

025921-22T

**USE OF EDGE-BASED FINITE ELEMENTS FOR  
SOLVING THREE DIMENSIONAL  
SCATTERING PROBLEMS**

A. Chatterjee  
J.M. Jin  
J.L. Volakis

NASA-Ames Research Center  
Moffet Field, CA 94035  
Grant NAG-2-541

Pacific Missile Test Center  
Pt. Mugu, CA 03042-5000

Technical Report 025921-22T



August 1991

**THE UNIVERSITY OF MICHIGAN**

**Radiation Laboratory**

**Department of Electrical Engineering  
and Computer Science**

**Ann Arbor, Michigan 48109-2122**

**USA**

(NASA-CR-188735) USE OF EDGE-BASED FINITE  
ELEMENTS FOR SOLVING THREE DIMENSIONAL  
SCATTERING PROBLEMS Technical Report, Feb. -  
Sep. 1991 (Michigan Univ.) 39 p CSCL 12A

N91-30860

Unclas  
0033700

G3/64

**TECHNICAL REPORT**  
**FOR**  
**NASA Grant NAG-2-541**

**NASA Technical Monitor: Alex Woo**

Grant Title: Use of Edge-Based Finite Elements for Solving  
Three Dimensional Scattering Problems

Institution: The Radiation Laboratory  
Department of Electrical Engineering  
and Computer Science  
The University of Michigan  
Ann Arbor, MI 48109-2122

Period Covered: February 1991 - September 1991

Report Authors: A. Chatterjee, J.M. Jin and J.L. Volakis

Principal Investigator: John L. Volakis  
Telephone: (313) 764-0500

## Table of Contents

### Use of Edge-Based Finite Elements for Solving Three Dimensional Scattering Problems

	Page
Introduction	1
Formulation	2
Derivation of finite element equations	2
Basis functions	4
Mesh termination	4
Vector ABC	5
Fictitious absorber model	6
Solution of the finite element equations	7
Vector ABC	7
Fictitious absorber model	7
Results	8
Conclusions and Future Work	9
Appendix: Derivation of matrix elements	9
References	10

---

Tables and figures follow page 11

Computer Program listings follow page 14

# USE OF EDGE-BASED FINITE ELEMENTS FOR SOLVING THREE DIMENSIONAL SCATTERING PROBLEMS

A. Chatterjee, J.M. Jin and J.L. Volakis

Radiation Laboratory

Department of Electrical Engineering and Computer Science

University of Michigan

Ann Arbor, MI 48109-2122

## Abstract

Edge-based finite elements are free from the drawbacks associated with node-based vectorial finite elements and are, therefore, ideal for solving three-dimensional scattering problems. The finite element discretization using edge elements is checked by solving for the resonant frequencies of a closed inhomogeneously filled metallic cavity. Significant improvements in accuracy are observed when compared to the classical node-based approach with no penalty in terms of computational time and with the expected absence of 'spurious' modes. A performance comparison between the edge-based tetrahedra and rectangular brick elements is carried out and tetrahedral elements are found to be more accurate than rectangular bricks for a given storage intensity. A detailed formulation for the scattering problem with various approaches for terminating the finite element mesh is also presented.

# 1 Introduction

The problem of computing the electromagnetic field scattered by a material body, when a field is incident on it, has great theoretical and practical importance. It is, usually, desirable to relate the characteristics of the scattered field in the far zone with the shape of the scatterer. Finite elements can be used to model complicated geometries but are of no help in computing the far field. The far field effect is thus represented in finite element analysis by enclosing the target within a fictitious boundary and enforcing a special boundary condition, often called the absorbing boundary condition, on the outer boundary. In this report, we discuss the choice of finite elements in the inner region. As a first step, we solve Maxwell's equations for the resonances of a closed cavity to verify the finite element discretization and decide on the type of basis functions and elements to use.

The occurrence of 'spurious' modes[1] in the node-based finite element approach has plagued the computation of cavity eigenvalues for years. This difficulty can be circumvented with the introduction of a penalty term[2] to render the finite element vector field solutions non-divergent. However, it is difficult to satisfy continuity requirements across material interfaces[3] or for geometries with sharp edges[4] using classical finite-elements, obtained by interpolating the nodal values of the vector field components. This is especially critical in solving scattering problems using classical finite elements where special techniques need to be used for satisfying normal and tangential continuity of the electric displacement and the electric field, respectively[5]. Edge elements, a type of vector finite element with their degrees of freedom associated with the edges of the mesh, have been shown to be free of these shortcomings[6],[7]. Edge-based finite elements are, therefore, a natural choice for treating three dimensional geometries. Generally these lead to more unknowns but the higher variable count is balanced by the greater sparsity of the finite element matrix so that the computation time required to solve such a system iteratively with a given accuracy is less than the traditional approach[8].

In this report, we have discussed the formulation for both the cavity and the scattering problems but have presented results only for the former. We have solved for the eigenvalues of an arbitrarily shaped metallic cavity using node-based and edge-based vector finite elements. The computed data are then compared with analytical results for empty and partially filled cavities. A comparison between the storage intensity and computational accuracy for edge-based rectangular bricks and tetrahedra is also presented. Finally, we compute the eigenvalues of a metallic cavity with a ridge along one of its faces.

## 2 Formulation

### 2.1 Derivation of finite element equations

Consider a three dimensional inhomogeneous body occupying the volume  $V$ . To discretize the electric field  $\mathbf{E}$  inside this volume, we subdivide it into a number of small tetrahedra or rectangular bricks, each occupying the volume  $V_e (e = 1, 2, \dots, M)$ , where  $M$  is the total number of elements. Within each element, the electric field satisfies the vector wave equation

$$\nabla \times \frac{1}{\mu_r} \nabla \times \mathbf{E} - k_o^2 \epsilon_r \mathbf{E} = \mathbf{0} \quad (1)$$

in which  $\mu_r$  is the permeability of the medium,  $\epsilon_r$  is the medium permittivity and  $k_o$  is the free space wave number. For a numerical solution of (1), we expand the electric field within the  $e$ th volume element as

$$\mathbf{E} = \sum_{j=1}^m E_j^e \mathbf{W}_j^e \quad (2)$$

where  $\mathbf{W}_j^e$  are edge-based vector basis functions,  $E_j^e$  denote the expansion coefficients of the basis,  $m$  represents the number of edges in the element and the superscript stands for the element number. On substituting (2) into (1) and upon applying Galerkin's technique, we obtain

$$\sum_{j=1}^m E_j^e \int_{V_e} \mathbf{W}_i^e \cdot \left( \nabla \times \frac{1}{\mu_r} \nabla \times \mathbf{W}_j^e - k_o^2 \epsilon_r \mathbf{W}_j^e \right) dv = 0$$

Further, upon making use of basic vector identities and the divergence theorem, we obtain the weak form of Maxwell's equation

$$\sum_{j=1}^m E_j^e \int_{V_e} \left[ \frac{1}{\mu_r} (\nabla \times \mathbf{W}_i^e) \cdot (\nabla \times \mathbf{W}_j^e) - k_o^2 \epsilon_r \mathbf{W}_i^e \cdot \mathbf{W}_j^e \right] dv = j k_o Z_o \oint_{S_e} \mathbf{W}_i^e \cdot (\mathbf{n} \times \mathbf{H}) ds \quad (3)$$

where  $\mathbf{n} \times \mathbf{H}$  is the tangential magnetic field on the exterior dielectric surface,  $S_e$  denotes the surface enclosing  $V_e$  and  $Z_o$  is the free-space intrinsic impedance. Equation (3) can be conveniently written in matrix form as

$$[A^e] \{E^e\} = k_o^2 [B^e] \{E^e\} + \{C^e\} \quad (4)$$

where

$$A_{ij}^e = \int_{V_e} \frac{1}{\mu_r} (\nabla \times \mathbf{W}_i^e) \cdot (\nabla \times \mathbf{W}_j^e) \quad (5)$$

$$B_i^e = \int_{V_e} \epsilon_r \mathbf{W}_i^e \cdot \mathbf{W}_j^e dv \quad (6)$$

$$C_i^e = j k_o Z_o \oint_{S_e} \mathbf{W}_i^e \cdot (\mathbf{n} \times \mathbf{H}) ds \quad (7)$$

On assembling the equations from all the elements making up the geometry, we obtain the system

$$\sum_{e=1}^M [A^e] \{E^e\} = k_o^2 \sum_{e=1}^M [B^e] \{E^e\} + \sum_{e=1}^M \{C^e\} \quad (8)$$

Due to the continuity of tangential  $\mathbf{H}$  at the interface between two dielectrics, an element face lying inside the body does not contribute to the last term of ( 8) in the final assembly of the element equations. As a result, the last term of ( 8) reduces to a column vector containing the surface integral of the tangential magnetic field only over the exterior surface of the body. In this paper, we are interested in a perfectly conducting surface surrounding the volume  $V$  and in this case, the surface integral vanishes altogether. Therefore, this system can be more compactly written as

$$[A] \{E\} = \lambda [B] \{E\} \quad (9)$$

where  $[A]$  and  $[B]$  are  $N \times N$  symmetric, sparse matrices with  $N$  being the total number of edges resulting from the subdivision of the body,  $\{E\}$  is a  $N \times 1$  column vector denoting the edge fields and  $\lambda = k_o^2$  gives the eigenvalues of the system. Solving ( 9), we obtain the resonant wavenumber  $k_o$  and the resonant field distribution  $\{E\}$  as well.

In the case of the scattering problem, ( 3) can be conveniently written in matrix form as

$$[A'^e] \{E^e\} = \{C^e\} \quad (10)$$

where

$$A'_{ij} = \int_{V_e} \left( \frac{1}{\mu_r} (\nabla \times \mathbf{W}_i^e) \cdot (\nabla \times \mathbf{W}_j^e) - k_o^2 \epsilon_r \mathbf{W}_i^e \cdot \mathbf{W}_j^e \right) dv \quad (11)$$

$$C_i^e = j k_o Z_o \oint_{S_e} \mathbf{W}_i^e \cdot (\mathbf{n} \times \mathbf{H}) ds \quad (12)$$

Summing over all  $M$  elements in the geometry, we obtain a system of equations whose solution yields the field components over the entire body.

$$\sum_{e=1}^M [A'^e] \{E^e\} = \sum_{e=1}^M \{C^e\}$$

which gives

$$[A'] \{E\} = \{C\} \quad (13)$$

where  $\{E\}$  are defined as in ( 9),  $[A']$  is a  $N \times N$  matrix and  $\{C\}$  is a column vector of size  $N$  related to the tangential magnetic field over the exterior surface of the body. On separating the on-surface edges from the edges inside the body for ease of representation, we obtain

$$\begin{aligned} [A'_{ss}] \{E_s\} + [A'_{si}] \{E_i\} &= \{C_s\} \\ [A'_{is}] \{E_s\} + [A'_{ii}] \{E_i\} &= 0 \\ \{C_s\} &= [B'_{ss}] \{H_s\} \end{aligned} \quad (14)$$

where the subscript  $s$  denotes the edges on the surface and  $i$  represents the edges inside the body. It is thus readily seen that (14) relates the electric field inside and on the surface of the body to the on-surface tangential magnetic field. However, (14) contains two unknown vectors  $\{E\}$  and  $\{H\}$  and the system can, therefore, be solved only when we relate the electric field with the magnetic field. This is done by introducing an absorbing boundary condition at the outer boundary of the mesh as discussed in section 2.3.

## 2.2 Basis functions

The vector edge basis functions for rectangular bricks are outlined in detail in [9]. The basis functions for tetrahedral elements merit detailed mention since they are more involved.

Vector fields within tetrahedral domains in three dimensional space can be conveniently represented by expansion functions that are linear in the spatial variables and have either zero divergence or zero curl. The basis functions defined in [8] are associated with the six edges of the tetrahedron and have zero divergence and constant curl. Assuming the four nodes and the six edges of a tetrahedron are numbered according to Table 1, the vector basis functions associated with the  $(7-i)$ th edge of the tetrahedron are defined as

$$\mathbf{W}_{7-i} = \begin{cases} \mathbf{f}_{7-i} + \mathbf{g}_{7-i} \times \mathbf{r}, & \mathbf{r} \text{ in the tetrahedron} \\ 0, & \text{otherwise} \end{cases} \quad (15)$$

with

$$\mathbf{f}_{7-i} = \frac{b_{7-i}}{6V} \mathbf{r}_{i_1} \times \mathbf{r}_{i_2} \quad (16)$$

$$\mathbf{g}_{7-i} = \frac{b_i b_{7-i} \mathbf{e}_i}{6V} \quad (17)$$

where  $i = 1, 2, \dots, 6$ ,  $V$  is the volume of the tetrahedral element,  $\mathbf{e}_i = (\mathbf{r}_{i_2} - \mathbf{r}_{i_1})/b_i$  is the unit vector of the  $i$ th edge and  $b_i = |\mathbf{r}_{i_2} - \mathbf{r}_{i_1}|$  is the length of the  $i$ th edge. All distances are measured with respect to the origin.

Since there are two numbering systems, local and global, a unique global edge direction is defined (e.g., always pointing from the smaller node number to the larger node number)[10] to ensure the continuity of  $\mathbf{n} \times \mathbf{E}$  across all edges. This implies that (15) should be multiplied by (-1) if the local edge vector (as defined in Table 1) does not have the same direction as the global edge direction, i.e. the local vector points from the larger node number to the smaller node number. Finally, since  $\nabla \cdot \mathbf{W}_i = 0$  the electric field obtained through (2) exactly satisfies the divergence equation within the element, i.e.  $\nabla \cdot \mathbf{E} = 0$ . Therefore, the finite element solution is free from contamination of spurious solutions.

## 2.3 Mesh termination

Differential equation methods, such as finite elements, can only solve boundary value problems. Since electromagnetic problems are open boundary-

infinite domain types, a means to truncate the solution domain to lie within a finite boundary must be found. On this boundary, a condition is enforced thus ensuring that the fields will obey the Sommerfeld radiation condition at distances asymptotically far from the object. These absorbing boundary conditions (ABCs) have a significant advantage over the global methods of solving unbounded problems using finite elements in that they are local in nature. Due to this, the sparse matrix structure of the finite element formulation is retained. One disadvantage, however, is that ABCs are approximate and do not model the exterior field exactly.

The objective of absorbing boundary conditions is to truncate the finite element mesh with boundary conditions that cause minimum reflections of an outgoing wave. These ABCs should provide small, acceptable errors while minimising the distance from the object of interest to the outer boundary. This minimal distance is required to reduce the number of unknowns in the problem for computational efficiency.

There are two ways to approach this problem. The first approach is to employ a three dimensional vector boundary condition for terminating the finite element mesh of the body described in section 2.1. The second method involves placing an artificial conducting boundary (electric or magnetic) to truncate the infinite region and then coating the inner surface of the boundary with a layer or several layers of fictitious dielectric whose thickness and constitutive parameters are chosen to minimise the non-physical reflections of the scattered field over a wide range of incidence angles[11].

### 2.3.1 Vector ABC

We begin with the Wilcox representation[12] of the electric field which has an expansion

$$\mathbf{E}(\mathbf{r}) = \frac{e^{-jkr}}{r} \sum_{n=0}^{\infty} \frac{\mathbf{A}_n(\theta, \phi)}{r^n} \quad (18)$$

From ( 18), we get

$$\nabla \times \mathbf{E} = \left\{ jk\hat{r} \times \frac{1 + D_1}{r} \right\} \mathbf{E} - \frac{e^{-jkr}}{r^2} \sum_{n=1}^{\infty} \frac{n\mathbf{A}_{nt}}{r^n} \quad (19)$$

where  $\mathbf{A}_{nt} = \hat{r} \times \mathbf{A}_n$  is the transverse component of  $\mathbf{A}_n$  and, for a vector  $\mathbf{F}$ ,  $D_1\mathbf{F}$  is given by

$$\begin{aligned} D_1\mathbf{F} = & \frac{1}{\sin\theta} \left[ \frac{\partial}{\partial\theta}(\sin\theta F^\phi) - \frac{\partial F^\theta}{\partial\phi} \right] \hat{r} \\ & + \frac{1}{\sin\theta} \left[ \frac{\partial F^r}{\partial\theta} - \sin\theta F^\phi \right] \hat{\theta} + \left[ F^\theta - \frac{\partial F^r}{\partial\theta} \right] \hat{\phi} \end{aligned} \quad (20)$$

Using the recursion relation

$$-2jkn\mathbf{A}_{nt} = n(n-1)\mathbf{A}_{n-1,t} + D_4\mathbf{A}_{n-1}$$

where

$$\begin{aligned}
D_4 \mathbf{A}_n &= (D A_n^\theta + D_\theta \mathbf{A}_n) \hat{\theta} + (D A_n^\phi + D_\phi \mathbf{A}_n) \hat{\phi} \\
D_\theta \mathbf{A}_n &= 2 \frac{\partial A_n^r}{\partial \theta} - \frac{1}{\sin^2 \theta} A_n^\theta - \frac{2 \cos \theta}{\sin^2 \theta} \frac{\partial A_n^\phi}{\partial \theta} \\
D_\phi \mathbf{A}_n &= \frac{2}{\sin \theta} \frac{\partial A_n^r}{\partial \phi} - \frac{1}{\sin^2 \theta} A_n^\phi + \frac{2 \cos \theta}{\sin^2 \theta} \frac{\partial A_n^\theta}{\partial \phi}
\end{aligned}$$

and  $D$  is Beltrami's operator[10], we can derive the representation correct to  $r^{-4}$ . Applying the recursion relation in (19) yields the desired relationship for the vector ABC:

$$\nabla \times \mathbf{E} = \alpha(r) \mathbf{E} + \beta(r) D_4 \mathbf{E} \quad (21)$$

where

$$\alpha(r) = jk \left\{ \frac{D_1}{jkr} - \left( 1 + \frac{1}{jkr} \right) \hat{r} \times \right\} \quad (22)$$

$$\beta(r) = \frac{1}{2jkr^2} \frac{1}{(1 + 1/jkr)} \quad (23)$$

The ABC formulated above was derived for spherical boundaries and hence would be storage intensive and numerically inefficient when used to terminate the mesh of long and thin geometries. It would be highly desirable to choose an outer boundary that conforms to the shape of the object. It is the authors' intention to extend the boundary condition discussed above to conformal boundaries. Another way to introduce a conformal outer boundary is to use the fictitious absorber model discussed below.

### 2.3.2 Fictitious absorber model

In this section, our intention is to develop a model which can absorb the reflections of the scattered field from the artificial outer boundary over as wide a range of incidence angles as possible. The reflection coefficient on applying the appropriate boundary condition can be symbolically written as

$$R = f(t_1, \epsilon_{r1}, \mu_{r1}; t_2, \epsilon_{r2}, \mu_{r2}; \dots; t_n, \epsilon_{rn}, \mu_{rn}; \lambda, \theta) \quad (24)$$

for an  $n$ -layer absorber. Here,  $t_i, \epsilon_{ri}$  and  $\mu_{ri}$  denote the thickness, relative permittivity and relative permeability of the  $i$ th dielectric layer. Using a multi-dimensional minimization algorithm such as that based on the downhill simplex method, we can find a set of  $t_i, \epsilon_{ri}, \mu_{ri}$  that minimises the magnitude of the reflection coefficient over a wide range of incidence angles. Further, the outer boundary of the mesh can be made conformal to the shape of the scatterer reducing the number of unknowns compared to the earlier approach which works solely for spherical outer boundaries.

## 2.4 Solution of the finite element equations

### 2.4.1 Vector ABC

An inspection of ( 13) reveals that for an inhomogeneous body, there is no a priori information about the tangential magnetic field over the exterior surface of the body. Relation ( 13) therefore contains two unknown vectors,  $\{E\}$  and  $\{C\}$ , and thus another condition is required involving the two variables to permit an evaluation of the fields inside and on the surface of the body. This condition relating the tangential electric field to the tangential magnetic field on the surface is provided by ( 21). Since the ABC in ( 21) refers to the scattered field, we can rewrite it as

$$\begin{aligned}\nabla \times \mathbf{E}_s^s &= \alpha(r)\mathbf{E}_s^s + \beta(r)D_4\mathbf{E}_s^s \\ \mathbf{H}_s^s &= \frac{j}{\omega\mu} [\alpha(r)\mathbf{E}_s^s + \beta(r)D_4\mathbf{E}_s^s] \\ &= \mathcal{K}\mathbf{E}_s^s\end{aligned}\quad (25)$$

where  $\mathcal{K} = \frac{j}{\omega\mu} [\alpha(r) + \beta(r)D_4]$  and the subscript  $s$  denotes the field on the surface and the superscript  $s$  represents the scattered field. As the total field is a sum of the incident field and the scattered field, therefore from ( 25), we obtain

$$\mathbf{H}_s - \mathbf{H}_s^{inc} = \mathcal{K}(\mathbf{E}_s - \mathbf{E}_s^{inc}) \quad (26)$$

Since  $\{H_s\} = [B_{ss}]^{-1}\{C_s\}$  from ( 14), we obtain on substituting ( 26) into ( 14)

$$\begin{aligned}([A'_{ss}] - [B_{ss}]\mathcal{K})\{E_s\} + [A'_{si}]\{E_i\} &= [B_{ss}]\left(\{H_s^{inc}\} - \mathcal{K}\{E_s^{inc}\}\right) \\ [A'_{is}]\{E_s\} + [A'_{ii}]\{E_i\} &= 0\end{aligned}\quad (27)$$

The above equation can thus be solved for the unknown electric fields both inside and on the surface of the body.

### 2.4.2 Fictitious absorber model

Since an artificial outer boundary is placed in this case, the column vector  $\{C\}$  in ( 13) is a function of the incident field and the integration is carried out over the outer and inner surfaces. Therefore, we can rewrite ( 14) as

$$\begin{aligned}[A''_{ss}]\{E_s^s\} + [A''_{si}]\{E_i^s\} &= \{C_s^{inc}\} \\ [A''_{is}]\{E_s^s\} + [A''_{ii}]\{E_i^s\} &= 0\end{aligned}\quad (28)$$

where the superscript *inc* stands for the incident field, the superscript  $s$  denotes the scattered field, the subscripts are as defined in ( 14) and  $[A'']$  contains contributions from the surface integral as well as  $[A']$ .

### 3 Results

In Table 2, the eigenvalues for a  $1\text{cm} \times .5\text{cm} \times .75\text{cm}$  rectangular cavity are calculated using nodal basis functions. This particular derivation is outlined in [13] and the existence of ‘spurious’ modes is clearly observed when the zero divergence condition is not rigidly enforced ( $s = 0$ ). For non-zero values of  $s$ , ‘spurious’ modes do not appear. However, arbitrary values of  $s$  lead to inaccuracies and, therefore, the most suitable value needs to be determined by trial and error.

Using edge-based rectangular bricks results in better accuracy as observed in Table 3. However, on comparing bricks with tetrahedra, it is seen from Table 4 that the tetrahedral edge element is the best in terms of accuracy for the same storage requirement. The maximum edge length for the rectangular brick elements was  $.15\text{cm}$  whereas that for the tetrahedral elements was  $.2\text{cm}$ .

In Tables 4-7, we compare the eigenvalues computed using edge-based tetrahedral finite elements with their analytical counterparts. The finite element mesh was generated using SDRC I-DEAS, a commercial pre-processing package and it is seen that the numerical results are in excellent agreement with the exact values for both homogeneous and inhomogeneous cavities. In Table 4, the edge-based approach predicts the first six distinct non-trivial eigenvalues with less than 4 per cent error for an empty rectangular cavity. The exact eigenvalues of the half-filled cavity as described in Table 5 are computed by solving the transcendental equation obtained by matching the tangential electric and magnetic fields at the air-dielectric interface. As seen, these results agree with the results of the finite element code to within 1 per cent. Table 6 compares the analytical and computed eigenvalues of a cylindrical cavity having a base radius of  $0.5\text{cm}$  and a height of  $0.5\text{cm}$ . The eigenvalues are again seen to be quite accurate and the accuracy is expected to increase further with higher mesh density. Similar comparisons are given in Table 7 of a sphere of  $1\text{cm}$  radius. Finally, Table 8 presents the eigenvalues of the geometry shown in Fig. 1. This is basically a closed metallic cavity with a ridge along one of its faces. We note again that it is difficult to treat such a geometry having sharp edges and corners using node-based finite elements. The storage requirement for the geometries discussed above can be further reduced by taking symmetry into account. Since we are interested in developing a code for arbitrary geometries, boundary conditions taking advantage of symmetry have not been introduced.

It is noted that as the degeneracy of the eigenvalues increases, the matrix becomes increasingly ill-conditioned and the numerical solution correspondingly less accurate[14]. This is clearly observed from the data in Table 7 for the case of a perfectly conducting hollow spherical cavity. Since the second lowest TM mode has five-fold degeneracy, the computational error is seen to be the greatest. However, for the partially filled rectangular cavity, the absence of degenerate modes gives results which are accurate to within 1 per cent of the exact eigensolutions.

## 4 Conclusions and future work

It has been shown that the resonant frequencies of an arbitrarily shaped inhomogeneously filled metallic resonator can be computed very accurately using edge-based tetrahedral elements. The nodal method is not very reliable and is dependent on the value of the  $s$  parameter which is a measure of how strongly one wants to enforce the divergence-free condition. Edge-based rectangular bricks do not provide as good an accuracy as edge-based tetrahedral elements and is limited to a small class of geometries. It has, therefore, been established that it is best to use edge-based tetrahedral elements for solving three-dimensional problems.

In the future, we intend to work on three dimensional scattering problems using edge-based tetrahedra and employing the mesh termination techniques discussed in section 2.3. We also plan to focus on the derivation of new absorbing boundary conditions conformal to the shape of the scatterer.

## 5 Appendix

### 5.1 Derivation of matrix elements

The derivation of the matrix elements in ( 9) amounts to evaluating the integrals in ( 5) and ( 6). Therefore, from ( 5), we have

$$\int_{V_e} \frac{1}{\mu_r} (\nabla \times \mathbf{W}_i^e) \cdot (\nabla \times \mathbf{W}_j^e) = \frac{4}{\mu_r} \mathbf{g}_i \cdot \mathbf{g}_j V_e \quad (29)$$

since  $\nabla \times \mathbf{W}_i^e = 2\mathbf{g}_i$ . The evaluation of the integral in ( 6) is more cumbersome. Substituting into ( 6) the basis functions defined in ( 16) and ( 17), we obtain

$$\begin{aligned} \epsilon_r \int_{V_e} \mathbf{W}_i^e \cdot \mathbf{W}_j^e dv &= \epsilon_r \int_{V_e} \{(\mathbf{f}_i \cdot \mathbf{f}_j) + (\mathbf{r} \cdot \mathbf{D}) + (\mathbf{g}_i \times \mathbf{r}) \cdot (\mathbf{g}_j \times \mathbf{r})\} dv \quad (30) \\ &= \epsilon_r (I_1 + I_2 + I_3) \end{aligned}$$

where

$$\mathbf{D} = (\mathbf{f}_i \times \mathbf{g}_j) + (\mathbf{f}_j \times \mathbf{g}_i)$$

and

$$I_1 = \int_{V_e} \mathbf{f}_i \cdot \mathbf{f}_j dv \quad (31)$$

$$I_2 = \int_{V_e} \mathbf{r} \cdot \mathbf{D} dv \quad (32)$$

$$I_3 = \int_{V_e} (\mathbf{g}_i \times \mathbf{r}) \cdot (\mathbf{g}_j \times \mathbf{r}) dv \quad (33)$$

Since  $\mathbf{f}$  is a constant vector,  $I_1$  reduces to

$$I_1 = \mathbf{f}_i \cdot \mathbf{f}_j V_e \quad (34)$$

Since

$$\begin{aligned} x &= \sum_{i=1}^4 L_i x_i \\ y &= \sum_{i=1}^4 L_i y_i \\ z &= \sum_{i=1}^4 L_i z_i \end{aligned}$$

where  $L_i$  are the shape functions for the tetrahedral element and  $x_i, y_i, z_i$  ( $i = 1, \dots, 4$ ) denote the  $x, y$  and  $z$  co-ordinates of the vertices of the tetrahedral element. Using the standard formula for volume integration within a tetrahedral element and simplifying, we have

$$I_2 = \frac{V_e}{4} \left[ D_x \sum_{i=1}^4 x_i + D_y \sum_{i=1}^4 y_i + D_z \sum_{i=1}^4 z_i \right] \quad (35)$$

where  $D_m$  is the  $m$ th component of  $\mathbf{D}$ . The evaluation of  $I_3$  can be simplified by the use of basic vector identities. Therefore,

$$\begin{aligned} I_3 &= \mathbf{g}_i \cdot \mathbf{g}_j \int_{V_e} |\mathbf{r}|^2 dv - \int_{V_e} (\mathbf{g}_i \cdot \mathbf{r})(\mathbf{g}_j \cdot \mathbf{r}) dv \\ &= (g_{iy}g_{jy} + g_{iz}g_{jz}) \int_{V_e} x^2 dv + (g_{ix}g_{jx} + g_{iz}g_{jz}) \int_{V_e} y^2 dv + (g_{ix}g_{jx} + g_{iy}g_{jy}) \int_{V_e} z^2 dv \\ &\quad - (g_{ix}g_{jy} + g_{jx}g_{iy}) \int_{V_e} xy dv - (g_{ix}g_{jz} + g_{jx}g_{iz}) \int_{V_e} zx dv - (g_{iy}g_{jz} + g_{jy}g_{iz}) \int_{V_e} yz dv \end{aligned} \quad (36)$$

where  $g_{im}$  represents the  $m$ th component of the vector  $\mathbf{g}_i$ . Each of the integrals in (36) can be easily evaluated analytically and the result expressed in the following general form:

$$\int_{V_e} a_l a_m dv = \frac{V_e}{20} \left[ \sum_{i=1}^4 a_{li} a_{mi} + \sum_{i=1}^4 a_{li} \sum_{i=1}^4 a_{mi} \right] \quad (37)$$

where  $l, m = 1, \dots, 3$  and  $a_1$  represents the variable  $x$ ,  $a_2$  stands for the variable  $y$  and  $a_3$  denotes the variable  $z$ .

## 6 References

1. Z.J. Cendes and P. Silvester, "Numerical solution of dielectric loaded waveguides: I - Finite element analysis", *IEEE Trans. Microwave Theory Tech.*, vol. 18, pp.1124-31, 1970.
2. B.M.A. Rahman and J.B. Davies, "Penalty function improvement of

- waveguide solution by finite elements”, *IEEE Trans. Microwave Theory Tech.*, vol. 32, pp.922-8, Aug. 1984.
3. J.P. Webb, “The finite-element method for finding modes of dielectric-loaded cavities”, *IEEE Trans. Microwave Theory Tech.*, vol. 33, no.7, pp.635-9, July 1985.
  4. J.P. Webb, “Finite element analysis of dispersion in waveguides with sharp metal edges”, *IEEE Trans. Microwave Theory Tech.*, vol. 36, no.12, pp.1819-24, Dec. 1988.
  5. X. Yuan, D.R. Lynch and K. Paulsen, “Importance of normal field continuity in inhomogeneous scattering calculations”, *IEEE Trans. Microwave Theory Tech.*, vol. 39, no.4, pp.638-42, April 1991.
  6. A. Bossavit, “A rationale for ‘edge-elements’ in 3-D fields computations”, *IEEE Trans. Magn.*, vol. 24, no.1, pp.74-9, Jan. 1988.
  7. A. Bossavit, “Solving Maxwell equations in a closed cavity, and the question of ‘spurious’ modes”, *IEEE Trans. Magn.*, vol. 26, no.2, pp.702-5, March 1990.
  8. M.L. Barton and Z.J. Cendes, “New vector finite elements for three-dimensional magnetic field computation”, *J. Appl. Phys.*, vol. 61, no.8, pp.3919-21, April 1987.
  9. J.M. Jin and J.L. Volakis, “Electromagnetic scattering by and transmission through a three-dimensional slot in a thick conducting plane”, *IEEE Trans. Antennas Propagat.*, vol. 39, no.4, pp. 543-50, April 1991.
  10. X. Yuan, “Three-dimensional electromagnetic scattering from inhomogeneous objects by the hybrid moment and finite element method”, *IEEE Trans. Microwave Theory Tech.*, vol. 38, no.8, pp. 1053-9, Aug. 1990.
  11. J.M. Jin, J.L. Volakis and V.V. Liepa, “An engineer’s approach for terminating finite element meshes in scattering analysis”, to appear.
  12. C.H. Wilcox, “An expansion theorem for electromagnetic fields”, *Comm. Pure Appl. Math.*, vol. 9, pp. 115-134, May 1956.
  13. J.M. Jin and J.L. Volakis, “A finite element-boundary integral formulation for scattering by three-dimensional cavity-backed apertures”, *IEEE Trans. Antennas Propagat.*, vol. 39, no.1, pp. 97-104, Jan. 1991.
  14. G.H. Golub and C.F. Van Loan, *Matrix Computations*, pp. 202-4, The Johns Hopkins University Press, 1985.

Edge no.	$i_1$	$i_2$
1	1	2
2	1	3
3	1	4
4	2	3
5	4	2
6	3	4

Table 1: Tetrahedron edge definition

Mode no.	Exact	s=0	s=.5	s=1	s=5
spurious		2.010			
spurious		3.312			
spurious		4.443			
spurious		4.928			
TE101	5.236	5.318	5.427	5.447	5.571
spurious		5.759			
spurious		6.255			
spurious		6.804			
TM 110	7.025	7.067	6.574	7.543	7.940
spurious		7.305			
TE 011	7.531	7.389	7.476	7.635	8.014
TE 201	7.531	7.640	7.659	8.072	8.348

Table 2: Eigenvalues for an empty 1cm  $\times$  0.5cm  $\times$  0.75cm rectangular cavity computed using nodal basis (230 unknowns)

Mode no.	Analytical	Computed	Error(%)
TE 101	5.236	5.307	-1.36
TM 110	7.025	7.182	-2.23
TE 011	7.531	7.725	-2.58
TE 201	7.531	7.767	-3.13
TM 111	8.1789	8.350	-2.09
TE 111	8.1789	8.350	-2.09
TM 210	8.886	9.151	-2.98
TE 102	8.947	9.428	-5.38

Table 3: Eigenvalues for an empty 1cm  $\times$  0.5cm  $\times$  0.75cm rectangular cavity using edge-based rectangular bricks (270 unknowns)

Mode no.	Analytical	Computed	Error(%)
TE 101	5.236	5.213	.44
TM 110	7.025	6.977	.70
TE 011	7.531	7.474	1.00
TE 201	7.531	7.573	-.56
TM 111	8.1789	7.991	2.29
TE 111	8.1789	8.122	.70
TM 210	8.886	8.572	3.53
TE 102	8.947	8.795	1.70

Table 4: Eigenvalues for an empty 1cm  $\times$  0.5cm  $\times$  0.75cm rectangular cavity (260 unknowns)

Mode no.	Analytical	Computed	Error(%)
TEz 101	3.538	3.534	.11
TEz 201	5.445	5.440	.10
TEz 102	5.935	5.916	.32
TEz 301	7.503	7.501	.04
TEz 202	7.633	7.560	.97
TEz 103	8.096	8.056	.50

Table 5: Eigenvalues for a half-filled 1cm  $\times$  0.1cm  $\times$  1cm rectangular cavity ( $\epsilon_r = 2$ ) (192 unknowns)

Mode no.	Analytical	Computed	Error(%)
TM 010	4.810	4.809	.02
TE 111	7.283	7.202	1.1
		7.288	-.07
TM 110	7.650	7.633	.22
		7.724	-.97
TM 011	7.840	7.940	-1.28
TE 211	8.658	8.697	-.45
		8.865	-2.39

Table 6: Eigenvalues for an empty cylindrical cavity of base radius 0.5cm and height 0.5 cm (380 unknowns)

Mode no.	Analytical	Computed	Error(%)
TM 010	2.744	2.799	-2.04
TM 111,even		2.802	-2.11
TM 111,odd		2.811	-2.44
TM 021	3.870	3.948	-2.02
TM 121,even		3.986	-2.99
TM 121,odd		3.994	-3.20
TM 221,even		4.038	-4.34
TM 221,odd		4.048	-4.59
TE 011	4.493	4.433	1.33
TE 111,even		4.472	.47
TE 111,odd		4.549	-1.25

Table 7: Eigenvalues for an empty spherical cavity of radius 1cm (300 unknowns)

1	4.941
2	7.284
3	7.691
4	7.855
5	8.016
6	8.593
7	8.906
8	9.163
9	9.679
10	9.837

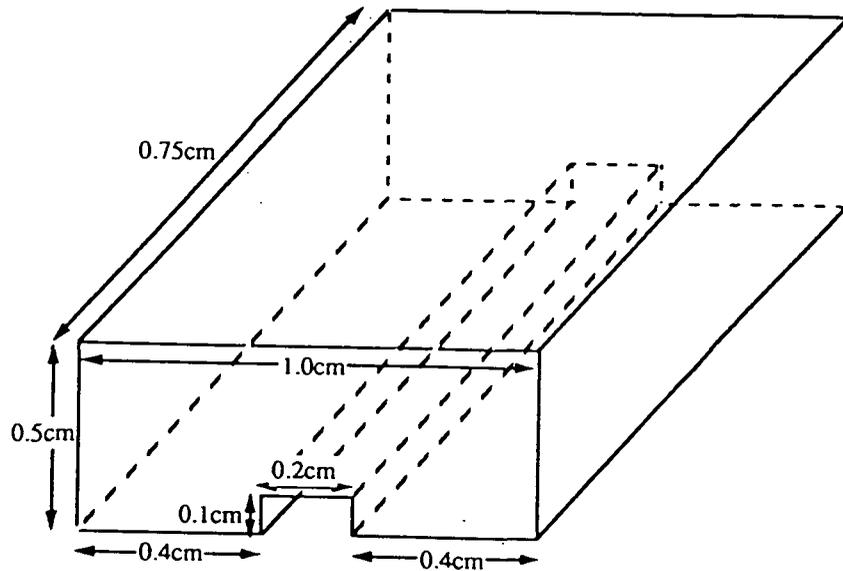


Figure 1: A ridged cavity

Table 8: Ten lowest non-trivial eigenvalues of Fig. 1 (267 unknowns)

**The following is a listing of the computer programs generating the node-based and edge-based elements, interfacing with SDRC IDEAS and computing the eigenvalues of an inhomogeneously filled, arbitrarily shaped cavity.**

=====  
Processes a universal file obtained from IDEAS and converts the nodal info to edge info needed for constructing an edge-based three-dimensional finite element mesh using tetrahedral elements.

Stores the node numbers and respective nodal coordinates in 'noddy'

Stores the element numbers and corresponding nodes in 'elno'

Processes 'noddy' and 'elno' and stores the edge nos. and nodal connections in 'glob' and edge nos. with corresponding edge vector in 'edgy'

Note: Edge overlaps are taken care of.

Storage limit: 800 nodes, 3000 elements, 4300 edges  
=====

```

program unv_file_processor
character string*80, yastrn*40, unv*20
integer n1(3000,4),tab(4300,2),nn(100),tr(3000),nun(3000),
1      bc(3000,3),edgv(18000,3),mat(3000)
real x(800),y(800),z(800)
common /bank/n1,x,y,z,ne,mat
common /dbase/edgv
common /local/ncount
write(6,*)'1) Cavity problem 2) Scattering problem'
read(5,*)ivar
write(6,*)'Name of universal file ?'
read(5,'(A)')unv
open(1,file=unv)
open(2,file='enoddy')
open(3,file='elno')
open(4,file='eglob')
open(7,file='edgy')
open(8,file='esurfed')
.Processing universal file for info on various parameters
read(1,'(A)')string
l=0
if (string(4:6).eq.'151') then
  write(6,*)'Encountered header'
  go to 15
elseif (string(4:6).eq.'747') then
  read(1,'(A)')string
  if (string(5:6).ne.'-1') then
    if (string(9:9).ne.' ') then
      write(4,*)string(2:13)
      do ik=1,4
        read(1,'(A)')string
      enddo
    endif
    go to 2
  endif
.Processing nodal info; data stored in 'noddy'
elseif (string(4:6).eq.' 15') then
  read(1,'(A)')string
  if (string(5:6).ne.'-1') then
    write(2,*)string(7:10),' ',string(41:53),' ',string(54:66),' '
1      ,string(67:79)
    l=l+1
    go to 5
  endif
  ll=l
  write(6,*)'There are ',l,' nodes.'
  write(4,*)l
.Processing element info; data stored in 'elno'

```

```

elseif (string(4:6).eq.' 71') then
  read(1,'(A)')string
  if (string(5:6).ne.'-1') then
    read(1,'(A)')yastrn
    write(3,*)string(7:10),' ',yastrn(7:10),' ',yastrn(17:20),
1    ' ',yastrn(27:30),' ',yastrn(37:40),' ',string(49:50)
    l=l+1
    go to 10
  else
    write(6,*)'There are ',l,' elements.'
    write(4,*)l
    l2=1
  endif
elseif (string(4:6).eq.'752') then
  ltmp=0
  nn(1)=0
  read(1,'(A)')string
  if (string(19:20).eq.' 0') then
    ltmp=ltmp+1
    read(string(57:60),'(I4)')numb
    nn(ltmp+1)=numb+nn(ltmp)
  elseif (string(5:6).eq.'-1') then
    write(6,*)'There are ',ltmp,' surfaces.'
    go to 20
  elseif (string(1:1).eq.' ') then
    do i=1,4
      if (string((20*i-3):20*i).ne.' ') then
        l=l+1
        read(string((20*i-3):20*i),'(I4)')tr(1)
      endif
    enddo
  endif
  go to 30
endif
go to 15
close(1)
.Data from 'noddy' and 'elno' stored in
n1 - table of nodes making up the corresponding element
x,y,z - nodal coordinate table
rewind 2
rewind 3
do i=1,11
  read(2,*)na,x(i),y(i),z(i)
enddo
do i=1,12
  read(3,*)nk,n1(i,1),n1(i,2),n1(i,3),n1(i,4),mat(i)
enddo
.Close 'noddy' and 'elno' for good
close(2)
close(3)
ncount=0
write(6,*)'Be patient #*!/?/#@*!!!'
do ne=1,l2
.Store edge info in an integer array 'tab' after checking for
overlap. The subroutine 'compare' is the heart of the program.
  call compare(tab)
.Commenting out the following statement causes a speedup of 250%
  write(6,*)'Processed element no. ',ne,' :edge count= ',ncount
enddo

```

```
write(6,*)'Edge count = ',ncount
rewind(4)
write(6,*)'No. of dielectric layers?'
read(5,*)itemp
read(4,*)(xtmp,i=1,itemp)
read(4,*)(nj,i=1,2)
do i=1,(6*12)
  read(4,*)nk,edgv(i,1),edgv(i,2),edgv(i,3),nj
enddo
close(4)
close(7)
nsurf=0
if (ivar.eq.1) then
  do i=1,ltmp
    write(6,*)'Processing surface ',i,' for on-surface edges.'
    do j=nn(i)+1,nn(i+1)
      do k=nn(i)+1,nn(i+1)
        do l=1,ncount
          if (tab(l,1).ne.0) then
            if ((tr(j).eq.tab(l,1)).and.(tr(k).eq.tab(l,2))) then
              write(8,*)l
              tab(l,1)=0
              nsurf=nsurf+1
              go to 40
            endif
          endif
        enddo
      enddo
    enddo
  enddo
  write(6,*)'Total no. of on-surface edges= ',nsurf
  write(6,*)'Fem matrix to be solved is of order ',(ncount-nsurf)
else
  ncnt=0
  do ii=1,ltmp
    do ik=1,12
      nun(ik)=0
    enddo
    do i=nn(ii)+1,nn(ii+1)
      do j=1,12
        do k=1,4
          if (tr(i).eq.n1(j,k)) then
            nun(j)=nun(j)+1
            bc(j,nun(j))=n1(j,k)
            if (nun(j).eq.3) then
              call edge(j,bc(j,1),bc(j,2),bc(j,3))
              ncnt=ncnt+1
              go to 80
            endif
          endif
        enddo
      enddo
    enddo
  enddo
  write(6,*)'There are ',ncnt,' surface elements.'
endif
close(8)
stop
end
```

```
=====
'compare' checks for all possible edges avoiding overlap and stores the
info in an array 'tab'. The file 'edgy' contains the element no.
and the six edge vectors corresponding to that element.
=====
```

```
subroutine compare(tab)
integer n1(3000,4),mat(3000)
real x(800),y(800),z(800)
integer nt(6,2),tab(4300,2)
common /bank/n1,x,y,z,ne,mat
common /local/ncount
nt(1,1)=n1(ne,1)
nt(1,2)=n1(ne,2)
nt(2,1)=n1(ne,1)
nt(2,2)=n1(ne,3)
nt(3,1)=n1(ne,1)
nt(3,2)=n1(ne,4)
nt(4,1)=n1(ne,2)
nt(4,2)=n1(ne,3)
nt(5,1)=n1(ne,2)
nt(5,2)=n1(ne,4)
nt(6,1)=n1(ne,3)
nt(6,2)=n1(ne,4)
```

```
.Arranging node couplets in ascending order; a personal choice
```

```
do i=1,6
  if (nt(i,1).gt.nt(i,2))then
    ntmp=nt(i,1)
    nt(i,1)=nt(i,2)
    nt(i,2)=ntmp
  endif
enddo
```

```
.A brute force search for overlapping edges
```

```
l=ncount
do ii=1,6
  if (ne.eq.1) go to 32
  do i=1,ncount
    if ((tab(i,1).eq.nt(ii,1)).and.(tab(i,2).eq.nt(ii,2))) then
      write(4,*)ne,i,nt(ii,1),nt(ii,2),mat(ne)
      go to 35
    endif
  enddo
  l=l+1
  tab(l,1)=nt(ii,1)
  tab(l,2)=nt(ii,2)
  write(4,*)ne,l,nt(ii,1),nt(ii,2),mat(ne)
  write(7,*)l,x(nt(ii,2))-x(nt(ii,1)),y(nt(ii,2))-y(nt(ii,1)),
1      z(nt(ii,2))-z(nt(ii,1))
enddo
ncount=l
return
end
```

```
=====
Determines edges corresponding to the surface element
=====
```

```
subroutine edge(m,j1,j2,j3)
integer edgv(18000,3),tmp(3)
common /dbase/edgv
do ij=(6*m)-5,(6*m)
  if (j1.eq.edgv(ij,2)) then
```

```
if (j2.eq.edgv(ij,3)) then
  tmp(1)=edgv(ij,1)
elseif (j3.eq.edgv(ij,3)) then
  tmp(2)=edgv(ij,1)
endif
elseif (j2.eq.edgv(ij,2)) then
  if (j3.eq.edgv(ij,3)) then
    tmp(3)=edgv(ij,1)
  endif
endif
enddo
write(8,*)m,j1,j2,j3,tmp
return
end
```

```
=====
.Computes the eigenvalues of an inhomogeneous cavity having arbitrary
shape using edge elements.
=====
```

```

program fem
integer edna(15000),gnn(15000,2),tab(6,3),sed(2000),edst(3000,2)
1      ,mat(2500)
character bit(6)*1
real xyz(3000,3),a1(6,6),x(500),y(500),z(500),b1(6,6),eps(10)
double precision a(700,700),b(700,700),alfr(700),alfi(700)
1      ,beta(700)
      logical matz
common /bank/edna,gnn,xyz,eps,mat
common /mess/x,y,z
. Reading in info
write(6,*)'Number of edges'
read(5,*)ned
write(6,*)'Number of on-surface edges'
read(5,*)nes
write(6,*)'If inhomogeneous, enter 1'
read(5,*)ivar
if (ivar.eq.1) then
  write(6,*)'Number of different permittivities'
  read(5,*)nl
endif
open(1,file='eglob')
open(2,file='edgy')
open(3,file='enoddy')
open(4,file='eigl')
open(7,file='esurfed')
read(1,*)(eps(i),i=1,nl)
read(1,*)nn
do i=1,nn
  read(3,*)k,x(i),y(i),z(i)
enddo
  write(6,*)'Finished reading in nodes'
read(1,*)nel
do i=1,6*nel
  itemp=1+(i/6.)
  read(1,*)elm,edna(i),gnn(i,1),gnn(i,2),mat(itemp)
enddo
write(6,*)eps(mat(1)),eps(mat(47)),eps(mat(48)),eps(mat(74))
write(6,*)'Finished reading in elements'
do i=1,ned
  read(2,*)k,xyz(i,1),xyz(i,2),xyz(i,3)
enddo
write(6,*)'Finished reading in edges'
read(7,*)(sed(i),i=1,nes)
close(1)
close(2)
close(3)
close(7)

```

```

.The following program segment generates the FEM matrix and imposes
the boundary condition for the on-surface nodes simultaneously.
It compares the on-surface edges stored in the array 'sed' and
stores the complement in 'a' and 'b'. It also keeps a record of
the new edge numbers and their corresponding old edge numbers in
the pointer array 'edst'.

```

```
net=ned-nes
```

```

do i=1,net
  do j=1,net
    a(i,j)=0.d0
    b(i,j)=0.d0
  enddo
enddo
write(6,*)'Generating FEM matrix'
do i=1,3000
  edst(i,1)=0
  edst(i,2)=0
enddo
nptrx=1
do i=1,nel
  .Generate the matrix elements for the corresponding finite element
  and store the result in 'a1' and 'b1'. 'tab' is a pointer array
  which stores the node combinations and local and global edge nos.
  call crux(i,a1,b1,tab)
  do ij=1,6
    bit(ij)='0'
  enddo
  .Run a check for the on-surface edges in the corresponding finite
  element. The character array 'bit' sets a flag for each on-surface
  edge in the finite element.
  do 100 j=1,6
    do ichk=1,nes
  .If the element edge is an on-surface edge, set bit(i) ='1'
      if (tab(j,3).eq.sed(ichk)) then
        bit(j)='1'
        go to 100
      endif
    enddo
  enddo
  .If bit(i)='1', forget it. If bit(i)='0', check to see whether
  the edge has occurred previously; if not, increment 'nptrx' and
  store the new edge no. and corresponding old edge no. in 'edst'
  do j=1,6
    if (bit(j).eq.'0') then
      if (edst(tab(j,3),2).ne.tab(j,3)) then
        edst(tab(j,3),1)=nptrx
        edst(tab(j,3),2)=tab(j,3)
        nptrx=nptrx+1
      endif
    endif
  enddo
  .Only the edges inside the body are stored in the final array,
  'a' and 'b'.
  do j=1,6
    do k=1,6
      if ((bit(j).eq.'0').and.(bit(k).eq.'0')) then
        a(edst(tab(j,3),1),edst(tab(k,3),1))=
1 a(edst(tab(j,3),1),edst(tab(k,3),1))+dble(a1(j,k))
        b(edst(tab(j,3),1),edst(tab(k,3),1))=
1 b(edst(tab(j,3),1),edst(tab(k,3),1))+dble(b1(j,k))
      endif
    enddo
  enddo
enddo
write(6,*)'Finished FEM matrix generation'
write(6,*)'Matrix is of order ',nptrx-1

```

```

if (net.ne.(nptrx-1)) then
  write(6,*)'Error in matrix assembly'
  stop
endif
ir=0
do i=1,nptrx-1
  do j=1,nptrx-1
    if ((b(i,j)-b(j,i)).gt..000001) then
      write(6,*)b(i,j),b(j,i),i,j
      ir=1
    endif
  enddo
enddo
if (ir.eq.0) then
  write(6,*)'Symmetry test passed'
else
  write(6,*)'Symmetry test failed'
endif

```

Solving the generalised eigenvalue problem:  $Ax = \lambda Bx$

```

eps1=.000001
matz=.false.
call qzhes(700,net,a,b,matz,z)
write(6,*)'Step 1 done'
call qzit(700,net,a,b,eps1,matz,z,ier)
write(6,*)'Step 2 done'
write(6,*)'error= ',ier
call qzval(700,net,a,b,alfr,alfr,beta,matz,z)
write(6,*)'Step 3 done'
do i=1,nptrx-1
  alfr(i)=alfr(i)/beta(i)
enddo

```

A bubble sort through the eigenvalue spectrum

```

do i=1,net-1
  do j=net,i+1,-1
    if (alfr(j).lt.alfr(j-1)) then
      beta(j)=alfr(j)
      alfr(j)=alfr(j-1)
      alfr(j-1)=beta(j)
    endif
  enddo
  if (alfr(i).ge.0.) then
    write(4,*)sqrt(alfr(i))
  endif
enddo
close(4)
stop
end

```

```

=====
subroutine crux(1,a,b,tab)
integer edna(15000),gnn(15000,2),tab(6,3),mat(2500)
real xyz(3000,3),x(500),y(500),z(500),a(6,6),b(6,6),f(6,3),
1   g(6,3),tmp(3),eps(10)
common /bank/edna,gnn,xyz,eps,mat
common /mess/x,y,z
common /local/sumx,sumy,sumz,xx,yy,zz,xy,yz,zx
lv=6*(1-1)
do j=1,6
  tab(j,1)=gnn(lv+j,1)
  tab(j,2)=gnn(lv+j,2)

```

```

    tab(j,3)=edna(lv+j)
  enddo
.Sorting the array 'tab' arranges it according to local node nos. so
that the array looks like the one in file 'input'.
  call sort(tab)
.'calc' calculates some data corresponding to the element
  call calc(tab(1,1),tab(1,2),tab(2,2),tab(3,2))
.'volume' computes six times the volume of the tetrahedral element
  call volume(tab(1,3),tab(2,3),tab(3,3),vol)
  do j=1,6
    call cross(x(tab(7-j,1)),y(tab(7-j,1)),z(tab(7-j,1)),x(tab(
1      7-j,2)),y(tab(7-j,2)),z(tab(7-j,2)),tmp)
.'bj' stores the length of the 'j' th edge.
  bj=sqrt((xyz(tab(j,3),1)**2)+(xyz(tab(j,3),2)**2)+(xyz
1      (tab(j,3),3)**2))
.The constant vectors, 'f' and 'g', are computed and the result
stored in 'f' and 'g', respectively.
  do k=1,3
    f(j,k)=bj*tmp(k)/vol
    g(j,k)=bj*xyz(tab(7-j,3),k)/vol
    if (j.eq.2) then
      g(j,k)=-1.*g(j,k)
    elseif (j.eq.5) then
      f(j,k)=-1.*f(j,k)
      g(j,k)=-1.*g(j,k)
    endif
  enddo
enddo
vol=vol/6.
  do j=1,6
    do k=1,6
.'a' contains the elemnts of the 'a' matrix in the main program.
This equals the volume integral over curl W_i . curl W_j and
is the same as 4.*g_i*g_j*v
  a(j,k)=4.*dot(j,k,g)*vol
.The function 'fl' computes the elements of the 'b' matrix in the
main program. This is taken directly from the formulation and
equals the volume integral over W_i . W_j
  b(j,k)=fl(j,k,f,g)*eps(mat(1))*vol
  enddo
enddo
return
end

```

```

=====
subroutine sort(tab)
integer tab(6,3)
nc=1
do ik=4,2,-1
  if (nc.eq.1) then
    ij=6
  else
    ij=ik
  endif
  do ii=1,ij-1
    do j=ij,ii+1,-1
      if (tab(j,nc).lt.tab(j-1,nc)) then
        do jk=1,3
          call exchg(tab(j,jk),tab(j-1,jk))
        enddo
      endif
    enddo
  enddo

```

```
endif
enddo
enddo
nc=2
enddo
if (tab(5,2).lt.tab(4,2)) then
do jk=1,3
call exchg(tab(5,jk),tab(4,jk))
enddo
endif
call exchg(tab(5,1),tab(5,2))
return
end
```

```
=====
subroutine volume(j1,j2,j3,v)
integer edna(15000),gnn(15000,2),mat(2500)
real xyz(3000,3),b1(3),b2(3),b3(3),eps(10)
common /bank/edna,gnn,xyz,eps,mat
do it=1,3
b1(it)=xyz(j1,it)
b2(it)=xyz(j2,it)
b3(it)=xyz(j3,it)
enddo
v=abs(b1(1)*((b2(2)*b3(3))-(b2(3)*b3(2)))-b1(2)*((b2(1)*b3
1 (3))-(b2(3)*b3(1)))+b1(3)*((b2(1)*b3(2))-(b2(2)*b3(1))))
return
end
```

```
=====
subroutine cross(x1,y1,z1,x2,y2,z2,tempo)
real tempo(3)
tempo(1)=y1*z2-y2*z1
tempo(2)=z1*x2-z2*x1
tempo(3)=x1*y2-x2*y1
return
end
```

```
=====
subroutine calc(j1,j2,j3,j4)
real x(500),y(500),z(500)
common /mess/x,y,z
common /local/sumx,sumy,sumz,xx,yy,zz,xy,yz,zx
sumx=x(j1)+x(j2)+x(j3)+x(j4)
sumy=y(j1)+y(j2)+y(j3)+y(j4)
sumz=z(j1)+z(j2)+z(j3)+z(j4)
xx=sumx*sumx+x(j1)*x(j1)+x(j2)*x(j2)+x(j3)*x(j3)+x(j4)*x(j4)
yy=sumy*sumy+y(j1)*y(j1)+y(j2)*y(j2)+y(j3)*y(j3)+y(j4)*y(j4)
zz=sumz*sumz+z(j1)*z(j1)+z(j2)*z(j2)+z(j3)*z(j3)+z(j4)*z(j4)
xy=sumx*sumy+x(j1)*y(j1)+x(j2)*y(j2)+x(j3)*y(j3)+x(j4)*y(j4)
yz=sumy*sumz+y(j1)*z(j1)+y(j2)*z(j2)+y(j3)*z(j3)+y(j4)*z(j4)
zx=sumz*sumx+z(j1)*x(j1)+z(j2)*x(j2)+z(j3)*x(j3)+z(j4)*x(j4)
return
end
```

```
=====
real function dot(j1,j2,vec)
real vec(6,3)
dot=(vec(j1,1)*vec(j2,1))+vec(j1,2)*vec(j2,2))+vec(j1,3)*vec
1 (j2,3))
return
end
=====
```

```
real function f1(j1,j2,f,g)
real f(6,3),g(6,3),tmp1(3),tmp2(3)
common /local/sumx,sumy,sumz,xx,yy,zz,xy,yz,zx
call cross(f(j1,1),f(j1,2),f(j1,3),g(j2,1),g(j2,2),g(j2,3),tmp1)
call cross(f(j2,1),f(j2,2),f(j2,3),g(j1,1),g(j1,2),g(j1,3),tmp2)
term1=dot(j1,j2,f)
term2=((tmp1(1)+tmp2(1))*sumx+(tmp1(2)+tmp2(2))*sumy+
1      (tmp1(3)+tmp2(3))*sumz)/4.
term3=(g(j1,2)*g(j2,2)+g(j1,3)*g(j2,3))*xx+(g(j1,1)*g(j2,1)+
1      g(j1,3)*g(j2,3))*yy+(g(j1,1)*g(j2,1)+g(j1,2)*g(j2,2))*zz
2      -(g(j1,1)*g(j2,2)+g(j1,2)*g(j2,1))*xy-(g(j1,1)*g(j2,3)+
3      g(j1,3)*g(j2,1))*zx-(g(j1,2)*g(j2,3)+g(j1,3)*g(j2,2))*yz
f1=term1+term2+(term3/20.)
return
end
```

```
=====
subroutine exchg(j1,j2)
ntmp=j1
j1=j2
j2=ntmp
return
end
```

=====  
 Processes a universal file obtained from IDEAS and stores the nodal info.  
 Checks the surface nodes and imposes suitable boundary conditions on them.

Stores the node numbers and respective nodal coordinates in 'noddy'  
 Stores the element numbers and corresponding nodes in 'elno'  
 Storage limit: 4000 nodes, 25000 elements  
 =====

```

program unv_file_processor
character string*80, yastrn*40, unv*20
integer nl(25000,4),nn(50),nun(25000),bc(25000,3)
integer count,tr(25000),tmp
real x(4000),y(4000),z(4000)
write(6,*)'1) Cavity problem 2) Scattering problem'
read(5,*)ivar
write(6,*)'Name of universal file ?'
read(5,'(A)')unv
open(1,file=unv)
open(2,file='noddy')
open(3,file='elno')
open(8,file='surfed')
Processing universal file for info on various parameters
read(1,'(A)')string
l=0
if (string(4:6).eq.'151') then
  write(6,*)'Encountered header'
  go to 15
Processing nodal info; data stored in 'noddy'
elseif (string(4:6).eq.' 15') then
  read(1,'(A)')string
  if (string(5:6).ne.'-1') then
    write(2,*)string(7:10),' ',string(41:53),' ',string(54:66),' '
1      ,string(67:79)
    l=l+1
    go to 5
  endif
  ll=1
  write(6,*)'There are ',l,' nodes.'
  write(8,*)l
Processing element info; data stored in 'elno'
elseif (string(4:6).eq.' 71') then
  read(1,'(A)')string
  if (string(5:6).ne.'-1') then
    read(1,'(A)')yastrn
    write(3,*)string(7:10),' ',yastrn(7:10),' ',yastrn(17:20),
1      ' ',yastrn(27:30),' ',yastrn(37:40)
    l=l+1
    go to 10
  else
    write(6,*)'There are ',l,' elements.'
    write(8,*)l
    l2=1
  endif
elseif (string(4:6).eq.'752') then
  ltmp=0
  nn(1)=0
  read(1,'(A)')string
  if (string(19:20).eq.' 0') then
    ltmp=ltmp+1

```

```

      read(string(57:60),'(I4)')numb
      nn(ltmp+1)=numb+nn(ltmp)
    elseif (string(5:6).eq.'-1') then
      write(6,*)'There are ',ltmp,' surface divisions.'
      go to 20
    elseif (string(1:1).eq.' ') then
      do i=1,4
        if (string((20*i-3):20*i).ne.' ') then
          l=l+1
          read(string((20*i-3):20*i),'(I4)')tr(l)
        endif
      enddo
    endif
    go to 30
  endif
  go to 15
close(1)
.Data from 'noddy' and 'elno' stored in
n1,...,n4   - table of nodes making up the corresponding element
x,y,z      - nodal coordinate table
rewind 2
rewind 3
do i=1,11
  read(2,*)na,x(i),y(i),z(i)
enddo
do i=1,12
  read(3,*)nk,n1(i,1),n1(i,2),n1(i,3),n1(i,4)
enddo
.Close 'noddy' and 'elno' for good
close(2)
ncnt=0
do i=1,12
  do j=1,3
    bc(i,j)=0
  enddo
enddo
if (ivar.eq.1) then
  do i=1,ltmp
    write(6,*)'Processing surface ',i,' for on-surface nodes.'
    do j=nn(i)+2,nn(i+1)
      if (x(tr(nn(i)+1)).eq.x(tr(j))) then
        flagx=0.
      else
        flagx=1.
      endif
      if (y(tr(nn(i)+1)).eq.y(tr(j))) then
        flagy=0.
      else
        flagy=1.
      endif
      if (z(tr(nn(i)+1)).eq.z(tr(j))) then
        flagz=0.
      else
        flagz=1.
      endif
    enddo
    do k=nn(i)+1,nn(i+1)
      if (flagx.eq.0.) then
        bc(k,1)=1

```

```

    elseif (flagy.eq.0.) then
      bc(k,2)=1
    elseif (flagz.eq.0.) then
      bc(k,3)=1
    endif
  enddo
enddo
do i=1,1-1
  do j=1,i+1,-1
    if (tr(j).lt.tr(j-1)) then
      call exchg(tr(j),tr(j-1))
      do k=1,3
        call exchg(bc(j,k),bc(j-1,k))
      enddo
    endif
  enddo
enddo
nuk=0.
do i=1,1
  if (i.eq.1) then
    tmp=0
  else
    tmp=tr(i-1)
  endif
  if (tr(i).ne.tmp) then
    count=1
    if (tr(i+count).eq.tr(i)) then
      count=count+1
      go to 50
    endif
    nt1=1
    nt2=1
    nt3=1
    do j=1,count
      nt1=nt1*bc(i+j-1,1)
      nt2=nt2*bc(i+j-1,2)
      nt3=nt3*bc(i+j-1,3)
    enddo
    write(8,*)tr(i),nt1,nt2,nt3
    ncnt=ncnt+1
    nuk=nuk+(1-nt1)+(1-nt2)+(1-nt3)
  else
    go to 100
  endif
enddo
write(6,*)'No. of on-surface nodes = ',ncnt
write(6,*)'No. of unknowns = ',3*11-nuk
else
  do i=1,ltmp
    write(8,*)i,nn(i+1)
  enddo
  do ii=1,ltmp
    do ik=1,12
      nun(ik)=0
    enddo
    do i=nn(ii)+1,nn(ii+1)
      do j=1,12
        do k=1,4
          if (tr(i).eq.n1(j,k)) then

```

```
      nun(j)=nun(j)+1
      bc(j,nun(j))=n1(j,k)
      if (nun(j).eq.3) then
        write(8,*)j,bc(j,1),bc(j,2),bc(j,3)
        ncnt=ncnt+1
        go to 200
      endif
    endif
  enddo
enddo
enddo
enddo
write(6,*)'There are ',ncnt,' surface elements.'
endif
close(3)
close(8)
stop
end
```

```
=====
subroutine exchg(j1,j2)
  ntmp=j1
  j1=j2
  j2=ntmp
  return
end
```

```
=====
This program computes the eigenvalues of a rectangular cavity
using divergenceless nodal basis and tetrahedral elements.
Storage limit: 500 nodes, 2000 elements, 300 surface nodes
                1500 matrix size
```

```
To run program on Apollos:
```

```
Need to run 'procn.obj' first; 'noddy', 'elno' and 'surfed' are created.
```

```
ftn 'filename'
```

```
bind 'filename'.bin /progs/math/naas/eispack.lib -b 'filename'.obj
```

```
'filename'.obj
=====
```

```
program fem_nodal_basis_3d
logical matz
integer elm(2000,4),surf(300),bc(300,3),tab(4)
real a1(12,4),b1(12,4),x(500),y(500),z(500)
double precision a(1500,1500),b(1500,1500),alfr(1500),alfi(1500)
1      ,beta(1500)
common /dbase/x,y,z,elm
common /var/s,vol
write(6,*)'No. of on-surface nodes'
read(5,*)nsn
write(6,*)'Penalty factor'
read(5,*)s
open(1,file='noddy')
open(2,file='elno')
open(3,file='surfed')
open(4,file='eig')
read(3,*)nn
nn2=2*nn
read(3,*)ne
do i=1,nn
  read(1,*)nk,x(i),y(i),z(i)
enddo
do i=1,ne
  read(2,*)nk,elm(i,1),elm(i,2),elm(i,3),elm(i,4)
enddo
do i=1,nsn
  read(3,*)surf(i),bc(i,1),bc(i,2),bc(i,3)
enddo
write(6,*)'Finished reading in data'
close(1)
close(2)
close(3)
```

```
=====
do iv=1,3
  do i=1,ne
    call crux(i,iv,a1,b1,tab)
    do j=1,12
      do k=1,4
        nt=(iv-1)*nn
        if (j.le.4) then
a(tab(j),(nt+tab(k)))=a(tab(j),(nt+tab(k)))+dble(a1(j,k))
b(tab(j),(nt+tab(k)))=b(tab(j),(nt+tab(k)))+dble(b1(j,k))
          elseif ((j.gt.4).and.(j.le.8)) then
a((nn+tab(j-4)),(nt+tab(k)))=a((nn+tab(j-4)),(nt+tab(k)))
1      +dble(a1(j,k))
b((nn+tab(j-4)),(nt+tab(k)))=b((nn+tab(j-4)),(nt+tab(k)))
1      +dble(b1(j,k))
        else
```

```

a((nn2+tab(j-8)),(nt+tab(k)))=a((nn2+tab(j-8)),(nt+tab(k)))
1 +dble(a1(j,k))
b((nn2+tab(j-8)),(nt+tab(k)))=b((nn2+tab(j-8)),(nt+tab(k)))
1 +dble(b1(j,k))
    endif
    enddo
    enddo
    enddo
enddo

```

```

=====
write(6,*)'Applying bc'
do j=1,nsn
  if (bc(j,1).eq.0) then
    a(surf(j),surf(j))=-1.d0
  endif
  if (bc(j,2).eq.0) then
    a(nn+surf(j),nn+surf(j))=-1.d0
  endif
  if (bc(j,3).eq.0) then
    a(nn2+surf(j),nn2+surf(j))=-1.d0
  endif
enddo
write(6,*)'shifting rows'
nptr=3*nn+1
do j=1,(3*nn)
  if (float(j/15).eq.(j/15.)) then
    write(6,*)j,nptr
  endif
  if (a(j,j).eq.-1.d0) then
    nptr=nptr-1
    if (j.gt.nptr) go to 30
    if (a(nptr,nptr).ne.-1.d0) then
      do k=1,nptr
        call exchg(a(j,k),a(nptr,k))
        call exchg(b(j,k),b(nptr,k))
      enddo
      do k=1,nptr
        call exchg(a(k,j),a(k,nptr))
        call exchg(b(k,j),b(k,nptr))
      enddo
    else
      go to 20
    endif
  endif
enddo

```

```

=====
ir=0
write(6,*)'Matrix generation complete; matrix of order ',nptr
do i=1,nptr
  do j=1,nptr
    if ((a(i,j)-a(j,i)).gt..000001) then
      ir=1
      write(6,*)a(i,j),a(j,i),j,i
    endif
  enddo
enddo
if (ir.eq.1) then
  write(6,*)'Symmetry test failed for A'
else

```

```

write(6,*)'Symmetry test passed for A'
endif

```

```

=====
eps1=.00001
matz=.false.
call qzhes(1500,nptr,a,b,matz,z)
write(6,*)'Step 1 done'
call qzit(1500,nptr,a,b,eps1,matz,z,ier)
write(6,*)'Step 2 done'
write(6,*)'error= ',ier
if (ier.ne.0) then
  write(6,*)'Erroneous computation; check FE matrices'
  stop
endif
call qzval(1500,nptr,a,b,alfr,alfr,beta,matz,z)
write(6,*)'Step 3 done'
do i=1,nptr
  alfr(i)=alfr(i)/beta(i)
enddo
do i=1,nptr-1
  do j=nptr,i+1,-1
    if (alfr(j).lt.alfr(j-1)) then
      beta(j)=alfr(j)
      alfr(j)=alfr(j-1)
      alfr(j-1)=beta(j)
    endif
  enddo
  if (alfr(i).gt.0.) then
    write(4,*)sqrt(alfr(i))
  endif
enddo
close(4)
stop
end

```

```

=====
subroutine crux(1,iv,a,b,tab)
integer elm(2000,4),tab(4)
real a(12,4),b(12,4),x(500),y(500),z(500)
common /dbase/x,y,z,elm
common /var/s,vol
do j=1,4
  tab(j)=elm(1,j)
enddo
call calc(iv,tab(1),tab(2),tab(3),tab(4))
call volume(tab(1),tab(2),tab(3),tab(4),vol)
do j=1,12
  do k=1,4
    call matx(iv,j,k,a(j,k),b(j,k))
  enddo
enddo
return
end

```

```

=====
subroutine volume(j1,j2,j3,j4,v)
integer elm(2000,4)
real x(500),y(500),z(500)
common /dbase/x,y,z,elm
v1=(x(j1)-x(j4))*(y(j2)-y(j4))*(z(j3)-z(j4))-(y(j3)-y(j4))*(z(j
1)
2)-z(j4)))

```

```

v2=(y(j4)-y(j1))*((x(j2)-x(j4))*(z(j3)-z(j4))-(x(j3)-x(j4))*(z(j
1  2)-z(j4)))
v3=(z(j1)-z(j4))*((x(j2)-x(j4))*(y(j3)-y(j4))-(x(j3)-x(j4))*(y(j
1  2)-y(j4)))
v=abs(v1+v2+v3)/6.
return
end

```

```

=====
subroutine calc(iv,j1,j2,j3,j4)
integer elm(2000,4)
real x(500),y(500),z(500),p(4),q(4),r(4)
common /dbase/x,y,z,elm
common /local/p,q,r
p(1)=(y(j2)-y(j4))*(z(j3)-z(j4))-(y(j3)-y(j4))*(z(j2)-z(j4))
p(2)=(y(j3)-y(j4))*(z(j1)-z(j4))-(y(j1)-y(j4))*(z(j3)-z(j4))
p(3)=(y(j1)-y(j4))*(z(j2)-z(j4))-(y(j2)-y(j4))*(z(j1)-z(j4))
p(4)=(y(j3)-y(j1))*(z(j2)-z(j1))-(y(j2)-y(j1))*(z(j3)-z(j1))
q(1)=(z(j2)-z(j4))*(x(j3)-x(j4))-(z(j3)-z(j4))*(x(j2)-x(j4))
q(2)=(z(j3)-z(j4))*(x(j1)-x(j4))-(z(j1)-z(j4))*(x(j3)-x(j4))
q(3)=(z(j1)-z(j4))*(x(j2)-x(j4))-(z(j2)-z(j4))*(x(j1)-x(j4))
q(4)=(z(j3)-z(j1))*(x(j2)-x(j1))-(z(j2)-z(j1))*(x(j3)-x(j1))
r(1)=(y(j3)-y(j4))*(x(j2)-x(j4))-(y(j2)-y(j4))*(x(j3)-x(j4))
r(2)=(y(j1)-y(j4))*(x(j3)-x(j4))-(y(j3)-y(j4))*(x(j1)-x(j4))
r(3)=(y(j2)-y(j4))*(x(j1)-x(j4))-(y(j1)-y(j4))*(x(j2)-x(j4))
r(4)=(y(j2)-y(j1))*(x(j3)-x(j1))-(y(j3)-y(j1))*(x(j2)-x(j1))

```

Checking routine follows; can be deleted if the user feels confident enough of the matrix generation process

```

t1=0.
t2=0.
t3=0.
do ijk=1,4
  t1=t1+p(ijk)
  t2=t2+q(ijk)
  t3=t3+r(ijk)
enddo
if (t1.gt..000001) then
  write(6,*)t1,t2,t3
endif
return
end

```

```

=====
subroutine matx(m,j,k,fa,fb)
real p(4),q(4),r(4)
common /local/p,q,r
common /var/s,vol
tt=0.
if (m.eq.1) then
  if (j.le.4) then
    t=(s*p(j)*p(k))+q(j)*q(k))+r(j)*r(k))
    if (j.ne.k) then
      tt=.05
    else
      tt=.1
    endif
  elseif ((j.gt.4).and.(j.le.8)) then
    jj=j-4
    t=(s*q(jj)*p(k))-p(jj)*q(k))
  else
    jj=j-8

```

```
      t=(s*r(jj)*p(k))-p(jj)*r(k)
    endif
  elseif (m.eq.2) then
    if (j.le.4) then
      t=(s*p(j)*q(k))-q(j)*p(k)
    elseif ((j.gt.4).and.(j.le.8)) then
      jj=j-4
      t=(p(jj)*p(k))+s*q(jj)*q(k)+r(jj)*r(k)
      if (jj.ne.k) then
        tt=.05
      else
        tt=.1
      endif
    else
      jj=j-8
      t=(s*r(jj)*q(k))-q(jj)*r(k)
    endif
  else
    if (j.le.4) then
      t=(s*p(j)*r(k))-r(j)*p(k)
    elseif ((j.gt.4).and.(j.le.8)) then
      jj=j-4
      t=(s*q(jj)*r(k))-r(jj)*q(k)
    else
      jj=j-8
      t=(p(jj)*p(k))+q(jj)*q(k)+s*r(jj)*r(k)
      if (jj.ne.k) then
        tt=.05
      else
        tt=.1
      endif
    endif
  endif
endif
fa=t/(36.*vol)
fb=tt*vol
return
end
```

---

```
subroutine exchg(x1,x2)
  tmp=x1
  x1=x2
  x2=tmp
  return
end
```