN}} = 645.5 \text{ K} \quad T_{\text{JET}} = 312.2 \text{ K} \quad \text{THEB} = 0.097 \]

\[ X/H = 1.00 \quad X/OJ = 9.85 \]

\[ 0.23, \text{ TEST SECTION IV, } T_{\text{MAIN}} = \text{CONST.} \quad J = 21.07 \quad S/D = 4.00 \quad H/D = 8.00 \]

Figure 58

117

ORIGINAL PAGE IS OF POOR QUALITY
$S = 0.0508$ METERS  $S/D = 5.000$  $H_0/D_0 = 10.000$  $V_{MAIN} = 16.9$ M/SEC  $V_{JET} = 105.1$ M/SEC  $T_{MAIN} = 642.8$ K

$X/H_0 = 0.250$  $X/OJ = 2.50$

$X/H_0 = 0.500$  $X/OJ = 5.00$

MEASURED THETA PROFILES FOR TEST NO. 24, TEST SECTION IV, TMAIN=CONST, J =

<table>
<thead>
<tr>
<th>CONTOUR</th>
<th>1</th>
<th>2</th>
<th>3</th>
<th>4</th>
<th>5</th>
<th>6</th>
<th>7</th>
<th>8</th>
</tr>
</thead>
<tbody>
<tr>
<td>VALUE</td>
<td>0.050</td>
<td>0.100</td>
<td>0.150</td>
<td>0.178</td>
<td>0.200</td>
<td>0.250</td>
<td>0.300</td>
<td>0.350</td>
</tr>
</tbody>
</table>

MEASURED THETA CONTOURS FOR TEST NO. 24, TMAIN=CONST, J=85.84, S/D=4
M/SEC  TMAIN = 642.8  K  TJET = 311.0  K  THEB = 0.1781  BFORAT = 13.792  DENRATIO = 2.217  TRATIO = 0.484

X/H0 = 0.500
X/OJ = 5.00

ON IV, TMAIN=CONST, J = 85.84, S/D = 4.00, H/D = 8.00

0.2500  0.3000  0.3500  0.4000  0.4500

MAIN=CONST, J=85.84, S/D=4.0, H/D=8.0

Figure 59

ORIGINAL PAGE IS OF POOR QUALITY
PREDICTED THETA CONTOURS FOR TEST NO. 24. TMAIN=CONST, J=85.84, S/D=4.0.

S/DJ = 5.00  HD/DJ = 10.00  VRATIO = 6.22  TRATIO = 0.484  DENRATIO = 2.217  TMAIN =

X/H = 0.25  X/DJ = 2.50

X/H = 0.50  X/DJ = 5.00

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 24, TEST SECTION IV. UNIFORM
\[ \frac{1}{2}, \text{TMAIN}=\text{CONST, } J=85.84, \text{S/D}=4.0, \text{H/D}=8.0 \]

\[ \text{TRATIO} = 0.484 \quad \text{DENCATION} = 2.217 \quad \text{TMAIN} = 642.8 \text{K} \quad \text{TJET} = 311.0 \text{K} \quad \text{THEB} = 0.178 \]

\[ \begin{align*}
X/DJ & = 5.00 \\
X/H & = 1.00 \\
X/OJ & = 10.00
\end{align*} \]

Test Section IV. Uniform TMAIN, J = 85.84, S/D = 4.00, H/D = 8.00

Figure 60
$S = 0.0508$ Meters  $S/OJ = 2.538$  $H0/OJ = 5.075$  $V_{MAIN} = 15.1$ M/SEC  $V_{JET} = 27.7$ M/SEC  $T_{MAIN} = 643.4$ K  $T_{JET}$

MEASURED THETA PROFILES FOR TEST NO. 25, TEST SECTION IV, $T_{MAIN}=\text{CONST}$. $J = 1$

<table>
<thead>
<tr>
<th>CONTOUR</th>
<th>1</th>
<th>2</th>
<th>3</th>
<th>4</th>
<th>5</th>
<th>6</th>
<th>7</th>
<th>8</th>
</tr>
</thead>
<tbody>
<tr>
<td>VALUE</td>
<td>0.0500</td>
<td>0.1000</td>
<td>0.1500</td>
<td>0.1830</td>
<td>0.2000</td>
<td>0.2500</td>
<td>0.3000</td>
<td>0.3500</td>
</tr>
</tbody>
</table>

MEASURED THETA CONTOURS FOR TEST NO. 25, $T_{MAIN}=\text{CONST}$, $J=6.73$, $S/D=2$.
IV. TRAN = CONST. J = 6.73, S/D = 2.0, H/D = 4.0

Figure 61

ORIGINAL PAGE IS OF POOR QUALITY
PREDICTED THETA CONTOURS FOR TEST NO. 25. TMAIN=CONST. J=6.73. S/D=2

S/DJ = 2.54   H0/DJ = 5.08   VRATIO = 1.83   TRATIO = 0.500   DENRATIO=2.003

X/H = 7.50   X/DJ = 2.54

X/H = 0.75   X/DJ = 3.81

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 25. TEST SECTION IV.UNIF
Figure 62: Test Section IV. Uniform T_MAIN, J = 6.73, S/D = 2.00, H/D = 4.00

T_MAIN = 643.4 K, T_JET = 321.6 K, TEB = 0.183

X/DJ = 3.81
X/H = 1.00, X/DJ = 5.08

T_MAIN - T_JET

ORIGINAL PAGE IS OF POOR QUALITY
S = 0.0508 METERS  S/DJ = 2.582  X/HO = 0.750  X/OJ = 3.87
VMAIN = 14.9 M/SEC  VJET = 55.1 M/SEC  TMAIN = 640.7 K  TJET

MEASURED THETA PROFILES FOR TEST NO. 26, TEST SECTION IV, TMAIN=CONST, J = 26

CONTOUR  VALUE
1   0.0500
2   0.1000
3   0.1500
4   0.2000
5   0.2500
6   0.2988
7   0.3500
8   0.4000
9   0.4500

MEASURED THETA CONTOURS FOR TEST NO. 26, TMAIN=CONST, J=26.73, S/D=2.0

ORIGINAL PAGE IS OF POOR QUALITY
SECTION IV. TMAIN=CONST., J = 26.73, S/D = 2.00, H/D = 4.00

Figure 63
PREDICTED THETA CONTOURS FOR TEST NO. 26, TMAIN=CONST. J=26.73, S/D=2.0

S/DJ = 2.58  MO/DJ = 5.16  VRATIO = 3.70  TRATIO = 0.515  DENRATIO=1.968  TMAIN

X/H = 0.50  X/DJ = 2.68  

X/H = 0.76  X/DJ = 3.87

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 26, TEST SECTION 'V.UNIFORE

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26. $T_{\text{MAIN}}=\text{CONST.}, J=26.73, S/D=2.0, H/D=4.0$

RATIO = 0.515  DENRATIO=1.958  $T_{\text{MAIN}} = 640.7 \text{ K}$  $T_{\text{JET}} = 329.8 \text{ K}$  THEB = 0.299

$x/DJ = ^{\circ} 97$

$x/H = 1.00$  $x/DJ = 5.16$

Figure 64

No. 26, Test Section IV. Uniform $T_{\text{MAIN}}, J = 26.73, S/D = 2.00, H/D = 4.00$

*(Original page is of poor quality)*
MEASURED THETA PROFILES FOR TEST NO. 27, TEST SECTION V, TMAIN=CONST, J

CONTOUR

1
2
3
4
5
6
7
8

VALUE

0.0500
0.1065
0.1500
0.2000
0.2500
0.3000
0.3500
0.4000

MEASURED THETA CONTOURS FOR TEST NO. 27, TMAIN=CONST, J=27.18, S/D
58.7 M/SEC  TMAIN = 646.4 K  TJet = 320.3 K  THEB = 0.1065  BLORAT = 7.470  DENRATIO = 2.053  TRATIO = 0.496

X/Ho = 0.500
X/DJ = 4.96

X/Ho = 1.000
X/DJ = 9.92

SECTION V, TMAIN=CONST, J = 27.18, S/D = 4.00, H/D = 8.00

6  7  8  9  10
0 0.3000 0.3500 0.4000 0.4500 0.5000

7, TMAIN=CONST, J=27.18, S/D=4.0, H/D=8.0

Figure 65

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ORIGINAL PAGE IS OF POOR QUALITY
COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 27. TEST SECTION V. UNIFORM

PREDICTED THETA CONTOURS FOR TEST NO. 27, $T_{\text{MAIN}}=\text{CONST.}$, $J=27.18$, $S/D=4.1$

<table>
<thead>
<tr>
<th>CONTOUR</th>
<th>1</th>
<th>2</th>
<th>3</th>
<th>4</th>
<th>5</th>
<th>6</th>
<th>7</th>
<th>8</th>
<th>9</th>
</tr>
</thead>
<tbody>
<tr>
<td>VALUE</td>
<td>0.0500</td>
<td>0.1065</td>
<td>0.1500</td>
<td>0.2000</td>
<td>0.2500</td>
<td>0.3000</td>
<td>0.3500</td>
<td>0.4000</td>
<td>0.45</td>
</tr>
</tbody>
</table>

$S/DJ = 4.96$  $H0/DJ = 9.92$  $VRATIO = 3.64$  $TRATIO = 0.496$  $DENRATIO = 2.053$  $T_{\text{MAIN}}$

$X/H = 0.25$  $X/DJ = 2.48$

$X/H = 0.50$  $X/DJ = 4.96$

ORIGINAL PAGE IS OF POOR QUALITY
\[
\frac{(T_{\text{MAIN}} - T)}{(T_{\text{MAIN}} - T_{\text{J}})}
\]

<table>
<thead>
<tr>
<th></th>
<th>6</th>
<th>7</th>
<th>8</th>
<th>9</th>
<th>10</th>
</tr>
</thead>
<tbody>
<tr>
<td>600</td>
<td>0.3000</td>
<td>0.3500</td>
<td>0.4000</td>
<td>0.4500</td>
<td>0.5000</td>
</tr>
</tbody>
</table>

\[
\begin{align*}
    & \text{TRATIO} = 0.496 \\
    & \text{DENRATIO} = 2.063 \\
    & T_{\text{MAIN}} = 646.4 \text{ K} \\
    & T_{\text{JET}} = 320.3 \text{ K} \\
    & \text{THEB} = 0.107
\end{align*}
\]

\[
\frac{X}{DJ} = 4.96
\]

\[
\begin{align*}
    & X/H = 1.00 \\
    & X/DJ = 0.92
\end{align*}
\]

**Figure 66**
ORIGINAL PAGE IS OF POOR QUALITY

S = 0.0608 METERS  S/DJ = 5.061  H0/DJ = 10.121  VMain = 16.0 M/SEC  VJet = 112.5 M/SEC  TMain = 645.1 K

X/H0 = 0.250  X/DJ = 2.53

X/H0 = 0.500  X/DJ = 6.06

MEASURED THETA PROFILES FOR TEST NO. 28, TEST SECTION V. TMAIN=CONST.

<table>
<thead>
<tr>
<th>CONTOUR</th>
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<th>3</th>
<th>4</th>
<th>5</th>
<th>6</th>
<th>7</th>
<th>8</th>
</tr>
</thead>
<tbody>
<tr>
<td>VALUE</td>
<td>0.050</td>
<td>0.100</td>
<td>0.150</td>
<td>0.188</td>
<td>0.250</td>
<td>0.300</td>
<td>0.350</td>
<td>0.400</td>
</tr>
</tbody>
</table>

MEASURED THETA CONTOURS FOR TEST NO.28. TMAIN=CONST. J=106.7. S/D
$V = 2.189 \times 10^{-3}$

$\text{TRAT} = 0.496$

$\text{BLORAT} = 16.176$

$\text{DENRAT} = 2.159$

$\text{JET} = 319.1 \text{ K}$

$\text{M/SEC} = 645.1 \text{ K}$

$\text{THEB} = 0.1988$

$X/HD = 0.500$

$X/DJ = 5.06$

$X/HD = 1.000$

$X/DJ = 10.12$

$V, TMAIN=\text{CONST., } J = 106.72, \ S/D = 4.00, \ H/D = 8.00$

$TMAIN=\text{CONST., } J = 106.7, \ S/D = 4.0, \ H/D = 8.0$

Figure 67

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@FOLDOUT FOLDER

S/DJ = 5.06   H0/DJ = 10.12   VRATIO = 7.03   TRATIO = 0.495   DENRATIO=2.159   TMAIN

X/H = 0.25   X/DJ = 2.63

X/H = 0.60   X/DJ = 5.06

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 28. TEST SECTION V.UNIFORM

ORIGINAL PAGE IS OF POOR QUALITY
Figure 68

Test No. 28, Test Section V. Uniform T\text{MAIN}, \( J = 106.72 \), \( S/D = 4.00 \), \( H/D = 8.00 \)

\begin{align*}
\text{MAIN-T} / (\text{MAIN-T} - \text{J}) & \quad \text{denratio} = 2.159 \\
\text{MAIN} = 645.1 \text{ K} & \quad \text{tjet} = 319.1 \text{ K} \\
\text{THEB} = 0.189 & \quad X/M = 1.00 \\
X/DJ = 5.06 & \quad X/DJ = 10.12
\end{align*}

\( T\text{AT} = 319.1 \) K, \( T\text{HEB} = 0.189 \)
S = 0.0508 METERS  S/OJ = 2.462  H0/OJ = 4.824  VMAIN = 15.7 K/SEC  VJET = 29.1 M/SEC  TMAIN = 645.0 K  TJET

X/H0 = 0.500  X/OJ = 2.46

X/H0 = 0.750  X/OJ = 3.69

MEASURED THETA PROFILES FOR TEST NO. 29, TEST SECTION V, TMAIN=CONST.. J = 7

CONTOUR  1  2  3  4  5  6  7  8  9
VALUE  0.0500  0.1000  0.1500  0.1984  0.2500  0.3000  0.3500  0.4000  0.4

MEASURED THETA CONTOURS FOR TEST NO.29, TMAIN=CONST, J=7.07, S/D=2.0

ORIGINAL PAGE IS OF POOR QUALITY
V. $T_{MAIN} = \text{CONST.}$, $J = 7.07$, $S/D = 2.00$, $H/D = 4.00$

Figure 69

ORIGINAL PAGE IS OF POOR QUALITY

Figure 69
PREDICTED THETA CONTOURS FOR TEST NO. 29. TMAIN=CONST, J=7.07, S/D=2.

\[
\begin{array}{c|c|c|c|c|c|c|c|c}
\text{CONTOUR} & 1 & 2 & 3 & 4 & 5 & 6 & 7 & 8 \\
\text{VALUE} & 0.0500 & 0.1000 & 0.1500 & 0.1984 & 0.2500 & 0.3000 & 0.3500 & 0.4000 & 0.4500 \\
\end{array}
\]

S/D = 2.46  H0/DJ = 4.92  VRATIO = 1.85  TRATIO = 0.486  DENRATIO = 2.064

\[
\begin{align*}
X/H &= 0.50  \quad X/DJ \approx 2.46 \\
X/H &= 0.75  \quad X/DJ \approx 3.69
\end{align*}
\]

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 29, TEST SECTION V, UNIFORM.

ORIGINAL PAGE IS OF POOR QUALITY.
Figure 70

TEST NO. 29, TEST SECTION V, UNIFORM TMAIN, J = 7.07, S/D = 2.00, H/D = 4.00

TRATIO = 0.486  DENRATIO = 2.064  TMAIN = 645.0 K  TJet = 313.5 K  THEB = 0.198

X/H = 1.00  X/DJ = 4.82

ORIGINAL PAGE IS OF POOR QUALITY
MEASURED THETA PROFILES FOR TEST NO. 30, TEST SECTION V. TMAIN=CONST., J =

<table>
<thead>
<tr>
<th>CONTOUR</th>
<th>1</th>
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<th>3</th>
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<th>5</th>
<th>6</th>
<th>7</th>
<th>8</th>
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</thead>
<tbody>
<tr>
<td>VALUE</td>
<td>0.0500</td>
<td>0.1000</td>
<td>0.1500</td>
<td>0.2000</td>
<td>0.2500</td>
<td>0.3149</td>
<td>0.3500</td>
<td>0.4000</td>
</tr>
</tbody>
</table>

MEASURED THETA CONTOURS FOR TEST NO.30, TMAIN=CONST. J=27.31, S/D=

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OF POOR QUALITY
Figure 71

S/DJ = 2.54  MG/DJ = 5.08  VRATIO = 3.62  TRATIO = 0.486  DENRATIO=2.087  TMAIN

X/H = 0.50  X/DJ = 2.54

X/H = 0.75  X/DJ = 3.81

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 30. TEST SECTION V. UNIFORM
No. 30, Test Section V, Uniform TMAIN, J = 27.31, S/D = 2.00, H/D = 4.00

Figure 72

ORIGINAL PAGE IS OF POOR QUALITY
MEASURED THETA PROFILES FOR TEST NO. 31. TEST SECTION VI. TMAIN=CONST. J =

<table>
<thead>
<tr>
<th>CONTOUR</th>
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<th>4</th>
<th>5</th>
<th>6</th>
<th>7</th>
<th>8</th>
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</thead>
<tbody>
<tr>
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<td>0.1500</td>
<td>0.2000</td>
<td>0.2500</td>
<td>0.3000</td>
<td>0.3500</td>
<td>0</td>
</tr>
</tbody>
</table>


ORIGINAL PAGE IS OF POOR QUALITY.
M/SEC  \text{ TMAIN } = 649.2 \text{ K}  \quad \text{TJET } = 319.5 \text{ K}  \quad \text{THEB} = 0.1066  \quad \text{BLORAT} = 7.421  \quad \text{DENRATID } = 2.072  \quad \text{TRATIO} = 0.492

X/\text{HO} = 0.500
X/\text{DJ} = 4.84
X/\text{HO} = 1.000
X/\text{DJ} = 6.88

\text{ION VI. TMAIN=CONST. J } = 26.59  \quad \text{S/D} = 4.00  \quad \text{H/D} = 8.00

0.2500  0.3000  0.3500  0.4000  0.4500

\text{MAIN=CONST. J=26.59, S/D=4.0, H/D=8.0}

\text{ORIGINAL PAGE IS OF POOR QUALITY}

\text{FOLDOUT FRAME}

\[
\frac{S}{D} = 4.94 \quad \frac{H}{D} = 9.88 \quad VRATIO = 3.58 \quad TRATIO = 0.492 \quad DENRATIO = 2.072
\]

\[
X/H = 0.25 \quad X/DJ = 2.47
\]

\[
X/H = 0.50 \quad X/DJ = 4.94
\]

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 31, TEST SECTION VI,UNI.

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FOLDOUT FRAME /
TMAIN=CONST. J=26.59, S/D=4.0, H/D=8.0

O.0 0.2500 0.3148 0.3500 0.4000 0.4500

It's TMAIN=CONST. J=26.59, S/D=4.00, H/D=8.00

Figure 74
3 = 0.0508 METERS  \( \Delta \theta / \Delta x = 5.081 \)  \( \Delta x / \Delta \theta = 10.183 \)  \( V_{\text{MAIN}} = 16.5 \) M/SEC  \( V_{\text{JET}} = 116.0 \) M/SEC  \( T_{\text{MAIN}} = 647.0 \) K

MEASURED THETA PROFILES FOR TEST NO. 32. TEST SECTION VI.  \( T_{\text{MAIN}} = \) CONSTANT.

<table>
<thead>
<tr>
<th>CONTOUR</th>
<th>1</th>
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<th>3</th>
<th>4</th>
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<th>6</th>
<th>7</th>
<th>8</th>
</tr>
</thead>
<tbody>
<tr>
<td>VALUE</td>
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<td>0.1500</td>
<td>0.1800</td>
<td>0.2500</td>
<td>0.3000</td>
<td>0.3500</td>
<td>0.4000</td>
</tr>
</tbody>
</table>

MEASURED \( \ln \theta \) CONTOURS FOR TEST NO. 32.  \( T_{\text{MAIN}} = \) CONSTANT.  \( \Delta = 107.8 \).
M/SEC: TMAIN = 647.0 K, TJET = 321.2 K, THEB = 0.1887, BLORAT = 15.297, DENRATIO = 2.176, TRATIO = 0.496

\[ X/H_0 = 0.500 \]
\[ X/D_J = 5.08 \]

IN VI, TMAIN = CONST. J = 107.76, S/D = 4.00, H/D = 8.00

<table>
<thead>
<tr>
<th>6</th>
<th>7</th>
<th>8</th>
<th>9</th>
<th>10</th>
</tr>
</thead>
<tbody>
<tr>
<td>9000</td>
<td>0.3500</td>
<td>0.4000</td>
<td>0.4500</td>
<td>0.5000</td>
</tr>
</tbody>
</table>

RAIN = CONST, J = 107.8, S/D = 4.0, H/D = 8.0

Figure 75
PREDICTED THETA CONTOURS FOR TEST NO. 32. TMAIN=CONST. J=107.8, S/D=

\[
\begin{array}{cccccccc}
\text{CONTOUR} & 1 & 2 & 3 & 4 & 5 & 6 & 7 & 8 \\
\text{VALUE} & 0.0500 & 0.1000 & 0.1500 & 0.1888 & 0.2500 & 0.3000 & 0.3500 & 0.4000 & 0
\end{array}
\]

\[
\begin{array}{ccc}
\text{TRANVERSE DIST. Z/S} & 0.1 & 0.5 & 1.0 \\
\text{ADIOUS DIST. Y/H} & -0.5 & 0 & 0.5 \\
\end{array}
\]

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 32. TEST SECTION VI. UNII

EOLDOUT FRAME

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No. 32. Test Section VI. Uniform TMain, J = 107.76, S/D = 4.00, H/D = 8.00

\[ T10 = 0.496 \quad \text{DENRATIO} = 2.176 \quad T\text{MAIN} = 647.0 \, \text{K} \quad T\text{JET} = 321.2 \, \text{K} \quad T\text{HEB} = 0.189 \]

\[ X/DJ = 5.08 \quad \text{X/M} = 1.00 \quad X/Dl' = 10.16 \]

Figure 76

Original

OF POOR QUALITY
MEASURED THETA PROFILES FOR TEST NO. 33, TEST SECTION VI, TMAIN=CONST. J = 7

MEASURED THETA CONTOURS FOR TEST NO. 33, TMAIN=CONST, J = 7.05, S/D = 2.0

ORIGINAL PAGE IS OF POOR QUALITY
$\frac{X}{H_0} = 0.750$
$\frac{X}{O_J} = 3.75$

ION VI. $T_{MAIN} = \text{CONST}$. $J = 7.05$. $S/D = 2.00$. $H/D = 4.00$

$6 \quad 7 \quad 8 \quad 9 \quad 10$
$0.3000 \quad 0.3500 \quad 0.4000 \quad 0.4500 \quad 0.5000$

$V_{INL} = \text{CONST.} J = 7.05. S/D = 2.0. H/D = 4.0$

Figure 77

136
CONTOUR
VALUE

1 2 3 4 5 6 7 8 9
0.0500 0.1000 0.1500 0.1969 0.2500 0.3000 0.3500 0.4000 0.45

PREDICTED THETA CONTOURS FOR TEST NO. 33. TMAIN=CONST. J=7.05, S/D=2.0

S/D = 2.50  H0/DJ = 5.00  VRATIO = 1.60  TRATIO = 0.464  DENRATIO = 2.165  TMAIN

X/H = 0.50  X/DJ = 2.50

X/H = 0.75  X/DJ = 3.75

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 33. TEST SECTION VI. UNIFORM
TMAIN=CONST. $J=7.05$, $S/D=2.0$, $H/D=4.0$

$T_{IO} = 0.464$, $DENRATIO = 2.165$, $T_{MAIN} = 649.6 \, K$, $T_{JET} = 301.3 \, K$, $THEB = 0.197$

$X/OJ = 3.75$

$X/H = 1.00$, $X/DJ = 5.00$

No. 33, Test Section VI. Uniform TMAIN, $J = 7.05$, $S/D = 2.00$, $H/D = 4.00$
S = 0.0508 METERS  S/0J = 2.561  H0/OJ = 5.122  VMAIN = 16.2 M/SEC  VJET = 55.9 M/SEC  TMAIN = 650.8 K

X/H0 = 0.500  X/OJ = 2.56

X/H0 = 0.750  X/OJ = 3.84

MEASURED THETA PROFILES FOR TEST NO. 34, TEST SECTION VI, TMAIN=CONST. J

MEASURED THETA CONTOURS FOR TEST NO. 34, TMAIN=CONST, J=26.4, S/D=

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FOLDOUT FRAME
TMAIN = 650.8 K  TJET = 296.9 K  THEB = 0.3144  BLORAT = 7.657  DENRATIO = 2.225  TRATIO = 0.456

X/H0 = 0.750
X/DJ = 3.64

X/H0 = 1.000
X/DJ = 5.12

VI. TMAIN CONST.  J = 26.40  S/D = 2.00  H/D = 4.00

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IN=CONST.  J=26.4.  S/D=2.0.  H/D=4.0

Figure 79
PREDICTED THETA CONTOURS FOR TEST NO. 34. $T_{MAIN}=\text{CONST.}$ $J=26.4$, $S/D=2.0$

$S/DJ = 2.56$  $H_0/DJ = 5.12$  $VRATIO = 3.44$  $TRATIO = 0.456$  $DEN RATIO = 2.225$  $T_{MAIN}$

$X/H = 0.50$  $X/DJ = 2.56$

$X/H = 0.75$  $X/DJ = 3.84$

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 34. TEST SECTION VI.UNIF

FOLDOUT FRAME

ORIGINAL PAGE IS OF POOR QUALITY
TMAIN = CONST. J = 26.4, S/D = 2.0, H/D = 4.0

\[ TMAIN = 650.8 \text{ K} \quad \text{TJET} = 296.9 \text{ K} \quad \text{THEB} = 0.314 \]

\[ X/H = 1.00 \quad \text{X/DJ} = 5.12 \]

NO. 34. TEST SECTION VI. UNIFORM TMAIN. J = 26.40, S/D = 2.00, H/D = 4.00

Figure 80

139
S = 0.0608 METERS  S/OJ = 4.961  HO/DJ = 9.921  VMAIN = 18.7 M/SEC  VJET = 70.9 M/SEC  TMAIN = 561.4 K

MEASURED THETA PROFILES FOR TEST NO. 35, TEST SECTION V, TOP COLD

<table>
<thead>
<tr>
<th>CONTOUR</th>
<th>1</th>
<th>2</th>
<th>3</th>
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<td>0.1500</td>
<td>0.2000</td>
<td>0.2500</td>
<td>0.3000</td>
</tr>
</tbody>
</table>

MEASURED THETA CONTOURS FOR TEST NO. 35, TOP COLD

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**VHO**

\[ VHO = 1.000 \]

\[ \theta = 9.92 \]

**ORIGINAL FIGURE 81**

---

**SECTION V, TOP COLD**

\[ J = 26.82 \]

\[ S/D = 4.00 \]

\[ H/D = 8.00 \]

---

**Figure 81**

---

*Original page is of poor quality*

---

*Ours for Test No. 35, Top Cold, J=26.82, S/D=4.0, H/D=8.0*
PREDICTED THETA CONTOURS FOR TEST NO. 35, TOP COLD.

S/D = 4.96
H0/D = 9.92
VRATIO = 3.79
TRATIO = 0.648
DENRATIO = 1.864
TMAIN =

X/H = 0.25
X/D = 2.48

X/H = 1.00
X/D = 9.62

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 35, TEST SECTION V, TOP

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FOLDOUT FRAME
FOR TEST NO. 35, TOP COLD, J=26.82, S/D=4.0, H/D=8.0

D = 0.648  
DENRATIO = 1.864  
TMAIN = 561.4 K  
TJET = 307.6 K  
THEB = 0.055

X/Y = 1.00  
X/DJ = 0.92

Figure 82
S = 0.0508 METERS  S/OJ = 5.163  HO/DJ = 10.327  VMAIN = 18.8 M/SEC  VJET = 139.1 M/SEC  TMAIN = 568.2 K

X/H0 = 0.250
X/DJ = 2.58

MEASURED THETA PROFILES FOR TEST NO. 36, TEST SECTION V, TOP COLD

<table>
<thead>
<tr>
<th>CONTOUR</th>
<th>1</th>
<th>2</th>
<th>3</th>
<th>4</th>
<th>5</th>
<th>6</th>
</tr>
</thead>
<tbody>
<tr>
<td>VALUE</td>
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<td>0.1500</td>
<td>0.1768</td>
<td>0.2500</td>
<td>0.3000</td>
</tr>
</tbody>
</table>

MEASURED THETA CONTOURS FOR TEST NO. 36, TOP COLD

FOLDOUT FRAME

ORIGINAL PAGE IS OF POOR QUALITY
FOR TEST NO. 36, TOP COLD, J = 109.8, S/D = 4.0, H/D = 8.0

Figure 83

QUALITY OF POOR QUALITY
PREDICTED THETA CONTOURS FOR TEST NO. 36, TOP COLL

\[ S/DJ = 5.16 \quad H/DJ = 10.39 \quad VRATIO = 7.39 \quad TRATIO = 0.537 \quad DENSITY = 2.012 \quad TMA \]

\[ X/H = 0.25 \quad X/DJ = 2.58 \quad X/H = 1.00 \quad X/DJ = ? \]

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 36, TEST SECTION V, TOP

ORIGINAL PAGE IS
OF POOR QUALITY
Figure 84

143

FOR TEST NO. 36, TOP COLD, J=109.8, S/D=4.0, H/D=8.0

$\theta = 0.537$  \hspace{1cm} DENRATIO=2.012  \hspace{1cm} TMAIN = 568.2 \text{ K}  \hspace{1cm} T\text{JET} = 306.2 \text{ K}  \hspace{1cm} THE8 = 0.101$

$X/H = 1.00$  \hspace{1cm} $X/\text{DJ} = 10.33$

ORIGINAL PAGE IS OF POOR QUALITY

36. TEST SECTION V, TOP COLD, J = 109.80, S/D = 4.00, H/D = 8.00

$\frac{T\text{MAX}-T}{T\text{MAX}-\text{TJ}} \geq $ FOLDOUT FRGMT.
\[ S = 0.0508 \text{ METERS} \quad \text{S/OJ} = 4.698 \quad \text{HO/DJ} = 9.396 \quad \text{VMAIN} = 16.0 \text{ M/SEC} \quad \text{VJET} = 40.7 \text{ M/SEC} \quad \text{THI} = 417.3 \text{ K} \]

\[
\text{X/HO} = 0.250 \\
\text{X/DJ} = 2.35
\]

Measured Theta Profiles for Test No. 37, Test Section V, Top Hot, \( J = 1 \)

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</tr>
</thead>
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</tr>
<tr>
<td>3</td>
<td>0.1500</td>
</tr>
<tr>
<td>4</td>
<td>0.2000</td>
</tr>
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<td>5</td>
<td>0.2500</td>
</tr>
<tr>
<td>6</td>
<td>0.3000</td>
</tr>
</tbody>
</table>

Measured Theta Contours for Test No. 37, Top Hot.

Original page is of poor quality.
TMain = 417.3 K  TJet = 319.0 K  Theb = 0.0641  Blorrt = 3.850  Dernatio= 1.316  Tratio = 0.764

\[ \frac{X}{H_0} = 1.000 \quad \frac{X}{D_J} = 9.40 \]

V. Top Hot, J = 8.51, S/D = 4.00, H/D = 6.00

FOR TEST NO. 37. TOP HUT, J = 8.51, S/D = 4.0, H/D = 8.0

Figure 85

144
PREDICTED THETA CONTOURS FOR TEST NO. 37, TOP HOT

\[
\begin{align*}
S/DJ &= 4.70 \\
H0/DJ &= 9.40 \\
VRATIO &= 2.54 \\
TRATIO &= 0.764 \\
DNRATIO &= 1.316 \\
TMA &= 1.00 \\
X/H &= 0.25 \\
X/DJ &= 2.35 \\
\end{align*}
\]

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 37, TEST SECTION V, TOP

FOLDOUT FRAME  ORIGINAL PAGE IS OF POOR QUALITY
FOR TEST NO. 37, TOP HOT, J=8.51, S/D=4.0, H/D=8.0

\[\frac{0.764}{0.764} = 1.316\]

\[T_{\text{MAIN}} = 417.3\, \text{K}\quad T_{\text{JET}} = 319.0\, \text{K}\quad \text{THEB} = 0.014\]

\[X/H = 1.00\quad X/DJ = 9.40\]

Figure 86

37. TEST SECTION V, TOP HOT, J = 8.51, S/D = 4.00, H/D = 8.00

ORIGINAL PAGE IS OF POOR QUALITY
\[ \rho = 0.0508 \text{ Meters} \quad S/DJ = 4.925 \quad H_0/DJ = 9.851 \quad V_{\text{MAIN}} = 16.0 \text{ M/SEC} \quad V_{\text{JET}} = 75.4 \text{ M/SEC} \quad T_{\text{MAIN}} = 416.1 \text{ K} \quad T_{\text{JET}} = \]

**Measured Theta Profiles for Test No. 38, Test Section V, Top Hot**

<table>
<thead>
<tr>
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</thead>
<tbody>
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<tr>
<td>6</td>
<td>0.3000</td>
</tr>
<tr>
<td>7</td>
<td>0.3500</td>
</tr>
</tbody>
</table>

**Measured Theta Contours for Test No. 38, Top Hot, J =**

*Original page is of poor quality*
Figure 87

For Test No. 38, Top Hot, J=30.24, S/D=4.0, H/D=8.0

M/SEC TMAIN = 416.1 K TJET = 314.5 K THEB = 6.1067 BLOBAT = 7.163 DENRATIO = 1.356 TRATIO = 0.756

X/HO = 1.000
X/OJ = 9.85

V, TOP K9T J = 30.24 S/D = 4.00 H/D = 8.00

0.2000 0.2500 0.3000 0.3500 0.4000 0.5000 0.6000 0.7000

0.0

TRANSVERSE DIST. Z/S

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ECOD UOT FRAMES

Figure 87

146
PREDICTED THETA CONTOURS FOR TEST NO. 38, TOP

S/DJ = 4.93  NO/DJ = 9.85  VRATIO = 4.72  TRATIO = 0.756  DENRATIO=1.356

X/H = 0.25  X/DJ =2.46

COMPARISON BETWEEN DATA AND CORRELATIONS FOR TEST NO. 38, TEST SECTION V, TOP

ORIGINAL PAGE IS OF POOR QUALITY.
CONTOURS FOR TEST NO. 38, TOP HOT, J=30.24, S/D=4.0 H/D=8.0

TRATIO = 0.756 DENRATIO = 1.356 TMAIN = 416.1 K TJET = 314.5 K THEB = 0.023
X/H = 1.00 X/DJ = 0.85

TEST NO. 38, TEST SECTION V, TOP HOT, J = 30.24, S/D = 4.00, H/D = 8.00

Figure 88
APPENDIX A

LIST OF SYMBOLS

A  test section cross-sectional area at survey plane
D  geometric orifice diameter
Dj  effective orifice diameter
Ho  duct height at the jet injection plane
H  local duct height at the survey plane
J  momentum ratio \( \left( \frac{p_j V_j^2}{p_m V_m^2} \right) \)
Pt  stagnation pressure
Ps  static pressure
S  orifice spacing
T  temperature
V  velocity
X  X direction, parallel to duct axis
y  y direction, parallel to orifice centerline (radial direction)
Z  Z direction, normal to duct axis (transverse direction)

Greek

\( \theta \)  temperature difference ratio
\( \rho \)  density
\( \alpha \)  jet injection angle

Subscripts

av  average
EB  equilibrium value
j  jet property
max  maximum
m  cross-flow property, average value
APPENDIX B

REFERENCES


