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Measurements of HO₂ Chemical Kinetics with a New Detection Method

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I. Introduction

This report covers the period from December 1, 1985 to May 31, 1986 for the research program currently supported by NASA under Grant No. NAGW-661 basic. In this program, the reaction rate constant of HO$_2$+O$_3$ has been measured with a discharge-flow-tube apparatus. The HO$_2$ radical was detected by the OH(A-X) photofragment emission produced from photodissociative excitation of HO$_2$ at 147 nm. In the meantime, the optical emissions produced by the vacuum ultraviolet excitation of chemical species in the flow tube were investigated and used to examine the possibility for their interference with the HO$_2$ detection. The research results are summarized below.

II. Research Accomplished

A. Reaction Rate Constant of HO$_2$+O$_3$

A discharge-flow-tube apparatus has been constructed and used to measure the reaction rate constant of HO$_2$+O$_3$. The flow tube consisted of three coaxial tubes. The innermost tube was a movable Teflon tube of 2 mm ID, and the second tube was a movable Teflon coated Pyres tube of 1 cm ID and 70 cm long. The main reactor was a Teflon coated Pyres tube. Two sizes of tubes were used – one 4.8 cm ID and the other 2.2 cm ID.

HO$_2$ was produced by the reaction sequence:

\[ \text{Cl} + \text{CH}_3\text{OH} \rightarrow \text{CH}_2\text{OH} + \text{HCl} \]

\[ \text{CH}_2\text{OH} + \text{O}_2 \rightarrow \text{HO}_2 + \text{CH}_2\text{O} \]

The Cl atom was produced by microwave discharge of a trace amount of Cl$_2$ in He. The HO$_2$ was detected by monitoring the
OH(A-X) emission from photodissociative excitation of H$_2$O$_2$ by a Xe resonance light at 147 nm,

\[ \text{H}_2\text{O}_2 + h\nu(147 \text{ nm}) \rightarrow \text{OH}(A^2\Sigma^+) + \text{O} \]

\[ \text{OH}(A^2\Sigma^+) \rightarrow \text{OH}(X^2\Pi) + h\nu (306-320 \text{ nm}). \]

The concentrations of Cl and the consequent reaction products (such as CH$_2$OH, CH$_2$O and H$_2$O$_2$) were limited to low values such that the requirements for the pseudo-first-order reaction were satisfied. H$_2$O$_2$ could be regenerated by the reaction sequence:

\[ \text{H}_2\text{O}_2 + \text{O}_3 \rightarrow \text{OH} + 2\text{O}_2 \]

\[ \text{OH} + \text{O}_3 \rightarrow \text{H}_2\text{O}_2 + \text{O}_2 \]

The regeneration was greatly reduced by adding C$_2$F$_3$Cl or C$_3$H$_8$ as the OH scavenger.

The reaction rate of H$_2$O$_2$ + O$_3$ at room temperature was measured as a function of reaction time and O$_3$ concentration. The reaction rate constants measured with different flow tube sizes and different OH scavengers are consistent to be $(1.9 \pm 0.3) \times 10^{-15} \text{ cm}^3/\text{s}$. A computer simulation modeling for the reaction kinetics occurring in the flow tube was carried out to confirm that the secondary reactions were negligible at the low H$_2$O$_2$ concentrations used in the experiment. This current reaction rate constant agrees very well with the value of $2 \times 10^{-15} \text{ cm}^3/\text{s}$ measured by the Laser-magnetic-resonance technique. Our results are described in more detail in a paper entitled "Reaction Rate Constant of H$_2$O$_2$+O$_3$ Measured by Detecting H$_2$O$_2$ from Photofragment Fluorescence" which is attached in this report as Appendix A.
We are measuring the H\textsubscript{2}O+O\textsubscript{3} reaction rate constant in the temperature range of 200-350 °C. The result will be presented in the next report.

B. Photofragment Emissions for VUV Excitation of Chemical Species in the Flow Tube

When the chemical species in the flow tube are excited by the 147 nm photons, they may produce UV light to interfere with the OH(A-X) emission from photoexcitation of H\textsubscript{2}O. Thus, the optical emissions from the vacuum ultraviolet (VUV) excitation of chemical species in the flow tube are needed to interpret our data. The fluorescence spectra of various chemical species were investigated using synchrotron radiation as a light source. The emission spectra were also produced by excitation of the chemical species with intense atomic lines, and they were dispersed to identify the emitting species.

The OH(A-X) emission from photoexcitation of CH\textsubscript{3}OH has been observed and the result has been reported in an earlier paper (J. B. Nee, M. Suto and L. C. Lee, Chem. Phys. 98, 147 (1985)). The result for photoexcitation of Cl\textsubscript{2} has been recently published in the Journal of Chemical Physics which is attached in this report as Appendix B. The spectroscopic data of HCl, CH\textsubscript{2}O, C\textsubscript{3}H\textsubscript{8} and C\textsubscript{2}F\textsubscript{3}Cl have been obtained and analyzed. Their results will be summarized in papers and published in scientific journals. Among all these molecules studied, only C\textsubscript{2}F\textsubscript{3}Cl emits at 147 nm. The cross section for the emission in the 300-330 nm region is, however, quite small such that this emission does not seriously
disturb the measurement of HO$_2$ concentration by the photofragment emission method.

In summary, the photofragment emissions of all chemical species in the flow tube have been investigated, and their possible interferences to the OH(A-X) emission, produced by photoexcitation of HO$_2$ have been examined. It is concluded that the possible optical emissions from other chemical species do not interfere the measurement of HO$_2$ concentration by the photofragment emission method. Thus, our measurement of the HO$_2$+O$_3$ reaction rate constant is not affected by the optical emissions from chemical species other than HO$_2$. 
Appendix A

"Reaction Rate Constant of HO₂+O₃ Measured by Detecting HO₂ from Photofragment Fluorescence"
Reaction Rate Constant of $\text{HO}_2 + \text{O}_3$ Measured by Detecting $\text{HO}_2$ from Photofragment Fluorescence

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ABSTRACT

The rate constant for the reaction $\text{HO}_2 + \text{O}_3 \rightarrow \text{OH} + 2\text{O}_2$ was investigated in a discharge-flow system at room temperature. $\text{HO}_2$ was produced from the reaction sequence: $\text{Cl} + \text{CH}_3\text{OH} \rightarrow \text{CH}_2\text{OH} + \text{HCl}$ and $\text{CH}_2\text{OH} + \text{O}_2 \rightarrow \text{HO}_2 + \text{CH}_2\text{O}$. $\text{HO}_2$ was detected by the $\text{OH}(A-X)$ fluorescence produced from photodissociative excitation of $\text{HO}_2$ at 147 nm. A computer modeling of the reaction kinetics occurring in the flow tube was carried out to confirm that contributions from secondary reactions were negligible at low $\text{HO}_2$ concentrations. The rate constant was determined from first order decay of $\text{HO}_2$ in excess $\text{O}_3$. The measured reaction rate constant of $\text{HO}_2 + \text{O}_3$ is $(1.9 \pm 0.3) \times 10^{-15}$ cm$^3$/s, which agrees well with published data.
I. INTRODUCTION

The reaction of odd hydrogen radicals, in particular, the reaction sequence

\[
\begin{align*}
\text{HO}_2 + \text{O}_3 & \rightarrow \text{OH} + 2\text{O}_2 \\
\text{OH} + \text{O}_3 & \rightarrow \text{HO}_2 + \text{O}_2
\end{align*}
\]

(1) (2)

has been implicated as major depletion reactions for \( \text{O}_3 \) in the lower stratosphere and important radical reactions in the troposphere. Several direct measurements of \( k_2 \) have been undertaken\(^1-^3\) but to date only the laser magnetic resonance (LMR) detection\(^4\) of \( \text{HO}_2 \) has been employed to directly measure \( k_1 \). In this present study, we demonstrate that the discharge-flow technique with photofragment emission (DF-PE) detection\(^5,^6\) of \( \text{HO}_2 \) can be used to directly measure the rate constant of reaction (1).

\( \text{HO}_2 \) was produced by microwave discharge of \( \text{Cl}_2 \), which then reacted with \( \text{CH}_3\text{OH} \) and \( \text{O}_2 \) by

\[
\begin{align*}
\text{Cl} + \text{CH}_3\text{OH} & \rightarrow \text{CH}_2\text{OH} + \text{HCl} \\
\text{CH}_2\text{OH} + \text{O}_2 & \rightarrow \text{HO}_2 + \text{CH}_2\text{O}
\end{align*}
\]

(3) (4)

\( \text{HO}_2 \) was detected by monitoring the \( \text{OH}(A^2\Sigma^+ \rightarrow X^2\Pi) \) emission from photodissociative excitation of \( \text{HO}_2 \) by a Xe resonance light at 147 nm,\(^6\)

\[
\begin{align*}
\text{HO}_2 + \text{hv (147 nm)} & \rightarrow \text{OH}(A^2\Sigma^+) + \text{O} \\
\text{OH}(A^2\Sigma^+) & \rightarrow \text{OH}(X^2\Pi) + \text{hv (306-320 nm)}
\end{align*}
\]

(5) (6)

The experimental conditions were such that the requirements for psuedo-first order reaction were satisfied. Regeneration of \( \text{HO}_2 \) via reaction (2) was greatly reduced by adding \( \text{OH} \) scavengers.\(^4,^7\) Two reagents, \( \text{C}_2\text{F}_3\text{Cl} \) and \( \text{C}_3\text{H}_8 \), were used as \( \text{OH} \)
scavengers in our experiments.

Since the measurement of reaction rate constant involves many experimental parameters, it is essential to apply different techniques to verify agreement among reported values. Both the methods of production and detection of H\textsubscript{2}O\textsubscript{2} for the study of reaction (1) in this experiment are different from previously reported experiments.\textsuperscript{4,7-9} This work reports the second direct measurement for the rate constant of reaction (1).

**II. EXPERIMENTAL**

The schematic diagram of the experimental apparatus is shown in Fig. 1. The experimental chamber consisted of a flow tube assembly and a gas cell. The flow tube consisted of three coaxial tubes. The innermost tube was a movable teflon tube of 2 mm i.d. through which CH\textsubscript{3}D\textsubscript{2}H and \textsubscript{O}\textsubscript{2} were fed. The second tube, a teflon coated Pyrex, was also a movable injector of 1 cm i.d. and 70 cm long. Chlorine atoms were produced upstream by a microwave discharge of a trace of Cl\textsubscript{2} in He. Helium was also used as a carrier gas and its flow rate (Q\textsubscript{1}) was regulated by a mass flow controller (MKS instruments). The production of H\textsubscript{2}O\textsubscript{2} was completed in this tube.

The main reactor was also a teflon coated Pyrex tube. Two sizes were used, one of 4.8 cm i.d. and the other 2.2 cm i.d. both 60 cm long. \textsubscript{O}3 and the OH scavenger, C\textsubscript{2}F\textsubscript{3}Cl or C\textsubscript{3}H\textsubscript{8}, were introduced into the flow tube upstream. \textsubscript{O}3 was produced, prior to use, by a high voltage a.c. discharge of \textsubscript{O}2 at atmospheric pressure and stored on two silica gel traps at 195 °K. The \textsubscript{O}3 was purified before use by pumping on the silica gel \textsubscript{O}3 traps
down to a few torr, where the O₃ concentration measured by
absorption of 253.7 nm agreed with the pressure measured by an
MKS Baratron manometer. O₃ was introduced into the flow tube
with He as a carrier gas with the He flow rate (Q₂) regulated by
another controller. The elution rate of O₃ was controlled by
varying both the flow rate and the temperature of the trap. The
partial pressure of O₃ was monitored by the attenuation of the
253.7 nm Hg line at two positions, upstream of the flow tube and
downstream after the gas cell. Both measurements agreed within
experimental uncertainty, indicating O₃ loss in the flow tube was
negligible.

HO₂ radicals reacted with O₃ in the main reaction tube. The
partial pressure of all gases were fixed, and the reaction times
were varied by moving the position of the HO₂ injector tube. The
reaction time is a function of the linear flow velocity which in
turn is dependent on the total flow rate. The total flow rate
(discussed in detail below) was determined for the flow
conditions of each experimental run. The pressures in the flow
tube and in the gas cell were monitored separately by two
Baratron manometers (MKS). The ratio of total pressures
(Ptube/Pcell)/Pcell ~ 0.05. Since the pressure drop was so
small, no corrections for Poiseuille drop were made (discussed in
Section C of Results).

The carrier gas was in excess over the reactants, so the
total flow rate was dependent largely on the He flow rate. The
total flow rate was determined as follows. First, the volume of
the chamber, VT, was determined using Boyle's Law with a
calibrated (at room temperature) 1000 cm³ container as a
reference volume, \( V_1 \). A known pressure of \( \text{He}, P_1 \), was contained in \( V_1 \) and then expanded to the total volume, \( V_2 = V_T + V_1 \), and the pressure in \( V_2 \), \( P_2 \), was recorded. Thus, \( V_2 = P_1 V_1 / P_2 \) in cm\(^3\).

With the flow rates of \( \text{He}, Q_1 \) and \( Q_2 \), kept constant, the chamber was isolated from the pump and the increase in pressure per min, \( \Delta P/\Delta t \) in torr/min, was recorded. The total standard flow rate, \( Q_T \), was obtained using:

\[
Q_T = V_2 \left( \frac{273}{T} \right) \left( \frac{\Delta P/\Delta t}{T} \right)
\]

where \( T \) is temperature in K, and \( Q_T \) is the flow rate in standard cubic centimeter per minute (SCCM). This equation was used to verify the instrumental flow rate settings \( Q_1 \) and \( Q_2 \). For the kinetic experiments, the ratio of \( \Delta P/\Delta t \) was determined for each individual run with all the major reactants in the flow as well.

The linear flow velocity in the tubes was derived from:

\[
v = V_2 \left( \frac{(\Delta P/\Delta t)/(60P))}{(1/\pi r^2)} \right)
\]

where \( P \) is the total pressure, \( P = (P_{\text{tube}} + P_{\text{cell}})/2 \), at which the experiment was performed, \( r \) is the radius of the flow tube and \( v \) is in cm/sec. The error estimates at 95% confidence level\(^{10} \) are: \( V_2 \) (± 2%), \( T \) (± 1%), \( P \) (± 5%), \( \Delta P/\Delta t \) (± 7%), and \( r \) (± 1%). The resultant error in \( Q_T \) or \( v \) is ± 9%. The total flow rates were typically in the range of 150-250 SCCM with the 4.8 cm i.d. and 80-100 SCCM with the 2.2 cm i.d., for which the linear flow velocities in the main reaction flow tube were in the range 100-130 cm/s and 150-200 cm/s, respectively.

The gas cell was a six-way-stainless steel-cross of 3 inch o.d. \( \text{HO}_2 \) radicals were detected by monitoring its \( \text{OH}(\Delta \rightarrow X) \) photofragment emission. A sealed \( \text{Xe} \) resonance lamp with a \( \text{MgF}_2 \) window was used as a light source. The light source intensity...
was monitored by a CsI photodiode (Hamamatsu R1187). A gas filter (1% CH₄ in Ar at atmospheric pressure) was used to cut-off the 129.5 nm line in the Xe lamp so that only the 147 nm line transmitted into the gas cell. The OH(A-X) emission from HO₂ was detected at the direction perpendicular to both the light source and the gas flow by a cooled PMT (EMI 9558 QB). A narrow band pass filter (310 ± 10 nm) was used to isolate the OH(A-X) band. The signal from the PMT was processed by an ORTEC counting system and the output fed to an IBM PC. The carrier gas flow rates, the total pressure, and the intensities of the 147 nm and 253.7 nm light sources were also simultaneously recorded by the computer.

The gas mixture of 2.0% Cl₂ in He and the lecture bottles of C.P. grade C₂F₃Cl (> 99.0%) and C₃H₈ (> 99.0%) were supplied by Matheson. The CH₃OH (supplied by Fisher, purity > 99.9%) vapor was carried by He into the gas cell. The concentration of CH₃OH was determined from the ratio of the CH₃OH vapor pressure (120 torr at room temperature) to the pressure of the carrier gas. O₂ was supplied by Amerigas and He of UHP grade (99.999%) was supplied by M.G. Scientific. Gases were used as delivered.

III. RESULTS AND DISCUSSION

A. Detection of HO₂ Radicals

The photofragment emission intensity can be described by,

\[ I_f = C \sigma f(\text{HO}_2) I_0 \exp(-\sigma i n_i l)/(1 + \tau f n_i k_i), \]

where \( C \) is a constant including the geometric factor and the PMT detection efficiency, \( \sigma f \) is the cross section for the OH(A → X)
fluorescence produced from excitation of HO₂ at 147 nm, [HO₂] is the HO₂ concentration, I₀ is the light source intensity of the Xe lamp, l is the path length of the light source from the MgF₂ window to the center of the PMT view region, τ is the radiative lifetime of the OH(A-X) transition; n₁, σ₁ and k₁ are the concentrations, the absorption cross sections at 147 nm, and the quenching rate constants of OH*(A) by various species in the flow tube, respectively. The exponential term represents the attenuation of the light source intensity at 147 nm by various species in the flow tube. The denominator represents the reduction in OH emission by the quenching of OH*(A) by the various gases.

The absorption cross sections for O₂, O₃, CH₃OH, C₂F₃Cl, and C₃H₈ at 147 nm were determined from the slope of the linear plot of absorbance versus pressure for each gas and are 1.4x10⁻¹⁷, 4.41x10⁻¹⁸, 1.30x10⁻¹⁷, 1.80x10⁻¹⁷ and 7.67x10⁻¹⁸ cm², respectively. The absorption cross-section of Cl₂ is < 10⁻¹⁸ cm². The attenuation of light source intensity by all gases for the optical path from the MgF₂ window to the detection region of about 1 cm was estimated to be about 10% at a typical experimental condition such as [O₃] = 2.5x10¹⁵ cm⁻³, [O₂] = 1.0x10¹⁵ cm⁻³, [CH₃OH] = 1.0x10¹⁴ cm⁻³, [Cl₂] = 6.5x10¹³ cm⁻³ and [C₂F₃Cl] = 4x10¹⁵ cm⁻³ (or [C₃H₈] = 6.5x10¹⁵ cm⁻³).

The quenching term (τ½n₁k₁) of OH*(A) by all gases in the flow tube is estimated to be about 1.6 and 2.6 with C₂F₃Cl and C₃H₈ as scavengers, respectively, assuming that the quenching rate constants of OH*(A) by all the gases are equal to the gas kinetic constant (3x10⁻¹⁰ cm³/s). The OH(A-X) emission intensity
may thus be reduced by a factor of 2.6 or 3.6, depending on C2F3Cl or C3H8 being used as the OH scavenger. With such attenuation, the light source intensity was still strong enough for the detection of HO2 radicals.

The photofragment emissions in the UV region from photoexcitation of various gases used in this experiment were also studied. The OH(A-X) emission was observed from excitation of CH3OH at 147 nm with fluorescence cross section of 3x10^-21 cm^2. An intense photofragment emission in the UV region (280-380 nm) was observed from excitation of C2F3Cl at 147 nm. The fluorescence cross section of C2F3Cl has been measured in the 105-170 nm region; however, when a narrow bandpass filter (310 ± 10 nm) was used, the fluorescence signal was greatly reduced such that it only contributed a small constant background. The other molecules do not fluoresce in the UV region when excited at 147 nm.

From the above results, it is conclusive that the relative HO2 concentration in the gas cell can be measured from the OH(A-X) emission. The estimated minimum detectable [HO2] is ~ 10^9 molecule/cm^3. In each measurement of the HO2 + O3 reaction rate, flow conditions, which included gas flow velocities, gas flow rates, gas pressures, and microwave discharge power were fixed, except for the reaction time which was varied by changing the position of the movable injector. Since the gas pressures in each measurement were kept constant, the light attenuation, quenching, and emission due to species other than HO2 were constant so that the relative [HO2] is proportional to the OH(A-X)
X) fluorescence intensity observed. For a fixed [O$_3$], relative [H$_2$O$_2$] was measured as a function of the reaction time.

**B. H$_2$O$_2$ Concentrations and Secondary Reactions**

The calibration of H$_2$O$_2$ by reaction with NO to give NO$_2$ and OH, where the [OH] was measured by OH(A-X) resonance fluorescence,$^5$ proved difficult for this chemical system. Instead, the [H$_2$O$_2$] was estimated by a titration method using CH$_3$OH as titrant and the data were compared with a kinetic model. For [Cl$_2$] = 5.5x10$^{13}$ cm$^{-3}$ and [O$_2$] = 1.3x10$^{15}$ cm$^{-3}$ kept constant, the data of $I_f$ versus [CH$_3$OH] are plotted in Fig. 2 for two reaction times, 45 and 65 msec, inside the central tube (1 cm i.d.) and for an additional 10 and 20 msec to the detection region, respectively. The error bars in $I_f$ represent one standard deviation and that in [CH$_3$OH] is the instrumental uncertainty of the pressure manometer. The reactions for the kinetic model are summarized in Table 1. The calculations were carried out using a program which uses the Gear routine for the solution of differential equations.$^{14}$

The reactions in the model are similar to those considered by Takacs and Howard in their modeling of the self-reaction of H$_2$O$_2$.$^{15}$ The estimates for the wall losses were deduced from other experimental data. Wall loss rate for H$_2$O$_2$ was not greater than 1.5 s$^{-1}$ in the central tubing (deduced from the intercepts of Figs. 9-11 as discussed later). When the O$_2$/CH$_3$OH injector was positioned so that the residence time of Cl was about 40 msec before interacting with CH$_3$OH and O$_2$, no fluorescence from H$_2$O$_2$ was detected, thus an upper limit to Cl loss rate is 25 s$^{-1}$. The wall loss rate of CH$_2$OH was estimated to be 185 s$^{-1}$ for a
halocarbon wax coated tube of 1.24 cm i.d. at comparable flow velocities used in our experiments. In the modeling, at each \([\text{CH}_3\text{OH}]\), the \([\text{O}_2]\) was given and \([\text{Cl}]\) was varied to give the best fit to the data. Best agreement was obtained between computer calculations and experiments when \(1\times10^{11} < [\text{Cl}] < 2\times10^{11} \text{ cm}^{-3}\) and wall loss rate of Cl was 10 s\(^{-1}\). Wall loss rates of HO\(_2\) and CH\(_2\)OH contributed insignificantly to the curve fitting. Experimental and calculation data were normalized at \([\text{CH}_3\text{OH}] = 1\times10^{14} \text{ cm}^{-3}\) and compared in Fig. 2.

First, ignoring wall losses of HO\(_2\), Cl and CH\(_2\)OH, plots (a) and (b) of Fig. 2 are the simulation curves with \([\text{Cl}] = 1\times10^{11}\) and \(2\times10^{11} \text{ cm}^{-3}\), respectively. Plot (c) is with \(k_w(\text{HO}_2) = 1.5 \text{ s}^{-1}\) for \([\text{Cl}] = 1\times10^{11} \text{ cm}^{-3}\). There is no substantial change in the simulation curve when \(k_w(\text{HO}_2)\) is considered. The same curve as (c) was obtained when \(k_w(\text{CH}_2\text{OH}) = 200 \text{ s}^{-1}\) was included in the modeling. Curve (d) is obtained when \(k_w(\text{Cl}) = 10 \text{ s}^{-1}\) and \(k_w(\text{CH}_2\text{OH})\) and \(k_w(\text{HO}_2)\) were set at zero. Including \(k_w(\text{Cl})\) improved the curve fitting at smaller \([\text{CH}_3\text{OH}]\). However, the change in curve (d) was not significant when wall losses from HO\(_2\) and CH\(_2\)OH were considered. The \([\text{Cl}]\) represents the Cl entering the central reactor. The amount of Cl formed in the discharge region is possibly high but wall losses and atom recombination can also be high so that the resulting \([\text{Cl}]\) is low.

Complications in the treatment of our kinetic data for the HO\(_2\) + O\(_3\) reaction could arise from (i) interference of the OH fluorescence from photodissociation of H\(_2\)O\(_2\) and (ii) contributions from secondary reactions. These are discussed
$H_2O_2$ is produced in the reaction of $HO_2+HO_2$. $H_2O_2$ is also photodissociated when irradiated by 147 nm photons:

$$H_2O_2 + h\nu (147) \rightarrow OH^* (A^2E^+ ) + OH (A^2I )$$

(10)

Thus, the $OH(A-X)$ emission (reaction 6) from $H_2O_2$ will also be detected. The $H_2O_2$ fluorescence cross section at 147 nm is $(H_2O_2) = 5x10^{-19}$ cm$^2$. The fluorescence from photodissociation of $H_2O_2$ will add a background that may interfere with the data analysis. However, this additional signal in a typical experimental condition was quite small such that it is negligible as discussed below.

A summary of the experimental conditions are given in Table II. The flow velocities correspond to an average reaction time of 80 msec in the central tube. The typical concentrations of reactants are: $[CH_3OH] = 1.2x10^{14}$, $[O_2] = 1.3x10^{15}$ and $[Cl_2] = 5.5x10^{13}$. Using these concentrations and assuming that wall losses for $HO_2$, $CH_2OH$ and $Cl$ are negligible so that the maximum contribution from secondary reactions can be obtained, the modeling predicts an $9.7x10^{10} \leq [HO_2] \leq 1.9x10^{11}$ cm$^{-3}$ and $1.1x10^{9} \leq [H_2O_2] \leq 4.5x10^{9}$ cm$^{-3}$ after 80 msec of reaction for $1x10^{11} \leq [Cl] \leq 2x10^{11}$ cm$^{-3}$. Since $[H_2O_2]$ is two-orders of magnitude smaller than $[HO_2]$, the contribution of $H_2O_2$ to the fluorescence is expected to be quite small if the fluorescence cross sections of $HO_2$ and $H_2O_2$ are the same order of magnitude. This is indeed true as justified below.

The fluorescence cross section of $HO_2$, $\sigma (HO_2)$, can be deduced from the current experimental data. $CH_3OH$, like $HO_2$ and $H_2O_2$, is also photodissociated by 147 nm photons to give $OH^* (A)$
which subsequently emits in the 310 ± 10 nm region. The \( \sigma(\text{HO}_2) \)

can be obtained by calibration against the \( \text{CH}_3\text{OH} \) emission whose fluorescence cross section\(^{12}\) at 147 nm is known, \( \sigma(\text{CH}_3\text{OH}) = 3 \times 10^{-21} \text{ cm}^2 \). Using the \([\text{HO}_2]\) from the modeling, we have \( 5 \times 10^{-20} \leq \sigma(\text{HO}_2) \leq 1 \times 10^{-19} \text{ cm}^2 \). Thus, \( \sigma(\text{HO}_2) \) is about a factor of 5 to 10 smaller than \( \sigma(\text{H}_2\text{O}_2) \). Considering the low \([\text{H}_2\text{O}_2]\), its contribution to the observed fluorescence is less than 10%. This percentage will be considerably reduced when the \([\text{HO}_2]\) is kept low.

To further verify that the \([\text{Cl}]\) is indeed small in our experiments, and thus, the \([\text{HO}_2]\) and \([\text{H}_2\text{O}_2]\) are likewise small, the fluorescence intensity was monitored as a function of \([\text{Cl}_2]\) as shown in Fig. 3. The plot of \( I_f \) versus \([\text{Cl}_2]\) is linear for the case without or with 0\(_3\). The plots (a) and (b) are fit to the respective data, where \([\text{Cl}] = 10^{11} \text{ cm}^{-3} \) is assumed for an initial \([\text{Cl}_2] = 5.5 \times 10^{13} \text{ cm}^{-3} \) and \( \sigma(\text{H}_2\text{O}_2) = 3 \sigma(\text{HO}_2) \). This linearity extends to about three times the \([\text{Cl}_2]\) used in the \( \text{HO}_2+0_3 \) experiments (\( \text{C}_3\text{H}_8 \) was used as the \( \text{OH} \) scavenger to inhibit reaction (2) for the data when 0\(_3\) was added). If \( \sigma(\text{H}_2\text{O}_2) = 10 \sigma(\text{HO}_2) \), is assumed, the dependence deviates from the linearity as shown in plots (c) and (d). When \([\text{Cl}] = 2 \times 10^{11} \text{ cm}^{-3} \) is assumed for an initial \([\text{Cl}_2] = 5.5 \times 10^{13} \), and \( \sigma(\text{H}_2\text{O}_2) = 10 \sigma(\text{HO}_2) \) then the dependence deviates further from the linearity as shown in plots (e) and (f). For plot (f), the \( \text{H}_2\text{O}_2+0_3 \) reaction rate constant is assumed equal to the \( \text{HO}_2+0_3 \) reaction rate constant (Section D). If the \( \text{H}_2\text{O}_2+0_3 \) reaction is slower, then the nonlinearity will occur sooner at lower \([\text{Cl}_2]\). To obtain the
linear relationship, the $H_2O_2 + O_3$ reaction must be faster than the $HO_2 + O_3$ reaction, at least five times faster or at the order of $10^{-14}$ cm$^3$/s. There is no indication in the available literature that suggests this reaction rate constant to be greater than $k_1$. These results clearly indicate that the upper limit of the $[Cl]$ is $2 \times 10^{11}$ cm$^{-3}$ and $\sigma(H_2O_2) < 10^{-9} \sigma(HO_2)$. For a typical experimental condition, the concentrations of reactants in the central tube, where $[CH_3OH] = 1.2 \times 10^{14}$ cm$^{-3}$, $[O_2] = 1.3 \times 10^{15}$ cm cm$^{-3}$, and $[Cl_2] = 5.5 \times 10^{13}$ cm$^{-3}$, the kinetic model predicts that the signal due to $H_2O_2$ is only a few percent of $HO_2$. Thus, the analysis of the $HO_2 + O_3$ reaction rate constant is not significantly interfered with by the secondary product of $H_2O_2$.

The predicted $[HO_2]$ originating from the injector is less than $1.9 \times 10^{11}$ cm$^{-3}$ and the concentration of all other radical products formed in the central tube are negligible compared to $[HO_2]$, thus, the loss rate of $HO_2$ by other reactions is negligible when compared with the $HO_2 + O_3$ reaction. Radical concentrations are small because, for the $[CH_3OH]$ and $[O_2]$ used in the experiment, all $Cl$ atoms are readily converted to $HO_2$ within a msec and the probability for the formation of radicals involving $Cl$ and its secondary products is thus small. The $O_3$ used is in the range $4 \times 10^{14} < [O_3] < 3 \times 10^{15}$ cm$^{-3}$, hence, the loss rate of $HO_2$ from $HO_2 + HO_2 \rightarrow H_2O_2 + O_2$ ($1.5 \times 10^{-12}$ cm$^3$/s) is minimal when compared with $HO_2 + O_3$. Analysis of our $HO_2 + O_3$ reaction (Section D) at all $[O_3]$ was consistent with a pseudo-first order loss rate for $HO_2$.

C. Flow Tube Parameters

The flow dynamics in a flow tube reactor are complicated by
the change of pressure along the length of the tube and the change of transport velocity of radicals caused by diffusion. The linear flow velocity in the central tube of 1 cm i.d. was about $10^3$ cm/s which is 4.84 times faster than that in main reactor tube of 2.2 cm i.d.. The pressure drop will be large if the linear flow velocity, $v$, is fast and the tube radius, $r$, is small, that is, $\Delta p/l \propto \left( v/r^2 \right)$ where $\Delta p/l$ is the pressure drop across the tube length. However, even if there is a pressure drop in the central tube and hence an $[HO_2]$ gradient, the initial $[HO_2]$ at the point entering the main reaction flow tube should be constant for a given experimental set-up. This assertion is supported by the evidence that in the central tube where $HO_2$ is formed, a 60% change in $v$ does not disrupt the linear dependence of $[HO_2]$ on $[Cl_2]$ (Fig. 3). The pressure gradient in the main reactor (2.2 cm i.d. and 60 cm long) is small (about 0.05). No corrections were made for this gradient, because this does not introduce any serious problem as shown in the next section.

There is no apparent complication arising from back diffusion. When the $[Cl_2]$ was increased, the $[HO_2]$ proportionally increased. If the addition of $Cl_2$ or increased $HO_2$ production caused changes in the flow velocities of the gases or the transport velocity of the radical then the linearity would not hold.

As shown in Fig. 3, changing the linear flow velocity and addition of $O_3$ and the $OH$ scavenger did not affect the linear dependence of $[HO_2]$ on $[Cl_2]$. This linearity held for different
reaction distances. Such linearity again indicates a low [HO2] and the [HO2] is distributed uniformly in the tube. The partial pressure of the He carrier gas is at least a factor of seven greater than the sum of the partial pressures of the additive gases and at least four orders of magnitude greater than [HO2]. Thus, the flow conditions and the gas pressures apparently constituted good mixing. This uniform distribution of [HO2] ensures that the reaction of HO2 with O3 was spatially uniform in the flow tube.

The above discussion concludes that (1) there was no substantial pressure gradient in the main reactor; (2) since the [HO2] was low (Section B), its transport velocity was the same as the carrier gas; and (3) the reactant gases were well mixed in the system. Thus, the experimental conditions were appropriate for studying the HO2+O3 reaction.

D. Reaction Rate Constant of HO2+O3

In the measurements of reaction rates, [O3] was in the 4.5x10^{14} - 3x0x10^{15} cm^{-3} range which was much larger than the [HO2] in the reaction flow tube. With [C2F3Cl] of about 3x10^{15} cm^{-3} or C3H8 of about 6x10^{15} cm^{-3}, reaction (2) (k2 = 6.5x10^{-14} cm^{3}/s)^4 was negligible since it is much slower than the reaction rates of OH+C2F3Cl (6x10^{-12} cm^{3}/s)^4 or OH+C3H8 (1.1x10^{-12} cm^{3}/s)^13 by about two-orders of magnitude. Thus, the decay of HO2 due to reaction with O3 can be represented by the pseudo-first-order approximation.

The pseudo-first order reaction rate, K, for a given [O3] is

$$K = - \frac{d(ln(I_f))}{dz}$$
where \( v \) is the linear flow velocity in the main reactor, \( z \) is the reaction distance from the tip of the 1 cm tube to the \( \text{HO}_2 \) detection point in the gas cell, and \( I_f \) is proportional to \([\text{HO}_2]\).

The bimolecular rate constant, \( k_1 \), is obtained from the slope of \( K \) versus \([\text{O}_3]\) since \( K = k_1[\text{O}_3] \).

Sample first-order \( \text{HO}_2 \) decay plots, \((\ln(I_f)\) versus \(z\)) are shown in Figs. 4 and 5 with \( \text{C}_2\text{F}_3\text{Cl} \) and \( \text{C}_3\text{H}_8 \) as the OH scavengers, respectively. For each experimental run, the movable \( \text{HO}_2 \) injector was moved 50 cm at 5-cm intervals. The \( z=0 \) points in Figs. 4 and 5 were set at about 6 cm from the \( \text{HO}_2 \) detection point. The reaction time between \( \text{HO}_2 + \text{O}_3 \) was increased for each increase in distance. Each plot was linear for the range of \( 0 < [\text{O}_3] < 3 \times 10^{15} \text{ cm}^{-3} \) used in these experiments which indicate that (i) the OH product from reaction (2) was effectively removed by the scavengers, and (ii) \( \text{HO}_2 + \text{HO}_2 \) reaction is negligible as indicated by the small decrease rate of \([\text{HO}_2]\) at \([\text{O}_3]=0\). This is consistent with predicted \([\text{HO}_2] < 1 \times 10^{11} \text{ molecule/cm}^3\). The experimental data is summarized in Table II.

The first-order rates of reaction (1) versus \([\text{O}_3]\) are shown in Figs. 6 and 7 for \( \text{C}_2\text{F}_3\text{Cl} \) and \( \text{C}_3\text{H}_8 \) as OH scavengers, respectively. The vertical error bars represent one standard deviation which includes the uncertainties in the determination of \( v \) and the linear least square fit of \( \ln(I_f) \) versus \(z\) (as in Figs. 4 and 5). The horizontal error bars represent the standard deviation in determining \([\text{O}_3]\). The lines are linear least squares fit. The bimolecular rate constants obtained from the slopes of Figs. 6 and 7 are \( 1.7 \times 10^{-15} \) and \( 2.0 \times 10^{-15} \text{ cm}^3/\text{s} \), respectively. A reasonable estimate of the precision is about
17% using a 95% confidence level from the errors: $k_1$ ($\pm 10\%$), $K$ ($\pm 10\%$), $[O_3]$ ($\pm 5\%$), and $v$ ($\pm 9\%$). Adding a systematic error of 10%, the experimental resultant error is 20%. The intercepts represent HO$_2$ loss to the walls of the reactor. The intercept of $K_0 = 0.3$ s$^{-1}$ in Fig. 6 and $\nu = 0$ in Fig. 7 are quite small, suggesting the apparent HO$_2$ loss due to the walls being quite small.

The reaction rate constants were also measured using a flow tube of 4.8 cm i.d. The results are shown in Fig. 8. With C$_2$F$_3$Cl as the OH scavenger, the slope gave $k_1 = (1.5 \pm 0.4) \times 10^{-15}$ cm$^3$/s, and with C$_3$H$_8$, $k_1 = (2.1 \pm 0.5) \times 10^{-15}$ cm$^3$/s. The experimental uncertainties for the measurements with such a large flow tube are relatively high. The flow velocity and the gas mixing in a large flow tube are more difficult to control than that of a small tube. Nevertheless, $k_1$ values obtained from the larger flow tube are in agreement with the small one.

**IV. CONCLUSION**

The current $k_1$ value at room temperature (298 K) determined from Figs. 6 and 7 is $(1.9 \pm 0.3) \times 10^{-15}$ cm$^3$/s, where error limit represents 95% confidence limit. This is in good agreement with the absolute rate constant of $2 \times 10^{-15}$ cm$^3$/s measured by the LMR method$^4$ and the value of $1.7 \times 10^{-15}$ cm$^3$/s indirectly measured by photolysis of dry H$_2$-O$_2$-O$_3$ mixtures.$^9$ In the indirect measurements, $k_1$ was determined from relative rates with the 2HO$_2$ $\rightarrow$ H$_2$O$_2$+O$_2$ reaction as the competing reaction. The lower $k_1$ values derived from relative rates from early photolysis
results\textsuperscript{7, 8} were reconciled to the later determination\textsuperscript{9} by taking into account that in the presence of water vapor the self-reaction of HO\textsubscript{2} increases.

The Arrhenius parameters in the temperature range 230-365 K indicate a low value for the A-factor (1.3\texttimes10\textsuperscript{-14} cm\textsuperscript{-3}/s) for a simple atom-transfer mechanism.\textsuperscript{4} The reaction rate constants at different temperatures will be further measured in our laboratory to verify the Arrhenius parameters. The reaction rate constants at various temperature are needed in the stratospheric modeling, since temperature changes with height in the stratosphere.

ACKNOWLEDGEMENT

The authors wish to thank Dr. W. B. DeMore, D. L. F. Keyser, Dr. M. T. Leu, and Dr. M. J. Molina at the Jet Propulsion Laboratory, Dr. C. J. Howard at the NOAA Environmental Research Laboratory, Dr. D. M. Golden at the SRI International, Dr. R. F. Hampson at the National Bureau of Standard, and Dr. J. B. Nee, Dr. W. C. Wang and Dr. X. Y. Wang in our laboratory for useful discussion and suggestions. The HO\textsubscript{2} detection method is based on the work supported by the NSF under Grant No. ATM-8412618. This work is supported by the NASA under Grant No. NAGW-661.
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<th>Number</th>
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<th>Rate Constants (cm$^3$/molec. $\cdot$ s)</th>
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<td>1</td>
<td>$\text{CH}_3\text{OH} + \text{Cl} \rightarrow \text{CH}_2\text{OH} + \text{HCl}$</td>
<td>$6.30 \times 10^{-11}$a</td>
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<td>2</td>
<td>$\text{CH}_2\text{OH} + \text{O}_2 \rightarrow \text{CH}_2\text{O} + \text{HO}_2$</td>
<td>$1.40 \times 10^{-12}$</td>
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<td>3</td>
<td>$\text{CH}_2\text{OH} + \text{Cl} \rightarrow \text{CH}_2\text{O} + \text{HCl}$</td>
<td>$3.00 \times 10^{-10}$b</td>
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<td>4</td>
<td>$\text{H}_2\text{O}_2 + \text{HO}_2 \rightarrow \text{H}_2\text{O}_2 + \text{O}_2$</td>
<td>$1.50 \times 10^{-12}$</td>
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<td>$\text{Cl} + \text{H}_2\text{O}_2 \rightarrow \text{HCl} + \text{HO}_2$</td>
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<td>$\text{Cl} + \text{HO}_2 \rightarrow \text{HCl} + \text{O}_2$</td>
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<td>$\text{OH} + \text{H}_2\text{O}_2 \rightarrow \text{H}_2\text{O} + \text{HO}_2$</td>
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(continued)  

Table I

a All reactions unless otherwise stated are similar to those considered in Reference 15 and the rate constants compared with Reference 16. The rate constant 6.30 E-11 reads 6.30x10^{-11}.

b Added to the list of reactions, while a negligible step in comparison to the CH₂OH+O₂ reaction because of our high [O₂], this step was necessary in the simulation of the data in Reference 6. The gas kinetic value was assumed for the rate constant.

c Cl + O₂ + M → ClO₂ + M with M principally He at 1.5 torr.

d Added to list for completion.

e Wall lost rates. See text.
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<th>([O_2]) ((10^{15} \text{ cm}^{-3}))</th>
<th>([\text{C}_2\text{F}_3\text{Cl}]) ((10^{15} \text{ cm}^{-3}))</th>
<th>(p^{**}) (torr)</th>
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\[^{*}\text{tub e radius is 2.2 cm i.d.}\]

\[^{**}\text{total cell pressure}\]
REFERENCES


FIGURE CAPTIONS

Figure 1  Schematic diagram of experimental apparatus.

Figure 2  Emission intensity versus [CH$_3$OH] with [Cl$_2$] = 5.5x10$^{13}$ cm$^{-3}$ and [O$_2$] = 1.3x10$^{15}$ cm$^{-3}$, for a reaction time of 65 msec (•) and 45 msec (○) in the central tube. See text for discussion.

Figure 3  If versus [Cl$_2$]. Concentrations in cm$^{-3}$: [O$_3$] = 0, [CH$_3$OH] = 1.1x10$^{14}$, [O$_2$] = 1.3x10$^{15}$, v = 292 cm/s (○); [O$_3$] = 2.0x10$^{15}$, [CH$_3$OH] = 1.2x10$^{14}$, [O$_2$] = 1.3x10$^{15}$, [C$_3$H$_8$] = 6.4x10$^{15}$, v = 183 cm/s (□), for z = 20 cm. (a) - (f) are the modeling curves (see text).

Figure 4  First order decay plots with C$_2$F$_3$Cl as OH scavenger. See Table II for experimental condition: (a) run 1, [O$_3$] = 0; (b) run 3, [O$_3$] = 8.30x10$^{14}$ cm$^{-3}$; (c) run 7, [O$_3$] = 2.13x10$^{15}$ cm$^{-3}$.

Figure 5  First order decay plots with C$_3$H$_8$ as the OH scavenger. See Table II for experimental condition (a) run 11, [O$_3$] = 6.42x10$^{14}$ cm$^{-3}$, (b) run 12, [O$_3$] = 1.25x10$^{15}$ cm$^{-3}$, and (c) run 15, [O$_3$] = 2.25x10$^{15}$ cm$^{-3}$.

Figure 6  K versus [O$_3$] with C$_2$F$_3$Cl as the OH scavanger. The tube radius was 2.2 cm i.d. The slope is $k_1$ = 1.7x10$^{-15}$ cm$^3$/s.
Figure 7  Same as Figure 6 but with C₃H₈ as the OH scavenger, $k_1 = 2.0 \times 10^{-15}$ cm³/s.

Figure 8  K versus [O₃]. The tube radius was 4.8 cm i.d. The slope is $k_1$. Plot (a) with C₂F₃Cl as the OH scavenger, $k_1 = (1.5 \pm 0.4) \times 10^{-15}$ cm³/s and plot (b) with C₃H₈, $k_1 = (2.1 \pm 0.5) \times 10^{-15}$ cm³/s.
Fig. 1

Diagram showing the flow of gases and reactions:
- CH₃OH → O₂
- O₃
- He(Q₂)
- Cl₂ & He(Q₁)
- C₂F₃Cl or C₃H₈
- Reaction tube
- Xe lamp
- CH₄/Ar

Components:
- Hg lamp
- UV phototube
- Solar blind phototube
- P cell
- Pump
Fig. 4

(a) $[O_3]=0$
$v=203 \text{ cm/s}$

(b) $[O_3]=25.6 \text{ mtorr}$
$v=197 \text{ cm/s}$

(c) $[O_3]=65.9 \text{ mtorr}$
$v=165 \text{ cm/s}$
Fig. 5

(a) $[O_3] = 19.8$ mtorr, $v = 197$ cm/s

(b) $[O_3] = 38.5$ mtorr, $v = 198$ cm/s

(c) $[O_3] = 69.4$ mtorr, $v = 172$ cm/s
Fig. 6
Fig. 7
Fig. 8

[Graph showing a plot of $K$ (s$^{-1}$) against $[O_3]$ ($10^{15}$ cm$^{-3}$) with two lines labeled (a) and (b).]