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Applications of Tethers in Space

Workshop Proceedings
Volume 2

Proceedings of a workshop held in
Venice, Italy
October 15-17, 1985
Applications of Tethers in Space

Workshop Proceedings Volume 2

William A. Baracat, Compiler
General Research Corporation
McLean, Virginia

Proceedings of a workshop sponsored jointly by the Italian National Space Plan, CNR, and NASA and held in Venice, Italy October 15-17, 1985
The Applications of Tethers in Space Workshop was held in Venice, Italy during the period October 15-17, 1985. The Hotel Excelsior, located on the island of Lido, provided outstanding accommodations for the workshop, which was jointly sponsored by the Italian National Space Plan, National Research Council, and the National Aeronautics and Space Administration, Office of Space Flight, Advanced Programs Division. Workshop coordination was provided by the Centro Internazionale Congressi and General Research Corporation. Aeritalia generously provided a gala dinner banquet for the workshop attendees and their guests, and the office of the Mayor of Venice hosted a reception at the city hall.

General Research Corporation would like to thank and commend everyone who organized, coordinated, and participated in the workshop. The panel co-chairmen are especially noteworthy in fulfilling their roles of directing and summarizing their respective panels. We are proud to have participated in the workshop and be a part of the advancement of this exciting and challenging field which, as is evident in these proceedings, is evolving into a technically sophisticated and mature science. The complete documentation of this workshop is contained in the Workshop Proceedings, Volumes 1 and 2. The Executive Summary, which contains an abbreviated compilation of the panel summaries, is also provided.

William A. Baracat
McLean, Virginia
March 1986
FOREWORD

The Tethers in Space Workshop held in Venice, Italy, follows by only two years the one held in Williamsburg, Virginia, in June 1983. Yet, much has happened. The most significant events are: (1) the passing of our beloved leader, Giuseppe Colombo, (2) the announcement by President Reagan of the Space Station as a national goal, and (3) the initiation of several tether demonstration missions, already in hardware development or design phases.

Bepi, whom we call the "Father of Tethers," would be pleased at the pace of this emerging technology. The development of the Tethered Satellite System (TSS), a joint U.S. - Italy project, is on a firm course, with the first launch scheduled for 1988. The announcement of the Space Station goal by the President has provided an anchor for serious studies of the use of tethers on the Space Station. A whole panel session was devoted to this subject at this workshop, and was the second best attended. NASA, Italy, and industry continue to examine the benefits and technological problems associated with placing a tether system on the Space Station. We fully expect to see this happen, although it may be after the Initial Operational Capability (IOC).

Are there other tether and tether related missions that can be flown in the next few years on the Shuttle in addition to the TSS? The answer is yes. NASA, with Italy's involvement, will be verifying the principles of electromagnetic tethers in space to produce power or drag. A series of flight experiments are either hardware ready, or in hardware development. These experiments should enhance the TSS-1 mission, and may use at some point the disposable tether, which itself will require a preliminary demonstration. Looking to the future, there is much interest in the tethered platform, with the tether assisting in platform pointing. NASA's Ames Research Center, again with the Italians, are engaged in a definition study on this, called the Kinetic Isolation Tether Experiment (KITE).
Our reach in this workshop has not only been to Earth orbit but also to the planets. Serious attention to tether operations near the Moon, Mars, and other planets is underway. Some of these ideas are presented in the workshop proceedings. Although it may sometimes seem that we are getting ahead of ourselves, these applications may be here sooner than we think.

Paul A. Penzo
March 1986
APPLICATIONS OF TETHERS IN SPACE
WORKSHOP COORDINATION

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Mr. Joseph Kolecki
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Transportation
Dr. Ernesto Vallerani
Aeritalia
Mr. Joseph Carroll
California Space Institute

Controlled Gravity
Prof. Luigi G. Napolitano
University of Naples
Dr. Charles A. Lundquist
University of Alabama

Constellations
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Aeritalia
Dr. Enrico Lorenzini
Smithsonian Astrophysical Observatory

Technology and Test
Prof. Carlo Buongiorno
Minister of Research
Mr. Paul Siemers
NASA/Langley Research Center

Space Station
Prof. Gianfranco Manarini
National Research Council
Dr. Georg von Tiesenhausen
NASA/Marshall Space Flight Center
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II

PANEL SUMMARIES AND PRESENTATIONS
TRANSPORTATION PANEL
The transportation panel has discussed the following applications and has ranked them. The ones having the best potential near-term payoffs are listed first. The rest depend increasingly on future developments, either in tether technology itself or in the remainder of the space infrastructure.

1. The Small Expendable Deployment System for boosting payloads from the shuttle
2. Electrodynamic propulsion for small and large orbit changes within LEO
3. Boosting of OTVs from the Shuttle, to reduce the delta-V needed to reach GEO
4. Launch vehicle capture & release by tethers hanging from permanent facilities
5. Artificial gravity on manned deep-space expedition vehicles during transit
6. Multi-pass remote aerobraking of planetary orbiters, to simplify navigation
7. An equatorial "staircase" or "fire brigade" to high orbits and escape
8. "Slings" of various sorts:
   a. Spinning lunar-orbiting rock collector/prospector
   b. Lunar-surface-based sling to throw rocks into low lunar orbit
   c. Asteroid-based sling (to throw rocks, or to move the asteroid itself)
   d. Hoops or solenoids with electromagnetic assist to the tether strength

The proceedings for the session are organized as follows:

1) General presentations (by Loftus and Vallerani).
2) Concept presentation and discussion summaries (1-8D).
3) Viewgraph presentations on selected concepts.
Joe Loftus, JSC

Space initiatives have moved away from single mission optimization. Space Shuttle and Space Station are complementary parts of a new, general-use infrastructure. With Space Shuttle launches normalized (e.g., to the 1st and 15th of the month), the Space Station becomes a temporary cargo storage facility, holding various satellites until their peculiar insertion windows open. As an accumulator, in this manner, Space Station almost becomes the equivalent of a 5th orbiter. The point is that Space Shuttle and Space Station are only parts of a total set, and all other space hardware and capabilities should be considered as complementary parts of a greater whole.

Ernesto Vallerani, Aeritalia

- Utilization of tethers for docking
- Explore advantages for use of tethers for planetary explorations

(A review of Chris Purvis' idea of multiple-pass tether aerobraking)
1. **Joe Carroll - Shuttle Expendable Tether System or SETS**
   (Presented at the miniworkshop)

   Initially, expendable tethers were considered in conjunction with the external tank of Space Shuttle. Since less than 1 lb. tension is needed to downward deploy the external tank, low tension deployment captured attention. A proposal for a study resulted. Deploy-only mode for expendable tethers with low (but not zero) tension means you do not need a take-up capability. The system that results is a low-tension high-braking capability system that can be used to deboost payloads by a pendulum swing release. A project to launch a 50 lb. payload from a GAS can is in the initial hardware development stage, and could fly before TSS. SETS has been approved for experimentation.

   **Critical Issues:**
   - Operations
   - Hardware
   - Safety
   - Reliability

   **Priority:** Near Term, High

   **Recommended Flight Tests:**
   - In works
   - Deboost
   - Preferred for 1st test

2. **Bill Loftus - Electrodynamic Propulsion of Tethers for Transport**

   **Critical Issues:**
   - TSS one mission & success of other early tests
   - **IMPORTANT** Value of electrodynamic propulsion is considered to be of such high priority that all possible methods should be looked at during early tether tests
   - Dynamics of orbital elements

   **Priority:** Near Term, High

   **Recommended Flight Tests:**
   - TSS I & other plasma contactor experiments needed
3. Mark Henley - Tethered OTV Operations

OTV is considered a Space Station element. OTV tether boost combined with stage and propulsive burn is the concept. Hanging and swinging tether options being considered, and Shuttle, E.T., and Space Station as launch mass options. Relative payload gains noted for all three OTV options: reusable; air propulsive; reusable aerobraked; or expendable (in decreasing order). Swinging tethers offer improved capabilities over hanging tethers without noticeable penalties. Expendable tethers are preferred over reusable tethers. Command and Control issues examined.

Mark Henley - Tether Boost Technology Demo Package

Using a Centaur to demonstrate potential to augment OTV deployment by tether. Demo in 1990s. After Centaur returns to LEO by aerobrake, it would rendezvous with Orbiter for tether demo. Called Centaur and Shuttle Tether (CAST) tether demonstration package.

Critical Issues:
-- Shuttle based v. Space Station launch
  --- maximize commonality
-- Attitude control of end mass
-- Release operations of end mass
-- TSS vs. expendable tether
  --- TSS Robust but instrumented

Priority: Near Term, High

Recommended Flight Tests: o Centaur & Shuttle Demo
Shuttle Demo
o TSS One & Other
Electrodynamic
(Plasma experiments)

4. Joe Carroll - Tethered Docking and Release of Shuttle with Space Station

Results in slightly lower apogee, much lower perigee, tethered deboost, and propellant scavenging (for transfer to an OMV).

Critical Issues:
-- Space Station SCAR design impact
-- Operation precision
-- Temporary S.S. orbit effects
-- Loads on Space Station
Priority: Near Term, High

Recommended Flight Tests: o Can be demo by SETS or TSS
 o Capture

5. Mark Henley – Low RPM Spinning Tethers for Artificial Gravity for Manned Planetary Excursions

Critical Issues:
-- Can it also be used in LEO?
 --- Proof of concept?
-- How much gravity is needed by human physiology?
-- Can it be Shuttle/TSS tested? Concept demonstration during TSS mission one or two?

Priority: Near Term, High

Recommended Flight Tests: o Some TSS I data applicable
 o TSS I in a spin mode
 o Future TSS or SETS experiments

6. Chris Purvis – Multiple-Pass Aerobraking Tethers

Using 100 km, 1 mm dia. tether hanging from a 2000 kg space probe circularized above a planet with an atmosphere, to reduce orbit height

Saves mass over a "hard shield" aerobrake.

Critical Issues:
-- Material options
-- Scheduling/control options
-- Meteoroid risk
 --- Ribbon is better?
 --- Multiple strands
-- Failure
-- Dynamics for tether
 --- Elliptical orbit?
-- How deep into atmosphere do requirements of science want probe to go?
-- Flow fields
-- Specular vs. diverse flow

Priority: Near Term, High

Recommended Flight Tests: o SETS or TSS II Demo
 o TSS II should yield data applicable
7. **Mark Henley - Use of Series of Equatorial Plane Tethers as a Stairway to Escape Velocity**

**Critical Issues:**
-- Need equatorial or polar plane launch
-- Nodes vs. Van Allen Belt

**Priority:** Later Development

**Recommended Flight Tests:**
- Other flight experiments should cover

---

8A. **Joe Carroll - Spinning Tethers to Pick Up Lunar Material**

**Critical Issues:**
-- Dynamics
-- Releasing-aiming-catching (especially core grabber)
-- Deployer hardware
-- Mass concentrations - lunar

**Priority:** Later Development

**Recommended Flight Tests:**
- Ground based tests
- TSS should be considered

---

8B. **Joe Carroll - Lunar-Surface Based Sling**

Launching 10 kg payloads, by a rotating sling on the lunar surface.

An Apollo lander sized vehicle lands and anchors itself to the lunar surface. A rover retrieves materials and passes them to the anchored sling, which throws 10 kg into lunar orbit. A lunar orbital tether station then slings payload into a lunar-Earth transfer.

**Critical Issues:**
-- Could it be scaled and tested in a vacuum chamber?
-- Does this have a customer? Are lunar materials needed?
-- Bearing loads
-- Release mechanisms
-- Can they be caught?
-- "Safety" issues
-- Shape of spinning tethers? Dynamics?
-- Manufacturing techniques for tapered tethers

**Priority:** Later Development

**Recommended Flight Tests:**
- Ground tests (vacuum)
8C. Chris Purvis - Rotating Constellation With A Center Reel, To Be Used To Sling Material From Asteroid Belt Without Landing

Critical Issues:
--- Basic design
--- On asteroid or in space?
--- Release, aiming, etc.?

Priority: Later Development

Recommended Flight Tests: o Ground tests

8D. Chris Purvis - Rotating Hoop of Tether Material, Under Magnetic Field to Reduce Tension, to be Used as a Method of Slinging Material from Lunar Surface

- Critical Issues:
  --- Super-magnetic technology
  --- Supplement the tensile properties of the material
  --- Dynamics
  --- Releasing-aiming-catching (especially core grabber)
  --- Deployer hardware
  --- Mass concentrations - lunar
  --- Electrical energy
  --- Throughput potential
  ---

Priority: Later Development

Recommended Flight Tests: o Ground tests seem in order
                     o Further examination
Symmetric Rotating Tether System For Returning Material From Near-Earth Asteroids (Can be in Free Flight or Bolted to Asteroid)
• Rotating Hoop Tether

Can Have Rim Velocities in Excess of Material Characteristic Velocity

SPINNING TETHER 1cm in diameter in very strong 100w/m² field can experience no tension at >2kms⁻¹ rim velocity could fling payloads capable of withstanding 4000g’s (Current power ~1000 w)
SMALL EXPENDABLE DEPLOYMENT SYSTEM (SEDS)

Joseph A. Carroll
Energy Science Laboratories, Inc.
11404 Sorrento Valley Rd., #113
San Diego, CA  92121
619/452-7039
OUTLINE OF PRESENTATION:

- Introduction to Basic Concept
- Summary of Phase I Findings
- Summary of Phase II Status
- Potential Applications
- Conclusions & Recommendations
Low-Tension Deployment Followed by Pendulum Swing & Release
What is special about this deployment concept?
Low tension deployment & swinging release
Disposable tether
Comparison of hanging and swinging releases for equal energy and momentum transfer:

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<th>35°</th>
<th>85°</th>
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<td>1</td>
<td>.89</td>
<td>.91</td>
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<tr>
<td>Meteoroid hazard</td>
<td>1</td>
<td>.27</td>
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<td>Power dissipation</td>
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What advantages does a disposable tether have?

- Eliminates time-consuming retrieval operation
- Simplifies deployer: no motors or level-winders needed
- Eliminates need for TSS-like boom & docking gear
- Minimizes tether degradation (new tether each time)
What have we studied during the SBIR Phase I study?

Control strategies
STS operational impacts
Safety & reliability
Deployer locations
Prototype hardware
New concepts
Early applications
Range of performance benefits
Benefits of GAS-sized Tether System to STS (Preliminary)
SUMMARY OF SBIR PHASE II EFFORT
(April 1985 — March 1987)

Primary objective:

- To bring our concept to flight-test-ready status

Secondary objectives:

- To determine the range of potential users & benefits;
- To make the test system similar to the operational one;
- To benefit the TSS & TAS programs.

Phase II Tasks & Fraction of Effort:

- Design, develop, test, & evaluate hardware: 40%
- Analyze systems integration, safety, & reliability: 25%
- Study control options & improve simulations: 20%
- Identify early applications & performance benefits: 15%
Possible Tether Recoil Trajectory if Prompt Snag Prevents Rewinding

Possible Tether Trajectory With RCS Use & "Rocking-Horse" Strategy
A TYPICAL INTEGRATION ISSUE:

"All nonmetallic materials exposed to the payload bay shall be selected for low outgassing characteristics. Material selection criteria of 1 percent, or less, total mass loss and 0.1 percent, or less, Volatile Condensible Material (VCM) as defined in NASA/JSC Specification SP-R-0022A, or its equivalent, shall be used."

ICD 2-19001, section 10.6.2

Kevlar 29 contains up to about 7% water at 55% RH, and that water comes out rather slowly in a vacuum.

Possible solutions to this problem include:

- Seek waivers (& hope other users don't object);
- Keep the deployer sealed until ready for use;
- Dry out the tether before launch & keep it sealed;
- Use non-hygroscopic tethers (e.g., Spectra 900).
CONTROLS & SIMULATION STUDIES

- Identify the most important design & operation parameters;
  (e.g., effects of payload mass, tether tension, etc.)

- Enhance & use simulation programs to support other analyses;
  (We plan to enhance our 2-D simulation program to run on
  a MacIntosh with simple input & real-time graphic output.
  We plan to use GTOSS for most detailed simulations, and
  maybe SLACK2 for severed-tether simulations.)

- Refine operations & controls for best-early-candidate users.
  (Some new applications require new control strategies.)
POTENTIAL APPLICATIONS OF SEDS

• Dilemma: "Useful" tests are desired with real payloads, but reliability worries, integration time, and payload problems may delay early tests.

• Response: Use cheap payloads that don't REQUIRE a boost:
  - Deployable GAS for calibrating airport radar;
  - Other "We'll take whatever we can get" STS users";
  - Controlled-reentry test for station priority cargo;
  - Chemical release experiments;
  - Dedicated passive payloads.

• Later operational uses:
  - Electrodynamiic power tether for extended STS missions;
  - (Re)boosting major payloads (LDEF, AXAF, SolarMax, etc.)
  - Boosting supply caches for future use on space station.
CONCLUSIONS:

• SEDS may provide larger benefits than most STS enhancements, at radically lower cost.

• SEDS & TSS have complementary capabilities & roles.

• SEDS may facilitate quick-turnaround tether experiments.

RECOMMENDATIONS:

• NASA fund one or more early flight tests of SEDS.

• STS users consider what "cheap boosts... can do for them.
TETHERED OTV OPERATIONS

Mark W. Henley
General Dynamics
Space Systems Division

INTRODUCTION

Do tethers make sense for the Orbital Transfer Vehicle? This question is addressed here, as a part of OTV flight operations, as the operational issues of tether launch for the OTV are considered to be more significant even than technical issues. The answer to this question is that tether boost is an attractive option for OTV in spite of the significant operational issues. Expendable shuttle-based swinging tether boost is recommended for near term applications requiring a moderate (~20%) increase in OTV payload capability. Heavier reusable tether systems are recommended for far term applications from the Space Station or other orbiting facilities, further improving OTV payload capacity, and with a corresponding increase in operational complexity.

TETHER PRINCIPALS

The concept of a tether boost for the OTV is based upon the exchange of momentum between the OTV and a lower orbiting object, such as the Space Station, Space Shuttle or External Tank. The OTV is given a small delta V upon release, which can be subtracted from the total delta V requirements of the mission, as illustrated to scale for the trajectory of a static vertical tether in figure 1. Because of the exponential relationship between delta V and payload delivery capability, a substantial payload gain is realized by a relatively small delta V reduction.

Figure 1. Tether boost for OTV is illustrated in an example trajectory.
TETHERED OTV OPERATIONS

For any action, there is an equal and opposite reaction. The reaction, in this case, is a loss of orbital velocity by the lower mass in the tethered system. Momentum (mass x velocity) gained by the OTV equals that lost by the lower mass, and thus a heavier lower mass will have a smaller change in velocity than the OTV (a lighter, upper mass).

A tether is acted upon by the gradient in the gravitational potential of the earth. The higher mass is farther from the earth's center of mass and experiences less gravitational attraction than the lower mass. This difference in gravitational attraction results in a tension in the tether which is proportional to the vertical displacement between the orbiting masses. A tether system which is vertically oriented with respect to the earth will actually make one rotation per orbit in an inertial frame of reference, adding a centrifugal term (half that from the gravity gradient) to the tension in the tether. A vertically oriented tether system is in a stable configuration, whereas a system with a component of horizontal displacement will not remain in that orientation, but will swing in response to gravitational forces (and initial velocity conditions). Both of these systems are considered here for OTV boost.

Figures 2a and b illustrate the trajectories resulting from release of an OTV from static (vertical) and swinging tether systems. The lower mass in these illustrations is considerably heavier than the OTV, causing less change in its orbit than the boost to the OTV upon release from the tether tip. The swinging tether strategy, as noted, results in a substantially greater apogee increase for a given tether length. Operations in the swinging strategy are simplified somewhat by the reduced tether length, but involve more complicated dynamics. The static case may actually be more difficult to achieve than the swinging case, as orbital dynamics cause a swinging motion upon extension of a tether in the vertical direction.
TETHERED OTV OPERATIONS

TETHER BOOST SYSTEM OPTIONS

OTV boost through tether operations may utilize a variety of lower masses for momentum exchange. The options of using the Space Shuttle, External Tank, and Space Station as the lower mass are illustrated in figure 3. Additional far term options are possible, such as a dedicated orbiting transportation node, similar to the Space Station in its transportation function, but without the constraints upon tethered operations imposed by Space Station users.

TETHERED OTV BOOST SYSTEM OPTIONS

![Diagram showing three options for OTV boost systems: OTV-NSTS, OTV-ET, OTV-SS.]

<table>
<thead>
<tr>
<th></th>
<th>OTV-NSTS</th>
<th>OTV-ET</th>
<th>OTV-SS</th>
</tr>
</thead>
<tbody>
<tr>
<td>Launch option</td>
<td>Swinging OK</td>
<td>Swinging OK</td>
<td>Hanging only</td>
</tr>
<tr>
<td>OTV mass</td>
<td>30 tons</td>
<td>30 tons</td>
<td>30 tons</td>
</tr>
<tr>
<td>Other mass</td>
<td>90 tons</td>
<td>35 tons</td>
<td>200 tons</td>
</tr>
<tr>
<td>OTV boost</td>
<td>10 × length</td>
<td>7 × length</td>
<td>6 × length</td>
</tr>
<tr>
<td>Other deboost</td>
<td>3 × length</td>
<td>6 × length</td>
<td>1 × length</td>
</tr>
<tr>
<td>Deboost effect</td>
<td>Lower Orbit</td>
<td>Re-entry</td>
<td>Undesireable</td>
</tr>
<tr>
<td>Accelerations</td>
<td>Inconsequential</td>
<td>Inconsequential</td>
<td>Undesireable</td>
</tr>
</tbody>
</table>

Figure 3. Several options exist for the lower mass in tethered OTV boost.
Momentum exchange is desirable for reducing the orbital energy of the Space Shuttle and External Tank, but may be detrimental to the Space Station. Space Station orientation constraints also limit the tether operations to near vertical deployment, and the microgravity environment on the Space Station is expected to exceed 10^-5 g during tether operations. Space Station operational considerations are noted below in figure 4.

Considerations for tether-launched OTV
- Momentum of OTV launched must be balanced by an opposite reaction to maintain Space Station altitude:
  - Use Space Station propulsion
  - De-orbit mass (ET, Shuttle, etc)
- Change in Space Station altitude must remain within acceptable limits
- Acceleration levels aboard the Space Station will exceed 10^-5 g during tether operations (may exceed allowable limits for materials processing)

Figure 4. Space Station operations would be constrained by OTV boost.
PERFORMANCE BENEFITS

OTV payload capability improvement is the object of tether boost scenarios. This increase in payload capability may be utilized in baseline OTV launch strategies, or in special circumstances when payload mass exceeds normal OTV capabilities. Relative payload gain from tether boost for a reference OTV is plotted in figure 5 as a function of initial delta V supplied by the tether. Payload improvement is illustrated for this vehicle in an all propulsive, aerobraked, and expendable mode of operation. The dramatic difference in percent payload improvement between these modes of operation is not duplicated on an absolute scale (pounds of payload gained). Total payload of this reference vehicle without the tether boost varies substantially depending upon mode of operation (all-propulsive, aerobraked, or expendable).

Figure 5. Relative payload gain depends upon OTV type.
TETHERED OTV OPERATIONS

STATIC vs SWINGING TETHER BOOST

The pros and cons of static and swinging tether boost systems are noted in figure 6. The static tether is in a lower energy state than the swinging tether, and must dissipate (or store / use) the energy generated during tether deployment. The swinging tether converts this energy, instead, to motion of the tether system (resulting in an approximately doubled tether delta V for a given tether length); the swinging tether apparatus is expected to suffice with a friction brake for low level energy dissipation, as opposed to the more elaborate devices required for the static tether system. System weight is reduced by the simpler energy dissipation mechanism, and the tether itself is approximately 12% lighter than that required for an equal delta V using a static tether. Reuse of either system would be operationally complex, probably requiring a tether tip satellite which assists in system control during the reeling in operation. The static tether system, however, is expected to be more amenable to reuse.

<table>
<thead>
<tr>
<th>Issue</th>
<th>Hanging*</th>
<th>Swinging</th>
</tr>
</thead>
<tbody>
<tr>
<td>Deployment</td>
<td>Vertical</td>
<td>Horizontal</td>
</tr>
<tr>
<td>Power dissipation</td>
<td>Needed</td>
<td>Not required</td>
</tr>
<tr>
<td>System weight</td>
<td>Heavier</td>
<td>Lighter</td>
</tr>
<tr>
<td>System volume</td>
<td>Greater</td>
<td>Lesser</td>
</tr>
<tr>
<td>Tether weight</td>
<td>10% heavier</td>
<td>10% lighter</td>
</tr>
<tr>
<td>Tether length</td>
<td>Longer (~double)</td>
<td>Shorter (~1/2)</td>
</tr>
<tr>
<td>OPS duration</td>
<td>Similar</td>
<td>Similar</td>
</tr>
<tr>
<td>OPS complexity</td>
<td>Similar</td>
<td>Similar</td>
</tr>
</tbody>
</table>

*Some swinging motion is generated (& damping operations needed) with vertical tether deployment & retraction

Figure 6. Swinging tether issues compare well to static (hanging) issues.
TETHERED OTV OPERATIONS

EXPENDABLE vs REUSABLE TETHER SYSTEM

Expendable and reusable tether systems both show potential benefits for OTV. A trade between these two alternatives, figure 7, shows that an expendable system is operationally more desirable, primarily because of the absence of retrieval operations. System mass is also a major issue—the reusable system is expected to be substantially heavier, due to the increased mass of the apparatus (which includes a tether tip satellite), and the substantial electrical power is required for the retrieval operations. An expendable tether may remain temporarily in LEO, as is suggested below, or may be released directly into a re-entry trajectory.

<table>
<thead>
<tr>
<th>Issues</th>
<th>Expendable</th>
<th>Reusable</th>
</tr>
</thead>
<tbody>
<tr>
<td>Timelines</td>
<td>Shorter duration</td>
<td>Longer duration</td>
</tr>
<tr>
<td>Complexity</td>
<td>Simpler operation</td>
<td>Added operation</td>
</tr>
<tr>
<td>Reliability</td>
<td>Affected by duration &amp; complexity</td>
<td></td>
</tr>
<tr>
<td>Weight</td>
<td>Lighter system</td>
<td>Heavier system</td>
</tr>
<tr>
<td>Control</td>
<td>Shuttle/OTV RCS</td>
<td>Sub-satellite</td>
</tr>
<tr>
<td>Debris</td>
<td>Tether stays in orbit</td>
<td>No debris release</td>
</tr>
<tr>
<td></td>
<td>(Rapid orbital decay)</td>
<td></td>
</tr>
</tbody>
</table>

Figure 7. Expendable tethers may simplify OTV tether boost operations.
TETHERED OTV OPERATIONS

An expendable system is only beneficial if the tether system is less massive than the propellant required for an equivalent payload increase. In figure 8, payload increase is plotted against tether mass. From the approximation that the tether mass is one half that of the expendable tether system, a limit is derived to the practical extent of an expendable tether. In the event that an OTV is insufficiently sized for a particular payload, expendable tether launch may be worthwhile beyond the approximate limit shown here. Note that the regimes below refer to a particular OTV design and do not necessarily indicate limits for other vehicle designs.

*Based upon equations for Kevlar from J. Carroll in "Guidebook for Analysis at Tether Applications"

Figure 8. Expendable tether boost for OTV is limited in scope.
TETHERED OTV OPERATIONS

EXPENDABLE SHUTTLE-BASED TETHER OPERATIONS

A swinging, expendable tether system is suggested for Space Shuttle operations. Operation of this system (figure 9) is divided into four time periods, deployment, swinging, release, and post-release operations. In this scenario, the tether is either left in a low orbit (with an orbital lifetime on the order of days, so that orbital debris hazard generation is minimal), or is released from the OTV into a re-entry trajectory.

SHUTTLE-BASED EXPENDABLE TETHER BOOST OPERATIONS

1) Tether deployment
   • NSTS RCS initiates deployment
   • Brake controls deployment rate
2) Tether swinging
   • Brake halts deployment
   • Gravity gradient causes swing
3) Tether release
   • Timed for maximum Delta V gain
   • Vehicles enter new orbits
4) Mission complete
   • NSTS prepares for reentry
   • OTV prepares for first burn
   • Tether orbit decays rapidly

Figure 9. An expendable tether is recommended for Shuttle-based OTV boost.
TETHERED OTV OPERATIONS

A more detailed view of a candidate tether system apparatus is shown in figure 10. The first member of the RMS arm is utilized as a part of the system, and is supported by two lines in order to spread the tether's tensional load across the Space Shuttle's center of mass. The tether itself resides within a protective sleeve running the length of the first RMS member; this serves to protect both the tether, by shielding it, and the orbiter, by preventing any potential tether breakage in this region from possible entanglement with the RMS arm. A remote disconnect mechanism is shown at the OTV, which is to be activated after a guillotine mechanism within the tether canister/deployer releases the Space Shuttle from the lower end of the tether. The canister/deployer suggested is a derivative of a predecessor currently being developed under MSFC funding. The system illustrated is not necessarily a final recommendation, but represents the best of several alternatives traded on the basis of weight and volume minimization.

Figure 10. Shuttle-based tether boost may use a system such as this.
TETHERED OTV OPERATIONS

COMMAND and CONTROL

Three options are explored in figure 11 for the command and control of shuttle-based tether boost operations for OTV. The primary difference between these alternatives of passive, assisted, and active control is the inclusion of operations by a tether tip satellite or the OTV itself for the latter two options, respectively. A sufficient degree of control is expected through passive operations, in which the Space Shuttle supplies the delta V for initial separation and subsequent corrections, and the OTV acts as a dumb mass, becoming activated after release from the tether tip. Assisted and active control options are desirable, but not mandated for tether operations.

<table>
<thead>
<tr>
<th></th>
<th>Passive</th>
<th>Assisted</th>
<th>Active</th>
</tr>
</thead>
<tbody>
<tr>
<td>Tether tip control</td>
<td>None</td>
<td>Sub-satellite</td>
<td>OTV RCS</td>
</tr>
<tr>
<td>Shuttle RCS control</td>
<td>Primary</td>
<td>Back-up</td>
<td>Back-up</td>
</tr>
<tr>
<td>Deployment rate</td>
<td>Tether brake</td>
<td>Tether brake</td>
<td>Tether brake</td>
</tr>
<tr>
<td>Libration damping</td>
<td>None/NSTS</td>
<td>Sub-satellite</td>
<td>OTV/NSTS RCS</td>
</tr>
<tr>
<td>Release at Shuttle</td>
<td>Guillotine</td>
<td>Guillotine</td>
<td>Guillotine</td>
</tr>
<tr>
<td>Release at OTV</td>
<td>Tether tip</td>
<td>Sub-satellite</td>
<td>OTV control</td>
</tr>
<tr>
<td>Degree of control</td>
<td>Sufficient</td>
<td>Precise</td>
<td>Precise</td>
</tr>
</tbody>
</table>

Figure 11. Control may be passive, active (sub-satellite), or through OTV RCS.
SAFETY CONSIDERATIONS

Tether entanglement and breakage hazards must be minimized, with thorough contingency planning if tether boost operations are to be considered a realistic option for the OTV. Figure 12 lists a number of precautions against these hazards. Hazards to Space Shuttle operations are more critical than to Space Station operations due to the more limited time and resources available for repair. Safety issues must be considered in depth in the design of tether boost systems for ouch.

### Safety Considerations

<table>
<thead>
<tr>
<th>Hazard</th>
<th>Precautions</th>
</tr>
</thead>
<tbody>
<tr>
<td>Tether entanglement</td>
<td>• Ensleeve tether in low abrasion tubing between reel &amp; “rod” tip</td>
</tr>
<tr>
<td></td>
<td>• Make system jettisonable</td>
</tr>
<tr>
<td></td>
<td>• Supply EVA tools &amp; training for contingency extrication</td>
</tr>
<tr>
<td>Tether breakage</td>
<td>• Minimize exposure period to micrometeoroids &amp; orbital debris</td>
</tr>
<tr>
<td></td>
<td>• Monitor tether tension &amp; integrity (e.g., fiber optics)</td>
</tr>
<tr>
<td></td>
<td>• Jettison tether in event of break</td>
</tr>
<tr>
<td></td>
<td>• Use RCS to maneuver away from jettisonned tether system</td>
</tr>
<tr>
<td></td>
<td>• Keep Shuttle altitude high enough to prevent re-entry</td>
</tr>
</tbody>
</table>

Figure 12. Safety issues must be resolved for tethered OTV operations.
TETHERED PROPELLANT DEPOT

The concept of a tethered propellant depot for OTV propellant storage and acquisition on the Space Station has been traded against that of an attached depot in figure 13. The Bond number (Bo, the ratio of gravity gradient forces to surface tension forces) associated with a propellant depot located at the bottom of the Space Station is sufficient for the settling of OTV propellants in large diameter tanks, removing part of the rationale for such a depot. Safety would be improved by the more distant location of potentially hazardous propellant supplies on a tethered depot, but safety would also be enhanced by a contingency supply of oxygen and water from OTV propellant supplies attached to the Space Station. Operations in general would be more difficult with a tethered depot, and the microgravity environment would be disrupted unless (and perhaps even if) a second tethered mass were extended from the Space Station in the opposite direction.

<table>
<thead>
<tr>
<th>Issues</th>
<th>Difficult rendezvous</th>
<th>Normal rendezvous</th>
</tr>
</thead>
<tbody>
<tr>
<td>Operations</td>
<td>Tether launch difficult</td>
<td>Tether launch ok</td>
</tr>
<tr>
<td></td>
<td>Impacts Space Station</td>
<td>Normal SS prox. ops.</td>
</tr>
<tr>
<td></td>
<td>prox. ops.</td>
<td></td>
</tr>
<tr>
<td>Safety</td>
<td>Distant propellants</td>
<td>Contingency O₂ &amp; H₂O</td>
</tr>
<tr>
<td>Commonality</td>
<td>More than 10⁻⁵g</td>
<td>Propulsion, ECLSS</td>
</tr>
<tr>
<td>Microgravity</td>
<td></td>
<td>Less than 10⁻⁵g</td>
</tr>
<tr>
<td>Propellant settling</td>
<td>LH₂ settles (B₀ &gt; 50)</td>
<td>LH₂ settles (B₀ &gt; 50)</td>
</tr>
</tbody>
</table>

Figure 13. A tethered OTV propellant depot is not necessarily recommended.
ADVANCED TETHER APPLICATIONS

Advanced applications of tethers for OTV extend as far as one's imagination wishes. Several of these potential applications are worthy of further study. Figure 14 illustrates the use of a tether to exchange momentum between the OTV and its payload, the scenario shown here is that of payload delivery to the moon, but the same concept can be applied to put a payload in an approximate final orbit. A rotating tether system might be useful for the creation of an artificial sense of gravity for manned OTV missions of long duration, such as would be expected in the exploration of Mars. Earlier it was mentioned that a separate orbital transportation node might be desirable in LEO, such a facility could use techniques beyond those already discussed for improving OTV payload capability. For example, rotational tether systems are feasible in addition to the static and swinging system alternatives which have been discussed. These are but a few of the potential applications of tethers which the OTV might evolve to use in the long term.

ADVANCED TETHER APPLICATION EXAMPLE

- Momentum transfer via rotating tether can supply part of the ΔV required for delivery of mass to the lunar surface
  - Less ΔV needed for Lunar Lander
  - Less ΔV needed for OTV return to Earth
- Similar strategy may be used for GEO delivery

Figure 14. Lunar delivery illustrates the evolution of tethered OTV operations.
SUMMARY

The preceding discussion has centered upon the operational aspects of tether boost for the OTV. Major conclusions from this discussion are listed in figure 15. Tether boost for the OTV is recommended as an option which deserves increased emphasis in the future. Swinging, expendable Shuttle-based operations have received little, if any, attention in the past, but have been identified here to have a potential for OTV payload improvement. Reusable, space-based tether systems are considered to be more feasible for long term applications involving larger delta V gains. Development and demonstration of OTV-associated tether technology and operations should be given a high priority by NASA.
Centaur And Shuttle Tether Technology Demonstration Package

Tether assisted OTV launch from an orbiting facility (Shuttle, Space Station, Platform, etc.) can supply an initial velocity boost and substantially increase OTV payload. Technology for tether boost of the OTV is relatively simple compared to other technology advancements with similar performance benefits, such as aerobraking or advanced engine development. The basic technology for tether assisted launch can be demonstrated early and effectively by the use of the Shuttle-Centaur as a mock OTV, as is suggested in figure 1.

Figure 1. An expended Shuttle-Centaur may be used to demonstrate the technology required for tethered boost operations for the OTV.
CAST TDP

The proposed Centaur and Shuttle Tether Technology Demonstration Package (CAST TDP) can test the operations and hardware for tethered launch of an OTV from the Shuttle, and can demonstrate an initial velocity boost achieved upon release of the tether (figure 2).

CENTAUR & SHUTTLE TETHER TECHNOLOGY
DEMONSTRATED PACKAGE
Trajectory

Figure 2. The CAST TDP trajectory simulates that of a tethered OTV boost.

The CAST TDP is a scaled-down simulation of an actual tethered OTV launch. The large size of the expended Shuttle-Centaur (Shuttle-Centaur) reasonably represents the OTV. Tether length, mass and tension, and "OTV" mass and delta V boost for this demonstration are a modest fraction of those occurring in an actual OTV launch. The deboost delta V received by the shuttle, a potential secondary benefit from a tethered OTV launch, is also less significant for the CAST TDP. Estimates of these parameters are listed in the following table for both the CAST TDP and a tethered OTV launch.
CAST TDP

<table>
<thead>
<tr>
<th>Lower vehicle</th>
<th>Shuttle</th>
<th>Technology</th>
<th>Shuttle</th>
<th>Technology</th>
</tr>
</thead>
<tbody>
<tr>
<td>Upper vehicle</td>
<td>Expended Centaur</td>
<td>14 n.m. (~25 km)</td>
<td>40 n.m. (~75 km)</td>
<td></td>
</tr>
<tr>
<td>Tether length</td>
<td>150 lbf (680 N)</td>
<td>4,000 lbf (18,000 N)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Tether mass</td>
<td>50 lbm (23 kg)</td>
<td>4,000 lbm (1,800 kg)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>V gain of upper mass</td>
<td>330 ft/s (100 m/s)</td>
<td>750 ft/s (230 m/s)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>V loss of lower mass</td>
<td>10 ft/s (3 m/s)</td>
<td>250 ft/s (76 m/s)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Tether guide system</td>
<td>RMS arm attachment</td>
<td>RMS arm attachment</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Tether container</td>
<td>Small canister</td>
<td>Compact pallet or canister</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

Interfaces for the CAST TDP include both data transmission and physical connections (Figure 3). The Shuttle-Centaur must return to LEO after fulfilling its primary mission, requiring avionics modifications identical to those found in other proposed TDPs which return the Shuttle-Centaur to LEO. Additional power may be required in order for the Shuttle-Centaur to collect and transmit experimental data such as accelerometer and inertial attitude readings. Data interfaces aboard the Shuttle include visual and radar observation, and the monitoring/control of tether tension, attitude, and deployment velocity.

<table>
<thead>
<tr>
<th>Interface</th>
<th>Requirements</th>
</tr>
</thead>
<tbody>
<tr>
<td>Shuttle/Centaur</td>
<td>As per aerobrake TDP for return to NSTS Replace double by quad thrusters Point through CM of expended Shuttle/Centaur</td>
</tr>
<tr>
<td>Tether system</td>
<td>EVA or RMS attachment to Shuttle/Centaur Contain &amp; deploy tether Spread load across NSTS CM Constrain tether relation to NSTS CM Control tension, velocity, release time</td>
</tr>
<tr>
<td>NSTS</td>
<td>Monitor position, attitude, dynamics Monitor distant Shuttle/Centaur motions Initiate deployment &amp; control attitude</td>
</tr>
</tbody>
</table>

Figure 3. CAST interfaces require minor modifications of existing systems.
CAST TDP

Physical interfaces consist of the connections between the tether system and the end masses (Shuttle and Shuttle-Centaur), and of the mechanisms which control tension and release. Tether tension must be transmitted directly through the Shuttle’s center of mass (CM) in order to avoid the introduction of a torque upon the Shuttle during tether operations; supporting lines are used here to effect the spreading of the tensional load across a region which includes the Shuttle’s CM. For the CAST TDP, the tether interface with the upper vehicle does not necessarily need to remotely disconnect, as it would in actual practice, it is desirable, however, to include a remote disconnect capability in order to accurately simulate a tethered OTV launch. A redundant tether release mechanism at the Shuttle is required both for the experiment and in practice, with EVA backup and jettisoning of tether apparatus available as contingency options to ensure separation of the tether from the Shuttle.

The CAST TDP offers a relatively lightweight and low cost method of demonstrating OTV tether launch operations and delta V gain upon tether release (Figure 4). The TDP achieves minimal weight through the selection of an expendable, rather than reusable, tether system, and by using the RMS arm in a dual role (for both manipulating the mock OTV and for spreading tether tension across the Shuttle’s CM). The volume required for the package is also minimal, allowing an essentially a full Shuttle Cargo Bay Envelope for the primary Shuttle-Centaur mission. Dimensions of the tether deployment canister are those of a Get Away Special canister, and would be scaled up for the tethered launch of an OTV and its payload. Other hardware designed for the CAST TDP is capable of later use in a tethered OTV launch.

Tether system
- Tether tip mechanism 25
- RMS attachment 100
- Supporting lines 20
- Tether canister 150
- Tether & controls 200
- Shuttle RCS propellant +200
- Subtotal; additional weight on Shuttle 695
- Contingency (= 15%) +105
Total 800 lbm 363 kg

Figure 4. The CAST TDP offers a lightweight and low cost method of testing tether boost operations and hardware for OTV.
CAST TDP

Timelines for the CAST TDP are dependent upon mission selection and comanifestation of other TDPs on the same mission. The CAST TDP requires the return of the expended Shuttle-Centaur to LEO, which is accomplished by several other proposed TDPs. Timelines (Figure 5) therefore begin after the return of the Shuttle-Centaur to LEO, in a reference scenario which uses an aerobraking technology demonstration to bring the Shuttle-Centaur back to the vicinity of the Shuttle.

**TIMELINE FOR CAST TECHNOLOGY DEMONSTRATION**

<table>
<thead>
<tr>
<th>Event title</th>
<th>Start</th>
<th>Duration</th>
<th>Finish</th>
</tr>
</thead>
<tbody>
<tr>
<td>Aerobrake TDP (returns expended Centaur to LEO)</td>
<td>00:00:00</td>
<td>34:20:00</td>
<td>34:20:00</td>
</tr>
<tr>
<td>Centaur phasing</td>
<td>34:20:00</td>
<td>06:00:00</td>
<td>40:20:00</td>
</tr>
<tr>
<td>Remaining Centaur propellants dumped</td>
<td>34:20:00</td>
<td>01:00:00</td>
<td>35:20:00</td>
</tr>
<tr>
<td>Tethered OTV TDP</td>
<td>40:20:00</td>
<td>00:00:00</td>
<td>40:20:00</td>
</tr>
<tr>
<td>Centaur co-orbits with Shuttle Orbiter</td>
<td>40:20:00</td>
<td>00:10:00</td>
<td>40:30:00</td>
</tr>
<tr>
<td>Orbiter maneuvers close to Centaur</td>
<td>40:30:00</td>
<td>00:30:00</td>
<td>41:00:00</td>
</tr>
<tr>
<td>Centaur captured with RMS</td>
<td>41:00:00</td>
<td>00:15:00</td>
<td>41:15:00</td>
</tr>
<tr>
<td>Visual inspection of Centaur/aerobrake</td>
<td>41:15:00</td>
<td>00:15:00</td>
<td>41:30:00</td>
</tr>
<tr>
<td>EVA to tether Orbiter to Centaur</td>
<td>41:30:00</td>
<td>04:00:00</td>
<td>45:30:00</td>
</tr>
<tr>
<td>Remove thermal material samples from Centaur</td>
<td>41:30:00</td>
<td>00:30:00</td>
<td>42:00:00</td>
</tr>
<tr>
<td>Tethered Centaur deployment</td>
<td>45:30:00</td>
<td>06:00:00</td>
<td>51:30:00</td>
</tr>
<tr>
<td>Release Centaur &amp; tether</td>
<td>51:30:00</td>
<td>00:00:00</td>
<td>51:30:00</td>
</tr>
</tbody>
</table>

Figure 5. CAST TDP timelines follow completion of the primary mission.

The CAST TDP timeline is of a relatively short duration, with tether system connection and tether deployment encompassing most of the operational time. EVA is used in this reference timeline partly for simplicity in making tether apparatus connections - alternatively, the RMS may be able to perform this function, shortening timelines and reducing costs. Tether deployment is expected to require approximately 90 minutes for extension and 30 minutes for swinging; a wide margin of excess time is allotted in this reference timeline, which might be shortened considerably in the actual mission.

The reference timeline estimates, while of relatively short duration, may be further shortened in order to reduce power storage requirements associated with longer mission durations. Shuttle-Centaur power availability during the CAST TDP can be omitted at the expense of the absence of data transmission from the Shuttle-Centaur. We recognize the value of active Shuttle-Centaur avionics throughout the CAST TDP however, and hence measures are being considered to reduce timelines and improve time-dependent power supplies.
CAST TDP

Many issues remain for the CAST Technology Demonstration Package, as summarized below in figure 6. It is hoped that a variation of the package discussed in the preceding pages can be flown in the relatively near future, in order to make this technology available for OTV applications.

ISSUES

Centaur & Shuttle Tether TDP

• Should avionics remain activated for TDP?
  — Three-axis accelerometer data desireable
  — Shuttle/Centaur RCS maneuvers possible
  — Requires additional power provision

• Should TDP scope be increased?
  — Current scope limited by selected mission
  — Larger TDP weight allocation desireable

• Is RMS modification appropriate?
  — Requalification required
  — Other options may be better suited to TDP

• Are alternate missions available for TDP?
  — Requires return of Centaur to Shuttle

• Several hardware elements required are TBD
  — Attach points on CISS, Centaur & RMS
  — Suitable deployer in early development

• Disposal of Centaur & aerobrake after TDP
  — Can RCS initiate re-entry?
  — Is downward tether boost alternative preferable?
CONTROLLED GRAVITY PANEL
During its deliberations, this Panel formulated a significant class of opportunities that the panel denoted as "controlled gravity". This capability offered by tether systems has unique aspects that seem not to have been fully appreciated or articulated previously. These topics reach to the very foundations of fundamental science and still have immediately apparent practical possibilities. In the experience of the Panel members this is a rare and precious circumstance deserving serious and careful attention. Therefore this report seeks first to convey the concepts of controlled gravity that the Panel found so intriguing and promising.

A parallel between electromagnetic and gravitational fields may be instructive. Man's control and use of electromagnetic fields is the very basis of modern technology. The same is not as true of gravitational fields or their equivalent acceleration fields (The equivalence of gravitational and acceleration fields is a fundamental tenet of relativistic mechanics). Most of man's experience is in a familiar and comfortable gravity field of about 9.8 m/s^2. To be sure, higher acceleration fields can be produced in centrifuge apparatus, and these have widespread practical applications. The advent of spacecraft gave the first possibility of appreciable durations of near-zero acceleration fields.

The vicinity of the center of mass of a small body in a free-fall gravitational orbit experiences very small acceleration fields. The term microgravity environment has come into common usage for this situation, although the actual accelerations may vary by at a factor ± 10^2 from the 10^-4g implied by a literal interpretation of the term, (g = the acceleration on the equator at mean sea level on the Earth surface). The possibility to perform experiments in microgravity and prospects for subsequent commercial operations is the motivation for serious scientific and development efforts in several national space programs.

Tether systems offer the new possibility of controlled acceleration fields, or controlled gravity, in the range from 10^-1g to values below 10^-6g, perhaps even 10^-8g. Still smaller accelerations require other techniques, as developed
for investigations of fundamental gravitational physics (See, for example, Robert L. Forward, "Flattening spacetime near the Earth," Phys. Rev. D 26 pp 735-744, 15 Aug 1982). Tether systems achieve their control through placing experiments at significantly large displacements from the orbit center or zero acceleration position of an orbiting system. The system may either be in a gravity gradient stabilized configuration (rotating once per orbit in an inertial frame), or it may be rotating more rapidly.

As used in the previous paragraph, controlled has broad interpretation. It includes not only the magnitude of the acceleration field, but also its vector properties, its time dependence, and the uncertainty or noise associated with them. For example, by varying the length of a tether in accordance with a prescribed control law, a desired time dependent acceleration field can be imposed on an experiment system. This changing field could be a step function of increasing or decreasing magnitude, it could be a periodic function or it could have some other pattern. As another example, the tether length could be varied to compensate for field variations due to orbital eccentricity, the oblateness of the Earth or thermal expansion displacements. Thus the applied acceleration fields might be held constant within tight uncertainty limits. These are only two examples from many that could be given to illustrate the manner in which the space tether concept can be used to provide a controlled gravity environment. In its range of applicability, this is a unique capability. It makes possible controlled gravity operations of great interest, in the same way that controlled magnetic and electric fields opened new vistas a century earlier.

The Panel in joint sessions with the Constellations Panel spent some time reviewing the specific modes in which tether systems can be employed to provide controlled acceleration fields. These fall conveniently into two cases: 1) gravity gradient stabilized configurations and 2) rotating configurations. The equilibrium acceleration field obtained in case 1) for various numbers of bodies and tethers and at different places in the system are given in subsequent sections of this document (Napolitano and Belivacqua; Lundquist).

For time-varying gravity gradient configurations, the control laws, motions and resulting acceleration fields are more complicated but amenable to analysis.
The radial acceleration field produced by a rotating system, as in case 2), is well known. The use of a long tethered system has the advantage that the relative change in acceleration with radial distance can be small (i.e. the field is more uniform across the dimensions of an experiment). Again a time varying tether length is a more involved but tractable situation.

Circumstances in which controlled gravity might be applied usefully are so diverse that the Panel had neither time nor composition to evaluate them in depth. The Panel did hear presentations and received written statements on several applications. The presentation and written materials are tabulated below and reproduced in subsequent parts of this report. Also the Panel as a group discussed other applications. From these considerations some broad observations can be drawn.

**PRESENTATIONS TO THE CONTROLLED GRAVITY PANEL**

<table>
<thead>
<tr>
<th>Name</th>
<th>Topic</th>
</tr>
</thead>
<tbody>
<tr>
<td>Luigi G. Napolitano</td>
<td>Tethered Constellations, Their Utilization as Microgravity Platforms and Relevant Features</td>
</tr>
<tr>
<td>and Franco Bevilacqua</td>
<td></td>
</tr>
<tr>
<td>Charles A. Lundquist</td>
<td>Artificial or Variable Gravity Attained by Tether Systems</td>
</tr>
<tr>
<td>James R. Arnold</td>
<td>Remarks to Controlled Gravity Panel</td>
</tr>
<tr>
<td>Dale A. Fester</td>
<td>Tethered Orbital Refueling Study</td>
</tr>
<tr>
<td>Enrico Lorenzini</td>
<td>Dynamics of Tethered Constellations in Earth Orbit (this appears in the Constellations Panel section)</td>
</tr>
<tr>
<td>Paul A. Penzo</td>
<td>Tethers and Gravity in Space</td>
</tr>
<tr>
<td>R. Monti</td>
<td>Tethered Elevator: A Unique Opportunity for Space Processing</td>
</tr>
<tr>
<td>Kenneth R. Kroll</td>
<td>Gravity Utilization Issues</td>
</tr>
</tbody>
</table>

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Biological response to different fixed magnitudes of gravity or to varying acceleration fields is a topic of significant interest. The organisms of concern range from microscope specimens to man himself. In the range from $10^{-10}$g to $10^{-8}$g, little is known about threshold values for biological phenomena. Measuring these is a fundamental scientific contribution. It also has practical implications for extended space missions such as a manned expedition to Mars. Is some level of artificial gravity necessary or desirable during such a trip? If so, what level is required or optimum? These issues could be explored on tethered platforms in orbit about the earth. If necessary, a mission to Mars could employ a rotating tethered configuration to supply the desired artificial gravity.

Fluid mechanics plays ubiquitous roles in space operations. These range from practical applications, such as propellant handling, to scientific applications, such as separation of organic molecules or living cells. In all these operations, the presence or absence of an acceleration field is a crucial matter. In some instances even a small acceleration field is advantageous, for example to settle propellants in the desired end of a tank. In other circumstances some stringent upper limit of acceleration must be respected, as may be the case in electrophoretic separation of biological materials. In each of these examples, a tether system can be applied beneficially. However, in many cases the optimum acceleration field is just not known. In growing some crystal from a solution, the dominant mass transport mechanism for the depositing material may change from turbulent flow, to laminar flow, to diffusion if the applied acceleration field is reduced over several orders of magnitude. The quality and quantity of the growing crystal presumably changes also, but where is the optimum? How sensitive is the product to noise or other unwanted variation of the field? Do important thresholds exist? Such questions can be answered definitively only if experiments can be done with different controlled acceleration fields. This control is again an appropriate role for a tether mechanism.

The answer to these optimization and threshold questions can have important fiscal implications both for anticipated commercial operations and for facilities such as the Space Station. The imposition of an unnecessarily restrictive
acceleration requirement on the Space Station can be very costly (Arnold, this report). On the other hand, refurbishment to correct for inadequate initial requirements is also costly. Tether systems can not only facilitate answers to these questions, but also they can provide a versatile mechanism for control of the acceleration field at desired positions within the Station.

The tether length to some auxiliary body or bodies can be adjusted to maintain the required environment at the position of a microgravity laboratory module when masses move about the station complex or when masses are added or removed from the station. In addition, active control should provide more precise placement of the acceleration field and allow a vertical distribution of microgravity experiments to be performed sequentially. An artificial intelligence system coupled with acceleration sensors on the station could prescribe continuous adjustment to accomplish these objectives.

The tethered auxiliary body could benefit as well from the greater acceleration field it will experience. This could be the case for a propellant management depot, which could have a fixed, non-zero, gravity field. These gravity control functions are but some of those discussed by the Space Station Panel.

An additional implication of a tether for controlled gravity is the isolation it provides from disturbances. A tether acts as a low frequency bypass filter to lateral disturbances, while work with tether weaves may also provide some damping of disturbances along the tether. This advantage can be achieved by moving the disturbances off the space station or moving the microgravity laboratory off the space station. The later option would minimize the acceleration level seen by the laboratory, but would hamper manned involvement with experiments.

When more complex, or constellation configurations of three or more bodies are examined, controlled gravity is a natural consideration. Perhaps the first example of this class will be an elevator mechanism that attaches to the tether between two primary bodies and carries a third body upward or downward along the tether. The acceleration field in the third body thus can be easily controlled by moving it up or down the tether.
Finally, the Panel noted that the orbital mechanics of tethered systems and the gravity control by them is a rapidly developing discipline for which little standard terminology or notation has evolved. In the interest of more efficient communication, the Panel recommended the nomenclature in the following diagram.

RECOMMENDED TERMINOLOGY

<table>
<thead>
<tr>
<th>Microgravity</th>
<th>$10^{-4}$ g and smaller</th>
<th>$10^{-1}$ g to $10^{-4}$ g</th>
<th>$1$ g</th>
<th>greater than $1$ g</th>
</tr>
</thead>
<tbody>
<tr>
<td>Low Gravity</td>
<td></td>
<td></td>
<td></td>
<td>enhanced gravity</td>
</tr>
<tr>
<td>Earth Gravity</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Hypergravity</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

RECOMMENDATIONS

The Panel was asked to organize its conclusions and recommendations as they pertain to three eras: 1) the Tethered Satellite System period extending through the first few TSS flights, 2) the period of Space Station Initial Orbital Capability embracing its first few years of operation, 3) a post-IOC period when the Space Station becomes mature and facilities are added systematically to it. The recommendations also should include a priority list of tether uses and of economical demonstrations of tether capabilities.

To accommodate this desired reporting format, the Panel prepared the matrix below. Its vertical columns indicate the three eras. The two horizontal divisions represent, respectively, 1) the controlled gravity uses or objectives that the Panel judged to be appropriate for each era and 2) the demonstrations and experiments that would address these objectives.
<table>
<thead>
<tr>
<th><strong>OBJECTIVES</strong></th>
<th><strong>AND USES</strong></th>
<th><strong>DEMONSTRATIONS AND EXPERIMENTS</strong></th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>TSS ERA</strong></td>
<td><strong>Gravity Controlled experimentation in Space Station applied to:</strong></td>
<td><strong>Recommended Opportunities for early demonstrations:</strong></td>
</tr>
<tr>
<td><strong>PRE-IOC</strong></td>
<td><strong>Life Sciences</strong></td>
<td><strong>Spinning Orbiter Mission</strong></td>
</tr>
<tr>
<td></td>
<td><strong>Materials Science</strong></td>
<td><strong>Orbiter experiments during tether missions</strong></td>
</tr>
<tr>
<td></td>
<td><strong>Fluid Science</strong></td>
<td><strong>Elevator on a tether.</strong></td>
</tr>
<tr>
<td><strong>IOC ERA</strong></td>
<td><strong>Fluid Science</strong></td>
<td><strong>Science and application experiments, possibly using TSS deployer</strong></td>
</tr>
<tr>
<td><strong>FOR SPACE STATION</strong></td>
<td><strong>Engineering Uses</strong></td>
<td><strong>Processes and applications.</strong></td>
</tr>
<tr>
<td><strong>POST-IOC ERA</strong></td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td><strong>Fully exploit gravity control in Space missions.</strong></td>
<td></td>
</tr>
</tbody>
</table>
The demonstrations of gravity control during the TSS era are of great importance to future applications. They fall in two general classes: 1) gravity-stabilized tethered systems and 2) rotating systems. These demonstrations deserve more detailed discussion than can be given in the matrix. This can best be done individually for some anticipated missions.

Disposable Deployer Mission, (1987). This mission may allow a measurement of the acceleration field change and particularly the associated acceleration noise at positions in the shuttle while the tether and payload are deployed. Appropriate instrumentation for these measurements needs to be identified and scheduled for the mission.

Spinning Shuttle Mission, (1987-8). This mission provides the first opportunity to begin investigations of controlled gravity and threshold phenomena in the low gravity range \((10^{-1} \text{ to } 10^{-4})\). Although a tether is not involved in this demonstration, the rotation principles for achieving low gravity are the same as for a rotating tethered system. Therefore the mission is included here. The experiment currently planned has attitude control thrusters firing for a 3 hour period; however, the spin may be extended for a longer period for those experiments that are sensitive to thruster firings. Maximum yaw spin rate is planned to be approximately 5 degrees per second. The acceleration level, of course, varies with position in the shuttle. Fluid science and applications are particularly pertinent for this mission. Necessary instrumentation and demonstration equipment should be planned.

TSS-1, (1988)

The first TSS mission provides a fine opportunity to demonstrate and analyze the resulting acceleration field on the Orbiter including the associated acceleration noise, during all phases of tether operations. These measurements should be correlated with other data such as accelerations on the satellite, tether length and tether tension. This mission should provide the necessary
information to extrapolate performance of a tether gravity control system for Space Station.

TSS-2

The controlled gravity experiments on the Orbiter for TSS-1 should be repeated and expanded with the greater deployment length planned for this mission. This mission may provide an opportunity to test an "elevator" that moves along the tether between the Orbiter and the Satellite. Such testing would determine the precision with which the elevator can be placed at a desired gravity level and would help map the acceleration noise resulting from desired gravity level profiles.

KITE

The disturbance isolation aspects of this proposed mission may make it particularly suited to studies of the uncertainties or noise levels that accompany the obtained acceleration fields.

TSS-3

The controlled gravity objectives for this mission would be similar to those for TSS-2, except that improved demonstrations should be expected based on experience with earlier missions.
TETHERED CONSTELLATION, THEIR UTILIZATION AS MICROGRAVITY PLATFORMS AND RELEVANT FEATURES

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Abstract

This paper summarizes the characteristics of the artificial gravity field acting on tethered platforms. The main characteristics of microgravity environments are identified and the improvements of tethered platforms over the classical platform configuration are emphasized. The new microgravity environment gives the possibility of studying a very large number of phenomena offering new potentialities to microgravity sciences.

A simplified analytical investigation is performed to point out the effects of three causes that affect the artificial gravity field, namely: the orbital eccentricity, the tether thermal field and the docking of space vehicles with the main platform. The eccentricity effects are due to the deviation of the tethered system from the ideal nominal circular orbit. A periodical variation of the tether length is induced from the change of tether temperature during each orbit, with a consequent effect on the gravity field. The docking of a space vehicle to the main platform can introduce on the global system of the tethered platforms a dynamical perturbation.

Ultimately, the order of magnitude of these effects are investigated and compared with each other.

1. Characterisation of the gravity field

The space evolution introduced by the Tethered Satellite and represented by the very large constellation of already studied complex tethered platforms cannot forget, as more and more times underlined, a new field of science such as microgravity.

Since the new kind of microgravity environment offered by Tethers is substantially different from the "classical" one, it seems necessary and appropriate at this stage to individuate the characteristics of the gravity field.

Obviously, the first parameter characterizing a gravity field is its level (Fig. 1), ranging, at present, from the ground value \(g/g_m=1\) to \(g/g_m=10\) of the aircraft flying parabolic Klappian orbits, to \(10^{-2}\) for Sounding Rockets, to \(10^{-6}\) of the terrestrial Drop Towers, to \(10^{-2}\) of Spacelab and to \(10^{-7}\) of the Automatic Platforms (Free Flyers). It must be recognized that, apart from the variability around them, these values define a discrete range of gravity levels.

One of the parameters never taken into account is the direction of the "residual" gravity vector; in the following paragraphs the reason of that is clarified.

Once the level and the direction of \(g\) have been considered and hopefully controlled, the time dependence of \(g\) represent further parameters. In particular, the duration and the quality of the chosen \(g\) level and direction must be analyzed, being the quality characterized in terms of persistence of the nominal value throughout the duration and of gravity pollution.

2. Microgravity environments of classical and tethered platforms and importance of \(g\)-variations.

The coming of the tethered platforms has changed the way of thinking about the gravitational conditions obtainable in space; in particular the concept of \(g\)-variations is changed. In fact, the classical platform gravity configuration is characterized by:

- single point nominal \(g\)-value
- unknown direction
- time independent or quasi-steady nominal \(g\)-value
- different \(g\)-quality

All this means that \(g\)-variations are neither considered nor controlled and, in any case, represent disturbing parameters.

On the contrary, tethered platforms allow to look at \(g\)-variations as a system performance and, such as that, they can be continuously controlled. Thus, the main characteristics of tethered platforms microgravity environment are:

- continuous function of nominal \(g\)-values (both in intensity and direction)
- controllability
- \(g\)-quality higher than classical one
- possible time dependent nominal \(g\)-value (both in intensity and direction)

Apart from the quality and controllability effects, the addition of the time dimension appears to be the most important and promising parameters offered by the tether constellations.

The new microgravity environment gives the possibility of studying a very large number of phenomena not yet investigated; an absolutely not complete list of them is reported below in order to give an idea on the possibilities offered by tethers:
- parametric g-value (intensity and direction) investigations in order to obtain a continuous E(g) curve (E represents any experimental parameter)
- imposed and controlled g-level time profiles; a particular case is represented by a periodic, both in intensity or direction, function of g(t), in order to study the effects of frequency and amplitude
- analysis of the g-jitters by simulating them; up to now g-jitters have been only measured
- effects of g-intermittencies or, in general, effects at g(t) step functions
- effects of g(t) hysteretic on different phenomena
- controllability of g-noise

3. New potentialities offered by tethers to microgravity sciences

The potentialities presented in the last paragraph are self-explanatory and the importance of them with respect to the different field of science should be self-evident. However, it is interesting to enter explicitly the three main fields of science involved with microgravity conditions: Life Sciences, Material Sciences, Fluid Sciences. For each of them it is easily possible to individuate a number of typical examples of user's needs:

- Life Sciences
  - Determination of threshold g values for biological processes
- Material Sciences
  - determination of the level-frequency acceptability regions for crystal growth processes
  - solidification front geometry any dynamics as function of g(t)
- Fluid Sciences
  - g-jitters
  - contact angle hysteresis
  - dynamic wetting
  - spreading
  - influence of g-history on critical point phenomena
  - stability enhancing by means of time variation of g-levels

The influence of a g-variation capability on processes is also important, for example, for the optimization of the process itself by means of the so-called g-tuning.

4. Main performances and Characteristics of a tethered platform

During our study on this argument we convinced ourselves on the opportunity to concentrate our effort on the dynamics issues related to these off-standard scientific platforms instead to distribute our attention on different aspects like configuration, architecture and mission, in order to clearly identify the main characteristics of this attractive microgravitational solution before to approach more general aspects.

It is clear that a tethered platform exhibits a net acceleration proportional to the distance from the center of gravity of the global tethered space system and vertically oriented when in stationary stabilised conditions.

This net acceleration opposed by the tether tension can be viewed as an "artificial gravity" that, at the end of a static vertical tether, can be tuned at different values by controlling the tether length: L i.e.:

$$\frac{g}{g_0} = \frac{2}{(R_0 + H)^3} \cdot L$$

where:
- g/g_0: artificial gravity referred to Earth Surface gravity
- R: Earth Surface Radius
- H: Altitude of Tethered System Center of gravity

In the Table 1 a preliminary evaluation on artificial gravity levels offered by a tethered platform for different altitudes and tether lengths is shown:

Tab. 1 - Artificial Gravity as function of altitude and tether length

<table>
<thead>
<tr>
<th>Altitude: H (km)</th>
<th>Artificial Gravity: g/g_0</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>L_min = 100 m</td>
</tr>
<tr>
<td>463</td>
<td>3.81 10^{-5}</td>
</tr>
<tr>
<td>1,000</td>
<td>3.04 10^{-6}</td>
</tr>
<tr>
<td>10,000</td>
<td>2.78 10^{-7}</td>
</tr>
<tr>
<td>35,786</td>
<td>1.63 10^1</td>
</tr>
</tbody>
</table>

In particular, limiting our attention on low orbit, we can evidenciate that the micro gravity performances offered by tethers cover all the range between Automatic Platforms and Aircraft performances.

In Fig. 1 we have shown three scales, relevant to low orbit (H = 463 km), medium orbit (H = 10,000 km) and geostationary orbit (H = 35,786 km), relating the tether length to the obtained artificial gravity levels.

It is important to say that the possibility to modify the artificial gravity level by modifying and controlling the tether length, unavoidably induces disturbing accelerations effects due to a quite complex orbital transient dynamics.

So an imposed and controlled g-level time profile is to be considered taking into account this transient disturbing effects.

Another important aspect affecting a tethered platform performance is the g-noise induced by different perturbing reasons like residual orbital eccentricity of the tethered system, thermal behaviours inducing tether length variation, rendez-vous and docking manoeuvres of the main station inducing dynamic perturbation on the tethered platforms. These different aspects will be analysed in a preliminary approach in the next paragraphs.
The dynamics model

Since the objective of this paper was to outline some aspects of microgravity environment, the analysis was based on a rather simplified dynamic model of the system.

The most significant simplifications were the omission of lateral tether dynamics and the use of only one normal mode for the elastic expansion of the tether.

The tether was assumed to have a constant diameter of 2.3 mm and uniform mass distribution per unit length.

The microgravity platform was assumed to have a mass of 10 ton.

From Lagrange's theory the stretch equation can be expressed in the following form:

\[ \frac{M}{m} \frac{d^2 \ell}{dt^2} = \frac{1}{3} \left( M_0 \frac{d^2 \ell}{dt^2} \right) + \frac{M}{m} \left( \frac{1}{2} \frac{d \ell}{dt} \right)^2 + \frac{m}{M} \left( \frac{1}{2} \frac{d \ell}{dt} \right)^2 + \frac{1}{2} \frac{d \ell}{dt} \left( 3 \cos \theta \cos \phi \right) \]

where the two Euler angles \( \theta \) and \( \phi \) describe the platform motion, \( \theta \) and \( m \) are the platform and the tether masses, \( Z \) is the tether elongation, \( L \) the unstrained tether length and \( L \) the tether length. \( \frac{d \ell}{dt} \) represents the angular velocity of orbital reference frame.

In this equation as generalized forces were assumed only first order gravity gradient field and elastic tether force. Aerodynamic forces were neglected.

The energy dissipation due to frictional losses in the tether material is in general small, and the damping was assumed to be null.

5.1 The dynamic effect of the thermal environment

The effect of the thermal field generated along the tether is one of the most interesting parameter to be considered in order to investigate the dynamic behaviour of a system compound by two bodies connected to this tether.

The main parameters which affect the tether temperature are the following:

- Solar Radiation
- Albedo
- Infrared Radiation
- Aerodynamic Heating

At the orbital altitudes that are interesting for the analysis of the microgravity phenomena, the effect of the atmospheric heating is negligible, therefore it has not been introduced in this analysis. The simulations considered during these preliminary thermal analysis have been performed assuming a tether default length of \( L = 100 \text{ km} \) (measured at a temperature of \( 20^\circ \text{C} \)) and placing the tether in a circular orbit where its center of mass altitude, with respect to the earth surface, is of 400 km.

A trade off about two different tether materials has been considered:
- 302 Stainless Steel
- Kevlar 29

Table 2 shows the main properties of the two tethers considered for the calculations.

<table>
<thead>
<tr>
<th>Tether Material</th>
<th>Configuration</th>
<th>Diameter</th>
<th>Density</th>
<th>Absorptivity</th>
<th>Emissivity</th>
</tr>
</thead>
<tbody>
<tr>
<td>302 Stainless Steel</td>
<td>1x19 Standed Bare braided Wire Rope (no Jacket)</td>
<td>0.89 mm</td>
<td>4.03 Kg/Km</td>
<td>0.44</td>
<td>0.12</td>
</tr>
<tr>
<td>Kevlar 29</td>
<td></td>
<td>2.00 mm</td>
<td>4.00 Kg/Km</td>
<td>0.44</td>
<td>0.83</td>
</tr>
</tbody>
</table>

A thermal mathematical model has been developed in which the 100 Km tether has been subdivided in 100 nodes. The energy balance equations have been solved using the SINDA thermal analyzer.

The analyses have been conducted considering the two extreme orbital conditions under a thermal point of view, as shown in Fig. 2.

A particular subroutine was improved to exactly simulate the twilight effect during the tether entry and exit from the earth shadow. With the knowledge of the temperature behaviour of all tether nodes during one orbit, it is possible to quantify the tether total expansion/contraction and the relevant velocities and accelerations with the hypotheses of considering a completely free tether.

The results obtained during the above mentioned analyses can be summarized as following:

- the maximum thermal gradient between the two tethers ends both for the stainless steel and for the kevlar is always lower than 15°C, during all the orbital phases
- the tether average temperature behaviour as function of the orbit time is shown in Fig. 3 for all the analyzed cases
- the tether length variation, the relevant velocities and accelerations are respectively shown in Figs 4, 5 and 6.

The analysis of the previous results shows the following conclusions:

- the maximum tether length variation during one orbit due to thermal loads variation is of approximately 300 meters for the stainless steel tether and of 25 meters for the kevlar tether;
- the maximum speed corresponding to the above variation is of approximately 0.5 m/s for the stainless steel and of 0.04 m/s for the kevlar;
- the maximum acceleration impulse obtained during the simulation is of 0.015 m/s² (1.5x10⁻⁶ g) for the stainless steel and of 0.008 m/s² (0.8x10⁻³ g) for the kevlar.

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To analyse the effective dynamic response of the system to thermal field generated by entry and exit from the earth shadow the eq. /1/ was used.

As additional simplifications the tether mass was neglected and the assumption of null in-plane and out-of-plane librations was made.

The system orbit was circular with semi-major axis $a = 6778 \text{ km}$ and the unstretched tether length (at a temperature of $20^\circ \text{C}$) was assumed $L = 100 \text{ km}$.

The basic elastic properties of two tether materials were considered.

For Kevlar 29 a spring constant $K = 5.55 \text{ N/m}$ was considered with basic mode frequency $f_0 = 3.75 \times 10^3 \text{ Hz}$.

For 302 Stainless steel a spring constant $K = 8.78 \text{ N/m}$ was found with natural frequency $f_s = 4.72 \times 10^3 \text{ Hz}$.

The system was assumed stretched but in equilibrium as initial condition.

The tether thermal behaviour (described in the previous par.) was applied to the system, and the dynamic response was found by numerical integration of eq. /1/.

The fig.'s 7 and 8 show the tether elongation and the dynamic radial acceleration for the Kevlar and Stainless materials and for the two beta values of 0 and 32 degrees.

For the Kevlar tether the equilibrium elongation results of about 697 m.

The thermal environment causes elongation oscillations of about 4 m peak to peak amplitude over one orbital period.

The global acceleration disturbance results of about $1.3 \times 10^{-3} \text{ m/s}^2$.

The Stainless-tether presents an equilibrium elongation of about 440 m. The thermal transient induces elongation oscillations of about 30 m amplitude during one orbit. The acceleration disturbance results of about $2.5 \times 10^{-3} \text{ m/s}^2$.

The stainless material induces perturbations of one order of magnitude greater than the Kevlar one.

Kevlar seems suitable material for micro-gravitational environment.

5.2 The dynamic effect of orbital eccentricity

To evaluate the microgravity disturbances due to small eccentricity of the system orbit the eq. /1/ was used.

As additional simplification the tether mass was neglected and the assumption of null in-plane and out-of-plane librations was made. In addition the elastic properties of the tether were neglected because this kind of disturbances is not expected to excite the elastic expansion mode of the tether.

The orbit semi-major axis was fixed at 6778 km and the orbital eccentricity was varied from $3 \times 10^{-5}$ to $15 \times 10^{-5}$.

The fig. 9 shows the orbital radius, the angular velocity and the radial acceleration in function of the true anomaly for five values of orbital eccentricity.

The gravity gradient acceleration relevant to a tether length $L = 100 \text{ km}$ for circular orbit is $0.384 \text{ m/s}^2$. Small orbit eccentricities cause a disturbance of orbital periodicity and amplitude function of eccentricity. For a typical circular error of about $5 \times 10^{-4}$ the disturbance results of about $1.5 \times 10^{-4} \text{ m/s}^2$ peak to peak amplitude.

5.3 The dynamic effects of docking

This section is devoted to give a preliminary assessment of the $g$-variations induced by a docking manoeuvre on a tethered platform. The simplified model, adopted to represent the system dynamics, considers the motion of the subsatellite as unidimensional along the z-axis of the tether. Both the geometrical and structural characteristics of the system components (namely, subsatellite, tether and upper platform) were assumed according to the definitions given in the previous sections; here, an additional system component (i.e. the shuttle) is considered to model the docking manoeuvre with the upper platform.

Basically, the effect of a docking manoeuvre on the subsatellite acceleration levels is twofold; one is a short-term effect representing the subsatellite dynamic response to an external impulse due to the docking and the other is a long-term effect due to the change of the overall system centre of mass.

The first effect was assessed by considering the target (that is, upper platform, tether and subsatellite) to be in a circular orbit with its centre of mass at 6778 km altitude, and the shuttle approximating to the upper platform with relative velocity along the z-axis.

By assuming a mass ratio $N/m = 100$ between the upper platform and the subsatellite, 100 km for the tether length (in Kevlar 29) whose longitudinal stiffness was previously estimated as $K = 5.55 \text{ N/m}$, and the worst case of impact in the range of the allowable conditions for the rendezvous and docking manoeuvre, the maximum variation of acceleration induced on the microgravity platform was about $1 \times 10^{-4} \text{ m/s}^2$. That is, the $0.15 \text{ m/s}^2$ of acceleration induced on the upper platform were damped via the tether flexibility until the above mentioned small value at the lower platform.

The long term effect arises because, when the shuttle docks with the upper platform, the overall system will change. In conditions of soft impact the velocities of the various parts of the composite system will all be the same as immediately before the docking, while the center of mass will be different and so the orbit of the new centre of mass. Energy and angular momentum preservation allow for calculating both the new semi-major axis and eccentricity of the orbit. Assuming that the velocity of the new centre of mass is greater than the local circular velocity, the composite system will be at the perigee of the new orbit immediately after the docking and so the maximum (negative) variation of acceleration on the microgravity will result after an orbital semiperiod. With the assumptions of the above simplified model, the variation of the centre of mass is restricted to a few meters along the negative z-axis and so negligible $g$-variations as resulting from the application of Eqns. /1/.

Thus, the $g$-variations induced by the
Conclusions

Tethered platforms provide a unique multi-disciplinary facility for conducting research on microgravity sciences.

The potentialities offered by a tethered platform are clearly represented in Fig. 1 in which a comparison between artificial microgravity performances offered by different solutions as Aircraft, Rockets, Spacelab, Drop Towers, Automatic Platforms and a Tethered System, evidence its advantages in capability to cover an extended microgravity range: \( 10^{-6} \leq g/g_0 \leq 10^{-2} \) for an indefinite time. The capability to perform a desired g-level time profile, acting on tether length with a suitable control law able to minimize transient disturbing effects, represents an important feature.

The results obtained by a preliminary analysis on g-noise induced by different perturbing reasons like residual orbital eccentricity, tether length thermal modification and docking induced dynamic effects are reasonably acceptable.

In particular, for a low orbit (\( H = 400 \) km) and considering a tether length of 100 km, the microgravity disturbances due to orbital eccentricity ranging between: \( 3 \times 10^{-3} \leq e \leq 15 \times 10^{-3} \) is limited to: \( 4 \times 10^{-8} \leq g \leq 2 \times 10^{-7} \) g i.e. from \( 1\% \) to \( 2\% \) of artificial gravity value: \( g/g_0 = 3.8 \times 10^{-2} \).

The dynamic effects induced by tether length variation as a function of temperature behaviour are essentially concentrated in the two sun-eclipse transitions per orbit in which the temperature presents a derivative discontinuity. Two different tether materials have been considered: Stainless Steel and Kevlar having a coefficient of thermal expansion of \( 2 \times 10^{-6} \) \(^{\circ}\)C and \( -2.5 \times 10^{-5} \) \(^{\circ}\)C respectively.

The global acceleration disturbance on a 100 km tethered platform in low orbit, as deduced by a simplified model neglecting damping effects, has been \( \pm 2.5 \times 10^{-7} \) g for stainless steel tether and \( \pm 1.3 \times 10^{-7} \) g for Kevlar tether i.e. of the order of \( 6\% \) and \( 0.3\% \) of artificial gravity respectively. Kevlar seems a suitable material for microgravity tethered platforms.

The g-variation induced by a docking manoeuvre at the upper platform, assuming a mass ratio of 100 between this platform and the sub-satellite, 100 km of tether length, is of the order of \( 1 \times 10^{-8} \) g, i.e. less than \( 1\% \) of artificial gravity. This perturbation can be considered negligible with respect to the others, taking also into account the singularity of this event.
FIG. 1 NOMINAL GRAVITATIONAL LEVELS AS A FUNCTION OF DURATION
ACHIEVABLE WITH THE MAIN AVAILABLE MICROGRAVITY PLATFORMS COMPARED WITH TETHERED PLATFORMS.

FIG. 2 ORBITAL CONDITIONS FOR TETHER THERMAL ANALYSIS
FIG. 3 TETHERS AVERAGE TEMPERATURE DURING AN ORBIT PERIOD
FIG. 4 TETHERS LENGTH VARIATION DUE TO TEMPERATURE
FIG. 5 TETHERS SPEED DUE TO TEMPERATURE VARIATIONS
AERITALIA-SETTORE SPAZIO

FIG. 6 TETHERS ACCELERATIONS DUE TO TEMPERATURE VARIATIONS
FIG. 7 TETHERS' ELONGATION DUE TO THE EFFECTIVE DYNAMIC RESPONSE OF THE SYSTEM
FIG. 8 TETHERS RADIAL ACCELERATION DUE TO THE EFFECTIVE DYNAMIC RESPONSE OF THE SYSTEM
FIG. 9 RADIAL ACCELERATION, ORBITAL RADIUS AND ORBITAL ANGULAR RATE DUE TO DIFFERENT RESIDUAL ECCENTRICITIES
I. MOTIVATION

The simplest orbiting tethered system demands for stability that the mass centers of two end bodies be displaced above and below the position of zero acceleration. Therefore, the contents of the end bodies are subjected necessarily to acceleration fields or "artificial gravity" whose magnitudes depend on the dimensions and masses of the system. If the length of the tether changes, so do the fields. Even for a fixed tether length, the acceleration field at a location in the system may be somewhat variable unless special means are employed to maintain a constant value.

These fundamental properties of a tethered system can be used to advantage if small or variable acceleration fields are desired for experimental or operational reasons. This potential use involves a few expressions from a formulation of tether system dynamics. Some of these formulae have been collected here for convenient reference.

A special application of acceleration field control using a tether system is attainment of near-zero gravity. In this application, even small variations about zero become a critical matter.

II. THE TWO BODY EQUILIBRIUM CASE

The most rudimentary model of an equilibrium tethered system assumes that a body of mass, \( m_2 \), is connected to another body of mass, \( m_3 \), by a tether of negligible mass oriented along a geocentric radius, (See figure 1). As shown in Figure 1, \( Q \) is the geocentric distance to the center of mass of \( m_2 \) and \( m_3 \), and \( S \) is the tether length between \( m_2 \) and \( m_3 \). Further let \( G \) be the fundamental gravitational constant, \( m \), the mass of the Earth, and \( m = m_2 + m_3 \). The Earth is treated as a point mass, and the orbit of the tethered system is assumed to be circular. It is easily shown, for this simplistic case, that the orbital angular rate, \( \omega \), is given by

\[
\omega^2 = \frac{Gm}{Q^3} \left\{ \frac{m_2}{m} \left[ 1 - \frac{m_3}{m} \left( \frac{S}{Q} \right) \right]^{-2} + \frac{m_3}{m} \left[ 1 + \frac{m_2}{m} \left( \frac{S}{Q} \right) \right]^{-2} \right\}
\] (2.1)

For analytical treatments of tether dynamics, the use of \( \frac{S}{Q} \) as a small

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parameter for series expansions is useful. To second order in this small quantity, equation (2.1) can be rewritten approximately as

\[ \omega^2 = \frac{Gm_1}{Q^3} \left\{ 1 + 3 \frac{m_2 m_3}{m^2} \left( \frac{S}{Q} \right)^2 \right\} \] (2.2)

Likewise the tension is

\[ \tau = \frac{Gm_1 m_2 m_3}{mQ^2} \left\{ \left[ 1 - \frac{m_3}{m} \left( \frac{S}{Q} \right) \right] - \frac{3}{m} \left( \frac{m_3 - m_2}{m} \right) \right\} \]

\[ - \left[ 1 + \frac{m_2}{m} \left( \frac{S}{Q} \right) \right] \left[ 1 - \frac{m_3}{m} \left( \frac{S}{Q} \right) \right] \] (2.3)

To second order in \( \left( \frac{S}{Q} \right) \) this can be written

\[ \tau = \frac{Gm_1 m_2 m_3}{mQ^2} \left\{ 3 \left( \frac{S}{Q} \right) + 3 \frac{m_3 - m_2}{m} \left( \frac{S}{Q} \right)^2 \right\} \] (2.4)

The corresponding radial acceleration fields to second order are

\[ \gamma_2 = -\frac{Gm_1}{Q^2} \frac{m_3}{m} \left[ 3 \left( \frac{S}{Q} \right) + 3 \frac{m_3 - m_2}{m} \left( \frac{S}{Q} \right)^2 \right] \] (2.5)

\[ \gamma_3 = \frac{Gm_1}{Q^2} \frac{m_2}{m} \left[ 3 \left( \frac{S}{Q} \right) + 3 \frac{m_3 - m_2}{m} \left( \frac{S}{Q} \right)^2 \right] \] (2.6)

where the positive sense is radially outward. These are the fields \( \gamma_i \) sensed by an experiment at the body centers of mass respectively and in a coordinate system rotating with the orbit of the system.

An orbiting point mass with the same angular rate as equation (2.1), or its approximation, equation (2.2) would have a radial distance \( \bar{Q} \) given by

\[ \omega^2 = \frac{Gm_1}{Q^3} \text{ or } \bar{Q}^3 = \frac{Gm_1}{\omega^2} \] (2.7)

The radius \( \bar{Q} \) is in some sense a "center of motion" for the tether system. It is related to the center of mass by the expression
\[
\frac{1}{\bar{Q}^3} = \frac{1}{Q^3} \left\{ \frac{m_2}{m} \left[ 1 - \frac{m_3}{m} \left( \frac{S}{Q} \right)^2 \right] + \frac{m_3}{m} \left[ 1 + \frac{m_2}{m} \left( \frac{S}{Q} \right)^2 \right] \right\} \quad (2.8)
\]

or approximately by

\[
\bar{Q} = Q \left\{ 1 - \frac{m_2 m_3}{m} \left( \frac{S}{Q} \right)^2 \right\} \quad (2.9)
\]

The \( \bar{Q} \) also differs from the center of gravity of this simplistic tether system.

The center of gravity is defined as the radius, \( \tilde{Q} \), at which a single body of mass \( m \) would be subject to the total gravitational force on bodies \( m_2 \) and \( m_3 \),

\[
\frac{m}{\tilde{Q}^2} = \frac{m_2}{r_2^2} + \frac{m_3}{r_3^2} \quad (2.10)
\]

The center of gravity, \( \tilde{Q} \), to second order is

\[
\tilde{Q} = Q \left\{ 1 - \frac{3}{2} \frac{m_2 m_3}{m} \left( \frac{S}{Q} \right)^2 \right\} = \bar{Q} \left\{ 1 - \frac{1}{2} \frac{m_2 m_3}{m} \left( \frac{S}{Q} \right)^2 \right\} \quad (2.11)
\]

The three centers are also related by

\[
\bar{Q}^3 = Q \tilde{Q}^2 \quad (2.12)
\]

The pertinence of \( \bar{Q} \) is its role as the position at which acceleration is zero for the angular rate from equation (2.1) or (2.2). Acceleration is not zero at the system center of mass or the center of gravity.

III. TETHER WITH SIGNIFICANT MASS

If the mass of the tether itself, \( m_T \), is significant relative to the mass of the two end bodies, then the expressions of Section II must be modified. For a tether of uniform mass density, the orbital rate for the equilibrium configuration is given by

\[
\omega^2 = \frac{Gm_1}{Qm} \left[ \frac{1}{r_2^2} m_2 + \frac{1}{r_3^2} m_3 + \frac{1}{r_T^2} m_T \right] \quad (3.1)
\]

where the total mass is

\[
m = m_2 + m_3 + m_T
\]
and the center of mass, $Q$, is

$$Q = \frac{m_2}{m} r_2 + \frac{m_3}{m} r_3 + \frac{m_T}{m} \left( \frac{r_2 + r_3}{2} \right)$$

The last term in the equation for $\omega^2$ corresponds to the gravitational force on the tether between bodies 2 and 3. Thus, the center of gravity, $\bar{Q}$, for the system is given by

$$m \frac{Q}{Q^2} = \frac{m_2}{r_2^2} + \frac{m_3}{r_3^2} + \frac{m_T}{r_2 r_3} \quad (3.2)$$

and

$$\omega^2 = \frac{G m_1}{Q^2} = \frac{G m_1}{Q^3} \quad (3.3)$$

Equation 3.3 has the same form as 2.7.

To the second order in $\left( \frac{S}{Q} \right)$, equation 3.1 becomes

$$\omega^2 = \frac{G m_1}{Q^3} \left[ 1 + \left\{ 3 \frac{m_2 m_3}{m^2} + \frac{m_T}{m} \left( \frac{m_2}{m} + \frac{m_3}{m} \right) \right\} \left( \frac{S}{Q} \right)^2 \right] \quad (3.4)$$

Correspondingly, the position of zero acceleration is

$$\bar{Q} = Q \left[ 1 - \left\{ \frac{m_2 m_3}{m^2} + \frac{m_T}{3m} \left( \frac{m_2}{m} + \frac{m_3}{m} \right) \right\} \left( \frac{S}{Q} \right)^2 \right] \quad (3.5)$$

Likewise, the tensions on body 2 and body 3 and the acceleration fields at their centers of mass are, respectively

$$\tau_2 = - m_2 y_2 = \frac{G m_1 m_2}{Q^2} \left\{ 3 \left[ \frac{m_3}{m} + \frac{m_3}{2m} \right] \left( \frac{S}{Q} \right) + \left[ 3 \frac{m_3 m_3}{m m} + \frac{m_T}{m} \left( \frac{m_3}{m} - \frac{m_2}{m} \right) + \frac{m_T}{m} \left( \frac{m_3}{m} + \frac{m_T}{2m} \right) \right] \left( \frac{S}{Q} \right)^2 \right\} \quad (3.6)$$
\[ -T_3 = m_3 \gamma_3 = \frac{G m_1 m_2}{Q^2} \left\{ \frac{m_2}{m} + \frac{m_1}{2m} \right\} \left( \frac{S^2}{Q} \right) + \]
\[ \left[ 3 \frac{m_2}{m} \left( \frac{m_3 - m_2}{m} \right) + \frac{m_1}{m} \left( \frac{m_3 - m_2}{m} \right) - \frac{m_1(m_2 + m_1)}{2m} \right] \left( \frac{S^2}{Q} \right) \]  

(3.7)

IV. THREE AND MORE TETHERED BODIES

A radial configuration of three bodies connected by two tethers is the first constellation system of interest for its resulting acceleration fields. As a special case, the middle body can be put at the position of zero acceleration.

For the three body case, let \( m_2 \) be the mass of the body closest to the Earth, \( m_3 \) be the middle body and \( m_4 \) be farthest from the Earth. The radial distances are \( r_2, r_3, r_4 \), respectively. Also for uniform linear mass densities, denote by \( m_{23} \) the total tether mass between bodies 2 and 3, and likewise use \( m_{34} \) for the tether between bodies 3 and 4. The tether tension pulling on body 2 due to the tether to body 3 will be denoted by \( \tau_{23} \). Similarly, the tension at body 3 due to the tether to body 2 is \( \tau_{32} \). By the same convention, \( \tau_{34} \) also acts on body 3 and \( \tau_{43} \) on body 4. Figure 4.1 illustrates these notations.

For the case in which the bodies execute circular orbits and the tethers lie along a geocentric radius, the force equilibria are specified by the equations below. Equation 4.1 pertains to body 2, Equation 4.2 to the tether between 2 and 3 etc.

\[ \tau_{23} + m_2 r_2 \omega^2 - \frac{G m_1 m_2}{r_2^2} = 0 \]  

(4.1)

\[ - \tau_{23} + \tau_{32} + m_3 r_3 \omega^2 - \frac{G m_1 m_2}{r_2 r_3} = 0 \]  

(4.2)

\[ - \tau_{32} + \tau_{34} + m_3 r_3 \omega^2 - \frac{G m_1 m_3}{r_3^2} = 0 \]  

(4.3)

\[ - \tau_{34} + \tau_{43} + m_3 r_4 \omega^2 - \frac{G m_1 m_4}{r_3 r_4} = 0 \]  

(4.4)

\[ - \tau_{43} + m_4 r_4 \omega^2 - \frac{G m_1 m_4}{r_4^2} = 0 \]  

(4.5)

These five equations have five unknowns, namely \( \omega^2, \tau_{23}, \tau_{32}, \tau_{34}, \tau_{43} \), where the radii and masses are considered as given.
Adding Equations (4.1) through (4.5) gives the solution for \( \omega^2 \)

\[
\omega^2 = \frac{Gm_1}{QQ^2} = \frac{Gm_1}{Q^3} \tag{4.6}
\]

where

\[
mQ = m_2 r_2 + m_23 \left( \frac{r_2 + r_3}{2} \right) + m_3 r_3 + m_34 \left( \frac{r_3 + r_4}{2} \right) + m_4 r_4 \tag{4.7}
\]

\[
\frac{m}{Q^2} = \frac{m_2}{r_2^2} + \frac{m_23}{r_2 r_3} + \frac{m_3}{r_3^2} + \frac{m_34}{r_3 r_4} + \frac{m_4}{r_4^2} \tag{4.8}
\]

\[
m = m_2 + m_23 + m_3 + m_34 + m_4 \tag{4.9}
\]

Equation 4.6 has the same form as 2.7 and 3.3. In fact, it is clear from the derivation that the same result can be generalized directly to any number of bodies and uniform density tethers in a radial linear configuration in circular orbits.

Using Equation 4.6, the tensions are immediately derived from 4.1 through 4.6. The acceleration fields at the center of mass of each body likewise follow immediately.

\[
\gamma_2 = -\frac{\tau_{23}}{m_2} = r_2 \omega^2 - \frac{Gm_1}{r_2^2} \tag{4.10}
\]

\[
\gamma_3 = \frac{\tau_{34}}{m_3} = r_3 \omega^2 - \frac{Gm_1}{r_3^2} \tag{4.11}
\]

\[
\gamma_4 = \frac{\tau_{43}}{m_4} = r_4 \omega^2 - \frac{Gm_1}{r_4^2} \tag{4.12}
\]

If body 3 is to be positioned at the point of zero acceleration (i.e., \( \gamma_3 = 0 \)) then as expected

\[
r_3^3 = \bar{Q}^3 = \frac{Gm_1}{\omega^2} \tag{4.13}
\]

But \( \omega^2 \) is also a function of \( r_3 \), and therefore Equation 4.13 must be solved for \( r_3 \). A cubic equation in \( r_3 \) results which can be solved analytically or numerically.

However, if the two tethers have the same linear mass density, the case reduces to that of Section 3. This can be seen intuitively because any third mass can be attached to the tether at the zero acceleration point between two
bodies without influencing the tension. The same result follows analytically from equations 4.1 through 4.5 using the uniform density condition,

$$\frac{m_{33}}{r_3 - r_2} = \frac{m_{34}}{r_4 - r_3}$$  \hspace{1cm} (4.14)

and the condition for zero acceleration at body 3,

$$-T_{32} + T_{34} = 0$$  \hspace{1cm} (4.15)

Thus, in this case, Equation 3.5 can be written to second order,

$$r_3 = \bar{Q} = Q\left[1 + \left\{ \frac{m_2 m_4}{m} + \frac{m_{24} (m_2 - m_4)}{3m} \right\} \left( \frac{S}{Q} \right)^2 \right]$$  \hspace{1cm} (4.16)

where

$$m = m_2 + m_{24} + m_4$$  \hspace{1cm} (4.17)

$$mQ = m_2 r_2 + m_{24} \left( \frac{r_2 + r_4}{2} \right) + m_4 r_4$$  \hspace{1cm} (4.18)
REMARKS TO THE CONTROLLED GRAVITY PANEL
James R. Arnold

The necessary level of acceleration for materials studies (microgravity) on the space station or other work platform in LEO is not now well defined. Some suggestions have placed this level as low as $10^{-7}$, $10^{-8}$ or even $10^{-9}$ g.

Discussions yesterday made it clear that such levels can only be achieved if many subtle second-order and third-order effects are controlled.

My colleagues in the materials field, and especially just those persons most active in experimental programs, have convinced me of one basic point:

"The level of microgravity must not be allowed to be the cost driver for the first facilities put into use".

What should be done is to achieve what can be done with the use of tethers and intelligent design, but not to attempt highly complex and difficult technologies beyond that point. I have the impression (perhaps wrong) that accelerations on the order of $10^{-5}$ g, or even perhaps better, can be achieved in this way. This will already allow a rich field of studies in materials science and related fields.

Venezia, 16 October, 1985
TETHERED ORBITAL REFUELING STUDY

PRESENTED BY

DALE A. FESTER
MARTIN MARIETTA DENVER AEROSPACE
DENVER, COLORADO

PRESENTED TO
APPLICATIONS OF TETHERS IN SPACE WORKSHOP
VENICE, ITALY/OCTOBER 15-17, 1985
PROGRAM OVERVIEW

PROGRAM TITLE: TETHERED ORBITAL REFUELING STUDY

CONTRACT: NAS9-17059

PROGRAM MANAGER: DALE FESTER (303) 977-8699

CUSTOMER: NASA-JSC
KENNETH R. KROLL, TECHNICAL MONITOR

PROGRAM OBJECTIVES: EVALUATE THE FEASIBILITY AND LIMITATIONS OF FLUID ACQUISITION AND TRANSFER UNDER AN ACCELERATION INDUCED IN A TETHERED ORBITAL REFUELING FACILITY AND PROVIDE CONCEPTUAL DESIGNS

PERIOD OF PERFORMANCE: NOVEMBER 1983 TO AUGUST 1985
PROGRAM TASKS

0 RECOMMEND THE FLUID TRANSFER METHOD AND PARAMETERS

0 EVALUATE DISTURBANCES, FLUID MOTION, AND DAMPING

  - ESTABLISH NECESSARY FACILITY CONFIGURATION DETAILS
  - DETERMINE TYPE, RELATIVE MAGNITUDE, AND SOURCES OF DISTURBANCES
  - DEVELOP DAMPING CRITERIA FOR EACH TYPE OF FLUID MOTION
  - DETERMINE ENVELOPE OF OPERATION IMPOSED BY THE DAMPING CRITERIA

0 SELECT PASSIVE DEVICES TO AUGMENT INHERENT FLUID DAMPING AND DETERMINE THE RESULTANT ENVELOPE OF OPERATION

0 ASSESS FACILITY IMPACTS ON SPACE STATION AND OTV DESIGN REQUIREMENTS

0 ASSESS THE EFFECT OF TETHER LENGTH ON HAZARDS ASSOCIATED WITH TANK OVERPRESSURE EXPLOSION AND CONTAMINATION DUE TO PROPELLANT LEAKAGE OR VENTING

0 IDENTIFY GROUND AND FLIGHT TESTS NECESSARY TO PROVE THE TETHERED ORBITAL REFUELING CONCEPT
STUDY LOGIC FLOW

START

FLUID TRANSFER ANALYSIS

FACILITY DETAILING

SYSTEM IMPACT ASSESSMENT

DISTURBANCE DEFINITIONS

INHERENT DAMPING ANALYSIS

AUGMENTED DAMPING ANALYSIS

HAZARDS ANALYSES

TESTING RECOMMENDATIONS

END
WORK STATEMENT GROUNDRULES

0 3 TETHER CASES
- STATIC, VERTICAL TETHER WHERE MOTION IS DUE TO FLUID MOTION ONLY
- GENERAL PENDULUM MOTION THROUGH A FIXED ANGLE EITHER ALONG OR PERPENDICULAR TO THE ORBITAL PLANE

0 FACILITY C.G. IS MAINTAINED ALONG THE TETHER AXIS

0 PROPELLANTS: L02/LH2: 100,000 LBM STORAGE AND 45,000 LBM TRANSFERRED
N2O4/MMH AND N2H4: CONSIDER ONLY IN A CURSORY SENSE

0 INDIVIDUAL TANKS ARE 14 FEET IN DIAMETER OR LESS AND 90%, 50% OR 10% FULL

0 TRANSFER METHODS: PRESSURE, PUMP, OR GRAVITY FEED

0 THE SPACE STATION, REFUELING FACILITY AND PROPULSION STAGE ARE LOCATED IN A NOMINAL ORBIT OF 250 NAUTICAL MILES
BOND NUMBER MUST BE OVER 50; THUS:

\[ L \geq \frac{4 \, B_0 \, \sigma}{1.16 \times 10^{-7} \, \rho \, B^2} \]

<table>
<thead>
<tr>
<th>PROPELLANT</th>
<th>( L, \text{ FT} )</th>
<th>ACCELERATION, ( \text{g} )</th>
</tr>
</thead>
<tbody>
<tr>
<td>LO2</td>
<td>120</td>
<td>( 1.4 \times 10^{-5} )</td>
</tr>
<tr>
<td>LH2</td>
<td>280</td>
<td>( 3.2 \times 10^{-5} )</td>
</tr>
</tbody>
</table>
REQUIRED TETHER LENGTH WAS FOUND BY EQUATING LINE PRESSURE DROP TO GRAVITY HYDROSTATIC HEAD.

LINE PRESSURE DROP IS BASED ON FANNING EQUATION:
- ASSUMES NOMINAL 30 FT LINE LENGTH
- NEGLECTS VALVE AND FILTER PRESSURE DROPS

![Graph showing minimum distance vs. feedline diameter for different times.](image)
# FLUID TRANSFER METHOD SELECTION

## TANK FILL METHODS
- 0 VENT WHILE FILLING
- 0 EVACUATED FILL
- 0 ULLAGE RECOMPRESSION

## TRANSFER METHODS
- 0 PRESSURIZED
- 0 PUMPED
- 0 GRAVITY

## SELECTION FACTORS
- 0 ABILITY TO ACCOMPLISH FILL
- 0 VENTING REQUIREMENTS
- 0 RELIABILITY

**AutoGenous Pressurized Transfer was chosen for cryogens**
TANK SHAPE ALTERNATIVES

LH₂ TANKS (19,000 LBM)

- D = 13.3 ft
- D = 11.6 ft
- D = 11 ft
- D = 8.7 ft
- D = 14 ft
- L = 41 ft
- θ = 34.5°

L/D = 1 —— L/D = 2 —— L/D = 5 —— L/D = 10 —— CONICAL BASED

- D = 13.7 ft
- D = 10 ft
- D = 7.1 ft
- D = 5.6 ft
- D = 13.3 ft
- L = 18.4 ft
- θ = 34.5°

LO₂ TANKS (81,000 LBM)
 allowanceslsh energy

\[ \Delta E = M \Delta g \Delta h \]

Energy for LH₂, ft-lbf

Tank Outlet

Tether Length, ft

10 - 10/15/85
## TANK ANALYSIS RESULTS

<table>
<thead>
<tr>
<th></th>
<th>L/D = 1</th>
<th>L/D = 2</th>
<th>L/D = 5</th>
<th>L/D = 10</th>
<th>CONICAL BASED</th>
</tr>
</thead>
<tbody>
<tr>
<td>LH2</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>TANK AND MLI MASS, LBM</td>
<td>5,716</td>
<td>4,362</td>
<td>5,008</td>
<td>6,163</td>
<td>4,110</td>
</tr>
<tr>
<td>BOILOFF, LBM</td>
<td>28,768</td>
<td>21,900</td>
<td>25,230</td>
<td>31,010</td>
<td>20,674</td>
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<tr>
<td>TOTAL MASS, LBM</td>
<td>34,484</td>
<td>26,262</td>
<td>30,238</td>
<td>37,173</td>
<td>24,784</td>
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<tr>
<td>SLOSH ENERGY, FT-LBF (10% FILL, 3000 FT TETHER)</td>
<td>2</td>
<td>3</td>
<td>4</td>
<td>6</td>
<td>6</td>
</tr>
<tr>
<td>LO2*</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>TOTAL MASS, LBM</td>
<td>1,202</td>
<td>1,299</td>
<td>1,830</td>
<td>2,525</td>
<td>1,262</td>
</tr>
<tr>
<td>SLOSH ENERGY, FT-LBF (10% FILL, 3000 FT TETHER)</td>
<td>6</td>
<td>7</td>
<td>11</td>
<td>16</td>
<td>14</td>
</tr>
</tbody>
</table>

* LO2 BOILOFF IS ZERO; LO2 VCS IS COOLED BY H₂
### Facility Design Characteristics

<table>
<thead>
<tr>
<th>Item</th>
<th>Mass, Lbm</th>
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</thead>
<tbody>
<tr>
<td>Tanks/Feed System</td>
<td>5,570</td>
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<tr>
<td>Structure and Debris Shielding</td>
<td>11,000</td>
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<tr>
<td>Thermal Control</td>
<td>4,000</td>
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<tr>
<td>Pressurization System</td>
<td>1,080</td>
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<tr>
<td>Power/Energy Storage</td>
<td>1,700</td>
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<tr>
<td>ACS/Propulsion</td>
<td>500</td>
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<tr>
<td>Control/Monitoring</td>
<td>1,000</td>
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<tr>
<td>Avionics</td>
<td>500</td>
</tr>
<tr>
<td>Grappling/Docking Equipment</td>
<td>3,000</td>
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<tr>
<td><strong>Dry Mass</strong></td>
<td>28,350</td>
</tr>
<tr>
<td><strong>Propellant</strong></td>
<td>100,000</td>
</tr>
<tr>
<td><strong>Total Mass</strong></td>
<td>128,350</td>
</tr>
</tbody>
</table>

---

*Martin Marietta*

12 - 10/15/85
TORF LAUNCH CONFIGURATION

0 STS AVAILABLE PAYLOAD BAY IS 60 FT
- DEPLOYMENT IS VIA SPRING LOADED TRUNNIONS AND STS RMS
- DEPLOYMENT WILL BE IN PROXIMITY (<100 m) OF SPACE STATION

0 TORF RMS LAUNCH CONFIGURATION
- STOWED IN CHANNEL ALONG TORF SIDE
- WRIST AND GRAPPLE FIXTURE SECURED ON TORF AFT END
- 6.9 FT (2.1 m) TELESCOPING SECTION IN UPPER ARM STOWED IN RETRACTED POSITION
AUXILIARY PROPULSION

- REQUIREMENTS INCLUDE ATMOSPHERIC DRAG MAKE-UP, SHUTTLE BERTHING, AND OTV BERTHING

- SHUTTLE AND OTV APPROACH VELOCITIES ARE ASSUMED TO BE 2 FT/S

- CONTINUOUS DRAG MAKE-UP IS NECESSARY TO MINIMIZE THRUSTER INDUCED TORF LIBRATION

- A SINGLE BURN OF A 30 DAY REBOOST INDUCES LIBRATION ANGLES OF OVER 30° WITH 25, 50 OR 100 LBF THRUSTERS

- USING ONLY H₂ BOILOFF IN COLD GAS THRUSTERS, THE APS REQUIREMENT CAN BE MET WITH A SPECIFIC IMPULSE OF 220 s

- BOTH TORF AND SPACE STATION DRAG MAKE-UP CAN BE DONE WITH A SPECIFIC IMPULSE OF 570 s

- BASELINE 220 s SPECIFIC IMPULSE THRUSTERS FOR TORF AUXILIARY PROPULSION, EXCLUDING SPACE STATION DRAG MAKE-UP
DEBRIS SHIELD DIMENSIONAL REQUIREMENTS

0 NASA SPECIFICATION - A 95% PROBABILITY OF NO PENETRATION OF SHIELD OR TANK IN A 10-YEAR PERIOD

0 TO MEET REQUIREMENT, AN ALUMINUM PARTICLE, 1 cm IN DIAMETER, MOVING AT 9 km/s MUST BE STOPPED

0 BASELINE SHIELD DESIGN IS A TWO-WALL TYPE WITH BUMPER AND BACKWALL

0 SHIELD WALL THICKNESSES GIVEN BY EXPERIMENTAL CORRELATION AS A FUNCTION OF

- PARTICLE MASS
- PARTICLE VELOCITY
- PARTICLE DENSITY
- WALL YIELD STRENGTH
- WALL DENSITY
- BUMPER-TO-BACKWALL SPACING

(REF. ESA SP 153, PROTECTION FOR HALLEYS COMET MISSION, BURTON G. COUR-PALAISS)
TORF DEBRIS SHIELD

0 ALUMINUM TANK WALL UTILIZED AS BACK WALL
   - DICTATED BY WELD LAND MINIMUM THICKNESS
   - REQUIRED THICKNESS IS 0.32 CM

0 ALUMINUM HONEYCOMB SUPPORT STRUCTURE OUTER SHEAR PANEL UTILIZED AS BUMPER

0 VCS, MLI, AND HONEYCOMB STRUCTURE INNER SHEAR PANEL PROVIDE ADDITIONAL PROTECTION

0 VCS TUBE EXPOSED AREA IS SMALL
   - HONEYCOMB STRUCTURE IS SUFFICIENT SHielding
   - MEETS NASA SPECIFICATION OF 95% PROBABILITY OF NO PUNCTURE
FACILITY/FLUID DYNAMICS STUDY

CONFIGURATION DEFINITION

DISTURBANCE DEFINITION

MOTION TYPES

DAMPENING CHARACTERISTICS

MATHEMATICAL MODEL

RESPONSE MOTIONS

OPERATIONAL AVOIDANCE

INHERENT STABILITY

AUGMENTED STABILITY

MARTIN MARIETTA

18 - 10/15/85
## DISTURBANCE TYPES AND MAGNITUDES

<table>
<thead>
<tr>
<th>TYPE</th>
<th>MAGNITUDE</th>
<th>DESCRIPTION</th>
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<tbody>
<tr>
<td>IMPULSIVE</td>
<td>0-16000 LBF-SEC</td>
<td>BERTHING</td>
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<tr>
<td></td>
<td>0-100 IN LBF-SEC</td>
<td>ATTITUDE CONTROL</td>
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<tr>
<td>RANDOM</td>
<td>0-10 LBF</td>
<td>CREW MOVEMENT</td>
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<tr>
<td>SINUSOIDAL</td>
<td>2 \times 10^{-2} LBF, 90 MIN PERIOD</td>
<td>DRAG ON SOLAR ARRAYS</td>
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<tr>
<td></td>
<td>10^{-6} g, 90 MIN PERIOD</td>
<td>LUNAR GRAVITY</td>
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<tr>
<td>STEADY STATE</td>
<td>3 \times 10^{-3} LBF</td>
<td>ATMOSPHERIC DRAG</td>
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<tr>
<td>STEP</td>
<td>0.028 LBF</td>
<td>STATIONKEEPING</td>
</tr>
<tr>
<td></td>
<td>100 LBF, 10 MIN/30 DAYS</td>
<td>REBOOST</td>
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<tr>
<td>TRANSIENTS</td>
<td>10^{-3} LBF</td>
<td>FLUID TRANSFER STARTUP</td>
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<tr>
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<td>10^{-2} LBF</td>
<td>STEADY FLOW</td>
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## INITIAL DYNAMICS ANALYSES

### SMALL-DISTURBANCE, LINEAR, PLANAR MODEL (2640 FT TETHER)

<table>
<thead>
<tr>
<th>MODE</th>
<th>MOTION</th>
<th>PERIOD, s</th>
<th>$g_{0}$ - RAD/LBF</th>
<th>$g_{11}$ - RAD/LBF</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>TETHER PENDULUM</td>
<td>3190</td>
<td>$6 \times 10^{-5}$</td>
<td>$1.5 \times 10^{-4}$</td>
</tr>
<tr>
<td>2</td>
<td>FACILITY PENDULUM</td>
<td>181</td>
<td>$1.6 \times 10^{-3}$</td>
<td>$5.3 \times 10^{-3}$</td>
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<tr>
<td>3</td>
<td>FACILITY FLUIDS</td>
<td>124</td>
<td>$1.3 \times 10^{-2}$</td>
<td>$2.2 \times 10^{-2}$</td>
</tr>
<tr>
<td>4</td>
<td>FACILITY FLUIDS</td>
<td>113</td>
<td>$7 \times 10^{-3}$</td>
<td>$3.9 \times 10^{-2}$</td>
</tr>
<tr>
<td>5</td>
<td>OTV FLUIDS</td>
<td>95</td>
<td>$3.1 \times 10^{-4}$</td>
<td>$4.8 \times 10^{-4}$</td>
</tr>
<tr>
<td>6</td>
<td>OTV FLUIDS</td>
<td>76</td>
<td>$7.3 \times 10^{-4}$</td>
<td>$2.4 \times 10^{-4}$</td>
</tr>
</tbody>
</table>

0 FREQUENCY IS A LINEAR FUNCTION OF TETHER LENGTH
MODEL APPROACH

THE MODEL IS A COLLECTION OF POINT MASS CONNECTED BY RIGID LINKS

THE FACILITY AND OTV AS A SINGLE RIGID BODY IS REPRESENTED BY 2 MASSES WHICH ARE SEPARATED BY A DISTANCE WHICH GIVES THE SAME CENTER OF MASS AND THE SAME PITCH AND YAW INERTIAS. EACH FLUID MASS IS REPRESENTED AS A PENDULUM WHOSE LENGTH IS BASED ON TANK GEOMETRY.
ANALYSIS APPROACH

0 IDENTIFY WORST-CASE DISTURBANCES
0 EVALUATE LIMITS FOR ZERO DAMPING
   - FLUID SLOSH AMPLITUDE
   - FACILITY SWING ANGLE
0 EVALUATE LIMITS FOR DAMPING TIME CONSTANT
0 SYSTEM PARAMETERS
   - FACILITY FILL: 10\%, 50\%, 90\%
   - OTV FILL: 10\%, 50\%, 90\%
   - TETHER LENGTH: 500 FT, 1000 FT, 2000 FT, 4000 FT
   - FACILITY MAXIMUM SWING ANGLE: 0°, 15°, 30°
DISTURBANCES

Various forcing functions originating on the space station were considered:
- In plane
- Out of plane
- Along radius
- Station delta = 1 ft/s (maximum).

Disturbances on torf during fluid transfer (~ .01 lbf) are negligible.

The worst case disturbance was used for all following analyses.
RESULTS

COMPARISON OF DAMPED AND UNDAMPED SLOSH RESPONSES DUE TO A 1 FT/SEC VELOCITY CHANGE OF THE SPACE STATION. TETHER LENGTH = 1000 FT.
RESULTS (CONTINUED)

TETHER AND FACILITY SWING ANGLES FOR THE UNDAMPED CASE OF A 1 FT/SEC VELOCITY CHANGE OF THE SPACE STATION
RESULTS (CONCLUDED)

FLUID SLOSH ANGLE AS A FUNCTION OF TETHER LENGTH FOR A 1 FT/SEC VELOCITY CHANGE OF THE SPACE STATION

SLOSH ANGLE - DEGREES

TETHER LENGTH - FEET

MARTIN-MARIETTA
26 - 10/15/85
CONCLUSIONS

0 WORST DISTURBANCES ARE IMPULSIVE
0 FLUID MOTION SENSITIVE TO TETHER LENGTH
0 DAMPING REQUIRED FOR MOTION PERSISTANCE
0 MAXIMUM MOTION INSENSITIVE TO DAMPING
0 MINIMUM DAMPING 5%
0 MINIMUM TETHER LENGTH 1000 FT
POWER TOWER SPACE STATION DESIGN

FLIGHT PATH
NADIR
MOBILE MANIPULATOR

0 50' SCALE

MOBILE MANIPULATOR
LOGISTICS
LAB

MASS: $10^6$ LBM

37.5 KW DYNAMIC POWER SYSTEM

UPPER KEEL
TRANSVERSE BOOM

MOBILE MANIPULATOR

LOWER KEEL
KEEL EXTENSION

RADIATORS
AIRLOCK

LAB
LAB

LOWER BOOM

RCS

ALPHA ADJUST
BETA ADJUST

ALPHA JOINT

WATER

MARTIN MARIETTA

28 - 10/15/85
SPACE STATION IMPACT ASSESSMENT

0 SPACE STATION HARDWARE NECESSARY TO SUPPORT THE TORF INCLUDES
   - TETHER DEPLOYMENT PALLET
   - TETHER DEPLOYMENT BOOM
   - TORF BERTHING MECHANISM
   - TRACKING/RANGING ELECTRONICS

0 MAJOR TECHNOLOGICAL ADVANCES ARE NOT NECESSARY TO DEVELOP THIS HARDWARE

0 ACCELERATION OF OVER $10^{-5}g$ ARE IMPOSED ON THE SPACE STATION

0 BERTHING THE ORBITER OFF-AXIS AT THE STATION WILL IMPOSE ATTITUDE TORQUES AND
   SHIFTS IN THE GRAVITY GRADIENT MAGNITUDE

0 PROXIMITY OPERATIONS MUST AVOID TETHER

0 RENDEZVOUS WITH EITHER THE TORF OR THE STATION INVOLVES NON-KEPLERIAN ORBITS
   AND MUST BE DONE "ON THE FLY"

MARTIN MARIETTA
29 - 10/15/85
SEVERAL OPTIONS EXIST FOR OTV DEPLOYMENT TO TORF

- THE OMV MANEUVERS THE OTV/PAYLOAD PACKAGE TO THE TORF
- A CRAWLER TRANSPORTS THE OTV/PAYLOAD DOWN THE TETHER TO THE TORF

THE OMV MANEUVER WAS BASELINED FOR THE BERTHING MANEUVER

- RENDEZVOUS WITH OUTBOARD END OF DEPLOYED FACILITY APPEARS BEST

HARDWARE NECESSARY FOR VEHICLE DOCKING INCLUDES

- STRONG RMSs
- BERTHING RING WITH LATCHES
- FLUID TRANSFER CONNECTOR

TIMELINE INCLUDES:

- SIX OTV REFUELING PER YEAR
- SIX OTV SCAVENGING (IF DESIRABLE) PER YEAR
- SIX STS RESUPPLY PER YEAR
PROXIMITY OPERATIONS

THE OMV MANEUVERS THE OTV AROUND THE SPACE STATION

- MAXIMUM OTV/PAYLOAD DRY MASS IS 23,000 LBM

OMV ORBITAL MANEUVERING DEPENDS ON TORF DEPLOYMENT DIRECTION WITH RESPECT TO THE SPACE STATION

- WITH THE TORF DEPLOYED TOWARDS THE EARTH, THE OTV/OMV/PAYLOAD PACKAGE RELEASES FROM THE SPACE STATION AND DROPS TO THE TORF. A MISDOCK RESULTS IN THE VEHICLE AND FACILITY DRIFTING AWAY FROM EACH OTHER

- WITH THE TORF DEPLOYED AWAY FROM THE EARTH, THE OMV MUST FIRE TOWARDS THE STATION TO MOVE AWAY. A MISDOCK RESULTS IN THE VEHICLE AND FACILITY DRIFTING TOWARDS EACH OTHER
GRAPPLE MANEUVER

0 GRAPPLING SCENARIO FOR OMV/OTV/PAYLOAD PACKAGE

- VEHICLE APPROACHES FACILITY.
- GRAPPLE ARM #1 ATTACHES TO OMV.
- GRAPPLE ARM #2 REACHES AROUND OTV AEROBRAKE AND ATTACHES TO OTV.
- GRAPPLE ARM #1 RELEASES OMV.
- OMV RELEASES OTV/PAYLOAD AND FLIES AWAY.
- GRAPPLE ARM #1 ATTACHES TO OTV.
- BOTH ARMS PULL OTV/PAYLOAD TO HARD DOCK ON TORF.
- FLUID TRANSFER LINES ATTACH.

0 A MODIFIED RMS IS BEING CONSIDERED FOR THE GRAPPLE ARM.

- LONGER AND STRONGER ARMS
- STRONGER JOINTS
- STRONGER ATTACH POINTS
- MODIFIED GRAPPLE FIXTURE
TETHER BREAKING OR SEVERING

0 ASSUME
- THE NOMINAL ORBIT ALTITUDE IS 250 NMI
- THE FACILITY IS ABOVE THE SPACE STATION
- THE FACILITY IS FULLY LOADED

0 FOR A 3000 FT DISTANCE FROM THE SPACE STATION TO THE CENTER OF MASS AFTER BREAKING:

- THE RESULTING SPACE STATION ORBIT HAS A PERIGEE OF 249.6 NMI
- THE RESULTING TORF ORBIT HAS AN APOGEE OF 251 NMI

0 FOR THE TETHER LENGTHS REQUIRED BY THE REFUELING FACILITY, IF THE TETHER BREAKS, THE SPACE STATION IS NOT IN DANGER OF DEORBITING
MAJOR CONCLUSIONS

0 A TORF APPEARS TO BE TECHNICALLY FEASIBLE

0 THE MAJOR SYSTEM CONCERNS FOCUS AROUND THE COMPLEX OVERALL OPERATIONS REQUIREMENTS

0 THE ADVANTAGES OF A TORF INCLUDE:

- POTENTIAL IMPROVED SPACE STATION STABILITY
- POTENTIAL EASIER FACILITY FLUID MANAGEMENT
- POTENTIAL IMPROVED SPACE STATION SAFETY
- PROBABLE REDUCED SPACE STATION CONTAMINATION

0 FURTHER ANALYSES SHOULD COMPARE TETHERED TO ZERO-G PROPELLANT STORAGE TO QUANTIFY THESE ADVANTAGES
CURRENT PROGRAM OVERVIEW

PROGRAM TITLE: TETHERED ORBITAL REFUELING STUDY

CONTRACT: NAS9-17422

PROGRAM MANAGER: DALE FESTER (303) 977-8699

CUSTOMER: NASA-JSC
KENNETH R. KROLL, TECHNICAL MONITOR


PERIOD OF PERFORMANCE: SEPTEMBER 1985 TO JUNE 1986
TETHERS AND GRAVITY IN SPACE

Paul A. Penzo
Jet Propulsion Laboratory
Pasadena, California

Office of Space Flight
Advanced Programs
NASA Headquarters

Life Science
GRAVITY IN SPACE—LIFE SCIENCE OBJECTIVES

• Ease transition between 0g in space and 1g on Earth
• Provide earth-like habitability at partial g
• Study effects of partial g on plant, animal development
• Study effects on man: cardiovascular, skeletal, vestibular systems; performance
• Study effects on individual development
• Simulate gravity conditions of moon, Mars
• Prepare for possible use of artificial gravity for manned missions to Mars, asteroids
PRODUCING VARIABLE GRAVITY IN SPACE

CENTRIFUGE
- ANY $g$-LEVEL
- SMALL VOLUME
- LARGE CORIOLIS
- DYNAMIC DISTURBANCE

TETHER
- LOW $g$-LEVEL (0.1)
- LARGE VOLUME
- LONG DURATION
- NEGLIGIBLE CORIOLIS

ROTATION
- ANY $g$-LEVEL
- LARGE RADIUS
- LOW CORIOLIS
- PLATFORM, BUT POSSIBLY SPACE STATION
FORCES IN TETHERED ORBITAL SYSTEM

RESULTANT FORCES CAUSE SYSTEM TO STABILIZE AT THE LOCAL VERTICAL

CENTRIFUGAL ACCELERATION

RESULTANT ACCELERATION COMPONENTS

GRAVITATIONAL ACCELERATION

CENTER OF MASS

ORBIT OF CENTER OF MASS

TETHER TENSION

LOCAL VERTICAL

EARTH
TETHER MASS AS FUNCTION OF LENGTH

MATERIAL: KEVLAR 29
SAFETY FACTOR = 3.5
WORKING STRESS = 0.7 x 10^8 nm^-2
DENSITY = 1450 kg m^-3
ALTITUDE = 500 km
STEADY STATE
TETHERED MICROGRAVITY FACILITY

<table>
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<tr>
<th>DISTANCE FROM CG</th>
<th>g's</th>
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<tbody>
<tr>
<td>200km</td>
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<tr>
<td>20km</td>
<td>$10^{-2}$</td>
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<tr>
<td>2km</td>
<td>$10^{-3}$</td>
</tr>
<tr>
<td>200m</td>
<td>$10^{-4}$</td>
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<tr>
<td>20m</td>
<td>$10^{-5}$</td>
</tr>
<tr>
<td>2m</td>
<td>$10^{-6}$</td>
</tr>
<tr>
<td>20cm</td>
<td>$10^{-7}$</td>
</tr>
<tr>
<td>2cm</td>
<td>$10^{-8}$</td>
</tr>
</tbody>
</table>

- **20,000lbs.**
- **5 x 10^{-4} g's**
- **Contamination-Free and Isolation Level**

**Platform**

- **Tension = 100 lbs**
- **Microgravity ("Zero G") Level**

**Space Processing Facility**

- **200,000 lbs**
- **5 x 10^{-5} g's**

**Space Station**

- g's due to drag are offset by thruster in space station, or electrodynamic force generated by tether motor.
LIFE SCIENCES GRAVITY LABORATORY (GRAVLAB)
TECHNOLOGY READINESS POST IOC

SHUTTLE ORBITER MISSIONS
- SOLAR POWER SYSTEMS
- BEAM BUILDING
- SPACELAB EXPERIENCE
- TETHER EXPERIENCE
- SATELLITE SERVICING

MISSING
- MANNED OMV

SPACE STATION PROGRAM
- PLATFORM CONSTRUCTION
- LONG TERM HABITATION
- MANNED OPERATIONS
- EXTENSIVE SERVICING

GRAVLAB
GRAVLAB DESIGN—TETHER PLATFORM CONCEPT

- END MASSES ASSUMED EQUAL AND ROTATING ABOUT COMMON CENTER
- SOLAR ARRAYS ARE DE-SPUN AND SUN ORIENTED

<table>
<thead>
<tr>
<th>DEPLOYED LENGTH</th>
<th>RPM</th>
<th>g—LEVEL</th>
</tr>
</thead>
<tbody>
<tr>
<td>4 km</td>
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<td>1.25</td>
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<tr>
<td>5 km</td>
<td>0.48</td>
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<tr>
<td>6 km</td>
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<td>0.38</td>
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<td>8 km</td>
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<td>0.16</td>
</tr>
<tr>
<td>10 km</td>
<td>0.12</td>
<td>0.08</td>
</tr>
</tbody>
</table>

PROPELLANT/MOTOR (ΔV — 125 m/s)
GRAVLAB DESIGN—STATION CONCEPT

- 4 MODULES, 2 AT EACH END ROTATE ABOUT A COMMON CENTER
- ELEVATOR TRANSfers MEN, SUPPLIES TO EITHER END

<table>
<thead>
<tr>
<th>RPM</th>
<th>ΔV</th>
<th>G-LEVEL</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
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<tr>
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<td>0.45</td>
</tr>
<tr>
<td>3</td>
<td>30 m/s</td>
<td>1.00</td>
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GRAVLAB STATION DESIGN—TETHER ENHANCEMENT

- TETHER MAY BE USED TO CONTROL ROTATION (HENCE G-LEVEL) WITHOUT USE OF PROPELLANT

<table>
<thead>
<tr>
<th>Deployed Length</th>
<th>RPM</th>
<th>G-Level</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
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<tr>
<td>400</td>
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<tr>
<td>700</td>
<td>1.2</td>
<td>0.16</td>
</tr>
<tr>
<td>900</td>
<td>1.0</td>
<td>0.11</td>
</tr>
</tbody>
</table>
CONCLUSIONS/RECOMMENDATIONS

• Life sciences should consider utilizing the low gravity level available with the shuttle launched tethered satellite system.

• This system can support long duration experiments when placed on the space station.

• Post IOC, space station and tether systems will be available to build a rotating separate variable gravity laboratory.

• For such a laboratory, tethers can provide a large and easily varied radius to reduce Coriolis effects, and vary the g-level.
1. INTRODUCTION

Latest Fluidodynamic and Material Science experiments in Microgravity Environment have emphasized the importance of the residual gravity level and of the g-jitter on Fluids Physics phenomena.

These studies point out at the importance of:

1) studying the combined steady residual g-level and/or the g-jitter on the different classes of experiments.

2) studying the non-linear effects on the fluid systems such as: accumulation during the experiment time, stability of fronts (liquid-fluids interfaces, solidification fronts, diffusion fronts) and consequently evaluating the effects upon the processes under study.

3) separating the effects of the residual constant gravity-level from the effects of g-jitter.

The above points are of interest not only for a proper analysis of the experimental results and for a rational design of microgravity experiments, but also for allowing the Sponsoring Space Agencies and/or the Manufacturing Companies to adopt useful criteria in the design requirements of the platforms and of the microgravity laboratories. Sound requirements are in fact desperately sought about the residual gravity levels, below which scientific returns from the various experiments can be ensured; the danger is to make expensive and useless efforts
in reducing the gravity field at too low levels that are too demanding for Space hardware.

A number of the above questions could be resolved by experimenting at conditions of zero-gravity (say at levels of 10 g) and by evaluating the effect of increasing gravity levels on single experiments, if the possibility exists of increasing at will the residual gravity.

2. G-LEVEL TOLERABILITY OF SPACE PROCESSING EXPERIMENTS

The strong reduction of the g-level ensured by the Space environments is not always sufficient to guarantee the thermofluidodynamics fields wanted by the experimenters (that is the fields corresponding to real zero-gravity conditions).

For instance, the problems of the stability of the solidification fronts, of the stability of the symmetry conditions (spherical, cylindrical and plane) points out at the possibility that there might be a number of accumulation processes (memory of the system) particularly when the boundary conditions are somehow dependent on the thermofluidynamics fields themselves.

As an example we briefly analyze the application of a g-level step disturbance and its effect on the propagation of a plane solidification front.

In consequence of the g-level, buoyancy forces are produced; they induce a convective velocity field which distorts the concentration and/or temperature fronts ahead of the solidification front in the liquid where the process of
solidification takes place and which is mainly controlled by diffusion processes in absence of gravity.

This distortion depends on the level of the residual gravity, on the characteristics of the fluid and on the boundary conditions.

The relation between the order of magnitude of the induced convective speeds and of the diffusion speed can be taken as a measure of the disturbance.

The ratio between the convective speed and the diffusive speed can be very high, also for small values of the imposed g-level, and, consequently, also the distortion of the solidification front can be relevant. The return of the g-level to very small values, even if the boundary conditions have not changed, seldom allows a return to the conditions of a plane front within a reasonable time (the thermal and mass diffusion velocities, are typically very small).

Another important example is the effect of a g-level on the spherical symmetry of a thermofluiddynamic field.

Let use consider a spherical drop of a liquid or a solid sphere that are dissolving or forming in a liquid matrix at condition of zero gravity; typical examples are those of the solution growth or of the drops formation (e.g. cooling through a miscibility gap).

Periodical g-jitter disturbances have different effects on the overall drop motion and on the thermofluiddynamic field around the drop: the overall drop motion may be not relevant in a purely g-jitter field with zero average value (displacements of the drop relative to the liquid tend to
cancel out during a cycle) but the temperature and concentration field distortion could be of importance if some stability limits are trespassed.

The order of magnitude of the times necessary to cause the distortion, in comparison to those needed to return to spherical fronts, are in the same ratios as the (induced) convective velocities and the diffusion velocities:

\[
\frac{V_c}{V_d} = gL^2 / \nu D \frac{\Delta \rho}{\rho}
\]

where \( D \) is the thermal (or mass) diffusion coefficient and \( \Delta \rho/\rho \) the density variation consequent to a temperature or to a concentration non uniformity.

Referring to typical values for the aqueous solutions it results (for \( g=10^{-4} \) g):

\[
\frac{t_n}{t_d} \approx 10^3 \quad \text{(mass diffusion)}
\]

\[
\frac{t_n}{t_d} \approx 10^2 \quad \text{(thermal diffusion)}
\]

This would mean that it is necessary to wait a time of the order of 15 minutes for each of \( 10^{-4} \) disturbance that lasts one second only, in order to obtain the zero-g concentration conditions again, and to wait a time of the order of 2 minutes, in order to obtain the conditions again for the zero-g temperature distribution.

Of course the real situation is more complex insofar as the convective motion has to decay to a zero velocity condition (the decay is related to the viscous momentum propagation time \( L^2 / \nu \)) and the zero-g concentration and/or temperature fields must have time to reach purely diffusive conditions. The evolution towards those conditions strongly depends on...
the problems under study and it is difficult to give general quantitative indications.

In the case of g-jitter with a certain frequency it is more difficult to anticipate what is the order of magnitude of the times involved, mainly because those caused during a semi-period might be compensated by that induced in the next semi-period.

The case becomes more difficult if limits of stability are trespassed, this occurs when, for instance, the g-disturbance is able to induce in the liquid sort of Benard cells that create a flow pattern that may be independent of the direction of the g-level during the semiperiod.

3. POTENTIALITIES OF A TETHERED ELEVATOR

It is desiderable the realization of a platform able to: 1) set levels of zero gravity to certain payload, 2) allow a controlled change of this level within values of $10^{-2} < g/g_c < 10^{-1}$ and 3) create accelerations with controlled amplitudes and frequency.

In fact application of controllable g-levels allows to answer a number of questions posed by recent results of the experimentation in microgravitational Fluidynamics.

The Tethered Elevator could have the possibility of providing variable g-levels (both steady and g-jitter) around a very low steady g-level (that can be realized when the Elevator is near the center of mass of the Space Station-Tether complex). Sliding the elevator at a distance (e) from the center of mass one gets a steady g-level that is approximatively equal to: $g/g_c = 31/R$; R being the
distance of the center of mass from the center of the earth (typically $g/q = 4.4 \times 10^{-2}$ for each meter of the distance (1)).

When positioning a variable periodic oscillation to the Payload a clean g-jitter disturbance can be obtain that would not be otherwise obtainable by other systems. These two possibilities make the Elevator a unique facility to help resolving a number of still open questions.

4. MODEL EXPERIMENTS

A number of experiments can be devised to ascertain the effect of the g-level on some class of experiments.

Two experiments falling within the fluidynamics problematics indicated in Section 2 are briefly described.

A) A copper sphere is suspended inside a transparent liquid matrix (See Fig.1) and is observed by holography or interferometry in order to visualize the isotherms. When heating the sphere by Joule heaters embedded in the copper sphere, starting from an isothermal spherical simmetry, (i.e. when locating the payload at the CG of the system, or very close to it) and before any interference occurs with non spherically-symmetric boundaries (if any) the isotherm pattern look as in Fig.2. The thermal field can then be disturbed either by moving the payload gently out of the CG (to a steady g-level) or inducing a preselected g-jitter. At those new conditions the isotherms (that will be axisymmetric along the induced g direction) will evolve towards another pattern due to the convective flow field induced by the thermal buoyancy forces (Fig.3).
evolution time depends on the values of the flow velocities. After a quasi-steady pattern has been established, the zero-g conditions are reestablished on the payload: the system will the evolve towards the initial, spherical symmetric, diffusion controlled situation. The time necessary to restore the zero-g thermal pattern will depend on the value of the flow field velocities and on the characteristic thermal diffusion time.

B) A very similar experiment can be device for a mass diffusion controlled experiment in which a dissolving sphere of solid material is suspended in a solution and the iso-concentration fronts are visualized by a similar diagnostic apparatus. A spherical symmetry can be ensured for the diffusion controlled (zero-g) process by suitable boundary geometry and conditions. The measurement of the times necessary to disturb the axisymmetry and to restore it at different steady and g-jitter levels will greatly help in the establishment of valid criteria for the g-level tolerability in a very important class of MS experiments (e.g. solution crystal growth and vapour crystal growth).

5. CONCLUSIONS

The Tethered Elevator will greatly contribute to the solutions of many still open problems that are preventing a much wider utilization of the Space environment in the Microgavity area. Detailed study must be carried out to enable the Elevator to perform along the briefly described lines.
Fig. 1 - Spherical heater suspended in a transparent box
Fig. 2 - Temperature field and isotherms in a zero-g conditions
Fig. 3 - Distorted isotherms in micro-g environment
Can the extra cost of a tether be justified?

Is movement of the space station center of gravity acceptable?
  Should microgravity laboratory modules be moved to the tether?
  Should balancing tether applications be used?

Is changing proximity operations procedures and hardware acceptable?
  Can a tether crawler be developed?
  Can docking be done at a center of gravity which is on the tether?

Will platforms be permanently deployed?
  Where will servicing be performed?
  Is tether movement to be limited?
  Can experiments be stopped for disturbances?

Which is more important: manned involvement low disturbance levels?
  Can experiments be remotely controlled?

Can power and communications be supplied through the tether to a moving platform?

Will laboratory movement adversely affect experiments?
  What are the best procedures for limiting tether movement?
  Can disturbance sensitivity and variable gravity laboratory coexist?

Is liquid settling the primary use of gravity?
  Are long tether lengths for small sizes practical?

How can higher gravity level medical experiments be integrated into the space station system using a tether?

Venezia, 16 October, 1985
CONSTELLATIONS PANEL
Introduction

The Constellations Panel, because of its limited number of attendees, shared its life during the Workshop in part with the Microgravity Panel and in part with the Space Station Panel. It could, therefore, benefit from the inputs of two different panels which are related to tethered constellations. Tethered constellations, in fact, can provide a valuable solution to projects such as the micro-g/variable-g laboratory, the multi-probe tethered system, and the centrifuge for low-gravity applications.

The following presentation highlights the versatility of tethered constellations and the various different configurations that have been conceived so far. The presentation is divided into three sequential timeframes which have, as a central reference point, the IOC (Initial Operating Capability) phase of the Space Station program. Therefore the demonstration flights of certain one-dimensional tethered constellations belong to the Pre-IOC-Era while the final, operational utilizations of the one-dimensional tethered constellations belong to the IOC-Era. All the other more complex configurations, such as the two-dimensional constellations and a couple of new ideas developed during the Workshop, have been listed under the Post-IOC-Era category.
Pre-IOC-Era

1. Demo flight for the micro-g/variable-g (space elevator) with a modified TSS system (e.g., adding a down-scaled elevator to the TSS)

2. Shuttle-borne, multi-probe 1-D system for simultaneous data collection (e.g., measurement of spatial geophysical gradients with good time correlation)
1. DEMO MULTI-\textit{g}/VARIABLE-\textit{g}

2. DEMO MULTI-PROBE SYSTEM (BEADS ON THE TETHER)
IOC-Era

3. Micro-g/Variable-g Lab (space elevator) Space Station-borne

4. Space Station c.o. (orbital center ~ center of mass) management

5. Space Station-borne multi-probe system
3. 1-D, 3-Mass, Vertical, Tethered Constellation (SS at one end)

PURPOSE - Multi-purpose system:
- micro-g/variable-g
- controlled g variations
- service to the end platform

NEED - Strongly requested by the micro-g community
- g-tuning
- g-jitter
- controlled-g time profile
- hysteresis cycles

BENEFITS - Unique capability of providing time varying g-profile from microgravity level to $10^{-2}g$
FEASIBILITY - high

PRACTICALITY - high

COST BENEFIT POTENTIAL - N/A for variable-g applications
   - TBD for micro-g applications

PRIORITY - 1st

REQUESTED TECHNOLOGY - Very accurate accelerometers for micro-g
   applications
   - Very smoothly operating reeling systems or
     crawlers

ALTERNATIVE APPROACHES - None for micro-g/variable-g combined
OTHER THAN TETHERS applications

NEAR TERM APPLICATION - Demonstration flights with the Shuttle (modify
   TSS system by adding a simplified elevator)

FUTURE APPLICATIONS - Attached to the Space Station
4. 1-D, 3-Mass, Vertical, Tethered Constellation (SS in the middle)

PURPOSE - Management of the system's orbital center

NEEDS - Especially required if another payload is deployed on a tether and the micro-g lab is on the SS

BENEFITS - Greater operation flexibility w.r.t. micro-g experiment schedule
FEASIBILITY - high

PRACTICALITY - high

COST BENEFIT POTENTIAL - TBD

PRIORITY - 1st

REQUESTED TECHNOLOGY - Very accurate accelerometers

ALTERNATIVE APPROACHES - Alone if tethered systems are deployed on one side and simultaneous micro-g experiments have to be performed

FUTURE APPLICATIONS - Attached to the Space Station
PURPOSE - Measurement of spatial geophysical gradients

BENEFITS - The system can reach low altitude orbits that are not achievable otherwise
- It provides simultaneous data at different locations (good time correlation of the measurements)
FEASIBILITY - high

PRACTICALITY - medium high

COST BENEFIT - N/A

PRIORITY - 1st

CRITICAL DESIGN AND REQUESTED TECHNOLOGY - o Dynamic analysis
  o Crawling system
  o Operational sequence for deployment and retrieval

ALTERNATIVE APPROACHES - None if simultaneous data collection is required
OTHER THAN TETHERS

FUTURE APPLICATIONS - Space Shuttle flight (or Space Station)
Post-IOC-Era

All the following applications are supposed to be free-flying systems.

6. Quadrangular 2-D constellations electrodynamically stabilized.

7. Quadrangular 2-D constellations stabilized by differential air drag.


9. Centrifuge for low-g application: $>10^{-3}$ g.

10. Torquing of a spinning station (or vehicle) for controlling the precession rate of the spin axis.
6. **2-D, Electrodynamically Stabilized Constellation (ESC)**

**PURPOSE** - Separation of junctions in a physically connected configuration

**FEASIBILITY** - Medium

**PRACTICALITY** - With complexities

**PRIORITY** - 2nd

**CRITICAL DESIGN** –
- Multi-reel system control
- Better dynamics analysis required

**FUTURE APPLICATIONS** - TBD
7. 2-D, Differential Drag Stabilized Constellations (DSC)

PURPOSE - Separation of functions in a physically connected configuration

FEASIBILITY - Medium

PRACTICALITY - With complexities

PRIORITY - 2nd

CRITICAL DESIGN -
- Multi-reel system control
- Better dynamics analysis required

FUTURE APPLICATIONS - TBD
8. 2-D, Electrodynamically Stabilized, Pseudo-Elliptical Constellation (PEC)

PURPOSE - External frame for stabilizing light structures (e.g., reflectors, solar sails)

FEASIBILITY - High

PRACTICALITY - Medium high

PRIORITY - 2nd

CRITICAL DESIGN - Multi-reel system control

FUTURE APPLICATIONS - TBD
NEW IDEAS

9. CENTRIFUGE FOR LOW GRAVITY: \( >10^{-3} \text{g} \)

10. TORQUING OF A SPINNING STATION FOR CONTROLLING THE PRECESSION RATE OF THE SPIN AXIS: (e.g., Keeping the spin axis aligned with the local vertical)
CONCLUSIONS

1-D vertical constellations provide unique capabilities (1st priority)
- 3-mass system (space elevator) can provide variable-g environment from microgravity level to $10^{-2}g$.
- More-than-3-mass system provides simultaneous data collection at different locations.
- 3-mass system (SS in the middle) for SS orbital center management allows simultaneous micro-g experiments and other tether assisted experiments.

2-D constellations (2nd priority)
- Stable configurations proposed for providing a separation of functions among physically connected platforms.
- Pseudo-elliptical constellations provide an external 2-D frame for stabilizing light structures (e.g., reflectors, solar sails).

RECOMMENDATIONS

Improve the fidelity of dynamics models, especially w.r.t. tether dynamics

Tether construction
- multi-function tether concept to be further developed
- tether physical characteristics; effects on the system dynamics

Ingenious design of crawling systems

Improve the knowledge of micro-g/variable-g requirements
PANEL PRESENTATION
ON
DYNAMICS OF TETHERED CONSTELLATIONS
IN EARTH ORBIT
BY
ENRICO LORENZINI

PRESENTED TO:
APPLICATIONS OF TETHERS IN SPACE WORKSHOP
VENICE, ITALY
15-17 OCTOBER 1985
SUMMARY OF PRESENTATION

- PHASE I STUDIES
  STATION KEEPING OF SINGLE-AXIS AND TWO-AXIS CONSTELLATIONS
  - WRAP-UP OF PHASE I STUDIES ALREADY PRESENTED TO NASA/MSFC
  - FURTHER ANALYSIS CARRIED OUT ON TWO-DIMENSIONAL CONSTELLATIONS
  - SINGLE-AXIS VERTICAL CONSTELLATIONS. LOW-G PLATFORM

- PHASE II STUDIES
  DEPLOYMENT OF CONSTELLATIONS
  - SINGLE-AXIS VERTICAL CONSTELLATIONS WITH THREE MASSES
    --DEPLOYMENT STRATEGY
    --DAMPING OF VIBRATIONAL MODES
PHASE I STUDIES

DYNAMICS AND STABILITY OF A HORIZONTAL TETHER
WITH A DOWNSTREAM BALLOON

STABILITY CONDITION WHEN NEGLECTING THE TETHER DRAG CONTRIBUTION IS GIVEN BY:

\[
\frac{1}{6} \rho \frac{a^2}{l} C_D \left( \frac{A_2}{m_2} - \frac{A_1}{m_1} \right) > 1
\]

THE SYSTEM DECAY BY:

\[
\frac{da}{dt} = 2 C_D \frac{A_2 + A_1}{m_1 + m_2} \rho \sqrt{\mu a}
\]

STABILITY AND SYSTEM LIFETIME, WITHOUT REBOOSTING, ARE CONTRASTING REQUIREMENTS.

MAXIMUM HORIZONTAL TETHER LENGTH ACHIEVABLE STRONGLY LIMITED BY TECHNOLOGICALLY ATTAINABLE A/M RATIO OF THE BALLOON (MAXIMUM A/M = 10 - 20 m²/kg)
DRAG STABILIZATION LIMITS FOR SINGLE-AXIS HORIZONTAL CONSTELLATIONS

\[
\text{AREA/MASS} = \frac{A}{M_2} = 10 \, m^2/kg
\]

<table>
<thead>
<tr>
<th>z(km)</th>
<th>( h_{\text{max}} ) (m)*</th>
<th>( \frac{da}{dt} ) (km/day)**</th>
<th>( h_{\text{max}} ) (m)</th>
<th>( \frac{da}{dt} ) (km/day)</th>
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<tr>
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</table>

*h_{\text{max}} = maximum horizontal length for stable configuration

**\( \frac{da}{dt} \) = orbital decay rate
ORIGINAL "FISH-BONE" CONFIGURATION STABILITY ANALYSIS

STABILITY CONDITION, WHEN NEGLECTING THE HORIZONTAL TETHER DRAG CONTRIBUTION, IS:

\[
\frac{1}{6} \rho \frac{a^2}{h} C_D \left( \frac{3A_2 + dt_2 \ell_2}{M_2} - \frac{3A_1 + dt_1 \ell_1}{M_1} \right) > 1
\]

-TETHER A/M RATIO INCREASES BY DECREASING ITS THICKNESS BUT IT IS NEVERTHELESS SMALL WHEN COMPARED TO THE BALLOONS.

-THE NECESSITY OF A MASSIVE DEPLOYER SYSTEM AT MASS M_{22} STRONGLY REDUCES THE MAXIMUM A/M RATIO OF THE DOWNSTREAM VERTICAL TETHER SUBSYSTEM.

CONCLUSIONS

-THE "FISH-BONE" CONSTELLATION, WITHOUT ANY MODIFICATIONS, HAS A STABILITY (MAXIMUM ALLOWABLE HORIZONTAL TETHER LENGTH) LOWER THAN THE SINGLE AXIS HORIZONTAL CONSTELLATION.
STABILITY LIMITS FOR A “FISH-BONE” CONSTELLATION VS. ORBITAL ALTITUDE

ASSUMPTIONS

\[ \ell_2 = \ell_1 = 20 \text{ km} \]

\[ A_{2/m_{12}} = 10 \text{ m}^2/\text{kg} \]; \[ A_{1/m_{11}} = 4 \times 10^{-3} \text{ m}^2/\text{kg} \]

\[ d_{t2} = 1 \text{ mm (kevlar)} \]; \[ d_{t1} = 2 \text{ mm (kevlar)} \]

\[ m_{11} = m_{12} = 200 \text{ kg} \]

\[ m_{21} = 1000 \text{ kg} \]; \[ m_{22} = 800 \text{ kg (deployer)} + 200 \text{ kg (balloon)} = 1000 \text{ kg} \]

<table>
<thead>
<tr>
<th>z(km)</th>
<th>( h_{\text{max}} ) (m)*</th>
<th>( \frac{da}{dt} ) (km/day)**</th>
<th>( h_{\text{max}} ) (m)</th>
<th>( \frac{da}{dt} ) (km/day)</th>
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<tr>
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<tr>
<td>300.</td>
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<td>1.86x10^3</td>
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<tr>
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<td>1.50</td>
<td>0.84</td>
<td>6.65x10^1</td>
<td>3.86x10^1</td>
</tr>
</tbody>
</table>

*\( h_{\text{max}} \) = maximum horizontal length for a stable configuration

**\( \frac{da}{dt} \) = orbital decay rate
SOME CONCEPTUAL EXAMPLES OF TWO-DIMENSIONAL CONSTELLATIONS HORIZONTALLY STABILIZED BY AIR DRAG (DSC)

WITH THIS CONFIGURATION THE DRAG FORCE IS FULLY EXPLOITED TO GUARANTEE THE MINIMUM TENSION LEVEL IN THE HORIZONTAL TETHERS AND NOT TO COUNTERACT GRAVITY GRADIENT.
Some conceptual configurations of two-dimensional constellations where shape stability is provided by electrodynamic forces (ESC).

-Electrodynamic forces stretch the constellation while the resultant is zero so that they don't increase the orbit decay.
DESIGN PARAMETERS FOR DSC AND ESC

*ASSUMPTIONS

Orbit Altitude = 500 km; \( m_{\text{tot}} = 4 \times 5000 \text{ kg} = 20 \text{ metric tons} \); \( h/\lambda = 0.5 \); Near Equatorial Orbit.

*^T = Tension in the horizontal tethers

**Orbit decay rate computed for average atmo. density.

'DSC WITH HORIZONTAL TETHER DIA. = .2 mm.'

<table>
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<tr>
<th>( \ast T(N) )</th>
<th>( T/3\mu^2 )</th>
<th>Min. Atmo. Density</th>
<th>Aver. Atmo. Density</th>
<th>Max. Atmo. Density</th>
<th>**Orbital Decay</th>
<th>h(km)</th>
<th>t(km)</th>
</tr>
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<tbody>
<tr>
<td></td>
<td></td>
<td>Exosp. Temp. = 600K</td>
<td>dia. balloon (m)</td>
<td>Exosp. Temp. = 800K</td>
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<tr>
<td>0.04</td>
<td>2.42 \times 10^8</td>
<td>195.05</td>
<td>73.22</td>
<td>29.31</td>
<td>1.25</td>
<td>14.08</td>
<td>28.08</td>
</tr>
<tr>
<td>0.06</td>
<td>3.63 \times 10^8</td>
<td>238.88</td>
<td>89.68</td>
<td>35.90</td>
<td>1.87</td>
<td>23.5</td>
<td>47.0</td>
</tr>
</tbody>
</table>

'ESC (OPTION 1) ALL ALUMINUM TETHERS WITH THE SAME DIA.'

<table>
<thead>
<tr>
<th>( \ast T(N) )</th>
<th>( V = \text{Electro Motive Force (KV)} )</th>
<th>( B_1 V ) ( 36\mu^2 )</th>
<th>h(km)</th>
<th>t(km)</th>
<th>Diameter Conductive Tether (mm)</th>
<th>Current (Amp)</th>
<th>Power (kw)</th>
<th>Solar Panel Area (m²)</th>
<th>**Orbit Decay (km/day)</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.06</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>0.21</td>
<td>0.2</td>
<td>2.76</td>
<td>20</td>
<td>1.61 \times 10^{-2}</td>
</tr>
<tr>
<td>0.1</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>0.27</td>
<td>0.33</td>
<td>4.55</td>
<td>32.5</td>
<td>1.83 \times 10^{-2}</td>
</tr>
<tr>
<td>0.2</td>
<td>13.80</td>
<td>10 \times 10^8</td>
<td></td>
<td>10</td>
<td>20</td>
<td>0.38</td>
<td>9.23</td>
<td>66.0</td>
<td>2.39 \times 10^{-2}</td>
</tr>
<tr>
<td>0.3</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>0.47</td>
<td>1.01</td>
<td>13.80</td>
<td>98.6</td>
<td>2.93 \times 10^{-2}</td>
</tr>
<tr>
<td>0.6</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>0.67</td>
<td>2.03</td>
<td>27.98</td>
<td>199.9</td>
<td>4.55 \times 10^{-2}</td>
</tr>
</tbody>
</table>
ESC (OPTION 2) HORIZONTAL WIRES ALUMINUM, VERTICAL WIRES COPPER
- COMPARATIVE TABLE

<table>
<thead>
<tr>
<th>T(N)</th>
<th>I(Amp)</th>
<th>V(KV)</th>
<th>Power(KW)</th>
<th>Comments</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.3</td>
<td>1.01</td>
<td>13.8</td>
<td>13.8</td>
<td>All wire aluminum</td>
</tr>
<tr>
<td></td>
<td></td>
<td>10.6</td>
<td>10.6</td>
<td>Horizontal Al + .38 mm dia. copper vertical</td>
</tr>
<tr>
<td></td>
<td></td>
<td>7.6</td>
<td>7.6</td>
<td>Horizontal Al + .54 mm dia. copper vertical</td>
</tr>
</tbody>
</table>

ESC (OPTION 3) HORIZONTAL WIRES KEVLAR VERTICAL WIRES COPPER
- FRONT VERTICAL WIRE AS ALFVEN ENGINE
- REAR VERTICAL WIRE AS POWER GENERATOR
- POWER TRANSFER (TRANSFER VOLTAGE 5kV, EFFICIENCY 90%)
  BIFILAR LINE TO DELIVER POWER MADE OF SAME COPPER WIRE

<table>
<thead>
<tr>
<th>I(A)</th>
<th>T(N)</th>
<th>V delivered(KV)</th>
<th>V(KV)</th>
<th>P(KW)</th>
<th>Comments</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.2</td>
<td>0.06</td>
<td>2.96</td>
<td>2.44</td>
<td>0.49</td>
<td>*</td>
</tr>
<tr>
<td>0.33</td>
<td>0.1</td>
<td>2.54</td>
<td>3.06</td>
<td>1.02</td>
<td>*</td>
</tr>
<tr>
<td>0.67</td>
<td>0.2</td>
<td>1.71</td>
<td>4.89</td>
<td>3.26</td>
<td>*</td>
</tr>
<tr>
<td>1.0</td>
<td>0.3</td>
<td>1.07</td>
<td>6.53</td>
<td>6.53</td>
<td>*</td>
</tr>
<tr>
<td>0.2</td>
<td>0.06</td>
<td>3.32</td>
<td>1.58</td>
<td>0.316</td>
<td>**</td>
</tr>
<tr>
<td>0.33</td>
<td>0.1</td>
<td>3.08</td>
<td>1.93</td>
<td>0.643</td>
<td>**</td>
</tr>
<tr>
<td>0.67</td>
<td>0.2</td>
<td>2.54</td>
<td>3.06</td>
<td>2.04</td>
<td>**</td>
</tr>
<tr>
<td>1.0</td>
<td>0.3</td>
<td>2.17</td>
<td>3.93</td>
<td>3.93</td>
<td>**</td>
</tr>
</tbody>
</table>

*Vertical tether copper R = 3000Ω dia. = .38 mm
**Vertical tether copper R = 1500Ω dia. = .54 mm
ASSUMPTIONS

- ALUMINUM WIRE DIA. = .67 mm

- THIS KIND OF STRUCTURE CAN BE USED AS EXTERNAL FRAME TO STABILIZE A LIGHT TWO-DIMENSIONAL STRUCTURE (e.g. A REFLECTOR)

<table>
<thead>
<tr>
<th>Case 1</th>
<th>Current (Amp)</th>
<th>Voltage (kV)</th>
<th>T1(N)</th>
<th>T2(N)</th>
<th>Perimeter</th>
</tr>
</thead>
<tbody>
<tr>
<td>h = 2a = 20 km</td>
<td>l = 2b = 40 km</td>
<td>1.130</td>
<td>12.4</td>
<td>1.35</td>
<td>.56</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Case 2</th>
<th>Current (Amp)</th>
<th>Voltage (kV)</th>
<th>T1(N)</th>
<th>T2(N)</th>
<th>Perimeter</th>
</tr>
</thead>
<tbody>
<tr>
<td>h = 2a = 10 km</td>
<td>l = 2b = 20 km</td>
<td>.565</td>
<td>3.10</td>
<td>.339</td>
<td>.141</td>
</tr>
</tbody>
</table>
TRIANGULAR CONSTELLATIONS STABILIZED BY AIR DRAG

*STABILITY ANALYSIS

- ASSUMPTIONS

  ORBITAL ALTITUDE = 500 km
  3-MASS 1000 kg EACH
  BALLOON BALLISTIC COEFFICIENT = 10 m²/kg
  BALLOON DIA. = 100 m

*CONCLUSIONS

A SMALL PITCH ROTATION OF THE
CONSTELLATION MAKES ONE OF THE
INCLINED TETHERS GO SLACK.

<table>
<thead>
<tr>
<th>Constellation Rotation (deg)</th>
<th>h=0.3</th>
<th>h=0.5</th>
<th>h=0.7</th>
<th>h=1.0</th>
<th>h/h</th>
</tr>
</thead>
<tbody>
<tr>
<td>5.</td>
<td>4.42</td>
<td>2.03</td>
<td>1.39</td>
<td>0.95</td>
<td>θ°</td>
</tr>
<tr>
<td>10.</td>
<td>2.22</td>
<td>1.01</td>
<td>0.69</td>
<td>0.47</td>
<td>θ°</td>
</tr>
<tr>
<td>15.</td>
<td>1.48</td>
<td>0.67</td>
<td>0.46</td>
<td>0.31</td>
<td>θ°</td>
</tr>
</tbody>
</table>

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ORIGINAL "FISH-BONE" CONSTELLATIONS ARE STABLE WITH VERY SHORT HORIZONTAL TETHERS (LESS THAN 100 M. AT 500 KM ALTITUDE).

ALTERNATIVE SOLUTIONS ARE QUADRANGULAR DSC's AND ESC's AND, FOR SPECIAL APPLICATIONS, PEC's.

IN ALL OF THEM ROTATIONAL STABILITY IS PROVIDED BY GRAVITY GRADIENT (SUITEABLE MASS DISTRIBUTION) WHILE SHAPE STABILITY IS PROVIDED BY DRAG FORCES OR ELECTRODYNAMIC FORCES.

SUITEABLE DESIGN PARAMETERS CAN PROVIDE GOOD STABILITY WITH A REASONABLY LOW POWER REQUIREMENT FOR ESC's AND FEASIBLE BALLOONS FOR DSC's.

ESC's HAVE A STRONGER TENSION IN THE HORIZONTAL TETHERS THAN DSC's AND AN ORBIT DECAY SMALLER BY AN ORDER OF MAGNITUDE.

ESC's ARE SUITEABLE FOR LOW INCLINATION ORBITS. AN OSCILLATION AROUND THE VERTICAL AXIS AT ORBITAL FREQUENCY IS UNAVOIDABLE BECAUSE ESC's TEND TO KEEP THEIR LONGITUDINAL PLANE PERPENDICULAR TO THE $\vec{B}$ VECTOR.

DSC's CAN FLY AT ANY ORBITAL INCLINATION. THE YAW OSCILLATION SHOWS UP AT HIGH INCLINATION ONLY DUE TO THE EARTH'S ROTATING ATMOSPHERE.
SINGLE-AXIS, VERTICAL CONSTELLATION WITH THREE MASSES

'GOOD STABILITY
'MIDDLE MASS LOCATED AT THE SYSTEM ORBITAL CENTER FOR LOW-G APPLICATIONS
'ORBITAL CENTER IS 1.2 m LOWER THAN THE SYSTEM C.M. IN THE CONSTELLATION UNDER INVESTIGATION
'DESIGN PARAMETERS ADOPTED
- ORBIT ALTITUDE = 500 km
- ORBIT INCLINATION = 28.5°
- TETHER LENGTH = 10 km
- \( m_1 \) (S/S) = 90.6 TON
- \( m_2 \) (BALLAST) = 9.06 TON
- \( m_3 \) (LOW-G) = 4.53 TON

'STATION KEEPING PHASE HAS BEEN SIMULATED
- \( J_2 \) GRAVITY TERM TAKEN INTO ACCOUNT
- TETHER TRANSVERSE MODES NEGLECTED
- LONGITUDINAL DAMPERS NOT INCLUDED IN THE SIMULATION
LOW-G APPLICATIONS, STATION-KEEPING PHASE

IN-PLANE COMPONENT VS. TIME

OUT-OF-PLANE COMPONENT VS. TIME
ACCELERATION LEVEL OF LOW-G PLATFORM PRELIMINARILY ESTIMATED TO BE AROUND $10^{-8}$ g. 

RADIAL COMPONENT, SHOWN IN THE FIGURE, IS THE DOMINATING COMPONENT

SINGLE-AXIS, VERTICAL CONSTELLATIONS APPEAR PROMISING FOR LOW-G/VARIABLE-G APPLICATIONS

HIGH FIDELITY ANALYSIS OF EXTERNAL PERTURBATIONS NECESSARY
PHASE II STUDIES

• Two-dimensional model implemented to study and optimize deployment maneuvers of single-axis vertical constellations with three masses
• Specialized software necessary for parametrical study of deployment
• Study goal is to devise a deployment strategy which minimizes the disturbances (acceleration level) on board the low-G platform
• Same design parameters and orbital characteristics as in station-keeping studies throughout deployment studies

Lagrangian coordinates:
- \( \theta \) = in-plane angle
- \( \xi \) = lateral deflection
- \( t_1 \) = tether length of tether #1
- \( t_2 \) = tether length of tether #2

\( a \) (orbit semi-major axis)
\( x \) (local vertical)
\( \mathbf{k} \) (to the center of the Earth)
SELECTION OF THE DEPLOYMENT STRATEGY

• ASSUMPTIONS
  - NO DAMPERS
  - UNSTRETCHABLE TETHERS
  - INITIAL ALIGNMENT ERROR OF THE THREE MASSES: $\epsilon = 5$ cm

• DEPLOYMENT STRATEGY
  - RATE CONTROL LAW DESIGNED IN ORDER TO KEEP THE MIDDLE MASS AT THE SYSTEM C.M. THROUGHOUT THE ENTIRE MANEUVER
  - LATERAL DEFLECTIONS (AND ACCELERATIONS) OF THE MIDDLE MASS ARE KEPT LOW BY FOLLOWING THE ABOVE MENTIONED STRATEGY
  - WHEN DEPLOYMENT IS COMPLETE THE MIDDLE MASS SHOULD BE MOVED TO THE ORBITAL CENTER

• DETAILS ON THE CONTROL LAW
  - ACCELERATION PHASE (CONSTANT ANGLE)
    \[ l(t) = l_I \exp(\alpha t) \quad 0 < t < t_T \quad \text{(TRANSITION TIME)} \]
  - DECELERATION PHASE
    \[ l(t) = l_I - (l_I - l_T) \exp[-\beta(t-t_T)] \quad t_T < t < t_{SK} \]
    \[ \beta = \alpha \frac{l_T}{(l_I - l_T)} \]
  - ALL THE CHARACTERISTIC LENGTHS ARE IN THE SAME RATIOS AS THE FULLY DEPLOYED TETHER LENGTHS.
(a) Lower Mass $m_1$

(b) Upper Mass $m_3$

Figure 2.4.1 Tether length vs. time. DEPLOYMENT
Figure 2.4.2 Tether speed vs. time. DEPLOYMENT
Figure 2.4.3 Constellation's in-plane angle vs. time. Initial value = 20°.

Figure 2.4.8 Lateral deflection of the middle mass vs. time. Initial value = 0.05 m. DEPLOYMENT
Figure 2.4.5 Trajectory's side view of the lower and upper mass deployment.
Figure 2.4.9 Horizontal acceleration component of the middle mass vs. time for an initial lateral deflection = 0.05 m.

Figure 2.4.10 Vertical acceleration component of the middle mass vs. time for an initial lateral deflection = 0.05 m.
COMMENTS ON DEPLOYMENT SIMULATIONS WITHOUT DAMPERS

- BY MAINTAINING THE MIDDLE MASS AT THE SYSTEM C.M. THE PERTURBATIONS ON IT ARE MINIMIZED DURING DEPLOYMENT.

- THE ACCELERATION LEVEL, HOWEVER, DEPENDS ON THE INITIAL MISALIGNMENT ERROR OF THE THREE MASSES.

- AT THIS STAGE OF THE STUDY DAMPING OF LATERAL OSCILLATIONS APPEARS THE MOST DIFFICULT.

- THE MIDDLE MASS SHOULD BE MOVED TO THE ORBITAL CENTER (ZERO ACCELERATION POINT IN STEADY STATE CONDITION), WHEN THE DEPLOYMENT HAS BEEN COMPLETED.
DAMPING OF VIBRATIONAL MODES

• IMPROVED TWO-DIMENSIONAL MODEL
  - ELASTIC TETHERS
  - LONGITUDINAL TETHER OSCILLATION DAMPERS

• MODIFIED TETHER CONTROL LAW
  - OPTIMIZED ANGULAR FEEDBACK FOR RATE CONTROL LAW
    -- OVERALL LIBRATION CONTROL
    -- EFFECTIVE ALSO IN DAMPING TRANSVERSE OSCILLATIONS

• THE ORBITAL VELOCITY STRONGLY AFFECTS THE IN-PLANE RESPONSE SO THAT
  THE BEST DAMPING CYCLE IS NO LONGER SHAPED LIKE A YO-YO CYCLE.

• THE BEST OSCILLATION CYCLE MAKES THE SATELLITE FOLLOW AN S-SHAPED
  TRAJECTORY WITH DECREASING TETHER LENGTH FOR RETROGRADE TETHER
  LIBRATION.
• TETHER LIBRATION DAMPING ($\theta$)
  - ENERGY DISSIPATED PER CYCLE

\[ E_d = 2 \int_0^\theta \ell (\theta - \Omega) \, d\theta \]

- THE TERM DEPENDING ON $\Omega$ (ORBITAL RATE) IS DOMINATING
- IN ORDER TO HAVE $E_d \gg 0$ A GOOD CONTROL LAW IS

\[ \ell_c = \ell_{sk} (1 - K_s \theta) \quad \text{so that} \quad E_d \approx 2 \ell_{sk}^2 K_s \left[ \int_0^{\theta^2} \Omega^2 \, dt - \int_0^{\theta^3} \, dt \right] \]

• TRANSVERSE OSCILLATION DAMPING ($\epsilon$)
  - ANGULAR FEEDBACK THAT TAKES INTO ACCOUNT THE LATERAL DEFLECTION DAMPS OUT LATERAL OSCILLATIONS

\[ \ell_{c1} = \ell_{sk_1} \left[ 1 - K_{1\theta} (\theta - \epsilon / \ell_1) \right] \quad \text{tether \#1} \]
\[ \ell_{c3} = \ell_{sk_3} \left[ 1 - K_{3\theta} (\theta + \epsilon / \ell_3) \right] \quad \text{tether \#2} \]
• Tether longitudinal oscillation and tether libration have frequencies different by an order of magnitude.

• Simultaneous multi-frequency damping by reel-control is an option. Reel-control tuned in time sharing to frequencies that are to be damped out is another option.

• A longitudinal damper (spring + dashpot) per each tether is probably a simpler solution. This solution is adopted in the following simulations. Each damper is tuned to the respective tether's longitudinal frequency. Critical damping factors are more effective than subcritical ones. Longitudinal dampers strongly reduce the likelihood of slack tether.
MODIFIED DEPLOYMENT STRATEGY + DAMPERS

- Longitudinal dampers active throughout the whole maneuver
- Acceleration phase equivalent to previous deployment (constant angle)
- When tether velocity of phase I matches tether velocity required by rotational damper on, rotational and transverse dampers are switched on
  -- A cosinusoidal transition law is used to match the tether lengths
  -- The rotational damper drives the system to a complete deployment

\[ l_c = l_i \exp(at) \text{ acceleration phase} \]
\[ l_c = l_{sx} \left[ 1 - f_{tr} - k_0(\theta - \epsilon/l) \right] \text{ rotational damper on} \]
\[ f_{tr} = (l_{ftr} - l_{itr}) \cos \left( \frac{\pi}{2} \frac{t}{T_{tr}} \right) \]

- Modified deployment strategy results in a fast maneuver
- The elastic tethers ask for extra care in the initial part of the maneuver
  -- In line thruster recommendable
  -- Present simulations start at a tether length (20 m and 200 m respectively) where the in-line thrusters are supposed to go off
3E-5
-4
E
-6
0
I
O
00 20
00
30
00 4
000 50
0
0
6
00
0
0
70
0
0
9
000 I0000
I
I
000
1
2000
TIM
E (Sec) Longi
L Damper CSI= .9, Deployment

DEPLOYMENT

199
Station-Keeping
STATION-KEEPING

202
- COMMENTS ON DAMPING OF VIBRATIONAL MODES DURING DEPLOYMENT
  - EFFECTIVE WAY OF DAMPING LONGITUDINAL, LATERAL AND SYSTEM LIBRATIONS HAS BEEN DEVISED
    -- DAMPING OF LATERAL OSCILLATIONS REQUIRES A GOOD KNOWLEDGE OF THE THREE-MASS ALIGNMENT
    -- ROTATIONAL ANGLE WITH RESPECT TO THE LOCAL VERTICAL ALSO REQUIRED. A LOWER ACCURACY THAN THAT FOR THE LATERAL DEFLECTION IS NECESSARY.
  - FAST DEPLOYMENT HAS BEEN ATTAINED
  - INITIAL OSCILLATIONS DAMPED OUT IN FEW HOURS SO THAT FINAL ACCELERATION LEVEL ON THE LOW-G PLATFORM IS LOWER THAN THAT ESTIMATED IN THE STATION-KEEPING STUDIES (THE FORCING TERMS ARE INACTIVE THIS TIME).
TECHNOLOGY AND TEST PANEL
APPLICATIONS OF TETHER
IN SPACE WORKSHOP

VENICE, ITALY

OCTOBER 15–17, 1985

TECHNOLOGY AND TEST PANEL
REPORT
October 16th Summary

Either the Technology and Test panel did an outstanding job at the Williamsburg workshop two years ago, or the same people are repeating the recommendations that were made then. In actuality, it is a combination of the two situations because the basic tether technology requirements have not changed nor have the people who were involved in 1983 changed all that much. In fact, the new panel members reinforce the position of the continuing members. As a result of this situation, the panel makes no new recommendation nor does it have any new applications to propose. This position is pending interfaces and inputs from the other discipline panels, but preliminary discussions indicate continuing technology concerns from the other panels also.

The Technology and Test panel spent the day in formal presentations and reviews of the ongoing technology related work. The morning session was spent reviewing the Atmospheric/Aerothermodynamic or tethered "wind tunnel" concept, specifically the TSS-2 proposal, and the Shuttle Tethered Aerothermodynamic Research Facility feasibility/definition study results. The panel endorses this work as an important near-term tether application and recommends an aggressive design and development program. (It was also brought to the panel's attention that a high priority recommendation of the S&A panel was a low atmosphere mission similar to that proposed by STARFAC).

The second technology area reviewed was tether mission (science) and system (engineering) instrumentation. Ongoing studies have concentrated on the definition of instrument requirements for the atmospheric/aerothermodynamic mission but have also touched on general tether applications system performance monitoring and control instrumentation such as satellite positioning laser systems to supplement GPS capabilities, tether temperature, and techniques for failure detection (fiber optic). An instrumentation issue surfaced as a result of a stated requirement for a tensiometer to be located at the satellite during TSS-2 and STARFAC missions to define system drag and support system control and post-flight dynamic modeling and performance analysis. If such a measurement is necessary for TSS-2, why shouldn't TSS-1 also have such a measurement to support similar analysis. As a result of discussions, the panel recommends that the inclusion of such a measurement be studied and implemented if possible.

The morning session was concluded with presentations, by Turci, relative to the status of Aeritalian studies: (1) Tether Pointing Platform, a system similar to that proposed by Lemke of NASA ARC to provide a controlled remote platform for TBD tether application; (2) Tether Space Elevator Mechanism Concepts, the development of which is an enabling technology for Variable Gravity Applications and transportation of platforms and systems along a tether.

The afternoon was spent reviewing various dynamic simulation/mission modeling capabilities. Although SKYHOOK and GTOSS were not formally presented, they were discussed and are considered the base simulation systems at this time.
The question being asked is "Is there a need for a 'universal' simulation capability and, if not, how can mission designs and analyses be regulated and controlled for consistency and reliability?" This subject will be discussed tomorrow, and a recommendation will be made.

Not included in today's summary because of a lack of interested or involved participants (which is probably a result of a lack of activity in the area) was the subject of tether materials and configurations. This lack of activity is of concern to the panel because a recommendation to initiate applications related tether requirements and development studies was made at the Williamsburg workshop. Tether materials and configurations is an enabling technology without which the tether application program cannot mature and evolve.

Tomorrow's activities will center around briefings from Joe Kolecki relative to Electrodynamic Technology and Joe Carol relative to Expendable Tether Capabilities. The latter will provide a method for accomplishing early technology related tether tests, as well as continued tests during the interim years between TSS-1 and TSS-2 which now may be as much as 3 years. Finally, the panel will review its activities and formulate its final recommendations.
TECHNOLOGY & TEST
OCTOBER 16, 1985 SUMMARY

REVIEWED:

- ATMOSPHERIC/AEROTHERMODYNAMIC (TETHERED WIND TUNNEL) CONCEPT
  - TSS—2 PROPOSAL—CARLOMAGNO
  - STARFAC FEASIBILITY/DEFINITION—SIEMERS
  PANEL ADVOCATES CONCEPT/RECOMMENDS CONTINUED DEFINITION
  AND DEVELOPMENT

- INSTRUMENTATION—WOOD
  - SCIENCE FOR ATMOSPHERIC/AEROTHERMODYNAMIC
  - ENGINEERING FOR TSS/TAS
    Tensiometer requirements for TSS dynamics modeling and
    control (?) Major concern relative to instrument
    at satellite

- TETHER POINTING PLATFORM CONCEPT STUDIES—TURCI
  - Technology supporting TAS missions TBD

- TETHER SPACE ELEVATOR MECHANISM CONCEPT (CRAWLER)
  - Enabling technology for variable gravity
  - Enabling technology for transportation along tether
    concepts

- DYNAMIC MODELING
  - "Universal" simulation capability (?)
This is the final oral report of the Technology and Test panel. Whereas the other workshop panels are primarily concerned with the definition of tether applications, the Technology and Test panel's emphasis has been relative to the accomplishment of promising tether applications. It is the opinion of the panel's members that the early definition of the enabling technologies and the initiation of programs required to resolve the tether-related technology issues is critical to the success of the TSS program as well as the growth and maturing of the tether concept. In addition to defining specific tether technology issues, the panel has defined a technology-based application as well as several systems concepts requiring technology development to realize their potential. The technology issues, application, and systems defined are:

1. Tether Requirements/Materials Configuration
2. Tether Dynamics
3. TSS-2 Supporting Technology
4. Shuttle Tethered Aerothermodynamic Research Facility--Application
5. TSS-1/Electrodynamic Tethers
6. Space Elevator--System
7. Tether Pointing Platform--System
8. Time

Technology Issue--Tether Requirements/Materials/Configuration

In spite of a lack of participants with a specific interest in this technology area which concerned the panel, the panel expressed considerable concern relative to the issue with the conclusion that the definition and development of tethers is the singular most critical technology related to the implementation of the tether applications defined to date. It is imperative that the tether characteristics/requirements necessary to accomplish the various proposed applications be defined. One of the ongoing tether technology-related activities which must be continued and expanded is the definition of potential tether environments and the development of tethers that are compatible with that environment. Issues such as temperature, atomic oxygen, ultraviolet and infrared radiation, micrometeoroid impact, and many others must be defined and addressed. An extremely important issue related to the Shuttle Tethered Aerothermodynamic Research Facility tether application is a high temperature tether capable of operating under large loads at temperatures in excess of 1000° K. Another significant tether characteristic that must be defined and will require considerable development is the requirement to be conductive in order to generate or transmit power or provide a communication link between tethered system and parent vehicle.

Another critical design consideration for future tethered applications is the incorporation of tether system redundancy to minimize or eliminate payload loss or parent vehicle damage due to tether damage or failure. A related
technology system recommended for design and definition is a system of instrument capability that would detect tether failure and provide early warning for system safety.

As a result of these tether issues, the Technology and Test panel recommends that (1) NASA and PSN initiate a coordinated program to define tether requirements and a development and test program to evaluate tether concepts and materials, (2) that, because of the importance of this issue and the lack of specific participation relative to this technology issue, a Tether Requirements/Materials/Configuration panel be established for the next workshop to generate interest and activity in the area.

Technology Issue--Tether Dynamics

The panel spent considerable time reviewing tether dynamic simulation capabilities. It is believed by the panel that the development of accurate dynamic simulation/mission modeling capabilities is critical to the acceptance of the tether concept. It is imperative that the dynamic characteristics of TSS-1 and TSS-2 be accurately predicted to ensure the acceptance of the concept. Nothing will do the program more damage than to have the flight dynamics differ from the predictions. With this in mind, the panel expressed concern that there are numerous special purpose simulation capabilities in existence and the number is growing at what seems to be an exponential rate. This lack of control of the dynamic modeling and simulation programs eliminates any basis for program comparison or checking relative to application feasibility studies and mission planning. This lack of a coordinated dynamics/mission simulation capability was of concern to the Technology and Test panel as was an inability, due to environment simulation capability, to generate a test case for evaluation of the various dynamic models. Even the major programs, SKYHOOK and the recently developed GTTOSS, require verification.

As a result of the panel concerns, it is recommended that the existing Tether Dynamics Working Group's activity be expanded to include the design, development, implementation, and review of a dynamics "test case" incorporating the TSS-1 and TSS-2 missions for program verification. Concepts for earlier simulation tests should be seriously studied and considered. The Tether Dynamics Working Group should oversee and provide a peer review function of the results of the "test case" simulation results and, as a result, make recommendations relative to future development of dynamic/mission simulation capabilities as required for tether applications. As with the Tether Requirements/Materials/Configuration issue, the establishment of a Dynamics panel for future workshops is recommended. (As major technology issues evolve into significant work areas, their considerations by the Technology and Test panel is no longer productive except in overview capacity.)

Technology Issue--TSS-2 Supporting Technology Programs

The success of TSS-1 and TSS-2 is critical to the evolution and growth of the tether concept. While the TSS-1 mission will be discussed later, the successful accomplishment of TSS-2 has significant implications to future atmospheric tether missions and related programs. There are several TSS-2
related technology issues which concerned the Technology and Test panel, namely:

Instrumentation
Materials
Aerothermal Analysis
Dynamics
Configuration (Satellite)

The issue of instrumentation relates to the design and development of both the mission control instrumentation; such as, tensiometers, which the panel recommends at each end of the tether for all the TSS missions for dynamic control and post-flight verification, and tether temperature sensing for mission control and tether performance verification as well as science related instrumentation. Relative to the science instrumentation, it is important to note that the TSS-2 mission will operate in a region of the upper atmosphere that imposes peculiar measurement requirements to define molecular species and determine ion and electron concentration at both the satellite surface as well as across the flow field; i.e. Mass Spectrometer and Rayleigh Scattering (laser systems), respectively. While Mass Spectrometers are flight qualified, their design is peculiar to each mission, and laser flow-field profiling is a ground-based capability requiring considerable study prior to flight certification. Finally of concern was the development of heat flux sensors for the satellite and the tether and the need for instrumentation capable of detecting tether failure.

The panel was also concerned about tether and satellite materials. Since the panel is interested in extending TSS-2's operating range (below 130 km altitude), studies relative to both tether and satellite materials that will perform at higher temperatures are recommended. The development of high temperature tether and satellite materials is a prerequisite to the accomplishment of aerothermodynamic research in the free-molecule and transition flow regimes proposed for TSS-2, as well as being of interest and value to the proposed STARFAC missions. These proposed TSS-2 studies are required to define thermal, as well as aerodynamic, design parameters for future atmospheric missions. Preliminary studies indicate rapid increases in tether temperature as well as significant increases in length of tether required to accomplish lower altitude missions. The increased tether requirement occurs as the aerodynamic drag on the tether and satellite approaches the gravity gradient force, and the tether deployment angle deviates significantly from the vertical. These aerothermodynamic phenomena result in requirements for considerable studies relative to tether/satellite dynamics as well as mission studies relative to the deployment, mission operations, and retrieval of the tethered system, specifically relative to communication, tracking and satellite/tether control. The TSS-2 mission, as well as extended capability baseline geometry missions, could significantly contribute to an understanding of the upper atmosphere and upper atmospheric aerothermodynamics.

Finally, the panel expressed considerable concern relative to the mission turn-around time between TSS-1 and TSS-2 and the lack of compatibility of the objectives of TSS-1 and TSS-2 satellite configurations. It is believed that such delays will considerably compromise the impact on the success of the first mission and thereby the potential growth of the concept and its
applications for space station particularly. Consideration should, therefore, be given to the development of two satellites—one for electrodynamic missions and one for atmospheric missions.

The primary recommendation relative to TSS-2 is the initiation of detailed system studies to define the mission limitations of the present TSS configuration and the definition of the modifications, both tether and satellite, required to extend the present capability to lower altitudes. Such studies would include all the previously discussed TSS-2 supporting technology issues.

Technology Issue--Shuttle Tethered Aerothermodynamic Research Facility - STARFAC

This is the Technology and Test panel's proposed tether application and is an extension of the proposals presented relative to TSS-2. STARFAC is a research proposal that would take advantage of the tether concept's peculiar capability to provide in-situ steady-state aerothermodynamic/atmospheric data. The proposal recommends the extension of the TSS-2 capability to an altitude of 90 km. While present studies indicate that a passive TSS-2 configured satellite may be limited to 100 km altitude, the inclusion of negative lift, propulsion, or tether configuration changes, could extend this capability. The supporting technologies as discussed relative to TSS-2 are:

- Instrumentation
- Materials (see Technology Issue--Tether Requirements/ Materials/Configuration)
- Configuration
- Dynamics/Mission Design (see Technology Issue--Tether Dynamics)

The STARFAC proposal extends the research capability to include the transition and possibly slip flow regimes while the TSS-2 is probably limited to the free-molecule regime. This capability expands the studies required to support the development of the enabling technologies.

The panel recommends that studies be initiated as soon as possible relative to mission design and limitation definition, as well as the development and test of required hardware systems with emphasis on instrumentation and high temperature components. These recommendations are complimentary to the TSS-2 recommendations.

Technology Issue--TSS-1/Electrodynamic Technology

The interaction between the Electrodynamic and Technology and Test panels was initiated as a result of concerns expressed by Technology and Test panel members relative to TSS-1 success. The interaction resulted in a "charged" discussion about the success potential of the planned mission. As a result of this discussion, it was jointly agreed, the details of the agreement were included in the Electrodynamic panel's final report as given by Joe Kolecki, "that a plasma contactor (hollow cathode) should be included and operated on the Orbiter during the TSS-1 mission."
For the future of the electrodynamic tether concept, the development of tether conductors and insulators is critical. It is recommended that, as discussed in Technology Issue--Tether Requirements/Materials/Configurations, tether materials receive priority study with significant emphasis on electrodynamic applications. (Electrodynamic and atmospheric high-temperature tether configurations are of particular significance to the tether program because of the TSS program and the near-term potential of these two concepts.) Finally, the success of the electrodynamic tether concept depends on the generation of power in kilowatts which requires the development of high voltage power management and control hardware. (See Electrodynamic panel's report for details.)

**Technology Issue--Space Elevator (Crawler)**

The implementation of many tether applications requires the development of a tether crawler for tether inspection but primarily for the transport of materials and equipment between a space station, for example, and a tethered work station. Such a system capability requires the development of technology and then the design and development of the required mechanisms. The panel encourages continued design effort relative to the Space Elevator (Crawler) concept. Such work is presently underway by Aeritalia.

**Technology Issue--Tether Pointing Platform**

The Tether Pointing Platform is a system proposed by both NASA and Aeritalia for various applications relative to tether controlled operational missions. The Technology and Test panel recommends continued study of this concept leading to feasibility definition and demonstration.

**Technology Issue--Time**

The Technology and Test panel is concerned relative to the timely definition and development of the application's enabling technologies. The development of these technologies must be accomplished to allow the evolutionary growth of the tether concept. Technology will control the future of the tether (second only to dollars).

The only recommendation that can now be made is that the technology related programs discussed be implemented as soon as possible, quickly, NOW!

That concludes the final report of the Technology and Test panel--thank you.
TECHNOLOGY AND TEST

TECHNOLOGY ISSUE:

• TETHER REQUIREMENTS / MATERIALS / CONFIGURATIONS

  • DEFINE TETHER CHARACTERISTICS TO SUPPORT TETHER APPLICATIONS
    
      • REDUNDANCY
      • ENVIRONMENT COMPATIBILITY
      • CONDUCTIVE / NON-CONDUCTIVE
      • HIGH TEMPERATURE
      • TRANSMISSION CAPABILITY
        POWER
        COMMUNICATION
      • FAILURE DETECTION

RECOMMENDATIONS:

• INITIATE COORDINATED NASA/PSN PROGRAM TO DEFINE REQUIREMENTS AND INITIATE DEVELOPMENT AND TEST OF TETHER CONCEPTS AND MATERIALS

• ESTABLISH TETHER REQUIREMENTS / MATERIALS / CONFIGURATION PANEL FOR NEXT WORKSHOP TO GENERATE INTEREST / ACTIVITY
TECHNOLOGY AND TEST

TECHNOLOGY ISSUES:

- ELECTRODYNAMICS
  - TETHER MATERIALS
    - CONDUCTORS
    - INSULATORS
  - POWER MANAGEMENT AND CONTROL
    - HIGH VOLTAGE
  - INCLUSION / OPERATION OF PLASMA CONTACTOR (HOLLOW CATHODE) ON ORBITER DURING TSS—1 MISSION

- SPACE ELEVATOR (CRAWLER)
  - MECHANISM DESIGN AND DEVELOPMENT

- TETHER POINTING PLATFORM
  - CONCEPT DEFINITION
TECHNOLOGY AND TEST

TECHNOLOGY ISSUE:

• TSS-2 SUPPORTING TECHNOLOGY PROGRAMS
  • INSTRUMENTATION
    • TENSIOMETER
    • TETHER TEMPERATURE
    • HEAT FLUX SENSORS
    • FLOW FIELD PROFILING INSTRUMENTS (RAYLEIGH SCATTERING)
    • MASS SPECTROMETER INLETS
    • TETHER FAILURE DETECTION
  • MATERIALS
    • TETHER
    • SATELLITE
  • AEROTHERMAL ANALYSES – THERMAL CONSTRAINTS
  • DYNAMICS / MISSION STUDIES
    • COMMUNICATION
    • TRACKING
    • CONTROL
  • CONFIGURATION (TSS-2 AND TSS-1)

RECOMMENDATIONS:

• DEFINE MISSION PLAN WITHIN CAPABILITIES OF PRESENT CONFIGURATION
• DEFINE MODIFICATIONS REQUIRED TO EXTEND PRESENT CAPABILITY
TECHNOLOGY AND TEST

TECHNOLOGY ISSUE:

- SHUTTLE TETHERED AEROTHERMODYNAMIC RESEARCH FACILITY CONCEPT TO EXTEND ATMOSPHERIC/AEROTHERMO CAPABILITY TO 90 km ALTITUDE

- SUPPORTING TECHNOLOGY
  - INSTRUMENTATION
  - MATERIALS
  - CONFIGURATION
  - DYNAMICS/MISSION DESIGN

RECOMMENDATIONS:

- INITIATE STUDIES RELATIVE TO STARFAC DESIGN DEVELOPMENT AND TEST WITH EMPHASIS ON:
  - INSTRUMENTATION
  - HIGH TEMPERATURE COMPONENTS
TECHNOLOGY AND TEST

TECHNOLOGY ISSUE:

- TETHER DYNAMICS
  - SPECIAL PURPOSE SIMULATION CAPABILITIES ARE NUMEROUS AND GROWING
  - NO BASIS FOR COMPARISON / CHECKING
  - NO COORDINATED DYNAMICS / MISSION STUDY CAPABILITY

RECOMMENDATIONS:

- DEFINITION / DEVELOPMENT OF TSS-1 / TSS-2 DYNAMICS TEST CASE

- EXPAND DYNAMICS WORKING GROUP'S ACTIVITY TO INCLUDE IMPLEMENTATION AND REVIEW OF TEST CASE RESULTS AND PROVIDE PEER REVIEW FUNCTION - RECOMMEND FUTURE DEVELOPMENT FOR TETHER APPLICATIONS

- ESTABLISH DYNAMICS PANEL FOR FUTURE WORKSHOPS AND TAS REVIEWS
TECHNOLOGY AND TEST

TECHNOLOGY ISSUE:

TIME

RECOMMENDATION:

IMPLEMENT TECHNOLOGY RELATED PROGRAMS QUICKLY

(NOW!)
AN EXPERT SYSTEM FOR DEPLOYMENT, RETRIEVAL AND CONTROL OF TETHERED SATELLITES

by

W. Teoh
M.C. Ziemke

The University of Alabama in Huntsville
Huntsville, Alabama 35899

October 1985
ABSTRACT

Within the next few years, there will be a Space Shuttle mission wherein a satellite on a conducting tether will be flown 20 km above the orbiter and a non-conducting tether satellite will be flown 100 km lower than the spacecraft orbit of 200 km to 240 km. These tethered satellites will be deployed by a system consisting of a precisely-controlled winch and an extendable boom-type projector. Once projected a distance above or below the spacecraft, the satellites will begin to feel the effects of the gravity gradient and pull away with increasing force, requiring winch braking to control deployment speed. For satellite retrieval, the winch will require power input. The process of optimum tethered satellite control obtained through braking and/or powering the winch can be rather complex and will require the development of a set of system control laws. This complexity arises from several factors of tethered satellite dynamics. The atmospheric drag on the satellite and its tether will vary with altitude, especially when the lower satellite moves down into the transition flow region below 130 km. It is also believed that the satellite will develop swinging motions which must be damped by precise tugging of the winch. Additional forces on the tether will result from the electrodynamic effects that occur when a current flows along the conducting tether. Other control complications arise from the use of moving subsatellite instrument packages deployed from the spacecraft or from the deployment of a subsatellite from the main tethered satellite.

It is believed that an expert system could be very beneficial to the optimum control of the tethered satellites by the winch and boom. The University of Alabama in Huntsville is currently developing an expert system (called DEX) that can be used for docking maneuvers of the OMV. A similar concept can be used to develop an expert system to control the tethered satellite system's reel and boom mechanism. The use of this expert system can substantially reduce the manpower requirements during the deployment and retrieval of tethered satellites. Additionally, it can maintain a stable configuration in the interim by introducing controlled damping through variation of the tether tension.

Because the only tethered satellite system data available to date is derived from simulation studies, it may not be initially possible to construct a complete knowledge base. Thus, the tethered satellite control laws, sensor signal processing, self-learning and manual over-ride capabilities must be built into this proposed expert system.
TECHNOLOGY AND TEST PANEL

PRESENTATION 1

APPLICATION OF TETHERS IN SPACE

SHUTTLE CONTINUOUS OPEN WIND TUNNEL (SCOWT)

OCTOBER 15-17, 1985

GIOVANNI M. CARLOMAGNO, UNIVERSITY OF NAPLES
LUIGI de LUCA, UNIVERSITY OF NAPLES
PAUL M. SIEMERS, NASA / LaRC
GEORGE M. WOOD, NASA / LaRC
SCIENTIFIC OBJECTIVES

- provide informations relative to the aerodynamic and heat transfer coefficients within the range of the thermo-fluid-dynamic conditions experienced by the satellite during TSS atmospheric flights.

- improve the understanding of the gasdynamic processes occurring downstream of the bow wave standing in front of the satellite.

- implement the knowledge of the chemistry and physics of the upper atmosphere related to satellite aerothermodynamics.

TECHNOLOGICAL OBJECTIVES

- define TSS capabilities with regard to atmospheric flights.

- exploit parallel feasibility studies concerning tether materials, aerodynamic stabilizers etc.

- provide valuable engineering informations on the TSS overall experimental envelope of operation.
MOTIVATIONS

- current wind tunnel technology does not provide reliable thermo-fluid-dynamic data in the combined low Reynolds number and large Mach number regime.

- present computational methods cannot yield the required thermo-fluid-dynamic coefficients because of computational limitations and/or lack of an experimental data base.

- designers who need free-molecule/transition-flow regime data are forced to resort to empirical representations based upon sparse flight data and/or extrapolation of wind tunnel data.

- the research will give preliminary results on the feasibility of a tethered system mainly devoted to aerothermodynamic research.
AIMS

- the present research yields a complete set of measurements within the extended range of flight conditions and/or the long time of operation encompassed by TSS.

- a proper instrumentation allows the execution of "in situ" measurements to characterize the upper atmosphere and provides the data base to develop and validate theoretical models of free molecule/transition flow fields.

- the comparison of computational data with flight measurements can produce a reliable design tool for future flight systems operating in this regime.

- in the first atmospheric mission the molecular mean free path of the free stream will vary by two orders of magnitude. Large variations are also present for temperature, pressure, density, molecular weight and speed ratio.
$\text{Kn} = \text{Free stream Knudsen number}$

$\text{Re}_S = \text{Reynolds number after shock}$

$S = \text{Speed ratio}$
RELATION TO OTHER ONGOING RESEARCH PROGRAMS

- research to define the Orbiter's aerothermodynamics in the free-molecule/transition flow regime is currently sponsored by the Office of Aeronautics and Space Technology (OAST) of NASA as part of the Orbiter Experiment (OEX) program.

- SCOWT is the first step toward development of the Shuttle Tethered Aerothermodynamic Research Facility (STARFAC)

- advanced hypersonic flight systems which operate in the rarefied atmosphere as Aeroassisted Orbiter Transfer Vehicle (AOTV) and Entry Research Vehicle (ERV) are presentely under feasibility study.

- SCOWT supports the development of the computational models required in order to design the above flight systems and to reduce the development time and flight demonstration costs.
INVESTIGATION APPROACH

A comprehensive set of measurements is performed to characterize:

- state vector of the satellite (position, velocity, attitude)

- free stream characteristics (composition, density, etc.)

- satellite/flow field interaction (forces, skin temperatures, heat fluxes, boundary layer composition)
<table>
<thead>
<tr>
<th>CURRENTLY IDENTIFIED MEASUREMENTS</th>
<th>CANDIDATE METHODS UNDER CONSIDERATION</th>
<th>PROJECTED R&amp;D REQUIREMENTS</th>
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<td>GROUND BASED SHUTTLE AND SATELLITE RELATIVE TO SHUTTLE TRACKINGS</td>
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<td>TSS ATTITUDE</td>
<td>3-AXES GYRO-SYSTEM</td>
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<td>TETHER TENSION</td>
<td>3-AXES TENSIOMETER</td>
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<td>SATELLITE ACCELERATION</td>
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<td>INTERNAL TEMPERATURES</td>
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<td>SURFACE TEMPERATURES</td>
<td>CO-AXIAL OR PARALLEL RIBBON THERMOCOUPLES</td>
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<td>HEAT FLUXES</td>
<td>STANDARD SENSORS AS THIN FILMS, CALORIMETERS, ETC.</td>
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<td>FREE STREAM GAS ANALYSIS</td>
<td>FREE STREAM MASS SPECTROMETER</td>
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<td>BOUNDARY LAYER GAS ANALYSIS</td>
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<td>FLOW-FIELD PROFILING</td>
<td>RAYLEIGH SCATTERING, IR, LASER FLUORESCENCE</td>
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</table>
STATE VECTOR OF THE SATELLITE

- the ground based Shuttle tracking and the satellite-relative-to-Shuttle tracking give the TSS Best Estimated Trajectory (BET).

- BET together with the outputs of the 3-axes accelerometer-gyro system give the complete state vector of the satellite (position, velocity and attitude).
DERIVATION OF TSS STATE VECTOR
TENSIOMETER

- the overall force exerted by the tether on the satellite is measured by a three component balance (tensiometer).
- the force measurement together with accelerometer data can provide the fluid dynamic drag.
- in the atmospheric mission the presence of tensiometer on the satellite will give valuable informations on tether dynamics.
TSS ACCELERATION IN TSS STATE
ACCELEROMETERS (Body axes)

TENSIO 
TENSIO 
IETER 
IETER 
 _ 

FREE STREAM 
FREE STREAM 
MASS 
MASS 
SPECTROMETER 
SPECTROMETER 

ACCELERATION IN 
ACCELERATION IN 
INERTIAL AXES 
INERTIAL AXES 

TSS STATE 
TSS STATE 
VECTOR 
VECTOR 

DRAG 
DRAG 
ON TSS 
ON TSS 

DRAG 
DRAG 
COEFFICIENT 
COEFFICIENT 

DERIVATION OF DRAG COEFFICIENT
THERMAL MEASUREMENTS

- internal temperatures can be measured with grounded junction thermocouples. Present in-house thermocouple calibration facilities are adequate without further development.

- surface temperatures can be measured with either co-axial or parallel ribbon thermocouples. An experimental measurements verification program will be performed to insure that the sensors meet the accuracy requirements.

- heat flux measurements can be performed by one of the standards methods selecting the sensor by temperature level and heat rate level and frequencies considerations.
DERIVATION OF CONVECTION HEAT TRANSFER COEFFICIENT
HEAT FLUX MEASUREMENTS

- heat flux sensors must be investigated with regard to their frequency response.

- heat flux sensors generally are bodies whose temperatures are measured at known points.

- four types of one-dimensional heat flux sensors have to be basically considered: thin film ($T_1$); thick film ($T$); wall calorimeter ($T_2$); gradient sensor ($\Delta T$).

- the slab back face can be either insulated (adiabatic; $Q_2=0$) or maintained at a given temperature (in contact with a heat sink; $T_2=0$).

- amplitude and phase lag are dependent on frequency $\omega$ and thermal diffusivity coefficient $\alpha$. 
NOTATION FOR ONE-DIMENSIONAL HEAT FLUX SENSORS

\[
Q_1 = |Q_1| \sin \omega t
\]

\[
T = |T| \sin (\omega t + \phi)
\]

\[
\Delta T = T_1 - T_2
\]

\[
\bar{T} = \int_0^1 T \, dx / L
\]
<table>
<thead>
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<th>Orbiter Altitude (km)</th>
<th>Target Altitude (km)</th>
<th>Tether Length (km)</th>
<th>Satellite Altitude (km)</th>
<th>Tether Temperature (°K)</th>
<th>Tension Orbiter (Newtons)</th>
<th>Deploy Time (Sec)</th>
<th>Orbiter Altitude Maintenance</th>
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<td>220</td>
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<td>95.1</td>
<td>1046</td>
<td>629</td>
<td>15800</td>
<td>None</td>
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</tbody>
</table>
FREQUENCY RESPONSE OF ONE-DIMENSIONAL HEAT FLUX SENSORS (PHASE LAG)
DATA REDUCTION OF MASS SPECTROMETERS MEASUREMENTS
- a "boundary layer" mass spectrometer is being developed to measure the
gas composition and the ratio of neutral to charged molecules and atoms
at the satellite surface (behind the bow wave).

- the instrument is a small double-focussing mass spectrometer projected
to weigh on the order of few kgs.

- to have minimal effects on the flow, an "effusive" inlet is being
developed based on a small disc containing parallel capillaries.
THE DOUBLE FOCUSSING MASS SPECTROMETER

Flow

Effusive inlet

Ion source

Spacecraft wall

Electrostatic lens

Inhomogeneous field magnetic lens

THE EFFUSIVE INLET

Gas flow through the effusive inlet

10^5 capillaries/cm^2

Glass disc

10 μm diameter capillaries
SENSOR FOR CONCENTRATION PROFILE

- With regard to the interaction between the satellite surface and the flow field, the possibility of measuring the concentration profiles in the boundary layer by means of an infrared (IR) concentration profile sensor will be evaluated.

- This study will define boundary layer resolution, spectral bandwidths and level of concentrations which can be measured.

- Alternatively the Rayleigh scattering and the laser fluorescence techniques will be investigated.
TSS - SECTION VIEW
TYPICAL MEASUREMENT LOCATIONS

Legend
FSMS - Free stream mass spectrometer
BLMS - Boundary layer mass spectrometer at TSS surface
- - Surface temperature sensor or heat flux sensor, not on same streamline as any other sensor
<- Housekeeping temperature sensor

Tether to shuttle
Tensiometer

FSMS - Free stream mass spectrometer
BLMS - Boundary layer mass spectrometer at TSS surface

2-4 Q or T channels
on stabilizer
boom and tail

Stabilizer

Legend
FSMS - Free stream mass spectrometer
BLMS - Boundary layer mass spectrometer at TSS surface
- - Surface temperature sensor or heat flux sensor, not on same streamline as any other sensor
<- Housekeeping temperature sensor

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CONCLUSIONS

- SCOWT's primary objective is to perform "in situ" measurements to provide aerodynamic and heat transfer coefficients at the conditions experienced by the satellite during TSS atmospheric flights.

- A complete set of measurements is performed in order to provide the data base to develop and validate theoretical models of free-molecule transition flow fields.

- The research is well related to other ongoing programs such as STARFAC, AOTV and ERV presently being investigated.

- SCOWT supports the development of the models required to design the above flight systems and to reduce development time and flight demonstration costs.
TECHNOLOGY AND TEST PANEL

PRESENTATION II

SHUTTLE TETHERED AEROTHERMODYNAMICS

RESEARCH FACILITY

(STARFAC)

INSTRUMENTATION REQUIREMENTS

OCTOBER 15 - 17, 1985

GEORGE M. WOOD
PAUL M. SIEMERS
SSD / IRD / LaRC

GIOVANNI M. CARLOMAGNO
UNIVERSITY OF NAPLES

JOHN HOFFMAN
UNIVERSITY OF TEXAS - DALLAS
### Typical Physical Properties of the Terrestrial Atmosphere

<table>
<thead>
<tr>
<th>Regions</th>
<th>Altitude km</th>
<th>Temperature °K</th>
<th>Pressure torr</th>
<th>Number Density N/cm³</th>
<th>Mean Molecular Weight</th>
<th>Research Vehicles</th>
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REPRESENTATIVE ATMOSPHERIC DAYTIME ION CONCENTRATIONS

[Graph showing ion concentrations as a function of altitude and temperature]
EQUILIBRIUM AND NONEQUILIBRIUM GAS PROPERTY COMPARISONS FROM AT POINT AWAY FROM THE WALL

Sphere cone at altitude = 58 km; Mach = 14; Angle of attack = 30°

Density, kg/m³

Viscosity, N·S/m²

Velocity, m/sec

Temperature, K

- Equilibrium flow
- Nonequilib. flow, catalytic wall
- Nonequilib. flow, noncat. wall

Distance, cm
STARFAC

AEROTHERMODYNAMIC MEASUREMENTS AND INSTRUMENTATION

- RESPONSIBILITY OF TSS (STARFAC) TECHNOLOGY AND TEST PANEL AT LaRC (SPACE SYSTEMS DIVISION; INSTRUMENT RESEARCH DIVISION)

- DEFINE ENGINEERING MEASUREMENTS NECESSARY FOR CONTROL AND HOUSEKEEPING

- DEFINE SCIENCE MEASUREMENTS NECESSARY TO INVESTIGATE AEROTHERMODYNAMIC ENERGY AND MOMENTUM TRANSFER

- DEFINE INSTRUMENTATION REQUIREMENTS AND ASSESS STATE-OF-THE-ART

- MEASUREMENT ADVISORY PANEL TO INTERFACE AEROTHERMODYNAMIC, ENGINEERING, AND MEASUREMENT SPECIALISTS

LaRC
7/18/85
<table>
<thead>
<tr>
<th>CURRENTLY IDENTIFIED MEASUREMENTS</th>
<th>CANDIDATE METHODS UNDER CONSIDERATION</th>
<th>PROJECTED R&amp;D REQUIREMENTS</th>
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<tr>
<td>SURFACE TEMPERATURE DISTRIBUTION</td>
<td>THERMOCOUPLES</td>
<td>EXTENDED</td>
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<td>HEAT FLUX RATE</td>
<td>THERMOCOUPLES, CALORIMETERS</td>
<td>MODERATE *</td>
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<td>SURFACE PRESSURE DISTRIBUTION</td>
<td>CAPACITANCE, VARIABLE RELUCTANCE</td>
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<td>FREE STREAM GAS ANALYSIS</td>
<td>FREE STREAM MASS</td>
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<tr>
<td>BOUNDARY LAYER GAS ANALYSIS</td>
<td>SPECTROMETER</td>
<td>*</td>
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<td>FLOW-FIELD PROFILING</td>
<td>BOUNDARY LAYER MASS SPECTROMETER</td>
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<td>GAS DENSITY</td>
<td>RAYLEIGH SCATTERING, IR, LASER FLUORESCENCE</td>
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<tr>
<td>BOUNDARY LAYER TRANSITION</td>
<td>PRESSURE, TEMPERATURE, MASS SPECTROMETER MEASUREMENTS</td>
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<tr>
<td>WALL CATALYSIS</td>
<td>PRESSURE, TEMPERATURE MEASUREMENTS</td>
<td>*</td>
</tr>
<tr>
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<td>MASS SPECTROMETER TEMPERATURE MEASUREMENTS</td>
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# STARFAC

## ENGINEERING MEASUREMENTS

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<th>PROJECTED R&amp;D REQUIREMENTS</th>
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<td>Tensiometers, Accelerometers,</td>
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<td>TETHER TEMPERATURE</td>
<td>Reflected Acoustic Wave Propogation</td>
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<td>SATELLITE SURFACE TEMPERATURE</td>
<td>Thermocouples</td>
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<tr>
<td>HEAT TRANSFER RATE</td>
<td>THERMOCOUPLES, CALORIMETERS</td>
<td>*</td>
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<td>SATELLITE INTERNAL TEMPERATURE</td>
<td>THERMOCOUPLES, RADIOMETERS</td>
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<td>DYNAMIC SURFACE PRESSURE</td>
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<td>INTERNAL PRESSURE</td>
<td>THERMOPILE, CAPACITANCE</td>
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<td>ACCELERATION (DRAG)</td>
<td>ACCELEROMETERS, GYROSCOPES</td>
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<td>SATELLITE COORDINATES</td>
<td>LASER RADAR</td>
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<tr>
<td>SATELLITE / STS COMMUNICATIONS</td>
<td>FIBER OPTICS, ELECTRONIC, LASER</td>
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</tr>
</tbody>
</table>

LaRC 7/18/85
TSS-2 FREE STREAM GAS ANALYSIS

Objectives: Quantitatively determine neutral and ionized gas concentrations \((N^0 \approx 10^9, N^+ \approx 10^6/cm^3)\), in order to relate global variations in free-stream composition to TSS-1 operational behavior and to electrodynamic measurements.

Approach: Modify and integrate an existing flight qualified Venus probe high resolution mass spectrometer for TSS use.

Development: Design and fabricate free-stream inlet; minor modification of electronics to optimize operation parameters for TSS mission, incorporate data storage system.
THE DOUBLE FOCUSING MASS SPECTROMETER

Flow

Effusive inlet

Ion source

Spacecraft wall

Electrostatic lens

Ion beam detector plane

Inhomogeneous field magnetic lens

THE EFFUSIVE INLET

Gas flow through the effusive inlet

10^5 capillaries/cm^2

Glass disc

10 μm diameter capillaries
## POTENTIAL NON-INTRUSIVE MEASUREMENT TECHNIQUES FOR HYPERSONIC BOUNDARY-LAYER RESEARCH

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<tr>
<th>Technique</th>
<th>Measurement</th>
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<td>Passive</td>
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<td></td>
</tr>
<tr>
<td>Mass spectrometry</td>
<td>Species concentration</td>
<td>Sampling and collecting, single point measurement</td>
</tr>
<tr>
<td>Thermal emissions</td>
<td>Temperature, species identity</td>
<td>Poor spatial resolution with averaging effect</td>
</tr>
<tr>
<td>Optical</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Rayleigh scattering</td>
<td>Total density</td>
<td>Noise from stray light, particulates, and high fluorescent emissions behind shock</td>
</tr>
<tr>
<td>Raman scattering</td>
<td>Temperature, species concentration</td>
<td>Same as Rayleigh - limited to N$_2$ identification below 52 km, N$_2$ thermometry below 40 km</td>
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## Quantitative Physical Measurements and Candidate Measurement Methods for Aerothermodynamic Studies

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<tr>
<th>Currently Identified Measurements</th>
<th>Candidate Methods Under Consideration</th>
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<td>Surface temperature</td>
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<td>Heat flux</td>
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<td>Internal temperature</td>
<td>Thermocouples, radiometers</td>
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<tr>
<td>Surface pressure</td>
<td>Capacitance, variable reluctance, thermopile</td>
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<tr>
<td>Acceleration</td>
<td>Accelerometers, gyros</td>
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<tr>
<td>Free-stream composition</td>
<td>Free stream neutral/charged particle mass spectrometer</td>
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<tr>
<td>Boundary-layer composition</td>
<td>Boundary-layer neutral mass spectrometer</td>
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<tr>
<td>Density</td>
<td>Pressure, temperature, mass spectrometer measurements</td>
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<td>Flow-field profiling</td>
<td>IR, Rayleigh scattering, laser fluorescence</td>
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<td>Boundary-layer transition</td>
<td>Surface temperature and pressure measurements</td>
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<tr>
<td>Wall catalysts</td>
<td>Determine from mass spectrometer measurements</td>
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</table>
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MEASUREMENT AND INSTRUMENTATION DEFINITION STATUS

- Major engineering and science measurements identified
- Candidate measurement methods identified, but not selected for each, state-of-the-art assessment continuing
- R & D required: All methods will require at least moderate engineering R & D to meet specific TSS requirements
- Data acquisition requirements, use of artificial intelligence, controlled data system, and communications methods being assessed

LaRC
7/18/85
STARFAC

EXAMPLES OF MEASUREMENTS REQUIRING R & D

• TETHER TEMPERATURE DISTRIBUTION - RECENTLY IDENTIFIED REQUIREMENT FOR 100 KM FLIGHT; REFLECTED ACOUSTIC WAVE PROPAGATION BEING CONSIDERED FOR MEASUREMENT

• FLOW FIELD PROFILING - MAJOR LIMITATIONS ARE LOW SIGNAL DUE TO LOW DENSITY ($N=10^{13}$/CM$^3$), REQUIREMENT FOR SMALL, HIGH POWER SOLID STATE LASER AND DETECTOR ARRAYS; RALEIGH OR RAMAN SCATTERING, FLOURESENCE ARE CANDIDATES

• DENSITY AND GAS ANALYSIS - R & D REQUIRED FOR NON-INTRUSIVE, NON-PERTURBING SAMPLE SYSTEMS AND FOR MULTIPLE ION BEAM DETECTOR; CURRENT FLIGHT MASS SPECTROMETER TECHNOLOGY IS ADEQUATE FOR TSS APPLICATIONS

LaRC
7/18/85
TECHNOLOGY AND TEST PANEL

PRESENTATION III

SHUTTLE TETHERED AEROTHERMODYNAMICS

RESEARCH FACILITY

(STARFAC)

OCTOBER 15 - 17, 1985

PAUL M. SIEMERS, LaRC

GEORGE M. WOOD, LaRC

HENRY WOLF, AMA
STARFAC

The Earth's atmosphere from 90 km to 200 km provides the last aerothermodynamics frontier. This atmospheric region is taking on even more significance as man advances into space on a more routine basis with plans for a permanent presence requiring even more extensive capabilities to "fly" in and through this region. Present NASA programs which require but also can provide an understanding of the aerodynamics and aerothermodynamics of the free molecule and transition flows that exist at these altitudes are the Aeroassisted OTV, Entry Research Vehicle and the Tethered Satellite. Each of these programs provides a unique opportunity to do flight research in the rarefied upper atmosphere. However, the Tethered Satellite Program provides, because of its capability to obtain global, in-situ, steady-state data, the greatest potential to:

1. Define the performance of aerodynamic shapes as a function of environmental characteristics (free molecule, transition, slip flow regimes).

2. Define the characteristics of the upper atmosphere and the global variability of properties such as composition temperature, pressure and density.

Such data are required to accomplish the systematic development and verification of analytical prediction techniques required to support advance configuration designs.

LuRC
1/22/85
SHUTTLE TETHERED AEROTHERMODYNAMIC RESEARCH FACILITY

FREE MOLECULE FLOW

TRANSITION FLOW

SLIP FLOW

CONTINUUM FLOW

STARFAC RESEARCH REGION (PROPOSED)

LaRC
1/22/R5
# STARFAC

## PROPOSED RANGE OF ATMOSPHERIC PROPERTIES

<table>
<thead>
<tr>
<th>ALT, km</th>
<th>Temp °K</th>
<th>Pressure, ( P ) \text{ torr}</th>
<th>Density ( \rho ), \text{ kg/m}^3</th>
<th>H.W.</th>
<th>H#P, m</th>
<th>Kn</th>
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<tbody>
<tr>
<td>90</td>
<td>176</td>
<td>1.4\times10^{-3}</td>
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<td>21.30</td>
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</table>
STARFAC

OBJECTIVE

ESTABLISH THE FEASIBILITY OF A TETHERED SATELLITE SYSTEM
CAPABLE OF OPERATING FROM THE SPACE SHUTTLE ORBITER AND
ACCOMPANYING AEROTHERMODYNAMIC RESEARCH AT AN ALTITUDE
BETWEEN 90 KM AND 200 KM
STARFAC

APPROACH:

- DEVELOP OR MODIFY AS REQUIRED A TETHER SYSTEM SIMULATION PROGRAM TO STUDY SYSTEM ELEMENTS RELATIVE MOTION, STABILITY FORCES, TEMPERATURE, DEPLOYMENT, RETRIEVAL, ETC.

- DEVELOP CONTROL LAWS AND LOGIC AS REQUIRED TO MEET STARFAC MISSION OBJECTIVES

- PERFORM SYSTEM TRAJECORY SHAPING STUDIES TO ESTABLISH OPERATIONAL CONSTRAINTS

- PERFORM MISSION SIMULATION TO DEFINE CONCEPT MISSION ENVELOPE

- DEFINE SYSTEM ENGINEERING AND SCIENCE DATA REQUIREMENTS AND ESTABLISH INSTRUMENT DEVELOPMENT REQUIREMENTS

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STARFAC SIMULATIONS

SIMPLIFIED MISSION

• EQUATORIAL, CIRCULAR ORBIT
• SHUTTLE ALTITUDE MAINTAINED
• SPHERICAL 500 kg SATELLITE
• STAINLESS STEEL TETHER, 1 1/2 mm DIAMETER
STAR PAC

TENSION Magnitude newtons

TEMPERATURE Kelvin

TIME ksec

Satellite Ht. = 100 km

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Satellite Ht. = 100 km

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Satellite Ht. = 110 km

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ELLiptical ORBit MISSIONS

- PURPOSE: PROVIDE THERMAL RELIEF FOR TETHER

<table>
<thead>
<tr>
<th>Tether Length (km)</th>
<th>Orbit Parameters (km)</th>
<th>Satellite Altitude (km)</th>
<th>Tether Temperature ('K)</th>
<th>Tension Orbiter (Newtons)</th>
<th>Deploy Time (sec)</th>
<th>Orbiter Altitude Maintenance</th>
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<td>Target</td>
<td>Actual</td>
<td>Perigee</td>
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CONCLUSIONS

- NO THERMAL RELIEF
- REDUCED DATA PERIOD
- TETHER DYNAMICS PROBLEMS

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## STARFAC

### SIMULATIONS

- **INCLINED ORBIT (REAL) MISSIONS**

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<th>Target Altitude (km)</th>
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INCLINED ORBIT SIMULATIONS

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INCLINED ORBIT SIMULATIONS

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INCLINED ORBIT SIMULATIONS

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ORBITER ALTITUDE LOSS VERSUS STARFAC ALTITUDE

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STARFAC
MISSION TIMELINE

TYPICAL MISSION
- DEPLOY TO INITIAL TARGET ALTITUDE
- MAINTAIN SHUTTLE ORBITER ALTITUDE BY CONTINUOUS ΔV MANEUVERS
- ACCOMPLISH MINIMUM OF ONE ORBIT DATA PERIOD
- DEPLOY SATELLITE TO SECOND ALTITUDE
- REPEAT SEQUENCE

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PROCESS MAY BE REPEATED UNTIL ORBITER MAINTENANCE ΔV BUDGET DEPLETED (TBD)

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CONCLUSIONS:

- The feasibility of deploying a tethered satellite to an altitude of 100 km has been established.

- The feasibility of deploying a tethered satellite to an altitude below 100 km is possible but costly.

- The accomplishment of aerothermodynamic research at altitudes between 100 and 200 km is practical.

- Circular shuttle orbits provide optimum mission timelines.

- Missions below 125 km altitude require the development of a high temperature tether.

- Tether missions are limited to orbital speeds.

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RECOMMENDATIONS:

- ACCOMPLISH DETAILED MISSION STUDIES
  - OPTIMIZE SKYHOOK
  - INCORPORATE GTASS
  - TSS BASELINE / MINI-MOD MISSIONS
  - FOREBODY MODIFICATIONS
    - CONICAL
    - RUDDER MODIFICATIONS
      - CONTROL
      - WAKE FLOW
  - DISPOSABLE TETHER MISSIONS
  - AERODYNAMIC (L/D) VEHICLE CONFIGURATIONS
  - PROPULSION AUGMENTED MISSIONS
  - INSTRUMENTATION DESIGN, DEVELOPMENT AND TESTING
  - TETHER DEVELOPMENT
TECHNOLOGY AND TEST PANEL

PRESENTATION IV

TETHER POINTING PLATFORM AND SPACE ELEVATOR MECHANISMS

ANALYSIS OF THE KEY CONCEPTS FOR SATP AND SCALED SATP

OCTOBER 15 - 17, 1985

E. TURCI
AERITALIA
TETHER POINTING PLATFORM AND SPACE ELEVATOR MECHANISMS

Analysis of the key concepts for SATP and scaled SATP

Panel Presentation

Prepared by: E. Turci
AERITALIA GSS: SPACE MECHANISMS LEADER

2nd Applications of Tether in Space Workshops
VENICE, ITALY
OCTOBER - 15, 17 1985
1. TETHER POINTING PLATFORM MECHANISM

1.1 Scope

The idea to control and stabilize the attitude of a platform by means of a movable tether attachment point was proposed in 1984 by Mr. Lemke, L.G., NASA-Ames. Controlled displacements of the attachment point generate torques on the platform providing the stabilization of the roll & pitch axes.

Stabilization accuracy as high as few arcsec is possible if the mechanism realizes precise attachment point displacements with a sufficiently large frequency band response.

Mechanism concepts and technological solutions are given here for a scaled SATP; the proposed configurations assume the following main constraints:
TETHER POINTING PLATFORM MECHANISMS

<table>
<thead>
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<th>Item</th>
<th>Specification</th>
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<tr>
<td>Tether Tilt Angle</td>
<td>±4 deg.</td>
</tr>
<tr>
<td>Pointing Area in X Y Plane</td>
<td>± 2 cm</td>
</tr>
<tr>
<td>Position Accuracy</td>
<td>&lt; 0.1 mm</td>
</tr>
<tr>
<td>Response Frequency Band</td>
<td>Max. Obtainable</td>
</tr>
<tr>
<td>Operative Lifetime</td>
<td>Limited to One Month</td>
</tr>
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1.2 Candidate Concepts

The concepts evaluated in this study are described by the following sketches of fig 1.

Fig. 1 tethered pointing platform mechanism concepts a), b), c).

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1.2 CANDIDATE CONCEPTS

The concepts evaluated in this study are described by the following sketches of Fig. 1:

FIG. 1 TETHERED POINTING PLATFORM MECHANISM CONCEPTS a), b), c)
TETHER POINTING PLATFORM MECHANISMS

**Concept A** - The position of \( P \) is controlled by the rotations \( \theta_1, \theta_2 \) (hinges of the arms \( l_1, l_2 \)).

The relationship between the commanded Cartesian coordinates \( x_p, y_p \) and the rotations \( \theta_1, \theta_2 \) is:

\[
\begin{align*}
    x_p &= l_1 \cos \theta_1 + l_2 \cos \theta_2 \\
    y_p &= l_1 \sin \theta_1 + l_2 \sin \theta_2
\end{align*}
\]

Rotations, \( \theta_1, \theta_2 \), controlled by \( M_1 \) and \( M_2 \), are trigonometric functions of the Cartesian coordinates.

The drawback of the concept is a too high inertial load of \( M_1 \).

**Concept B** - An improvement of A) where \( M_2 \) motor is axially aligned with \( M_1 \); the improvement minimizes the inertial load of \( M_1 \) due to \( M_2 \) but does not avoid heavy arms and very tight ball bearing assemblies due to cantilever arms. The toothed gears \( g_1, g_2 \) generate further pointing errors.

Motor, control unit is complex and generates errors due to trigonometric algorithms.
TETHER POINTING PLATFORM AND SPACE ELEVATOR MECHANISMS

Concept C) Utilizes a completely different approach. Motors M1, M2 control directly azimuth and elevation of the tether attachment point P; cantilever is avoided; the inertial loads on the rotation axes are minimized. Commands, signals are given in polar coordinates; trigonometric algorithms are no more necessary.
1.3 Baseline Concept-Description

Concept c) has been assumed as baseline and analyzed - the engineering drawings in Fig. 2 illustrate the configuration and the layout.

Identical rotary actuators control azimuth and elevation angles (standardization).

Both actuators consist of: motor, synchro, optical encoder.

The elevation actuator is axially aligned with the azimuth one so as to minimize its inertial load.

Irreversible gear couplings (worm & wormgear - sprocket toothed sector) provide a full range of tilt elevation angles when the motor turns a full rotation: the response time can be designed identical on both channels. The overall assembly is rugged so to ensure good accuracies; backlash is minimized or made null.
Fig. 2 Tether pointing platform mechanisms
1.4 Baseline concept-control analysis

The control block diagram for the azimuth channel is illustrated in Fig. 3.
Temporal responses to step commands are given (computer simulations) in Fig. 4 and 5 without and with lead/lag filter.
The motor has been assumed to be a D.C. brushed motor, the angular transducer a plastic film potentiometer and the speed feedback to be an ideal derivative function.
TETHER POINTING PLATFORM AND SPACE ELEVATOR MECHANISMS

\[ A_1/A_2 = 100 \]
\[ K_m = 4.9 \times 10^{-2} \text{ Nm/V} \]
\[ K_v = 3.72 \times 10^{-2} \text{ V} \cdot \text{s/\text{rad}} \]
\[ K_\theta = 118 \text{ V/\text{rad}} \]
\[ J = 10^{-4} \text{ kg} \cdot \text{m}^2 \]
\[ \tau_m = 17.3 \text{ ms} \]
\[ \tau_1 = 20 \text{ ms} \]
\[ \tau_2 = 2 \text{ ms} \]

FIG. 3 AZIMUTH CHANNEL CONTROL BLOCK DIAGRAM
The system has a very high time constant so it is necessary to use the filter. If we assume $\tau_1 = \tau_m$, we would only have a lag as high as $\tau_n$, but this procedure would cause unchecked modes.

It is so better to use an higher lead $\tau$, and a very little $\tau_2$.

In this way the system response is the following:

---

**FIG. 5** - Response with lead/lag filter
It is so possible to evaluate the transient without or with the lead/lag filter simply imposing respectively $\tau_1 = \tau_2 = 0$ or $\tau_1 = 20 \text{ m sec}$ and $\tau_2 = 2 \text{ m sec}$.

The response without the filter is shown in fig. 4.

FIG. 4 - Response without lead/lag filter
1.5 Baseline concept- components and technologies

To meet the torque requirements, a brushed samarium cobalt D.C. (14 cm.N) torque motor is mandatory; the feedbacks can be obtained in different ways.

ANGULAR TRANSDUCERS

- PLASTIC FILM POTENTIOMETER
- SYNCHRO
- OPTICAL ENCODER
- ELECTRONIC DERIVATE OF THE D.C. ANGULAR SIGNALS.

The most simple solution utilizes: potentiometer and electronic derivate. All controls are in D.C. The drawback is constituted by the non controlled angles of the potentiometer at its extremities.
The more accurate solution utilizes: synchro and optical encoder.

This solution requires a more sophisticated electronic and probably gives higher response times.

The dwg. in fig.2 utilizes synchro and a flat disc optical encoder feedbacks.
2. SPACE ELEVATOR MECHANISM FOR SCALED SATP

2.1 Scope

A moving elevator along a tether deployed to a fixed length has been already proposed in the frame of system studies as a space station facility. The concept proposed in this chapter is referred to a scaled SATP where the tether interaction length is limited to 1.0 (approx. meter), the tether is made of Kevlar (ϕ ~ 2 mm) and the interaction max. force is 10 N. The elevator will be hooked to the tether by means of the RMS of the shuttle. The speed range is zero to 1.0 meter/second or more, if possible. The movement has to be smoothed and controlled by programmed speed profiles. The operative lifetime is limited to one month.
2.2 Candidate concepts

The idea to drag the tether gripping it between two rotating wheels has been evaluated because of its simplicity.

A design approach, on the other side, requires investigation on friction between the tether (KEVLAR, Ø ~ 2 MM) and the material (rubber) covering the wheels.

In Fig. 6 test set-up and test results are given.

Utilizing the measured coefficient of friction, a preliminary design has been done. The concept is considered the baseline for the scaled SATP, while other solutions proposed for the SATP (next chapter) will be considered appropriate configurations also for the scaled one.
FIG. 6

Test set-up for friction measurement and test results.

\[ f = \tan \alpha \approx 0.5 \]

Tether sample (Kevlar)

Wheels covered with rubber

\[ D = 120 \text{ mm} \]
TETHER POINTING PLATFORM AND SPACE ELEVATOR MECHANISMS

FIG. 6
TEST SET-UP FOR FRICTION MEASUREMENT AND TEST RESULTS
2.3 Scaled SATP baseline concept description

Looking at Fig. 7 we can see that the active wheel is rotated by a brushed samarium cobalt D.C. torque motor (redundant for reliability reasons), the speed control is realized by a tachogenerator. The torque is measured by a piezo-electric torque/axial force transducer. The wheel is covered by a strip of appropriate friction material (rubber). The pressure of the active wheel on the passive one is controlled by a second (linear) actuator utilizing a screw and a spring; the pushing force is measured by a similar torque/axial transducer. The rotation of the screw is controlled by (redundant) brushed D.C. torque motors, the feedbacks are: tachogenerator and piezo-electric transducer. An electromagnetic clutch is also foreseen; the windings are redundant (for reliability reasons).
FIG. 7 - SPACE ELEVATOR MECHANISM FOR SCOLED SATP
TETHER POINTING PLATFORM AND SPACE ELEVATOR MECHANISMS

If slippings occur, the torque transducer evidences the event and an increase of pushing force is commanded to the linear actuator. The signals from the piezo-electric transducers and from the tachogenerators will be used also as monitors.

2.4 Scaled SATP baseline concept - components and technologies

An alternative solution to the brushed redundant D.C. motors is the brushless synchronous torque motor (with redundant winding and redundant E.C.U.). This machine requires the use of a rotor position encoder (hall sensor encoder) and three phase bridge commutation circuit (three phase configuration). The switches are operated sequentially at intervals according to the signals generated by the magnetic encoder. This solution looks too complicated for the scaled SATP when the operative life is of the order of one month. In alternative to the piezo-electric transducers strain gauges can be used.
3. SPACE ELEVATOR MECHANISM FOR SATP

3.1 Scope

This space station facility requires a specific concept as the main requirements are completely different from the scaled SATP. In fact, the tether has a diameter of \(~ 17\) mm, the interaction max. force is \(~ 150\) N, the elevator mass is (probable of) \(~ 5\) tons, and the operative lifetime is, as minimum, an order of magnitude longer than the scaled one.
3.2 SATP ELEVATOR BASELINE CONCEPT DESCRIPTION

The concept described in Chap. 2.3 cannot be used on SATP, for, as minimum, two reasons:
- The dragging force is so high that the gripping between the two wheels can damage the tether.
- The surface of contact between the two wheels and tether is too limited and slipping events cannot be avoided.

The concept proposed in this paragraph will ensure an uniform surface of contact utilizing two endless toothed belts dragging the tether along a linear length. The belts are pressed by sliding blocks. Fig. 8 describes clearly the concept: the rotary actuator utilizes two redundant D.C. brushed torque motors of 0.92 Nm and tachogenerator, or a single synchronous, brushless torque motor with redundant windings and ECU; the gear coupling (worm & wormgear) ensures irreversibility of
TETHER POINTING PLATFORM AND SPACE ELEVATOR

The rotations, the sliding blocks press the tether with controlled forces utilizing a linear actuator similar to the proposed in the scaled concept. A torque transducer assembled on the active wheel measures the dragging providing a proportional control of the sliding block pressures.

If further analysis or more detailed requirements will reject the sliding blocks because of the wear and debits, an array of needles can be used satisfactory (see part, Fig. 8b).

Accurate evaluation of the toothed belt technology has still to be done; anyhow, metal tapes or Posidrive belts made of Neoprene with the teeth covered by nylon, internally reinforced with metallic cables can be used.

Details of the design and the technologies are represented in Fig. 8b.
FIG. 8a- SATP ELEVATOR MECHANISM (TOOTHED BELT CONCEPT)
1 - belt
2 - needle sliding block
3 - needles assembly
4 - linear actuator
5 - toothed pulley
6 - torque transducer

FIG. 8 B - SATP ELEVATOR MECHANISM - DETAILS AND TECHNOLOGIES
3.3 SATP Elevator-robotic concept description

The possibility to drag the tether utilizing two pincers and an alternative linear motion has been investigated. The concept is described in Fig. 9a.

Two long screws with recirculating ball bearings drive, in both directions, two pincers. The pincer grasps the tether and drags it along the screw while the second one (open) returns to its initial position. Continuity of the motion is ensured by a contemporary dragging of both pincers for a while under controlled identical speeds, when at the end of its stroke, the pincer opens, the other one starts its strokes having completed the inversion of motion and initial transitory.
FIG. 9

ASTP ELEVATOR ROBOTIC CONCEPT CONFIGURATION AND PINCER
The pincer is described in Fig. 9 (b). Opening/closure operations are realized by a small d.c. brushless torque motor, the grasping by an electromagnet; current is controlled by the dragging force measured by a piezo-electric transducer (or strain-gauges) (Fig. 10). When a slipping event arises, an increase of current is commanded to the electromagnet. The sleeping events are taken by a pick-off (differential transformer) located inside the two jaws grasping the tether.
TETHER POINTING PLATFORM AND SPACE ELEVATOR

**FIG. 10**

**Electromagnet, Jaws grasping the Tether with measurement transducers**

- Electromagnet

Grasping assembly with

p-e = piezo-electric force transducer,

Jaws, differential transformer for slipping
SATP Elevator - Electromagnetic Propulsion Concept Description

The possibility to drag a mass of 500 kg (elevator) along a tether of 17 mm diameter exchanging a max. force of 150 N with a max. speed of few meters / per second utilizing electromagnetic forces has been evaluated.

The investigated concept utilizes the force of a core immersed in a magnetic field created by a coil.

The formula of the force is: \( F = \frac{1}{2} I \frac{dL}{dx} \) where \( \frac{dL}{dx} \) is the variation of the induction due to the core movement inside the coil. \( I \) is the current of the coil.

In Fig. 11 is indicated the behaviour of a core moving inside a coil.

\[ V \quad \rightarrow \quad F \quad \rightarrow \quad V \quad \rightarrow \quad F = 0 \quad \rightarrow \quad V \quad \rightarrow \quad F \]

\[ \frac{dL}{dx} > 0 \quad \left\{ \frac{dL}{dx} = 0 \right\} \quad \frac{dL}{dx} < 0 \]

Fig. 11
THE FORCE ACTING ON A CORE IMMERGED IN A SINGLE COIL INCREASES AND INVERTS ITS DIRECTION WHERE CROSSING THE COIL.

THE REALIZATION OF A HIGH MEAN FORCE AND MINIMUM RIPPLE IS POSSIBLE IF:

- MANY COILS ARE USED: THE COILS HAVE TO BE OPPORTUNELY OUT OF PHASE IN REFERENCE TO THE CORE POSITIONS.
- COILS ARE SWITCHED OFF WHEN CORES CROSS THE COILS: THIS AVOIDS BRAKING FORCES
- A SWITCHING PROCEDURE IS USED: IN SUCH A WAY TO REALIZE A CONTINUOUS MOVEMENT IN BOTH SENSES.

FIG. 12 - GEOMETRICAL ARRANGEMENT OF THE COILS AND CORES

- coil switches on: 2
- coils already on: 4, 6, 8, 10, 12, 14, 16, 18, 20, 22, 24, 26, 28, 30
- coils already off: 1, 3, 5, 7, 9, 11, 18, 15, 17, 19, 21, 23, 25, 27, 29, 31
- coil switches off: 32

N = 32

l = 14/16 l
l' = 19/16 l
K = 16
The dimensions of the coil package are dependent on many parameters, anyhow a congruent set of values is indicated in Fig. 13 where 

\[ H = 2.0 \text{ m}, \quad D = 6.25 \text{ cm}, \quad \phi = 21 \text{ mm}, \quad \ell_s = 6.25 \text{ cm} \]

**Fig. 13** Coil package layout
The tether section including electrical cables, cores, and structural skin is sketched in Fig. 14.

**Fig. 14  Tether Section**

The dynamic behaviour can be investigated utilizing the formula:

\[ F_T(y) - F = M_{elev} \frac{d^2y}{dt^2} \quad \delta \leq y \leq (\delta + \delta^*) \]

If \( F = 150 \, \text{N} \), \( M_{elev} = 5000 \, \text{kg} \)

The propulsive force \( F_T(y) \) is variable inside the limits

\( F_{\text{min}} = 160 \, \text{N} \), \( F_{\text{max}} = 267 \, \text{N} \)  

The current in the coils is \( I = 5.34 \, \text{A} \) and the total electric power is 2860 W, where the mechanical power is \( P_m = 150 \, \text{(N)} \times 5 \, \text{(m/s)} = 750 \, \text{W} \). Cooling of the coils results necessary.
TECHNOLOGY AND TEST PANEL

PRESENTATION V

THE DEVELOPMENT OF OPTIMAL CONTROL LAWS
FOR ORBITING TETHERED PLATFORM SYSTEMS

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The Development of Optimal Control Laws for Orbiting Tethered Platform Systems

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THE DEVELOPMENT OF OPTIMAL CONTROL LAWS
FOR ORBITING TETHERED PLATFORM SYSTEMS

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A mathematical model of the open and closed loop in-orbit plane dynamics of a space platform-tethered-subsatellite system is developed. The system consists of a rigid platform from which an (assumed massless) tether is deploying (retrieving) a subsatellite from an attachment point which is, in general, offset from the platform's mass center. A Lagrangian formulation yields equations describing platform pitch, subsatellite tether swing, and varying tether length motions. These equations are linearized about the nominal station keeping motion. Control can be provided by both modulation of the tether tension level and by a momentum type platform-mounted device; system controllability depends on the presence of both control inputs. Stability criteria are developed in terms of the control law gains, the platform inertia ratio, and tether offset parameter. Control law gains are obtained based on linear quadratic regulator techniques. Typical transient responses of both the state and required control effort are presented.

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INTRODUCTION

The Smithsonian Astrophysical Observatory\(^1\) proposed the Shuttle based "Skyhook" concept consisting of a tether of approximately 100km length to be deployed from the Shuttle Orbiter and transporting at its end a subsatellite experimental package. The subsatellite could be deployed either above or below the Shuttle for purposes of conducting a variety of upper atmospheric experiments; an in-orbit demonstration of the tethered satellite system could occur as early as 1987.\(^2\)

The analyses of the dynamics and control of the tethered subsatellite system (TSS) has been performed by a host of investigators; a recent survey article by Misra and Modi\(^3\) describes over sixty papers treating various aspects of tether (or cable) connected orbiting two-body systems. A preliminary treatment of the TSS system was addressed by Rupp\(^4\) who assumed that motion was restricted to the orbital plane and neglected the tether mass. A tether tension station keeping control law was proposed such that the tension would vary as a linear function of the tether line length, rate of change of length, and desired (commanded) length. For deployment/retrieval the commanded length could be varied according to a prescribed function of time. Subsequently, the three dimensional dynamics and control including the inertia effect of the tether mass and aerodynamic forces (and heating) on the tether and subsatellite was treated. It was noted that for local vertical station keeping, within the linear range, tether tension would not provide control of the out-of-orbit-plane swing motion (roll), but such control would be implemented in the non-linear system due to higher order coupling\(^5\), or by including nonlinear feedback terms in the tension control law.\(^6\)

Bainum and Kumar\(^7\) introduced a new tether tension control law (for a massless tether) where the tension was assumed to vary as a linear function of the in-plane length and angular variational coordinates and their rates based on an application of linear optimal control theory. By proper selection of the state and control penalty matrices it was possible to obtain faster responses with no increase in power levels during station keeping as compared with alternate control strategies. As an extension to this Diarra\(^8\) showed that the effect of a massive but taut tether is to reduce the stability region in the
parametric space formed by the optimal control gains of Ref. 7.

Advanced space platform-based applications of the tethered satellite system were recently described by Laue and Manarini. As an autonomous subsystem it could be used to deploy and recover payloads from the platform with advantages of higher payload mass and longer mission durations than would be possible with the original Shuttle based systems. Another application of tethered-platform systems could involve tethers attached to astronauts who would be servicing experiments which are designed to function at a pre-set distance from the platform monitoring deck.

The objective of the present paper is the development of a mathematical model for an advanced space platform-based application of the TSS and the synthesis of appropriate control laws based on an application of optimal control theory. To the authors' knowledge this is the first such development of a mathematical model based primarily on tethered-platform applications.

DEVELOPMENT OF THE SYSTEM EQUATIONS OF MOTION

The system is idealized as containing a rigid platform from which an assumed (massless) tether is deploying or retrieving a subsatellite (Fig. 1) at a distance, l, from a point on the platform which is offset by a distance, h, from the platform's mass center. The point of tether attachment is assumed to be along the platform's roll axis (h>0). The tether is considered to be massless and remains taut for all subsatellite motion.

For this study the mass of the subsatellite is assumed to be significantly less than that of the platform. Therefore, the composite system center of mass can be assumed to be coincident with the platform center of mass and shifts in the composite center of mass can be neglected.

Only the platform pitching motion and the subsatellite motion in the orbit plane will be
Considered. Environmental disturbances such as solar pressure, aerodynamic drag and torques, and the dynamic effects due to the earth's oblateness are considered to be negligible.

A Lagrangian formulation is used to derive the system equations of motion. Figure 1 illustrates the system geometry. The body axes $\hat{e}_x, \hat{e}_y, \hat{e}_z$ coincide with the platform principal axes of inertia. The transformation between the body frame of reference and the orbit frame of reference is given by, $\mathbf{R} = \mathbf{R}_o + \mathbf{l}$

\[
\begin{bmatrix}
\mathbf{R}_x \\
\mathbf{R}_y \\
\mathbf{R}_z
\end{bmatrix} =
\begin{bmatrix}
\cos \psi & 0 & -\sin \psi \\
0 & 1 & 0 \\
\sin \psi & 0 & \cos \psi
\end{bmatrix}
\begin{bmatrix}
\mathbf{R}_x \\
\mathbf{R}_y \\
\mathbf{R}_z
\end{bmatrix}
\]

where $\hat{e}_x, \hat{e}_y, \hat{e}_z$ are orbit frame axes, with $\hat{e}_z$ in the direction of the local vertical and $\hat{e}_y$ normal to the orbital plane. The angle $\psi$ describes the orientation of the platform with respect to the local vertical. The position vector describing the location of the subsatellite is

\[
\mathbf{R} = \mathbf{R}_o + \mathbf{l}
\]

Equation (2) may be further developed as:

\[
\mathbf{R} = -(R_0 \sin \psi + h + l \sin \theta) \hat{e}_x + (R_0 \cos \psi + l \cos \theta) \hat{e}_y + (R_0 \sin \psi + h) \hat{e}_z
\]

where $R_o$ represents the distance between the center of the earth and the platform center of mass and $l$ represents the length of the tether line. The distance, $h$, is the tether attachment offset from the platform center of mass. The angle, $\theta$, represents the angular displacement of the tether line relative to a local normal in the platform.

The subsatellite velocity is

\[
\dot{\mathbf{R}} = \dot{\mathbf{R}}_o + \dot{\mathbf{l}}
\]
which, after expansion takes the form:

\[ \ddot{R} = \left[ -l \dot{\theta} + \Theta \dot{c} \theta \right] + (\ddot{\psi} + \dot{\omega}) l c \theta + R_\omega c \psi \right] + \left[ (\dot{\nu} - \dot{\theta} l s \theta) - (\ddot{\psi} + \dot{\omega}) (h + l s \theta) + R_\omega s \psi \right] \eta \]

where \( \omega \) is the orbital rate of the platform.

The total system kinetic energy can be represented in terms of the platform and subsatellite components:

\[ T = T_p + T_s = T_p + \frac{1}{2} m (R \cdot R) \]  

Expansion of Eq. (6) yields:

\[ T = (1/2) \left[ I_\zeta (\ddot{\psi} + \omega)^2 + M \omega^2 R_\omega^2 \right] + m [\dot{\phi}^2 + \dot{\theta}^2 l^2 \]

\[ - 2(\ddot{\psi} + \omega) \dot{\phi} l^2 + 2 i \dot{\phi} \omega s (\psi - \Theta) - 2 \dot{\phi} R_\omega l \omega c (\psi - \Theta) + i^2 (\ddot{\psi} + \omega)^2 \]

\[ + R_\omega^2 \omega^2 + 2(\ddot{\psi} + \omega) R_\omega l \omega c (\ddot{\psi} - \Theta) + (\ddot{\psi} + \omega)^2 (h^2 + 2 i h s \theta) \]

\[ + 2(\ddot{\psi} + \omega) h R_\omega s \psi + 2(\ddot{\psi} + \omega) h \dot{\nu} c \theta - 2(\ddot{\psi} + \omega) \dot{\theta} h \theta s \theta \]

where \( M \), \( m \), and \( I_\zeta \) are the platform mass, subsatellite mass, and platform pitch principal moment of inertia, respectively.

The subsatellite potential energy is given by:

\[ V_s = -G M_\omega m / |\vec{R}| \]  

where \( G \) and \( M_\omega \) are the Universal gravitational constant and mass of the Earth, respectively.
Substitution of Eq. (3) into Eq. (8) yields,

\[ V_s = -\frac{GM_om}{R_o} \left[ R_o^2 + h^2 + \ell^2 + 2\ell hs\theta \right] + 2R_o hs\psi + 2R_o \ell c(\psi-\theta) \right]^{-1/2} \]

(9)

Equation (9) can be rewritten as:

\[ V_s = -\left(\frac{GM_om}{R_o}\right) \left[ 1 + \frac{(h^2 + \ell^2 + 2\ell hs\theta)}{R_o} \right]^{-1/2} \]

\[ + 2 \left( \frac{hs\psi + \ell c(\psi-\theta)}{R_o} \right) \]

(10)

Because \( h^2, \ell^2, \) and \( \ell h \ll R^2 \) the expansion of certain components of the second term inside the bracket yields higher order terms as compared with the remaining terms. With the binomial expansion, retaining terms of order \((h/R)^2\), etc. from the brackets,

\[ V_s = -\left(\frac{GM_om}{R_o}\right) \left[ 1 - \frac{(hs\psi + \ell c(\psi-\theta))}{R_o} \right] \]

\[ -\left(\frac{h^2 + \ell^2 + 2\ell hs\theta}{(2R_o)^2}\right) \]

\[ + \left( \frac{3/2}{R_o} \right) \left[ h^2 s^2 \psi + 2hs\psi c(\psi-\theta) + \ell^2 c^2(\psi-\theta) \right] \]

(11)

Based on Kepler's third law

\[ \omega^2 = \frac{GM_o}{R_o^3} \]

and

(12)

therefore, Eq (11), becomes

\[ V_s = -\omega^2 m \left[ R_o^2 - hR_o \psi - \ell R_o c(\psi-\theta) - \left( h^2 + \ell^2 + 2\ell hs\theta \right)/2 \right] \]

\[ + \left( \frac{3/2}{R_o} \right) \left[ h^2 s^2 \psi + 3hs\psi c(\psi-\theta) + \left( \frac{3/2}{R_o} \right) \ell^2 c^2(\psi-\theta) \right] \]

(13)

The platform potential energy is denoted by,

\[ V_p = -GM_om/R_o + \left( \frac{3/2}{\omega} \right) s^2 (I_\eta - I_\xi) \]

\[ (s^2\psi - 1) \]

(14)

Where \( I_\eta \) and \( I_\xi \) are the platform yaw and roll principal moments of inertia, respectively. The second term represents the effects of a distributed massive rigid body under the influence of a gravitational gradient. The total system potential energy is a combination of the platform and subsatellite contributions as given in Eqs. (14) and (13),

\[ V = V_p + V_s \]

(15)
The general form of Lagrange's equations

\[
\frac{d}{dt} \left( \frac{\partial T}{\partial q_i} \right) - \frac{\partial T}{\partial q_i} + \frac{\partial V}{\partial q_i} = Q_i \tag{16}
\]

will be considered for the generalized coordinates: \( q_i = l, \theta, \psi \); where \( Q_i \) is the corresponding generalized force. Application of Eqs. (16) renders independent equations for each of the three generalized coordinates. After substitution and expansion these equations are:

**Length \((l)\) equation**

\[
\ddot{l} + \psi h c \theta - ((\dot{\psi} - \dot{\theta}) + \omega) 2l - (\dot{\psi} + \omega)^2 h s \theta \\
+ \omega^2 l (1 - 3c^2 (\psi - \theta)) + \omega^2 h s \theta - 3 \omega^2 h s \psi c (\psi - \theta) = \frac{Q_l}{m}
\]

**Swing angle \((\theta)\) equation**

\[
(\ddot{\theta} - \ddot{\psi}) + 2 \left( \frac{l}{h} \right) \left[ (\dot{\theta} - \dot{\psi}) - \omega \right] \ddot{\psi} \left( \frac{h}{l} \right) \theta \\
- (\dot{\psi}^2 - 2 \omega \dot{\psi})(h/l) \theta - 3 \omega^2 (h/l) \psi \theta (\psi - \theta) \\
- (3/2) \omega^2 s (2(\psi - \theta)) = \frac{Q_{\theta}}{m l^2}
\]

**Pitch angle \((\psi)\) equation**

\[
\ddot{\psi} + (3/2) \omega^2 l^2 s^2 + (m/I_\perp) (-2h(\dot{\psi} - \dot{\theta}) + \omega^2 c \theta \\
+ (\ddot{\psi} - \dot{\theta}) h s \theta + \ddot{\psi}^2 + l h c \theta + 2h (\dot{\psi} - \dot{\theta}) s \theta \\
- (3/2) \omega^2 h^2 s^2 - \omega^2 h c \theta (2(\psi - \theta)) - \omega^2 h c \psi (\psi - \theta) - \frac{Q_\psi}{I_\perp}
\]
where 
\[ \lambda^2 = \frac{(I + I)}{I} \eta \xi \zeta \]

**NON-DIMENSIONALIZATION OF SYSTEM EQUATIONS OF MOTION**

The offset parameter, tether length, and time will be nondimensionalized using: \( \beta = h/l_0 \); \( \xi = \lambda/l_0 \); \( \tau = \omega t \); where \( l_0 \) is the nominal reference length. Eqs. (17)-(19) can be rewritten in the following non-dimensional form, which may be more appropriate for the subsequent numerical parametric studies.

**Length**

\[ \xi'' = \left[ (\psi'' + \theta') + 1 \right]^2 + 3c^2(\psi \theta) + 1 \xi \]
\[ \xi'' = \left[ \psi'' + \omega^2(\psi' + 1)^2 \theta + \omega ^3 \psi \theta (\psi + \theta) \right] - Q_\theta / (m \omega^2 l_0) \]

**Swing angle**

\[ (\theta'' + \psi'') + (2 \xi' / \xi) \left[ (\theta' + \psi') - 1 \right] - (3/2) s [2(\psi + \theta)] \]
\[ \theta'' = \left[ \psi' + \omega^2(\psi' + 2 \psi') c \theta + \omega^3 \psi \theta (\psi + \theta) \right] - Q_\psi / (l^2 \omega^2) \]

**Pitch angle**

\[ \psi'' + (3/2) \lambda^2 s^2 \psi + (m/I \lambda^2 c \theta^2 \left[ - (\psi' - \zeta \theta') + 1 \right]^2 \theta + (\psi' - \theta') \psi' + \omega^2 (\psi + \theta) - c(\psi + \theta) \] + \[ \left[ \xi' + \omega^2(3/2) s^2 \psi + \psi' + 2 \xi' ((\psi - \theta') + 1) s \theta \right] \]
\[ \psi'' = Q_\psi / (l_0 \omega^2) \]

**LINEARIZATION OF SYSTEM EQUATIONS OF MOTION**

By assuming that the pitch and swing angles remain small (i.e. \( \theta \ll 1, \psi \ll 1 \)) and also their rates, and by having \( \xi = 1 + \epsilon \) where \( \epsilon \ll 1 \), then \( \sin \epsilon = \epsilon, \cos \epsilon = 1 \) and Eqs. (20) & (21) can be approximated by the
following linear equations for length, swing angle, and pitch angle, respectively,

\[ (23) \]
\[ 
\varepsilon'' + 2(\psi' - \theta') = 3 \varepsilon + 3(\varepsilon' - 3 \psi) = 3 + Q/(m \omega^2 l_c) = \Delta Q_l 
\]
\[ (24) \]
\[ 
\theta'' - \psi' \beta (\psi - \theta) = 2 \varepsilon' - 2 \beta \psi' = Q_\phi/(m l^2 \omega^2) = \Delta Q_\phi 
\]
\[ (25) \]
\[ 
\psi'' + 3 \lambda^2 \psi + (m/I_\zeta) \beta l_c^2 [\lambda (3 \varepsilon + 2 (\psi' - \theta'))] = Q/(\zeta \omega^2) + 3(m/I_\zeta) \beta l_c^2 = \Delta Q_\psi 
\]

The \( \Delta Q_l \) on the right hand side of Eqs. (23)-(25) represent potential control laws. The 3 on the right hand side of Eq. (23) represents the equilibrium tension required at length, \( l_c \). This tension force may be provided by either the control system or the tether's natural elasticity or combinations of both. The \( 3(m/I_\zeta) \beta l_c^2 \) represents the equilibrium nondimensional torque (acceleration) required for the platform pitch angle to be zero. Without any attachment offset \( (\beta = 0) \), Eq. (25) decouples from the length and swing angle equations.

At equilibrium for \( Q_\zeta = Q_\phi = Q_\psi = 0 \), \( q''_i = q'_i = 0 \). By choosing \( l = l_c \) therefore \( \varepsilon = 0 \). The equilibrium values of pitch angle and swing angle (in the absence of control) are:

\[ \theta_{eq} = \psi_{eq} = (m/I_\zeta) \beta l_c^2 (\lambda^2 - m^2 h^2 m/I_\zeta)^{-1} \]  

(26)

These equilibrium values are independent on the physical properties of the platform such as its principal moments of inertia and on the attachment offset distance and the subsatellite mass. For the range of numerical parameters considered here, there are no singularity problems with the denominator terms in Eq. (26).

DEVELOPMENT OF SYSTEM CONTROL

In state variable form in the absence of external disturbances, \( Q_\zeta \), \( Q_\phi \), \( Q_\psi \), but in the presence of control, Eqs. (23) - (25) can be rewritten as:
\[
\frac{dX}{dt} = AX + BU
\]  
(27)

where

\[
X_T = \begin{bmatrix} \varepsilon & \psi & \varepsilon' & \psi' & \theta' \end{bmatrix}
\]  
(28)

and

\[
A = \begin{bmatrix}
0 & 0 & 0 & 1 & 0 & 0 \\
0 & 0 & 0 & 0 & 1 & 0 \\
0 & 0 & 0 & 0 & 0 & 1 \\
3 & 3\beta - 3\beta\lambda^2 & 0 & 0 & 2 & -2 \\
0 & -3\lambda^2 & 0 & 0 & 0 & 0 \\
0 & 3 - 3\lambda^2 & -3 & 2 & 2\beta & 0 \\
\end{bmatrix}
\]

where: A is the system state matrix; X is the system state vector; B is the control influence matrix and U is the control vector, respectively. Matrices X, A, B, and U have dimensions nxl, nxn, nxr, rxl, respectively, where n is the order of the system and r is the number of control inputs. For the system under consideration n = 6.

For this application it is assumed that control could be realized through appropriate modulation of the tension in the tether line and the momentum-type controller for the platform pitching motion. Thus, the control influence matrix is given by,

\[
B_T = \begin{bmatrix}
0 & 0 & 0 & 1 & 0 & 0 \\
0 & 0 & 0 & 0 & 1 & 0 \\
\end{bmatrix}
\]  
(30)
CONTROLLABILITY AND OBSERVABILITY OF THE SYSTEM

Before the development of a suitable control law for $U$, it is necessary to show that the system satisfies the following controllability condition. The system $X' = AX + BU$ is controllable if and only if the rank of $P = n$ where:

$$ P = [B \mid AB \mid A^2B \mid \ldots \mid An^{+1}B] \quad (31) $$

In addition to $B$, the partitions of $P$ (in transposed form) are:

$$(AB)^T = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 2 \\ 0 & 1 & 0 & 2 & 0 & 2 \beta \end{bmatrix}$$

$$(A^2B)^T = \begin{bmatrix} 0 & 0 & 2 & \lambda^1 & 0 & 0 \\ 2 & 0 & 2 \beta & (\lambda + 3 \lambda^2)(\lambda^3 + \lambda^2) & (7 \lambda^3 + \lambda^2) \end{bmatrix}$$

$$(A^3B)^T = \begin{bmatrix} \lambda^1 & 0 & 0 & 0 & 0 & -8 \\ (\lambda + 3 \lambda^2)(\lambda^3 + \lambda^2)(7 \lambda^3 + \lambda^2) & -8 & 0 & (8 \lambda + 12 \lambda^2) \end{bmatrix}$$

$$(A^4B)^T = \begin{bmatrix} 0 & 0 & -8 & 13 & 0 & 0 \\ -8 & (8 \lambda + 12 \lambda^2)(6 \lambda^2 + 13 \lambda + 9 \lambda^4) & (9 \lambda^4) & (9 \lambda^4 - 37) \end{bmatrix}$$

$$(A^5B)^T = \begin{bmatrix} 13 & 0 & 0 & 0 & -8 \quad 50 \\ (6 \lambda^2 + 13 \lambda + 9 \lambda^4) & 9 \lambda^4 & (9 \lambda^4 - 37) & 50 \cdot (503 + 48 \lambda^2 + 36 \lambda^4) \end{bmatrix}$$

By using a particular submatrix of $P$, formed from its first, second, third, fourth, fifth and seventh...
columns, \((P')\) it can be verified that \(\text{Det } P' = 20 \neq 0\); therefore, the rank of \(P\) is 6 and the system is completely controllable. It can also be verified that with control generated by a single input represented only by tether tension modulation, then the system is uncontrollable. On the other hand, for the case where only a platform pitch controller is used (except for possibly some singular values of the inertia ratio, \(\lambda\)), and when \(\beta = 0\), the system is controllable. For the general case with offset a further numerical analysis would be required, but due to the increased coupling it is thought the same results would prevail.

If all the state variables are available as measurable outputs, \(Y\), the matrix, \(C\), in the equation: \(Y = CX\) is an identity matrix (6x6) in which case the observability condition becomes trivial. But, if due to practical limitations only two of the state variables, length \((\ell)\) and length rate \((\ell')\) are available as outputs, then, the output vector, \(Y\), can be written as

\[
Y = CX
\]

where

\[
C = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \end{bmatrix}
\]

Through the rotation of a drum, \(\ell\) can be measured, and with a chronometer, an average \(\ell'\) can be determined at all instants of time. A linear control strategy, \(U\), as based on linear state feedback of the form: \(U = -KX\), requires the complete knowledge of all state variables at all instants of time.

In the system under consideration the swing angle, \(\theta\), swing rate, \(\theta'\), pitch, \(\psi\), and pitch rate, \(\psi'\), would then have to be estimated from the output measurements. This is possible only if the system equations satisfy the observability condition. The system is observable if and only if the matrix

\[
\overline{Q} = [C^T | A^T C^T | (A^T)^2 C^T | \ldots | (A^T)^{n-1} C^T]
\]

has rank = \(n\)

It can be verified that the rank of \(\overline{Q}\) is 6 and the system is completely observable. By measuring only the length \((\ell)\) and length rate \((\ell')\) the other system state variables can be estimated. For many applications of the tethered platform system it will...
be relatively easy to measure these two components of the state, whereas measurements of the other state components may require different types of sensors, which may be more difficult to implement.

APPLICATION OF THE LINEAR QUADRATIC REGULATOR PROBLEM TO DEVELOP CONTROL LAWS

In order to develop a control law based on linear state feedback, the linear quadratic regulator problem from optimal control theory will be applied.\textsuperscript{11}

The optimal control, \( U \), which minimizes the performance index

\[
J = \int_{0}^{\infty} (X^T Q X + U^T R U) \, dt
\]

(35)

is given by,

\[
U = -(R^{-1} B^T P) X = -K X
\]

(36)

where \( Q \) is the positive semi-definite state penalty matrix, \( R \) is the positive definite control penalty matrix which penalizes the system more severely for large control, and \( P \) is the positive definite solution to the steady state Riccati matrix equation,\textsuperscript{11}

\[
MPA^{-1}PT + PBR^{-1}B^T P - Q = 0
\]

(37)

The linear control strategy, \( U \), requires gains proportional to all positions and rates. The appropriate gain matrix, \( K \), is given by

\[
K = \begin{bmatrix}
K_x & K_y & K_\theta & K_{x'} & K_{y'} & K_{\theta'} \\
C_x & C_y & C_\theta & C_{x'} & C_{y'} & C_{\theta'}
\end{bmatrix}
\]

(38)

This control scheme is suitable for a closed loop system having tension modulation on the tether line and a momentum-type device for controlling the pitching motion of the platform. A computer algorithm developed by Melsa and Jones\textsuperscript{12} has been implemented for solving for the elements of the gain (K) matrix, given the elements of the state and control penalty weighting matrices, \( Q \) and \( R \), the state matrix, \( A \), and control influence matrix, \( B \), and
after the controllability of the system has been established.

STABILITY CONDITIONS FOR THE LINEAR SYSTEM WITH LINEAR CONTROL

By assuming solutions for length, swing angle, and pitch angle to be, respectively:

\[ \epsilon(t) = \epsilon_e \quad ; \quad \Theta(t) = \Theta_e + \Theta_{eq}; \Psi(t) = \psi_e + \Psi_{eq}, \]

where \( \Theta_{eq} \) (or \( \Psi_{eq} \)) is given by Eq. (26), the variational coordinates for the swing and pitch angles are used to bias the nonzero equilibrium values for the pitch angle, and the swing angle in Eqs. (23) - (25).

The linear control strategy, \( U \), renders two separate control laws for controlling the tether tension and the platform pitch angle. The two control laws can be written as,

\[ \Delta Q_\theta = -(K_\epsilon \epsilon + K'_\epsilon \epsilon' + K_\Theta Y + K'_\Theta \Theta' + K_\Psi \psi + K'_\Psi \psi') \]

\[ \Delta Q_\psi = -(C_\epsilon \epsilon + C'_\epsilon \epsilon' + C_\Theta \Theta + C'_\Theta \Theta' + C_\Psi \psi + C'_\Psi \psi') \]

where \( \epsilon \) and \( \psi \) are the swing and pitch angle variational coordinates, respectively.

Eqs. (39) - (41) can be substituted into Eqs. (23) - (25) with the assumption that \( \Delta Q = 0 \) to develop the closed-loop system characteristic equation. In this process it is also noted that one of the subdeterminants also corresponds to that used to develop the characteristic equation for the TSS system. For the lower order system of Ref. 7 a graphical interpretation of the stability boundaries in terms of the gains in the tension control law was previously obtained (Ref. 7, Fig. 2.). For the case of zero offset (\( h = 0 \)) and where the platform mass distribution approximates that of a uniform sphere, this figure can still give insight into the stability of the more complex system studied here. For the present study the necessary and sufficient conditions have been fully developed in terms of the control law gains, tether offset parameter, platform inertia ratio, subsatellite mass, and desired tether length. Because of their complexity, a simple geometric
interpretation has not been successfully implemented, but these complex conditions appear in full in Ref. 13.

NUMERICAL RESULTS

Three modes of operation are involved with the platform/subsatellite system. They are: deployment of the subsatellite; maintaining its position at some nominal location (station keeping); and subsatellite retrieval. Here attention focuses only on the station keeping phase of the operation. For the subsequent numerical work in this study the following platform and subsatellite properties are considered,

Platform mass, \( M = 10000.0 \) Kg; Subsatellite mass, \( m = 100.0 \) Kg
Platform pitch principal moment of inertia, \( I_{zz} = 5.33 \times 10^6 \) Kg-m²
Platform moment of inertia ratio, \( \lambda^2 = 1.200 \)
Platform altitude = 500.0 Km;
Platform orbital rate, \( \omega = 1.1068 \times 10^{-3} \) rad/sec
Tether line reference length, \( l_c = 100.0 \) m;
Platform length = 30.0m; Tether attachment offset = 20.0m

With the above system properties the equilibrium tether line swing angle, \( \theta_{eq} \) and platform pitch angle \( \Phi_{eq} \) are calculated (Eq. (26)), to be 0.0314 rad.

PARAMETRIC STUDIES OF THE STATE AND CONTROL PENALTY MATRICES

Assuming that the information about all the state variables is available either through direct measurement or by estimation, only the feedback gains in Eq. (38) need to be computed for implementation of the control. Optimal feedback gains for a given set of state and control penalty weighting matrices, \( Q \) and \( R \), respectively, in the performance index, \( J \), are obtained by solving the nonlinear algebraic matrix Riccati equation for \( P \). It is difficult to obtain an analytic expression for \( P \) in terms of the weighting matrices, \( Q \) and \( R \), for a high order system. However, many numerical algorithms are available for solving
the matrix Riccati equation with the aid of a digital computer. The numerical procedure adopted in the present analysis is as given in Melsa and Jones 12 with inclusion of a subroutine from ORACLS 14, which determines closed-loop system eigenvalues.

The matrices, Q and R, in the performance index, J, are selected such as to yield the desired system performance. For the present analysis it is desired to have the settling time as small as possible without excessive energy in the state or control. Only by trial and error can one arrive at suitable values for Q and R which result in the desired closed-loop system response. Figures 2-4 show typical variations of the real part of the leased damped oscillatory mode with R and different components of the Q matrix. Figure 2 represents the case where the diagonal elements of Q are varied and the tether is assumed to be attached at the platform mass center. Figure 3 illustrates the effect of the same variations with a tether attachment offset of 20.0 meters.

The effect of the offset is to increase the natural coupling of the system. This increased coupling improves the performance in the least damped mode (i.e., shifts the curves upward). This tendency is more pronounced for the smaller values of weights in the state penalty matrix. Larger weighting elements in the state penalty matrix result in higher coupling from the control effort which overshadows that due to the attachment offset. Increases in the control penalty weighting result in more rapid damping of the system's oscillations (i.e., more negative values for the real part of the eigenvalue). This tendency is more apparent for smaller weighting elements in the state penalty matrix.

When only one of the diagonal elements of the state penalty matrix is varied at a time, the performance is improved when that element penalizes a position state as compared with the situation where the diagonal element being varied penalizes the corresponding rate state. As an example, Fig. 4 shows the effect of varying only the tether length penalty element in the Q matrix on the real part of the least damped mode while holding the other elements in the Q matrix constant where the offset parameter, h = 20m. From the results of the more extensive parametric study 13 it is seen that similar weighting of all states gives better results than split weighting, for the range of parameters considered here.
Table 1 lists the control system characteristics of the platform/subsatellite system with a 20.0 meter tether attachment offset. These control parameters render a desirable settling time without excessive energy in the state and control effort. Table 2 lists similar characteristics for the case of no offset.

**TABLE 1**

**TETHER AND PLATFORM CONTROL CHARACTERISTICS AND CONTROL LAW GAINS**

Offset = 20.0 m
Least Damped Modal Time Constant = 0.243 hr
State penalty matrix, $Q=10^6 i j$

Control penalty matrix,

$$ R = \begin{bmatrix} 2 & 0 \\ 0 & 2 \end{bmatrix} $$

Gains,

\[
\begin{align*}
K_0 &= 8.03247 \\
K_\psi &= 1.56196 \\
K_\phi &= 3.44483 \\
K_\phi' &= 6.76085 \\
K_\psi' &= 1.43246 \\
K_\phi' &= 2.92402 \\
C_\phi &= 1.91681 \\
C_\psi &= 2.16826 \\
C_\phi &= 1.80729 \\
C_\phi' &= 1.43246 \\
C_\psi' &= 5.38079 \\
C_\phi' &= 1.17312
\end{align*}
\]
TABLE 2

TETHER AND PLATFORM CONTROL CHARACTERISTICS AND
CONTROL LAW GAINS

Offset = 0.0 m
Least Damped Modal Time Constant = 0.243 hr
State penalty matrix, $Q^{-1}_{ij}$

Control penalty matrix,

$$ R = \begin{bmatrix} 2 & 0 \\ 0 & 2 \end{bmatrix} $$

Gains,

- $K_\epsilon = 7.99860$
- $K_\Psi = 1.48671$
- $K_\Theta = 3.37475$
- $K_{\epsilon'} = 6.86226$
- $K_{\Psi'} = 1.19052$
- $K_{\Theta'} = 3.12771$
- $C_\epsilon = 2.00348$
- $C_\Psi = 2.05478$
- $C_\Theta = 1.30765$
- $C_{\epsilon'} = 1.19052$
- $C_{\Psi'} = 5.23986$
- $C_{\Theta'} = 0.083203$
TRANSIENT RESPONSES

By using Euler integration techniques, Eqs. (23) and (25) were numerically integrated to give the transient response of the system states for different initial conditions. As an example, Fig. 5 shows the response of the differential length (from a desired reference length of 100m), the platform pitch, and the tether line swing angle for initial conditions of 101m in tether length and 0.01 rad in both the platform pitch angle and the tether line swing angle for a tether attachment offset of 20m. The tether and platform control law gains for this application are shown in Table 1. It is seen that the tether line swing motion is the most poorly damped requiring about 1.75 hr to reach the nominal value, whereas the platform pitch motion is damped out within approximately 1.0 hr.

CONTROL EFFORTS

The two dimensional control laws for controlling tether tension and platform pitch angle are, respectively,

\[ \Delta Q = -m \omega^2 l_c (K \varepsilon + K \varepsilon' + K \gamma + K \gamma' + K \alpha + K \alpha') \]

\[ \Delta Q = -I \omega^2 l_c (C \varepsilon + C \varepsilon' + C \gamma + C \gamma' + C \alpha + C \alpha') \]

These control laws represent the control effort the designer must supply to ensure that the tether line remains taut at all times and that the local normal at the platform's center of mass remains aligned with the local orbit vertical. Equation (42) represents the tether tension added to the tether line's natural tension (represented by the 3 on the right hand side of Eq. (23)).

Figure 6 represents the time history of the tether tension and platform torque control efforts for the same initial conditions and attachment offset of Fig. 5. The transient responses of the tension control effort illustrate that at certain intervals of time the designer supplied tension amplitude becomes negative. However, when this level of tension is added to the system's natural tension (0.037N) the total tension remains positive. Therefore, the tether line remains taut.
For all cases of initial conditions and offsets studied the settling time on the tension control effort was about 1.5 hour. The torque control effort has a settling time of approximately 1.0 hour. The attachment offset is associated with increases in the amplitudes of the control efforts but the order of magnitudes of the amplitudes do not change.

CONTROL POWER LEVELS

An important interest to the designer is the amount of power which must be supplied to control a given system in a desirable manner. As an example of the amount of power needed to supply tether tension and platform torque control for the case of increased initial conditions of 0.05 (dimensionless) and no offset, it was seen that the maximum (differential) tension power level was less than $3 \times 10^{-4}$ watts and platform torque power level required was less than 0.08 watts.

CONCLUSIONS AND RECOMMENDATIONS FOR FUTURE INVESTIGATIONS

In this study of the in-plane dynamics and control of a space platform with a tethered subsatellite, it has been seen that:

(1) within the linear range the system is controllable with momentum-type control on the platform and with tension modulation on the tether line; (2) equilibrium values of swing and pitch angles are dependent on the physical properties of the platform inertia, subsatellite mass, and tether attachment offset; (3) the linear system is observable with tether length and length rate measurements only; (4) tether attachment offset increases the system's natural coupling and improves transient performance in the least damped mode, but at the cost of slightly larger control force amplitudes; and (5) the linear quadratic regulator problem has been utilized for determining tether and platform control law gains which provide for stable closed-loop systems.

The authors suggest the following topics for future research:

(1) development of a three dimensional model of the platform--subsatellite system; (2) development of a two dimensional model of the platform--subsatellite
system to include tether mass and platform flexibility. Include in this model an examination for resonance interaction between the flexible tether and the platform; (3) include disturbances in either model such as solar pressure, aerodynamics, and plant and measurement noise; and (4) examine effects of other control devices on the platform or subsatellite, such as active thrusters.

ACKNOWLEDGEMENT

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REFERENCES


Figure 1  System Geometry
Figure 2  Variation of the Real Part of Least Damped Mode with R and Q with No Offset
Figure 3  Variation of Real Part of Least Damped Mode with R and Q with Offset
Figure 4 Variation of Real Part of Least Damped Mode with $R$ and $Q_\varepsilon$ (remaining $Q_{ii}=1.0$); with Offset
Fig. 5 Transient Response of Position Coordinates

I.C. = 0.01
OFFSET = 20.0M
Fig. 6 Time History of Required Control Effort

I.C. = 0.01
OFFSET = 20.0M

PLATFROM TURQE (N-M)

DIFFERENTIAL TENSION CONTROL (N)
RECOMMENDATIONS TO THE TECHNOLOGY
AND TEST PANEL

Recommendations:

1) Recommendations of committee should be coordinated with those of the
Space Station panel due to obvious overlay.

2) Regarding dynamic simulation capability, general purpose complete
software programs should be used only after extensive preliminary
design parametric studies are performed using simpler routines
oriented toward a specific configuration, but often neglecting some
of the physical effects. The general purpose and specific software
routines should thus be used in a logical complimentary fashion.

3) There is an impending need to provide an in-orbit demonstration test
of the validity of existing dynamic simulations. This should be done
in three distinct phases: (a) during deployment; (b) during
station-keeping; and (c) during retrieval operations. As a start,
the TSS-1 mission in which atmospheric drag effects are expected
to be small is suggested. A confidence in the accuracy of dynamic
models will provide a significant boost to the more complex TSS-2
mission in which the effect of the rotating atmosphere will be Impor-
tant, especially if altitudes as low as 90 km will be considered. An
experiment should also be designed for the TSS-2 mission to test the
accuracy of the way in which atmospheric effects are modeled.

Needless to say, if either of the first two missions is not
successful, or encounters partial dynamic problems, the potential
jeopardy to the whole TSS concept and its many exciting applications
should be obvious.

It would appear that some care in validating existing dynamic
analysis (and making necessary changes) in this initial phase may pay
greater dividends in the long run.

Respectfully submitted by

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TECHNOLOGY AND TEST PANEL

PRESENTATION VI

EFFECTS OF DAMPING ON THE CONTROL
DYNAMICS OF THE SPACE SHUTTLE BASED ON
TETHERED SYSTEMS

OCTOBER 15 – 17, 1985

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THE UNIVERSITY OF BRITISH COLOMBIA
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CANADA
LOW ALTITUDE SCIENCE APPLICATIONS

sounding rocket

120km
100km
Earth

satellite

CARGO TRANSFER

ALFVEN WAVE GENERATOR

RELEASE OF ARTIFICIAL METEORS

meteor

Earth

cargo

CARGO TRANSFER
Figure 1. Geometry of motion.
THE SPACE SHUTTLE BASED TETHERED SYSTEMS

In its utmost generality the problem is quite challenging as the system dynamics is governed by a set of ordinary and partial nonlinear, nonautonomous and coupled equations which account for:

- three-dimensional rigid body dynamics (librational motion) of the Shuttle and the subsatellite;
- swinging in-plane and out-of-plane motions of the tether, of finite mass and elasticity, with longitudinal and transverse vibrations superimposed on them;
- offset of the tether attachment point from the Shuttle's center of mass;
- aerodynamic drag in a rotating atmosphere.


* ROTATIONS AND VIBRATIONS OF THE TETHER ARE INHERENTLY UNSTABLE DURING RETRIEVAL OF THE SUBSATELLITE.

* SCHEMES EXIST TO CONTROL ROTATIONAL MOTION SUCCESSFULLY.

* CONTROL OF LONGITUDINAL AND TRANSVERSE VIBRATIONS STILL REMAINS A PROBLEM.

* NONLINEAR COUPLING BETWEEN TRANSVERSE AND LONGITUDINAL VIBRATIONS IS IMPORTANT.
\[ i = 0, \quad L_0 = 10 \text{m}, \quad \theta_0 = 0 \quad \text{--- no damping} \]
\[ e = 0, \quad \theta_0 = \phi_0 = 3^\circ, \quad \phi_0 = 1.0 \quad \text{--- with damping} \]
\[ \dot{i} = 90, \quad L_0 = 10 \text{m}, \quad \theta' = 0 \]

\[ e = 0.00076, \theta_0 = \phi_0 = 3^\circ, \quad \phi' = 1.0 \]

- no damping
- with damping

\[ c_\theta = c_\phi = 0 \]
\[ c_\theta' = c_\phi' = 0.1 \]
\[ c_\theta = 1, \quad c_\phi = 0 \]
\[ c_\theta' = c_\phi' = 3.366 \]
\[ i = 0, \quad \theta_0 = 0, \quad \phi_0 = 3^\circ, \quad L_0 = 100 \text{ km} \]
\[ e = 0, \quad \theta_0' = \phi_0' = 0, \quad L = L_0 e^{-t/p} \]
\[ p = 5000 \text{ sec} \]

- no damping
- with damping, \( C_\theta = C_\phi = 0 \), \( C_\theta' = C_\phi' = 0.1 \)
CONTROL STRATEGIES

Tension control strategy as proposed by Kissel (Baker et al.)*

Optimal law based on an application of the linear regulator

problem as proposed by Bainum and Kumar **;

Several nonlinear control strategies sensitive to the
tether length, length rate, librational and vibrational
dynamics***;

Nonlinear control strategies together with thrusters†.


** P.M. Bainum, and V.K. Kumar, "Optimum Control of the Shuttle-

Tethered Subsatellite System," 30th Congress of the Interna-
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of Tethered Satellite Systems," NASA/JPL Workshop on Applica-
tion of Distributed System Theory to the Control of Large
Space Structures, Jet Propulsion Laboratory, Pasadena, Calif.,
U.S.A., July 1982, NASA/JPL Publication 83-46, Editor:


† Xu, D.M., Misra, A.K., and Modi, V.J., "On Thruster Augmented

Active Control of a Tethered Subsatellite System During Retrieval,"
AIAA/AAS Astrodynamics Conference, Seattle, Wash., U.S.A.,
i = 90°, L₀ = 100 km, φ₀ = 10°
e = 0, θ₀ = -20°, θ₀' = φ₀' = 0

- no aerodynamics
- with aerodynamics
- with aerodynamics and damping

Cθ = 1, Cφ = 0
Cθ' = Cφ' = 3.366
\[ \begin{align*}
i &= 90^\circ, \\
L_0 &= 100\text{km}, \\
\phi_0 &= 10^\circ, \\
e &= 0.00076, \\
\theta_c &= -20^\circ, \\
\theta'_c &= \phi'_c = 0.0.
\end{align*} \]
\[
\begin{align*}
i &= 90^\circ, & L_0 &= 100 \text{ km}, & K_2 &= 7.0 \\
e &= 0, & L_c &= L_0 e^{-t/p}, & K_\xi &= 4.0 \\
\theta' &= \phi' = 0, & \rho &= 5000 \text{ sec}, \\
\theta_0 &= \phi_0 = 0 \\
\theta_0 &= -8^\circ, \phi_0 = 0 \\
\theta_0 &= -15^\circ, \phi_0 = 3^\circ
\end{align*}
\]
\[ i = 90^\circ, \quad L_0 = 100\,\text{km}, \quad K_\zeta = 7.0 \]
\[ e = 0, \quad L_c = L_0 e^{-t/P}, \quad K_\zeta = 4.0 \]
\[ \theta_0' = \phi_0' = 0, \quad P = 5000\,\text{sec}, \quad K_{\phi'} = 100 \]
\[ \theta_0 = -15^\circ, \quad \phi_0 = 3^\circ \]

---

- **No damping**: \( \cdots \)
- **With damping**: \( \cdots \)

\( C_{\theta'} = C_{\phi'} = 0.1 \)

---

**Legend**: 
- \( L, \text{km.} \)
- \( \theta^\circ \)
- \( \phi^\circ \)

**Axes**: 
- **Time, hr.**

---

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\( \dot{i} = 90^\circ \), \( L_0 = 100 \text{ km} \), \( K_\xi = 7.0 \)

\( e = 0 \), \( L_c = L_0 e^{-t/p} \), \( K_\xi = 4.0 \)

\( \theta'_0 = \phi'_0 = 0 \), \( p = 5000 \text{ sec} \), \( K_{\phi'} = 100 \)

\( \theta_0 = -15^\circ \), \( \phi_0 = 3^\circ \), \( \zeta_0 = 295 \text{ m} \), \( C_{\theta'} = C_{\phi'} = 0.1 \)
- Length Rate Control Law
- Thruster Augmented Active Control Law
  - Exponential Retrieval
  - Constant Velocity Retrieval

\[ \bar{T} = \bar{I} T_y + \bar{J} T_c + \bar{K} T_d \]

Maximum thrust provided is limited to ± 5N

Example:
- Circular polar orbit
- Spherical satellite with projected area of 1 m²
  - Mass = 170 kg
- 1 mm diameter Kevlar tether
- Initial Conditions
  All the generalized co-ordinates excited
  - transverse as well as longitudinal disturbances
  - Pitch = 15°
    Roll = 1°

- Total Thrust Impulse Required
  \[ \approx 1 \times 10^4 \text{ Ns} \]

Retrieval Time from 100 km to 250 m \( \approx 2 \text{ hrs.} \)
\[ \eta' = \left( \frac{c}{\omega} \right) \left\{ 1 - 5\alpha' - 18\gamma'^2 \right\} - 1.8 \omega \epsilon C_1 \] 

\[ + 5 \times 10^3 \left[ B_1^2 - B_2(0) \right] \] 

\( l_0 \geq 20 \text{ km} \)
\[ C_2(0) = -0.28 \times 10^{-3} \]

\[ C_1(0) = 0.49 \times 10^{-2} \]
\[ B_2(0) = 0.48 \times 10^{-3} \]
\[ B_1(0) = -1.6 \times 10^{-3} \]
\[ A_2(0) = 0.5 \times 10^{-4} \]
\[ A_1(0) = -0.5 \times 10^{-4} \]
\[ T_c = 0 \]

\[ T_c = -5 \omega \epsilon (C_1 + C_2) \ell_t = 3 \text{ km} + 3 (\ell_t - \ell_0) / \ell_0 \]

\[ T_\gamma = 0 \]

\[ T_\gamma = -2 \eta' \gamma + 2 \gamma' + \left[ 10 - \frac{3 \pi \eta}{\ell_0} \right] (A_1' - A_2') \]

\[ T_\alpha = 0 \]

\[ T_\alpha = 2 \eta' (1 + \alpha') - 2 \alpha' + \left[ 10 - \frac{3 \pi / \ell_0}{\eta'} \right] (B_1' - B_2') \]
SUMMARY OF RESULTS

(i) The analysis suggests that a relatively simple point mass model can provide useful information concerning librational dynamics during deployment and retrieval of the Space Shuttle based tethered subsatellite system. The results show that a nonlinear tension control strategy of the form $T = T(\dot{\xi}, \dot{\xi}', \phi', \dot{\phi}')$ in conjunction with a suitable choice of gains and realistic damping can lead to stable retrieval manoeuver with amplitudes in pitch and roll limited to acceptable values.

(ii) Longitudinal and lateral vibrations of the tether are strongly coupled and can lead to the slackening of the tether.

(iii) Tether vibrations can be controlled quite effectively by speeding up the retrieval at smaller tether length and/or using thrusters.
COMMENTS

GENERAL:

• IF ONE JUDGES FROM THE MATERIAL PRESENTED AT THIS CONFERENCE, THE PROGRESS MADE SINCE THE FIRST WORKSHOP APPEARS TO BE MINIMAL.

• TIME HAS COME TO GROW OUT OF THE INFANTILE PHASE OF ENUMERATING A WIDE VARIETY OF POSSIBLE TETHER APPLICATIONS AND SETTLE DOWN ON DETAILED STUDIES OF A FEW APPLICATIONS CONSISTENT WITH COMMITTED PROGRAMS AND AVAILABLE RESOURCES.

TO BE TAKEN SERIOUSLY BY ALLOCATORS OF FUNDS AND PROGRAM MANAGERS, THE WORKSHOP OF THIS NATURE SHOULD FOCUS ATTENTION, NOT DIFFUSE IT.

• WITH THE U. S. COMMITMENT TO A SPACE STATION, THE FUTURE OF THE TETHER CONCEPT HAS THE MAXIMUM PROMISE IN THAT AREA.. JUST AS THE SPACE STATION HAS A BASELINE CONFIGURATION, THIS WORKSHOP, OR THE FUTURE ONE, SHOULD IDENTIFY "BASELINE CONFIGURATIONS" FOR POSSIBLE TETHER PROJECTS. WHAT IS NEEDED IS A CONCERTED EFFORT IN A FEW WELL THOUGHTOUT PROJECTS RATHER THAN AN TORRENTIAL OUTPOUR OF CONCEPTS WHICH REMAIN CONCEPTS.
COMMENTS

SPECIFIC:

• SUCCESS OF MOST OF THE CONCEPTS TALKED ABOUT AT THIS WORKSHOP RELY ON THE FUNDAMENTAL REQUIREMENT OF DYNAMICS, STABILITY AND CONTROL OF TSS DURING DEPLOYMENT, STATIONKEEPING AND RETRIEVAL. MORE ATTENTION SHOULD BE DIRECTED TOWARDS NUMERICAL MODELING OF THE DYNAMICS AND CONTROL WITH PRE-TSS-1 EXPERIMENT(S) ABOARD THE ORBITER TO VALIDATE THE MODEL AND OBTAIN RELIABLE INFORMATION CONCERNING KEY INPUT PARAMETERS. IT SEEMS TO ME THAT THIS IS OF FUNDAMENTAL SIGNIFICANCE.

• FOCUS ATTENTION ON APPLICATIONS OF THE TETHER CONCEPT TO THE SPACE STATION "SPACE CRANE", MRMS BASED TETHERED SYSTEM FOR CONTROLLED GRAVITY EXPERIMENTS, AND DEPLOYMENT OF A PLATFORM AT A DESIRED DISTANCE ARE THE ONES WHICH SHOW PROMISE.

WE HAVE BEEN VISIONARIES TO DATE, AND RIGHTLY SO. THE TIME HAS COME TO BE PRAGMATIC.
TECHNOLOGY AND TEST PANEL
PRESENTATION VII

ELECTRODYNAMIC TETHER
TECHNOLOGY CONSIDERATIONS

OCTOBER 15 – 17, 1985

JOSEPH C. KOLECKI
LEWIS RESEARCH CENTER
Electrodynamie Tether Operation

\[ \mathbf{E} = \mathbf{v} \times \mathbf{B} \]

Figure 1. Electrodynamic Drag $\mathbf{i} \mathbf{B} \times \mathbf{v}$. Decrease in Orbiter Total Energy = Electric Energy in Electrodynamic Tether Circuit.

Some Technology Areas

- Plasma Contactors
  - Hollow Cathodes
  - Hollow Cathode Based Plasma Contactor
  - Electron Gun

- Power Management and Conditioning
  - Interface Electronics Between End Of Tether And User
  - High Power Components
  - Switching
  - Storage
Materials
- Any materials to be exposed in the LEO environment must be able to withstand a harsh atomic oxygen environment.

Status

Plasma Contactors
- Study program which involves experimental and theoretical characterization of hollow cathodes and hollow cathode based plasma contactors
- Some early results: improved electron collection characteristics seem to occur with increased ion production efficiency.
  For \( m_i/m_e \sim 300, i_{i+} \sim 1/30i_e \): i.e., to collect \( x \) amps of electron current from the magnetoplasma, an ion current of \( \sim x/30 \) amps is sufficient for an ion to electron mass ratio of 300.
- Advantage exists in the fact that a plasma contactor can "clamp" a spacecraft to within a few volts of plasma potential.

Power Management and Conditioning
- There are no tether related activities in this area at present.
- Need to identify electrodynamic tether operational voltage and current ranges. This will be done in the System Studies presently underway.
- Need to identify state-of-the-art vs. advanced technology requirements.
- Need to begin the necessary component and circuit development programs early enough so as not to impact schedules later on.

Materials
- Study program includes in-air and in-vacuo techniques for applying oxygen resistant, insulating coatings onto electrodynamic tethers.
Summary

- High power, i.e., multikilowatt electrodynamic tether systems need a variety of supporting technologies in order to be viable.
- Study programs show that some of the necessary subsystems should prove workable.
- The area of interface between the high voltage end of the electrodynamic tether and the user has not been addressed. This area is vital to the successful and safe operation of an electrodynamic tether system, and should begin to be addressed as operating ranges of multikilowatt systems are defined.
TECHNOLOGY AND TEST PANEL

PRESENTATION VIII

COMLINK

PROPOSAL

FOR FUTURE MISSIONS

OF TETHERED SATELLITE

OCTOBER 15 - 17, 1985

FILIPPO SCIARRINO

CONTRAVES ITALIANA
OBJECTIVES:

- Test the quality of the communications links between satellites

- Investigate the interaction between the VLF and ELF waves, generated by the conducting tether, and the SHF and YHF electromagnetic waves, generated by the 20/30 GHz transmitter on satellite

- Measurement on ionospheric electron density irregularities by means of phase-coherent RF transmission between the two vehicles

- Observe motion of the tethered satellite, through the Doppler link established between the shuttle and the satellite

- Test the technology and deployment of space-born antennas of larger diameter

- Data collection on board the shuttle
INSTRUMENTATION:

THE PAYLOAD WILL CONSIST OF A TEST ANTENNA AND RECEIVER, MOUNTED ON THE SHUTTLE PLATFORM AND A TRANSMITTER, PLACED ON THE SATELLITE, WHICH GENERATES MICROWAVE ELECTROMAGNETIC WAVES.
FILIPPO SCIARRINO

A PAYLOAD FOR UTILIZATION OF SPACE PLATFORM IN THE FIELD OF COMMUNICATION AND EARTH OBSERVATION
4. PAYLOAD FOR COMMUNICATION LINK EXPERIMENT ON
THE SHUTTLE-TETHERED SATELLITE

Shuttle-Tethered Satellite System will utilize the Shuttle, in orbit to
earth at an altitude of approximately 200 km in order to deploy, by means
a tether, a satellite up to a distance of 100 km and hold it in a fixed
position with respect to the Shuttle.

This system, the long conducting tether with lengths of 10-100 km would
strongly with the ionosphere and magnetosphere. A number of space
perturbation experiments can be accomplished with the conducting tether
the instrumented electromagnetics satellite, deployed at a distance of
20 km above the Shuttle. Operation of these electromagnetics experiments would
deconflict with participation of Shuttle-Orbiter personnel and remote measurements
in ground stations. But this measurement technique suffers the disadvantages
limited contact times and the disturbing effects due to the different
orbital positions.

In this paper describes a payload which is suitable to create a measurement
reference system for continued operation and with steady environmental para-
ters.

The proposed payload will perform an experiment on communication link
(COMLINK) between the Shuttle and the tethered satellite.

1. THE OBJECTIVES OF COMLINK

The objectives of the communication link experiment are as follows:

- Test the quality of the communication links between satellites in space;
- Investigate the interactions between the VHF and UHF waves, generated by the
  conducting tether, acting as an antenna in the ionosphere, and the UHF and VHF
  electromagnetic waves, generated by the satellite;
- Make measurement of ionospheric electron density irregularities, by means
  of phase-coherent radiofrequency transmission between the two vehicles
  (Shuttle and sub-satellite);
- Observe motion of the tethered satellite, through the doppler link establish-
  ed between the Shuttle and sub-satellite;
- Test the technology and deployment of space borne antennas of larger di-
  ameter for communications application.

The Shuttle-tethered Satellite Communication link is shown in Fig. 1.

2. THE DESCRIPTION OF COMLINK PAYLOAD

The proposed payload consists of a test antenna, mounted on the Shuttle plat-
form, and a transmitter, placed on the sub-satellite which is wire suspended
from the Shuttle and rotates around it in a space fixed orbital plane. The
transmitter will establish plasma and electromagnetic waves, at a frequency
above 1 GHz, varying with modulation techniques.

The type of antenna on the Shuttle platform, will be an offset fed parabolic
reflector of about 3 m. diameter.

RILIA, ALLI 25, 1-20154 MILANO, ITALY, NOSA 1985
FIG. 4: SHUTTLE-TETHERED SATELLITE Communication link
TENSIOMETER:
IT IS DESIRABLE TO PERFORM A TECHNOLOGICAL / STATE OF THE ART SURVEY (OR ANALYSIS) IN ORDER TO ASSESS FEASIBILITY / AVAILABILITY
(SPACE QUALIFICATION IS NEEDED)

"EQUATORIAL" ATTITUDE CONTROL OF TETHERED SATELLITE:
IN ORDER TO AVOID PLUME POLLUTION AROUND THE S/C, THE POSSIBILITY OF ATTITUDE STABILIZATION BY MEANS OF "MAGNETIC DIPOLE" TECHNIQUE CAN BE INVESTIGATED
INPUT TO TECHNOLOGY AND TEST
FROM GUALTIERO MARONE
SOCIETA ITALIANA AVIONIOA (S.I.A.)

THE GROWING IN EXPERIMENT COMPLEXITY REQUIRE:

- INCREMENT OF ENERGY AVAILABLE
- INCREMENT OF COMMUNICATION BIT RATE

STUDIES ARE LOOKING AT THE POSSIBILITY TO USE THE TETHER AS:

- POWER LINE TRANSPORTATION SYSTEM
- COMMUNICATION LINK (WITH OPTICAL FIBERS)

CRITICAL AREAS AND TECHNOLOGICAL ASPECTS THAT ARE TO BE INVESTIGATED ARE:

HIGH VOLTAGE POWER TRANSPORTATION

- TETHER CONDUCTORS
- TETHER INSULATORS
INPUT TO TECHNOLOGY AND TEST
FROM GUALTIERO MARONE (con't)

POWER MANAGEMENT AND CONDITIONING

- HIGH VOLTAGE POWER SUPPLY
- HIGH VOLTAGE ELECTRICAL INTERFACES

COMMUNICATION WITH OPTICAL FIBERS

- OPTICAL FIBERS CHARACTERISTICS (ELECTRICAL/ THERMAL)
- OPTICAL TRANSMITTER/RECEIVER DEVICES

TETHER CONFIGURATIONS

- MECHANICAL / ELECTRICAL CONSTRAINTS
- TETHER MANUFACTURING ASPECTS
SPACE STATION PANEL
Table of Contents

1. Introduction and General Background
2. Tether Applications to Space Station
3. Space Station Benefits From Tether Applications
4. Flight Demonstrations
5. Required Technology Emphasis
6. Impact on Space Station Configuration and Operation
7. Space Station Tether Applications Priorities
8. Future Tether Applications
9. Conclusions and Recommendations
1. INTRODUCTION AND GENERAL BACKGROUND

It has not happened very often in space flight that a long dormant but radical new element of space flight is about to appear at the scene of space operations. The last several years have seen the advent and growth of a new avenue to space utilization: the tether. Well-organized and structured efforts of considerable magnitude have explored and defined the engineering and technological requirements of the use of tethers in space and have discovered their broad range of operational and economic benefits. The results of these efforts have produced a family of extremely promising candidate applications. The extensive efforts now in progress are gaining momentum and a series of flight demonstrations are being planned and can be expected to take place in a few years. This report is structured to cover the general and specific roles of tethers in space as they apply to NASA’s planned Space Station.

The evolution of the tether concept into an engineering program is phased with the growth of the Space Station program. In such a way there is the possibility to have the tether applications compatible with the Space Station configuration and/or to be aware of what kind of tether related operations have to be eliminated due to evident conflict with respect to the Space Station requirements. Specific studies - started even before the Space Station program became officially approved - have been very useful in terms of a fast and efficient evaluation of what and how the tether concept could be of benefit to the Space Station program. In addition, the results of system investigation/dynamic studies/simulations and, later on, flight demonstration through the first TSS mission are major drivers for tether concept application, particularly to the Space Station. The success of early flight demonstrations will officially open a new door for the tether space activity, and the Space Station area will not be second to any other kind of application. Many attractive ideas have been generated so far on tether concept applications to Space Station. Therefore we are now in a position to start filtering out what, at present, is considered feasible and at the same time useful in terms of science, technology, and operation. The major final goal is to have tether concept application in conjunction with the IOC-phase Space Station. In that regard, after having assured/verified the compatibility
with the Space Station configuration, the associated benefits should automatically facilitate any final decision. It is anticipated that total or partial demonstration is required in order to complete the technical and safety scenario, considering also the technology and operation derived from the new proposed solutions. The major hope is that the impacts on the Space Station configuration can be easily accommodated. That can more probably become a reality if the specific issues are approached as soon as possible and in the most proper way.
2. TETHER APPLICATIONS TO SPACE STATION

Fundamental Items

- Specific Tether Applications
- Issues and Concerns
- Priorities
- Flight Demonstrations
- Application Priorities
- Conclusions and Recommendations

Space Station Facilities and Capabilities (IOC era) - priorities will vary with program changes

- Tethered Orbiter Deployment (with OMS Propellant Scavenging)
- Tethered Launch of OTV
- IOC Tethered Space Station C.G. Vernier (C.G. Management)
- IOC Electrodynamic Reserve Power
- IOC Electrodynamic Thrust (Drag Make-up)
- IOC Tethered Platform (short mission)
- IOC "Zero G" Laboratory (soft suspension)
- IOC Tethered Elevator (soft suspension)
- Remote Docking of Orbiter
- IOC Deboosting Small Cargo Modules
- IOC Electrodynamic Tether (Research)
  - Tethered Propellant Depot and Fuel Transfer
  - Tethered Antenna Farm
- IOC Multi-Probe (beads on string)(short mission)
  - Remote Wake Shield
3. SPACE STATION BENEFITS FROM TETHER APPLICATIONS

- "Zero G" Laboratory
- Reserve Power Generator
- Halve Orbiter Deboost Propellant Requirement Through Tether Assisted Deboost
- C.G. Management
- Waste Disposal by Tether
- Quick Sample Return
- Eliminate OMV Propellant Tanker
  - Scavenge OMS Propellant During Tether Assisted Deorbit of Orbiter
- Eliminate Instrument Contamination
  - Tethered Instrument Modules
- Transfer of Hard Point For MRMS/Tether Operations From Orbiter to Space Station
- Platform Useful to Settle Materials Before Processing
- Periodic Supply of OMS Bi-Propellant for OMV and Platforms
- Reduction of Stationkeeping Propellant Deliveries
- Reduced Requirements for De-Orbit Logistic Through Tethered Waste Disposal
- Tether Assisted Attitude Control (Contamination Reduction)
- Combination of Center Mass Control Antenna Farm, Tether Assisted Attitude Control and Collision Avoidance Maneuver Capability by a Specific Tether System (Deployed Mass)
- Maintenance of Constant Altitude Capability for Specific Earth Observations
- Utilization of Power Surge Caused by Orbiter Deployment for Material Melting Coincident with the Generated G-Field for Settling the Melt
- Tether is the Only Way to Maintain and Exercise Control Over Various Variable Gravity Fields (10^-2 to 10^-5) and Thus Responding to an Urgent Scientific Requirement (Evolution of Gravity Maps)
4. FLIGHT DEMONSTRATIONS

- Tether Shape Measurements
- KITE/Scaled-SATP
- Disposable Tether System Verification
- Fluid Transfer Experiments Under Various DC and AC Accelerations
- Experiments Already Made to be Repeated Under Different G-Levels
- Needed: Tether Mediated Rendezvous Demonstration
  - P/L Deployment and Subsequent Retrieval
- Elevator/Crawler Demonstration (Gravity Field Mapping and Perturbation Determinations)
- Verifying and Refining Dynamic Models in Flight Dems
- Attachment/Detachment of Crawler to Tether
  - RMS
  - EVA
- Drive Mechanism for Crawler
  - Electromechanical
  - Electromagnetic
- Variable/Minimum Gravity
  - Accuracy
  - Duration
- Attitude Control
  - Rotation About Tether
  - Stabilization for Instrument Pointing
- Power Generation/Dissipation
- C.G. Location and Maintenance for P/L's and Experiments Attached to Crawler
- Degree of Automation/Robotics
- Internal Suspension System
5. REQUIRED TECHNOLOGY EMPHASIS

- Tether Technology
  - Materials and Configurations
  - Maintainability
  - Tension Control
  - Damping Characteristics
  - Environmental Compatibility

- Deployer Technology
  - Motor/Generator
  - Motor/Reel Coupling

- Electrodynamic Technology
  - Plasma Contactors
  - High Voltage Insulation
  - High Voltage Conversion and Control
  - Specific Tether Construction
  - Environmental Compatibility

- Engineering Instrumentation

- Science Instrumentation

- Critical Systems Hardware (Mechanisms, Devices, etc.)
6. IMPACT ON SPACE STATION CONFIGURATION AND OPERATION

Issues and Concerns

- Space Station Collision Avoidance Maneuvers
  - 20 km Displacement in any Direction
  - Up to 24 Hours Notice

- Space Station Quiet Periods Up to 30 Consecutive Days \((10^{-6} \text{ g})\)

- Proximity Operations

- Debris Collision Probability of Long Duration Platform Tether

- Platform May Have to be Retrievable Without Tether

- Manned Zero G Laboratory

- High G Levels During Orbiter and OTV Deployment \((10^{-2} \text{ g})\)

- Zero G Tether Module Should Also Serve as Transportation to Platform

- On-Board Zero-G Laboratory Quite Massive \((25,000 \text{ kg})\)

- Platform May Have to Have An Autonomous Power System because Electrical Tethers Introduce Perturbations

- Energy Supply and Dissipation for Elevator

- Tethered Fuel Facility Has Severe Operational Problems

- Thrust Generation Due to Punctured Tank Cannot Be Handled

- Requirement to Support 20,000 N Longitudinal Force By Space Station Structure
7. SPACE STATION TETHER APPLICATIONS PRIORITIES

Criteria:
- IOC Space Station Applicability
- Improved Operational Capability
- Solution to Space Station Problems

Priorities:
- Variable Gravity Laboratory (Controllable)
- Deboosting Small Cargo Modules
- Electromagnetic Reserve Power
- Tether Space Station C.G. Control (Vernier)
- Tethered Orbiter Deboost
- Tethered Remote Docking of Orbiter
- Tethered Science/Applications Platform
8. FUTURE TETHER APPLICATIONS

A. Other Potential Tether Facilities in Earth Orbit
   A-1 Electrodynamic OMV and Debris Collector
   A-2 Spinning Facility for Simulating Lunar and Martian Gravity
   A-3 Spinning Transport Node near GEO

B. Potential Lunar, Martian, and Asteroidal Tether Facilities
   B-1 Surface-Based Slings (on the Moon, Phobos, and Asteroids)(see Figure 1)
   B-2 Transport Node in Low Lunar Orbit (See Figure 2)
   B-3 Space Station in Low Mars Orbit
Lunar-Surface-Based Sling

- "Minimal mass-driver" = fishing reel on Apollo 11
- Launcher for 10 kg payloads should fit in 1 shuttle
  - 300 m tether @ 54 rpm imposes <1000 g on payloads;
  - bearing loads are similar to those on a train axle;
  - 1 launch/5 min. uses <100 kW, boosts 1,000 tons/yr
- An orbiting tether facility collects launched payloads
- Collision and debris generation may be a major problem

Figure 1

EARTH-MOON TETHER-TRANSPORT INFRASTRUCTURE

AFV (AEROBRAKING FERRY VEHICLE)

1. AEROBRAKES AND IS CAPTURED BY TAMPS
2. IS UNLOADED & REFUELED
3. IS TETHER/ROCKET BOOSTED TO MOON
4. IS CAPTURED & LOADED BY LOTS
5. IS SLUNG BACK TOWARDS EARTH BY LOTS

LESS

(LUNAR EQUATOR SURFACE SLING)
THROWS ~10kg MOONROCKS INTO LOW-LIFETIME
(1 MONTH) EQUATORIAL ORBITS

TAMPS
(TETHER AND MATERIALS PROCESSING STATION)

1. CATCHES AEROBRAKED AFV, RETRIEVES & UNLOADS IT
2. PROCESSES MOONROCKS INTO LO, ETC
3. FUELS AFV & REBOOSTS IT TOWARDS MOON
4. RECOVERS MOMENTUM W/ELECTRODYNAMIC TETHER
5. ALSO CAPTURES, REFUELS, REBOOSTS AFV'S GOING TO GEO & DEEP SPACE

AFV
AFV

LOTS
(LUNAR ORBITING TETHER STATION)

1. CATCHES ROCKS, SPINS-UP, CATCHES AFV
2. LOADS AFV WITH ½ OF ROCKS
3. SPINS-UP & THROWS AFV TO TEI
4. DESPINS & LOADS OTHER ROCKS ON TETHER
5. SPINS-UP & DEBOOSTS ROCKS FOR MOMENTUM RECOVERY

LOTS

Figure 2
9. CONCLUSIONS AND RECOMMENDATIONS

- Tethers can uniquely provide for the accomplishment of the Space Station basic objectives
- Tether applications have solutions to significant Space Station problems
- Tether applications can greatly improve Space Station capabilities and operational efficiencies
- The complex interactions and interrelations of the many parameters of tether dynamics require improved understanding and an increased level of activity
- Tether applications should be incorporated into Space Station design for use at IOC
TETHERED ELEVATOR AND PLATFORMS AS SPACE STATION FACILITIES

SYSTEM STUDIES AND DEMONSTRATIVE EXPERIMENTS

PANEL PRESENTATION

"2ND APPLICATIONS OF TETHERS IN SPACE WORKSHOP"

VENICE, ITALY, OCTOBER 15-17, 1985
SCIENCE AND APPLICATIONS TETHERED PLATFORM

WHAT TO DO IT
- SEVERAL PROMISING APPLICATIONS: KEY CONCEPTS
  - MICROGRAVITY SCIENCE IN A CONTROLLED-G ENVIRONMENT
  - HIGHLY STABLE POINTING PLATFORM FOR ASTRONOMY AND EARTH SCIENCE
  - TRANSPORTATION TO AND FROM THE PLATFORM
  - ACCESSIBILITY/UNCONTAMINATED ENVIRONMENT

HOW TO DO IT
- AUTONOMY VS. SHARING OF SPACE STATION RESOURCES
- TETHER TECHNOLOGY: POWER LINE, COMMUNICATIONS LINK
- SPACE ELEVATOR AS MICROGRAVITY FACILITY
- POINTING PLATFORM BY MOVABLE ATTACHMENT POINT CONTROL
- SPACE ELEVATOR AS TRANSPORTATION FACILITY

WHY DO IT
- COMPARISON WITH CONVENTIONAL SOLUTIONS.
KEY CONCEPT - 1 - THE SPACE ELEVATOR

THE SPACE ELEVATOR IS AN ELEMENT ABLE TO MOVE ALONG THE TETHER IN A CONTROLLED WAY. THE MOST INTRIGUING TECHNOLOGICAL FEATURE IS THE ACTUATOR MECHANISM, DEVOTED TO CONTROL ELEVATOR MOTION ALONG THE TETHER. SEVERAL IDEAS ARE UNDER STUDY IN THE FOLLOWING TWO BROAD CLASSES:
- MECHANICAL DEVICES (FRICTION INTERACTION WITH TETHER)
- ELECTROMAGNETIC DEVICES (MAGNETIC INTERACTION WITH TETHER)

THE SPACE ELEVATOR MAY BE USED AS SPACE STATION FACILITY IN A TWO FOLD WAY.
- MICROGRAVITY FACILITY TO TAP DIFFERENT LEVELS OF RESIDUAL GRAVITY
- TRANSPORTATION FACILITY TO EASY ACCESS TETHERED PLATFORMS;
THE MICROGRAVITY SPACE ELEVATOR

THE SPACE ELEVATOR AS MICROGRAVITY FACILITY SEEMS TO BE THE MOST PROMISING CONCEPT. IN FACT THE MICROGRAVITY SCIENTISTS HAVE CONSIDERED THIS CONCEPT VERY INTRIGUING BECAUSE OF THE UNIQUE CAPABILITIES THAT IT ALLOWS.

TO EVALUATE THE PERFORMANCE OF A MICROGRAVITY FACILITY TWO MAIN FEATURES HAVE TO BE CONSIDERED:

- THE MICROGRAVITY ENVIRONMENT
- THE RESOURCES/LOGISTIC SUPPORT

UP TO NOW AN UNMANNED FREE-FLYING PLATFORM OFFERS THE BEST MICROGRAVITY ENVIRONMENT, BUT A SPACE STATION MAY OFFER THE BEST RESOURCES/LOGISTIC SUPPORT.

WHAT IS THE ELEVATOR CONCEPT ROLE?
THE MICROGRAVITY SPACE ELEVATOR (CONT'D)

THE MICROGRAVITY ENVIRONMENT

The order of magnitude of the minimum gravity acceleration attainable by elevator close to the center of orbit of a tethered system has been found $10^{-8}$ g. This result needs further analysis, mainly for the disturbances coming from the space station. However this result is comparable with minimum g-level by free-flying platform.

Tethered elevators allow a new microgravity environment. The new main characteristics of elevator microgravity environment are:

- Wide, continuous range of g-values obtainable
- Known g-direction
- G-quality higher than classical one
- Controllability vs time both in intensity and direction

The addition of the time dimension appears to be the most promising feature offered by elevator.
Duration and level of reduced Microgravity

- 6 -

15-17/10/85
Example of a typical metallurgical candidate payload

<table>
<thead>
<tr>
<th>Microgravity Facility</th>
<th>Free - Flying Space Platforms</th>
<th>Tethered Space Elevator</th>
</tr>
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<tbody>
<tr>
<td>Micro-G Environment</td>
<td>G-value</td>
<td>Direction</td>
</tr>
<tr>
<td></td>
<td>Single Point</td>
<td>Unknown</td>
</tr>
<tr>
<td></td>
<td>Variable</td>
<td>Known</td>
</tr>
<tr>
<td>Controllability Vs Time</td>
<td>NO</td>
<td>YES</td>
</tr>
<tr>
<td></td>
<td>both in intensity and direction</td>
<td></td>
</tr>
<tr>
<td>G-Noise Control</td>
<td>NO</td>
<td>YES</td>
</tr>
<tr>
<td>G-Quality</td>
<td>Medium</td>
<td>High</td>
</tr>
</tbody>
</table>

Microgravity Environment Comparison
THE MICROGRAVITY SPACE ELEVATOR (CONT'D)

RESOURCES/LOGISTIC SUPPORT

The microgravity elevator will operate near the space station. A proposed system configuration is constituted by S/S, 10 km tether, a shuttle external tank as a ballast, and the elevator. In this configuration, the elevator moves along 1 km of tether from the station; it is possible with a short and slack cable to use space station resources, including:

- Electrical power by power line transmission
- Data, control and monitoring by optical fibre link

Moreover, the elevator can be retrieved at any time providing easy access to repair malfunctions and exchange experiments, samples, etc.

The elevator is able to fully utilize the space station support and to avoid the S/S contaminated environment from a micro-G point of view by tether mediation.
THE MICROGRAVITY ELEVATOR CONCEPT

Space Station

Microgravity Elevator

Shuttle ET

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SG-PB-AI-018

15-17/10/85
THE TRANSPORTATION SPACE ELEVATOR

THE IDEA OF USING LARGE TETHERED PLATFORMS CONNECTED TO THE SPACE STATION BY POWER LINE AND COMMUNICATIONS LINK (VIA TETHER TECHNOLOGY) MAKES UNREALISTIC FREQUENT OPERATIONS OF DEPLOYMENT AND RETRIEVAL.

ON THE OTHER HAND, THE PLATFORM MAY REQUIRE EASY ACCESS FOR MAINTENANCE, SUPPLY OF CONSUMABLES, MODULE AND EXPERIMENT EXCHANGE.

THE ELEVATOR, AS TRANSPORTATION FACILITY ABLE TO MOVE ALONG THE TETHER TO AND FROM THE PLATFORM, MAY BE THE TOOL FOR TETHERED PLATFORM EVOLUTION.

SEVERAL TECHNOLOGICAL PROBLEMS HAVE TO BE ANALYSED TO VALIDATE THE FEASIBILITY OF THIS IDEA, BUT THE FIRST STEP IS TO EVALUATE THE DYNAMICS OF THE SYSTEM DURING THE ELEVATOR MOTION.
THE TRANSPORTATION SPACE ELEVATOR (CONT'D)

DYNAMICS MODELS

TWO DIFFERENT MODELS WERE DEVELOPED TO SIMULATE THE SPACE ELEVATOR DYNAMICS:
- 5 D.O.F. MODEL TO SIMULATE SYSTEM C.G., SPACE STATION, PLATFORM AND ELEVATOR MOTION.
  ASSUMPTIONS: o STATION, ELEVATOR AND PLATFORM ARE POINT MASSES
  o TETHER ELASTICITY IS NEGLECTED
  o ONLY IN-PLANE MOTION IS MODELLED

- CONTINUOUS MODEL TO SIMULATE TETHER LATERAL AND LONGITUDINAL VIBRATIONS ORIGINATED BY ELEVATOR MOTION.
  ASSUMPTIONS: o ELASTIC AND ORBITAL EFFECTS ONLY WEAKLY COUPLED
  o TENSION CONSTANT ALONG THE TETHER
  o ELEVATOR MOTION SIMULATED AS AN EXTERNAL FORCE
  o ELEVATOR TRAVELS WITH CONSTANT VELOCITY.
THE TRANSPORTATION SPACE ELEVATOR (CONT'D)

SYSTEM DYNAMICS

SYSTEM PARAMETERS:
SPACE STATION MASS = $10^6$ Kg
ELEVATOR MASS = $5 \cdot 10^3$ Kg
PLATFORM MASS = $5 \cdot 10^4$ Kg
TETHER LENGTH = 10 Km
INITIAL ORBIT = CIRCULAR, 500 Km HEIGHT

ELEVATOR FREE MOTION WAS INVESTIGATED BY IMPARTING THE NECESSARY IMPULSE TO REACH THE C.O.G. FROM THE SPACE STATION.
SYSTEM DYNAMICAL BEHAVIOUR SHOWS THAT VELOCITY CONTROL IS NEEDED.

CONTROLLED TRANSFER WAS ANALYSED FOR CONSTANT TRANSFER VELOCITY.
FOR SMALL VELOCITIES, MOTION IS STABLE AND TETHER DEFLECTION IS BOUNDED. AS VELOCITY INCREASES PERTURBING OSCILLATIONS ARE EXCITED.
ELEVATOR - DYNAMICS OF FREE MOTION
ELEVATOR - DYNAMICS OF CONTROLLED MOTION

TIME REQUIRED = 6875 SEC.

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SG-PB-A1-018

- 14 - 15-17/10/85
INPLANE-RADIAL DYNAMIC VIEW
TETHER LATERAL VIBRATIONS

SYSTEM PARAMETERS:

- **Platform Mass**: $5 \times 10^4$ Kg
- **Elevator Mass**: $5 \times 10^3$ Kg
- **Tether Length**: 10 Km
- **Orbit**: Circular, 500 Km Height

Tether lateral vibrations are induced by the Coriolis force acting on the elevator as it moves along the tether.

The elevator was assumed to travel with 2 m/s constant velocity, the first twenty modes were included and the tether damping was neglected.

The viewing of the vibrations of selected points along the tether shows that the smaller the distance from the S/S the greater the effect of higher modes.

Tether shape as a function of time is two quite linear sections with slope change at elevator position.
TETHER VIBRATIONS CAUSED BY ELEVATOR MOTION
SATP(50 TON), ELEV(5 TON), TL=10 KM, VEL=2 M/S

LATITUDINAL DISPLACEMENT VS TIME: X=1,2,4 KM
LATITUDINAL DISPLACEMENT VS TIME: X=6,8,10 KM

TURIN JUNE 1985
TSS APPLICATIONS
TETHER VIBRATIONS CAUSED BY ELEVATOR MOTION
SATP(50 TON), ELEV(5 TON), TL=10 KM, VEL=2 M/S

LAT. DISP. VS TETHER DIST. T=500, 1000, 2000 SEC

LAT. DISP. VS TETHER DIST. T=3000, 4000, 5000 SEC
THE TRANSPORTATION SPACE ELEVATOR (CONT'D)

TETHER LONGITUDINAL VIBRATIONS

SYSTEM PARAMETERS SAME AS FOR LATERAL VIBRATIONS.

TETHER LONGITUDINAL VIBRATIONS ARE INDUCED BY ELEVATOR CONTROL FORCES TO MAINTAIN CONSTANT VELOCITY OF 2 M/S.

THE FIRST TWENTY MODES WERE INCLUDED AND THE TETHER DAMPING WAS NEGLECTED.

THE DISPLACEMENTS ARE RELATIVE TO TETHER STRETCHED CONFIGURATION UNDER CONSTANT TENSION.

THE VIEWING OF DISPLACEMENTS FOR THE COMPLETE TRANSFER OF THE ELEVATOR FROM THE S/S TO THE SATP SHOWS ONLY DISPLACEMENTS CAUSED BY MASS TRANSFER. VIBRATIONS ARE NO APPRECIABLE.

THE PLOTS OF THE FIRST 250 SEC. OF THE MOTION CONFIRMS THAT VIBRATIONS ARE PRESENT BUT OF QUITE NEGLIGIBLE AMPLITUDE.
TETHER VIBRATIONS CAUSED BY ELEVATOR MOTION
SATP(50 TON), ELEV(5 TON), TL=10 KM, VEL=2 M/S

LONGITUDINAL DISPLACEMENT VS TIME: X=1, 2, 4 KM
LONGITUDINAL DISPLACEMENT VS TIME: X=6, 8, 10 KM
TETHER VIBRATIONS CAUSED BY ELEVATOR MOTION
SATP(50 TON), ELEV(5 TON), TL=10 KM, VEL=2 M/S

LONGITUDINAL DISPLACEMENT VS TIME: X=4 KM

LONGITUDINAL DISPLACEMENT VS TIME: X=10 KM
KEY CONCEPT - 2 - THE POINTING PLATFORM

THE USE OF A TETHERED PLATFORM AS A SUPPORT FOR OPERATING ASTROPHYSICAL AND OTHER OBSERVATIONAL INSTRUMENTS REQUIRING PRECISION POINTING AND CONTROL PRESENTS SEVERAL ADVANTAGES:
- ELECTRICAL POWER FROM SPACE STATION
- HIGH CAPACITY OF DATA TRANSMISSION BY OPTICAL FIBRES
- POSSIBILITY OF HUMAN INTERVENTION
- EASE OF ACCESS
- FREEDOM FROM CONTAMINATION

THIS CONCEPT COULD BECOME ATTRACTIVE ONCE IT IS DEMONSTRATED THAT A POINTING PERFORMANCE ON THE ORDER OF ARCSECONDS CAN BE REACHED BY THE COMBINATION OF DISTURBANCES ATTENUATION THROUGH TETHER AND ACTIVE CONTROL OF A MOVABLE ATTACHMENT POINT.

THIS IDEA REPRESENTS A NEW WAY TO CONTROL THE ATTITUDE OF A TETHERED BODY.
THE POINTING PLATFORM (CONT’D)

MOVABLE TETHER ATTACHMENT POINT

THEORETICAL CONTROL PHILOSOPHY WAS INVESTIGATED

- INTRODUCTION OF DAMPING TERM PROPORTIONAL TO ATTITUDE ANGULAR RATE
- ROUGH DETERMINATION OF CRITICAL DAMPING COEFFICIENTS
- INTRODUCTION OF STABILIZATION TERM TO COMPENSATE DISTURBANCES DUE TO TETHER DYNAMICS.

CHECK SIMULATION WAS PERFORMED WITH DATA FROM TSS ELECTRODYNAMIC MISSION

- HARDWARE AND CONTROL ERRORS WERE NEGLECTED
- ATTITUDE (ANGLES, ANGULAR RATES) AND TETHER TENSION (3-AXIS) MEASUREMENT WERE ASSUMED

- DRAG, ELECTRODYNAMIC FORCES (1 A), TETHER LIBRATIONS AND FIRST TWO LONGITUDINAL VIBRATIONS WERE INCLUDED IN THE MODEL.
RESULTS ARE ENCOURAGING. THEORETICAL CONTROL ALLOWS STABILIZATION TO ARCSEC MAGNITUDE.

AREAS TO BE INVESTIGATED:
- MECHANISM, SENSORS AND CONTROL ERRORS
- MOUNTING MISALIGNMENTS
- THERMO-STRUCTURAL STABILITY.
ROLL ANGLE (ATTACHMENT POINT AT THE REST)

ROLL ANGLE (ATTACHMENT POINT CONTROL)
THE POINTING PLATFORM (CONT'D)

INITIAL CONFIGURATION

As initial step to tethered platforms evolution, a medium size pointing platform seems the most suitable facility for a class of observational applications.

In fact if ambitious astrophysical projects justify the design of a dedicated complex free-flyer, medium observational applications of relatively short duration could take advantage of a standard pointing facility able to arrange at different time several observational instruments.

This pointing facility could allow great reduction of costs, avoiding the cost of separate service functions for each application.

Preliminary configuration study of the pointing platform is in progress.
THE POINTING PLATFORM (CONT'D)

PRELIMINARY GENERAL REQUIREMENTS

- DEPLOYMENT TO 10 KM FROM THE SPACE STATION
- POWER TRANSMISSION AND DATA LINK BY TETHER TECHNOLOGY
- INERTIAL POINTING AND STABILIZATION ABOUT 3-AXIS
- RESCUE OPERATION COMPATIBLE
- MOUNTING OF PAYLOADS BOTH FOR ASTROPHYSICAL OBSERVATION AND FOR EARTH SURVEY
- STANDARD SERVICE MODULE WITH CENTRALIZED FUNCTIONS:
  - ELECTRICAL POWER SUPPLY
  - DATA TRANSMISSIONS
  - ON-BOARD DATA HANDLING
  - AUXILIARY PROPULSION SYSTEM
  - ATTITUDE MEASUREMENT AND CONTROL
  - STANDARD PAYLOADS INTERFACE.
POINTING PLATFORM - PRELIMINARY CONFIGURATION

Platform configuration for payload to be tilted (e.g. space observation)

Platform configuration for fixed payload (e.g. earth observation)
TECHNICAL ISSUES

0 SPACE STATION IMPACTS
   - STATIC ACCELERATION LEVELS \(10^{-4} \, g\)
   - DEPLOYER SYSTEM LOCATION REQUIREMENTS
   - ELECTRICAL POWER SUPPLY REQUIREMENTS
   - DATA HANDLING REQUIREMENTS
   - OPERATIONS CONTROL

0 TETHER
   - DEBRIS COLLISION HAZARD
   - ELECTRICAL POWER LINE TECHNOLOGY
   - OPTICAL FIBRE TECHNOLOGY
   - DURABILITY
   - DESIGN FOR PERIODICAL RECOIL
TECHNICAL ISSUES (CONT'D)

0 DYNAMICS AND CONTROL
   - ELEVATOR MOTION DYNAMICS AND CONTROL
   - PLATFORM ATTITUDE DYNAMICS AND CONTROL
   - TETHER DYNAMICS

0 NEW SPACE TECHNOLOGY
   - MECHANISMS FOR ALONG TETHER MOTION
   - MECHANISMS FOR MOVABLE ATTACHMENT POINT CONTROL
   - DEPLOYER SYSTEMS
   - COMPLEX-MULTIFUNCTION TETHERS.
BENEFITS ANALYSIS

- THE SPACE ELEVATOR
  - UNIQUE CAPABILITY AS MICROGRAVITY FACILITY
  - THE BEST FACILITY TO ACCESS LARGE TETHERED PLATFORMS

- THE POINTING PLATFORM
  - HIGH POINTING PERFORMANCE
  - HIGH CAPACITY OF DATA TRANSMISSION
  - ACCESS READINESS
  - FREEDOM FROM CONTAMINATION
  - COST EFFECTIVENESS FOR A LARGE CLASS OF OBSERVATIONAL APPLICATIONS.
SHUTTLE-DEPLOYED "DOWN-SCALED PLATFORM"

DEMONSTRATION OF FEASIBILITY AND PERFORMANCE IS NEEDED BEFORE APPLICATION IS PROPOSED FOR THE SPACE STATION.

TO SAVE TIME AND LIMIT COSTS: USE OF STANDARD TSS DEPLOYER.

QUESTION TO BE ANSWERED:
- o TO WHAT EXTENT IS DOWN-SCALING MEANINGFUL ("SCALING LAWS")
- o WHAT FEATURES ARE TO BE MODELLED:
  - MICROGRAVITY ENVIRONMENT
  - STABILITY PROPERTIES
  - OTHER
- o IMPLEMENTATION OF CONCEPT
  - ELEVATOR
  - MOVABLE TETHER ATTACHMENT POINT
AN ASSESSMENT STUDY OF THE CAPABILITIES OF A SATP REDUCED-SIZE MODEL TO GIVE SATP FEASIBILITY AND PERFORMANCE DEMONSTRATION WAS PERFORMED.

PARTICULAR REFERENCE WAS MADE TO APPLICATIONS OF MICROGRAVITY AND OF VERY FINE INSTRUMENT POINTING. SPECIAL CARE WAS GIVEN TO THE ELEVATOR MOTION OUTLINE.

ON THE BASIS OF THIS ANALYSIS SOME CONSIDERATIONS CAN BE MADE ABOUT THE EXPERIMENTAL PROBLEM:

- FULL SIMILARITY OF ALL EFFECTS IS POSSIBLE ONLY FOR ONE-TO-ONE SCALE. IT SEEMS ALSO TO BE NOT NECESSARY.
- RESTRICTED SIMILARITY IS POSSIBLE.
  SCALED SATP KEEPS FULL EFFECTIVENESS FOR TESTING Refined MODELS
  OF PHENOMENA (IT IS COMMON ATTITUDE IN THE FIELD OF COMPLEX MODEL-
  LING).

- THE DIFFERENT ASPECTS DEALING WITH THE PROPOSED CONCEPTS AND THE
  COMPLEXITY OF PHENOMENA SEEMS TO MAKE ESSENTIAL THE IN-FLIGHT
  TESTS.
CONFIGURATION STUDY

THE NECESSITY TO UTILIZE THE ON-GOING TETHERED SATELLITE SYSTEM APPEARS EVIDENT FOR COSTS AND SCHEDULE REASONS.

AS A GENERAL APPROACH:
- THE INTERFACES AND THE GENERAL REQUIREMENTS DEFINED FOR THE TSS CANNOT BE CHANGED.
- ONLY THE TSS-SATELLITE MUST BE CHANGED, AS LITTLE AS POSSIBLE IN ORDER TO MAXIMIZE THE EXISTING HARDWARE UTILIZATION.

A CONFIGURATION STUDY WAS PERFORMED IN ORDER TO EVALUATE THE SATELLITE DESIGN CHANGES REQUIRED TO LOCATE THE MOVABLE ATTACHMENT MECHANISMS AND THE ELEVATOR INSIDE THE SATELLITE.

THE MOVABLE ATTACHMENT POINT CONCEPT REQUIRES ONLY SMALL MODIFICATIONS OF THE CURRENT DESIGN.

THE ELEVATOR HOUSED IN THE SATELLITE REQUIRES LARGE DESIGN MODIFICATIONS (E.G., THE TANK HAVE TO BE SHIFTED).
ELEVATOR ACCOMMODATION STUDY

PRESENT TSS-S
CONFIGURATION

HYTHOTESIS FOR
ELEVATOR
ACCOMMODATION

ROOM DEDICATED TO MOBILE
ATTACH. POINT MECHANISM
PROPOSED CONFIGURATION

THE INTRODUCTION OF BOTH CONCEPTS (ELEVATOR AND MOVABLE ATTACHMENT POINT) ON THE PRESENT SATELLITE DESIGN APPEARS VERY CRITICAL BECAUSE OF THE VARIATION INDUCED ON THE STRUCTURE.

MOUNTING ONLY THE MOVABLE ATTACHMENT POINT HARDWARE ON THE SATELLITE SEEMS TO BE A VERY CHEAP SOLUTION CONSIDERING THAT THE DESIGN MODIFICATION COULD BE SIMPLE.

THE ELEVATOR COULD BE DESIGNED TO PERMIT ITS MOUNTING ON THE TETHER (BY MEANS OF THE SHUTTLE RMS) ONCE THE SATELLITE IS FAR OFF THE DEPLOYER AND RECOVERED BEFORE SATELLITE RETRIEVAL.

A PRELIMINARY STUDY OF THIS CONFIGURATION IS IN PROGRESS. THE SCALED ELEVATOR WILL BE DESIGNED TO PROVIDE:

- RMS GRAPPLE FIXTURE
- FRONT SLOT FOR THE POSITIONING ON THE TETHER
- FINAL TETHER GUIDE-CAPTURE SENSORS AND MECHANISMS.
SCALED ELEVATOR MOUNTING ON THE TETHER
PRELIMINARY ELEVATOR CHARACTERISTICS

- **DIMENSIONS**: 0.65 x 0.65 x 1.05 m
- **MASS**: 70 Kg
- **MAX VELOCITY**: 2 m/s (TETHER REFERENCE FRAME)
- **POWER CONSUMPTION**: ≤ 100 W
- **ONE-AXIS ATTITUDE CONTROL (YAW AXIS) BY MAGNETIC COILS**
- **PASSIVE THERMAL CONTROL AND DEDICATED HEATERS**
- **HYBRID STRUCTURE (COMPOSITES, AL ALLOYS)**
- **FRICTION DRIVE MECHANISM**
- **S-BAND COMMUNICATIONS** (5 Kb/sec-tentative)
Scaled Elevator - Preliminary Configuration

Legenda:

1. Tether (working position)
2. Grapple fixture mounted on removable back cover
3. Back room (P/L dedicated)
4. Front rooms (service dedicated)
5. Hinges for the equipment mounting in front rooms
6. Front slot for the elevator positioning on tether
7. Final tether capture and guide mechanism (two positions)
8. Drive mechanism
9. Cargo bay joint points (TBD) on this side
10. Main frame
CONCLUSIONS

- TETHERED ELEVATOR AND PLATFORMS COULD IMPROVE THE SPACE STATION SCIENTIFIC AND APPLICATIVE CAPABILITIES.
- THE SPACE ELEVATOR PRESENTS UNIQUE CHARACTERISTICS AS MICROGRAVITY FACILITY AND AS A TETHERED PLATFORM SERVICING VEHICLE.
- POINTING PLATFORMS COULD REPRESENT A NEW KIND OF OBSERVATION FACILITY FOR LARGE CLASS OF PAYLOADS.
- THE DYNAMICAL, CONTROL AND TECHNOLOGICAL COMPLEXITY OF THESE CONCEPTS ADVISES DEMONSTRATIVE EXPERIMENTS.
- THE ON-GOING TETHERED SATELLITE SYSTEM OFFERS THE OPPORTUNITY TO PERFORM SUCH EXPERIMENTS.
- FEASIBILITY STUDIES ARE IN PROGRESS.
  THE MAJOR EFFORT WILL BE DEDICATED TO OUTLINE CONCEPTS AND TECHNIQUES OF SUCH A DEMONSTRATION.
ROLES FOR TETHERS ON AN EVOLVING SPACE STATION

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SUMMARY OF CONTRACT WORK STATEMENT:

1. Develop a scenario for evolution of space station tether capabilities. Minimize tether-imposed constraints on station development & operations, but derive maximum benefit from a mutually compatible combination of:

   - Electrodynamic tethers for power, thrust, and libration control;
   - Momentum transfer operations involving the STS or upper stages;
   - Aeromaneuvering devices for space station orbital plane change;
   - Tethered constellations and tether/free-flyer combinations.

2. For advanced tether facilities orbiting the moon, determine:

   - Stationkeeping deltaVs to stay in precise equatorial or polar orbits;
   - Ratio of facility mass to maximum payload mass (surface-orbit-escape);
   - Electric-thruster power requirements & maximum rendezvous frequencies;
   - Overall capabilities and major constraints on such facilities.
### ATTRACTIVE ROLES IDENTIFIED DURING STUDY:

<table>
<thead>
<tr>
<th>Facility/Operation</th>
<th>Location:</th>
<th>Operational:</th>
</tr>
</thead>
<tbody>
<tr>
<td>1. Gravity-Gradient Fluid Settling</td>
<td>Near top &amp; bottom</td>
<td>Usually</td>
</tr>
<tr>
<td>2. Tethered MicroGee Platform</td>
<td>Station CG</td>
<td>Usually</td>
</tr>
<tr>
<td>3. Tethered Earth-Viewing Platform</td>
<td>Bottom</td>
<td>Usually</td>
</tr>
<tr>
<td>4. Electrodynaminc Power Management</td>
<td>Top or bottom</td>
<td>As needed</td>
</tr>
<tr>
<td>5. Electrodynaminc OMV</td>
<td>LEO free-flyer</td>
<td>As needed</td>
</tr>
<tr>
<td>6. Payload Boosting, STS Deboosting</td>
<td>Top &amp; bottom</td>
<td>Occasionally</td>
</tr>
<tr>
<td>7. Payload Juggling by Tether</td>
<td>Top &amp; bottom</td>
<td>Occasionally</td>
</tr>
<tr>
<td>8. Tethered Docking of STS by SS</td>
<td>Bottom</td>
<td>Occasionally</td>
</tr>
<tr>
<td>9. Hazardous or contaminating ops.</td>
<td>Bottom</td>
<td>Occasionally</td>
</tr>
<tr>
<td>10. Lunar-Orbiting Tether Facility</td>
<td>Lunar orbit</td>
<td>When needed</td>
</tr>
<tr>
<td>11. Lunar-Surface-Based Sling</td>
<td>Lunar equator or pole</td>
<td>When needed</td>
</tr>
<tr>
<td>12. Mars-Orbiting Tether Facilities</td>
<td>Various Mars orbits</td>
<td>When needed</td>
</tr>
</tbody>
</table>
1. GRAVITY-GRADIENT FLUID SETTLING

- Gravity-gradient fluid settling need not be limited to propellants: Fluids are also used in science, materials processing, & habitation.

- Gravity-gradients of 20–30 microgee may often be enough for settling; when more is needed, all that is needed is to deploy ANY tethered mass.
2. TETHERED MICROGEE PLATFORM

- This facility can be moved when the station CG moves, or another tether can be adjusted to trim the station CG.
3. TETHERED EARTH-VIEWING PLATFORM

- Minimizes contamination & disturbances.
- Provides stationkeeping & attitude control.
- Allows convenient power & data transfer.
- Allows station CG adjustment (adjust length).
4. ELECTRODYNAMIC POWER (& MOMENTUM) MANAGEMENT

- Off-peak power can be used for orbit boosting.
- Stored orbital energy can offset drag makeup, or can be recovered during peak-power times.
5. AN ELECTRODYNAMIC ORBITAL MANEUVERING VEHICLE

- ~10 km tether (1 cm diameter aluminum + 3 kV insulation)
- In the middle: OMV-like RCS, TV, end effectors, etc.
- At each end: variable voltage DC power supply (0-3 kV) electron gun and large sail (or ion emitter)
- DC & AC currents can alter all 6 orbital elements. In LEO:

  about 1.3 kWh is required per tonne.km altitude change
  altitude changes over 100 km/day may be possible
  inclination changes over .5 deg/day may be possible
6. PAYLOAD BOOSTING, STS DEBOOSTING

- Large boosts & deboosts must be paired so SS can return to formation. Pairing can also be with electrodynamic ops or tethered rendezvous.

- Propellant savings scale with station loads & orbit change: for each 100 lb load & 1 nmi delta-a, 200 lbs/op is saved. Questions:

  What loads should the station be designed or scarred for?
  What are maximum allowable short-term orbit perturbations?

Effects of Tether Deployment and Release

\[ M_1 r_1 + M_2 r_2 = M_{12} r_{12} \]

\[ \{ \begin{array}{l}
7L \text{ if hanging release} \\
<14L \text{ if swinging release} \\
>14L \text{ if spun or winched}
\end{array} \]
7. PAYLOAD JUGGLING BY TETHER: NEAR & FAR-TERM POTENTIALS

Using a Momentum Transfer Tether to "Juggle" Payloads:

Station-Tended Swarm of Free-Flyers:

Payload is boosted & released by hanging or swinging tether; Released payload flies free for months while its orbit decays; When payload passes under station, tether recaptures it. Station does any necessary servicing & maintenance on payload.

Single-orbit aerodynamic sensing, testing, or air collection:

Vehicle is slung upwards from station by spinning tether; Station damps tether spin by active length control; 3/4 orbit after release, vehicle reaches perigee; 1/4–1/2 orbit later, vehicle is recaptured from decayed orbit.
8. TETHERED DOCKING OF SHUTTLE WITH SPACE STATION

- Hardware & constraints mostly common w/STS deboost.
- Vary tether length with prop. needs & solar cycle.
- Savings scale with tether length up to about 60 km.
- Potential 60% increase in STS throughput!

Slightly lower apogee
Much lower perigee
Tethered deboost
Cryo scavenging
9. HAZARDOUS OR CONTAMINATING OPERATIONS

- Tether isolates contaminating & hazardous ops, while providing attitude, power, stationkeeping.

- Downward deployment shortens debris orbital life.

- An example: skin, cut up, & melt down ETs:
10. LUNAR-ORBITING TETHER FACILITY

- Long swinging tethers or short spinning ones?
- Three ranges of deltaV have utility:
  - small, for capturing payloads in orbit \((Mt \ll Mp)\)
    - 850 m/s, to get 2/3 of surface-TEI deltaV \((Mt \approx Mp)\)
  - 1700 m/s, to pick up objects on surface \((Mt \approx 10Mp)\)

Required Technology:
- Advanced tether controls
- Powerful tether deployer
- Maneuverable tether tip
- Large power supply
- High-Isp propulsion
- Propellant extraction

Transport Capabilities:
- Surface-Orbit-Escape
- Handles large payloads
- Max g-loads < .3 gee
- Rocket backup if desired
- Two-way mass flow is "free"
- Net boosting costs \(~25\) MWH/tonne
- Polar orbit: frequent access to poles & infrequent access everywhere
- Equatorial: frequent access to equator
11. LUNAR-SURFACE-BASED SLING

- "Minimal mass-driver" = fishing reel on Apollo 11?
- Launcher for 10 kg payloads should fit in 1 shuttle.
  300 m tether @ 54 rpm imposes <1000 gees on payloads;
  Bearing loads are similar to those on a train axle;
  1 launch/5 min. uses <100 kW, boosts 1,000 tonnes/yr.
- An orbiting tether facility collects launched payloads.
- Collision & debris generation may be a major problem.
12. MARS-ORBITING TETHER FACILITIES

Mars & its moons are uniquely suited to tether operations:

- Both moons are in relatively low equatorial orbits;
- Most required deltaVs are well under 1 km/sec, so $M_t < M_p$.

A system of 3 facilities could have powerful capabilities:

- Sling on Phobos (inner moon) throws mass into low-periapsis orbits;
- Station in low orbit collects mass from Phobos & from atmosphere;
- Facility in eccentric orbit throws payloads to earth or asteroids.

Phobos-Based Sling  Mars Space Station  Tether "Upper Stage"
CONCLUSIONS:

- Most proposed tether concepts on a space station are compatible: full-time operation is not needed, so time-sharing can be done.
- Many concepts are synergistic (e.g., STS deboost & rendezvous), so cost-benefit studies of single concepts understate the true benefits.
- Some concepts may require station scars IN THE DESIGN PHASE.

RECOMMENDATIONS:

- NASA & Phase-B contractors should study concepts #1-#9 for relevance.
- Cost-benefit studies should include combinations of concepts #1-#9.
- Microgee tethered platforms should be built & tested on KC-135 & STS.
- Already-flown "micro-gee" experiments should be reflown on TSS-1, to see if 20-40 microgees (typical g.g. levels on station) make a difference.
III

WORKSHOP SUMMARY OF RECOMMENDED APPLICATIONS AND DEMONSTRATIONS
The Friday morning session of the Applications of Tethers in Space Workshop in Venice included the panel co-chairmen, and was devoted to listing those applications which would be appropriate for the following eras:

A. Shuttle
B. Space Station - IOC
C. Space Station - Post IOC
D. Post IOC - General

Some discussion was also devoted to demonstration and TSS missions, which would provide high science return and/or proof of an operational capability. This input is provided in outline form only. Detailed discussion of most of these applications may be found in the proceedings, or the attached references.

A. Operational Applications of Tethers for the Shuttle era.

1. Small Payload Placement
2. Electrodynamic Power Supply
3. Multiprobe (Constellation) System
4. Open Wind Tunnel
5. Gravity Controlled Experiments

B. Space Station Facilities and Capabilities in the IOC era.

1. Variable Length Tether for Space Station C.G. Management
2. Electrodynamic Power Supply
3. Electrodynamic Thrust (Drag Makeup)
4. Tethered Platform (Short Term Missions)
5. "Zero G" Laboratory using a Tethered Elevator
6. Deboosting Small Cargo Modules
7. Electrodynamic Tether for Research
8. Multi-probe "Beads on String" Constellation
C. Space Station in the Post IOC era.

1. Tethered Orbiter Deployment with OMS Propellant Scavanging
2. Tethered Launch of OTV
3. Remote Docking of Orbiter
4. Tethered Propellant Depot and Fuel Transfer
5. Tethered Antenna Farm
6. Remote Wake Shield

D. Post IOC - General

1. Spinning Manned Facility
2. Tethers on Platforms
3. Electrodynamic OMV
4. Remote Aerobraking
5. Two Dimensional Constellations
6. Station in LEO to Capture Launch Vehicles in Suborbital Trajectories (LEO Node)
7. Higher Orbit Tether Transfer Nodes
8. Rotating Tether (Sling) attached to the Moon or an Asteroid to Eject Surface Material into Orbit
9. Tether Facilities at other planets

In addition to these applications, some discussion was given to demonstration missions and their candidate objectives. The following are somewhat in chronological order of development.

A. Plasma Motor Generator (McCoy - 86)
   o Demonstrate feasibility and performance of hollow cathode
   o Dynamics and Temperature Response
   o Pulse Effects on Ambient Plasma
   o KU-Band Radar Tests

(Frequent reflights are planned)
B. Disposable Deployer (Carroll - 87)
   o Test Successful Release of Tether
   o Vibration Dynamics
   o Aerobraking Effects of Tether
   o Aerothermal Effects using Balloon
   o Tether Recoil and Shape
   o Conduct low gravity experiments on orbiter during Tether deployment
     (Frequent reflights are planned)

C. Spinning Orbiter with Tethered Satellite
   o Test Fluid Settling and Slosh
   o Conduct low-gravity science

D. Tethered Satellite System (TSS-1)
   o Accurate Dynamics Verification
   o Data Collection for other applications
   o Passive Electron/Ion Collection Efficiency
   o Effectiveness of Hollow Cathode on Orbiter
   o Test Accelerometers on Orbiter
   o Test Tensiometers on Satellite
   o Satellite Passive Retrieval mode for backup

E. Shuttle released Dumbell Satellite
   o Test Rendezvous Feasibility
   o Dynamic Behavior
   o Elevator attachment

F. Tethered Centaur
   o Test feasibility

G. Kinetic Isolation Tether Experiment (KITE)
   o Pointing Stability and accuracy
   o Disturbance Isolation
   o Test Extension Cord Concept
   o Do low gravity experiment on orbiter
H. Tethered Satellite System (TSS-2)
   o Planned Aerodynamic Experiments
   o Low Gravity on Orbiter
   o Possible Elevator test

I. Tethered Satellite System (TSS-3)
   o (See TSS-1 Applications)
   o Plasma Contactor on Orbiter and Satellite
   o Test Spin Mode
APPENDIX A

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APPENDIX C

WORKSHOP AGENDA
APPLICATIONS OF TETHERS IN SPACE WORKSHOP
AGENDA
15-17 October 1985

14 October, 1985 - Monday
6:00pm -- 9:00am REGISTRATION

15 October, 1985 - Tuesday
8:00am -- 8:30am REGISTRATION

SESSION I - INTRODUCTION
8:30am -- 8:45am Orientation and Purpose...L. Guerriero
8:45am -- 9:00am Welcome...representing the Mayor of Venice, Mr. A. Salvadori
9:00am -- 9:30am Opening Address...Sen. Luigi Granelli, Minister of Scientific Research and Technology
9:30am -- 10:00am BREAK
10:00am -- 10:15am Keynote Address...T. Bekey

SESSION II - GENERAL PRESENTATIONS
10:15am -- 10:30am Tethered Satellite System...J. Sisson
10:30am -- 10:45am Tethered Satellite Design...G. Manarini, A. Lorenzonii
10:45am -- 11:15am Tether Fundamentals...J. Carroll/S. Bergamaschi
11:15am -- 11:45am Science Applications...F. Mariani/P. Penzo
11:45am -- 12:15pm Electrodynaminc Interactions...M Dobrowolny/J. E. McCoy
12:15pm -- 12:45pm Transportation...G. von Tiesenhausen
12:45pm -- 2:30pm LUNCH
2:30pm -- 3:00pm Variable and/or Artificial Gravity...L. Napolitano/K. Kroll
3:00pm -- 3:30pm Space Station...W. Nobles/P. Merlin
3:30pm -- 4:00pm Technology and Test...C. Buongiorno/P. Siemons
4:00pm -- 4:30pm Constellations...E. Lorenzini
4:30pm -- 5:15pm Tether Dynamics Movie...J. Loftus
7:15pm RECEPTION HOSTED BY THE MAYOR OF VENICE
APPLICATIONS OF TETHERS IN SPACE WORKSHOP
AGENDA (CONT.)
15-17 October 1985

16 October, 1985 - Wednesday

SESSION III - PANEL MEETINGS

8:30am -- 12:00pm Panels Meet in Assigned Rooms
12:00pm -- 2:00 pm LUNCH
2:00pm -- 4:00pm Panels Meet in Assigned Rooms
4:00pm -- 5:00pm Plenary Session - Preliminary Panel Reports
8:00pm -- 11:00pm GALA DINNER...J. ARNOLD GUEST SPEAKER

17 October, 1985 - Thursday

SESSION III - PANEL MEETINGS (CONTINUED)

8:30am -- 12:00pm Panels Meet in Assigned Rooms
12:00pm -- 1:30pm LUNCH

SESSION IV - WORKSHOP SUMMARY

1:30pm -- 3:30pm Final Report Preparation - Panel Chairmen Meet
3:30pm -- 5:30pm Plenary Session - Summary of Workshop Recommendations

18 October, 1985 - Friday

8:30am -- 12:30pm Panel Chairmen Turn in Final Panel Reports,
Legibly Prepared with Sketches, Diagrams and Reproducible Graphics as Available
APPENDIX D

BIBLIOGRAPHY
VENICE WORKSHOP
APPLICATIONS OF TETHERS IN SPACE
LIBRARY


44. The Process of Space Station Development Using External Tanks, California Space Institute of the University of California, Scripps Institution of Oceanography, La Jolla, CA, Report to Director of the Space Station Review Project, Office of Technology Assessment, 11 March 1983.


The proceedings of the second workshop on Applications of Tethers in Space, sponsored jointly by the Italian National Space Plan, CNR, and NASA, held in Venice, Italy, October 15-17, 1985, are presented here. The workshop was attended by persons from government, industry, and academic institutions to discuss the rapidly evolving area of tether applications in space.

This volume contains the complete documentation of the workshop, including opening addresses, tether fundamentals, and panel reports and summaries.