

Digital Temperature and Velocity Control of Mach 0.3 Atmospheric Pressure Durability Testing Burner Rigs in Long Time, Unattended Cyclic Testing

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DIGITAL TEMPERATURE AND VELOCITY CONTROL OF MACH 0.3 ATMOSPHERIC
PRESSURE DURABILITY TESTING BURNER RIGS
IN LONG TIME, UNATTENDED CYCLIC TESTING

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SUMMARY

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Hardware and software were developed to implement the hybrid digital control of two Jet A-1 fueled Mach 0.3 burners from startup to completion of a preset number of hot corrosion flame durability cycle tests of materials at 1652 °F. This was accomplished by use of a basic language programmable micro-computer and data acquisition and control unit connected together by the IEEE-488 Bus. The absolute specimen temperature was controlled to ± 3 °F by use of digital adjustment of the fuel flow using a P-I-D (Proportional-Integral-Derivative) control algorithm. The specimen temperature was within ± 2 °F of the set point more than 90 percent of the time. Pressure control was achieved by digital adjustment of the combustion air flow using a proportional control algorithm. The burner pressure was controlled at 1.0 ± 0.02 psig.

Logic schemes were incorporated into the system to protect the test specimen from abnormal test conditions in the event of a hardware or software malfunction.

INTRODUCTION

Material durability testing in dynamic flame combustion products is in common use in the gas turbine and high temperature alloys industries (refs. 1 to 3). The determination and control of the true surface temperature has been a continuing problem and source of uncertainty in the results obtained from such tests. The burner rigs used in this testing have utilized analog (electromechanical) controlling instruments which implement proportional-integral control modes. With this type of control system, a temperature signal is usually obtained from an infrared optical sensor aimed at the test specimen and compared by electronic circuitry to a set point signal. The resulting error signal is used to adjust the position of a fuel valve in such a manner as to return the temperature to the set point. This is a real time feedback control system and if the proportional and integral parameters are set properly, it yields good average temperature control. The infrared temperature sensor requires calibration to account for specimen emissivity. If the emissivity changes as the test proceeds, for example from changing scale composition, the test results may be adversely affected. The use of a two-color optical pyrometer holds some promise of minimizing this problem provided that any changes in the emissivity of the surface are independent of the wavelength. This appears to be a good assumption for most oxides formed during high temperature metal corrosion.

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An absolute method of near surface temperature measurement can be attained by placing a small thermocouple in a hole located 5 to 10 mils (0.127 to 0.254 mm) beneath the surface. This has several practical drawbacks when applied to long time routine testing. First, the specimen is rotating so a slip ring must be used to bring out the signal. The slip ring assembly can require much maintenance when used in long time testing and may also introduce noise into the signal. Furthermore, a hole for the thermocouple must be drilled in each test specimen which increases their cost. Finally, small diameter thermocouple wire is fragile and may tend to rupture when changing specimens.

The setting of the proportional and integral parameters of an analog controller is tedious and requires often readjustment. Furthermore, even with the best settings, the low thermal inertia of the burner rig system causes large and rapid changes in the fuel valve throughput to quickly reduce the temperature error to zero and achieve the desired temperature control. This action causes large variations in the instantaneous fuel-to-air ratio which in turn produces a flame with a pulsating temperature and this causes excessive carbon buildup in the combustor. This latter problem can alter the flame pattern and parameters of the burner.

To control the flame velocity a second controller is required for the combustion air flow. This controller compensates for pressure changes in the combustion chamber caused by changes in the flame temperature. There is thus some interaction between the fuel and air flow controllers.

A further complication of the analog control system is imposed by the temperature cycling required in most material durability testing. At the conclusion of the heating cycle time, the flame is removed from the test specimen and its temperature falls rapidly. The specimen temperature sensor then signals the analog controller to open the fuel valve in an effort to raise the specimen temperature to the set point. If this action is not quickly arrested, the flame is blown out. The arrest of the fuel valve travel is accomplished by deviation circuitry in the analog controller which switches the controller from automatic to manual control mode. The setting of this cutoff point is critical and tedious. For example if set too high, a large temperature overshoot occurs on heatup in the next heating cycle: on the other hand if set too low, the test temperature is not reached on heat up and the controller remains in the manual mode. Furthermore, experience has demonstrated that the cutoff point setting changes with time.

Durability testing usually involves long duration tests in which the test is proceeding unattended much of the time. During these periods many changes in the environment to which the specimen is exposed may occur, such as the change in test temperature caused by a variation in the cutoff setting described above. The interpretation of test results for specimens tested under varying and sometimes questionable conditions is greatly suspect. Also, specimens become more costly as the test time increases and the prevention of non-normal testing is a necessary goal. Experience has proven that this is not easily achieved by analog (electromechanical) technology alone. The purpose of the work reported here was to determine the feasibility of using a digital computer to control one or more burner rigs.

The approach used was to control the temperature and pressure through the use of a digital microcomputer system (refs. 4 to 9). This approach uses a

programmable computer which, via a suitable interface, acquires information about the temperature, pressure, and other system parameters. The computer program then calculates appropriate feedback control signals. This type of control is really a simulation of a manual mode whereby the fuel or air valve are adjusted by small incremental steps ("tweaked") only when needed. In this way the fuel to air ratio is not varied rapidly or over a large range; it is only slowly "nudged" in the direction necessary to adjust the temperature and pressure to their respective set points. The frequency and magnitude of this fine adjustment ("nudging") can be readily obtained by software using any one or a combination of control algorithms. One of the most commonly used is a real time P-I-D feedback loop. Also, the special and difficult problem of transition from heating to cooling and back to heating, presented by cyclic testing, can be easily handled in a positive way through software by using a hardware generated burner position signal. Tests for abnormal conditions can be made through software logic and burner shutdown action can be initiated.

Satisfactory digital control of two independent burner rigs, burning Jet A-1 fuel, has been accomplished using a single computer. The absolute specimen temperature was controlled to ± 3 °F. For >90 percent of the time the temperature was within ± 2 °F of the set point. Burner pressure was controlled at 1.0 ± 0.02 psig to yield flame velocity control at Mach 0.3 ± 0.02 .

HARDWARE

Figure 1 is a photograph of a burner rig used in this study and shows the layout of the major components. The burner is in position to heat the specimen. In the cooling position it rotates about the pivot so that the flame misses the test specimen and a flow of compressed air impinges on the specimen. The fiber optic cable conducts the light from the specimen to the two color optical pyrometer detector located beneath the table. A cutaway specimen rotating on its own long axis is shown. This specimen geometry is used to reduce temperature gradients and yield more meaningful test results (ref. 10). A two color optical pyrometer provides the temperature dependent control signal. This type of pyrometer compensates for emissivity.

Figure 2 is a schematic diagram of the total control system. The data acquisition and control unit is the heart of the system. It contains circuit boards for input and output of signals and is totally controllable by the computer. The level of the input voltages from the transducers are measured by a 5-1/2 digit system voltmeter. These voltages are converted to engineering units by software. The digital outputs from the computer are converted to current flows by the output boards. The boards output 0 to 20 mA in 10 000 digital steps, that is 0.002 mA per step. It was found that a change of 10 digital steps moved the fuel valve stem a distance of 1 mil (0.0254 mm) and changed the temperature of the specimen by 1 °F for the burner configuration used. It should be kept in mind that the above digital calibration of the analog system is given for reference purposes and was found to vary slightly on day-to-day basis. The data acquisition and control unit is connected to the microcomputer and printer by the standard IEEE-488 Handshake Bus.

It will be noticed that this is a hybrid system that is partly computer controlled (digital) and partly analog (electromechanically) controlled. This configuration evolved because the computer was applied to an existing system

which has previously totally controlled by analog (electromechanically) systems. For example, while the combustion air preheater is turned on by computer control the air temperature is controlled by an analog-electro-mechanical controller. Likewise, the ignitor is turned on by the computer but it is turned off after 30 sec by a timer actuated electromechanical switch. With further effort the system could be converted to total computer control. This may result in a cost saving and surely easier programming.

SOFTWARE

Software was developed so that the computer could make observations and then adjustments in burning parameters and burner actions in conjunction with the existing system hardware. The program listing is presented in the appendix with the logic and sequencing reviewed schematically in figure 3.

The program performs three main tasks. The first is to startup the burner and then adjust the specimen temperature and burner pressure, within small ranges of their respective set points before transferring to the P-I-D fuel loop and proportional air control loop in the first cycle. The second task is the operation of the P-I-D and proportional air control loops. Task three consists of the scheme for cooling and reheating without temperature overshoot. Associated with these tasks is a certain amount of safety, record-keeping, measurement, display and calculation activity. A brief description of the operation of these main parts through the first complete cycle for a single rig (number 3) follows.

Task one is the startup and establishment of the temperature and burner pressure with subsequent transfer to the P-I-D temperature control loop. Figure 3(a) presents the steps involved. First the desired rig is selected by keyboard selection through a special function key. Screen prompts then ask for operator keyboard inputs of cycle data as number of cycles desired, number of previous cycles completed, and specimen identification. No further operator attention is needed. The combustion air valve is opened as the computer outputs a preset digital valve to the digital to analog board where it is converted to an electrical signal that actuates the air valve and the combustion air heater is turned on. Program execution then returns to the rig selection segment thus completing the first loop. On subsequent program executions through this loop a branching flag directs the execution to the next segment where the temperature of the combustion air is checked and if it has not reached 440 °F execution returns to the rig selection segment. By use of branching flags each loop is executed in succession throughout the program. Once the air temperature reaches the 440 °F set point, the fuel is turned on and ignited. Next the fuel pressure is set to 91 to 92 psig after which the cooling timer is started. During the initial cooling period of three minutes the fuel to air ratio is set to 0.025 to 0.026. From prior experience this value was known to produce a flame temperature which would not heat the specimen beyond the desired test temperature. However, a fuel pressure lower limit of 86 psig was used to prevent flame out. After the initial cooling period the burner is pivoted so the flame strikes the specimen. The specimen now enters the heatup stage and if the specimen is new and without any previous test cycles it is held for 30 min in the flame before final adjustment to the set point temperature. This procedure was found necessary because machined specimens had a highly reflective or polished surface. These surfaces produced high valued two color pyrometer readings. It was found during this

initial 30 min heating period that the high apparent temperature decreases rapidly as the surface darkens and takes on a matte appearance due to oxidation and corrosion. If the test specimen was previously exposed to the flame, as in previous test cycles, no initial heating period is used and the program immediately proceeds to adjust the fuel and air flows in the proper direction so that the temperature and burner pressure closely approach their respective set points. This is achieved by stepwise incrementing or decrementing the fuel flow and proportional control of the air flow. Once the temperature is within the arbitrarily chosen range of 1648 to 1654 °F control is transferred to the P-I-D loop. If this temperature range cannot be achieved within 10 min or the fuel pressure exceeds 155 psig then the burner is shutoff. Transfer to the P-I-D loop is accomplished by setting the branching flag, control 3, to a value of 2. This causes the program to always branch to "running" at point "A" in figure 3(b). At point "A" a check of the burner position signal is made, because the burner is now in the heating position and the heatup flag, Out 3, is >2, execution enters the P-I-D loop. The first cycle startup segment is not used again.

The steps of task two include the P-I-D loop and the cooling and heatup branching tests. A schematic of the logic steps are presented in figure 3(b). The major function of this loop is the calculation of the fuel and air control digits and adjustment of the fuel and air flows. However, several other functions appropriate to this program segment, as, screen display of data, safety checks, and other housekeeping tasks are also accomplished.

The P-I-D calculation of the fuel digit is:

$$\text{Outfuel3} = \text{Outfuel3s} - (\text{Errt} * \text{Gai3}) - (\text{Sumint3} * \text{Res3}) - (\text{Rate} * \text{Rcon3}) \quad (1)$$

where Errt is the error in temperature, that is (measured temperature - set point); Sumint is the integral of the temperature error curve versus time determined by a numerical approximation; and Rate is the temperature change per unit of time; Gai3, Res3 and Rcon3 are tuning constants. The tuning constants are used to tune the control loop to maximum control quality. Tuning constants can be determined by analytical procedures (ref. 5) or by trial. The latter method was employed here to determine the optimum constants. Outfuel3s is the bias term and takes on its value when the temperature is in a narrow range of the set point during initial setting of the temperature on heatup, and this value is retained for the cycle. The final digit is then the algebraic sum of the terms in equation (1). This digit is sent to the digital to analog hardware which converts the digit to an electrical control signal and via an electropneumatic transducer positions the fuel valve.

The proportional calculation of the air digit is:

$$\text{Air3} = \text{Air3} - (\text{Errp} * \text{Air3c}) \quad (2)$$

where Errp is the error in the burner pressure, that is (measured pressure - set point pressure) and Air3c is a tuning constant. No bias is used, that is, the final output digit is obtained by readjusting the presently stored digit. This scheme was found to give sufficiently good control of the burner pressure and hence flame velocity so no further terms were used. The tuning constant was determined by trial. The readjustment of the fuel and air occurred 10 times per minute for each burner. While this was sufficient, with

more efficient programming it is estimated that a rate of 15 to 20 times per minute may be possible.

Afterwards or concurrently with the fuel and air adjustment several other functions are performed in the P-I-D loop. For example display on the CRT screen of the burner pressure, the specimen temperature, and the fuel to air ratio as a function of time is performed. This is useful for on-line visual assessment of burner action.

Also the fuel flow digit is stored when the temperature is within a 2° band of the set point. This digit is adjusted by decreasing its value by a 1/2 percent and is used as the initial value in heatup in the next cycle. This 1/2 percent setback is actually calculated in the cooling and heatup loop to be described later. The maximum and minimum temperatures attained in each heating cycle are tracked and recorded within the P-I-D loop. A most useful bit of information is the temperature distribution in a heating cycle. This was calculated as the time spent in three temperature bands. The first is the percentage of the cycle heating time that the temperature is greater than the minimum but less than 1650 °F, the next is the percent of time the temperature is between 1650 and 1654 °F, this is ± 2 °F of the set point, and lastly the portion above 1654 °F but less than the maximum temperature. An examination of these values gives the operator a means of judging the control action. Very good control was considered to show >90 percent of the time in the center band. Less than 80 percent was not accepted and the test was stopped if this occurred. This latter action is taken in the cooling and heating loop to be described later. Also, if the time distribution in each band is symmetrical then the control action is generally considered to be desirable. If the distribution is skewed then this may indicate that the control action is undesirable and operator corrective action may be called for, such as, changing the tuning constants and/or hardware.

Distributed in the program are several software checks for "out of limit" operations. Operation beyond these limits results in shutdown of the burner to prevent possible extended testing under abnormal conditions. Due to the hybrid nature of this system most of these software checks are involved with protection of the specimen because the burner hardware has several analog safety overrides to shutoff the fuel flow if certain conditions hazardous to equipment and personnel develop. The software provides some redundancy which is not undesirable from a safety standpoint. If the temperature of the combustion chamber falls below 900 °F or the fuel pressure exceeds 155 psig the fuel flow is shutoff. Also, if the ac line power to the computer fails and the failure lasts more than 1 sec then the computer switches to battery operation. The 1 sec delay allows for short term power loss before going irreversibly to the battery mode. During the one minute of battery operation the fuel flow is shutoff and the test is terminated. If the line power to the data acquisition units fails then the burner is automatically shutoff with no assist from the computer.

At the end of the present heating time a separate electromechanical timer actuates a solenoid valve which actuates an air driven piston that causes the burner to rotate so that the flame misses the specimen and the cooling cycle starts. When the burner position signal is checked by the computer it will indicate that the burner is in the cooling position. This causes the program to branch to the cooling segment which starts at point "B" in figure 3(b).

The software for task three is involved with the cooling and heatup of the specimen. A schematic of the major logical steps is presented in figure 3(c). The first step is to determine whether this is the first pass through the cooling cycle loop. When the branching flag "N" is equal to 1, the program proceeds to execute the statements of the first pass segment. These include printing a hard copy of the heating parameters and calculating the initial fuel digit for the next heating cycle. This is performed on the fuel digit stored during the heating cycle when the temperature was within ± 2 °F of the set point. This latter digit is decreased by 1/2 percent (set-back). The resulting digit is output to the fuel valve so that the flame temperature is lowered to a point where it will not heat the specimen up to the set point in the next heating cycle. This allows a slow and controlled approach to the set point in the next cycle heatup and prevents temperature overshoot. Next comes incrementing the software cycle counter, setting the integral term in the P-I-D loop to zero, checking the residence time in the middle temperature band and shutting off the burner if it is less than 80 percent. Also, the initial values of T_{max} and T_{min} are reset to 1652 °F for the next cycle and two branching flags (N and Out3) are reset. A software cooling timer is also started. The second and all subsequent passes through the cooling loop until the 3 min of cooling cycle time has elapsed then go to the path where $N = 2$. Here several checks are made. If the cycles desired equals the cycles completed then the main power to the burner is shutoff and execution of the program is stopped. If more cycles have to be run, a check of the elapsed software cooling time is made and if more than 10 min or the fuel pressure is more than 155 psig then the burner is shutoff because of some malfunction in the analog system.

Upon the completion of the cooling cycle the burner is rotated by the electromechanical timer and pneumatic actuator to the heating position and the electromechanical heating timer is started. The burner position signal test at point "A" will now direct execution to heating and test of the heatup branching flag, Out3, will be found to be two so branching to point "C" in figure 3(c) will occur. In this loop the fuel flow is incremented in small steps until the temperature set point is nearly reached. When this is achieved the heatup flag, Out3, is set to three and further passes through the heatup branching test point will send the execution to the P-I-D control loop in figure 3(b). This completes the first heating and cooling cycle.

The program also incorporates several other functions. A special purpose key can be pressed at any time that a comparison of the transducer determined values of fuel and air flow and those read by the operator from calibrated analog rotometers is desired. The operator readings of fuel and air flow are input at the keyboard in response to a screen prompt and the fuel and air flows and the fuel to air ratio for each set of values are printed on the hard copy printer.

If an execution time error occurs, an error interrupt message sends the program execution to an error handling subroutine where the fuel flow and burner ac power are shutoff and the execution error number is hard copy printed to aid the operator in determination of the software cause of the error and its correction. At initial startup a test of the burner pivot cylinder air supply is made via the position signal to warn the operator if it is off and stop execution until this condition is operator corrected. A test is also made to determine if the peripherals (printer and data acquisition unit)

attached to the IEEE-488 Bus are energized and if not to stop program execution and warn the operator. There is a special purpose key for operator use to shutoff a burner at any time.

A critical parameter in hot corrosion testing is the salt solution flow to the injector which aspirates the solution into the combustor. If this flow stops or deviates too far from an acceptable range the testing must be discontinued or erroneous results will be obtained. In our system the rate is manually hardware set by the operator and no further control is provided. Flow is monitored by continuously measuring the weight of the salt solution container supported by a load cell. If the flow, as reflected by weight change, is within preset limits, testing is allowed to continue, if not the test is stopped. This aspect of operation has been hardware implemented but the software has not as yet been developed. During actual use of the control program described here the salt solution flow monitoring is provided by another computer based monitoring system developed previously. The function of this latter system will be briefly described later.

RESULTS

Typical burner rig flame hot corrosion test parameters taken at 15 min intervals over a 14 hr period are presented in figure 4. The burner rig was operated under digital control. Examination of this data indicates that good results of the digitally maintained specimen temperature and burner pressure and thusly Mach number were obtained. The "see-saw" nature of the calculated sodium content of the flame is due to the low sensitivity of the strain gauge load cell used to weigh the salt solution container and not actual flow variations.

The data points reported in figure 4 were gathered by a separate computer based monitoring system. The data are recorded on a floppy disc for off-line printing or plotting. This system was previously developed to track certain burner parameters and shutoff the burner if any of the parameters exceeded preset limits for three consecutive measurements. The monitor system uses a separate microcomputer, program and data acquisition unit. Both the control and monitor systems derive their input signals from the same burner rig transducers for pressure and etc. The monitor system functions equally well with analog or digital burner control.

From analysis of screen plotted data during each cycle (fig. 5) it is concluded that the digital control system can maintain an absolute temperature control of ± 3 °F with greater than 90 percent of the time the temperature is within ± 2 °F of the set point. Also, temperature overshoot of no more than 3 °F was achieved. The burner pressure can concurrently be maintained at 1.0 ± 0.02 psig which produces a Mach number of 0.3 ± 0.02 .

CONCLUSIONS

The digital control mode of operation of burner rigs is a viable, highly flexible, and accurate means of long time, unattended materials durability hot corrosion testing. Limits of acceptable testing can be set and easily changed. Also, test modes can be easily changed, such as ramp or other heating and cooling patterns can be programmed. Data can be collected on disk or tape and

used to make calculations and correlations off-line. Also, on line hard copy and screen plotting of information is readily implemented for real time assessment of burner operation. Furthermore, the computer starts and operates the burner in a more reproducible and predictable manner than a human operator. This greatly minimizes carbon buildup and frequency of cleaning of the burner. The computer based control system starts, runs the tests and turns off the burner when finished or when the test conditions are out of preset limits. This latter mode of operation protects the test specimen from abnormal testing.

APPENDIX

A listing of the entire digital control program is presented in the following pages. This program is written in a commercial basic language. The variables and function of the various program sections are defined in REM statements. It must be emphasized that this set of instructions (program) is not a general control program for all burner rigs, rather it was written to do a specific job and experience has demonstrated that it does that job very well.

APPENDIX

```

1          !*****
3          ! DIGITAL CONTROL PROGRAM
4          !*****
5
11 CLEAR 709
12 ON INTR 5 GOTO Pfail INITIALIZE POWER FAIL INTERUPT
13 ENABLE INTR 5;1
14 CONTROL 5,5;50,4000,400
16 ON ERROR GOTO Error
17 PRINTER IS 701
20 ON TIMEOUT 7,5 GOTO 7104
21 PRINT "PRINTER ON"
23 PRINTER IS 1
24 ! *****
26 ! CHECKING AIR SUPPLY TO BURNER RIG PIVOT CYLINDER
27 ! *****
29 OUTPUT 709;"VC3"
30     OUTPUT 709;"AI31"
31     ENTER 709;Pos13
32     OUTPUT 709;"AI32"
33     ENTER 709;Pos14
34     IF Pos13>2. OR Pos14>2. THEN GOTO Abort
35 !~~~~~
37 REAL Const(15),Qtot(50)
38 Spt=1652! TEMP SETPOINT BOTH RIGS 3&4 (DEGREES F)
39 Bpspt=1.0! BURNER PRESS. SET POINT BOTH RIGS 3&4 (psig)
40 Start3=0
41 Start4=0
42 Samp3=0
43 Samp4=0
44 Ctt=0
45 Ctt44=0
46 Control3=0
47 Control4=0
48 Tmax4=1652
49 Tmin4=1652
50 Tmax3=1652
51 Tmin3=1652
52 Mmm=0
53 Tup3=0
54 Tdn3=0
55 Tup4=0
56 Tdn4=0
57 ! *****
58 ! INITIAL PID LOOP CONSTANTS
59 ! *****
60 ! FUEL FLOW LOOP
61 ! ~~~~~
62 !
63 Ga13=8 ! PROP. GAIN BURNER RIG 3 INIT. VALUES
64 Res3=3! RESET BURNER RIG 3
65 Rcon3=10! RATE CONSTANT BURNER RIG 3
66 Ga14=15! PROP. GAIN BURNER RIG 4
67 Res4=3! RESET BURNER RIG 4
68 Rcon4=20! RATE BURNER RIG 4
69 !
70 ! ~~~~~
71 ! AIR FLOW LOOP
72 ! ~~~~~
73 !
74 Air3c=200! AIR FLOW PROP. GAIN RIG 3
75 Air4c=200! AIR FLOW PROP. GAIN RIG 4
76 !*****
77 IMAGE AAAAAA,2X,DD,2X,DD,2X,DDD,2X,DDDD,2X,DD.D,2X,DD.D,2X,DD.D,2X,DDDD,2X,
DDDD,2X,D.DDD,2X,DDD
78 ALLOCATE Outfue13s(10)

```

```

79 ALLOCATE Outfuel4s(10)
80 REAL To(10,10)
90 REAL Timer(10,10)
91 REAL Tot(50),E1(50),Rater(50),Errrt(50)
92 REAL T1(50),Bprrr(50),Errrp(50)
100 First3=1
110 First4=1
130 Outc3=0
140 Outc4=0
150 Sumint3=0
160 Sumint4=0
170 Sumerrt3=0
180 Sumerrt4=0
190 Ht3=0
200 Ht4=0
210 Ct1me3=0
220 Ct1me4=0
250 Ct3=0
260 Ct4=0
270 ALLOCATE Rn(25)
280 N=0
290 L=0
291 Nn=0
292 Nx=0
293 Cycl3=1
294 Cycl4=1
300 Cycles3=1
310 Cycles4=1
311 Cyflag3=0
312 Cyflag4=0
320 GOSUB Clearscreen
321 Dumm=1
330 OFF KEY
331 | *****
333 | SCREEN DISPLAY OF SPECIAL FUNCTION KEYS
334 | *****
340 ON KEY 9 LABEL "STOP" GOTO Stop
341 ON KEY 4 LABEL "SENSOR CK" GOSUB Check
350 ON KEY 0 LABEL "STR3" GOTO Str3
360 ON KEY 1 LABEL "STR4" GOTO Str4
370 ON KEY 5 LABEL "P.GAIN" GOSUB Gain
380 ON KEY 6 LABEL "RESET" GOSUB Reset
390 ON KEY 7 LABEL "RATE" GOSUB Rates
400 ON KEY 3 LABEL "AIR3C" GOSUB Airrate
401 ON KEY 8 LABEL "AIR4C" GOSUB Airrate4
410 Spin: DISP X
420 GOTO Spin
430 |
440 OUTPUT 2 USING "#,B";255,75
441 | ~~~~~
442 | BRANCHING AND TIME DISPLAY
443 | ~~~~~
450 GOSUB Control
460 OUTPUT 709;"TD"
470 ENTER 709;Time$
480 DISP Time$[7,14]
490 GOTO 450
500 | =====
510 | CLEAR SCREEN
511 | =====
530 Clearscreen: |
540 OUTPUT 2 USING "#,B";255,75
550 RETURN
560 | =====
561 | START BURNER RIG 3

```

```

562 |      =====
564 Str3:|
565 PRINT TABXY(1,10);"TURN ON PRINTER"
566   Wa13=5
567 INPUT "TOTAL NO. OF HEATING CYCLES",Nocy3
568 INPUT "NO. OF PREVIOUS CYCLES",Prevcy3
569 INPUT "BAR NO.",Barno3$
570 Totcy3=Prevcy3+1
571 GOSUB Clearscreen
572 OUTPUT 709;"D02,6"|      TURN ON SYST. PWR.
573   Control3=1
574   Air3=5500
575   OUTPUT 709;"A03,0,"&VAL$(Air3)|      OPEN AIR VALVE
576   WAIT 1
577   OUTPUT 709;"DC2,2"|AIR HTR 3|      START AIR PREHEATER
578   Start3=1
579   GOTO 450
580 Airtem:|
581 GOSUB Tep|      MEASURE COMBUSTION AIR AND COMB. CHAMB.TEMP
582 IF Cat3<440 THEN RETURN
583 Start3=2
584 Outfue13=3000      | FUEL NOZ.=1.00
585 OUTPUT 709;"A03,1,"&VAL$(Outfue13)|      OPEN FUEL VALVE
586 WAIT 1
587 OUTPUT 709;"DC2,0"|TURN ON IGNITOR
588 RETURN
589 Chamt:|
590 GOSUB Tep
591 IF Chamb3<800 THEN RETURN
592 |#####
593 GOSUB 1760
594 |#####
595 |      SET FUEL PRESSURE TO 90-92 psig
596 |#####
598 PRINT TABXY(1,1);"FU NOZ. PR.=";Fupress
599 IF Fupress>92 THEN |      FUEL NOZ.=1.00
600   Outfue13=Outfue13-50
601   OUTPUT 709;"A03,1,"&VAL$(Outfue13)
602   END IF
603 IF Fupress<90 THEN
604   Outfue13=Outfue13+25
605   OUTPUT 709;"A03,1,"&VAL$(Outfue13)
606   END IF
607 IF Fupress>92 OR Fupress<90 THEN RETURN
608 |#####
609 Start3=3
610 OUTPUT 709;"DC2,1"| START CYCLE TIMER
611 RETURN
612 |      =====
613 |      START BURNER RIG 4
614 |      =====
615 Str4:|
616 PRINT TABXY(27,10);"TURN ON PRINTER"
617 PRINT TABXY(27,11);"TURN ON POWER RIG 3- "
618 PRINT TABXY(27,12);"TURNS ON 2-COLOR PWR."
619 Wa14=5
620 INPUT " NO. OF HEATING CYCLES",Nocy4
621 INPUT "NO. OF PREVIOUS CYCLES",Prevcy4
622 INPUT "BAR NO",Barno4$
623 Totcy4=Prevcy4+1
624 GOSUB Clearscreen
625 OUTPUT 709;"D02,7"|TURN ON SYST. PWR.
626   Control4=1
627   Air4=4750
628   OUTPUT 709;"A04,0,"&VAL$(Air4)
629   WAIT 1

```

```

630     OUTPUT 709;"DC2,5"! AIR HTR 4
631     Start4=1
632     GOTO 450
633 Airtem4: !
634     GOSUB Tep
635     IF Cat4<440 THEN RETURN
636     Start4=2
637     Outfuel4=4400
638     OUTPUT 709;"A04,1,"&VAL$(Outfuel4)
639     WAIT 3
640     OUTPUT 709;"DC2,3"! IGN 4
641     RETURN
642 Cham4: !
643     GOSUB Tep
644     IF Chamb4<650 THEN RETURN
645     OUTPUT 709;"A04,0,4650"!AIR
646     !#####
647     GOSUB 1760
648     PRINT TABXY(27,1);"FU.NOZ.PRES.=";Fupress
649     IF Fupress>92 THEN
650         Outfuel4=Outfuel4-50
651         OUTPUT 709;"A04,1,"&VAL$(Outfuel4)
652         PRINT TABXY(27,2);"FUEL DIG";Outfuel4
653         END IF
654     IF Fupress<90 THEN
655         Outfuel4=Outfuel4+15
656         OUTPUT 709;"A04,1,"&VAL$(Outfuel4)
657         PRINT TABXY(27,2);"FUEL DIG";Outfuel4
658         END IF
659     IF Fupress>92 OR Fupress<90 THEN RETURN
660     !#####
661     Air4=4650
662     Start4=3
663     OUTPUT 709;"DC2,4"!TIMER 4
664     RETURN
665     !#####
666     !          MANUAL STOP OF RIGS
667     !#####
669 Stop: !
670     INPUT "WHICH RIG",Rig
671     IF Rig=4 THEN GOTO 682
672     OUTPUT 709;"A03,1,10"
673     Control3=0
674     OUTPUT 709;"DC2,6"
675     GOSUB Clearscreen
676     PRINTER IS 701
677     PRINT "RIG 3 STOPPED";" "; "TOTAL CYCLES=";Totcy3
678     PRINTER IS 1
679     First3=1
680     IF Control4=0 THEN GOTO 731
681     GOTO 450
682     OUTPUT 709;"A04,1,10"
683     OUTPUT 709;"DC2,7"
684     Control4=0
685     GOSUB Clearscreen
686     PRINTER IS 701
687     PRINT "RIG 4 STOPPED";" "; "TOTAL CYCLES=";Totcy4
688     PRINTER IS 1
689     First4=1
690     IF Control3=0 THEN GOTO 731
691     GOTO 450
692     CLEAR 709
693     STOP
740     !=====
750 Rates: !
751     INPUT "RIG NO.",Rigcon

```



```

1608     IF Cat4>575 THEN GOTO Shutoff4
1610     GOSUB Heatup4
1611     GOTO 1730
1612     END IF
1613 |-----|
1617     GOSUB Meas1      MEASUREMENT OF RIG PARAMETERS
1647 |-----|
1720     GOSUB 1760
1730     NEXT Rignum
1740     RETURN
1750 |*****|
1760     IF Rignum=3 THEN Fupre=24
1770     IF Rignum=4 THEN Fupre=29
1780     OUTPUT 709;"AI"&VAL$(Fupre)
1790     ENTER 709;Fvolt
1800     Fupress=Fvolt*10000
1801     IF Rignum=3 AND Start3=2 THEN RETURN
1802     IF Rignum=4 AND Start4=2 THEN RETURN
1810     IF Rignum=3 AND Control3=1 THEN GOTO 6957
1820     IF Rignum=4 AND Control4=1 THEN GOTO 6957
2030 |-----|
2040     IF Rignum=3 THEN Xp=1
2050     IF Rignum=4 THEN Xp=27
2051     IF Rignum=3 THEN Cyo=Cycles3
2052     IF Rignum=4 THEN Cyo=Cycles4
2060     PRINT TABXY(Xp,1);"BP";DROUND(Bp2,3);"FP";DROUND(Fupress,3);"CY";
Cyo
2120     IF Rignum=3 THEN PRINT TABXY(Xp,3);"PG";Ga13;"RS";Res3;"RA";Rcon3;"AC";A1r
3c
2121     IF Rignum=4 THEN PRINT TABXY(Xp,3);"P.G";Ga14;"RES";Res4;"RA";Rcon4;"AC";A
1r4c
2130     IF Rignum=3 THEN A1rp=A1r3
2140     IF Rignum=4 THEN A1rp=A1r4
2150     IF Rignum=3 THEN Fuelp=Outfuel3
2160     IF Rignum=4 THEN Fuelp=Outfuel4
2170     PRINT TABXY(Xp,4);"F DIG";Fuelp;"A DIG";A1rp
2180 |-----|
2210     IF Rignum=3 THEN GOTO 2510
2220     IF Rignum=4 THEN GOTO 2940
2230     IF Rignum=3 THEN GOSUB 2280
2240     IF Rignum=4 THEN GOSUB 2390
2250     Cxxxx=0
2260     RETURN
2261 |-----|
2272 |-----|
2273 |-----|
2280     Outc3=Outc3+1
2295     IF Outc3>1 THEN GOTO 2310
2300     Outfuel3s(1)=Outfuel3
2310     Outfuel3=Outfuel3s(1)-INT(Errt*Ga13)-INT(Res3*Sumint3)-INT(Rate*Rcon3)
2330     OUTPUT 709;"A03,1,"&VAL$(Outfuel3)
2340     A1r3=A1r3-INT(Errp*A1r3c)
2350     OUTPUT 709;"A03,0,"&VAL$(A1r3)
2351     GOSUB Tep
2352     IF Cat3>575 THEN GOTO Shutoff3
2360     PRINT TABXY(Xp,5);"S";INT(Sumint3);"FF1";DROUND(Fuelflow,2);"F/A";DROU
ND(F3,3)
2362     PRINT TABXY(Xp,6);">54";INT(Pctup3);"5054";INT(Pctmid3);"<50";INT(Pctdn3)
2363     PRINT TABXY(Xp,2);"CA";DROUND(Cat3,3);"CH";DROUND(Chamb3,4);"AF1";DROU
ND(A1rflow,3)
2370     RETURN
2380 |-----|
2390     Outc4=Outc4+1
2404     IF Outc4>1 THEN GOTO 2420
2410     Outfuel4s(1)=Outfuel4
2420     Outfuel4=Outfuel4s(1)-INT(Errt*Ga14)-INT(Res4*Sumint4)-INT(Rcon4*Rate)

```



```

2748         END IF
2749         !+++++
2750         GOTO 2230
2751         !-----
2752         !           COOLING
2753         !^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^
2760         N=N+1
2770         IF N>=2 THEN GOTO 2880
2771         Ht3=0
2772         Samp3=0
2774         Sumint3=0
2775         Outc3=0
2776         Tup3=0
2777         Tdn3=0
2779         Outfuel3=INT(Outf3-(Outf3*.005))
2780         OUTPUT 709;"A03,1,"&VAL$(Outfuel3)
2781         PRINTER IS 701
2782         PRINT USING 77;Barno3$,Rignum,Cycles3,Totcy3,Tmax3,Pctup3,Pctmid3,Pctdn3,T
min3,F3,Bp2,Fupress
2783         IF Pctmid3<80 AND Cycles3>1 THEN GOTO Shut3
2785         PRINTER IS 1
2786         Tmax3=1652
2787         Tmin3=1652
2788         Ct3=0
2840         Sumerrt3=0
2850         Time13=TIMEDATE
2870         GOSUB Display1
2880         Time3=TIMEDATE
2890         Ctime3=(Time3-Time13)/60
2893         IF Ctime3>=2.0 THEN GOSUB Cyclrt3
2900         PRINT TABXY(Xp,7);"CLTIM";DROUND(Ctime3,3);"TEM";DROUND(Tempt,4)
2901         !^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^
2902         IF Ctime3>10 OR Fupress>165 THEN GOTO Shutoff3'IF BURNER STICKS IN COOLIN
G POSITION
2908         !-----
2910         GOTO 2250
2920         !-----
2921         !           RIG 4 PID LOOP BRANCHING CONTROL
2930         !-----
2940         OUTPUT 709;"A132"
2941         ENTER 709;Pos4
2942         IF Pos4<=2. THEN GOTO 3170
2950         !-----
2951         !           HEATING
2952         !^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^^
2960         IF First4=1 THEN Time4=TIMEDATE
2970         First4=5
2980         L=0
2990         Timeht=TIMEDATE
3000         Ht4=(Timeht-Time4)/60
3001         IF Ht4>4 THEN Cyflag4=0
3010         PRINT TABXY(Xp,7);"HT";DROUND(Ht4,3);"TEM";DROUND(Tempt,4)
3011         IF Tempt>Tmax4 AND Ht4>.2 THEN Tmax4=Tempt
3013         IF Tempt<Tmin4 AND Ht4>2 THEN Tmin4=Tempt
3014         IF Tempt>1654 AND Tempt<=Tmax4 AND Ht4>.2 THEN Tup4=Tup4+(E1(Wa1)/60)
3015         IF Tempt<1650 AND Tempt>=Tmin4 AND Ht4>2 THEN Tdn4=Tdn4+(E1(Wa1)/60)
3016         IF Samp4=0 THEN GOTO 3022
3018         Pctup4=(Tup4/Samp4)*100
3019         Pctdn4=(Tdn4/Samp4)*100
3020         Pctmid4=100-(Pctup4+Pctdn4)
3021         PRINT TABXY(Xp,8);"TMAX";DROUND(Tmax4,4);"TMIN";DROUND(Tmin4,4)
3022         !-----
3023         Temptc=INT((Tempt-32)*5/9)
3024         IF Temptc<=860 THEN GOTO 3145
3030         IF Temptc>=940 THEN GOTO 3145
3031         !*****

```

```

3040     Txx=(Temp1c-860)/(80/60)
3050     GOSUB 6800
3090 MOVE Ht4,Txx
3100 DRAW Ht4,Txx
3120 Bpp=45+((Bp2-.95)*150)
3130 MOVE Ht4,Bpp
3140 DRAW Ht4,Bpp
3141 Ftox=(F4-.025)*1500
3142 MOVE Ht4,Ftox
3143 DRAW Ht4,Ftox
3145 IF Fupress>155 THEN GOTO Shutoff4
3146 !~~~~~
3147 IF Outc4>=1 THEN GOTO 3165
3148 !*****
3149 IF Temp1<1636 AND Ht4<1 THEN GOTO 2250
3150 IF Temp1>1660 AND Temp1<1680 THEN
3151     Outfuel4=Outfuel4-8
3152     GOTO 2440
3153     END IF
3155 IF Temp1<1620 THEN
3156     Outfuel4=Outfuel4+8
3157     GOTO 2440
3158     END IF
3159 IF Temp1>1620 AND Temp1<1650 THEN
3160     Outfuel4=Outfuel4+6
3161     Sumint4=0
3162     GOTO 2440
3163     END IF
3164 !*****
3165     GOTO 2230
3166 !-----
3167 !             COOLING
3168 !~~~~~
3170     L=L+1
3180     IF L>=2 THEN GOTO 3290
3181     Ht4=0
3182     Samp4=0
3184     Sumint4=0
3185     Outc4=0
3186     Tup4=0
3187     Tdn4=0
3189     Outfuel4=INT(Outf4-(Outf4*.005))
3191     OUTPUT 709;"A04,1,"&VAL$(Outf4)
3192     Ct4=0
3202     PRINTER IS 701
3212     PRINT USING 77;Barno4$,Rignum,Cycles4,Totcy4,Tmax4,Pctup4,Pctmid4,Pctdn4,
Tmin4,F4,Bp2,Fupress
3213     IF Pctmid4<80 AND Cycles4>1 THEN GOTO Shut4
3222     PRINTER IS 1
3232     Tmax4=1652
3242     Tmin4=1652
3250     Sumerrt4=0
3260     Time14=TIMEDATE
3280     GOSUB Display2
3290     Time4=TIMEDATE
3300     Ctime4=(Time4-Time14)/60
3303     IF Ctime4>=2.0 THEN GOSUB Cyclrt4
3310     PRINT TABXY(Xp,7);"CLTIM";DROUND(Ctime4,3);"TEM";DROUND(Temp1,4)
3311 !~~~~~
3313     IF Ctime4>10 OR Fupress>155 THEN GOTO Shutoff4
3318 !-----
3320     GOTO 2250
3321 !+++++
3322 !             CYCLE COUNTING RIG 3
3323 !~~~~~
3325 Cyclrt3: !

```

```

3326     IF Cyflag3>=1 THEN GOTO 3330
3327         Cycles3=Cycles3+1
3328         Totcy3=Prevcy3+Cycles3
3329     IF Cycles3=(Nocy3+1) THEN GOTO Shutoff3
3330         Cyflag3=Cyflag3+1
3331     RETURN
3332 |-----|
3333 |             CYCLE COUNTING RIG 4
3334 |-----|
3336 Cyclrt4:|
3337     IF Cyflag4>=1 THEN GOTO 3341
3338         Cycles4=Cycles4+1
3339         Totcy4=Prevcy4+Cycles4
3340     IF Cycles4=(Nocy4+1) THEN GOTO Shutoff4
3341         Cyflag4=Cyflag4+1
3342     RETURN
3343 |-----|
3344 |             SHUTOFF RIGS 3&4 IF TEMP. CONTROL DEGRADES
3345 |-----|
3347 Shut3:|
3348     PRINTER IS 701
3349     PRINT "RIG 3 BURNER OFF--LESS THAN 80 % IN BAND-CYCLES=";Totcy3
3350     PRINTER IS 1
3351     OUTPUT 709;"A03,1,0"|    FUEL VALVE  CLOSED
3352     WAIT 2
3353     OUTPUT 709;"DC2,6"|    POWER OFF
3354     GOTO 3387
3355 |*****|
3357 Shut4:|
3358     PRINTER IS 701
3359     PRINT "RIG 4 BURNER OFF---LESS THAN 80 % IN BAND-CYCLES=";Totcy4
3360     PRINTER IS 1
3361     OUTPUT 709;"A04,1,0"
3362     WAIT 2
3363     OUTPUT 709;"DC2,7"
3364     GOTO 3419
3365 |*****|
3366 |             SHUTOFF RIGS 3&4 IF CYCLES COMPLETED OR A MALFUNCTION
3367 |-----|
3369 Shutoff3:|
3370     OUTPUT 709;"A03,1,10"|FUEL OFF
3371     GOSUB Clearscreen
3372     IF Cycles3=Nocy3 THEN GOTO 3380
3373     IF Cycles3<>(Nocy3+1) THEN
3374     PRINTER IS 701
3375     PRINT "BURNER RIG 3-MALFUNCTION"
3376     PRINTER IS 1
3377     OUTPUT 709;"DC2,6"|SYST. PWR OFF
3378     GOTO 3387
3379     END IF
3380     PRINT TABXY<1,5>;"CYCLES COMPLETED"
3381     PRINTER IS 701
3382     PRINT "RIG 3-CYCLES COMPLETED"
3383     PRINTER IS 1
3384     OUTPUT 709;"DC2,6"
3385     Control3=0
3386     OUTPUT 709;"A03,0,10"|AIR OFF
3387     Control3=0
3388     IF Control4<>0 THEN GOTO 450
3389     CLEAR 709|OPENS ALL RELAYS
3390     GOSUB Clearscreen
3391     PRINT TABXY<3,8>;"DONE"
3392     GOTO 7123|END
3393 |*****|
3394 Shutoff4:|
3395     OUTPUT 709;"A04,1,10"

```

```

3396         GOSUB Clearscreen
3397         IF Cycles4=Nocy4 THEN GOTO 3405
3398         IF Cycles4<>(Nocy4+1) THEN
3399         PRINTER IS 701
3400             PRINT "BURNER RIG 4-MALFUNCTION"
3401         PRINTER IS 1
3402             OUTPUT 709;"DC2,7"
3403             GOTO 3419
3404         END IF
3405             PRINT TABXY(27,5);"CYCLES COMPLETED"
3406         PRINTER IS 701
3407         PRINT "RIG 4-CYCLES COMPLETED"
3408         PRINTER IS 1
3409             OUTPUT 709;"DC2,7"
3410             Control4=0
3411             OUTPUT 709;"A04,0,10"
3412             Control4=0
3413             IF Control3<>0 THEN GOTO 450
3414             CLEAR 709
3415             GOSUB Clearscreen
3416             PRINT TABXY(29,8);"DONE"
3417             GOTO 7123'END
3418 *****
3419 MEASURE COMBUSTION AIR AND COMBUSTION CHAMBER TEMP.
3420 *****
4360 Tep: !
4370             IF Rignum=3 THEN Cat=0
4380             IF Rignum=4 THEN Cat=2
4390             IF Rignum=3 THEN Cham=1
4400             IF Rignum=4 THEN Cham=4
4410             OUTPUT 709;"AI"&VAL$(Cat)
4420             ENTER 709;T
4430         GOSUB Tempcal
4440             OUTPUT 709;"AI"&VAL$(Cham)
4450             ENTER 709;T
4460         GOSUB Tempcal2
4470 IF Rignum=3 AND Control3=1 THEN PRINT TABXY(1,4);"CAT";DROUND(Cat3,4);"CHAM
";DROUND(Chamb3,4)
4471 IF Rignum=4 AND Control4=1 THEN PRINT TABXY(27,4);"CAT";DROUND(Cat4,4);"CHA
M";DROUND(Chamb4,4)
4480             RETURN
4490 Tempcal: !
4510             OUTPUT 709;"AI019"
4520             ENTER 709;R
4530             C=25+(R-2.5)/.1
4540             D=T+C*4.0E-5
4550             Tc=.2265+D*(24150+D*(67230+D*(2.21E+6+D*(-8.61E+8+D*4.835E+10))))
4560             Tf=Tc*1.8+32
4570             IF Rignum=3 THEN Cat3=Tf
4580             IF Rignum=4 THEN Cat4=Tf
4590             RETURN
4600 Tempcal2: !
4610             OUTPUT 709;"AI019"
4620             ENTER 709;R
4630             C=25+(R-2.5)/.1
4640             D=T+C*4.0E-5
4650             Tc=.2265+D*(24150+D*(67230+D*(2.21E+6+D*(-8.61E+8+D*4.835E+10))))
4660             Tf=Tc*1.8+32
4670             IF Rignum=3 THEN Chamb3=Tf
4680             IF Rignum=4 THEN Chamb4=Tf
4690             RETURN
4781 *****
4782 !             FIRST CYCLE HEATUP RIG 3
4783 *****
4790 Heatup3: !
4800             OUTPUT 709;"AI"&VAL$(20)

```



```

6830  LORG 2
6840  U=860
6850  FOR Inn=15 TO 45 STEP 15
6860  MOVE 0,Inn
6870  U=U+20
6880  LABEL U
6890  NEXT Inn
6900  LORG 7
6910  FOR Hz=15 TO 45 STEP 15
6920  MOVE Hz+5,0
6930  LABEL Hz
6940  NEXT Hz
6950  RETURN
6951  |*****
6952  |           RIG PARAMETER MEASUREMENTS AND CALCULATIONS
6953  |*****
6955  Meas: |
6957      Sumfuel=0
6958      Sumairfl=0
6959      Sumto=0
6960      Sumrater=0
6961      Sumbpr=0
6962      Sumerrt=0
6963      Sumerrp=0
6964      IF Rignum=3 THEN Af1=33
6965      IF Rignum=4 THEN Af1=27
6966      IF Rignum=3 THEN Ful=23
6967      IF Rignum=4 THEN Ful=28
6968      IF Rignum=3 THEN Chatemp=20
6969      IF Rignum=4 THEN Chatemp=25
6970      IF Rignum=3 THEN Chapress=21
6971      IF Rignum=4 THEN Chapress=30
6972      IF Rignum=3 THEN Wai=Wai3
6973      IF Rignum=4 THEN Wai=Wai4
6974  FOR Gz=1 TO 4
6975      OUTPUT 709;"AI"&VAL$(Ful)
6976      ENTER 709;Fle
6977      IF Rignum=3 THEN Fuel=1.83348+(.37836*1000*Fle)
6978      IF Rignum=4 THEN Fuel=1.7715+(.28282*1000*Fle)
6979      Sumfuel=Sumfuel+Fuel
6980      OUTPUT 709;"AI"&VAL$(Af1)
6981      ENTER 709;Af1e
6982      Zx1=Af1e*1000
6984      IF Rignum=3 THEN Airfl=113.91+(38.075*Zx1)
6985      IF Rignum=4 THEN Airfl=107.04+(33.366*Zx1)
6986      Sumairfl=Sumairfl+Airfl
6987  NEXT Gz
6988      Airflow=Sumairfl/4
6989      Fuelflow=Sumfuel/4
6990      Ftoair=Fuelflow/Airflow
6991  |-----
6992      IF Rignum=3 THEN F3=Ftoair
6993      IF Rignum=4 THEN F4=Ftoair
6994      |*****
6996      IF Rignum=3 AND Control3=1 THEN GOTO 4860
6997      IF Rignum=4 AND Control4=1 THEN GOTO 6070
6998      |*****
7002  FOR Nzz=1 TO Wai
7003      OUTPUT 709;"AI"&VAL$(Chatemp)
7004      ENTER 709;Rzz
7005      IF Rignum=3 THEN Tconst=4400
7006      IF Rignum=4 THEN Tconst=3800
7008      Tot(Nzz)=(800+(Rzz*Tconst))*1.8+32
7009      Errrt(Nzz)=Tot(Nzz)-Spt
7010      Sumerrt=Sumerrt+Errrt(Nzz)
7011      T1(Nzz)=TIMEDATE

```



```

7130     OUTPUT 709;"A03,1,10"
7131     OUTPUT 709;"A04,1,10"
7132     OUTPUT 709;"DC2,6"
7133     OUTPUT 709;"DC2,7"
7134     CLEAR 709
7135     OUTPUT 1;"AC POWER FAILED"
7136     WAIT 5
7137         PRINTER IS 701
7138         PRINT "AC POWER FAILED"
7139         PRINTER IS 1
7140     CONTROL 5;1
7141 STOP
7142 !*****
7143 !     CHECK FUEL AND AIR TRANSDUCERS
7144 !*****
7146 Check: !
7147 INPUT "RIG NO.=",Rignum
7148 IF Rignum=4 THEN F=28 !RIG 4 FUEL
7149 IF Rignum=3 THEN F=23 !RIG 3 FUEL
7150 IF Rignum=3 THEN A=33 !AIR RIG 3
7151 IF Rignum=4 THEN A=27 !AIR RIG 4
7152 Sumfu=0
7153 Suma1=0
7154 FOR Z=1 TO 10
7155 OUTPUT 709;"A1"&VAL$(F)
7159 ENTER 709;Fu
7169 Sumfu=Sumfu+(Fu*1000)
7179 OUTPUT 709;"A1"&VAL$(A)
7189 ENTER 709;A1
7199 Suma1=Suma1+(A1*1000)
7209 NEXT Z
7219 Fuel=Sumfu/10
7220 Airf=Suma1/10
7221 IF Rignum=3 THEN Fuels=1.83348+(.37836*Fuel)
7222 IF Rignum=4 THEN Fuels=1.7715+(.28282*Fuel)
7223 IF Rignum=3 THEN Airfs=113.91+(38.075*Airf)
7224 IF Rignum=4 THEN Airfs=107.04+(33.366*Airf)
7229 INPUT "FUEL ROT.<DECIMAL NO.>=",Frot
7230 Gph=-.573827+.672138*Frot-.124521*Frot^2+1.92399E-2*Frot^3
7231 Gph1=Gph-1.48557E-3*Frot^4+4.34668E-5*Frot^5
7233 Fpph=Gph1*6.78 !lbs/hr FUEL
7234 INPUT "AIR ROT.<INTEGER NO.>=",Arot
7235 IF Arot=0 AND Rignum=4 THEN GOTO 7234
7236 IF Rignum=4 THEN Apph=((Arot/100)*5.3*60) !lbs/hr FISCHER FLOW METER
7237 IF Rignum=3 THEN Apph=31.494394+2.73432459364*Arot !lbs/hr LITE BROOKS FLO
AT
7238 PRINTER IS 701
7239 PRINT TABXY(6,2),"RIG NO.=",Rignum
7249 PRINT "SENSOR FUEL FL.",DROUND(Fuels,5),"SENSOR AIR FL.",DROUND(Airfs,6)
7251 PRINT "ROT. FUEL FL.",DROUND(Fpph,5),"ROT. AIR FL.",DROUND(Apph,6)
7252 PRINT "ROT F/A",DROUND(Fpph/Apph,5),"SEN F/A",DROUND(Fuels/Airfs,5)
7254 PRINTER IS 1
7255 RETURN
8020 END

```

REFERENCES

1. Lowell, Carl E.; Sidik, Steven A.; and Deadmore, Daniel L.: High Temperature Alkali Corrosion in High Velocity Gases. NASA TM-82591, 1981.
2. Lowell, Carl E., et al.: The Effects of Trace Impurities in Coal-Derived Liquid Fuels on Deposition and Accelerated High Temperature Corrosion of Cast Superalloys. NASA TM-81678, 1981.
3. Barrett, Charles, A.; Johnston, James R.; and Sanders, William, A.: Static and Dynamic Cyclic Oxidation of 12 Nickel-, Cobalt- and Iron-Base High-Temperature Alloys. Oxid. Met., vol. 12, no. 4, Aug. 1978, pp. 343-377.
4. Weissberger, A.; and Bryant, W.R., eds.: Automatic Recording and Control; Computers in Chemical Research. Wiley-Interscience, 1971.
5. Herndon, William.: A User-Oriented Approach to The Application of PCs for PID Control. Computer Software for Industrial Control, E.J. Kompass and T.J. Williams, eds., Control Engineering, 1981, pp. 169-180.
6. Genet, Russell M.: Real Time Control With The TRS-80. Howard W. Sams and Co., Inc., 1982.
7. Schmitt, Neil M.; and Farwell, Robert F.: Understanding Electronic Control of Automation Systems. Texas Instruments, 1983.
8. Stire, Tom G.: Process Control Computer Systems. Ann Arbor Science, 1983.
9. Malmstadt, Howard V.; Encke, Christie G., and Crouch, Stanley R.: Electronics and Instrumentation for Scientists. The Benjamin/Cumming Publishing Co., 1981.
10. Deadmore, D.L.: Effects of Alloy Composition on Cyclic Flame Hot-Corrosion Attack of Cast Nickel-Base Superalloys at 900 °C. NASA TP-2338, 1984.

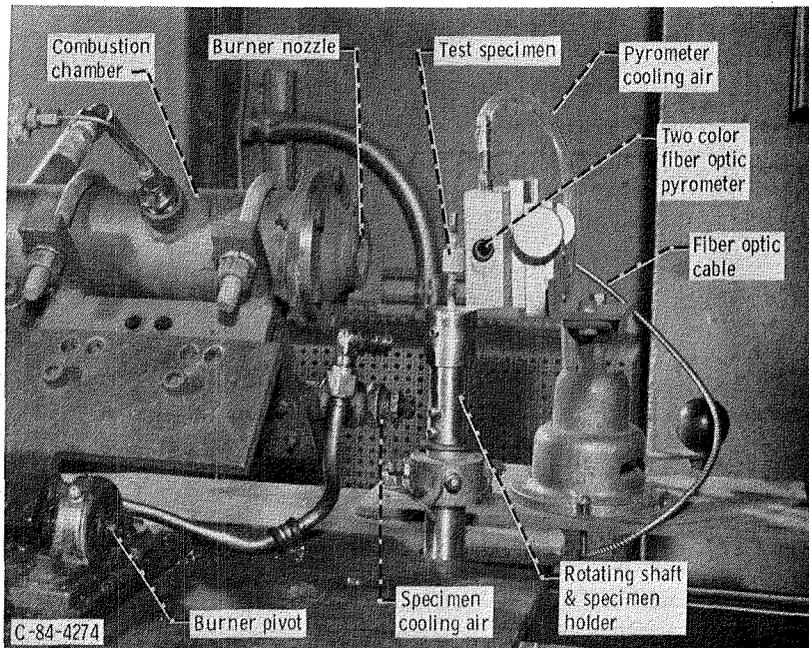


Figure 1. - Burner rig and specimen (heating position).

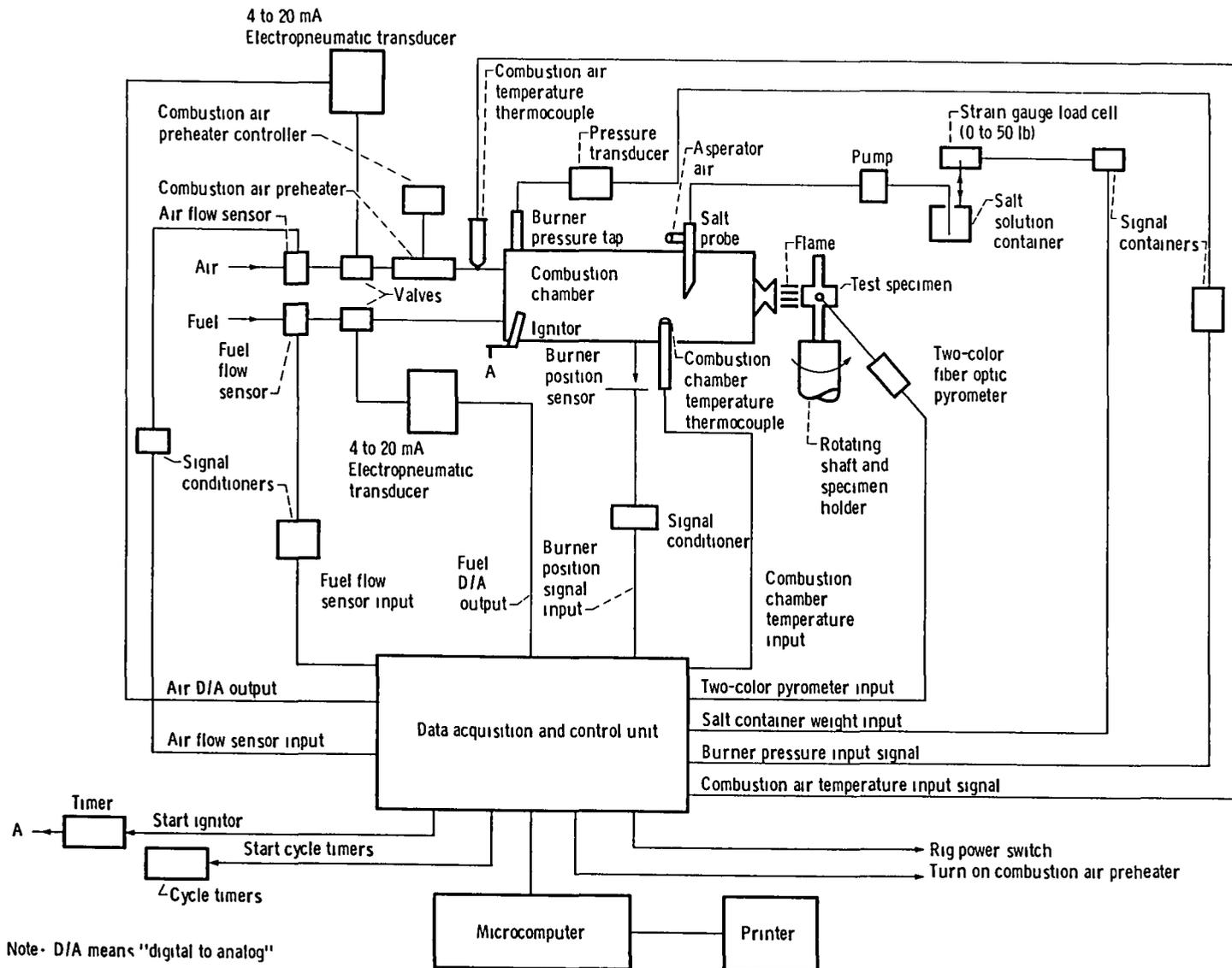
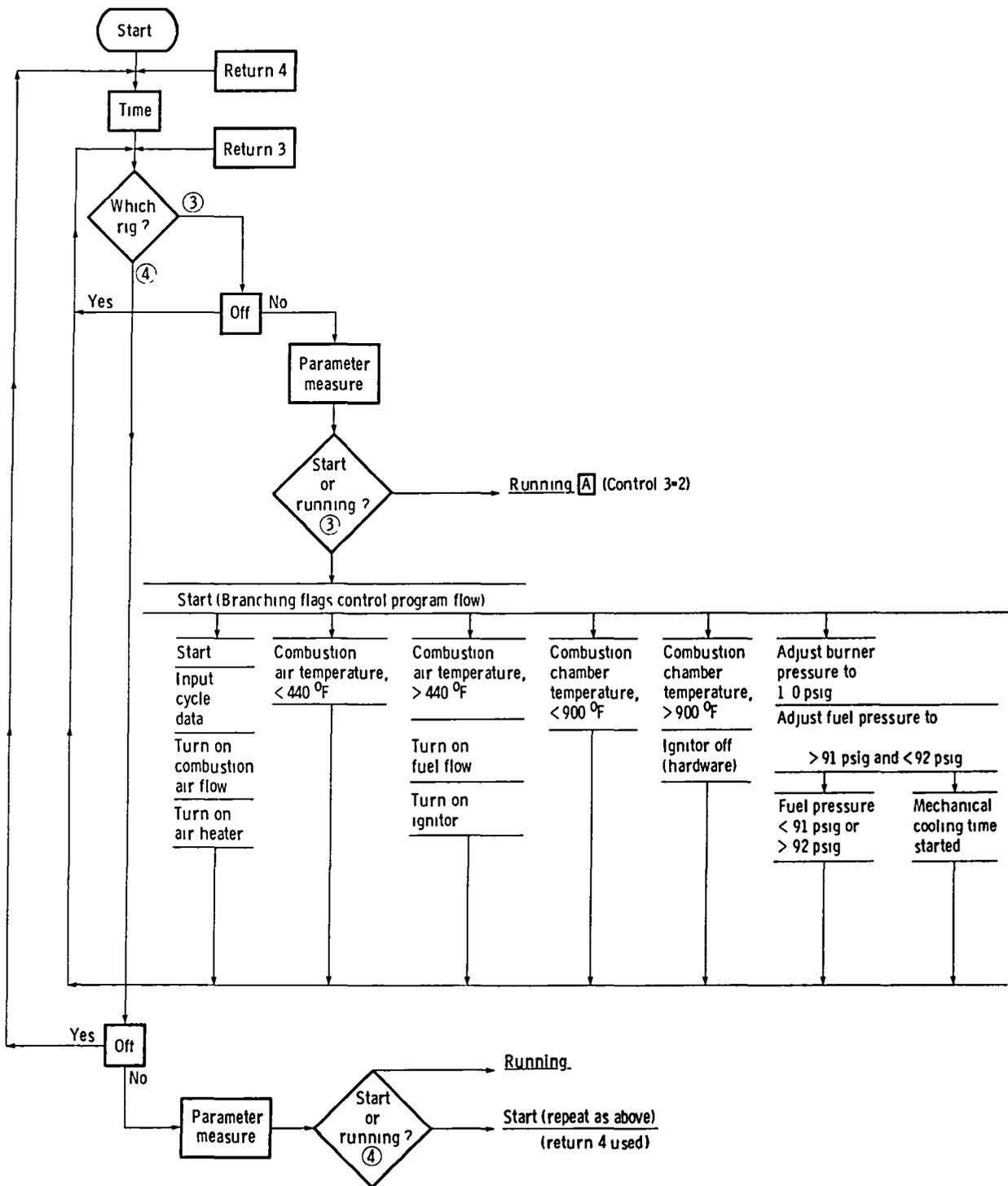
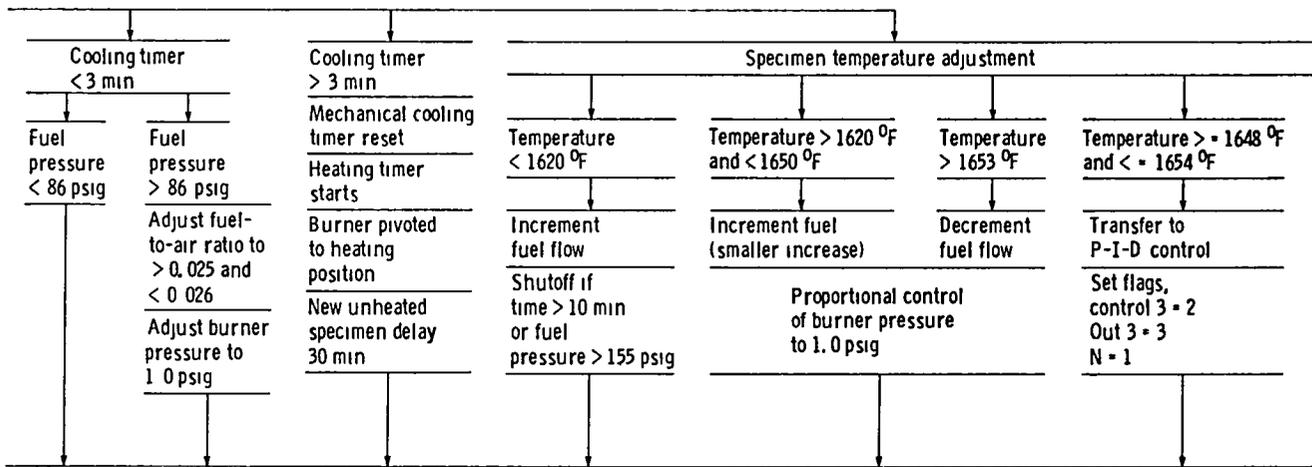


Figure 2 - Schematic diagram of the burner rig control system hardware. (All thermocouples are room temperature compensated via software.)

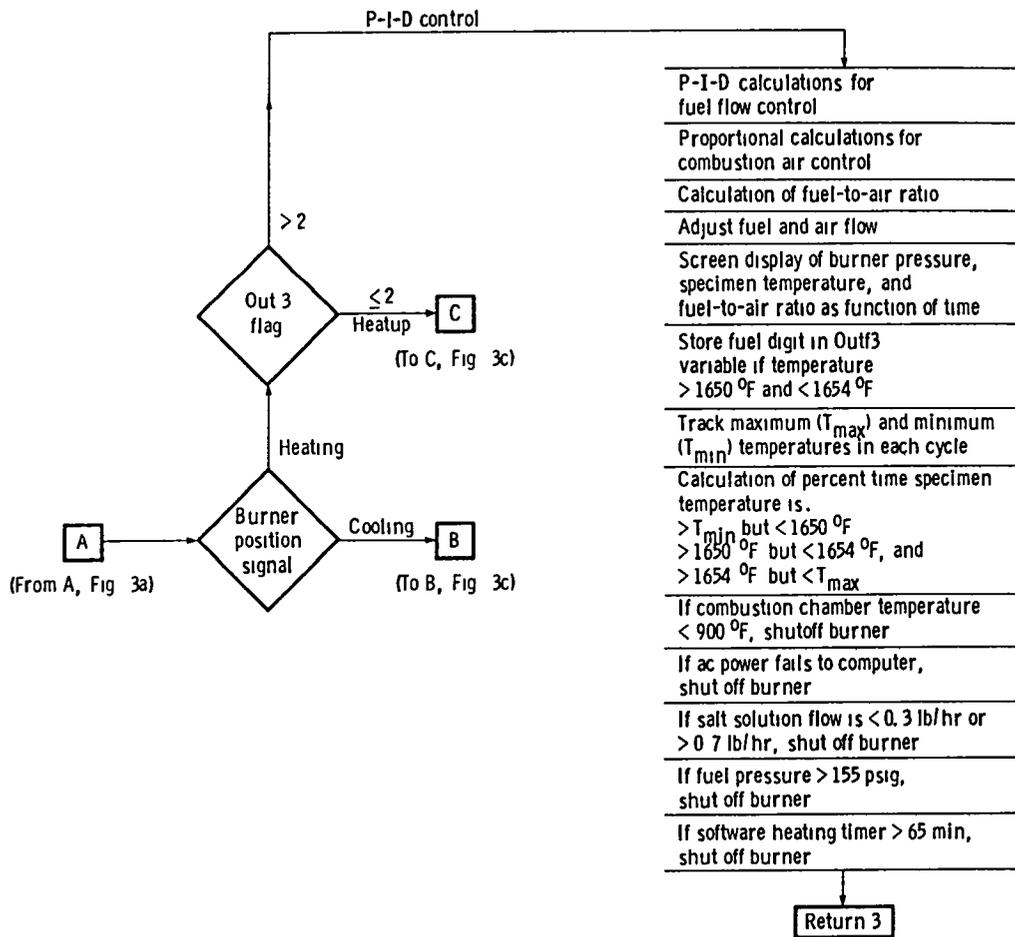


(a) First cycle startup loop.

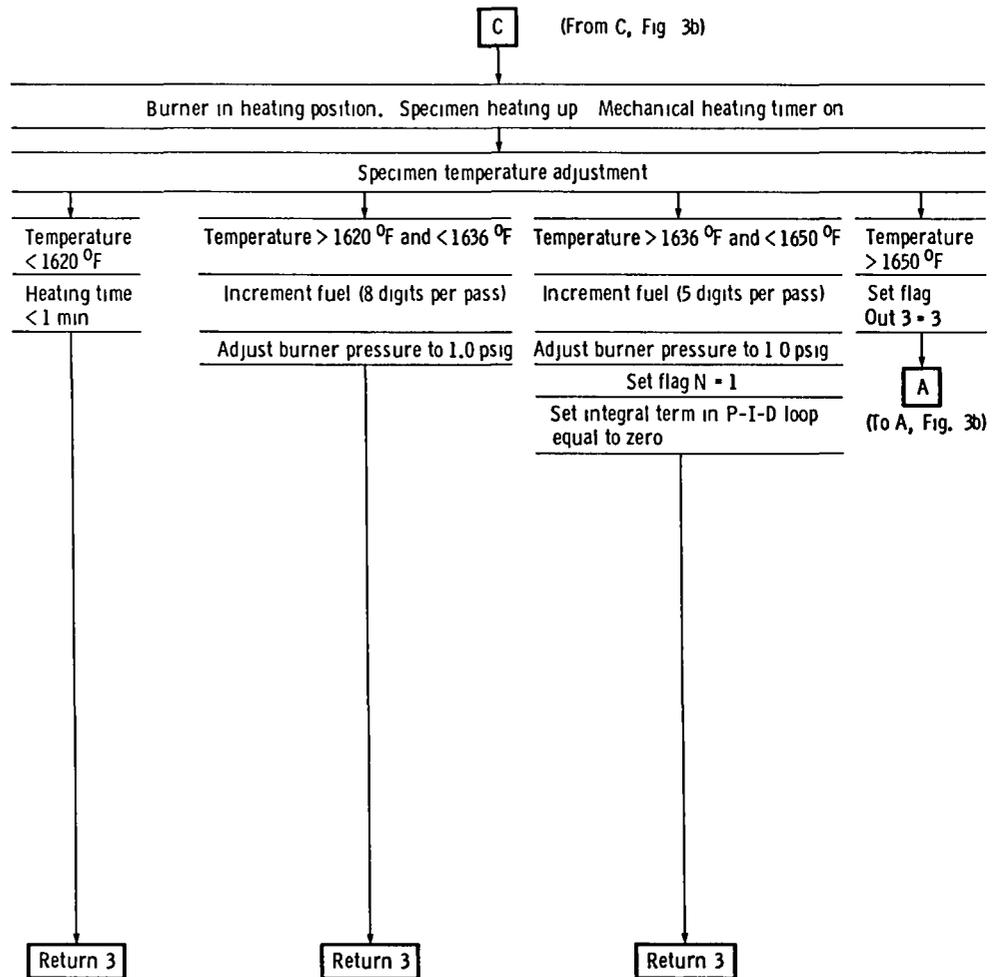
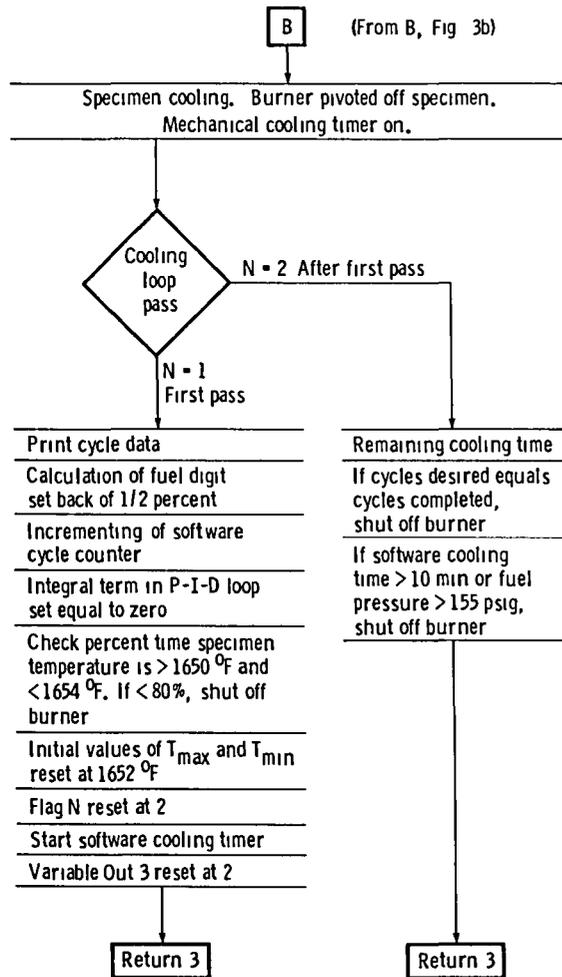
Figure 3 - Schematic of software logic steps for digital-hybrid control system.



(a) Concluded



(b) P-I-D and proportional control loop for Rig 3



(c) Cooling and heatup control for Rig 3.
Figure 3 - Concluded

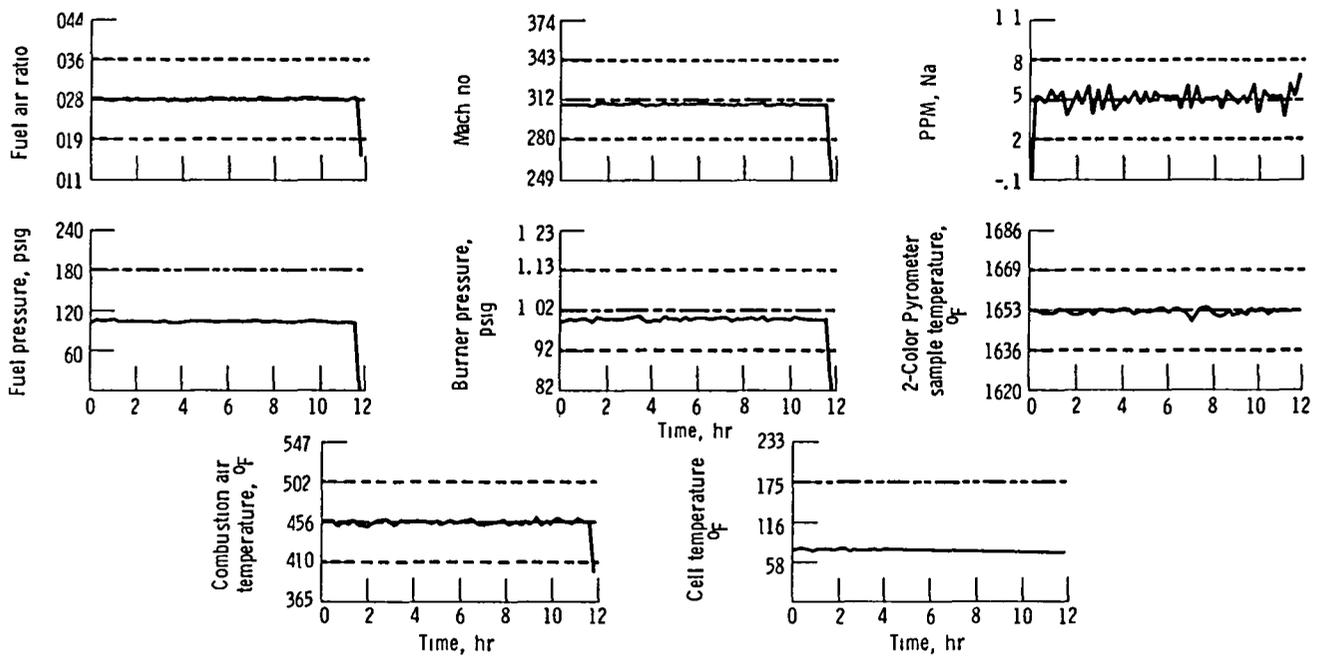
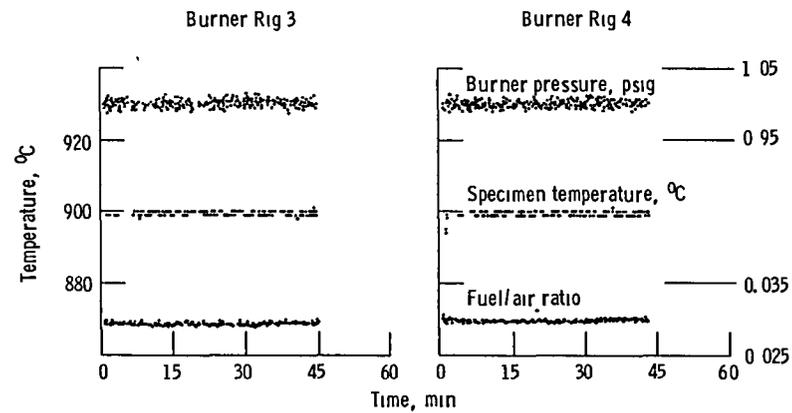


Figure 4 - Burner rig parameters using digital control (Measurement frequency was 15 min.)



(a) Screen display

Alloy identification	Burner rig. no	Current cycle no	Total no of cycles	T_{max} during cycle	Percent time temperature is $>1654^{\circ}\text{F}$ but $<T_{max}$	Percent time temperature is $>1650^{\circ}\text{F}$ but $<1654^{\circ}\text{F}$	Percent time temperature is $>T_{min}$ but $<1650^{\circ}\text{F}$	T_{min} during cycle	Fuel/air ratio	Burner pressure, psig	Fuel nozzle pressure, psig
G28-1	3	5	5	1654	0.5	98.6	0.9	1649	0.293	0.993	105
G27-1	4	5	37	1655	6	99.2	2	1650	0.300	995	104
G28-1	3	6	6	1654	6	98.9	4	1650	0.288	997	101
G27-1	4	6	38	1654	2	99.7	2	1649	0.302	1.013	102

(b) Cycle data (set point = 1652°F (900°C))

Figure 5 - Screen display and cycle data printout.

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16 Abstract Hardware and software were developed to implement the hybrid digital control of two Jet A-1 fueled Mach 0.3 burners from startup to completion of a preset number of hot corrosion flame durability cycle tests of materials at 1652 °F. This was accomplished by use of a basic language programmable microcomputer and data acquisition and control unit connected together by the IEEE-488 Bus. The absolute specimen temperature was controlled to ± 3 °F by use of digital adjustment of the fuel flow using a P-I-D (Proportional-Integral-Derivative) control algorithm. The specimen temperature was within ± 2 °F of the set point more than 90 percent of the time. Pressure control was achieved by digital adjustment of the combustion air flow using a proportional control algorithm. The burner pressure was controlled at 1.0 ± 0.02 psig. Logic schemes were incorporated into the system to protect the test specimen from abnormal test conditions in the event of a hardware or software malfunction.			
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