Minimization of Deviations of Gear Real Tooth Surfaces Determined by Coordinate Measurements

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MINIMIZATION OF DEVIATIONS OF GEAR REAL TOOTH SURFACES DETERMINED BY COORDINATE MEASUREMENTS

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ABSTRACT

The deviations of a gear's real tooth surface from the theoretical surface are determined by coordinate measurements at the grid of the surface. A method has been developed to transform the deviations from Cartesian coordinates to those along the normal at the measurement locations. Equations are derived that relate the first order deviations with the adjustment to the manufacturing machine-tool settings. The deviations of the entire surface are minimized. The minimization is achieved by application of the least-square method for an overdetermined system of linear equations. The proposed method is illustrated with a numerical example for hypoid gear and pinion.

INTRODUCTION

Coordinate measurements of gear tooth surfaces coupled with the ability to correct the initially applied machine-tool settings is becoming a significant part of advanced gear technology. We may consider two stages of this technique:

(i) Application of coordinate measurements of the manufactured gears for numerical determination, in 3D space, of deviations of real tooth surfaces.

(ii) The goal of minimization of deviations can be achieved by proper corrections of initially applied machine-tool settings. The determination of corrected machine-tool settings is found numerically.

The technological aspects of the problem to-be discussed are as follows:

(i) The deviations of real tooth surfaces are inevitable due to surface distortion by heat-treatment, errors of initial machine-tool settings, deflection by manufacturing, etc.

(ii) Application of an additional finishing operation for elimination of the deviations would be too expensive in comparison with the approach based on corrections of initially applied machine-tool settings. The advantage of this approach is the possibility of using the same equipment to correct the deviations.

The disadvantage is that the approach will be successful only if the deviations are repeatable.

(iii) The coordinate measurements must be performed with high precision, which currently prohibits them from being performed simultaneously with the manufacturing. Therefore, the coordinate measurements are performed after manufacturing, but only the first gear of the whole gear set to-be manufactured is tested.

(iv) In some cases master-gears are used and the coordinate measurements provide the information about the deviations from the master-surface for the surface being tested. The authors consider this approach less effective as compared to computerized determination of surface deviations and corrections of machine-tool settings.

The mathematical solutions to this problem are represented in the Appendix to this paper. The technique described in the paper has been developed in the response to the increasing requirements of high quality gear transmissions. Minimizing the deviations of real tooth surfaces results in a reduction in the level of transmission errors that cause gear noise and vibration.

The proposed approach is applied to hypoid gear drives that have found a wide application in transmissions [1,2]. The contents of the paper are complemented with a numerical example for a hypoid pinion and gear to illustrate the effectiveness of the proposed approach. The level of deviations of the pinion surface has been reduced from 30 microns to the theoretical level of 2-3 microns.

1. OVERVIEW OF MEASUREMENT AND MODELING METHOD

The approach developed in this paper enables the determination of deviations of a real surface from the known theoretical surface. This is accomplished by two steps: (i) coordinate measurements for determination of surface deviations and (ii) minimization of the deviations through correction of the previously applied machine-tool settings.
The surface deviations obtained initially in Cartesian coordinates are transformed into deviations along the normal to the theoretical surface. The coordinate measurements are performed by a machine with four or five degrees-of-freedom. In the case of four degrees-of-freedom, the probe performs three translational motions (fig. 1); the fourth motion, rotation, is performed by a rotary table. The axis of rotational motion coincides with the axis of the workpiece. In the case of a five degree-of-freedom machine, the fifth degree of freedom is used to provide the deflections of the probe in the direction of the normal to the theoretical surface. The probe is provided with a changeable spherical surface whose diameter can be chosen from a wide range.

The motions of the probe and the workpiece by coordinate measurements are computer controlled and therefore a grid comprising of the set of surface points to be measured must be chosen (fig. 2). There is a reference point on the grid that is necessary for the initial installments of the probe. There are two orientations of the probe installment that are used to measure a gear (fig. 1(a)) and a pinion (fig. 1(b)), depending on the angle of the pitch cone.

The mathematical aspects of coordinate measurements will now be described [2]: First, it is necessary to derive the equations of the theoretical surface. In many cases this surface can be derived as the envelope to the family of generating surfaces, namely the tool surfaces. Next, the results of coordinate measurements must be transformed into deviations of the real surface represented in the direction of the surface normal. Then, the relations between the surface variations and the corrections to the machine-tool settings must be determined. The surface deviations obtained from coordinate measurements and the surface variations determined by the corrections of machine-tool settings can be represented by an overdetermined system of linear equations. The number of these equations, k, is equal to the number of points of the grid, and the number of unknowns, m, is equal to the number of corrections of machine-tool settings (m << k). The optimal solution to such a system of linear equations results in the determination of the machine-tool setting corrections.

2. EQUATIONS OF THEORETICAL TOOTH SURFACE Σₜ

Considering that the theoretical surface can be determined directly, we represent it in coordinate system Sc in two parametric form as:

\[ r(t, \theta), \quad n(t, \theta) \]  

Here: \( r(t, \theta) \) and \( n(t, \theta) \) are the position-vector and the surface unit normal, respectively; \((u, \theta)\) are the Gaussian coordinates (surface coordinates).

For the case when surface \( \Sigmaₜ \) is the envelope to the family of generating surface \( \Sigma_c \), we represent surface \( \Sigma_c \) and the unit normal \( n_c \) to \( \Sigma_c \) in \( S_c \) as [3]

\[ r_c(u_c, \theta_c), \quad f(u_c, \theta_c, \phi) = 0 \]  

\[ n_c = L_{cc} n_c(u_c, \theta_c), \quad f(u_c, \theta_c, \phi) = 0 \]  

Here: \((u_c, \theta_c)\) are the Gaussian coordinates of the generating surface \( \Sigma_c \); \( \phi \) is the generalized parameter of motion in the process for generation. The equation of meshing is given by:

\[ f(u_c, \theta_c, \phi) = N^{(c)} \cdot \nu^{(c)} = 0 \]  

where \( N^{(c)} \) is the normal to \( \Sigma_c \); \( \nu^{(c)} \) is the relative motion for a point of contact of \( \Sigma_c \) and \( \Sigma_t \). The 4 × 4 matrix \( M_{tc} \) and 3 × 3 matrix \( L_{cc} \) describe the coordinate transformation from \( S_c \) to \( S_t \) of a position vector and surface unit normal, respectively. Position vectors in 3-D space are represented with homogeneous coordinates.

3. COORDINATE SYSTEMS USED FOR COORDINATE MEASUREMENTS

Coordinate systems \( S_m \) and \( S_t \) are rigidly connected to the coordinate measuring machine (CMM) and the workpiece being measured, respectively (fig. 3). The back face of the gear is installed flush with the base plane of the CMM. The distance \( l \) between the origins \( O_m \) and \( O_t \) is known but the parameter of orientation \( \delta \) must be determined (see section 4). The coordi-
nate transformation from \( S_i \) to \( S_m \) is represented by the matrix equation

\[
      r_m = M_{m1} r_i
\]  

(5)

\[
    O_m \quad M \quad r_m \quad x_m \quad y_m \quad z_m
\]

Fig. 3. Coordinate Transformation.

4. GRID AND REFERENCE POINT

The grid is a set of points on \( \Sigma_i \) chosen as points of contact between the probe and \( \Sigma_i \) (fig. 3). Fixing the value of \( z_i \) for the point of the grid, and the value of, say \( y_i \) (or \( x_i \)), we can obtain the following equations

\[
y_i(u_i, \theta_i) = h_i, \quad z_i(u_i, \theta_i) = l_i \quad (i = 1, \ldots, k)
\]

(6)

where \( k \) is the number of grid points.

We consider \( h_i \) and \( l_i \) as given and solve equations (6) for \((u_i, \theta_i)\). Then we can determine the position vectors and the unit normals for \( k \) points of the grid using the equations

\[
r_i^{(i)} = [x_i(u_i, \theta_i) \quad y_i(u_i, \theta_i) \quad z_i(u_i, \theta_i)]^T, \quad (i = 1, \ldots, k)
\]

(7)

\[
n_i^{(i)} = [n_{x_i}(u_i, \theta_i) \quad n_{y_i}(u_i, \theta_i) \quad n_{z_i}(u_i, \theta_i)]^T, \quad (i = 1, \ldots, k)
\]

(8)

The position vector for the center of the probe, if the deviations are zero, is represented by the equation

\[
    R_{c}^{(i)} = r_{c}^{(i)} + \rho n_{c}^{(i)} \quad (i = 1, \ldots, k)
\]

(9)

where \( \rho \) is the radius of the probe tip.

The reference point

\[
r_{c}^{(i)} = [x_{c}(u^{(0)}, \theta^{(0)}) \quad y_{c}(u^{(0)}, \theta^{(0)}) \quad z_{c}(u^{(0)}, \theta^{(0)})]^T
\]

(10)

is usually chosen as the mean point of the grid.

The center of the probe that corresponds the reference point on \( \Sigma_i \) is determined from equation (9) as

\[
    R_{c}^{(i)} = [X_{c}(u^{(0)}, \theta^{(0)}) \quad Y_{c}(u^{(0)}, \theta^{(0)}) \quad Z_{c}(u^{(0)}, \theta^{(0)})]^T
\]

(11)

Here: \((u^{(0)}, \theta^{(0)})\) are known values.

The coordinates of the reference center of the probe are represented in coordinate system \( S_m \) of the measuring machine by the matrix equation

\[
    \begin{bmatrix}
    x_m^{(0)} \\
    y_m^{(0)} \\
    z_m^{(0)}
    \end{bmatrix} = M_{m1}(\delta) \begin{bmatrix}
    x_c^{(0)} \\
    y_c^{(0)} \\
    z_c^{(0)}
    \end{bmatrix}
\]

(12)

Equation (12) yields

\[
    \begin{bmatrix}
    x_m^{(0)} \\
    y_m^{(0)} \\
    z_m^{(0)}
    \end{bmatrix} = \begin{bmatrix}
    x_c^{(0)}(\delta, u^{(0)}, \theta^{(0)}) \\
    y_c^{(0)}(\delta, u^{(0)}, \theta^{(0)}) \\
    z_c^{(0)}(\delta, u^{(0)}, \theta^{(0)})
    \end{bmatrix}
\]

(13)

The three equations (13) contain four unknowns: \( \delta, x_m^{(0)}, y_m^{(0)}, z_m^{(0)} \). To solve these equations we may consider that one of the coordinates of the reference point of the probe center, say \( y_m^{(0)} \), may be chosen equal to zero. Then the system of equations (13) allows the determination of \( \delta, x_m^{(0)} \) and \( z_m^{(0)} \) [2]. Coordinates \( x_m^{(0)}, y_m^{(0)} = 0, z_m^{(0)} \) are necessary for the initial installment of the center of the probe.

5. DEVIATIONS OF THE REAL SURFACE

The deviations of the real surface are caused by errors of manufacturing, heat treatment, etc. Vector positions of the center for the theoretical surface and the real surface can be represented as follow

\[
    R_m = r_m(u, \theta) + \rho n_m(u, \theta)
\]

(14)

\[
    R_m^* = r_m(u, \theta) + \lambda n_m(u, \theta)
\]

(15)

Here: \( r_m \) and \( n_m \) are the position vector and the unit normal to the theoretical surface, respectively, that are represented in coordinate system \( S_m \) of the measuring machine; \( \lambda \) determines the real location of the probe center and is considered along the normal to the theoretical surface; \( R_m \) and \( R_m^* \) represent in \( S_m \) the position vector of the probe center for the theoretical and real surfaces, respectively. Equations (14) and (15) yield

\[
    R_m^* - R_m = (\lambda - \rho)n_m = \Delta n_m
\]

(16)

and

\[
    \Delta n = (R_m^* - R_m) \cdot n_m
\]

(17)

The position vector \( R_m^* \) is determined by coordinate measurements for points of the grid. Equation (17) determines numerically the function:

\[
    \Delta n_i = \Delta n_i(u_i, \theta_i) \quad (i = 1, \ldots, k)
\]

(18)

that represents the deviations of the real surface for each point of the grid.

6. MINIMIZATION OF DEVIATIONS

The procedure of minimization of deviations can be repre-
sented in two stages: (i) determination of variations of theoretical surface caused by changes of applied machine-tool settings, and (ii) minimization of deviations of real surface by appropriate correction of machine-tool settings.

We consider that the theoretical surface is represented in $S_r$ as

$$r_i = r_i(u, \theta, d_j) \quad (j = 1, \ldots, m)$$

where parameters $d_j$ are the machine-tool settings.

The surface variations are represented by

$$\delta r_i = \frac{\partial r_i}{\partial u} \delta u + \frac{\partial r_i}{\partial \theta} \delta \theta + \sum_{j=1}^{m} \frac{\partial r_i}{\partial d_j} \delta d_j$$

We multiply both sides of equation (20) by the surface unit normal $n_t$ and take into account that $\frac{\partial r_i}{\partial u} \cdot n_t = \frac{\partial r_i}{\partial \theta} \cdot n_t = 0$ since $\frac{\partial r_i}{\partial u}$ and $\frac{\partial r_i}{\partial \theta}$ lie in the plane that is tangent to the surface. Then we obtain:

$$\delta r_i \cdot n_t = \left( \sum_{j=1}^{m} \frac{\partial r_i}{\partial d_j} \cdot n_t \right) \delta d_j = \sum_{j=1}^{m} \delta d_j$$

We can now consider a system of $k$ linear equations in $m$ unknowns ($m \ll k$) of the following structure

$$a_{11} \delta d_1 + a_{12} \delta d_2 + \ldots + a_{1m} \delta d_m = b_1$$

$$a_{s1} \delta d_1 + a_{s2} \delta d_2 + \ldots + a_{sm} \delta d_m = b_s$$

$$\vdots$$

$$a_{k1} \delta d_1 + a_{k2} \delta d_2 + \ldots + a_{km} \delta d_m = b_k$$

Here:

$$b_i = \Delta n_t = (R_{mi} - R_{mi}) \cdot n_m$$

The system of linear equations (22) is overdetermined since $m \ll k$. The essence of the procedure of minimization of deviations is determination of such unknowns $\delta d_j$ that will minimize the difference between the left and right sides of equations (22). The solution was accomplished by the least-square method. The subroutine DLSQRR of IMSL MATH / LIBRARY [4] was used for computerization of the procedure.

The success of minimization of deviations depends on the number of parameters that may be varied (the number of machine-tool settings that may be corrected). The number of pinion machine-tool settings is larger than for the gear. The minimization of deviations can be performed for each pinion tooth side separately. However, it must be performed simultaneously for both sides of the gear tooth since the gear is cut by the duplex method. For these reasons the minimization of deviations for the pinion is more effective than for the gear (see below the numerical examples).

7. APPLICATION TO INSPECTION OF FORMATE HYPOID GEAR

Each tooth side of a formate face-milled gear is generated by a cone and the gear tooth surface is the surface of the generating cone. Two cones that are shown in fig. 4(a) represent both sides of the gear space. The following equations represent in coordinate system $S_e$ gear surfaces for both sides and the unit normals to such surfaces (fig. 4(b))

$$r_e = \begin{bmatrix} -s_C \cos \alpha_G \\ (r_C - s_C \sin \alpha_G) \sin \theta_G \\ (r_C - s_C \sin \alpha_G) \cos \theta_G \\
1 \end{bmatrix}$$

$$n_e = \begin{bmatrix} \sin \alpha_G \\ -\cos \alpha_G \sin \theta_G \\ -\cos \alpha_G \cos \theta_G \end{bmatrix}$$

Here: $r_e$ is the position vector and $n_e$ is the surface unit normal; $r_C$ is the cutter tip radius; $\alpha_G$ is the cutter blade angle ($\alpha_G > 0$ for the concave side and $\alpha_G < 0$ for the convex side).

Fig. 5 shows the installment of the generating cone on the cutting machine. Coordinate systems $S_o$ and $S_i$ are rigidly connected to the cutting machine and the gear being generated, respectively. Systems $S_e$, $S_r$, and $S_i$ are rigidly connected to each other since the gear is formate cut (no relative motion between the cutter and workpiece). To represent in $S_i$ the theoretical gear tooth surface $\Sigma_t$ and the unit normal to $\Sigma_t$ we use the following matrix equations

$$r_i(s_G, \theta_G, d_j) = M_{rc} r_c(s_G, \theta_G)$$

Fig. 4. Generating Cones for Format Face-milled Gear.
7. EQUATIONS OF PINION THEORETICAL TOOTH SURFACE

The pinion tooth surface is generated as the envelope to the family of tool surfaces that are cone surfaces (fig. 9).

Henceforth, we will consider the following coordinate systems:

(i) the fixed ones, \( S_0 (x_0, y_0, z_0) \) and \( S_f (x_f, y_f, z_f) \) that are rigidly connected to the cutting machine (fig. 10 and fig. 11); (ii) the movable coordinate systems \( S_r \) and \( S_p \) that are rigidly connected to the cradle of cutting machine and the pinion, respectively; (iii) coordinate system \( S_t \) that is rigidly connected to the head cutter. In the process of generation the cradle with \( S_r \) performs rotational motion about the \( z_r \)-axis with angular velocity \( \omega_r \), and the pinion with \( S_p \) performs rotational motion about the \( x_r \)-axis with angular velocity \( \omega_p \) (fig. 11).

The tool (head-cutter) is mounted on the cradle and performs rotational motion with the cradle. Coordinate system \( S_t \) is rigidly connected to the cradle. To describe the installment of the tool
with respect to the cradle we use coordinate system $S_b$ (fig. 9 and fig. 10). The required orientation of the head-cutter with respect to the cradle is accomplished as follows: (i) coordinate systems $S_b$ and $S_f$ are rigidly connected and then they are turned as one rigid body about the $z_f$-axis through the swivel angle $j = 2\pi - \delta$ (fig. 10); (ii) then the head-cutter with coordinate system $S_f$ is tilted about the $y_f$-axis under the angle $i$ (fig. 9(b)). The head-cutter is rotated about its axis $z_f$ but the angular velocity in this motion is not related with the generation process and depends only on the desired velocity of cutting.

It will be shown later that the deviations of real pinion tooth surface can be minimized by corrections of parameters of installment of the pinion and the head-cutter. These pinion setting parameters are $E_m$ - the machine offset, $g_m$ - the machine-root angle, $\Delta B$ - the sliding base, $\Delta A$ - the machine center to back (fig. 11). The head-cutter settings parameters are: $S_R$ - radial setting, $\theta_0$ - initial value of cradle angle, $j$ - the swivel angle (fig. 10), and $i$ - the tilt angle (fig. 9(b)).

**Tool Surface Equations**

The head-cutter surface is a cone and is represented in $S_t$ (fig. 9) as

$$r_t(s, \theta, \phi) = \begin{bmatrix} (r_c + s \sin \alpha) \cos \theta \\ (r_c + s \sin \alpha) \sin \theta \\ -s \cos \alpha \\ 1 \end{bmatrix}$$  \hspace{1cm} (29)$$

Here: $(s, \theta)$ are the Gaussian coordinates, $\alpha$ is the blade angle and $r_c$ is the cutter point radius. Vector function (29) with $\alpha$ positive and $\alpha$ negative represents surfaces of two head-cutter that are used to cut the pinion concave side and convex side, respectively.

The unit normal to the head-cutter surface is represented in $S_t$ by the equations

$$n_t = [-\cos \alpha \cos \theta \quad -\cos \alpha \sin \theta \quad -\sin \alpha]^T$$  \hspace{1cm} (30)$$

The Family of Tool Surfaces is represented in $S_p$ by the matrix equation

$$r_p(s, \theta, \phi) = M_{p1} M_{p2} M_{p3} M_{p4} M_{p5} r_t(s, \theta)$$  \hspace{1cm} (31)$$

Here: $S_a$ is an auxiliary fixed coordinate system whose axes parallel to $S_a$ axes.
\[ \mathbf{M}_{\text{st}} = \begin{bmatrix} \cos i & 0 & \sin i & 0 \\ 0 & 1 & 0 & 0 \\ -\sin i & 0 & \cos i & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \]

\[ \mathbf{M}_{\text{cb}} = \begin{bmatrix} -\sin j & -\cos j & 0 & 0 \\ \cos j & -\sin j & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \]

\[ \mathbf{M}_{\text{oe}} = \begin{bmatrix} \cos q & \sin q & 0 & 0 \\ -\sin q & \cos q & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \]

\[ \mathbf{M}_{\text{ao}} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & -\Delta B \\ 0 & 0 & 0 & 1 \end{bmatrix} \]

\[ \mathbf{M}_{\text{em}} = \begin{bmatrix} \cos \gamma_m & 0 & \sin \gamma_m & -\Delta A \\ 0 & 1 & 0 & 0 \\ -\sin \gamma_m & 0 & \cos \gamma_m & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \]

\[ \mathbf{M}_{\text{pm}} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos \phi_p & \sin \phi_p & 0 \\ 0 & -\sin \phi_p & \cos \phi_p & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \]

\[ \delta = 2\pi - j; \varphi = \theta_c + m_{\text{rp}} \phi_p \text{ where } \theta_c \text{ is the initial cradle angle} \]

\[ \mathbf{r}_s = \mathbf{M}_{\text{soc}} \mathbf{M}_{\text{cb}} \mathbf{M}_{\text{st}} \mathbf{r}_t \]

\[ \mathbf{O}_x \mathbf{A} = \begin{bmatrix} 0 & -E_m & \Delta B \end{bmatrix}^T \]

\[ \omega^{(p)}_{\omega} = \begin{bmatrix} \cos \gamma & 0 & \sin \gamma \end{bmatrix}^T \]

\[ \omega^{(c)}_{\omega} = \begin{bmatrix} 0 & 0 & m_{\text{rp}} \end{bmatrix}^T \]

**Pinion Tooth Surface**

Equations (31) and (32) represent the pinion tooth surface in three-parametric form with parameters \( s, \theta \) and \( \phi_p \). However, since equation (32) is linear with respect to \( s \) we can eliminate \( s \) and represent the pinion tooth surface in two-parametric form as

\[ \mathbf{r}_p(\theta, \phi_p, d_j) \]

Here: \( d_j \) \((j = 1, \ldots, 8)\) designate the installment parameters: \( E_m, \gamma_m, \Delta B, \Delta A, S_R, \theta_c, j \) and \( i \).

The normal to the pinion tooth surface is represented as

\[ \mathbf{n}_p(\theta, \phi_p, d_k) \]

where \( d_k \) \((k = 1, 2, 3, 4)\) designate the installment parameters \( \gamma_m, \theta_c, j \) and \( i \).

**Results of Minimization**

Fig. 12 and fig. 13 illustrate the initial deviations \( \Delta h \) of the real surface, that have been obtained by measurements and calculations for the concave side and convex side, respectively. The blank data, the basic machine-tools settings, the corrections of machine-tool settings and the corrected machine-tool settings are shown in Table 2-3. Based on the corrected machine-tool settings, we can manufacture a new surface that will optimally fit the theoretical surface after the surface is distorted by manufacturing processes and heat treatment. The minimized deviations between the new surface and the theoretical surface are shown in fig. 14 and fig. 15. These figures confirm the effectiveness of the proposed approach. The deviations of approximately 30 microns have been reduced to 2-3 microns.

**8. CONCLUSION**

A general approach for computerized determination of deviations of a real surface from the theoretical one based on coordinate measurements has been proposed. An algorithm for minimization of deviations by corrections of initially applied machine-tool settings through application of a least square approach has been developed. The approach is illustrated with an example of the tooth surface of a hypoid pinion and gear.

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**REFERENCES**


Table 2: Blank Data of Hypoid Pinion

<table>
<thead>
<tr>
<th>Number of Teeth</th>
<th>13</th>
</tr>
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<tbody>
<tr>
<td>Shaft Angle</td>
<td>1.57079 rad.</td>
</tr>
<tr>
<td>Pitch Diameter</td>
<td>88.22 mm</td>
</tr>
<tr>
<td>Outside Diameter</td>
<td>103.96 mm</td>
</tr>
<tr>
<td>Pitch Angle</td>
<td>0.32055 rad.</td>
</tr>
<tr>
<td>Face Angle</td>
<td>0.41480 rad.</td>
</tr>
<tr>
<td>Root Angle</td>
<td>0.30136 rad.</td>
</tr>
<tr>
<td>Mean Spiral Angle</td>
<td>0.84677 rad.</td>
</tr>
<tr>
<td>Face Width</td>
<td>38.30 mm</td>
</tr>
<tr>
<td>Whole Width</td>
<td>11.63 mm</td>
</tr>
<tr>
<td>Hand of Spiral</td>
<td>R. H.</td>
</tr>
</tbody>
</table>

Table 3: Basic, Corrected, and Machine-Tool Setting Differences of the Pinion

<table>
<thead>
<tr>
<th>Machine Setting</th>
<th>Convex Side</th>
<th>Concave Side</th>
<th>Convex Side</th>
<th>Concave Side</th>
<th>Setting Differences</th>
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<tr>
<td>Basic Tilt Angle</td>
<td>0.3761899</td>
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<td>0.3712125</td>
<td>0.4165375</td>
<td>0.047786E-02</td>
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<td>Swivel Angle</td>
<td>5.766247</td>
<td>6.000656</td>
<td>5.768892</td>
<td>6.042001</td>
<td>0.04466E-02</td>
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<tr>
<td>Machine Root Angle</td>
<td>6.233756</td>
<td>6.272372</td>
<td>6.236861</td>
<td>6.301894</td>
<td>0.031529E-02</td>
</tr>
<tr>
<td>Cradle Angle</td>
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<td>1.561631</td>
<td>4.845368</td>
<td>1.573218</td>
<td>0.059817E-03</td>
</tr>
<tr>
<td>Radial Setting</td>
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<td>109.6660</td>
<td>113.6455</td>
<td>110.4463</td>
<td>-0.37806E-03</td>
</tr>
<tr>
<td>Sliding Base</td>
<td>23.8700</td>
<td>14.8200</td>
<td>23.8700</td>
<td>14.8200</td>
<td>0.00000000E+00</td>
</tr>
<tr>
<td>Machine Center to Back</td>
<td>3.280000</td>
<td>-3.100000</td>
<td>3.767510</td>
<td>-3.970493</td>
<td>0.579074E-05</td>
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<td>-39.63248</td>
<td>-35.45049</td>
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<td>Cutting Ratio</td>
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<td>0.3230215</td>
<td>0.00000000E+00</td>
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<tr>
<td>Cutter Point Radius</td>
<td>114.9350</td>
<td>113.0200</td>
<td>114.9350</td>
<td>113.0200</td>
<td>0.00000000E+00</td>
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<tr>
<td>Cutter Blade Angle</td>
<td>-0.5410521</td>
<td>0.2443461</td>
<td>-0.5410521</td>
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</tr>
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Fig. 12. Deviations of Pinion Real Tooth Surface (Concave Side).

Fig. 13. Deviations of Pinion Real Tooth Surface (Convex Side).

Fig. 14. Minimized Deviations of the Pinion (Concave Side).

Fig. 15. Minimized Deviations of the Pinion (Convex Side).
Minimization of Deviations of Gear Real Tooth Surfaces Determined by Coordinate Measurements

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The deviations of a gear’s real tooth surface from the theoretical surface are determined by coordinate measurements at the grid of the surface. A method has been developed to transform the deviations from Cartesian coordinates to those along the normal at the measurement locations. Equations are derived that relate the first order deviations with the adjustment to the manufacturing machine-tool settings. The deviations of the entire surface are minimized. The minimization is achieved by application of the least-square method for an overdetermined system of linear equations. The proposed method is illustrated with a numerical example for hypoid gear and pinion.

Gear; Grid surface; Deviations of gear; Measurements

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Subject Category 37

Unclassified

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