ADVANCED CERAMIC MATRIX COMPOSITES FOR TPS

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Abstract

Recent advances in ceramic matrix composite (CMC) technology provide considerable opportunity for application to future aircraft thermal protection systems (TPS), providing materials with higher temperature capability, lower weight, and higher strength and stiffness than traditional materials. The Thermal Protection Material Branch at NASA Ames Research Center has been making significant progress in the development, characterization, and entry simulation (arc-jet) testing of new CMC's. This presentation gives a general overview of the Ames Thermal Protection Materials Branch research activities, followed by more detailed descriptions of recent advances in very-high temperature Zr and Hf based ceramics, high temperature, high strength SiC matrix composites, and some activities in polymer precursors and ceramic coating processing. The presentation closes with a brief comparison of maximum heat flux capabilities of advanced TPS materials.
Long Range Goal of the Ames Thermal Protection Materials Branch

To Provide Thermal Protection Materials, Systems, and Analysis Methods for Heat Shields of Entry, Aerobraking and Hypersonic Cruise Vehicles and Planetary Probes

THERMAL PROTECTION MATERIALS

AMES VEHICLE → GROUND/FLIGHT EXPERIMENTS → FLIGHT TPS DEVELOPER

TPS TECHNOLOGY DEVELOPMENT, ARC JET TESTING & COMPUTATIONAL ANALYSES

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<td>• KEY SHUTTLE TPS CONTRIBUTIONS:</td>
<td>• NASP:</td>
<td>• NEW 4000°F + REUSABLE CERAMICS AND TPS</td>
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<tr>
<td>- L.I.Z200°</td>
<td>- CMC &amp; COATINGS TMP’S</td>
<td>- HOT STRUCTURE CMC TPS</td>
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<td>- FRCI-12°</td>
<td>- GWP #93 &amp; #95</td>
<td>- DURABLE ALL-WEATHER TPS</td>
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<td>- RCG COATING*</td>
<td>- ARC-JET TESTING</td>
<td>- ADVANCED ABLATORS:</td>
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<td>- AFRSI&quot;</td>
<td>- LEAD CENTER FOR SEI AEROBRAKE TPS</td>
<td>- CERAMIC/POLYMER</td>
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<td>- GAP FILLERS*</td>
<td>- 3 AFE EXPERIMENTS</td>
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<td>- IN FLIGHT PROOF OF CATALYTIC EFFECTS</td>
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<td>- ARC-JET TESTING FOR SHUTTLE, GALILEO, APOLLO, DOD VEHICLES</td>
<td>- PEGASUS FLIGHT EXP’S</td>
<td>- X-30, DELTA CLIPPER</td>
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<td>- X-24B/C FIRST SUPersonic FLIGHT TEST OF TILE TPS</td>
<td>- NEW MATERIALS AND TPS:</td>
<td>- HYFLEX, JSC FLIGHT EXP.</td>
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<td>- Ames Patent</td>
<td>- AETB*, TUFIB</td>
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<td>- Tech Brief</td>
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<td>- CMC DEVELOPMENT</td>
<td>- NUCLEAR ROCKET REENTRY</td>
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<tr>
<td></td>
<td>- TOP HAT*</td>
<td>- ADVANCED TPS MODELING</td>
</tr>
<tr>
<td></td>
<td>• NUMEROUS APPLICATIONS</td>
<td></td>
</tr>
</tbody>
</table>
Projects

NASA Programs

- SEI: Recent Langley "Aerobrake Assembly with Minimum Accommodation" study performed by Lockheed baselined Ames developed "TOP HAT" CMC/rigid tile TPS.

- Shuttle: Working with KSC, JSC, NASA HQ and Rockwell to fly Ames developed TUFI TPS on the Orbiters in high erosion areas.

- MESUR: Performed initial TPS sizing and trades. Identified a light weight silicon rubber TPS (SLA-561) which allows a 50% increase in scientific payload.

- Pegasus: Teaming with Dryden and LaRC for boundary layer cross flow transition experiment (scheduled to fly in FY92). Constructing Pegasus Wing-Glove and PI for and TPS performance evaluation experiment. Wing fillet heating experiment flown on first two Pegasus launches.

- HYFLEX: Working with a multi-agency team to define vehicle. Diboride leading edges and nosetip being evaluated.

- Wave-Rider: Discussions with McDonnell Douglas regarding leading edge design.

NASP

- Responsibility for government work packages #93 and #95 for arc-jet testing and internal TPS insulation design.

- Both have been highly praised by NPO/JPO and Industry Leads (i.e. General Dynamics, Rockwell, Pratt Whitney).

DoD

- Delta Clipper: Cooperative research program being developed with McDonnell Douglas and SDIO. Cooperative efforts proposed in three areas:
  1) TPS design and consultation
  2) Arc-jet testing
  3) Computational studies
Material/TPS Testing Areas

- Arc-Jet Testing
  - Aerodynamic Heating Facility (20 MW)
  - Interactive Heating Facility (60 MW)
  - Panel Test Facility (20 MW)
- Material Characterization
  - SEM, XRF, Optical Microscopes
  - XRD, Large Sample TGA
  - Dilatometer, Instron
  - Infrared & Ultraviolet Spectrometers
  - ICP Mass Spectrometer (inorganic)
- Special Testing
  - Laser Time-of-Flight Mass Spectrometer (SALI)
  - Side Arm Reactor

Material/TPS Analysis Areas

- Computational Surface Thermochemistry
  - Surface heating and catalysis effects (NSCAND, BLIMPK, LAURA, VSL, GASP)
  - Ablation, erosion, and shape change computations (ASC, CMA, ACE)
- Computational Solid Mechanics
  - Multi-dimensional conduction/radiation analyses (SINDA, TRASYS)
  - Multi-dimensional thermal-stress analyses (COSMOS)
- Computational Materials
  - CVD/CVI Processing (GENMIX, NACHOS)
  - Reflective TPS analyses
  - Composite material properties (MATX)
**Material/TPS Development Areas**

**Advanced Material Families**

- **Ceramic Matrix Composites**
  - Very-High Temperature Ceramics (HfB₂ + SiC)
  - High Temperature, High Strength Ceramics (C/SiC)
  - Polymer Precursors (Si/C/B fibers, tape casting)
  - Ceramic coatings processing

- **Light Weight Ceramic Insulations**
  - Rigid Tiles (AETB, SMI, UltraLight)
  - TABI and CFBI Flexible Blankets
  - Aerogel Studies

- **Light Weight Ablators**
  - Rigid Ceramic Insulation with a Polymer Filler

- **Surface Coatings**
  - Low Catalytic Efficiency, High Emissivity
  - Reflective

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**Diboride Materials**

- Manlabs Inc. (Cambridge MA) tested and compiled a database on a large number of refractory materials in the 60's and early 70's
- The diborides of zirconium and hafnium (ZrB₂ and HfB₂) were found to be the most oxidation resistant, high temperature materials in the study, e.g.

<table>
<thead>
<tr>
<th>Arc testing of ZrB₂ + 20 v/o SiC</th>
</tr>
</thead>
<tbody>
<tr>
<td>surface temp. 2510 C, stagn. press. 1.0 atm, stagn. enthalpy 11.5 kJ/gm</td>
</tr>
<tr>
<td>recession: 0.66 mm/2 hrs</td>
</tr>
<tr>
<td>equivalent graphite recession: 30 cm !</td>
</tr>
<tr>
<td>equivalent SiC recession: 45 cm !</td>
</tr>
</tbody>
</table>

"These results illustrate the reuse capability of the boride composites... This capability is unrivaled by any other material system." - Quote from Dr. Larry Kaufman, Principal Investigator in the Manlabs Studies
Research Highlights for FY91

Very-High Temperature Ceramics
- Phase I arc-jet testing completed
- 19 reinforced Zr and Hf based ceramics tested (from Manlabs, Cerac, Lanxide, SAIC)
- Arc-jet data in good agreement with earlier Manlabs results
- Over 2 times RCC maximum heat flux capability demonstrated
- 2200°C+ (4000°F+) capability demonstrated
- Successfully applied ZrB₂ coatings to RCC using RF sputtering
- Phase II testing of disk samples, nosetip and leading edge components currently in progress

Sample Model Holder
Post-Test Photographs of RCC and ZrB$_2$ + 20 v/o SiC Samples

Test Conditions: test time = 3 min, cold wall heat flux = 295 W/cm$^2$
stag. press. = 0.046 atm, stag. enth. = 25 kJ/gm

LTV-t1n2a
RCC
Recession: 2.0 mm
Weight loss: 1.31 gm
Peak temp.: 2040 C
SiC coating lost after approximately 100 sec.

Cerac-t2n4a
ZrB$_2$ + 20v/o SiC
Recession: -0.03 mm
Weight loss: 0.01 gm
Peak temp.: 1820 C
Adherent, thin, glassy coating formed on sample
Post-Test Photographs of Two HfB$_2$ + 20 v/o SiC Samples

Test time = 5 min
Cold wall heat flux = 560 W/cm$^2$
Stag. press. = 0.075 atm
Stag. enth. = 27 kJ/gm

Recession: -0.05 mm
Weight loss: 0.00 gm
Peak temp.: 1740 C

Clear glassy coating formed on sample

Test time = 3 min
Cold wall heat flux = 730 W/cm$^2$
Stag. press. = 0.105 atm
Stag. enth. = 27 kJ/gm

Recession: -0.03 mm
Weight loss: 0.08 gm
Peak temp.: 2460 C

Adherent, thin oxide coating formed on sample
Disk Sample (3" diam. x 0.25")

Leading Edge (4.0" x 0.5" diam.)

Diboride Components

ZrB₂ + 20v/o SiC & HfB₂ + 20v/o SiC Materials

Hypersonic Vehicle Noisetip (0.141" nose radius)
<table>
<thead>
<tr>
<th>Sample Component</th>
<th>Matrix/Reinforcement</th>
<th>Geometry/Dimension</th>
<th>Quantity</th>
</tr>
</thead>
<tbody>
<tr>
<td>ManLabs-C1</td>
<td>ZrB2/SiCp</td>
<td>Coupons/2.8&quot;Dia. x 0.25&quot;</td>
<td>3</td>
</tr>
<tr>
<td>ManLabs-C2</td>
<td>ZrB2/SiCp</td>
<td>Coupons/2.8&quot;Dia. x 0.25&quot;</td>
<td>3</td>
</tr>
<tr>
<td>ManLabs-C3</td>
<td>ZrB2/SiCp+CfCf</td>
<td>Coupons/2.8&quot;Dia. x 0.25&quot;</td>
<td>3</td>
</tr>
<tr>
<td>ManLabs-1E</td>
<td>ZrB2/SiCp</td>
<td>Leading Edge/0.75&quot;Dia. x 2.75&quot;</td>
<td>2</td>
</tr>
<tr>
<td>ManLabs-H1</td>
<td>HfB2/SiCp</td>
<td>Hemisphere/0.700&quot;Radius</td>
<td>1</td>
</tr>
<tr>
<td>ManLabs-H2</td>
<td>HfB2/SiCp</td>
<td>Hemisphere/0.500&quot;Radius</td>
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<tr>
<td>ManLabs-H3</td>
<td>HfB2/SiCp</td>
<td>Hemisphere/0.125&quot;Radius</td>
<td>1</td>
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<tr>
<td>ManLabs-NT</td>
<td>HfB2/SiCp</td>
<td>Nose Tip/0.141&quot;Radius on 5.25 Deg. Cone Half Angle</td>
<td>3</td>
</tr>
<tr>
<td>ManLabs-S</td>
<td>ZrB2/SiCp</td>
<td>5.25 Deg. Cone Half Angle</td>
<td>1</td>
</tr>
<tr>
<td>Cerac-S</td>
<td>ZrB2/SiCp</td>
<td>Skirt</td>
<td>2</td>
</tr>
<tr>
<td>Cerac-C</td>
<td>ZrB2/SiCp</td>
<td>Coupons/2.8&quot;Dia. x 0.25&quot;</td>
<td>3</td>
</tr>
<tr>
<td>ACR C1</td>
<td>ZrB2/SiCp*CfCf</td>
<td>Coupons/2.8&quot;Dia. x 0.25&quot;</td>
<td>2</td>
</tr>
<tr>
<td>ACR C2</td>
<td>ZrB2/SiCp*SiCf</td>
<td>Coupons/2.8&quot;Dia. x 0.25&quot;</td>
<td>2</td>
</tr>
<tr>
<td>ARC C1</td>
<td>ZrB2 Coated RCC</td>
<td>Coupons/2.8&quot;Dia. x 0.25&quot;</td>
<td>1</td>
</tr>
<tr>
<td>ARC C2</td>
<td>ZrB2 Coated RCC</td>
<td>Coupons/2.8&quot;Dia. x 0.25&quot;</td>
<td>1</td>
</tr>
<tr>
<td>GA C1</td>
<td>RS HfB2 Coated C/C</td>
<td>Coupons/2&quot;Dia. x 0.25&quot;</td>
<td>2</td>
</tr>
<tr>
<td>GA C2</td>
<td>HfB2 Coated RS</td>
<td>Coupons/2&quot;Dia. x 0.25&quot;</td>
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</tr>
<tr>
<td>SAIC C1</td>
<td>ZrB2/SiCp*CfCf</td>
<td>Coupons/2.8&quot;Dia. x 0.25&quot;</td>
<td>1</td>
</tr>
<tr>
<td>SAIC C2</td>
<td>ZrB2/SiCp*SiCf</td>
<td>Coupons/2.8&quot;Dia. x 0.25&quot;</td>
<td>1</td>
</tr>
<tr>
<td><strong>Total</strong></td>
<td></td>
<td></td>
<td><strong>3.5</strong></td>
</tr>
</tbody>
</table>

Subscript definitions: p = particulate, pl = platelet, cf = continuous fiber, fch = chopped fiber
Material/TPS Development Areas

Advanced Material Families

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  - Ceramic coatings processing

- Light Weight Ceramic Insulations
  - Rigid Tiles (AETB, SMI, UltraLight)
  - TABI and CFBI Flexible Blankets
  - Aerogel Studies

- Light Weight Ablators
  - Polymer Filler + Rigid Ceramic Insulation

- Surface Coatings
  - Low Catalytic Efficiency, High Emissivity
  - Reflective

Research Highlights for FY91

Ceramic Matrix Composites

- DuPont and SEP fabricated Nicalon, Nextel, and carbon fiber reinforced SiC matrix composites evaluated for aerothermal and mechanical performance

- Pre and post-test mechanical property characterization showed that carbon fiber reinforced materials have little degradation after arc-jet exposure to 2700°F for ten cycles of ten minutes each

- DuPont material found to be equivalent or better (particularly in quasi-isotropic configuration) than SEP material.

- Mass loss and mechanical property retention results in very good agreement with radiative heating testing data recently reported by General Dynamics

- New Ames developed "TOP HAT" CMC/rigid tile TPS, using Ames CVD/CVI fabricated C/SiC CMC, shown to survive multiple arc-jet exposures to 3100°F
CERAMIC MATRIX COMPOSITES PROGRAM

"TOP HAT" Assembly
Edge View

Average Tensile Strength vs. Temperature Pre-aeroconvective Exposure (U)

Average Tensile Strength (70 F, Ar) of Carbon/SiC, Nextel/SiC, and SiC/SiC vs. Time of Aeroconvective Exposure (2700 F)

Ceramic felt
0.6
1.25
FRCI-12
0.125 PD-200
0.062 Aluminum plate

Section A-A

Test temperature (°F)

Time of exposure (min)

C: SiC
O: Nextel/SiC
△: SiC/SiC

Tensile strength (ksi)

0 500 1000 1500 2000 2500 3000

0 10 20 30 40 50 60 70

0 10 20 30 40 50 60 70 80 90 100

0 10 20 30 40 50 60 70
TOPHAT Thermal Protection System
Arc-Jet Model Design

Cross Section View

TOP HAT
Weight = 0.4 lb/ft²

TOP HAT MODEL
T1, T2: Tungsten TC
T3, T4, T5: Pt/Pt Rd (15%)
Volume of model above the aluminum back plate: 10.59 cu in
System Density: 14.7 lb/ft³

Aluminum backplate:
41 gm = 0.09 lbs

Thermal Response Of TOPHAT Model
In An Aeroconvective Environment

Model B
Runtime: 5 min
Cycle 1 of 5
\[ \dot{q} = 100 \text{ Btu/ft}² \cdot \text{s} \]

Temperature (°F)

Time (sec)
TOP HAT
Thermal Protection System

Ceramic matrix composite

High temperature felt

Rigid reusable insulation

Spacecraft structure
Material/TPS Development Areas

Advanced Material Families

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- Surface Coatings
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Research Highlights for FY91

Polymer Precursors
- Low oxygen content Si/C/B polymers synthesized
- UV air and non-oxygen cure procedure demonstrated
- Ceramic fibers show tensile strength retention to 1300°C
- Successfully synthesized Zircon/ZrB2/SiC 20 mil tapes using a combination of tape casting and sol-gel processing

Ceramic Coating Processing
- Successfully applied thin (20 micron) coatings for ZrB2 to a SiC substrate using RF sputtering
- Planning initial trials for plasma spraying ZrB2 and ZrB2/SiC using a constricted arc-jet

![Tensile Strength of SiC, Si-C-N and Si-C-B Fibers as a Function of Fiber Diameter](image1)

![Temperature Effects on Fiber Tensile Strength in Air](image2)

Maximum Cold Wall Heat Flux Computations

For one-dimensional, radiative equilibrium, the maximum cold wall heat flux, \( Q_{cw} \), can be computed from the maximum material use temperature, \( T_{max} \), by:

\[
Q_{cw} = \varepsilon \frac{T_{max}}{1 - \frac{H_{w}}{H_{r}}}
\]

where \( \varepsilon \) is the emissivity and \( H_{w} \) is the wall gas enthalpy at \( T_{max} \), and \( H_{r} \) is the local recovery enthalpy.

Surface catalytic effects all roll into the value of \( H_{w} \).

With values for the material maximum use temperature and emissivity, \( Q_{cw} \) can be easily computed.

<table>
<thead>
<tr>
<th>Material</th>
<th>Maximum Use Temp. (°C)</th>
<th>Emissivity</th>
</tr>
</thead>
<tbody>
<tr>
<td>HfB₂+SiC</td>
<td>2480</td>
<td>0.62</td>
</tr>
<tr>
<td>SiC (or Coated C-C)</td>
<td>1760</td>
<td>0.76</td>
</tr>
<tr>
<td>Rigid Tiles</td>
<td>1540</td>
<td>0.85</td>
</tr>
<tr>
<td>Coated Niobium</td>
<td>1530</td>
<td>0.65</td>
</tr>
</tbody>
</table>

Maximum Cold Wall Heat Flux Computations

\( Q_{cw} \) for a Fully Catalytic Surface

\( Q_{cw} \) evaluated assuming chemical equilibrium.
Maximum Cold Wall Heat Flux Computations

Range of Catalytic Effects on $Q_{cw}$ for SiC*

- Altitude 100 kft

- Oxygen Dissociation Lobe
- Nitrogen Dissociation Lobe
- SiC (or Coated C-C)

- * $Q_{cw}$ evaluated varying from equilibrium to maximum non-equilibrium value