

PERFORMANCE ASSESSMENT OF PLANETARY MISSIONS
AS LAUNCHED FROM AN ORBITING SPACE STATION

PRESENTED BY

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TO

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AT

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INTRODUCTION

THE PLANETARY/SPACE STATION ISSUE

WOULD DEVELOPMENT OF A LOW EARTH-ORBIT SPACE STATION
ENABLE NEW PLANETARY EXPLORATION OPPORTUNITIES?.....

.....ALTERNATIVELY, WOULD THE EXISTENCE OF A LOW EARTH-
ORBIT SPACE STATION AND ITS MANDATED USE ADVERSELY AFFECT
PLANETARY EXPLORATION OPPORTUNITIES?

APPROACH AND SCOPE OF ANALYSIS

- DESCRIBE THE BASIC CHARACTERISTICS AND MANEUVER STRATEGIES FOR LAUNCHING PLANETARY MISSIONS FROM A SPACE STATION IN EARTH ORBIT.

- QUANTIFY THE "INHERENT" PROS AND CONS IN TERMS OF:
 - INJECTED MASS CAPABILITY OF SELECTED UPPER STAGES
 - PLANE CHANGE PENALTIES
 - LAUNCH TIMING PENALTIES

- COMPARE STATION-LAUNCHED AND STANDARD SHUTTLE-LAUNCHED PERFORMANCE FOR A WIDE RANGE OF PLANETARY MISSION OPPORTUNITIES OVER LAUNCH ENERGY AND INJECTED MASS SPACE.
 - MARS GEOCHEMICAL ORBITER (LOW ENERGY, MODERATE MASS)
 - MARS SAMPLE RETURN (LOW ENERGY, LARGE MASS)
 - MULTIPLE ASTEROID RENDEZVOUS (LOW ENERGY, LARGE MASS)
 - ANTEROS RENDEZVOUS (MODERATE ENERGY, MODERATE MASS)
 - MERCURY ORBITER (MODERATE ENERGY, LARGE MASS)
 - TITAN PROBE (HIGH ENERGY, SMALL MASS)
 - URANUS/NEPTUNE PROBES (HIGH ENERGY, MODERATE MASS)
 - SATURN ORBITER/PROBE (HIGH ENERGY, MODERATE MASS)
 - GANYMEDE ORBITER (HIGH ENERGY, MODERATE MASS)
 - COMET RENDEZVOUS (HIGH ENERGY, MODERATE MASS)

GROUND RULES AND ASSUMPTIONS

RATIONALE

- STATION ORBIT PARAMETERS

ALTITUDE 200 NM, CIRCULAR
INCLINATION 28.3°
NODAL POSITION ANY AND ALL

MOST PROBABLE PLACEMENT WITH MAX-
IMUM UTILIZATION OF SHUTTLE CARGO
CAPACITY; YIELDS CONSERVATIVE
PLANETARY PERFORMANCE CONCLUSIONS

- UPPER STAGE SELECTION

IUS(II)
WIDE BODY CENTAUR
OTV (MSFC 18' OTV)
STAR 48 AS NEEDED

SET HAS WELL-DEFINED PERFORMANCE
PARAMETERS OVER A RANGE OF CAP-
ABILITY; OTV ADDS OPPORTUNITY FOR
EXTENDED DEPARTURE MANEUVERS AND
REUSABILITY

- SPACECRAFT PROPULSION

EARTH-STORABLES
SOLIDS

UTILIZES PRESENT PROPULSION TECH-
NOLOGY YIELDING CONSERVATIVE
PERFORMANCE RESULTS

- STATION DEPARTURE

ON TIME (0^d WINDOW)

COMPARABLE TO SHUTTLE UPPER-STAGE
CRITERIA; PERFORMANCE CONSEQUENCE
OF DEPARTURE DELAYS IS EXAMINED

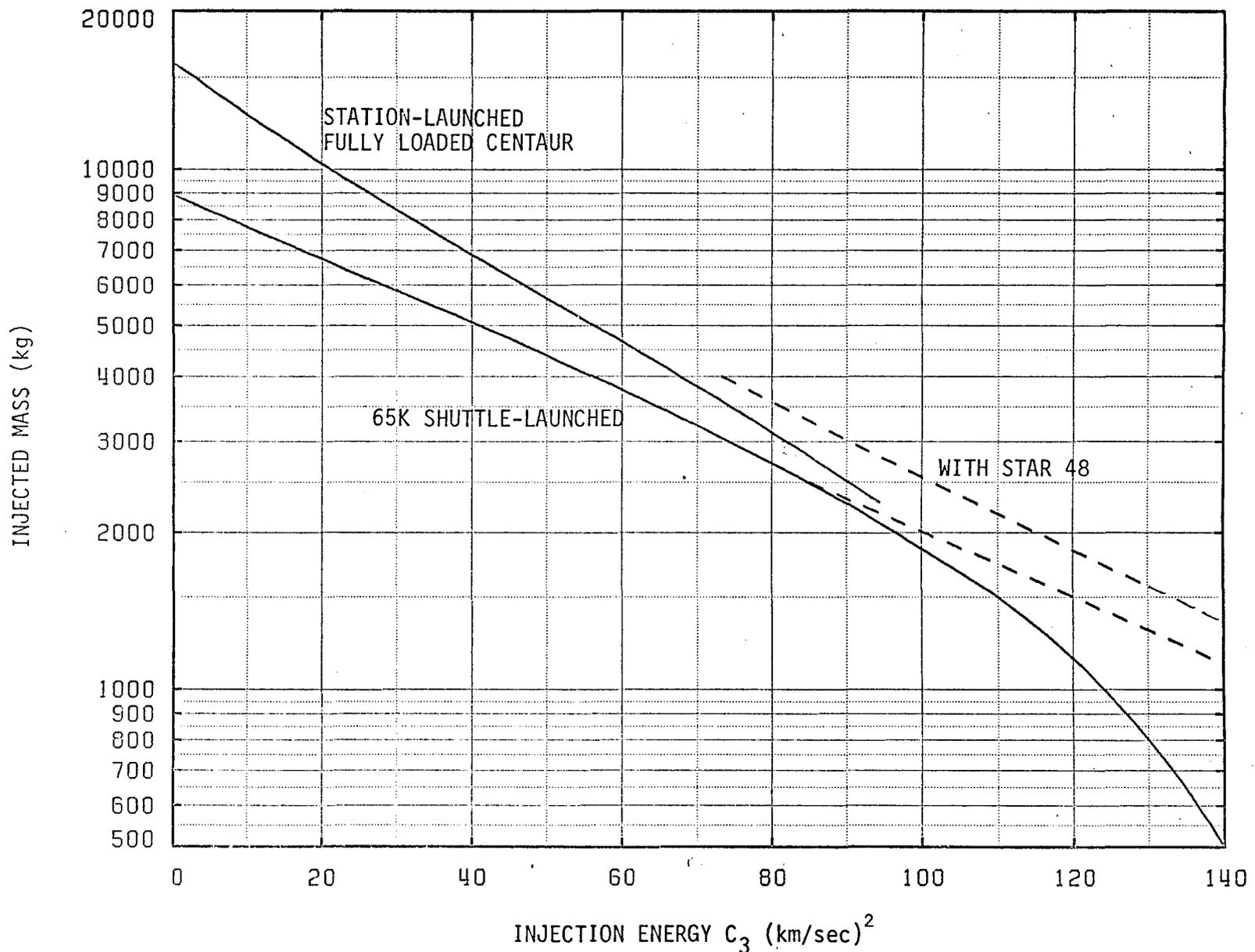
SPACE STATION PROS & CONS - QUALITATIVE ASSESSMENT

PROS

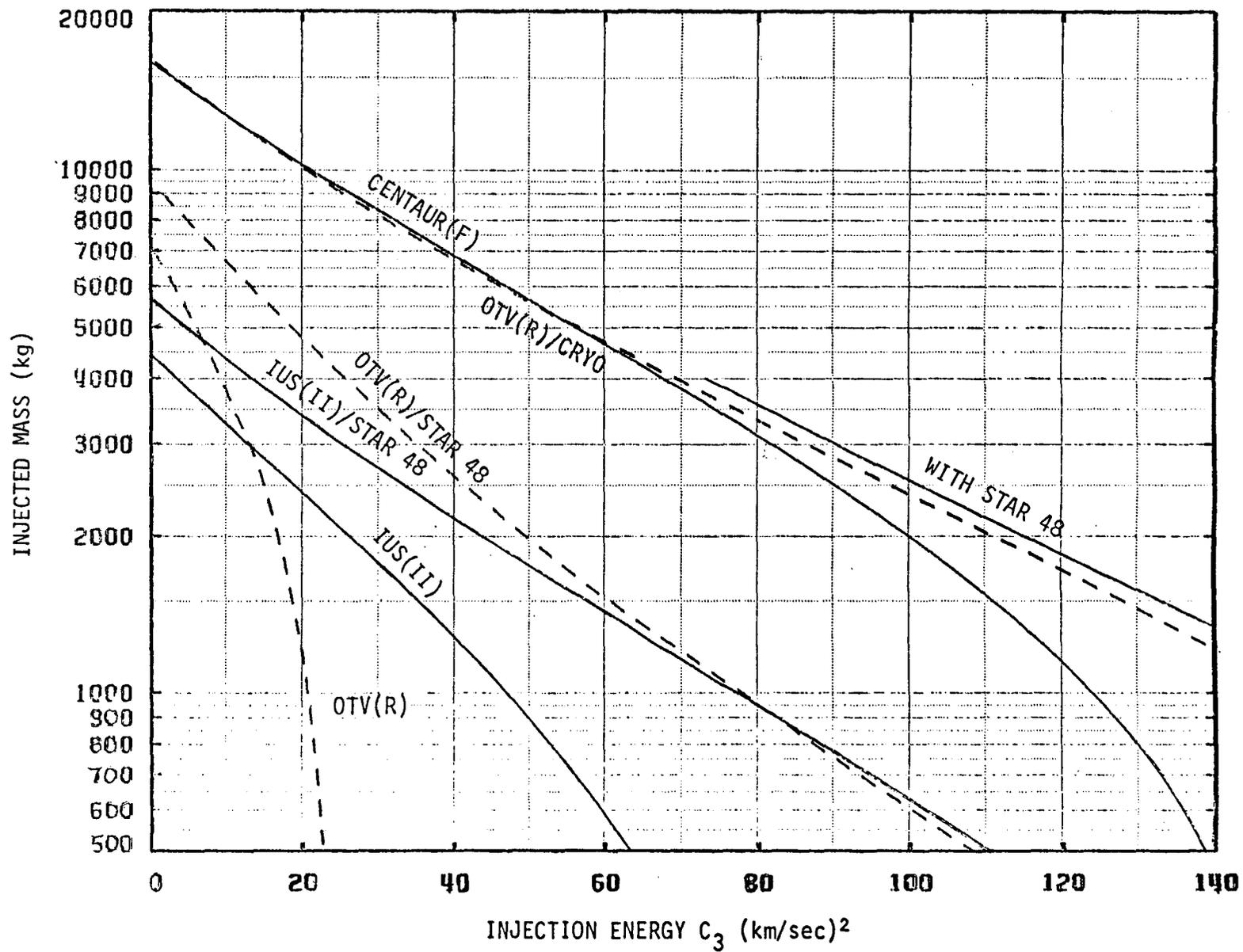
- MAXIMIZES SHUTTLE UTILIZATION
- ALLEVIATES SHUTTLE MANIFESTING THROUGH EARLY AND/OR FRACTIONAL LAUNCHES OF PAYLOAD
- ALLOWS FINAL CHECK-OUT AND ASSEMBLY IN SPACE ENVIRONMENT AFTER LAUNCH
- ASSURES FULLY LOADED STAGES
- POTENTIAL FOR "BEST-TIME" PLANETARY LAUNCHES (NO LAUNCH WINDOWS REQUIRED)
- ENHANCES REUSABLE STAGE OPTION

CONS

- HIGH PROBABILITY OF MISSING OPTIMUM LAUNCH DATE DUE TO NODAL MISALIGNMENT
- HIGHER SENSITIVITY TO DLA-INCURRED PERFORMANCE PENALTIES
- MAXIMIZED PERFORMANCE IMPLIES MORE SHUTTLE LAUNCHES
- ADDED COST FOR ON-ORBIT PAYLOAD STORAGE, CHECK-OUT AND ASSEMBLY



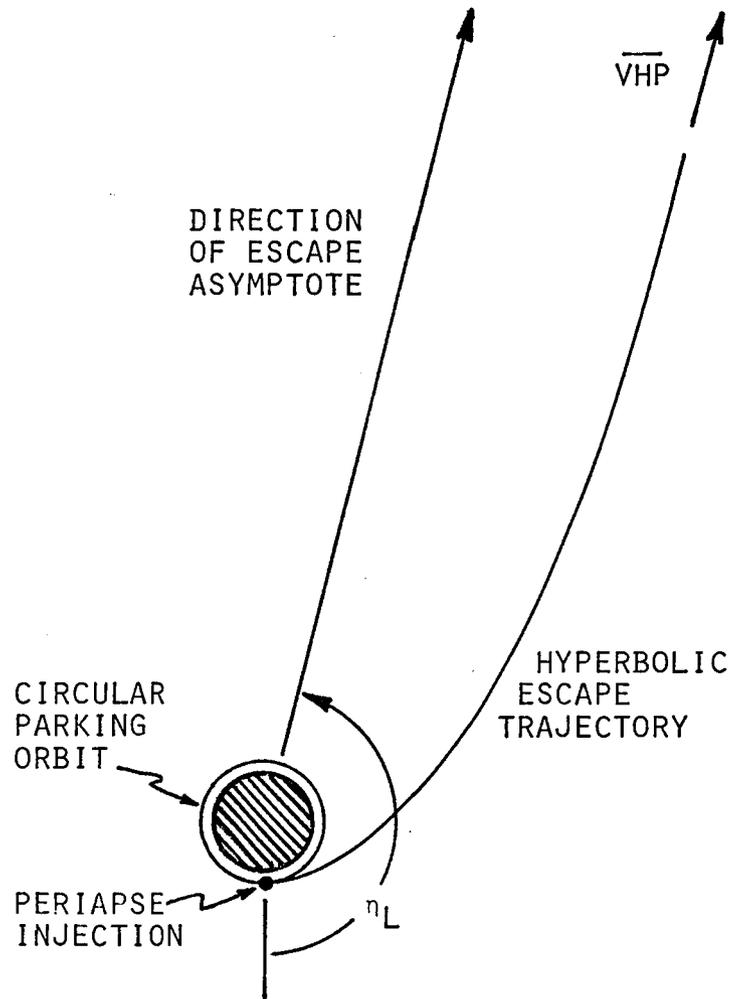
WIDE BODY CENTAUR LAUNCH PERFORMANCE



SPACE STATION-LAUNCHED UPPER STAGE PERFORMANCE

DESCRIPTION

CHARACTERISTICS OF PLANETARY ESCAPE



$$C_3 = |\overline{VHP}|^2$$

$$\eta_L = \cos^{-1} \left[\frac{-\mu}{\mu + R_p C_3} \right]$$

WHERE: μ = EARTH'S GRAVITATIONAL PARAMETER

R_p = PERIAPSE RADIUS

C_3 = VIS VIVA INJECTION ENERGY

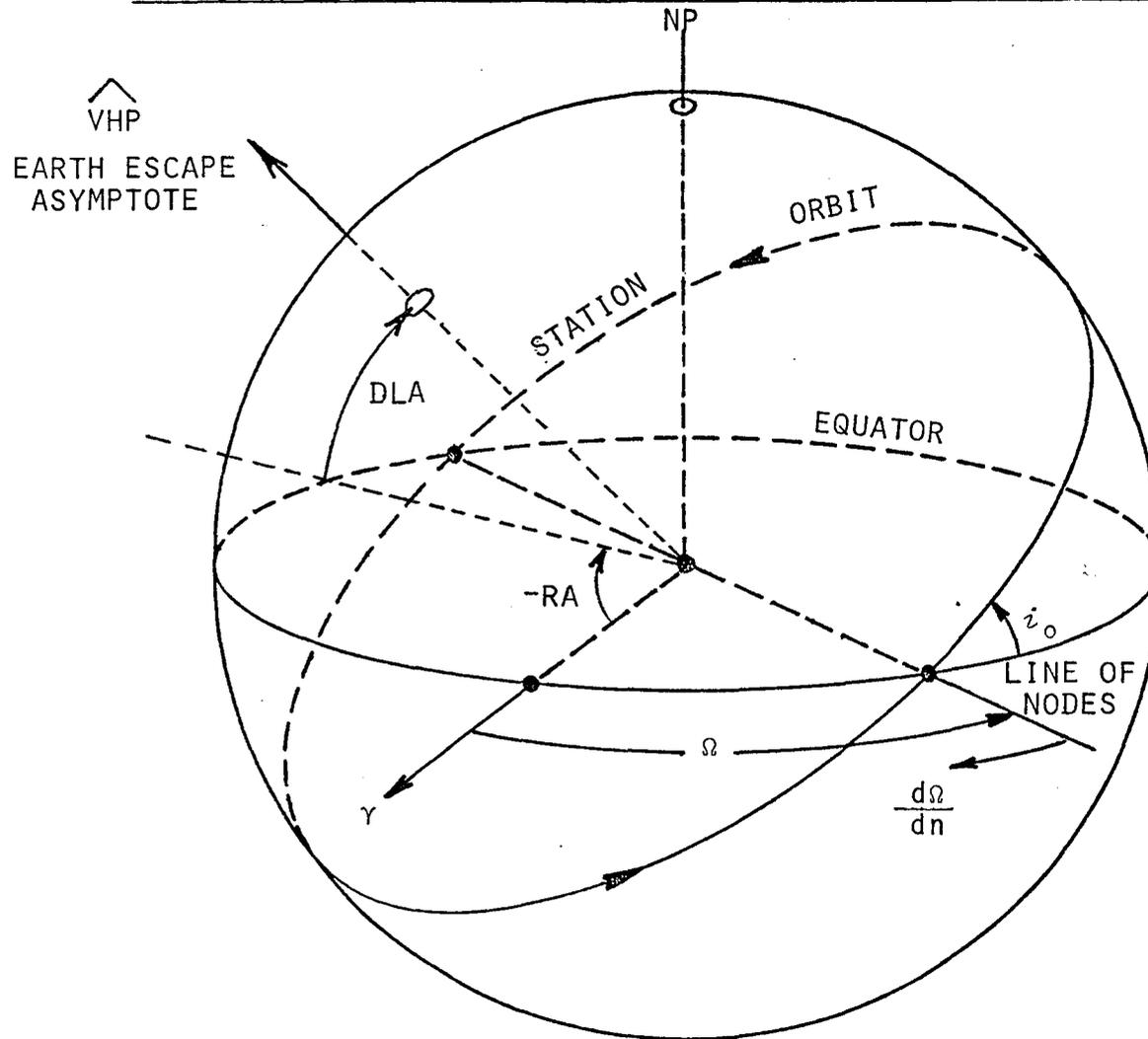
$\eta_L = 180^\circ$ WHEN $C_3 = 0$ (PARABOLIC ESCAPE)

$\eta_L = 90^\circ$ WHEN $C_3 = \infty$

$$E = \frac{mv^2}{2}$$

$$\frac{2E}{m} = v^2$$

SPACE STATION ORBITAL GEOMETRY



ORBIT PARAMETERS:

ALTITUDE, $h = 200\text{nm}$ (CIRCULAR)

INCLINATION, $i_0 = 28.3^\circ$

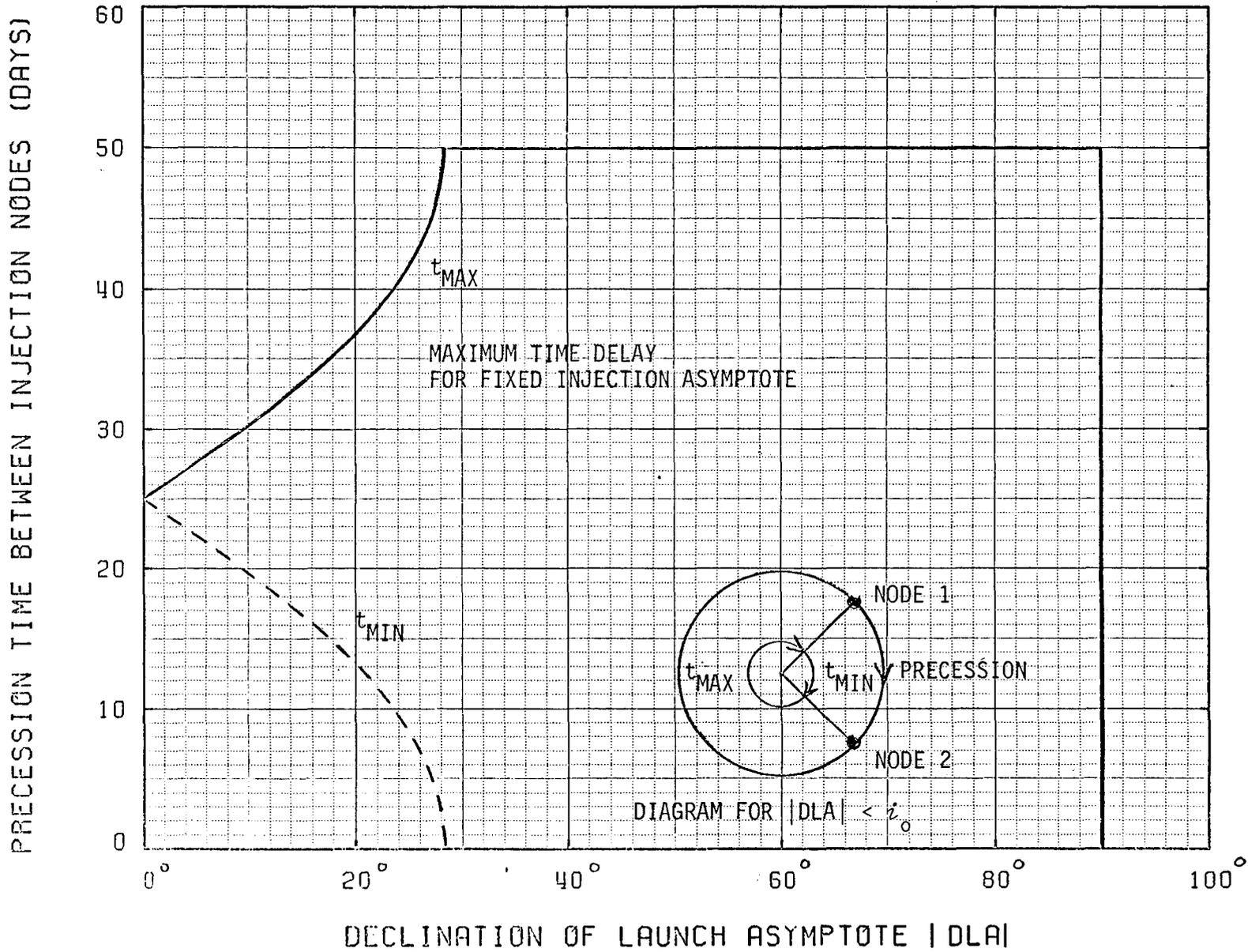
ASCENDING NODE, $\Omega = \text{VARIABLE}$

NODAL REGRESSION, $\frac{d\Omega}{dt} = 0.46^\circ/\text{REV}$
 $= 7.2^\circ/\text{DAY}$

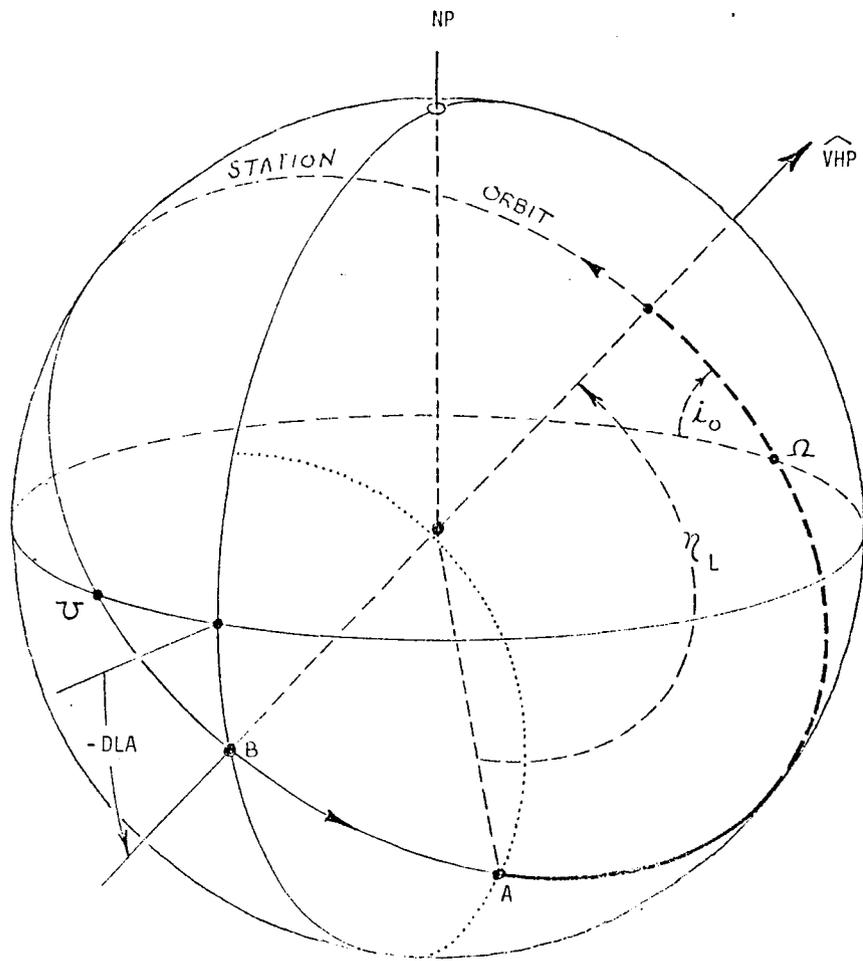
LAUNCHING PLANETARY MISSIONS FROM A SPACE STATION

- WHEN A PLANETARY MISSION OPPORTUNITY OCCURS, THE DIRECTION OF EARTH ESCAPE (\hat{VHP}) IS RELATIVELY CONSTANT ACROSS THE LAUNCH WINDOW, WHICH TYPICALLY LAST 20 - 40 DAYS DEPENDING ON THE TARGET.
- CONVERSELY, THE STATION ORBIT PLANE IS CONSTANTLY PRECESSING DUE TO THE OBLATENESS OF THE EARTH; FOR THE ASSUMED ORBIT (200 NM CIRCULAR AT 28.3° INCLINATION) THE NODAL PRECESSION IS 7.2%/DAY IN THE OPPOSITE DIRECTION TO THE STATION'S ORBITAL MOTION.
- ASSUMING THE ANGLE (DECLINATION, DLA) OF \hat{VHP} TO THE EARTH'S EQUATOR IS LESS THAN THE ORBIT INCLINATION, THERE WILL, THEREFORE, BE ONLY TWO TIMES EVERY 50 DAYS ($360^\circ/7.2$) WHEN \hat{VHP} LIES IN THE STATION ORBIT PLANE, WHICH IS THE CONDITION FOR OPTIMUM COPLANAR ESCAPE. AT ALL OTHER TIMES A PLANE CHANGE (AND PERFORMANCE LOSS) IS REQUIRED TO ACHIEVE THE CORRECT ESCAPE CONDITIONS.
- IF THE DECLINATION OF \hat{VHP} IS GREATER THAN THE ORBIT INCLINATION, AT NO TIME WILL \hat{VHP} BECOME COPLANAR WITH THE STATION ORBIT PLANE, AND ONLY ONCE EVERY 50 DAYS WILL IT COME CLOSEST TO THE PLANE MINIMIZING THE REQUIRED PLANE CHANGE (AND PERFORMANCE LOSSES).
- SINCE THESE CONDITIONS FOR OPTIMUM STATION DEPARTURE WILL NOT, IN GENERAL, COINCIDE WITH THE TIME OF MINIMUM C_3 ($C_3 = |\overline{VHP}|^2$) A TRADE-OFF EXISTS BETWEEN THE AMOUNT OF PLANE CHANGE REQUIRED AND THE C_3 OF OFF-OPTIMAL LAUNCH DATES.

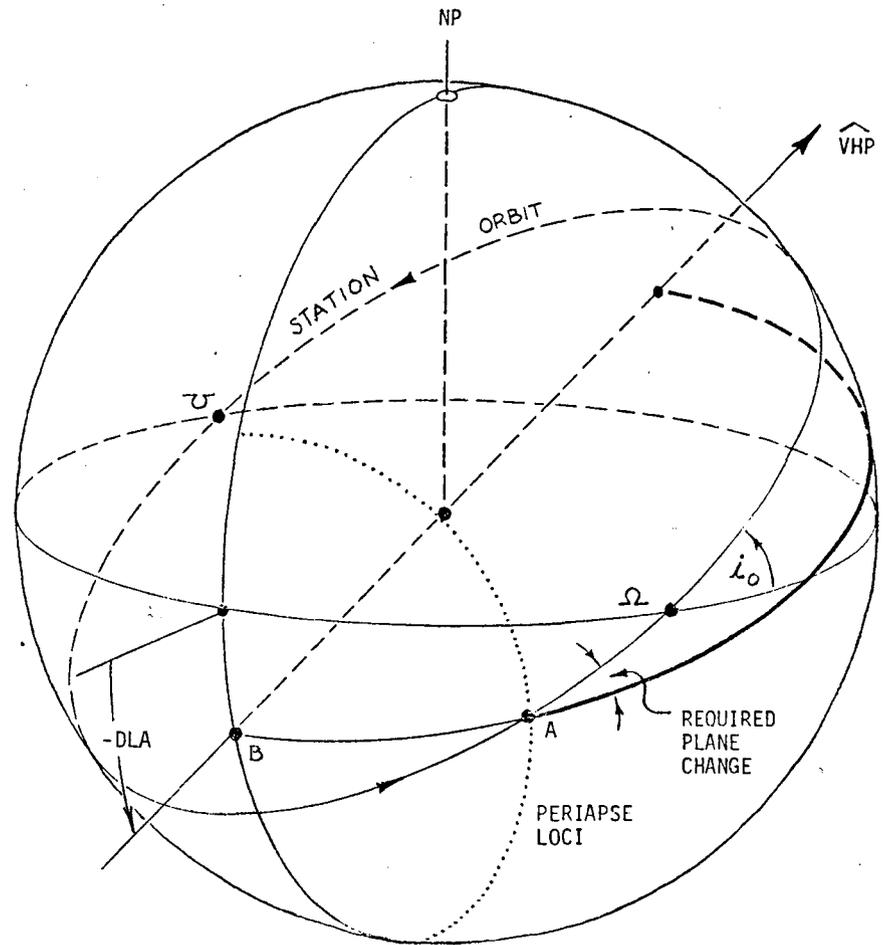
ORBIT ALTITUDE = 200 NM
 INCLINATION = 28.3 DEG
 PRECESSION = 7.2 DEG/DAY



LAUNCH TIMING EFFECT OF SPACE STATION ORBIT PRECESSION



CASE A
OPTIMUM STATION ORBIT ORIENTATION



CASE B
OFF-OPTIMUM STATION ORBIT ORIENTATION
(COMBINED MANEUVER STRATEGY SHOWN)

NOTE: $DLA < i_0$
A \equiv ESCAPE IMPULSE POINT

SPACE STATION/PLANETARY INJECTION STRATEGIES

UTILIZATION PRIORITIES

- ACTIVE (PROPULSIVE PLANE CHANGES)

- EARTH-ORBITAL

- SPLIT MANEUVER
 - COMBINED MANEUVER
 - THREE-IMPULSE MANEUVER

AS NEEDED FOR DLA TARGETING & LAUNCH DELAYS

- STATION ORBIT REALIGNMENT: EXPENSIVE
 - NON-PLANAR ESCAPE: LESS EXPENSIVE
 - APOAPSE PLANE CHANGE: LEAST EXPENSIVE
(BUT REQUIRES 24^h INTERMEDIATE ORBIT)

- INTERPLANETARY

- BROKEN PLANE TRANSFERS

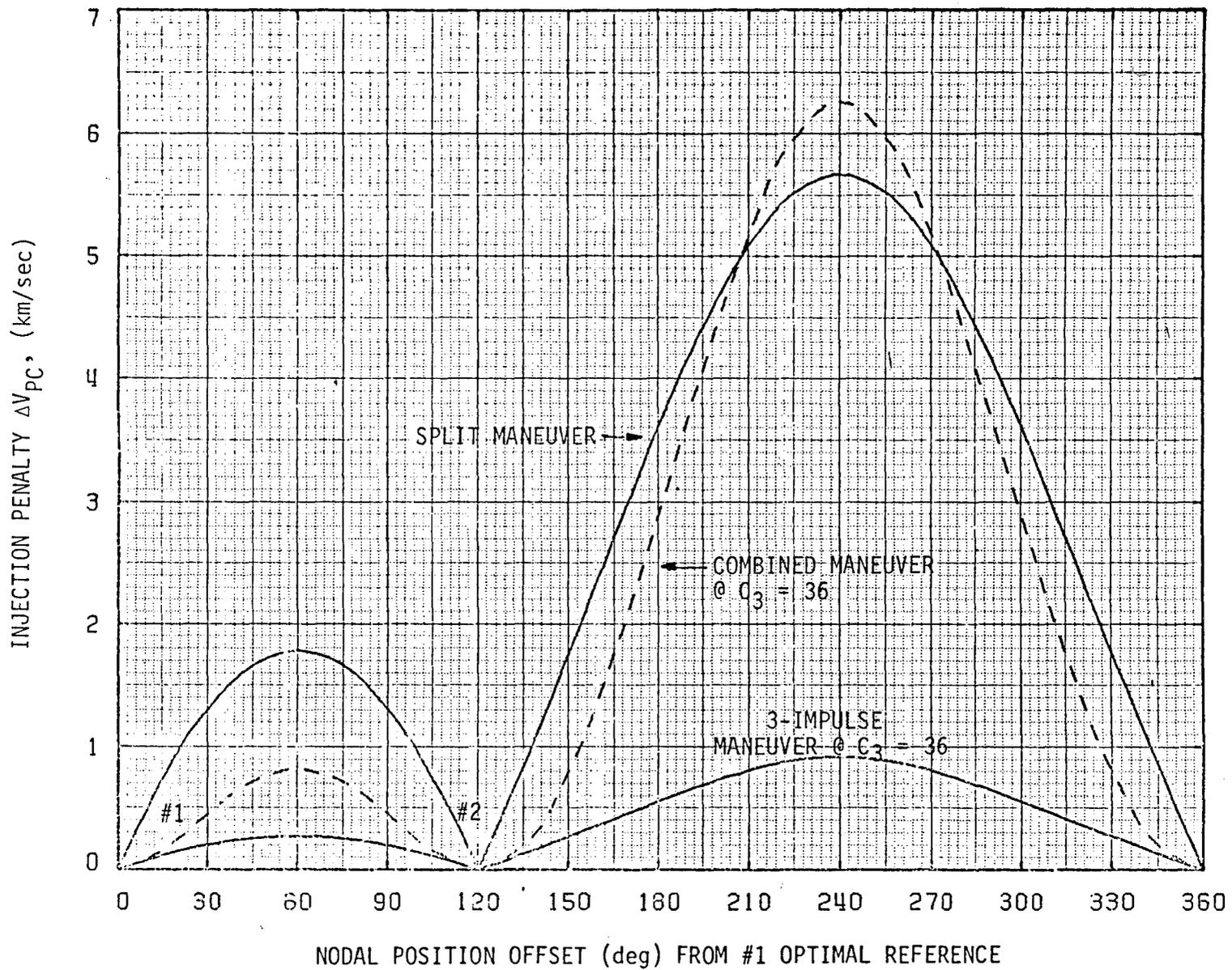
VERY EFFECTIVE ON SOME MISSIONS IN REDUCING DLA PENALTIES AND IN IMPROVING OFF-OPTIMAL ESCAPE REQUIREMENTS FOR PASSIVE STRATEGY (SEE BELOW)

- PASSIVE (LAUNCH DATE TIMING)

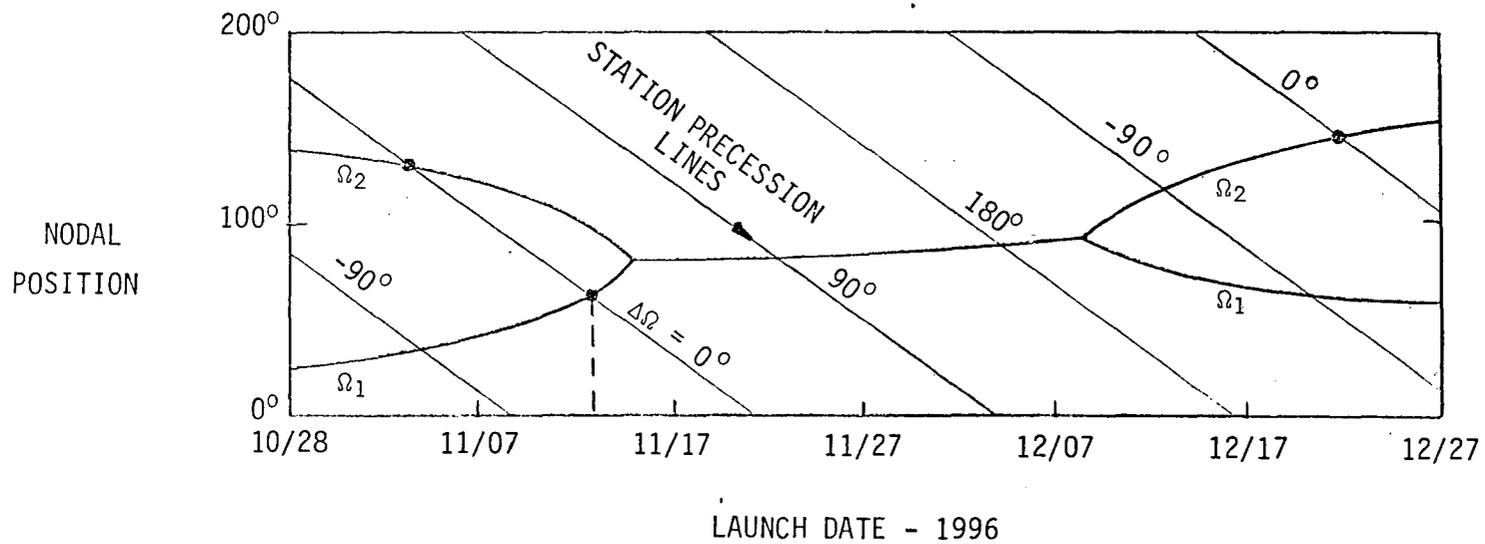
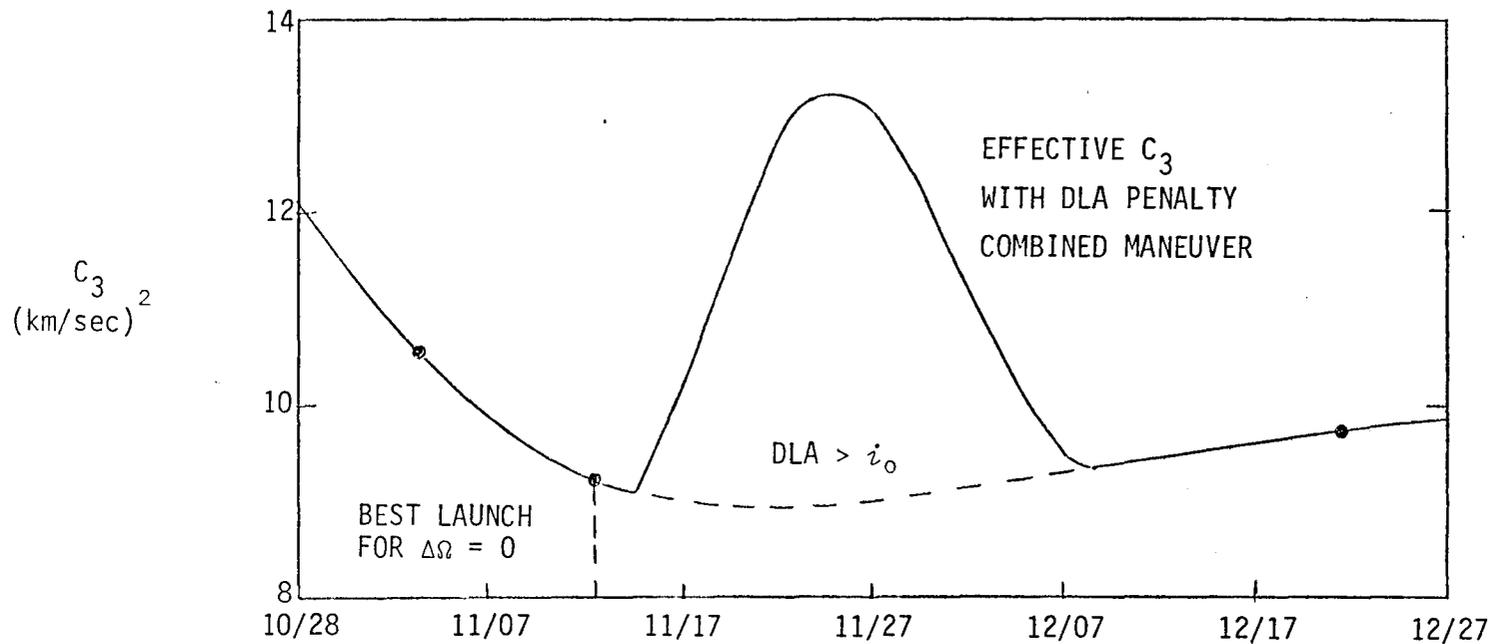
- STATION ORBIT PRECESSION

BASELINE SOLUTION

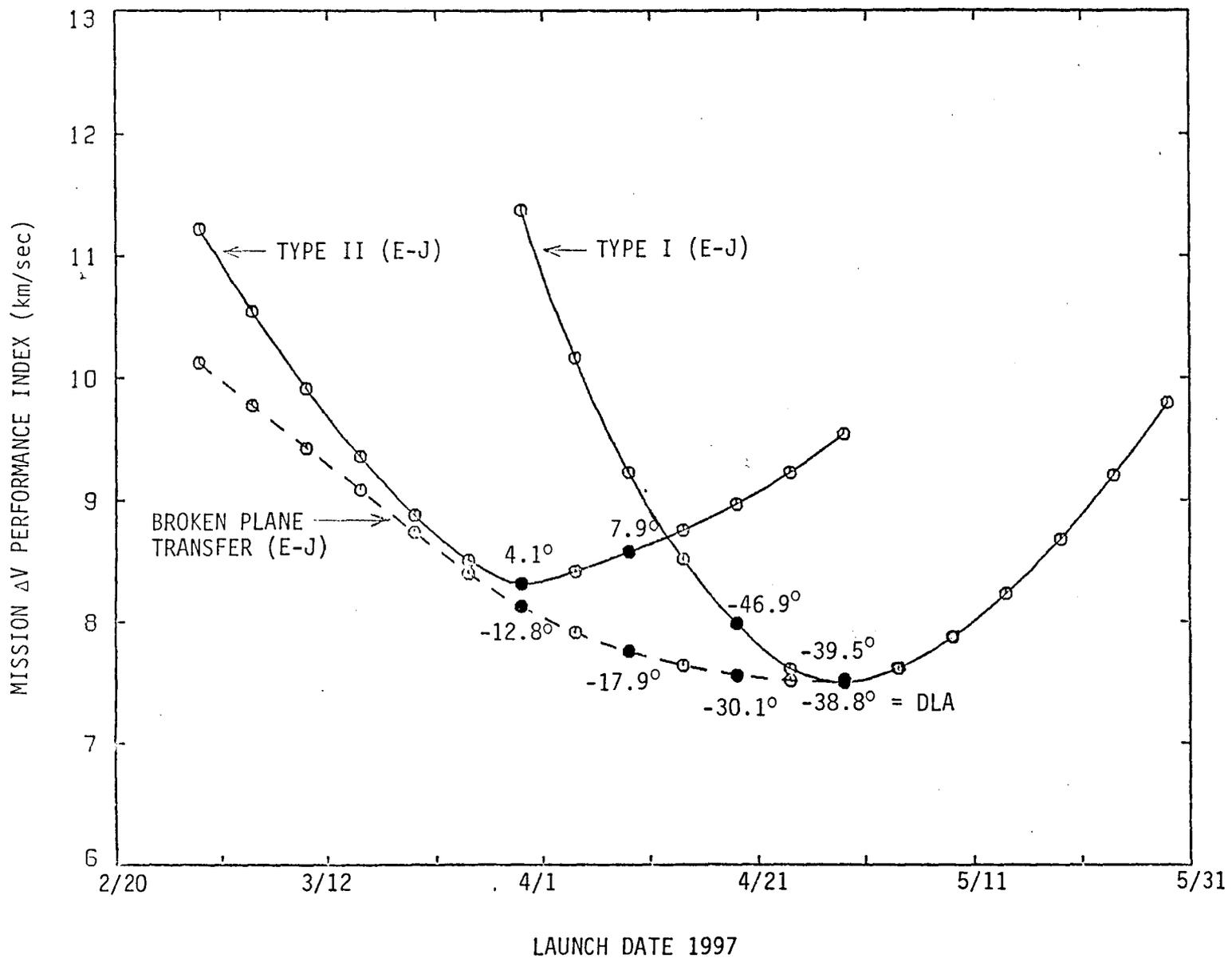
WAITS FOR ORBIT REALIGNMENT, ACCEPTING SOME PERFORMANCE LOSS FROM RESULTING OFF-OPTIMAL LAUNCH DATE



STATION ORBIT INJECTION TO $|DLA| = 15^\circ$ WITH CORRECTION OF NODAL POSITION OFFSET



SELECTION OF LAUNCH DATE VIA PRECESSION - 1996 MARS SAMPLE RETURN



ADVANTAGE OF BROKEN-PLANE TRANSFERS - 1997 J/S SATURN ORBITER/PROBE MISSION

EXAMPLE
RESULTS

CHARACTERISTICS OF EXAMPLE MISSIONS

<u>MISSION</u>	<u>LAUNCH YEAR</u>	<u>FLIGHT MODE/OPTION</u>	<u>NOMINAL PAYLOAD*</u>	<u>COMMENTS</u>
MARS GEOCHEMICAL ORBITER	1992	300km CIRCULAR ORBIT	505 KG	$T_F = 0.9^y$
MARS SAMPLE RETURN	1996	a) ORBIT RENDEZVOUS b) DIRECT RETURN	5 MODULES SEE BREAKDOWN	$T_F = 2.7^y$ AEROCAPTURE TECH.
MERCURY ORBITER	1994	a) HI-LO ORBITER b) DUAL ORBITERS	725 KG IN 12 ^h ORBIT** 1050 KG IN 12 ^h ORBIT**	VENUS SWINGBY (2) $T_F = 2.4^y$
ANTEROS RENDEZVOUS	1997 1999	a) GOOD OPPORTUNITY b) POOR OPPORTUNITY	600 KG	$T_F = 1.2^y$ $T_F = 1.1^y$, HIGH DLA
ASTEROID MULTIPLE RENDEZVOUS	1992	MARS SWINGBY	600 KG	$T_F = 4.5^y$, 2 TARGETS
COMET TEMPEL 2 RENDEZVOUS	1994	DIRECT	600 KG	$T_F = 5^y$
TITAN PROBE	1995	DIRECT, SATURN FLYBY	250 KG PROBE 580 KG BUS	$T_F = 3.5^y$
URANUS/NEPTUNE PROBES	1992	DIRECT, TANDEM LAUNCH JUPITER SWINGBY	235 KG PROBE (x2) 560 KG BUS (x2)	$T_F = 6.7^y$ $T_F = 10^y$
SATURN ORBITER/PROBE	1997 1998	a) FAIR J/S OPP. b) GOOD J/S OPP.	250 KG PROBE 650 KG ORBITER	$T_{FU} = 5.5^y$, HIGH DLA $T_{FU} = 5.5^y$
GANYMEDE ORBITER	2000	DIRECT	650 KG	$T_F = 3.5 - 4.3^y$ WITH SATELLITE G/A TOUR

*NET SPACECRAFT MASS EXCLUDING PROPULSION

**MERCURY ORBITERS INCLUDES PROPULSION FOR CIRCULARIZATION

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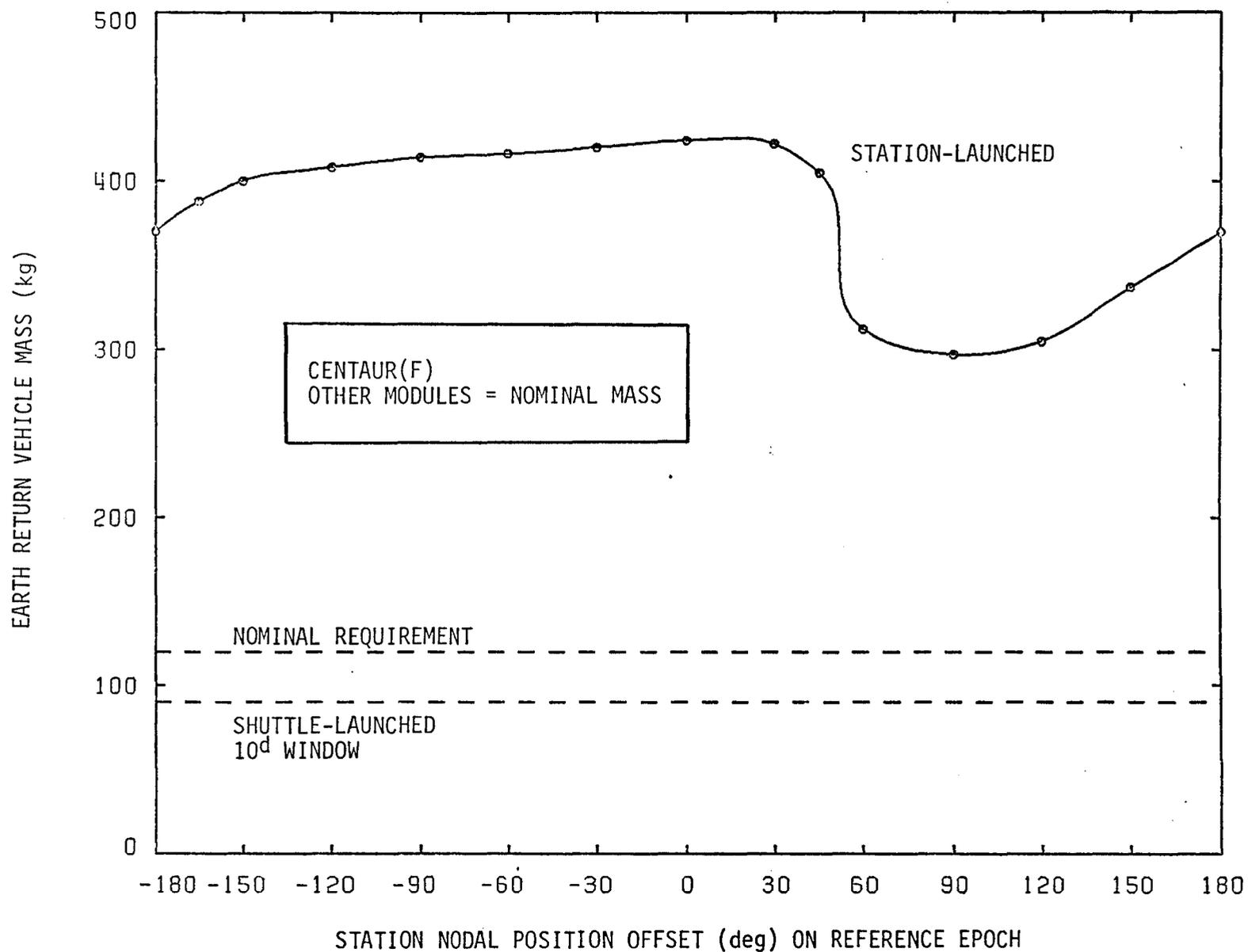
1996 MARS SAMPLE RETURN MISSION - MASS DEFINITION

<u>SYSTEM MASS ELEMENT</u>	- - - NOMINAL VALUE (KG) - - -	
	<u>DIRECT RETURN MODE</u>	<u>MOR MODE</u>
AEROCAPTURE/ENTRY	1500	1500
ORBITER	-	550
LANDER (W/ROVER)	650	650
ASCENT VEHICLE SUBSYSTEMS	-	95
EARTH RETURN VEHICLE	120	-
SAMPLE CAPSULE	30	30
SAMPLE	<u>5</u>	<u>5</u>
SUBTOTAL W/O PROPULSION	2305	2830

INJECTED MASS REQUIREMENT		
SHUTTLE-LAUNCHED	8320	5555
STATION-LAUNCHED*	8345 - 9085	5515 - 5910

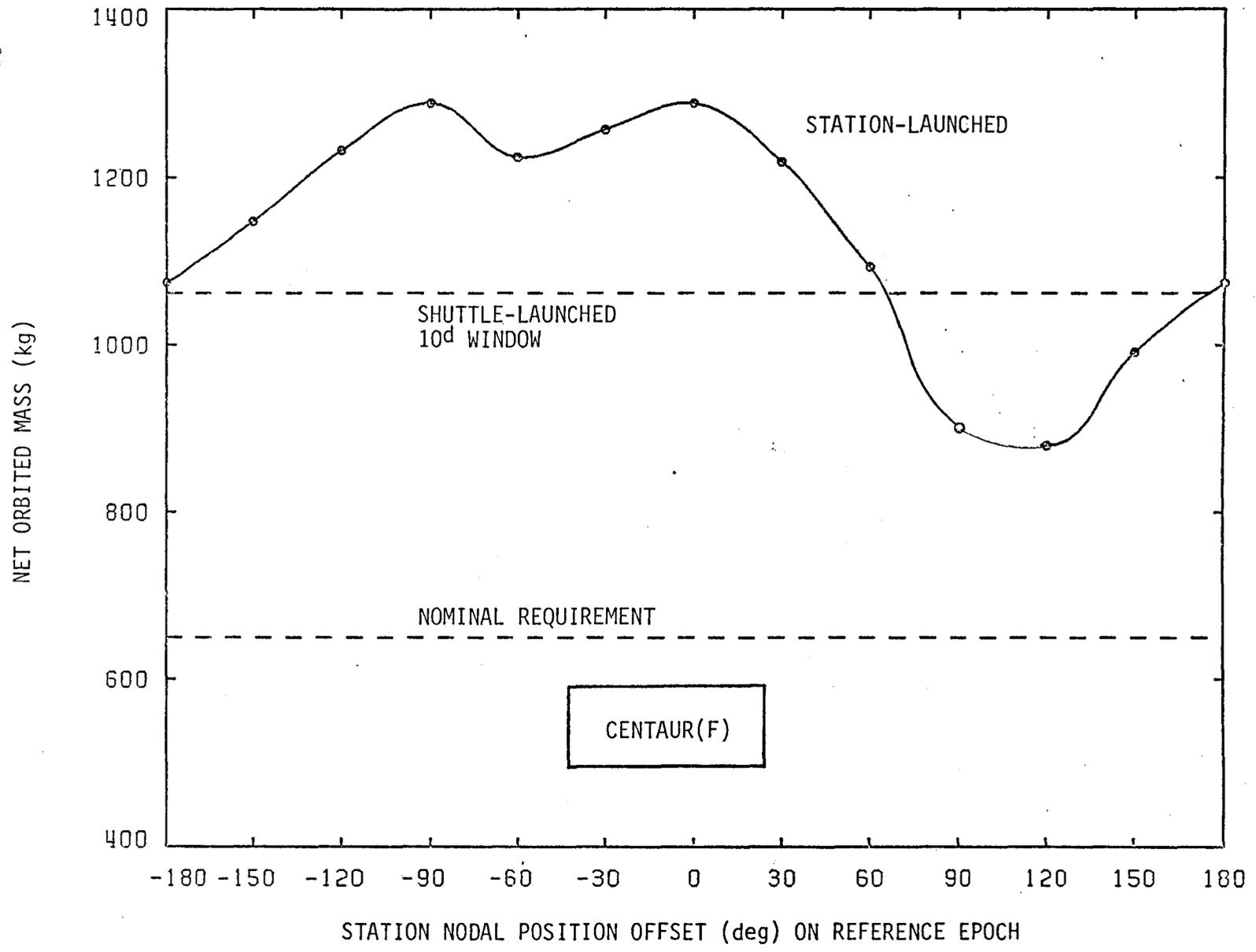
*RANGE OVER ALL POSSIBLE NODAL POSITIONS OF SPACE STATION

REFERENCE EPOCH = 15 NOV 1996
OPTIMAL LAUNCH TIMING STRATEGY



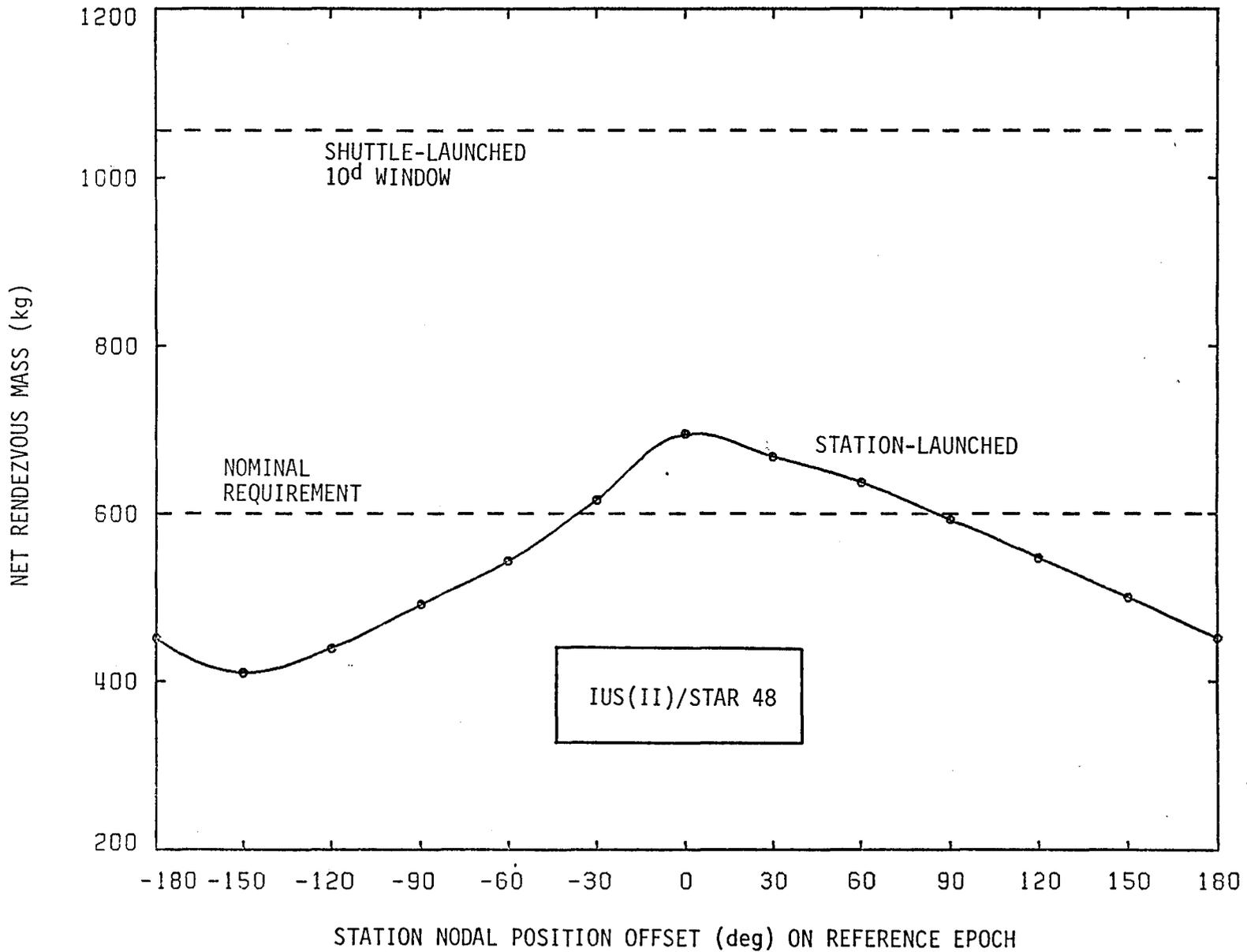
PERFORMANCE COMPARISON FOR 1996 MARS SAMPLE RETURN - DIRECT RETURN MODE

REFERENCE EPOCH = 28 MAY 1998
OPTIMAL LAUNCH TIMING & BROKEN PLANE STRATEGY



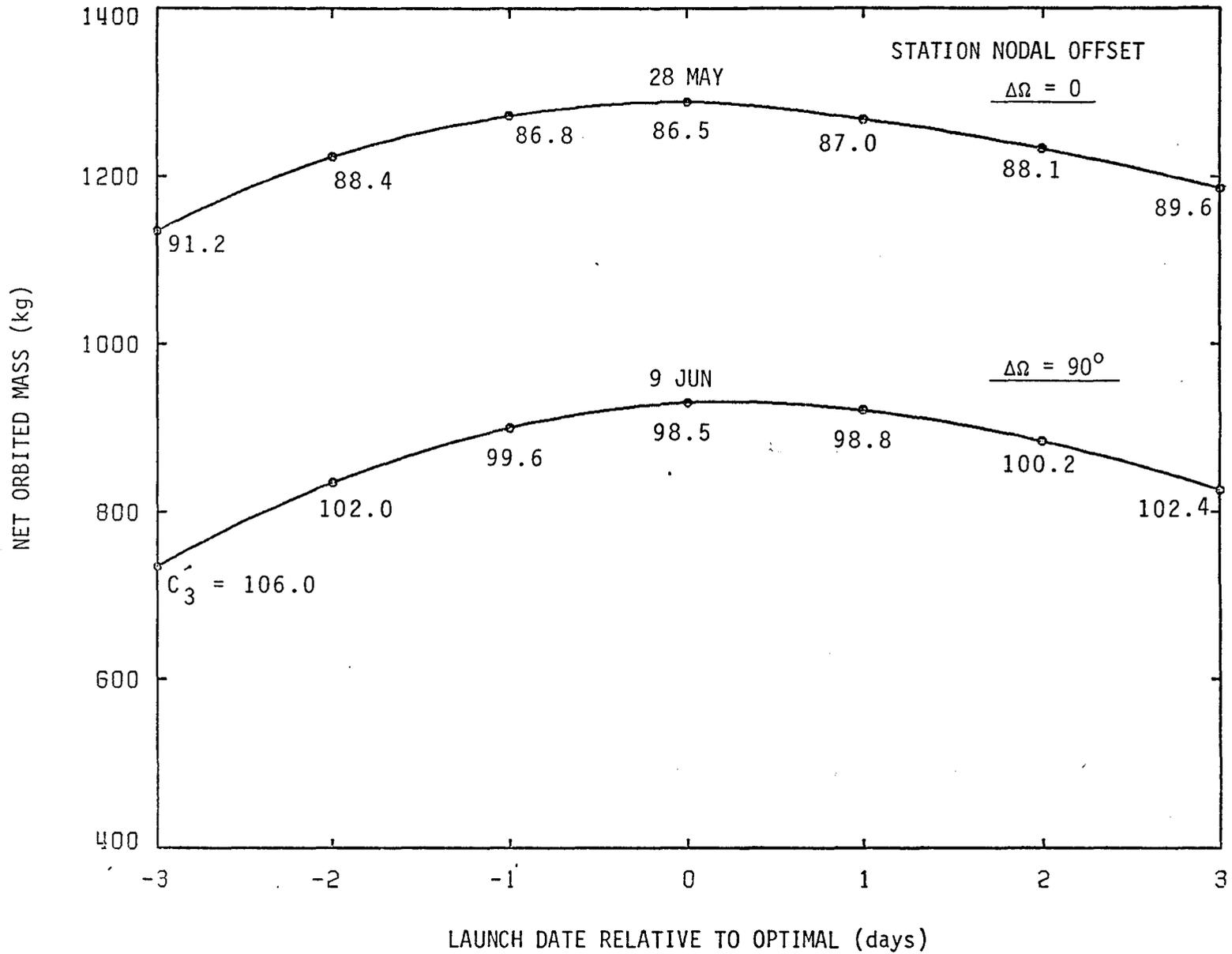
PERFORMANCE COMPARISON FOR 1998 J/S SATURN ORBITER (250 KG PROBE)

REFERENCE EPOCH = 30 JUN 1999
OPTIMAL LAUNCH TIMING & BROKEN PLANE STRATEGY



PERFORMANCE COMPARISON FOR 1999 ANTEROS RENDEZVOUS

CENTAUR(F) PERFORMANCE

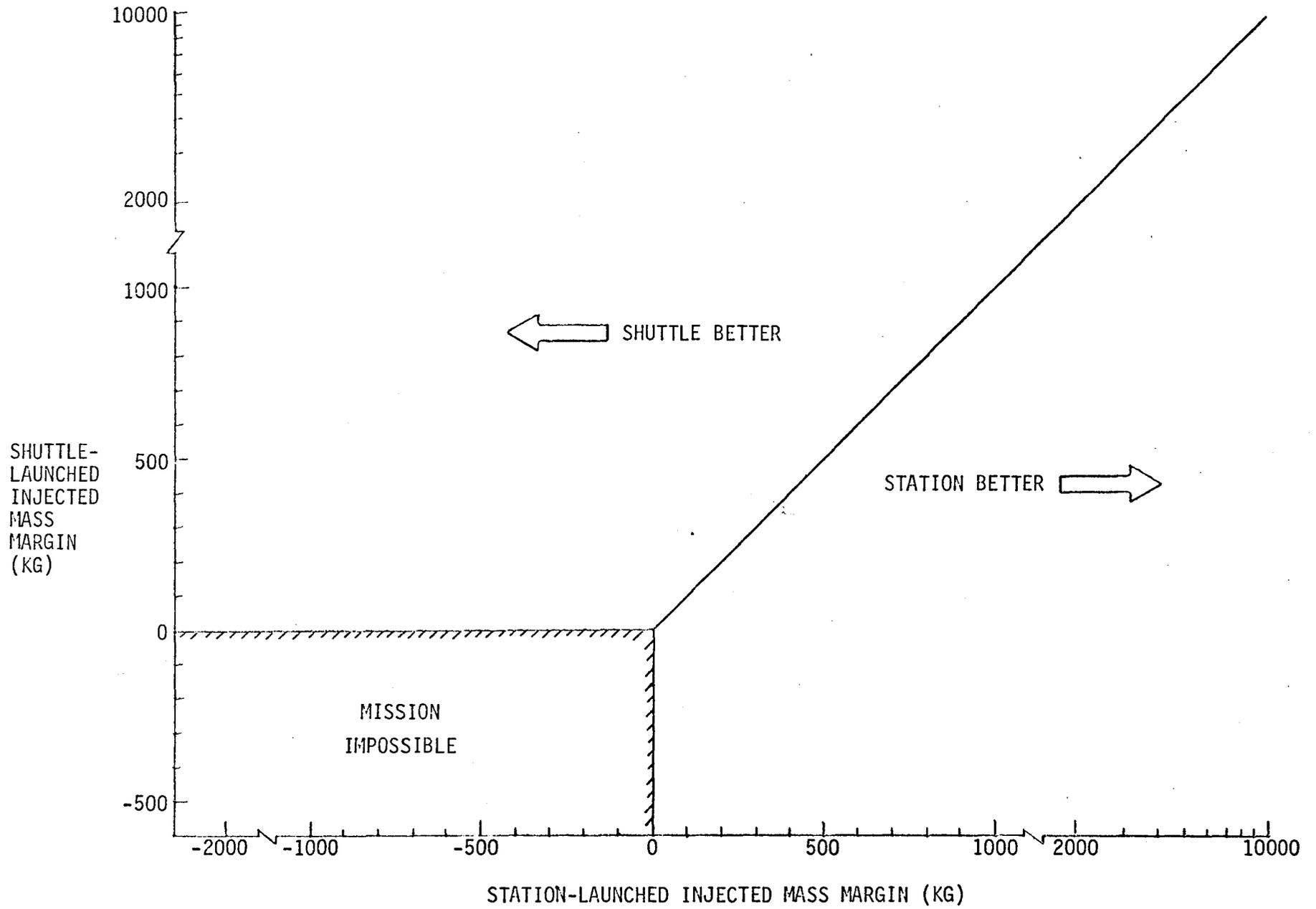


LAUNCH ON-TIME PENALTY - 1998 J/S SATURN ORBITER/PROBE MISSION

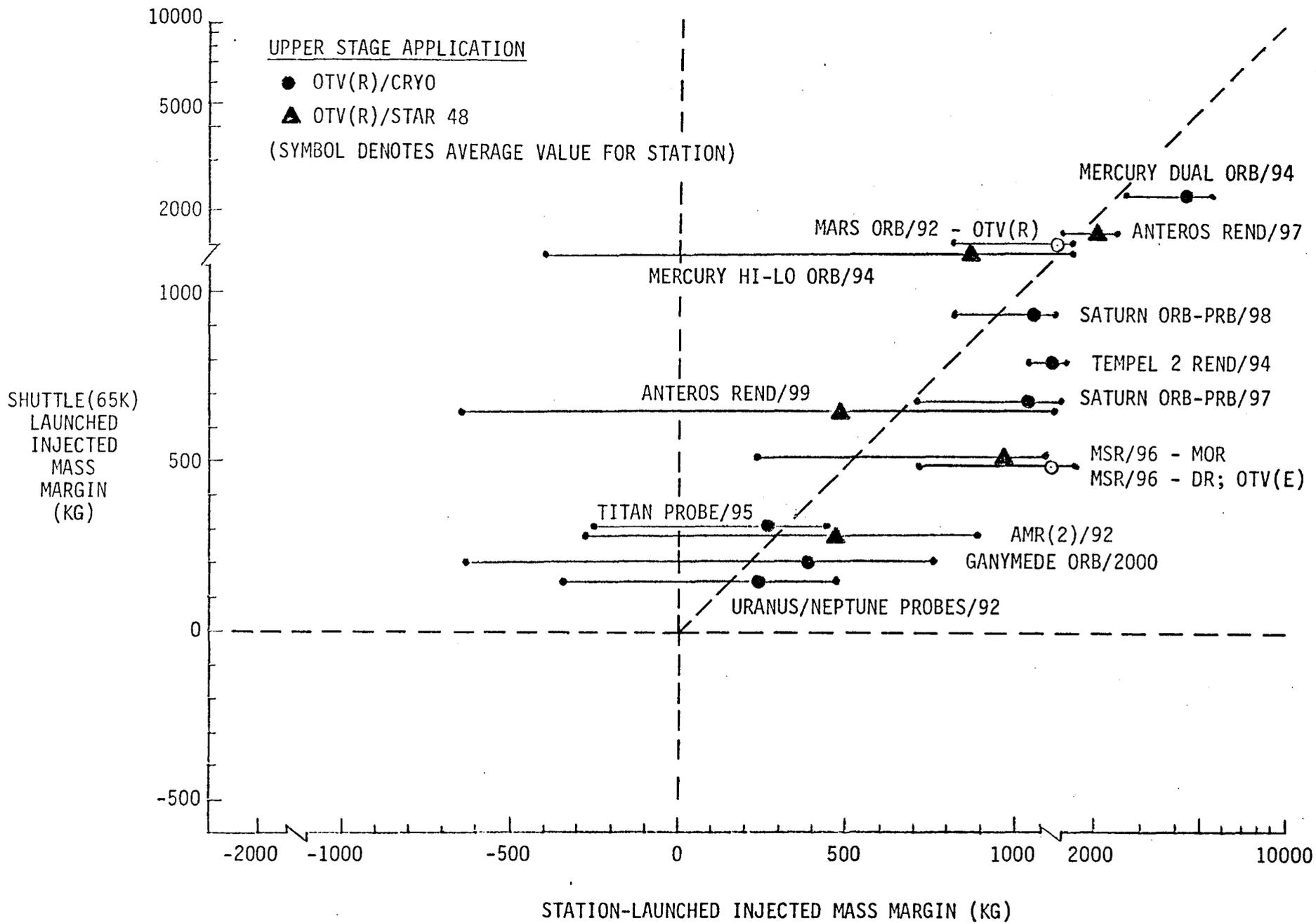
SUMMARY
OF RESULTS

CRITERIA FOR PERFORMANCE COMPARISON

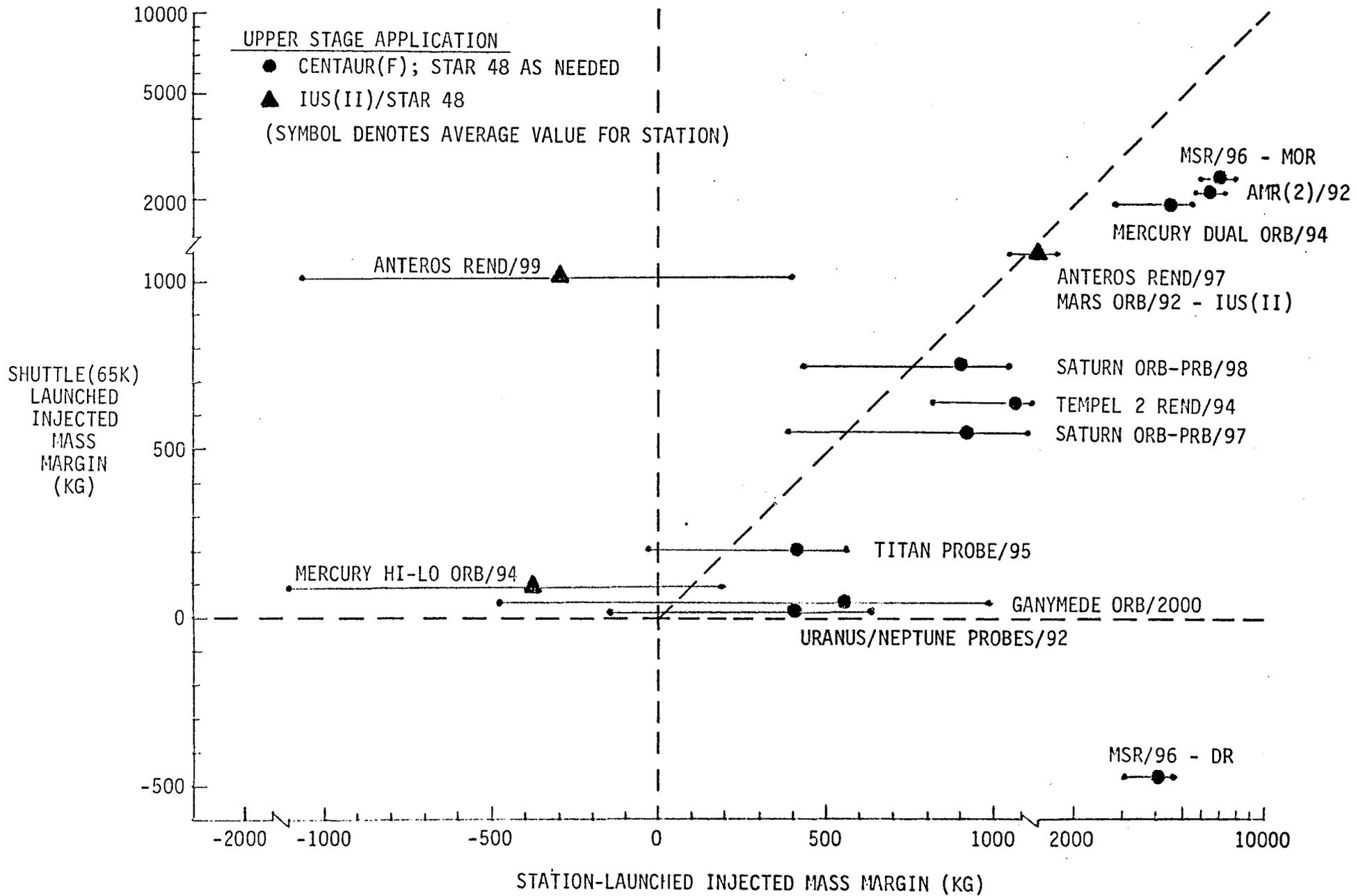
- FOR SPECIFIED NOMINAL PAYLOAD MASS, EXPRESS PERFORMANCE IN TERMS OF INJECTED MASS MARGIN. POSITIVE MARGIN IS MEASURE OF 'SAFETY' OR PAYLOAD GROWTH.
- FOR EACH MISSION, SELECT MINIMUM CAPABILITY UPPER STAGE THAT CAPTURES MISSION WITH SHUTTLE LAUNCH. IF MISSION CANNOT BE CAPTURED, SELECT MAXIMUM CAPABILITY STAGE.
- APPLY SAME UPPER STAGE FOR STATION-LAUNCHED MISSION.
- SHUTTLE LAUNCH WINDOW = 10 DAYS
STATION LAUNCH WINDOW \equiv 360° OF ALL POSSIBLE NODAL POSITIONS



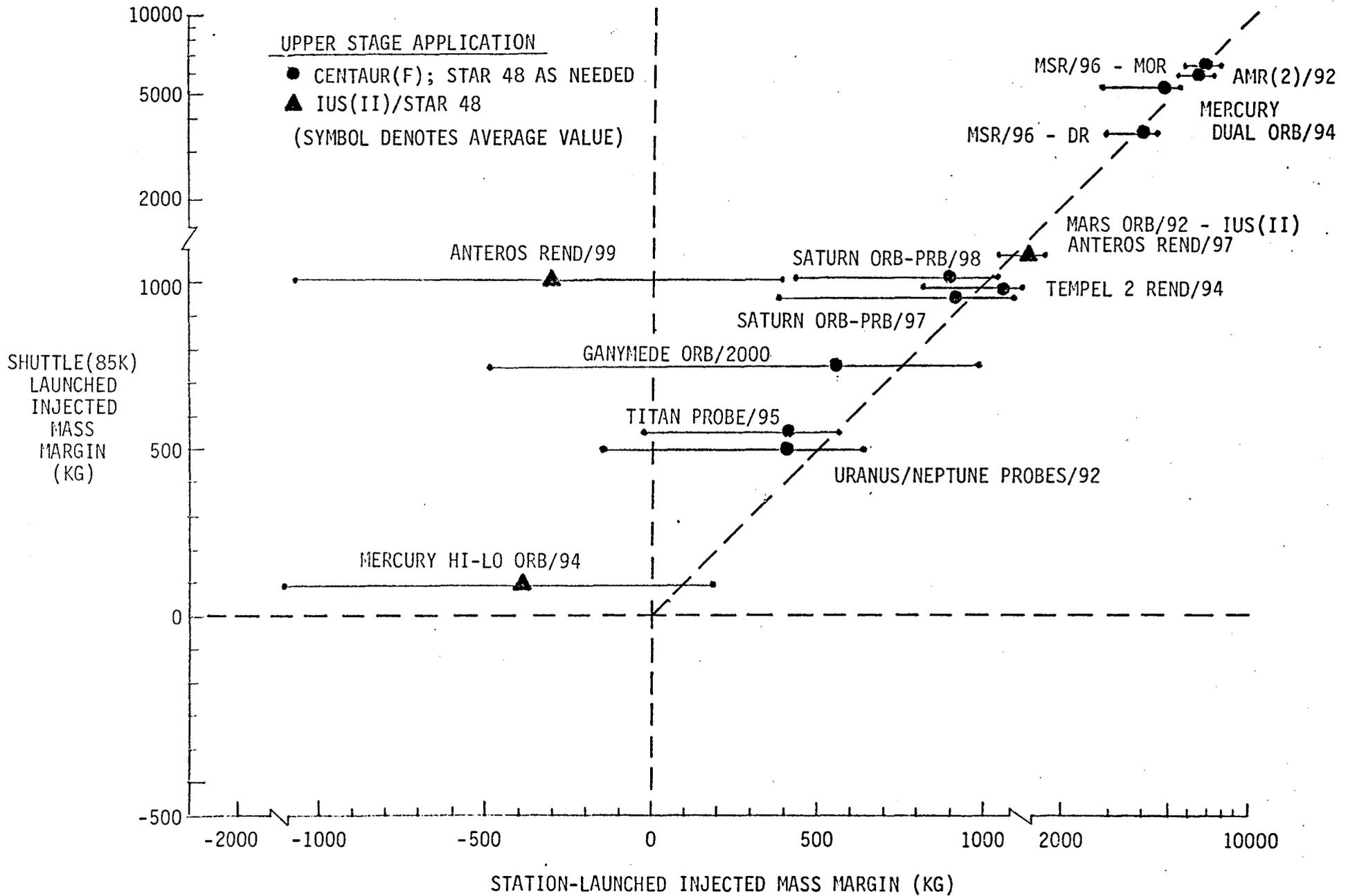
COMPARISON OF SHUTTLE AND SPACE STATION LAUNCHED MISSION PERFORMANCE



COMPARISON OF SHUTTLE(65K) AND SPACE STATION-LAUNCHED MISSION PERFORMANCE



COMPARISON OF SHUTTLE (65K) AND SPACE STATION-LAUNCHED MISSION PERFORMANCE



COMPARISON OF SHUTTLE (85K) AND SPACE STATION-LAUNCHED MISSION PERFORMANCE

CONCLUSIONS

- A FUNDAMENTAL TRADE-OFF EXISTS BETWEEN SHUTTLE-LAUNCHED AND STATION-LAUNCHED PLANETARY MISSIONS:
 - SHUTTLE LAUNCHES ARE FAVORED BY A MORE ADAPTIVE LAUNCH SITUATION WHICH, FOR A PROPELLANT-FIXED UPPER STAGE, WILL PRODUCE (ON AVERAGE) BETTER PAYLOAD PERFORMANCE
 - STATION LAUNCHES ARE FAVORED BY FREEDOM FROM STAGE PROPELLANT OFF-LOADING DUE TO SHUTTLE CARGO MASS CONSTRAINTS (WHICH MAY PRODUCE BETTER PERFORMANCE), AND BY AN ASSUMED LAUNCH-ON-TIME CAPABILITY

- FOR A BROAD RANGE OF MISSIONS, THESE TRADE-OFFS TEND TO FAVOR:
 - THE SHUTTLE FOR SMALLER PAYLOAD MISSIONS IMPLEMENTED WITH SMALLER UPPER STAGES (e.g. THE IUS(II))
 - THE SPACE STATION FOR LARGER PAYLOAD MISSIONS IMPLEMENTED WITH LARGER UPPER STAGES (e.g. THE WIDE-BODY CENTAUR) OR SPACE-BASED REUSABLE OTV'S
 - ASSUMING A 65K SHUTTLE, THE STATION IS ENABLING ONLY IN A NARROW SENSE FOR SOME MISSIONS (e.g. MSR-DIRECT RETURN MODE). FOR MOST MISSIONS OF INTEREST THE PAYLOAD MARGINS ARE QUITE SUFFICIENT WHETHER SHUTTLE OR STATION LAUNCHED.

- GIVEN THE AVAILABILITY OF AN UPRATED SHUTTLE (e.g. 85K), THE STATION OFFERS NO SIGNIFICANT PAYLOAD DELIVERY BENEFIT. THE ADVANTAGE SHIFTS SLIGHTLY IN FAVOR OF SHUTTLE-LAUNCHED MISSIONS.

- IN SUMMARY, PLANETARY MISSIONS CAN BE LAUNCHED FROM A SPACE STATION WITH NEITHER SIGNIFICANT PERFORMANCE BENEFIT NOR PENALTY.

- OTHER POTENTIAL NON-PERFORMANCE ADVANTAGES OF SPACE STATION (e.g. SHUTTLE MANIFESTING AND ORBIT CHECK-OUT) WILL BE SENSITIVE TO SPECIFIC DESIGN AND OPERATIONAL CHARACTERISTICS OF THE STATION AND ITS SHUTTLE INTERFACE.

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