Analysis of the Space Shuttle Main Engine Simulation

J. Alex De Abreu-Garcia and John T. Welch

University of Akron
Akron, Ohio

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ANALYSIS OF THE SPACE SHUTTLE MAIN ENGINE SIMULATION

J. Alex DeAbreu-Garcia and John T. Welch
University of Akron
Akron, Ohio 44325

ABSTRACT

This report analyzes the digital code used to simulate dynamic performance of the Space Shuttle Main Engine. This simulation program is written in Fortran. The purpose of the analysis is to identify a means to achieve faster simulation execution, and to determine if additional hardware would be necessary for speeding up the simulation. The analysis included the use of custom integrators based on the Matrix Stability Region Placement method. In addition to speed of execution the accuracy of computations, the useability of the simulation system, and the maintainability of the program and data files were examined. A revised code implementing the study recommendations was implemented but not verified for accuracy.
1. INTRODUCTION

This is a final report on an analysis of the Space Shuttle Main Engine Program, a digital simulator code written in Fortran. The research was undertaken by the authors in ultimate support of future design studies of a shuttle life-extending Intelligent Control System (ICS). These studies are to be conducted by NASA Lewis Space Research Center.

The primary purpose of the analysis was to define the means to achieve a faster running simulation, and to determine if additional hardware would be necessary for speeding up simulations for the ICS project. In particular, the analysis was to consider the use of custom integrators based on the Matrix Stability Region Placement (MSRP) method.

In addition to speed of execution, other qualities of the software were to be examined. Among these are the accuracy of computations, the usability of the simulation system, and the maintainability of the program and data files.

Accuracy involves control of truncation error of the methods, and roundoff error induced by floating point operations. It also involves the requirement that the user be fully aware of the model that the simulator is implementing.

The usability of the simulation system affects the productivity of ICS designers. The simulation system should support a large number of runs, with reliable tracking, archiving, and retrieval of run results. Setting up simulation runs and reviewing results should be easy to do, and not be subject to hard to detect errors.

Simulation of intelligent control methods for the main shuttle engine is expected to involve considerable manipulation of the shuttle engine control systems. The ICS design studies will take into account new perturbation modes, and may consider variations in shuttle engine design.

Thus the studies will place high maintainability requirements on the simulation code. The SSME Simulation Program must be readable, and organized to permit easy and safe alteration.

Long exposure to the SSME code compels us to acknowledge with special appreciation the work of Ten-Huei Guo of NASA Lewis Space Center, whose extensive interpretive comments made the source intelligible enough for analysis. We have preserved most of his commentary in the report version. A careful reading of the SSME simulation code, as received by NASA Lewis Space Center, would
affirm that our criticisms of the coding do not apply to Dr. Guo's work, or that of NASA Lewis Research Center.

Organization of this Report

The report begins with a summary of results and recommendations. It ends with a suggested implementation and tuning sequence for the simulation.

The next three chapters are devoted to numerical integration methods. Multi-step integration methods and the basis for their analysis are explained in Chapter 3. The next chapter presents the analysis results obtained in the study. Chapter 5 then describes the integration function module of the report version, explaining the numerical and coding techniques implemented.

The remaining chapters cover interpolation methods, energy balance monitoring and control, exponentiation, and simulation output.

The remainder of the report is a set of appendices defining a Fortran 77 code and set of supporting data files. This represents the form of the simulation recommended for ICS design studies. This version is also delivered with the report as ASCII files on diskette. For convenient reference, the appended listing will be called "the report version" throughout this report. The code and run data we received from NASA Lewis, for purposes of study, we will call "the study version".

The research was expected to produce analysis results, rather than a revised code. However, it became obvious on examination of the study version that the line-by-line optimization and the new function modules required could not be adequately defined without a full code revision. The report version is a revised code fully implementing the immediate recommendations, but is not verified to be in accurate running condition, as this report goes to print.

The report version code is itself an important product of the research study. It shows in specific detail how the recommendations may be followed, and can contribute directly to their full implementation. If a majority of the recommendations are accepted, then the report version would certainly be a time-saving source of implementation code, if not the basis for a rapid implementation.
2. SUMMARY OF RESULTS

Study of the SSME Simulation Program revealed many problems that could seriously impede ICS development, if left uncorrected. In the form given to us, the program

- is unacceptably slow in running time.
- produces too much output for reasonable review and handling of results.
- is difficult to set up accurately.
- is of questionable numerical accuracy in some subsystems.
- is difficult to maintain as a testbed simulator for new control methods.

The report version of the system, reprinted in Appendix A, addresses all of these issues in specific terms.

Speedup Results

Slow running time was a primary focus of the study. Lack of significant improvements in this area would have indicated a requirement for hybrid computing hardware. The original proposal anticipated analysis of implementation technique in ADSIM on the ADI AD100 system.

Instead, many opportunities for speedup were found, which can be exploited independently, and therefore work as multiplying factors to produce a very high expected speedup. A negative aspect of this is that the opportunities were so ample and interwoven, that we were hard pressed within the time available to adequately define all of the contributing changes, or to construct more than a conservatively low estimate of the achievable speedup. We predict a speedup in running time of about 20. It could be higher.

With this kind of speedup available, the use of special purpose hardware for the SSME Simulation is not recommended. We believe the additional programming costs and limited access associated with special hardware can be avoided in this case. In fact, with the decrease in bulk of program and data that is demonstrated by the report version, we can recommend that the ICS project use desktop 386 PC Systems or similar workstations to house the SSME simulation, perhaps with management of results data on mainframe systems.
The identification of many available methods of speedup leads us to recommend also a course of action that exploits the most readily available speedup first, and defers the most difficult until it is known to be necessary. Most of the available speedup can be achieved with the following steps, listed by decreasing expected effect:

1. Replacing formatted character output of every output variable by selective output in unformatted binary form. Conversion can be done offline, along with printing and/or plotting. Conversion and output transfer of character strings representing data, and output of headings identifying data, compares with computations in running time. With no changes here, significant improvements in computation time would be severely limited in effect.

2. Replacing Euler integration with a modified version of the multistep Adams-Bashforth Second Order integration formula (MAB2). This integration method, developed by our colleague, Dr. Tom Hartley, permits a step size five times greater than the Euler method used in the study version. An integration module supporting this change is provided in the report version.

3. Replacing interpolation routines implemented with varying levels of efficiency with a single set of routines coded as efficiently as possible. These routines are provided in the report version.

4. Improving code which computes results unnecessarily, code which uses unnecessarily many operations, code which uses divisions where equivalent multiplications are available, and code which makes unnecessary reference to costly special functions. These improvements have been made in the report version.

5. Monitoring the convergence of energy balancing loops more closely and introducing under-relaxation and over-relaxation factors to minimize convergence iterations. A convergence control module is provided in the report version.

6. Confining the use of double precision to the integration process where it is actually required. Using exact integer arithmetic, rather than double precision, for the accurate advancement of time.

7. Replacing high precision, software supported real exponentiation by linear interpolation or by forms better supported in hardware on the host computer system.

All of the above methods are implemented, with every module
undergoing revision, in the report version of the code.

It is the conclusion of the study that, due to changing modes of the model, and its size, a full matrix version of MSRP would not be practical. The number of variables would make both the analysis and implementation impractical.

Step sizes of up to 100 times those achievable with the modified AB2 can be obtained with local versions of MSRP, but at the cost of a more complex and less flexible integration process, requiring additional analysis of the SSME model. The theoretical gain in step size could not be fully realized, since important dynamics of the system would not be followed at such large step sizes. Also there is the fact that evaluation of the SSME model at every time step requires sensitive energy balancing. Since the effect of SSME dynamics on energy balancing at larger time steps is unknown, it seems more prudent to implement the other methods of speedup before undertaking a conversion to local MSRP. The required analysis for local MSRP is continuing beyond the study, in master's thesis work described later.

The report version integration module allows for the progressive extension to higher order multistep integrators, and can accommodate local forms of MSRP, should they prove later prove desirable.

Accuracy results

The time step set in the study version was barely within stability limits for the integration method used. This generally implies that considerable distortion is being introduced by the numerical integration process itself. Reasonable accuracy limits on the time step are definitely exceeded in the valve dynamics module, according to the analysis, even though a higher sampling rate is used in this module.

The analysis shows that the recommended modified AB2 is an integration method better suited to the shuttle engine model, and produces less integration distortion than Euler's method, even when operated at the larger time step recommended for decreased running time.

Two potential floating point roundoff problems are noted, and corrected in the report version. All integration was converted to use a double precision accumulator, to avoid losing significant digits when small integration increments are added to large integrand variables in floating point.

The same floating point roundoff effect causes a significant drift in the time scale as the time step is repeatedly added to
the current time, but double precision is not the best answer to this problem. Instead, the report version keeps time as an integer number of step increments, which stays exact.

A potentially serious source of inaccuracy in the study version was the practice of limiting the input variable to keep it within the input range of an interpolation table. This has the effect of extrapolating the table by a constant value, without warning to the user when it is being done. Since interpolation tables can be readily extended, with little storage cost, there is no justification for this policy. The report version interpolators give a specific complaint and stop the simulation when a range is exceeded. The user can then extend the table by word processing an ASCII file. The simulation can then be rerun without change.

Finally, accuracy of the simulation is potentially enhanced by a new method of storage recommended for tabulated functions. The new method allows more points to be assigned to one function, without incurring a storage penalty on all other functions, and with minimal impact on running time.

Useability Recommendations

A sufficiently fast and accurate simulation program could still fail as a tool for the ICS design studies if it were too difficult to operate. The study version had several other major shortcomings of this nature, which are addressed in the report version.

One failing in this area has already been mentioned, an inflexible output system that dumps everything on every run. Adding to this burden on the program's users is the automatically echoed output of every input parameter. This flood of mostly unread data is no virtue. Aside from the running time it costs, uncontrolled amounts of output inhibits simulation activity and makes archiving and retrieval of simulation results unmanageable. Results are consequently lost or never obtained.

The recommended system of selectable binary output, along with a faster running simulation, offers a better approach to data archiving. Simulations can be rerun to repeat and amplify interesting results. The requirement to restart the simulation, which is difficult to support with higher order integrators, can be dropped.

Quality of simulation runs can be improved, when tuning of conditions leading up to archived results can be done without running at full output mode. The report version decouples the selection of input parameters and output configuration,
supporting this mode of operation.

Selected binary data is a much more practical form of archived simulation data than fully annotated hard copy. Results can be viewed and correlated in new ways, deferring hard copy until significant results are observed.

As important as running time and manageable archiving of data are, the opportunities for greater exploitation of NASA Lewis' graphics hardware in the interpretation of simulation results, made possible by a more flexible output system, may contribute as much to the success of the ICS design studies.

Another hurdle to the effective use of the SSME simulation by an ICS design team is the study version's file design for the bulk of the input data. This design mixes run parameters and interpolation data in the file 'dtminp.dat'. Run parameter values appear in this file without identifiers or limiters of any kind. Users are rightly advised to be cautious in altering the file.

We recommend replacing 'dtminp.dat' by two files, one for interpolation tables and another for run parameters. Both files contain identifiers and field markings that are not read by the program, but make it easy to find the field to be changed and to be sure that the change is made within the desired field. Since these files contain identifying headers, they can serve as documentation for the run parameters and function generation data used in a run. This relieves the program of echoing input data, with identifiers. Examples are provided in Appendix B.

Finally, we consider it a potential useability hazard to depend on Fortran IV, through use of obsolete language features like NAMELIST. The superseding Fortran 77 standard was adopted in 1978, and only the most forgiving of maintained compilers still accepts Fortran IV. Reliance on Fortran IV unnecessarily limits the portability of the program, and will shut off, more and more, opportunities to house it in more productive ways.

Evidence of the above can be offered from our own experience in the study. We were unable to get our copy of the original code to run without eliminating NAMELIST data, although it compiled without complaint. No manual was available, because the compiler we had to use is not actively supported at our facility. We did get around it, but the experience makes the point.

Having the use of the latest in compilers is an advantage soon realized in working with the SSME code. Many artifacts of past changes, which should have been removed when their function became obsolete, were identified in the listings.
The report version is written in Fortran 77. NAMELIST input was absorbed into the run parameter file, where it is almost as convenient to access as it was in the NAMELIST file 'start4.dat'. An added advantage is that there is only one place to set input parameters. The danger in having two entry points for a data item, with one overriding the other, is obvious.

An interim plan to divide the input parameter file into two similar files was abandoned. The idea was to have frequently changed parameters in a smaller file, and infrequently changed parameters in a longer one. It complicates parameter setting to have two possible sites for the value to be changed. With "find" commands in modern word processors, this division is unnecessary.

Maintenance for ICS Design Studies

A serious failing of the study version from the maintenance standpoint was that all executing code was packaged as a single file, a form which forces a complete compilation to accomplish any change in any module. In the report version, source code for each major subroutine is on a separate file. Only changed modules need be compiled on a revision.

The study version included a line number on every line, a format which requires most systems to support the blank space with space characters. Files were cut by about 45% in size by eliminating nine out of every ten line numbers, ending all lines with a line return character following the last nonspace character. Every tenth line number was retained, to allow for reference in the report version back into the study version. These line numbers should also be eliminated when this function is no longer served.

Better overall readability of the code was obtained in the report version by insertion of punctuating white space. Many originators seemed to think it a virtue to pack all of the information into as little space as possible.

Readability was improved considerably in some sections by reduction of spaghetti code sequences to structured code, using nested block IF constructions. This improvement would not be available in Fortran IV. An especially counterproductive style used in some of the study version's "spaghetti" sequences parked GO TO statements far to the right of the line. These statements often escape the attention of readers, misdirecting them as to the effect of the code.

Another change made for the sake of readability was to eliminate selection of a special mode of a subroutine by the value of an integer argument. For the major system component
subroutines, the subroutine was divided into an initialization entry and a time step entry, using different entry names for the two functions. This also eliminates the subroutine having to test to see which mode it is in.

Finally, it should be observed that the study version's output system places an unnecessary burden on the maintenance of the simulation. In the main program of the study version, output variables were renamed and saved again, and new combinations of output variables were computed for the sake of output alone. In some cases, data was saved again on separate files for the expressed purpose of plotting. These represent special needs for simulation output, many probably no longer current, but not removed. Undoubtedly, less obvious extra computations of this type remain in the simulation.

In the recommended output system, no alterations of the simulation program are made to create plot files or to output computed combinations of output variables. Instead, small programs are written for these purposes, all reading the same binary data files, but presenting the data in differing ways offline. These programs have in common the SSME output file format. Some of them, designed to run on machines other than the host of the SSME compiler, might require binary floating point conversions of the data. Each such program builds upon the SSME simulation system, and does not require additional maintenance on it.
A Procedure for Tuning the SSME Simulation

The report version of the SSME Simulation anticipates the following recommended procedure for tuning the simulation to its highest level of efficiency for the ICS design studies:

1. Run the report version, comparing with previous study version results. Account for differences. Changes made for faster execution should not significantly affect results. Euler's method remains as the default integration method so that these verification runs can be made before changing integration methods.

2. Decrease the step size in the valve dynamics module to recommended values. This is to establish a baseline of runs known to be more accurate, but consistent with previous results and real data.

3. Examine energy balance convergence and adjust relaxation factors, under-relaxing slow converging sections and over-relaxing fast converging sections. Look into relaxation of convergence criteria, and for accuracy problems which might account for residual slow convergence.

4. Attempt to eliminate cubic spline interpolation, and to select the most efficient form of real exponentiation for host system.

5. Switch to recommended integration methods and increase step sizes gradually, monitoring effects on energy balancing convergence and adjusting relaxation factors accordingly. Continue to recommended step sizes and beyond, pulling back to assured accuracy levels.
This chapter gives a brief review of the derivation of and definitions associated with linear multistep methods. Although implicit methods provide more accurate results than explicit methods, they require greater computational times. Therefore, implicit methods are, in general, not used in real-time applications. As a result, only explicit methods will be considered here. It should be pointed out that the material presented in this chapter borrows heavily from the results of references [1] and [2].

In the study version of the SSME simulation numerical integration is done using Euler's method. One of the main reasons being that Euler's method is well understood and simple to implement. However, it will be seen that care must be exercised when choosing the Euler's integration timestep to provide a more accurate simulation. Increased accuracy requires that very small timesteps be used at the expense of a considerably slower running simulation. In this analysis the concept of stability region of an integrator is used to show that it is possible to obtain a faster and more accurate simulation of the SSME should other linear multistep methods be used. Custom designed integrators will also be considered.

This chapter is organized as follows: first, the general linear multistep method is developed. Included in this development are the important notions of order, accuracy, consistency, and zero-stability. Both Euler's method and AB-2 are derived. Then, the concept of stability region of an integrator is discussed. Comparisons are made between the stability region of Euler's integrators and the stability region of AB-2 type integrators. It is shown that AB-2 integrators may result in a more accurate and faster running simulation. To guarantee a stable simulation of those modules whose eigenvalues have large imaginary parts with respect to their real parts, a modified AB-2 integration method is presented [3]. To conclude this analysis, the applicability of the matrix stability region placement method of [4] to the SSME simulation is discussed.

A. LINEAR MULTISTEP METHODS

The general linear multistep method can be written as follows:

$$\sum_{j=0}^{r} a_j x_{k+j} = T \sum_{j=0}^{r} b_j \dot{x}_{k+j} . \tag{1}$$

where $\dot{x}$ is the first derivative of $x$, $a_j$ and $b_j$ are constants, $a_0$ and $b_0$ are not allowed to be both zero, and, to avoid ambiguity, it is assumed that $a_r=1$.

The method of equation (1) is said to be explicit if $b_r=0$, and implicit if $b_r \neq 0$. For an implicit method the present value of the output is a function of present and past values of the output and the input. For an explicit method only past values of the output and the input are required to determine the present value of the output. Here
we will be concerned only with explicit methods as implicit methods are not suitable for real-time simulation.

Associated with the linear multistep method of equation (1) is the operator:

\[ L[x(t),T] = \sum_{j=0}^{r} [a_j x(t+jT) - b_j \dot{x}(t+jT)] . \]  

(2)

where \( x(t) \) is an arbitrary continuously differentiable function on some closed interval.

Expanding \( x(t+jT) \) and \( \dot{x}(t+jT) \) as Taylor series about \( t \), and grouping similar terms yield:

\[ L[x(t),T] = C_0 x(t) + C_1 T x(t) + \ldots + C_q T^q x^q(t) \ldots . \]  

(3)

where \( C_q : q=0,1,2,\ldots \) are constants, and \( x^q(t) \) refers to the \( q \)th derivative of \( x(t) \).

The integrator of equation (1) is said to be of order \( p \) if the \( C_i \) coefficients are such that \( C_i : i=0,1,2,\ldots, p \) are all zero and \( C_{p+1} \neq 0 \). Clearly, knowledge of the \( C_i \)'s allows the derivation of linear multistep methods of a given order and structure. It turns out that the order of accuracy of the integrator is the same as the order of the operator \( L[.\] \) of equation (3). Notice that this order is precisely the number of constants \( C_i \) which are identically zero. From equation (3) it is possible to determine expressions for the constants \( C_i \) as follows:

\[ C_0 = a_0 + a_1 + a_2 + \ldots + a_r \]

\[ C_1 = a_1 + 2a_2 + \ldots + ra_r - (b_0 + b_1 + b_2 + \ldots + b_r) \]

\[ C_q = \frac{1}{(a_1 + 2q a_2 + \ldots + r^q a_r)(b_1 + 2q^{-1} b_2 + \ldots + r^{q-1} b_r)} \]  

\( q=2,3,\ldots \)  

(4)

B. EULER'S METHOD

Euler's method can be easily derived by letting \( r=1 \) in equation (1); that is, a one step method. Then equation (1) implies that:

\[ a_0 x_k + a_1 x_{k+1} = b_0 T \dot{x}_k + b_1 T \ddot{x}_{k+1} . \]  

(5)

Using the expressions (equation (4)) for the \( C_i \)'s it follows that:

\[ C_0 = a_0 + 1 \]  

(recall that \( a_r = a_1 = 1 \)) \Rightarrow \[ C_0 = 0 \] \text{if } \[ a_0 = -1 \]

\[ C_1 = 1 - b_0 - b_1 \] \Rightarrow \[ C_1 = 0 \] \text{if } \[ b_0 = 1 \] (recall that \( b_r = b_1 = 0 \) for an explicit method)

\[ C_2 = 1/2 - b_1 \] \Rightarrow \[ C_2 = 1/2 \] since \( b_1 = 0 \).
Then, substituting these values into equation (5) yields the already familiar Euler's integration method:

\[
x_{k+1} = x_k + T \dot{x}_k = \frac{T}{z-1} H(z) .
\]  

Clearly, Euler's method is only first order accurate as \( C_0 \) and \( C_1 \) are both zero while \( C_2 \) is different from zero.

C. ADAMS-BASHFORTH TWO STEP METHOD (AB-2)

Following the procedure just used to derive Euler's method, an AB-2 integrator can be obtained by letting \( r=2 \) in equation (1) and solving equation (4) for the appropriate \( C_i \)'s; that is,

\[
a_0 x_k + a_1 x_{k+1} + a_2 x_{k+2} = T b_0 \dot{x}_k + T b_1 \dot{x}_{k+1} + T b_2 \dot{x}_{k+2} .
\]

\( C_0 = a_0 + a_1 + a_2 \) (recall that \( a_r = a_2 = 1 \))

\( C_1 = a_1 + 2a_2 - b_0 - b_1 - b_2 \) (recall that \( b_r = b_2 = 0 \) for an explicit method)

\( C_2 = 1/2 (a_1 + 4a_2) - (b_1 + 2b_2) \)

\( C_3 = 1/6 (a_1 + 8a_2) - 1/2 (b_1 + 4b_2) \)

Substituting \( a_2 = 1 \) and \( b_2 = 0 \) in these equations gives:

\( C_0 = a_0 + a_1 + 1 = 0 \)

\( C_1 = a_1 + 2 - b_0 - b_1 = a_1 + 2 - b_0 - b_1 = 0 \)

\( C_2 = 1/2 (a_1 + 4) - b_1 = (a_1/2) + 2 - b_1 = 0 \Rightarrow a_1 = -4 + 2b_1 \)

\( C_3 = 1/6 (a_1 + 8) - 1/2 b_1 \)

Solving the resulting set of equations yields the following values: \( a_0 = 0, a_1 = -1, b_0 = -0.5, b_1 = 1.5 \), and \( C_3 = 5/12 \). Therefore, the two-step Adams-Bashforth (AB-2) integration method can be written as:

\[
x_{k+2} = x_{k+1} + T(1.5\dot{x}_{k+1} - 0.5\dot{x}_k) = \frac{T(1.5z-0.5)}{z^2-z} \; H(z) .
\]

Clearly, AB-2 is second order accurate as \( C_0, C_1, \) and \( C_2 \) are zero while \( C_3 \) is nonzero. This implies that for a given timestep \( T \) AB-2 will result in a more accurate simulation than Euler's method.

D. CHARACTERISTICS OF LINEAR MULTISTEP METHODS

Two important concepts associated with linear multistep integrators are the concepts of consistency and zero stability. A
A linear multistep method is said to be consistent if it has order greater or equal to one \((l)\). Zero stability is defined via two polynomials. These polynomials are usually referred to as the first and second characteristic polynomials, and are given as:

\[
\rho(\tau) = \sum_{j=0}^{n} a_j \tau^j, \text{ referred to as the first characteristic polynomial}
\]

\[
\sigma(\tau) = \sum_{j=0}^{n} b_j \tau^j, \text{ referred to as the second characteristic polynomial}
\]

The method is said to be consistent if the first characteristic polynomial always has a root at \(+1\). The method is said to be zero-stable if the roots of the first characteristic polynomial \(\rho(\tau)\) lie on or inside the unit circle with any root on the unit circle being simple. And the method is convergent if and only if it is consistent and zero-stable.

**E. STABILITY REGION OF AN INTEGRATOR**

Another important concept in the analysis of linear multistep methods is that of stability region. Essentially, the stability region of an integrator is that region where the \(\lambda T\)-product should lie in order for the simulation to be stable. Within this region the degree of accuracy of the simulation changes depending on where the \(\lambda T\)-product is located. Thus, when designing integrators for a specific application it is important to use the integrator's stability region as a criterion for determining the maximum allowable timestep \(T\). This will not only guarantee a stable simulation but also an accurate one. To determine the stability region of a given integrator it is expedient to work in the frequency domain. Hence, consider the Z-transform of equation (1):

\[
\left[ \sum_{j=0}^{\infty} a_j z^j \right] X(z) = \left[ T \sum_{j=0}^{\infty} b_j z^j \right] \dot{X}(z)
\]

\[
\rho(z) X(z) = T \sigma(z) \dot{X}(z)
\]

From this equation it follows that the open loop transfer function of the integrator is:

\[
X(z) = \frac{T \sigma(z)}{\rho(z)} \dot{X}(z)
\]

Now, the frequency response of the integrator is obtained by replacing \(z\) by \(\exp(j\omega T)\); that is,

\[
z = e^{j\omega T}
\]
The performance of the integration process on an actual dynamic system is determined using closed loop stability analysis. This closed loop stability analysis is accomplished by introducing the linear test equation:

$$\dot{x} = \lambda x + u$$

$$\Rightarrow \dot{X}(z) = \lambda X(z) + U(z)$$  \hspace{1cm} (11)

To close the loop substitute the above linear test equation into equation (8) to yield the closed loop transfer function, viz.

$$\rho(z)X(z) = T\sigma(z)[\lambda X(z) + U(z)]$$

$$\Rightarrow X(z) = \frac{T\sigma(z)}{\rho(z) - \lambda T\sigma(z)} U(z)$$  \hspace{1cm} (12)

Clearly, the stability of the integrator is determined by the poles of the closed loop transfer function of equation (12); that is, the root of the equation:

$$\rho(z) - \lambda T\sigma(z) = 0$$  \hspace{1cm} (13)

Notice that in equation (13) the product $\lambda T$ can be thought of as the gain of the closed loop system. Thus, a root locus can be plotted. Therefore, it is always possible to determine the region of the $\lambda T$-plane where the integration is stable by considering the expression:

$$\frac{\rho(z)}{\sigma(z)}$$  \hspace{1cm} (14)

Hence, mapping the $z$-plane unit circle into the $\lambda T$-plane the stability region of the integrator can be obtained, viz.

$$z^n = e^{jn\theta} = \cos(n\theta) + jsin(n\theta)$$  \hspace{1cm} (15)

The stability regions corresponding to Euler's method (AB-1) and AB-2 method are shown in Figures 1 and 2. For a given integrator the simulation will be stable provided that the $\lambda T$-product is inside the integrator's stability region. For the simulation to be accurate, the $\lambda T$-product should be within the region where the "squares" are the least distorted. Notice that although Euler's integrator has a larger stability region, it requires very small timesteps in order to produce an accurate simulation (The $\lambda T$-product should lie within the squares that are closest to the origin). This is especially the case when the systems being integrated have eigenvalues of large magnitude. This problem is further aggravated by situations where the eigenvalues of the system under consideration are complex with large imaginary parts relative to the real parts. As the stability region of Euler's method touches only the origin of the $\lambda T$-plane, it is almost impossible to guarantee that the timestep $T$ can be chosen small enough so that the
λT-product lies inside the stability region. In sharp contrast, the stability region of AB-2, although smaller than that of Euler's method, allows the use of larger timesteps with improved accuracy. Moreover, the problem associated with large complex eigenvalues is alleviated due to the fact that AB-2's stability region is asymptotic to a larger portion of the imaginary axis of the λT-plane. Thus, it can be said that although Euler's method is simple to use and implement, care must be exercised when choosing the integration timestep to guarantee a stable and accurate simulation. It should be pointed out that AB-2 integrators do not provide a significant improvement over Euler's method in situations such as those just mentioned. However, using AB-2 it is possible to improve running times by a factor of about five with improved or comparable accuracy.

Figure 1. Stability Region of Euler's Method (AB-1)
Figure 2. Stability Region of AB-2
F. MODIFIED ADAMS-BASHFORTH TWO STEP METHOD (MAB-2)

To obtain more stable and accurate simulations of systems whose eigenvalues are complex with large imaginary parts relative to their real parts a modified AB-2 method can be used. This modified method can even be used in situations where purely imaginary roots are to be stably integrated [3]. The modification of AB-2 is possible due to the flexibility presented by the $C_i$'s of equation (4). Notice that this flexibility is greatly reduced if it is demanded that the integration method be of maximal accuracy (that is, that as many $C_i$'s as possible be set to zero). However, if accuracy requirements can be relaxed, then the extra freedom that is gained can be used to tailor the integration method to the particular system's dynamics. In this case it is desired to modify the AB-2 method so that the imaginary axis is just enclosed by the stability region of the new integrator.

Recall that AB-2 is second order accurate. This implies that $C_0$, $C_1$, and $C_2$ are all equal to zero while $C_3$ is different from zero ($C_3=5/12$). Recall further that, for a two step explicit method, the $C_i$'s satisfy the following set of equations:

\begin{align*}
C_0 &= a_0 + a_1 + 1 \\ 
C_1 &= a_1 + 2 - b_0 - b_1 \\ 
C_2 &= 1/2a_1 + 2 - b_1 \\ 
C_3 &= 1/6a_1 + 4/3 - 1/2b_1
\end{align*}

Next, suppose that the order of accuracy is relaxed so that only $C_0$ and $C_1$ are required to be zero. Since there are three equations in four unknowns (the equation involving $C_3$ does not count in this case) it follows that there are two free parameters. Without loss of generality these free parameters can be chosen to be $a_0 = \alpha$ and $b_0 = \beta$. Since $C_0$ and $C_1$ are both zero, equation (16) can be solved for $a_1$ and $b_1$ to yield the modified AB-2 integrator (MAB-2), viz.

\begin{align*}
\dot{x}_{k+2} &= (\alpha+1)x_{k+1} - ax_k + T(1-\alpha-\beta)[\dot{x}_{k+1} + \beta/(1-\alpha-\beta)\dot{x}_k] \\
H(z) &= \frac{T(1-\alpha-\beta)[z+\beta/(1-\alpha-\beta)]}{z^2 - (1+\alpha)z + \alpha}
\end{align*}

The transfer function of the MAB-2 integrator (equation (17)) is:

Notice that equation (17) is indeed the transfer function of an integrator. This is seen once it is realized that the poles of equation (18) are located at $z=1$ and $z=\alpha$. It should be kept in mind that the pole at $z=\alpha$ must lie inside the unit circle to maintain open loop stability. Therefore, $\alpha$ is allowed to vary between $+1$ and $-1$. Notice as well that the zero of equation (18) lies at $z=\beta/(1-\alpha-\beta)$. The flexibility offered by the arbitrary location of this zero allows an entire family of integrators to be generated for different pole locations. It turns out that setting $\alpha$ to zero and $\beta$ to $-0.6$ results...
in an integrator whose stability region closely approximates that of AB-2. The only difference between the stability regions of MAB-2 and AB-2 is that the stability region of MAB-2 just encloses the imaginary axis of the $\lambda T$-plane. Thus, allowing systems with complex poles and purely imaginary poles to be stably simulated. The actual integrator and corresponding transfer function are given as:

$$x_{k+2} = x_{k+1} + T(1.6x_{k+1} - 0.6x_k) = H(z) = \frac{T(1.6z-0.6)}{z^2-z}.$$  \hspace{1cm} (19)

The difference between the stability region of AB-2 and the stability region of MAB-2 can be clearly seen from Figure 3. Although these stability regions are almost identical, there are several important points to be noticed. The stability region of MAB-2 is slightly shifted to the right of the $\lambda T$-plane and thus it encloses the $j\omega$-axis of this plane. The portion of the stability region where the $\lambda T$-product gives an accurate and stable simulation is slightly distorted relative to the corresponding region for an AB-2 integrator. This implies that MAB-2 is not as accurate as AB-2. This should not come as a surprise as MAB-2 was derived assuming that accuracy could be traded off with the ability to stably integrate systems with either purely imaginary eigenvalues or eigenvalues with large imaginary parts. However, in actuality MAB-2 is expected to produce as good a simulation as AB-2. The reason for this being that the level of distortion of the stable and accurate region of MAB-2 is not too severe. This can be easily seen by considering the $C_i$ coefficients. Recall that these coefficients determine the order of accuracy of the integration method. Some simple arithmetic gives that for MAB-2 these coefficients are $0, 0, -0.1, \text{ and } 11/30$ corresponding to $C_0, C_1, C_2, \text{ and } C_3$ respectively. A comparison of these values with those of AB-2 is given in Table 1 below.

<table>
<thead>
<tr>
<th>$C_i$ Coefficient $a_r=1 b_r=0$</th>
<th>Integration Method</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>AB-1</td>
</tr>
<tr>
<td>$C_0=a_0+a_1+a_2$</td>
<td>0</td>
</tr>
<tr>
<td>$C_1=a_1+2a_2-b_0-b_1-b_2$</td>
<td>0</td>
</tr>
<tr>
<td>$C_2=1/2a_1+2a_2-b_1-2b_2$</td>
<td>1/2</td>
</tr>
<tr>
<td>$C_3=1/6a_1+8/6a_2-1/2b_1-2b_2$</td>
<td>*</td>
</tr>
</tbody>
</table>

| Order of Accuracy | first | second | first |

Notice that although MAB-2 is first order accurate, the difference between the $C_i$'s for MAB-2 and the $C_i$'s for AB-2 is rather small. Thus, MAB-2 should perform almost as well as AB-2.
Figure 3. Stability Regions of AB-2 (top) and MAB-2 (bottom)
G. TWO STEP MATRIX INTEGRATORS (MSRP-2)

In this section the two step matrix integrator (MSRP-2) presented in [4] is reviewed. This method is the generalization of the method of [5] to vector systems of differential equations. It is shown that this type of integrators can be very useful in the real-time simulation of stiff systems. The material presented in this section is essentially that of [4] however.

When performing numerical integration it is important to maintain the overall system transient response while the integration operator maintains the character of an integrator. This is normally done by deriving integrators that reproduce the transient response better as the timestep goes to zero [5]. However, for a specific system, the SRP method derives an integrator that improves the transient response for a given nonzero timestep.

The SRP method has the minimum number of coefficients necessary to maintain both the transient response and the integration property for a scalar system, while also allowing arbitrary choice of timestep [5]. MSRP-2 extends the SRP method to vector systems.

The linear MSRP-2 integrator can be written as:

\[ x_{k+2} = -A_1 x_{k+1} - A_0 x_k + T(B_1 x_{k+1} + B_0 x_k) \]  \hspace{1cm} (20)

where \( T \) is the integration timestep, \( kT \) is the time, \( x \) is the \( n \)-dimensional state vector at time \( t \), and \( A_i \) and \( B_i : i=0,1 \) are the \( n \times n \) regression coefficient matrices.

As in the general linear multistep method, the performance of MSRP-2 is evaluated using a linear test equation of the form:

\[ \dot{x}_k = Jx_k + Gu_k \]  \hspace{1cm} (21)

where, \( u \) is an \( m \)-vector of input functions, and \( J \) and \( G \) are the system and input matrices, respectively.

To close the loop substitute equation (21) into equation (20) to yield a closed-loop discrete-time linear system, viz.

\[ x_{k+2} = -A_1 x_{k+1} - A_0 x_k + T(B_1 Jx_{k+1} + B_0 Jx_k) + T(B_1 Gu_{k+1} + B_0 Gu_k) \]  \hspace{1cm} (22)

Notice that this system is \( 2n \)-dimensional and thus has \( 2n \) eigenvalues. The \( n \) principal roots are those corresponding to the mappings of the eigenvalues of \( J \). The remaining \( n \) roots are due to the fact that the first order differential equation (21) is being replaced by a second order difference equation (21). These roots are spurious roots and act as noise sources in the simulation. It is clear that the location of the \( 2n \) eigenvalues of the system of (22) determines the stability of the integration process. Taking the \( z \)-transform of equation (22) yields:

\[ [z^2 I + (A_1 -TB_1 J) z + (A_0 -TB_0 J)] X(z) = [B_1 z + B_0] TGU(z) \]  \hspace{1cm} (23)
The transfer function matrix (TFM) $H(z)$ of the system of (23) is:

$$H(z) = \left[ z^2 I + (A_1 - TB_1 J) z + (A_0 - TB_0 J) \right]^{-1} \left[ B_1 z + B_0 \right] T G .$$  \hspace{1cm} (24)

Recall that the regression coefficients $(A_i, B_i : i=0,1)$ are square $n \times n$ matrices. Therefore, there are $4n^2$ unknowns to be determined which place the $2n$ eigenvalues of equation (24). It is clear that the poles of the resulting closed-loop system can be arbitrarily placed in an infinite number of locations. The problem is how to determine the regression coefficients $A_i$ and $B_i : i=0,1$ so that the system transient response is maintained while still having equation (20) perform as an integrator.

To solve the first problem, place the $n$ principal roots at the exact $z$-plane mapping of the eigenvalues of $J$, that is, the usual discrete-time system matrix $e^{JT}$. To guarantee the accuracy of the method, place the $n$ spurious roots as close to the origin in the $z$-plane as possible [4]-[5]. This pole assignment requires that $A_i$ and $B_i : i=0,1$ satisfy the following matrix equations:

$$A_i - TB_i J = -e^{JT} . \hspace{1cm} (25a)$$

$$A_0 - TB_0 J = 0 , \text{ where } 0 \text{ is the } n \times n \text{ null matrix}. \hspace{1cm} (25b)$$

Note that there are $2n^2$ equations and $4n^2$ unknowns. Therefore, more constraints are required. The remaining $2n^2$ constraints are obtained by forcing equation (20) to act as an integrator. Recall that for a linear multistep method, and thus MSRP2, to be convergent it is necessary and sufficient that the method be consistent and zero-stable. Equivalently, the steady state gain of the discrete-time system should be that of the continuous-time system, and an open-loop integrator pole should be at $Z=+1$, respectively. Algebraically, these constraints can be written, again respectively, as (see [4]):

$$A_i - B_0 - B_i = -2I , \text{ where } I \text{ is the } n \times n \text{ identity matrix}. \hspace{1cm} (26a)$$

$$I + A_0 + A_i = 0 . \hspace{1cm} (26b)$$

It is shown in [5] that these constraints imply that the integrator is first order accurate.

Equations (25a)-(26b) provide $4n^2$ equations to be solved for the $4n^2$ unknowns of the $A_i$'s and $B_i$'s. Provided that $J$ is invertible (for the case when $J$ has zero eigenvalues refer to [6]), this set of equations can be solved using linear algebra techniques as follows:

$$\begin{bmatrix}
I & I \\
\vdots & \vdots \\
-(JT)^{-1} & I - (JT)^{-1} \\
\end{bmatrix}
\begin{bmatrix}
A_0 \\
A_1 \\
\end{bmatrix}
= \begin{bmatrix}
-I \\
-e^{JT} (JT)^{-1} - 2I \\
\end{bmatrix}. \hspace{1cm} (27a)$$

Postmultiplying the first row of this equation by $(JT)^{-1}$ and adding the result to the second row yields:
From this equation it is seen that $A_1$ and $A_2$ are given as:

$$A_1 = e^{JT} (JT)^{-1} - (JT)^{-1} - 2I .$$

$$A_0 = -e^{JT} (JT)^{-1} + (JT)^{-1} + I .$$

While the $B_i$'s follow directly from the $A_i$'s as:

$$B_1 = [A_1 + e^{JT}] (JT)^{-1} .$$

$$B_0 = A_0 (JT)^{-1} .$$

The above expressions for the $A_i$'s and $B_i$'s can be easily computed using a software package such as PC-Matlab [7] by inputting $T$ and $J$.

Using equations (25a)-(26b) in conjunction with the regression coefficients, a state space representation for $H(z)$ can be written as:

$$x(k+1) = x(k) + T_0^G \cdot U(k) = x(k+1) = Ax(k) + Bu(k)$$

$$y(k) = 0 \cdot I \cdot x(k) = x_2(k) = x_k .$$

Notice that this is the well known observable canonical form. Thus, using MSRP-2 it is always possible to recover the state of the system being integrated as this representation is guaranteed to be observable.

The integration method just presented can also be implemented using recursive identification of $J$ and $G$ to adaptively determine the regression coefficients. However, this variant of the method will not be considered here as it is believed that due to the nature of the SSME simulation this method will not provide any significant speedup. The main reason being the computational burden associated with the identification and updating required per time step. Moreover, at present there are no numerically reliable techniques for updating the matrix exponential on-line.

**H. COMPUTATIONAL ASPECTS OF LINEAR MULTISTEP METHODS**

In this section some computational aspects of linear multistep methods are considered. It is important to realize, however, that
while Euler's method, AB-2, and MAB-2 are localized integrators, in MSRP-2 the integrators are no longer localized, that is, one per system state. As a consequence, the computational burden associated with matrix integration increases rapidly with the number of states (approximately $4n^2$ multiplies in addition to the derivative function evaluation). Therefore, it is necessary that techniques for reducing the number of computations be considered. Also, a detailed analysis of the computational burden associated with MSRP integrators is in order. These are the major topics of this section.

Before proceeding further it should be mentioned that comparisons among integrators and numerical details of the different algorithms being used will be done using the number of floating point operations (flops) of each algorithm. A flop is approximately the amount of work involved in a floating point add, a floating point multiply, and the required subscripting [8]. In mathematical terms, this is equivalent to the amount of work associated with the following statement:

$$s:=s+a_k b_{kj}.$$

which in terms of the well-known Fortran computer language can be written as:

$$S=S+A(I,K)*B(K,J).$$

### H.1. Computational Cost Associated with AB-1, AB-2, and MSRP-2

Regarding the real-time simulation methods considered here, the bulk of the computations results from products of the type $Ax$, where $A$ can be either an $n \times n$ or an $n \times m$ matrix and $x$ is either an $n$-dimensional or an $m$-dimensional vector, accordingly. It is not hard to see that when $A$ is an $n \times n$ matrix, the product $Ax$ requires $n^2$ flops. On the other hand, when $A$ is $n \times m$ this product can be performed in $nm$ flops. The amount of work associated with multiplying a given vector by a scalar quantity requires approximately $n$ flops. At this time, it is important to point out that these flop counts are simply rough approximations that are used by computer theorists in an effort to acknowledge the countless operations that take place during program execution (paging, subscripting, etc.). The approximate number of flops required by AB-1, AB-2 (MAB-2), and MSRP-2 for every timestep is given in Table 2.

It is clear from this table that while Euler's method and AB-2 (MAB-2) cost about the same, MSRP-2 requires approximately 5 times more computations than either one of them. Therefore, to break even, the timestep for MSRP-2 must be at least 5 times that of either Euler's method or AB-2 (MAB-2). Letting the timestep for either one of the latter methods be the normal timestep, the speedup factor is:

$$\text{speedup} = \frac{T_{MSRP-2}}{5T_{NORMAL}}.$$
Therefore, MSRP-2 can be made more numerically efficient than either Euler's method or AB-2 (MAB-2) provided that the timestep for MSRP-2 is chosen appropriately. This is clearly illustrated by the results obtained in the simulation of the valve dynamics module using these integration methods (more about this later).

Table 2. Computational cost associated with AB-1, AB-2, and MSRP-2

<table>
<thead>
<tr>
<th>Required Operations (real-time)</th>
<th>Number of Flops</th>
<th>Total Number of Flops</th>
</tr>
</thead>
<tbody>
<tr>
<td>Linear test equation</td>
<td>n²+nm</td>
<td>n²+nm</td>
</tr>
<tr>
<td>( \dot{x} = Jx + Gu )</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Euler's (AB-1)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>( x_{k+1} = x_k + T\dot{x}_k )</td>
<td>n</td>
<td>n²+n+m</td>
</tr>
<tr>
<td>AB-2 (MAB-2)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>( x_{k+2} = x_{k+1} + T(1.5\dot{x}_{k+1} - 0.5\dot{x}_k) )</td>
<td>2n</td>
<td>n²+2n+nm</td>
</tr>
<tr>
<td>MSRP-2</td>
<td></td>
<td></td>
</tr>
<tr>
<td>( x_{k+2} = -A_1 x_{k+1} - A_0 x_k + T(B_1 \dot{x}_{k+1} + B_0 \dot{x}_k) )</td>
<td>4n²</td>
<td>5n²+nm</td>
</tr>
</tbody>
</table>

It should be pointed out that the comparison established in Table 2 above is based on the assumption that a linear system is being integrated. For nonlinear systems the computational burden is usually much larger. Thus, MSRP-2 is expected to provide better results with a timestep less than five times the timestep of either Euler's method or AB-2 (MAB-2).

H.2. IMPLEMENTATION OF MSRP-2

In Table 1 above the approximate flop count for MSRP2 is given assuming that the integration is performed using the original system. However, in an effort to reduce the number of computations in real-time, it is always possible to first transform the coordinates of the original system. This transformation can be done off-line and the results stored. Then the integration process can be carried out on the resulting system. Of special interest here are transformations which yield diagonal or Jordan, Schur, and Hessenberg forms of the original system matrix J. The diagonal form gives essentially the classical linear multistep method, that is, one integrator per system state. It is important to keep in mind that, although this may seem
appropriate, computing the diagonal form of a matrix is, in general, not a numerically reliable process. This is especially the case when the matrix being diagonalized has repeated eigenvalues [8]. In contrast, The well-known Schur and Hessenberg decompositions of a matrix are easily obtained via orthogonal transformations. Since orthogonal matrices are perfectly conditioned, these decompositions are considered to be very stable and numerically robust [8]. Furthermore, both Schur and Hessenberg decompositions of a matrix result in quasi-triangular forms. Thus, it is possible to reduce the number of on-line computations during the integration process by using these matrix decompositions. These approaches are considered next in what follows.

The first approach consists of transforming the initial system to either diagonal or Jordan co-ordinates, then performing the integration process. Recall that, in general a diagonal form results when the system poles are all distinct, while a Jordan form results when the system has multiple poles. As the regression coefficients of MSRP-2 are a function of \((JT)^{-1}\) and \(e^{JT}\), and as these functions of \(J\) have a triangular structure whenever \(J\) is in Jordan form, and finally, as the Schur and Hessenberg forms of \(J\) are also triangular matrices, the case when \(J\) is in Jordan form is considered a part of the approach in which the \(A,\)'s and \(B,\)'s are triangular matrices.

The foregoing indicates that localized integrators can only be obtained provided \(J\) is diagonalizable. Recall that diagonalizing a matrix involves determining its eigenstructure. Further, recall that \(J\) is, in general, an unsymmetric matrix. In the usual situation, the standard procedure to diagonalize an unsymmetric matrix involves three steps. First, the matrix is reduced to upper Hessenberg form using Householder transformations. Then the Q-R algorithm is used to produce the upper real Schur form of the matrix resulting from step one to yield \(H=Q'JQ\) (\(Q'\) is the transpose of \(Q\)). These two steps require about \(15n^3\) flops [8] (this includes the computation of both \(Q\) and \(H\)). Finally, to obtain the diagonal form of \(J\), a block diagonalization method requiring approximately \(n^3\) extra flops is used. Therefore, the diagonalization of \(J\) can be accomplished in about \(16n^3\) flops.

Having determined the eigenstructure of \(J\), a transformation matrix whose columns are the eigenvectors of \(J\) can be formed and its inverse computed off-line and stored. The latter computation is usually done via the singular value decomposition method, thus requiring about \(7n^3\) flops [8]-[9]. Then this transformation matrix is used to transform the system of (21) into diagonal coordinates. This process is given in what follows, assuming that the original system is that of equation (21); that is,

\[
\dot{x}_k = Jx_k + Gu_k.
\]  

(34)

First, let \(P\) be the matrix whose columns are the eigenvectors of \(J\). Then it follows that \(P^{-1}JP=\Lambda\), where \(\Lambda\) is a diagonal matrix with the eigenvalues of \(J\) along its main diagonal. Next, use \(P\) as a coordinate transformation matrix to obtain localized integrators, viz.
At this point it only remains to carry out the integration process, using one integrator per system state, as follows:

\[ z_{k+2} = -a_{1z} z_{k+1} - a_{10} z_{k} + T[b_{1z} z_{k+1} + b_{10} z_{k}] \]

for \( i=1,2,3,\ldots,n \).

As a last step, use \( P \) to determine the state vector, \( x \), in the original set of coordinates by transforming the state vector \( z \) obtained from the integration process, viz.

\[ x_{k+2} = P z_{k+2} \]

This completes the first approach of diagonalization and integration. It is worth mentioning at this point that determining the \( a_i \)'s and \( b_i \)'s requires approximately \( 4n \) flops. However, these computations are done prior to the actual run and the results are stored. Therefore, the total number of off-line computations is \( 23n^3 + 4n \) flops. Also, notice that, when \( J \) is diagonal, the total number of flops required per timestep is \( 4n^2 + (4+m)n \). Of this total, the function evaluations of equation (34) constitute the bulk of the computations, that is, \( n^2 + nm \) flops. The coordinate transformations of equation (35) require \( n^2 \) flops each for \( z \) and its derivative. Finally, the computations of equation (36) represent a total of \( 4n \) flops, while the transformation of equation (37) requires \( n^2 \) extra flops.

The second approach, or triangular approach, consists on reducing the original system matrix \( J \) to an upper quasi-triangular form. There are several methods to do this. One of these methods involves using a sequence of Householder transformations to reduce the system matrix \( J \) to its upper Hessenberg form. Equivalently, determine \( U \) and \( H \) such that \( H = U'JU \), where \( U \) (orthogonal) is a product of Householder matrices and \( H \) is upper Hessenberg, that is, \( h_{ij} = 0 \) whenever \( i > j+1 \). This process requires \( (7/3)n^3 \) flops [8]. A second method is to compute the Schur decomposition of \( J \), that is, determine an orthogonal matrix \( U \) such that \( H = U'JU \), where each \( H_i \) is either a scalar or a \( 2 \times 2 \) matrix having complex conjugate eigenvalues. This decomposition can be done using the Q-R algorithm in approximately \( 15n^3 \) flops [8]. At this point it is important to mention that these two processes are very numerically stable.

The third and last approach considers the Jordan reduction of \( J \). As mentioned before, the Jordan form of a matrix can be obtained in approximately \( 16n^3 \) flops. However, it should be emphasized that this reduction is, in general, ill-conditioned. A common aspect among these three methods is that they all yield upper quasi-triangular integrator coefficients. Thus, the total number of on-line computations...
decreases as compared to the number of computations required for the unreduced system. However, there might be an increase in the total number of off-line computations. This is seen by considering the amount of work involved in determining the $A_i$'s and $B_i$'s. A detailed description of this process is given next as follows.

As just mentioned, the latter three methods being considered here for reducing the number of computations of the integration process all result in upper quasi-triangular matrices. Therefore, without loss of generality, the number of flops required to compute each integrator coefficient is given next assuming that these coefficients are strictly upper triangular matrices.

For simplicity, the expressions for the $A_i$'s and $B_i$'s for MSRP-2 are repeated here as a function of $H$ the corresponding form of $J$, viz.

$$A_1 = e^{HT}(HT)^{-1} - (HT)^{-1} - 2I$$
$$A_0 = -e^{HT}(HT)^{-1} + (HT)^{-1} + I$$
$$B_1 = e^{HT}(HT)^{-1} + A_1(HT)^{-1}$$
$$B_0 = A_0(HT)^{-1}.$$  \tag{38}

1. Computation of $e^{HT}$: The matrix exponential is usually computed using Pade approximations. Although the number of flops for this algorithm is a function of $||H||_\infty$, a typical number is somewhere between $8n^3$ and $10n^3$ flops. However, since $H$ is upper triangular, only about $6n^3$ flops are required \cite{8}.

2. Computation of $(HT)^{-1}$: This matrix inversion can be done via the singular value decomposition of $H$. From \cite{9}, this algorithm takes about $5n^3$ flops for an upper triangular matrix.

3. Computation of matrix products: All the required matrix products involve only upper triangular matrices. Therefore, these products require only $(1/6)n^3$ flops each \cite{8}.

From the foregoing it is seen that once that $e^{HT}$ and $(HT)^{-1}$ have been determined and the results stored, the integrator coefficients can be computed in approximately $(1/2)n^3$ flops. Notice that in this process the product $e^{HT}(HT)^{-1}$ is computed only once and then stored.

The approximate flop counts just given are only for those operations which can be done off-line. Therefore, it still remains to consider the number of on-line computations required per timestep. These computations include the function evaluations of equation (34), the state vector coordinate transformations of equations (35)-(36), and the integration process of equation (20) with the coefficients replaced by the matrices of equation (38). As in the case when $J$ is diagonalizable, the function evaluations and coordinate transformations require $4n^2 + nm$ flops. Each of the products in the integration process requires $(1/6)n^2$ flops, for a total of $(2/3)n^2$ flops. Therefore, when the integrator coefficients are upper
triangular, the total number of on-line computations can be approximated to \((14/3)n^2 + nm\) flops. Notice that this flop count compares very favorably with that of the case when \(J\) is diagonalized. At the same time, however, this flop count is very close to the one obtained when the original system is used in the integration. That is, \(5n^2 + nm\) flops. For ease of comparison, the results just given in the paragraphs above are compiled in Tables 3 and 4 below. The quantities inside the round brackets in these tables indicate the number of times a particular operation is done.

Table 3. Off-line computational cost associated with MSRP-2

<table>
<thead>
<tr>
<th>Required Operations</th>
<th>System Matrix J (Computational Cost in Flops)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Original</td>
</tr>
<tr>
<td>Coordinate X-formation</td>
<td>0</td>
</tr>
<tr>
<td>Matrix Inversion</td>
<td>7(n^3)</td>
</tr>
<tr>
<td>Matrix Exponential</td>
<td>10(n^3)</td>
</tr>
<tr>
<td>Matrix Product</td>
<td>3(n^3)</td>
</tr>
<tr>
<td>Off-line Computation</td>
<td>20(n^3)</td>
</tr>
</tbody>
</table>

Table 4. On-line computational cost associated with MSRP-2

<table>
<thead>
<tr>
<th>Required Operations</th>
<th>System Matrix J (Computational Cost in Flops)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Original</td>
</tr>
<tr>
<td>Function Evaluations</td>
<td>(nm+n^2)</td>
</tr>
<tr>
<td>Coordinate X-formation</td>
<td>0</td>
</tr>
<tr>
<td>Integration Process</td>
<td>4(n^2)</td>
</tr>
<tr>
<td>On-line Computation</td>
<td>(nm+5n^2)</td>
</tr>
</tbody>
</table>
From these tables it is clear that transforming the original system to upper Hessenberg form prior to performing the integration process requires the least number of off-line computations, while the number of on-line computations compares well with that of the case when the original J matrix is used. This, coupled with the fact that the Hessenberg decomposition of a matrix can be obtained via orthogonal transformations, makes this approach highly desirable. Moreover, the excellent numerical properties of this decomposition guarantees the reliability of the computations.

Notice that although diagonalizing J requires the least on-line computational effort, it should be kept in mind that, in general, not all matrices are diagonalizable and that this process can be numerically ill-conditioned. However, matrix diagonalization is a common practice in actual applications.

Associated with specific hardware and software implementations there are several aspects of MSRP that should be emphasized. As MSRP-2 only involves adds and multiplies, and as most hardware and software packages support these two basic arithmetic operations, MSRP-2 allows real-time simulation on a wide variety of computer systems and software packages. Therefore, the usual constraints associated with the real-time simulation of physical systems are no longer encountered when using MSRP-2 integrators. It should be realized, however, that although MSRP-2 allows timesteps much larger than would be normally possible, the hardware which is attached to the simulator may restrict the stepsize. Hence, the only constraining factors in real-time simulation using MSRP-2 are those due to hardware constraints.

MSRP-2 can be implemented in three steps. The first step consists of obtaining the computation time for the given system. The second step involves choosing the desired timestep T. And the third step designing MSRP-2 by solving for the integrator coefficients using the appropriate formulas.
In the SSME simulation numerical integration is done using Euler's method. This method is very attractive because of its simplicity and ease of implementation. However, care must be exercised in selecting the appropriate integration timestep. This is important since the stability and accuracy of the simulation are a direct function of the integration timestep. It is shown here that a faster and more accurate simulation of the SSME can be obtained by replacing Euler's integrators by a two step method. More specifically, the Valve Dynamics and the Oxidizer Turbopump modules are used as case studies to demonstrate that it is possible to speed up the SSME simulation without requiring additional hardware.

This chapter is organized as follows. First a brief description of the valve dynamics module is given. Then, the results obtained from simulating this module using Euler's method, and AB-2 and MSRP-2 integrators are presented. This is followed by a brief review of the oxidizer turbopump module along with some recommendations to provide a faster simulation.

A. VALVE DYNAMICS MODULE: CASE STUDY I

To throttle the SSME there are a total of five control valves. These valves are:

- MFV - Main Fuel Valve
- MOV - Main Oxidizer Valve
- FPV - Fuel Preburner Valve
- OPV - Oxidizer Preburner Valve, and
- CCV - Coolant Control Valve

These five valves reside in the valve dynamics module of the SSME simulation. Figure 4 shows the block diagram for valve position control, and Figure 5 gives the fortran code for the main integration loop of the valve dynamics module. From these figures it is seen that position control of each valve is described by a 6th order system. Moreover, the valve position control system is linear within the integration timestep as the nonlinearities (stiction, backlash, and wind-up) introduced by valve linkage remain constant within the integration loop. Notice that multirate sampling is used as the outer timestep $DT=2\times10^{-4}$ is added to $10^{-5}$ and divided by $\Delta t=2\times10^{-5}$. Some simple arithmetic shows that the timestep being used within this module is ten times smaller than the external timestep. The main integration loop is run 5 times, one for each valve. Therefore, in actuality this module represents a 30th order system (6 states times 5 valves). Since each main integration loop is run 10 times, the simulation basically sees 300 integrations per outer timestep. It is clear that the computational demands of this particular module can considerably slow down the SSME simulation. In a situation such as this there are two possible solutions to the problem. One solution is to use additional hardware. The other solution is to provide integrators which would allow the use of larger timesteps and thereby reduce simulation time. The latter is the purpose of this study.
Figure 4. Functional block diagram of valve position control

where:

\( K_a \) = servo amplifier gain, ma/volt

\( K_L \) = actuator linkage gain, deg/in.

\( X_A \) = actuator piston linear motion, in.

\( \theta_A \) = actuator output rotary motion, deg.

\( \theta_v \) = valve ball rotary motion, deg.

\( G(S)_{sv} \) = servovalve transfer function

\( K_{sv} \) = servovalve gain, cis/ma

\( A \) = piston area, in\(^2\)

\( K_{RVDT} \) = position indicator gain, volts/deg.

\[ \begin{align*}
\omega_a &= \frac{\omega}{\omega_{n0}} \\
\gamma &= 0.7
\end{align*} \]

Figure 23. Functional Block Diagram of Valve Position Control
LOOP=(DT+0.00001)/DELTA
!
DO 300 I=1,5
!
! IF(TPA.GT.0.0.AND.TIME.GE.TPA) GO TO 218
!
!
MAIN INTEGRATION LOOP
!
DO 210 J=1,LOOP

EVP = THETAC(I)*CRVDT-VR(I)

DDESA = CA*WA**2*EVP-WA**2*ESAC(I)-2.0*SA*WA*DESA(I)
DDESV = WSV**2*ESA(I)-WSV**2*ESV(I)-2.0*SSV*WSV*DESV(I)
DTHETA(I) = CL(I)*CSV(I)/A(I)*ESV(I)
DVR = THETA(I)*CRVDT*CRS/TRS-VR(I)/TRS

INTEGRATORS

ESAC(I) = ESAC(I) + ALIM(DESA(I)) * DELTA
ESA(I) = ESAC(I)
DESA(I) = DESA(I) + ALIM(DDESA) * DELTA
ESV(I) = ESV(I) + ALIM(DDESV) * DELTA
DESV(I) = DESV(I) + ALIM(DDESV) * DELTA
THETA(I) = THETA(I) + ALIM(DTHETA(I)) * DELTA
VR(I) = VR(I) + ALIM(DVR) * DELTA

LIMITS ON INPUT AMPLIFIER ARE ±23 VOLTS.

IF (ESA(I).GT.23.) ESA(I)=23.
IF (ESA(I).LT.-23.) ESA(I)=-23.
IF (ABS(ESA(I)).LT.0.25) ESA(I)=0.0

LIMITS ON SERVO AMPLIFIER ARE ±20 VOLTS.

IF (ESV(I).GT.20.) ESV(I)=20.
IF (ESV(I).LT.-20.) ESV(I)=-20.

THETA(I)=AMAX1(0.0, AMIN1(THETA(I),THETAMAX(I)))

210 CONTINUE
!

END OF INTEGRATION LOOP
!

218 CONTINUE
!
BACKLASH IS DEFINED AS THE AMOUNT OF ACTUATOR OUTPUT SHAFT TRAVEL REQUIRED TO REVERSE DIRECTION OF VALVE BALL MOTION UNDER CONDITION OF ZERO LINKAGE WINDUP AND TORQUE LOADING. THE VALUES USED HERE I
! HALF OF THE AMOUNT OF THE TOTAL TRAVELING, WELL HALF ON EACH SIDE.

FAC=1.0
IF(I.EQ.3.AND.(THETA(I).GT.33.8.AND.THETA(I).LT.84.0)) FAC=0.0
IF(I.EQ.4.AND.(THETA(I).GT.38.3.AND.THETA(I).LT.75.8)) FAC=0.0
IF(ABS(THETA(I)-THETA(I)).GE.(THETBL(I)*FAC)) GO TO 212

Figure 5. Valve dynamics main integration loop fortran code
An integration analysis of the valve dynamics module requires that a mathematical model describing the valve position control system be determined. It turns out that a state space model of this system can be obtained directly from the main integration loop of Figure 5, viz.

\[
\begin{bmatrix}
\dot{x}_1 \\
\dot{x}_2 \\
\dot{x}_3 \\
\dot{x}_4 \\
\dot{x}_5 \\
\dot{x}_6
\end{bmatrix} =
\begin{bmatrix}
0 & 1 & 0 & 0 & 0 & 0 \\
-w_a^2 & -2s_a^2 & 0 & 0 & 0 & -c_a^2 \\
0 & 0 & 1 & 0 & 0 & 0 \\
-w_{SV}^2 & 0 & -2s_{SV}^2 & 0 & 0 & 0 \\
0 & 0 & [C_v C_{SV}] (I) & 0 & 0 & 0 \\
0 & 0 & 0 & 0 & [1/C_rvdt] (I) & \frac{C_rvdt}{T_{rs}}
\end{bmatrix}
\begin{bmatrix}
x_1 \\
x_2 \\
x_3 \\
x_4 \\
x_5 \\
x_6
\end{bmatrix} +
\begin{bmatrix}
0 \\
c_a^2 w_a^2 c_rvdt \\
0 \\
0 \\
0 \\
0
\end{bmatrix}
\theta_c (I)
\]

Using the notation of Figure 5, the states \(x_1\) through \(x_6\) correspond to the actual states as: \(x_1 = \text{ESAC}\), \(x_2 = \text{DESA}\), \(x_3 = \text{ESV}\), \(x_4 = \text{DESV}\), \(x_5 = \text{THETA}\), and \(x_6 = \text{VR}\).

Although there are five different valves, it was found that three of them are described by the same set of data while the other two are described by another set of data. As a result, only two different systems were considered. However, it turned out that both these systems have the same set of eigenvalues. These eigenvalues are:

\[
\lambda_1, \lambda_2 = -3499.7 \pm j3570.4 \\
\lambda_3, \lambda_4 = -48.9 \pm j136.5 \\
\lambda_5 = -2184 \\
\lambda_6 = 1058.5
\]

Clearly, this system is very stiff. Therefore, to obtain a stable and accurate simulation a very small timestep must be used. Notice as well that the complex poles have very large imaginary parts. This can make the selection of a suitable integration technique a difficult task.

Recall that for a simulation to be stable it is required that the \(\lambda T\)-product be inside the stability region of the integrator being used. In addition, the simulation will be accurate if the \(\lambda T\)-product is inside the region where there is minimum distortion. Therefore, for Euler's method the largest timestep that could be used to obtain an accurate and stable simulation of the valve dynamics module is \(T = 2 \times 10^{-5}\). A larger timestep would not guarantee accurate results. For a timestep \(T = 3 \times 10^{-4}\) the integrator would be operating on the verge of instability, with the slightest roundoff error making the simulation unstable. This timestep would also give very inaccurate results. This
is clearly seen in Figures 6 through 9, which show the results of simulating the system under consideration using Euler's method with different timesteps. The exact solution was obtained using Euler's method with a timestep T=10^{-5}. Notice that when a timestep T=2\times10^{-4} is used, the simulation is not very accurate, with the initial transient being almost lost. Therefore, if the transient is important in the simulation, Euler's method should not be used with a timestep larger than T=2\times10^{-5}. However, should either AB-2 or an MSRP-2 integrator be used to simulate this system, timesteps of T=10^{-4} and T=10^{-2} could be used, respectively. Although these timesteps would not approximate the transient too well, the results will be more accurate. Figure 10 shows the corresponding allowable timesteps for AB-2. From Figure 11 it is seen that if AB-2 is used with a timestep of 2\times10^{-4} the simulation will be unstable. However, for a timestep T=10^{-4} AB-2 performs quite well, this can be seen in Figures 12 through 14. Thereby given an improvement of a factor of 5. Recall that, for a linear system, MSRP-2 requires five times more computations than either AB-2 or AB-1 and thus its timestep must be five times as large. It turns out that MSRP-2 gives very accurate and stable results even for timesteps as large as T=10^{-2}. Figures 15 through 17 give the response using MSRP-2 with T=2\times10^{-3} while Figures 18 through 20 give the results of using MSRP-2 with T=10^{-2}. Clearly, MSRP-2 offers the best simulation results with the largest possible timestep for this particular module.

Notice that this module has some of the largest eigenvalues present in the SSME simulation. In addition, their magnitudes differ by several orders of magnitude. Thus, this system is very stiff. It is well known that the real-time simulation of stiff systems poses some of the most challenging problems to the control engineer. Hence, this module could be thought of as typifying some of the problems associated with the SSME simulation.

Although MSRP-2 integrators provide excellent results with a substantial speed improvement, it is only recommended that they be implemented locally within each module. The nature of the SSME simulation coupled with the wide range of operating points do not make this problem amenable to an easy implementation using this type of integrators. However, if AB-2 integrators were used in place of Euler's method, a reasonable speedup could be expected. This would involve only a fraction of the work and complexity should MSRP-2 integrators be used.

Recall that to design an MSRP-2 integrator for a nonlinear system requires that the system be linearized about some operating point. Thus, to replace the integrators of the SSME simulation by MSRP-2 integrators, it would be necessary to linearize the different modules about the operating points of interest. This would involve a tremendous effort as the SSME simulation is highly nonlinear. Although this approach was considered, the time constraints associated with this project did not allow its realization.

A further point worth mentioning is the fact that the eigenvalues of this system are complex with very large imaginary parts. Recall
that this type of eigenvalues can cause instability problems when Euler's method is used. This is due to Euler's stability region being asymptotic to only the origin of the \( NT \)-plane. Thus, in order to stably and accurately simulate systems with this type of eigenvalues very small timesteps are required. Since the stability region of AB-2 is asymptotic to a larger portion of the imaginary axis of the \( NT \)-plane, it is expected that AB-2 would perform better in this type of situations. However, if the magnitude of the imaginary parts of the eigenvalues is much larger than their real parts, MAB-2 may be used. That is, the instability problems that may arise due to almost purely complex eigenvalues can be alleviated by replacing the classical AB-2 method by the modified AB-2 method. Keep in mind, however, that the simulation results may not be as accurate as MAB-2 is only first order accurate.

Finally, the concept of stability region in the simulation of nonlinear systems must be used with care. This is due to the fact that for nonlinear systems the margin of the stable region cannot be clearly distinguished from the unstable region. Essentially, there will be an inner region in which the simulation will be stable, an outer region where the simulation will be unstable, and a "fuzzy" region in between these two regions.

B. OXIDIZER TURBOPUMP MODULE: CASE STUDY II

This module presents some of the most challenging integration problems in the SSME simulation. An analytical study of this module was carried out to determine the range of frequencies of the system. Although it is recognized that this is not the best approach to linearizing this type of systems, the intent was to obtain an approximate frequency range of the system's eigenvalues. It is felt that for integration purposes this approximate range suffices. This analytical study was done because the maps describing the nonlinear functions in this module make it very hard to determine an accurate model of the system. Determining an accurate model of the oxidizer turbopump module requires a considerable amount of time and effort; both of which are beyond the scope of this project. Therefore, the 37th order nonlinear model was linearized analytically using the Jacobian method. By considering the maximum and minimum values specified in the maps, a reasonable estimate of the eigenvalues of the actual system could be obtained. It was found that the stable eigenvalues of the linearized system vary from -20 to about -8000. This range agrees well with the actual range of frequencies specified in [10]. The few unstable eigenvalues are believed to be a result of our crude approach to linearization. The numerical values of the eigenvalues of the linearized system are listed in Table 5. Although, it was expected that some lightly damped modes were going to be present in this module, only two sets of complex eigenvalues with a damping ratio of about 0.2 were found. At this time the authors cannot provide any further insight into this last aspect as it was very difficult to determine whether the ducts were actually being modeled inside or outside the module. However, further analysis is being done to determine a linearized model of the entire SSME
simulation by recording the change in the states due to perturbations introduced into each state. This analysis will provide linearized models and thus more accurate accounts of the eigenvalues of the system at different operating points. Another study being done is the determination of reduced order linear models of the SSME. This study will consider several techniques to obtain the reduced order models. As the transient response is of essence in the SSME simulation, singular perturbation cannot be used as a model reduction technique as it reduces the order by deleting the fast dynamics of the system.

Table 5. Approximate location of the eigenvalues of the oxidizer turbopump linearized model

<table>
<thead>
<tr>
<th>i</th>
<th>$\lambda_i \times 10^3$</th>
</tr>
</thead>
<tbody>
<tr>
<td>1→12</td>
<td>0</td>
</tr>
<tr>
<td>13→18</td>
<td>-0.020</td>
</tr>
<tr>
<td>19</td>
<td>-7.9452</td>
</tr>
<tr>
<td>20</td>
<td>-0.0116</td>
</tr>
<tr>
<td>21</td>
<td>-0.0050</td>
</tr>
<tr>
<td>22</td>
<td>-2.5104</td>
</tr>
<tr>
<td>23→24</td>
<td>0.0088 ± 0.0373i</td>
</tr>
<tr>
<td>25</td>
<td>-0.0393</td>
</tr>
<tr>
<td>26</td>
<td>-0.0237</td>
</tr>
<tr>
<td>27</td>
<td>-0.0113</td>
</tr>
<tr>
<td>28</td>
<td>-0.0344</td>
</tr>
<tr>
<td>29</td>
<td>0.0022</td>
</tr>
<tr>
<td>30</td>
<td>0.0013</td>
</tr>
<tr>
<td>31</td>
<td>-0.0025</td>
</tr>
<tr>
<td>32</td>
<td>-0.0023</td>
</tr>
<tr>
<td>33→34</td>
<td>-0.0002 ± 0.0010i</td>
</tr>
<tr>
<td>35</td>
<td>-0.0147</td>
</tr>
<tr>
<td>36</td>
<td>-0.0062</td>
</tr>
<tr>
<td>37</td>
<td>-0.0039</td>
</tr>
</tbody>
</table>
From Table 5 it is clear that the oxidizer turbopump module is a stiff system. Therefore, the discussion just given for the valve dynamics module also applies to this system. Notice that this implies that if Euler's method were to be replaced by AB-2, a speedup factor of approximately 5 could be realized. However, if MSRP-2 were used the time savings will be much larger. Since this module and the Fuel.F module are very similar in nature, it is expected that the eigenvalues of Fuel.F be within the same range. These two modules comprise most of the states in the SSME simulation.

The complexity of the linearized system can be observed from the following pictorial representation of the system A matrix, viz.

```
0000000000111111122222222233333333
1234567890123456789012345678901234567
01x x x x x x x x x 01
02xx 02
03x 03
04 x x x x x x 04
05 x x x x x x 05
06 x x x x x x 06
07 x x x x x x 07
08 x x x x x x x x x 08
09 x x x x x x x x x 09
10 x x x x x x x x x 10
11 x x x x x x x x x 11
12 x x x x x x x x x 12
13 x x x x x x x x x 13
14 x x x x x x x x x 14
15 x x x x x x x x x 15
16 x x x x x x x x x 16
17 x x x x x x x x x 17
18 x x x x x x x x x 18
19 x x x x x x x x x 19
20 x x x x x x x x x 20
21x x x x x x x x x 21
22 x x x x x x x x x 22
23 x x x x x x x x x 23
24 x x x x x x x x x 24
25 x x x x x x x x x 25
26 x x x x x x x x x 26
27 x x x x x x x x x 27
28 x x x x x x x x x 28
29 x x x x x x x x x 29
30 x x x x x x x x x 30
31 x x x x x x x x x 31
32 x x x x x x x x x 32
33 x x x x x x x x x 33
34 x x x x x x x x x 34
35x x x x x x x x x 35
36x x x x x x x x x 36
37 x x x x x x x x x 37
00000000001111111122222222233333333
1234567890123456789012345678901234567
```
Figure 6. Simulation of the valve dynamics module using Euler's
Figure 7. Response of $x_1$ and $x_2$ of valve dynamics using Euler's
Figure 8. Response of $x_3$ and $x_4$ of valve dynamics using Euler's
Figure 9. Response of $x_5$ and $x_6$ of valve dynamics using Euler's
Figure 10. Simulation of valve dynamics module using AB-2
Figure 11. Simulation of valve dynamics module using AB-2 (unstable)
Figure 12. Response of $x_1$ and $x_2$ of valve dynamics using AB-2
Figure 13. Response of $x_3$ and $x_4$ of valve dynamics using AB-2
Figure 14. Response of $x_5$ of valve dynamics using AB-2
Figure 15. Response of $x_1$ and $x_2$ of valve dynamics using MSRP-2
Figure 16. Response of $x_3$ and $x_4$ of valve dynamics using MSRP-2
Figure 17. Response of $x_5$ and $x_6$ of valve dynamics using MSRP-2
Figure 18. Response of $x_1$ and $x_2$ of valve dynamics using MSRP-2
Figure 19. Response of \( x_3 \) and \( x_4 \) of valve dynamics using MSRP-2
Figure 20. Response of $x_5$ and $x_6$ of valve dynamics using MSRP-2
5. IMPLEMENTING INTEGRATION IN THE SSME SIMULATION

The previous two chapters explain our recommendations of the modified AB2 integration method, over Euler's method. Local MSRP methods, which could be used for much larger step sizes, were also explained. This chapter deals with the practical implementation of the SSME integration methods. It ends with a description of the report version integration module 'integ.for'. A log showing all references to the integration module is included in Appendix C. This log is also available as the file 'integ.log' on the report version diskette.

Numerical Accuracy of an Integration Step

The SSME study version simulation addressed the numerical accuracy of each Euler integration step

\[ x = x + xdot \times dt \]

by selecting DOUBLE PRECISION as the type for dt. The code generated by Fortran does the following steps:

1. Convert xdot to double precision.
2. Multiply xdot * dt.
3. Convert x to a double precision temporary.
4. Add in double precision.
5. Truncate the sum back to single precision for storage.

Since x and xdot are carried in single precision, extra digits beyond single precision that are generated by the product are not actually significant to the result. The useful part of the above sequence is the way it preserves the significant digits of the product by doing the addition in double precision. Floating point addition of the relatively small increment tends to lose significant digits of the increment, as the increment's mantissa is shifted for binary point alignment with the variable's mantissa. Double precision addition uses a longer register, limiting this loss to extreme cases.

In the report version integration module, all integrators use a method which preserves the significance of the time step increment, and also minimizes floating point conversions. The technique is generally known as "double precision accumulation". The method maintains a double precision variable as an accumulator for x. The time step dt is of single precision REAL type, so that computations of the increment, such as the product x * xdot in Euler's method, are done in single precision. The increment is then converted and the addition is done in double
precision. The double precision accumulator prevents the truncation of significant digits from the time step increment, and $x$ does not have to be re-converted to double precision on the next step. The output value of $x$ returned to the simulation is of single precision type, so that its use in other computations in the simulation does not generate conversions and double precision operations.

Limiting Integration Outputs

When the outputs of integrators are limited, as they frequently are in the SSME simulation, some difficulties arise with both double precision accumulation and multistep integration technique. These complications should not be considered a reason for not implementing the methods, however, because in the SSME simulation, so much computation is required on every time step that almost any method which allows a larger time step is justified, regardless of complications.

If the output of an integrator is changed by a limit, there is the issue of whether or not to adjust the integration process to this change. The study version's Euler method simply replaces the integrated value of $x$ with the limited value, in effect, restarting the integration process. Nothing is lost because Euler's method carries no information from time step to the next time step.

When the output of a multistep method is changed by a limit, the past values are compromised, if not invalidated. Several options are available:

- ignore the discrepancy, using the past values unmodified.
- adjust the past values, taking into account the difference between the unlimited and limited outputs of the integrator.
- discard the past values and use a starting integrator while the output value is on the limit, and for restarting the multi-step method when the output leaves the limit.

The third option is recommended in general for SSME, using Euler's open formula as the starting integrator, for the following reasons:

- it is a fast method, compared to the second option.
- as a starting formula, the Euler's method would only determine the output of the integrator when the integrated value is coming away from its limit. With the low order multi-step methods recommended, these periods are limited to
one time step.

- using the linear approximation of Euler's to restart is at least as good as doing a linear extrapolated adjustment of past values, in the second option above.

The use of Euler's method as a restarting formula is not necessarily recommended for local MSRP implementation, because of the larger step size. A higher order restarting method may be required, but the question was not investigated.

Limiting the output also introduces complications in the double precision accumulation method. To apply the limit to the double precision accumulator, it is not appropriate to reset the accumulator unconditionally to either the output or the limit. This would render the accumulator single precision, despite its double precision type. Instead, it is necessary to know when the output is limited, and to replace the accumulator only then.

In double precision accumulation, efficiency demands that the limits be converted to double precision when the integrator is initialized, and kept in that form, so that continual reconversion of the limit is not required every time it replaces the accumulator. The report version handles limits in that manner.

It is possible that unlimited integrators are more appropriate for some limiting situations in SSME. In this method of limiting, the limits are applied after the integration and are not made known to the integration routine. This would be the case where an integrated process is unaffected by the limit except through feedback into the driving rate. A characteristic of this situation would be that the variable is not expected to come off the limit as soon as the rate changes direction, but only when the underlying unlimited integrator's value would cross the limiting value. It is beyond the scope of the study to distinguish these kinds of limiting situations from others, so all limiting situations are modeled in the report version code by limited integrators.

In situations where operation on the limit is not expected, a limit should not be silently imposed on an integrator, just to stay within bounds of tabulated data. In the report version, the corresponding unlimited integrator is used, and the interpolation routine stops the simulation with an identifying message, if the interpolated table's range is exceeded.

The Report Version Integration Module

The report version integration module 'integ.for' implements
the recommended modes of operation, and also provides a recoded form of the study version's Euler method integration. This makes it practical to operate the simulation with all other forms of speedup in place, but with no change in integration policy or step size, as called for in the earlier recommendations for tuning the SSME simulation. The integration method may then be changed to the modified AB2 with minor recommenting and recompilation of the 'integ.for' source code alone, followed by a relinking step.

A number of integration routines are required to handle the different situations encountered in the SSME simulation. The following short glossary covers the terminology used in the report and in the report version comments to distinguish integration routines:

- **primary integrator** - an integrator used outside of any energy balancing loop. It produces a final value for the time step.

- **trial integrator** - an integrator used in an energy balancing loop. It produces a trial value which is accepted as the final step value when the balancing loop has converged.

- **unlimited integrator** - an integrator whose accumulator is controlled only by initialization and rate input.

- **limited integrator** - an integrator whose accumulator is subject to limits given to it at initialization. The behavior of limited integrators was described above.

- **flow integrator** - an unlimited integrator with the SSME gas flow rate calculation built in. In 'integ.for', it comes in primary and trial flavors.

- **method** - the integration method, such as Euler's method, Adams-Bashforth Second Order, or MSRP.

The integration module consists of the following routines:

- initiation subroutines for limited and unlimited integrators of any method, and of either primary or trial, or flow types.

- primary integrators of limited and unlimited forms, and using Euler and modified AB2 methods. Comments in the source code of these routines are edited to switch integration methods throughout the simulation.

- trial integrators of unlimited form, using Euler and modified AB2 methods. These routines are selected by recommenting
whenever the primary integrators are.

- flow integrators of primary or trial types. These call the primary and trial integrators, and are not changed when switching integration methods.

- step update functions each method of the trial integrators. These are recommended to select the one corresponding to the trial integrator.

The flow integrators replace study version flow integrators based on solving an equation representing the implicit, or closed form of Euler's formula. This method computed the flow rate in double precision, even carrying out a square root to this accuracy. The method is costly in computing time, especially since the flow integration occurs frequently inside of energy balancing loops.

The effort of this calculation is not justified. The Euler formula is only first order, so the double precision results obtained represent only a linear approximation to a curve being followed to single precision accuracy. Implicit formulas are normally used in corrector formulas, where they represent one or more corrective iterations at the same time step.

Double precision in the flow rate calculation may have been adopted in the face of balancing convergence problems. If so, it is of no more than accidental value as a solution to those problems. A more detailed monitoring system and relaxation controls for balancing convergence is recommended instead.

The integration module hides past multi-step values, double precision accumulators, and trial accumulators from the rest of the program. Only the integration routines have access to them. The calling routines refer to these values by a unique number assigned by the programmer to the integrand value. A major reason for the log file is to have a compact record of the number assignments.

Space can be saved in the report version by having different sets of arrays supporting the hidden values for the different types of integrators, rather than one set of arrays for all. The hidden values are defined in the integrator module's labelled common block 'integ' in the file 'integ.com'.
6. INTERPOLATION IN THE SSME SIMULATION

Interpolation of values from tabulated data is a major consumer of computer time in the SSME simulation. Linear interpolation of unequally spaced data points is the prevalent form of interpolation. It is used for function generation, with \((x,y)\) data read from the file 'dtminp.dat' in initialization sections of each module. Two dimensional linear interpolation on temperature and pressure surfaces was used for gas properties. Cubic spline interpolation was used in one such table.

Linear interpolation routines in the study version were not coded for optimum efficiency, and there was a large adverse effect on running time.

With unequally spaced data points, it is necessary on each interpolation to identify the interval

\((x_i, x_{i-1})\)

of the independent variable enclosing

the input value \(x\). The study version's 'fgen' does a linear search from the low end of the table, comparing \(x\) to values \(x_i\) in increasing order. This is suitable for short tables, or for tables in which most of the simulation time is spent within the few lowest intervals. Otherwise the expected number of comparisons, half the size of the table, is excessive.

From one time step to the next, one would expect the input variable to be in the same interval as it was previously, most of the time. Accordingly, a generally better strategy is to test the endpoints of the previous interval, and if exceeded, search in that direction for the enclosing interval. The report version of 'fgen' does that, favoring the upward direction by testing the upper side of the interval first. Two comparisons are required when the input variable stays within the same interval, two are required when it moves up an interval, and three are necessary when it moves down an interval, for an average close to two.

Another serious fault with the study version function generation is the failure to precompute coefficients for the interpolation polynomial. The study version interpolation, given the interval index \(i\), is of the form

\[
f(x) = y_{i-1} + \frac{(y_i - y_{i-1}) \ast (x - x_{i-1})}{(x_i - x_{i-1} + 10^{-20})}
\]

For an inner loop operation of a major simulation, this coding is truly ugly. Three additions and the division can be done once,
when the function values are loaded. Instead they are done on every interpolation. The extra constant term guards against division by zero when x values are repeated in the table. Such an occurrence makes no sense in a function table. The program is spending simulation time to quiet the operating system's complaint about an error in the function data!

In the report version, the corresponding interpolation is of the form

\[ f(x) = a_i + b_i \cdot x \]

and the loading routine complains if \( x_i \) is too close to \( x_{i-1} \).

The function generation module assigns each function table a unique number, to be used on interpolation calls. The number is a key to the previous interval, the starting point for the interval search. In the report version, this number locates precomputed coefficient values \( a_i \) and \( b_i \) as well.

In the study version, tables were stored in a two dimensional array. The function number was a row index in the array. There were 15 values per row, so functions were limited to that many points. Functions shorter than 15 points did not fully occupy their rows. In the report version, a one dimensional arrays are used for x and y values. The function number locates the starting point and size of the table in the large array. This method places no constraint on the size of a function table, allowing more accurate approximations to be formulated where necessary, by using more than 15 data points. The method also avoids wasting memory where functions have fewer than 15 points.

In the SSME simulation interpolations within the same table can be used to obtain current values for several variables within the same time step. Therefore the function number, which identifies only the table, cannot be used to recall the previous interval expected to enclose the input value. Instead, a unique value is assigned to the variable within the routine which calls the interpolation module. The interpolation module provides array space for the index of the previous interval, and calling routine passes the variable's index to the interpolation module.

New functions are added to the simulation by placing \((x,y)\) points in the file 'ssme.dat', adding a call to the function loading routine 'fgset', and adding interpolation function references to 'fgen'. All one dimensional linear interpolations should be treated this way, to take advantage of the optimal coding of fgen. The function TLIMIT in the control module 'control.for' was redefined as an fgen reference.
Interpolation of Functions of Two Variables

Several forms of interpolation are used on gas property tables defining temperatures and pressures as functions of two variables. Data points were unequally spaced in both dimensions.

The study version interpolation routines used the search method recommended above to find the enclosing interval in each dimension. Running time was excessive, however, because interpolation coefficients were not precomputed.

The study version two-variable interpolations differed from the function generation routines in that the data tables were incorporated into the simulator as arrays initialized by Fortran DATA statements. There are no compelling reasons to prefer this method over loading from a data file. The DATA statement method does the conversion to binary at compile time, rather than during initialization, and input from a data file becomes input from the load module. With virtual memory the load module data is not actually loaded into memory until needed. But in the SSME simulation all of it is needed during initialization, for the precomputing of interpolation coefficients. It is doubtful that the saving in initialization time would be noticed.

In the event there is a simulation requirement to manipulate gas properties, such as investigation of the effect of impurities, gas property tables should be moved to data files, and an open, accessible format for editing the tables should be adopted, such as in 'ssme.dat.

Cubic Spline Interpolation

Cubic spline interpolation is used in the two dimensional interpolation routine 'O2PROP' (SSM52510). There was no explanation available as to why cubic spline interpolation was required for this table, when linear interpolation was sufficient for hydrogen and OXPROP oxygen properties. Perhaps it was adopted in an attempt to get convergence within energy balancing iteration of OPRIME, which calls O2PROP.

In O2PROP, two-way cubic interpolation is attempted, in the same manner that two-way linear interpolation is done in other modules. Spline interpolation is done on the two adjacent columns of the table which bound the row input value, then the spline interpolation routine is called to interpolate along the row. This procedure does not actually achieve cubic spline interpolation smoothing, however. To do that, additional row values would be required. Two are not enough to define the smooth curve which is desired.
For the report version, the erroneous application of the spline routine is replaced by linear interpolation. Apparently, true two-way spline interpolation is not actually required for energy balancing convergence, or whatever purpose it was intended to serve.

For the sake of speedup, the elimination of cubic spline interpolation from O2PROP should be attempted. The report version coding shows the large initialization time and coefficient space required. Better observations of the convergence problems, and relaxation adjustments will make energy balancing more robust, and will probably make spline interpolation unnecessary.

Without addressing further the need for cubic spline interpolation, which was outside the scope of the study, it was possible to assess the efficiency of cubic spline implementation in the study version, and to recommend an improved version for use where it may be required. In keeping with the modularization policy of the report version, cubic spline routines were added to the interpolation module 'fgen.for', so that cubic spline interpolation could be tried in other table lookup situations within the simulation, with a minimum of programming effort.

The deficiency of the study version's cubic spline implementation is that it does not carry precomputation of interpolation coefficients far enough. Ideally, once the index of the interval enclosing the input value has been determined, an interpolated value on the cubic arc for the interval can be computed with three multiplications and three additions, as

$$f(x) = a_i + x \times (b_i + x \times (c_i + x \times d_i)) .$$

The study version of the spline interpolation precomputes second derivative constants, instead of cubic polynomial coefficients, and the interpolation routine working with this precomputed data requires 7 additions or subtractions, 12 multiplications and a division. This is at least four times the cost of the report version's cubic polynomial evaluation.

True two-way cubic spline interpolation is very costly, compared to the interpolations used in the simulation, not only because many points are needed for interpolation in the row direction, but also because the precomputation of cubic segment coefficients is not possible.

The linear interpolation module

The report version module 'fgen.for' contains all routines of one and two dimensional linear interpolation, and cubic spline interpolation. Interval finding, precomputing of interpolation
coefficients and the interpolating routines are included. The file 'fgen.com' defines the labelled COMMON block used by the interpolation routines.

The study version's FGEN routine was replaced by a subroutine 'fgset' for loading function values and precomputing interpolation coefficients, and a separate linear interpolation function 'fgen'. Two-way linear interpolation is also provided in a split package, with precomputing handled in the subroutine 'xyset', and interpolation by the function 'xylint'. One interval searching routine, 'intval' serves for all interpolation with unequally spaced independent variable data.

A maintenance aid file 'fgen.log' records the references to the function generation routines 'fgset' and 'fgen'. A copy is included on the report diskette.
7. ENERGY BALANCE CONVERGENCE DIAGNOSIS AND CONTROL

Two energy balance iterations are performed at every time step in the SSME simulation. The fuel flow module contains an iteration loop carrying a sequence of calculations over 12 stages. The oprime module, called by hotgas during the first 1.5 seconds, iterates over four stages.

Limits on these iterations were set within the study version source code at 30 iterations. Any difficulty in convergence of these energy balancing loops can be very costly in simulation running time. These loops involve flow rate calculations, which were implemented in a time-consuming manner in the study version.

The study version monitors the convergence of these iteration loops by writing out messages, and the last two iteration changes, when the iteration limits are exceeded. The number of iterations is also written as an output. While this monitoring is sufficient to determine when there is a convergence problem, it is not adequate to diagnose what could be wrong, and it provides no corrective tuning action.

The report version contains an energy balance diagnosis and control module, in the file 'change.for'. This module associates a unique number with each energy balance variable, and uses it as an index to store the number of iterations required for that particular variable to converge. Thus slow converging variables can be identified, and the computation of these variables examined for disturbances to convergence.

The warning system for energy balance convergence problems is similar to the study version's, but provides more information. A diagnostic file is written on any run in which the iteration limits are exceeded. The diagnostic file shows the number of iterations and the relative change level achieved, for each energy balance variable. After this information is written, the diagnostic data output is repressed for 100 iterations, so the simulation may continue to run, and information over a longer period of time may be collected.

A second means of monitoring is available, suitable for close inspection of troublesome intervals. The number of iterations for convergence of each variable can be chosen as an output variable, and thus can be collected at the data collection interval, throughout the simulation.

'Change.for' also provides for a commonly applied remedy to multi-variable convergence problems, the relaxation technique. A relaxation factor for each energy balance variable is included in
the run parameters on file 'ssme.run'. This factor can be changed to brake, or accelerate, the influence of newly calculated values on the iterated value. Instead of simply replacing the old value, the relaxation method computes the iterated value by

\[ \text{iterated} = \text{factor} \times \text{new} + (1 - \text{factor}) \times \text{old}, \]

where \(0 < \text{factor} < 2.0\).

The normal default value is 1.0, implementing a simple replacement. For a variable that tends to converge slowly, the factor is decreased, under-relaxing or damping the corrective calculations. Fast converging variables can be over-relaxed by increasing their factors above 1.0. Their convergence can often be accelerated in this way, providing more stable conditions for the slow convergers.

Contents of the 'Change' Module

The source file 'change.for' provides initialization routines for setting the relative change tolerances, and for initializing convergence iteration counts of energy balance variables at each time step. The FUNCTION 'relax' applies the relaxation factors, and counts iterations in which the variable change is above tolerance. A convergence alert routine 'wrchg' writes the diagnostic file 'ssme.cvg' and a message on the monitor screen.
8. REAL EXPONENTIATION

One possibility for speedup in a digital simulation system is to take advantage of the fact that the six to seven significant digits of accuracy normally delivered by software supported special functions may be more than is required. This is probably the case in the SSME simulation. It appears that a significant reduction in running time can be derived by using special means to compute the function

\[ f(x) = x^{(0.1*n)} \]

This function is used frequently in the simulation loop, in the form shown, and as the square root function \( n = 5 \). In the report version, a module is devoted to special methods to compute it.

Without hardware support, the function \( x^y \), where \( y \) is a real data type, is normally computed by normalizing both \( x \) and \( y \) to unit intervals, and using economized series or rational approximations for a logarithm of \( x \), and the exponent of \( (y \log x) \). The logarithm approximation is particularly slow to converge, and many terms are necessary for the 7 place accuracy normally required in Fortran libraries.

Many floating point hardware systems provide hardware support for real exponentiation, and the use of this hardware by the compiler makes special methods of computation unnecessary.

In the report version of the SSME simulation, all exponentiation and square root function calls have been replaced with calls to routines in the module 'xtoy.for'. The primary routine in this module does a two-way linear interpolation of

\[ f(x,n) = x^{(0.1*n)} \]

in one of two tables of equally spaced points \((x, n)\). One table covers normalized \( x \) values from zero to 0.2, and the other covers normalized \( x \) from 0.2 to 1.0. Other routines in the module perform normalizations and call the primary module.

The module as implemented provides maximum speedup over a software supported exponentiation. The maximum relative error is close to 0.5 per cent. The accuracy could be improved, at the cost of more operations per exponentiation, by using more tables, or by going to a higher order interpolation. In cases where exponentiation is hardware supported, the 'xtoy' module routines can be replaced by simple routines using exponentiation expressions which take maximum advantage of the hardware support. No changes need be made in the calling simulation modules, to implement such a customized version.
9. AN OUTPUT SYSTEM FOR THE SSME SIMULATION

The advantages of selected binary output have been described earlier in the results summary of this report. A recommended implementation is provided in the report version of the code, and is described here.

The output system consists of several components:

1. An ASCII output definition file 'output.def' lists all output variable names, and can be edited to select those variables to be collected on a particular run. The selection file is identified by an 80-character header.

2. An output initialization segment in the main program reads the output definition file, and sets collection index arrays for the run. The segment opens the output file and writes the input parameter header to identify the run set up, and the output selection header to identify the selection. The collection index array and corresponding variable names are written to the output file.

3. A code segment in the main program monitors the simulation loop counter and triggers output collection. The report version uses integer operations, and is simpler than the study version, offering a single collection frequency.

4. All potential output variables are contained in the COMMON block 'outvar', integer variables first.

5. The routine 'writer' views the 'outvar' COMMON block as an integer array and a real array. It reads output variable index numbers and collects the corresponding data from the COMMON block. It writes the collected data to the output file in one binary record, including the simulation time.

6. Offline print and plot programs read headers, variable names, and data from the output files, convert the data as necessary, compute functions of output data as required, and present the output.

An example of an offline output program of item 6 is the program RTable in the report version file 'rtable.for'. This program tabulates selected real data from the simulation run in up to 10 columns. Whenever there is a function of output variables to be plotted, or a new display device to utilize, a small program similar to RTable can be written, instead of altering the simulation program.
10. A ROUGH ESTIMATE OF SPEEDUP

Our time had to be spent on analysis of the SSME model, and the definition of changes needed for a faster and more accurate simulation program. An inspiration for this effort was the following rough model, offers some insight into the problem of how far to go optimizing the SSME simulation.

Assume the running time about equally divided between output operations and computation. Selective output will encourage more runs, but should reduce the output per run by at least a factor of 10. The encouraged extra runs are worth the price, and should not be assessed as penalty.

Doing data conversions offline relieves the simulation host of a huge load. Binary to decimal conversion is iterative, and floating point conversion to characters costs. Of course, this means that conversions will be repeated, as data is viewed, but on personal computers and workstations, this time is free.

If the output processing per datum is reduced by a factor of 10, we have achieved 100 to 1 speedup on the output operations side.

On the computation side, some of the savings are additive, some multiplicative. It is reasonable to assume the integration processing time is no more than one thousandth of the rate computation time on each integration time step. So if integration methods adopted are 10 times more costly than Euler's, if doesn't matter. Five times the step size still essentially means one fifth of the computation.

Given the size of tables, there is probably a factor of three saving in search time, and precomputation of slope data preserves that factor through interpolation computations on the interval. Optimization outside interpolation may be close to that. The saving on flow integration by going to single precision can be counted here. So can replacement of series evaluations for exponentiation. We believe there is an overall factor of three available from all numerical optimization sources.

A large part of the simulation is subject to a third factor, the reduction in the number of energy balancing iterations. Relaxation of energy balancing loops would dramatically reduce large iterations. Smaller ones would require less improvement to register a good factor of improvement. We estimate a factor of two for energy balancing optimization, applying to 1/3 of the simulation. Roughly, we are assuming that energy balancing portions occupy a third and valve dynamics
requires a third. We ignore the initialization and loading time.

In this rough model of computing time, the half devoted to output is subject to a 10 * 10 speedup. The time for energy balancing loops, say one third of computing time, or a sixth of total time, benefits from integration (speedup = 5) and balancing relaxation (speedup = 2). There is also a predominance of flow integration in this part, so we project a speedup of three from numerical optimization and elimination of the double precision closed Euler's scheme. To the nonbalancing part, we predict a numerical speedup closer to two.

According to this rough model, the running time is reduced by a factor of

\[
\frac{1}{2} \left( \frac{1}{100} \right) + \frac{1}{5} \left( \frac{1}{6} \frac{1}{3} \frac{1}{2} + \frac{1}{3} \frac{1}{2} \right) = \frac{1}{22.8}
\]

According to this rough model, the running time is reduced by a factor of

\[
\frac{1}{2} \left( \frac{1}{100} \right) + \frac{1}{5} \left( \frac{1}{6} \frac{1}{3} \frac{1}{2} + \frac{1}{3} \frac{1}{2} \right) = \frac{1}{22.8}
\]

Under these assumptions, suppose local MSRP were introduced, with a time step of 20 times the Euler step size. At worst, the computation costs might equal the numeric savings of the report version. We might expect to lose the speedup due to relaxation, due to larger "first guess" errors on energy balancing. The resulting running time factor would be about

\[
\frac{1}{200} + \frac{1}{20} \left( \frac{1}{6} + \frac{1}{3} \right) = \frac{1}{33.3}
\]

This would be a good result, but the resulting simulation would be only half again faster. On the other hand, it is possible that energy balancing iterations would increase significantly at this step size. If balancing iterations were to double the current values, in spite of the relaxation technique, then the resulting time factor could be

\[
\frac{1}{200} + \frac{1}{20} \left( \frac{2}{6} + \frac{1}{3} \right) = \frac{1}{26.1},
\]

largely negating the gain from MSRP.

Finally, consider what happens if integration and numeric speedup works as expected, but no action is taken on the output system. The first running time factor above becomes

\[
\frac{1}{2} + \frac{1}{5} \left( \frac{1}{6} \frac{1}{3} \frac{1}{2} + \frac{1}{3} \frac{1}{2} \right) = \frac{1}{1.86}
\]

and there is no prospect of doing much better, since infinite computational speedup results in a factor of 1/2.
REFERENCES


APPENDIX A. REPORT VERSION CODE

We start with the simulation function modules. The interpolation module 'fgen.for' was constructed out of parts of the study version code, bringing all interpolation to the same level of optimization, and adding some features. The integration module 'integ.for' and balancing loop control module 'change.for' are new.

Additional files '*.def' and '*.log' are included on the report version diskette delivered with this report. The '*.def' files are reference prototypes which can be inserted or viewed when coding, as reminders of the form of the reference. The '*.log' files are copies of referencing lines, which aid in the maintenance of programmer assigned index numbers used in all of the function modules.

The remaining report version code sections have similarly named counterparts in the study version code. All code is presented here without additional commentary, outside of report page numbering. For reference, we provide the following table of contents for Appendix A:

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</table>
* This module contains all interpolation routines
* General one dimensional interpolation:
* For initializations, see blockdata.for

PARAMETER ( NCURVE = *, NWORD = *, NCALL = * )
COMMON / fcns /
+ nstart(NCURVE), npts(NCURVE), last(NCALL),
+ xp(NWORD), a(NWORD), b(NWORD), now

FUNCTION fgset( number )
*****************************************************************
* Loads function points from run.dat file.
* Precomputes coefficients a and b for linear interpolation in the
* form a + b * x.
* The coefficients go into large arrays, with starting
* point and length defined.
* Lengths are initialized to 0, meaning 'undefined'.
*****************************************************************
INCLUDE 'units.com'
INCLUDE 'fgen.com'
* IF ( number > NCURVE ) THEN
  PRINT *, 'Function ', number, ' has too many points.'
  STOP
ELSEIF ( npts( number ) .GT. 0 ) THEN
  PRINT *, 'Function ', number, ' was previously defined.'
  STOP
ENDIF
READ(run,'(/215, A )') num, n, title
IF ( num .NE. number ) THEN
  PRINT *, 'Function ', num, ' read, expecting ', number.
  STOP
ENDIF
nstart( num ) = now
npts( num ) = n
nend = now + n - 1
READ(run,'(6(/2X,G10.0))') ( xp(i), a1(i), i = now, nend )
DO 10 i = now, nend, -1
  IF ABS( xp(i) - xp(i-1) ) .LT. 1.E-4 ) THEN
    PRINT *, 'X difference too small in function ', num
    STOP
  ENDIF
  slope = ( a1(i) - a1(i-1) ) / ( xp(i) - xp(i-1) )
a0(i) = a1(i) - xp(i) * slope
  a1(i) = slope
10 CONTINUE
* Initializes fgen's previous interval to first interval
last( num ) = 2

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now = nend + 1
END

* FUNCTION fgen( nfcn, ncall, x )
*****************************************************************
* Linear interpolation of curve(nfcn) at x.
* Stops with error message if curve is undefined or x out of range.
* Supply a unique index for the interpolated variable in ncall.
* Previous interval index is saved under that index.
* Search for the new interval starts with previous interval.
* Coefficients for each interval are precomputed by fgset.
*****************************************************************

C
INCLUDE 'fgen.com'

C
IF ( npts(number) = 0) THEN
  PRINT *, 'Invoked function ', number, ' was not loaded.'
  STOP
END

i0 = nstart( number )
CALL intval( last(number), x, npts(number), xp( i0, nerr )
IF ( nerr .NE. 0 ) THEN
  IF ( nerr .LT. 0 ) THEN
    PRINT *, 'Value too low for function ', number
  ELSE
    PRINT *, 'Value too high for function ', number
  ENDIF
  STOP
ENDIF

itop = i0 + last(number)
fgen = a(itop) + x * b(itop)
END

* Two-way linear interpolation:
*
FUNCTION xylint( x, y, nx, px, ny, py, sx, vdy, table, itop, jtop )
****************************************************************
* Two-way linear interpolation, with precomputed slopes sx and
* y differences dy.
*****************************************************************
REAL px(nx), py(ny), sx(nx,ny), vdy(*), table(nx, ny)

  ilow = itop - 1
  jlow = jtop - 1
  dx = x - xp(ilow)
  p = table( ilow, jlow ) + sx(itop, jlow) * dx
  q = table( ilow, jtop ) + sx(itop, jtop) * dx
  xylint = p + ( q - p ) * (y - yp(jlow) ) * vdy(jlow)
END
SUBROUTINE intval( itop, x, n, array, below, above )

* Locates enclosing interval, searching from last one.
* Interval is specified by index at higher value.
* Stops if out of range, with below or above message

CHARACTER*(*) below, above
REAL array(*)

IF( x .GT. array(itop) ) THEN
  Search from there up
  DO 10 k = itop + 1, n
      IF x .LE. array(k) THEN
          itop = k
          GO TO 30
      ENDIF
  10 CONTINUE
  Here, x is above array
  itop = npres
  PRINT *, above
  RETURN
ELSEIF ( x .LT. array(i - 1) ) THEN
  Search down from there
  DO 20 k = itop - 2, i, -1
      IF x .GE. array(k) THEN
          itop = k + 1
          RETURN
  20 CONTINUE
  Here, x is below array
  PRINT *, below
  STOP
ENDIF
END
SUBROUTINE XYset( nx, xp, ny, yp, table, sx, vdy )

* Precomputes slopes sx and reciprocal differences vdy for linear two-way interpolation

REAL xp( nx ), yp( ny ), table( nx, ny )

DO 20 j = 2, ny
  DO 10 i = 2, nx
    sx(i,j) = (table(i,j) - table(i-1,j)) / (xp(i) - xp(i-1))
  10 CONTINUE
  vdy(j) = 1.0 / (yp(j) - yp(j-1))
20 CONTINUE

DO 30 i = 2, nx
  sx(i,ny) = (table(i,ny) - table(i-1,ny)) / (xp(i) - xp(i-1))
30 CONTINUE

END

FUNCTION spline( i, x, a, b, c, d )

* Evaluates cubic segment for cubic spline interpolation with x(i) < x < x(i+1).

REAL a(*), b(*), c(*), d(*)

spline = a(i) + x * ( b(i) + x * ( c(i) + x * d(i) ) )

END

SUBROUTINE splin0( nx, x, y, a, b, c, d )

* Precomputes cubic spline segment coefficients a, b, c, d for spline, given x, y coordinates.
* Coded with reference to Hornbeck's Numerical Methods

PARAMETER (maxspl = 21)

REAL rhs(maxspl), dx(maxspl), gpp(maxspl),
     vdx(maxspl), x2(maxspl)

REAL a(*), b(*), c(*), d(*)

* Set up right hand side of equations (4.30)

nxml = nx - 1
DO 10 i = 1, nxml
  rhs(i) = y(i+1) - y(i)
  dx(i) = x(i+1) - x(i)
  vdx(i) = 1. / dx(i)
10 CONTINUE
10 CONTINUE  
   DO 20 i = nxm1, 2, -1  
      rhs(i) = ( rhs(i) - rhs(i-1) ) / dx(i)**2  
20 CONTINUE  
*  
*   Solve the tri-diagonal system (4.30) for gpp(i), the  
*      second derivative divided by 6,  
*   by flowchart of Fig. 6.3, where a(i) = c(i) = 1, b(i) = 4  
*  
   DO 30 I = nxm1, 3, -1  
      rhs(I-1) = ( rhs(I-1) - rhs(I) ) * 0.3333333  
30 CONTINUE  
   gpp(2) = rhs(3)  
   DO 40 I = 3, nxm1  
      gpp(I) = rhs(I) - gpp(I-1)  
40 CONTINUE  
*  
*   Use the natural cubic spline end conditions of (4.31) and (4.32)  
*  
   gpp(1) = 0.0  
   gpp(nx) = 0.0  
*  
*   Precompute cubic polynomial coefficients from (4.26)  
*  
   DO 50 i = 1, nx  
      x2(i) = x(i) ** 2  
50 CONTINUE  
   DO 60 i = 1, nxm1  
      dg = gpp(i+1) - gpp(i)  
      dxg = x(i+1) * gpp(i) - x(i) * gpp(i+1)  
      a(i) = ( gpp(i) * x2(i+1) + y(i) ) * x(i+1)  
      + ( gpp(i+1) * x2(i) + y(i+1) ) * x(i)  
      + dxg * dx(i)  
      b(i) = ( 3.0 * ( gpp(i+1) * x2(i) - gpp(i) * x2(i+1)  
             + y(i+1) - y(i) ) * vdx(i) - dg * dx(i)  
      + c(i) = 3.0 * dxg  
      d(i) = dg * vdx(i)  
60 CONTINUE  
END
The file 'integ.com' contains:

DOUBLE PRECISION accum, acctry, xlow, xhigh
PARAMETER ( integs = * )
COMMON / integ / h(0:1),
  + nstart( integs ), limted( integs ),
  + accum( integs ), acctry( integs ),
  + xlow( integs ), xhigh( integs ),
  + fml( integs ), trfml( integs )

SUBROUTINE uint0( x, npast )
*****************************************************************************
* Initializes any unlimited integrator.
* Loads double precision accumulator.
*****************************************************************************
* INCLUDE 'integ.com'
*
  accum(npast) = x
  nstart(npast) = 0
END
*

SUBROUTINE lmint0( x, npast, botm, top )
*****************************************************************************
* Initializes any limited integrator.
* Loads double precision accumulator and double precision limits.
*****************************************************************************
* INCLUDE 'integ.com'
*
  accum(npast) = x
  xlow(npast) = botm
  xhigh(npast) = top
  nstart(npast) = 0
END
* FUNCTION pruEul( rate, nh, npast ) selected unlimited integrator
  FUNCTION pruint( rate, nh, npast )
 ************************************************************************
  Explicit Euler as the primary unlimited integrator.
  Does not use past values. Initialized by unint0.
 ************************************************************************
  DOUBLE PRECISION x
  INCLUDE 'integ.com'

  x = accum(npast) + rate * h(nh)
  accum(npast) = x
  pruint = x
  pruEul = x  reactivate to deselect, but compile Euler.
END

* FUNCTION pruAB2( rate, nh, npast )
  FUNCTION pruint( rate, nh, npast ) AB2 is not currently selected.
 ************************************************************************
  Modified Adams-Bashforth 2nd Order as unlimited primary.
  Uses one past rate (right hand side f) value.
  Euler is used once for starting value. Initialized by unint0.
 ************************************************************************
  DOUBLE PRECISION x
  INCLUDE 'integ.com'

  IF ( nstart(npast) .EQ. 0) THEN
    x = accum(npast) + rate * h(nh)
    nstart(npast) = 1
  ELSE
    x = accum(npast)
    x = accum(npast) + h(nh) * 
      ( 1.6 * rate - 0.6 *.fml(npast) )
  ENDIF
  accum(npast) = x
  pruint = x  reactivate to select AB2
  pruAB2 = x
  fml(npast) = rate
END
FUNCTION truEul( rate, nh, npast ) selected unlimited trial integration.
FUNCTION truint( rate, nh, npast )
************************************************************************
* Unlimited, trial Euler for use within balancing loops.
* Requires 'step' to accept trial value.
* Initialized with unint0.
************************************************************************
* DOUBLE PRECISION x
INCLUDE 'integ.com'
*
    x = accum(npast) + rate * h(nh)
    acctry(npast) = x
    truint = x
    truEul = x     reactivates to deselect, but still compile truEul.
END
*
FUNCTION truAB2( rate, nh, npast )
FUNCTION truint( rate, nh, npast ) AB2 is not currently selected
************************************************************************
* Unlimited trial Modified Adams-Bashforth 2nd Order.
* Requires 'step' to accept trial values and start itself.
* Initialized with unint0.
************************************************************************
* DOUBLE PRECISION x
INCLUDE 'integ.com'
*
    IF ( nstart(npast) .EQ. 0 ) THEN
        x = accum(npast) + rate * h(nh)
    ELSE
        x = accum(npast) + h(nh) *
            ( 1.6 * rate - 0.6 * past(npast) )
    ENDIF
    acctry(npast) = x
    trfml( npast ) = rate
    truAB2 = x
    truint = x     reactivates to select AB2
END
* FUNCTION prlEul( rate, nh, npast ) selected limited integrator
* FUNCTION prlint( rate, nh, npast )
************************************************************************
* Explicit Euler as the primary limited integrator.
* Does not use past values. Initialized by lmint0.
************************************************************************
DOUBLE PRECISION x
INCLUDE 'integ.com'

x = accum(npast) + rate * h(nh)
IF ( x .LT. xlow(npast) ) THEN
  x = xlow(npast)
ELSE IF( x .GT. xhigh(npast) ) THEN
  x = xhigh(npast)
ENDIF
accum(npast) = x
prlint = x
* prlEul = x reactivex to deselect, but compile Euler.
END

FUNCTION prlAB2( rate, nh, npast )
* FUNCTION prlint( rate, nh, npast ) AB2 is not currently selected.
************************************************************************
* Modified Adams-Bashforth 2nd Order as the primary limited integrator.
* Uses a past rate. Initialized by lmint0.
************************************************************************
DOUBLE PRECISION x
INCLUDE 'integ.com'

IF ( nstart(npast) .EQ. 0 ) THEN
  x = accum(npast) + rate * h(nh)
ELSE
  x = accum(npast) + h(nh) *
    ( 1.6 * rate - 0.6 * fml(npast) )
ENDIF
IF ( x .LT. xlow(npast) ) THEN
  x = xlow(npast)
nstart(npast) = 0
ELSEIF( x .GT. xhigh(npast) ) THEN
  x = xhigh(npast)
nstart(npast) = 0
ELSE
  fml(npast) = rate
ENDIF

END

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nstart(npast) = 1
ENDIF
accum(npast) = x
* prlint = x     reactivate to select AB2
prlAB2 = x
END
*
FUNCTION trlEul( rate, nh, npast ) selected limited trial integrator
FUNCTION trlint( rate, nh, npast )
************************************************************************
* Explicit Euler as the trial limited integrator.
* Does not use past values. Initialized by imint0.
*
************************************************************************
DOUBLE PRECISION x
INCLUDE 'integ.com'
*
IF ( nstart(npast) .EQ. 0 ) THEN
  x = accum(npast) + rate * h(nh)
ELSE
  x = accum(npast) + h(nh) * 
     ( 1.6 * rate - 0.6 * fml(npast) )
ENDIF
IF ( x .LT. xlow(npast) ) THEN
  x = xlow(npast)
ENDIF
acctry(npast) = x
trlint = x
trlEul = x     reactivate to deselect, but compile Euler.
END
*
FUNCTION trlAB2( rate, nh, npast )
FUNCTION trlint( rate, nh, npast ) AB2 is not currently selected.
************************************************************************
* Modified Adams-Bashforth 2nd Order as the trial limited integrator.
* Uses one past rate value. Initialized by imint0.
************************************************************************
DOUBLE PRECISION x
INCLUDE 'integ.com'
*
IF ( nstart(npast) .EQ. 0 ) THEN
  x = accum(npast) + rate * h(nh)
ELSE
  x = accum(npast) + h(nh) * 
     ( 1.6 * rate - 0.6 * fml(npast) )
ENDIF
IF ( x .LT. xlow(npast) ) THEN
  x = xlow(npast)
limited(npast) = .TRUE.
ELSEIF( x .GT. xhigh(npast) ) THEN
  x = xhigh(npast)
  limited(npast) = .TRUE.
  nstart(npast) = 0
ELSE
  trfml(npast) = rate
  limited(npast) = .FALSE.
ENDIF
accum(npast) = x
* trlint = x   reactivate when selecting AB2
trlAB2 = x
END
* FUNCTION stpEul( npast ) selected as the trial value acceptor
FUNCTION step( npast )
************************************************************************
* Euler step. Accepts trial accumulator as step accumulator.
* Returns accepted value in single precision
************************************************************************
DOUBLE PRECISION x
INCLUDE 'integ.com'
x = acctry(npast)
accum(npast) = x
step = x
* stpEul = x   reactivate to deselect, but compile stpEul
END
* FUNCTION stpAB2( npast )
FUNCTION step( npast )
************************************************************************
* Modified Adams-Bashforth 2nd Order step accepts trial accumulator and
* past rate, and starts itself.
************************************************************************
INCLUDE 'integ.com'
x = acctry(npast)
accum(npast) = x
stpAB2 = x
* step = x   reactivate to select as acceptor of trial values
fml(npast) = trfml(npast)
IF ( limited(npast) ) THEN
  nstart(npast) = 0
END
ELSE
  nstart(npast) = 1
ENDIF
END

FUNCTION trflow( W, Z, R, P, npast )
**********************************************************************************************
*                                  Trial unlimited flow integration, previously                 *
*                                  FUNCTION FLOW( W, Z, R, T, P).                             *
* * Trial integration of flow acceleration of form                                           *
*  dW/dt = ( pressure - resistance * W**2 )/z                                               *
* * THIS IS THE FUNCTION TO CALCULATE THE FLOW RATE OF A INCOMPRESSIBLE FLOW                *
* ON A GIVEN DUCT WITH KNOWN INERTIA (Z), AND NORMALIZED RESISTANCE (R = RESISTANCE/FLOW DENSITY). *
* INPUT PARAMETERS ARE PREVIOUS FLOW RATE (W), PRESSURE DIFFERENCE (P) AND                  *
* INTEGRAL TIME INTERVAL (T).                                                             *
*
COMPILER (LINK=IBJS$)
DOUBLE PRECISION ZI,RI,TI,WI,PI,A,B,C
REAL W,Z,R,T,P

WILL COMPUTE NEGATIVE FLOW
  W = LAST VALUE OF FLOWRATE
  Z = INERTIA,L/AG
  R = RESISTANCE
  T = DELTA TIME
  P = DELTA PRESSURE

UNDER THE GIVEN CONDITION THE FLOW ACCELERATION IS GIVEN BY:
  DDW=(P - R * (W**2))/Z
IF W' IS THE NEXT FLOW VALUE AFTER TIME INTERVAL T THEN
  DDW = (W' - W)/T
AND THE W' CAN BE APPROXIMATED BY THE FOLLOWING STEADY STATE CONDITION
  (W' -W)/T = (P - R * (W'**2))/Z
W' IS THE ONLY UNKNOWN IN THE EQUATION.

DUMMY VARIABLES
  Z1 =DBLE(Z)
  R1 = ABS(DBLE(R))    repeatedly converts an unchanging variable
  T1 =DBLE(T)
  W1 =DBLE(W)
  P1 =DBLE(P)
  A = Z1/2.D0/R1/T1    requires two unnecessary divisions
  B = A * 2.D0*W1
  C = P1/R1

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The above use of implicit Euler, without any iterative correction, is not justified, and is implemented in a costly manner.

The simulation step $h = dt$ is always used.

The replacement uses the selected trial integrator, in limited and unlimited forms. The flow rate is computed in single precision, using the previous $W$. Because of the possible limit, the integrator is initialized by `imint0`, with a practically infinite upper limit.

A call to `step` is required to accept trial values.

```plaintext
FUNCTION prflow( W, Z, R, P, npast )

* Primary flow integration, for use outside of balancing loops.
* Uses the selected primary integrator in limited and unlimited forms.
* Initialized by `imint0`, with a practically infinite upper limit.
*
```

```plaintext
IF ( R .GE. 0.0 ) THEN
   prflow = prlint( (P - R * W**2)/Z, 0, npast )
ELSE
   prflow = pruint( (P - R * W**2)/Z, 0, npast )
ENDIF
END
```
change.com contains:

PARAMETER ( maxchg = 16 )
COMMON / change / chgtol, rxfact( maxchg ), change( maxchg )

FUNCTION relax( okloop, xnew, xold, ix )
***********************************************************************
* Applies relaxation factor to monitored variable changes.
* Counts iterations in which relative change is over tolerance.
* Returns relaxed change value.
* For converging values ix, increase rxfact(ix) above 1.0 to speed up
* convergence. Keep it less than 2.0.
* For slow converging values ix, try decreasing rxfact(ix) below 1.0.
***********************************************************************

LOGICAL ok, okloop
INCLUDE 'change.com'
INCLUDE 'out.com'

diff = xnew - xold
change(ix) = diff / xold
ok = ABS( change(ix) ) .LE. chgtol
okloop = okloop .AND. ok
IF ( .NOT. ok ) its(ix) = its(ix) + 1
relax = xold + diff * rxfact(ix)
END

SUBROUTINE its0
***********************************************************************
* Initialize balancing iteration counts
***********************************************************************

INCLUDE 'out.com'
INCLUDE 'change.com'

DO 10, I = 1, maxchg
its(I) = 0
10 CONTINUE
END
SUBROUTINE wrchg( iter, nfirst, nlast, heading )

* Writes change monitor counts and last changes to event file
* Allows no more than one full report per 100 iterations, but
* reports the number of non-converging iterations of any kind
* not reported.

CHARACTER*(*) heading
INCLUDE 'change.com'
DATA / last, nskipd / -100, 0 /
SAVE last, nskipd

IF ( iter - last .GE. 100 ) THEN
  WRITE( event, '( A, I6 / A )' )
  heading, iter, ' item iterations over last change'
  DO 10, I = nfirst, nlast
    WRITE( event, '( I3, 10X, I, CONTINUE
      I, its(I), change(I)
    10 CONTINUE
    last = iter
    IF ( nskipd .GT. 0 ) THEN
      WRITE( event, '(I4, A )' )
      nskipd + 1
    ENDIF
  ELSE
    nskipd = nskipd + 1
  ENDIF
END
* The x to the y module, supporting degrees of normalization.
* Implements x to y through table lookup and linear interpolation.

* FUNCTION Xnl0th( Xnorm, Nl0th ) ****************************
* Table lookup of ( normed X ) ** (0.1*Nl0th), for 0 < Nl0th < 10,
* where 0.0 < normed X < 1.0
****************************************************

REAL X10(0:10, 0:18)
DATA ( X10(0, J), J = 0, 18 ) / 19 * 0.0 /
DATA ( X10(1, J), J = 0, 18 ) /
+ 0.0, .6780, .7254, .7551, .7770, .7945, .8090, .8216, .8326,
+ .8424, .8514, .8870, .9126, .9333, .9503, .9650, .9780, .9896,
+ 1.0 /
DATA ( X10(2, J), J = 0, 18 ) /
+ 0.0, .4596, .5261, .5702, .6037, .6311, .6545, .6750, .6932,
+ .7097, .7248, .7867, .8329, .8708, .9031, .9313, .9564, .9792,
+ 1.0 /
DATA ( X10(3, J), J = 0, 18 ) /
+ 0.0, .3113, .3816, .4305, .4690, .5013, .5295, .5545, .5772,
+ .5979, .6171, .6976, .7602, .8126, .8582, .8987, .9354, .9690,
+ 1.0 /
DATA ( X10(4, J), J = 0, 18 ) /
+ 0.0, .2108, .2767, .3250, .3643, .3983, .4284, .4555, .4805,
+ .5037, .5254, .6186, .6937, .7582, .8154, .8672, .9147, .9589,
+ 1.0 /
DATA ( X10(5, J), J = 0, 18 ) /
+ 0.0, .1427, .2006, .2453, .2830, .3164, .3465, .3742, .4001,
+ .4243, .4473, .5485, .6330, .7075, .7748, .8369, .8946, .9488,
+ 1.0 /
DATA ( X10(6, J), J = 0, 18 ) /
+ 0.0, .0965, .1454, .1851, .2199, .2513, .2803, .3075, .3331,
+ .3575, .3808, .4862, .5775, .6601, .7363, .8076, .8748, .9390,
+ 1.0 /
DATA ( X10(7, J), J = 0, 18 ) /
+ 0.0, .06519, .1030, .1397, .1708, .1996, .2268, .2526, .2773,
+ .3011, .3242, .4310, .5269, .6158, .6996, .7792, .8555, .9290,
+ 1.0 /
DATA ( X10(8, J), J = 0, 18 ) /
+ 0.0, .04401, .0762, .1054, .1326, .1585, .1834, .2075, .2309,
+ .2537, .2760, .3820, .4807, .5746, .6647, .7519, .8366, .9193,
+ 1.0 /
DATA ( X10(9, J), J = 0, 18 ) /
+ 0.0, .02969, .05525, .07953, .1030, .1259, .1484, .1704, .1922,
+ .2137, .2350, .3385, .4385, .5360, .6315, .7255, .8181, .9096,
+ 1.0 /
DATA ( X10(10, J), J = 0, 18 ) /
+ 0.0, 0.02, 0.04, 0.06, 0.08, 0.10, 0.12, 0.14, 0.16,
+ 0.18, 0.2, 0.3, 0.4, 0.5, 0.6, 0.7, 0.8, 0.9,
IF ( Xnorm .GE. 0.2 ) THEN
    U = Xnorm * 0.1
    V = AINT( U )
    I = INT( V ) + 8
ELSE
    U = Xnorm * 0.02
    V = AINT( U )
    I = V
ENDIF
Xn10th = X10( N10th, I ) + (U - V) * X10( N10th, I + 1)
END

FUNCTION X10th( X, N10th )

IF ( X .GT. 1.0 ) THEN
    X10th = 1.0 / Xn10th( 1.0 / X, N10th )
ELSE
    X10th = Xn10th( X, N10th )
ENDIF
END

FUNCTION XntoYn( Xnorm, Ynorm )

UX = Xnorm * 0.1
VX = AINT( UX )
J = VX
UX = UX - VX
UY = Ynorm * 0.1
VY = AINT( UY )
I = VY
XnYlo = X10(I, J) + UX * X10(I, J + 1)
XnYhi = X10(I + 1, J) + UX * X10(I + 1, J + 1)
XntoYn = XnYlo + (UY - VY) * XnYhi
END

FUNCTION XtoY( X, Y )

IF ( Y .GT. 1.0 ) THEN
    UY = AINT( Y )
END
N = UY
VY = Y - UY * 10.
IF ( X .GT. 1.0 ) THEN
    XtoY = 1.0 / XntoYn( 1.0 / X, VY )
ELSE
    XtoY = XntoYn( X, VY )
ENDIF
XtoY = XtoY * X ** N
ELSE
    IF ( X .GT. 1.0 ) THEN
        XtoY = 1.0 / XntoYn( 1.0 / X, Y )
    ELSE
        XtoY = XntoYn( X, Y )
    ENDIF
ENDIF
ENDIF
END
PARAMETER (nints = 16, nreals = 551)
INT INTEGER inidx, rlidx
COMMON /output/ ninsel, nralsel,
+ inidx( nints ), rlidx( nreals )

SUBROUTINE writeset( time, runid )

* Reads the set of write variables from the 'select.out' file
* Saves set numbers and headings for collection of data during
* the simulation run
* Opens the output variable file, and writes on it:
  * an 80-character identifying header from 'ssme.run'
  * an 80-character identifying header from 'select.out'
  * the time interval between data records
  * the numbers of selected integer and real output variables
  * indexes of selected integer and real output variables
  * names of selected integer and real output variables

INCLUDE 'units.com'
INCLUDE 'output.com'

CHARACTER*8 name
CHARACTER*1 ok

OPEN( UNIT = set, FILE = 'select.out', STATUS = 'OLD',
+ ERR = 1 )
GO TO 2
1 PRINT *, 'The ''select.out'' file was not found.'
STOP

2 OPEN(UNIT = out, FILE = 'ssme.out', STATUS = 'NEW',
+ ERR = 3 )
GO TO 5
3 PRINT *,
+ 'Is it OK to overwrite the ''ssme.out'' file? (y/n)' READ *, ok
IF( ok .EQ. 'y' .OR. ok .EQ. 'Y' ) THEN
  OPEN(UNIT = out, FILE = 'ssme.out', STATUS = 'OLD' )
ELSE
  STOP
ENDIF

5 WRITE( out, '(A)' ) runid
READ( set, '(A)' ) slctid
WRITE( out, '(A)' ) slctid

WRITE(out) time
* Count integer variables and save integer indexes and headings

```
ninsel = 0
DO 10, i = 1, nints
   READ( set, '( I1, 1X, A8 )' ) iyes, name
   IF ( iyes .EQ. 1 ) THEN
      ninsel = ninsel + 1
      inidx( ninsel ) = i
      inhead( ninsel ) = name
   ENDIF
10 CONTINUE
* Write unformatted: integer outputs, indexes and headings

WRITE( out ) ninsel
IF ( ninsel .GT. 0 ) THEN
   WRITE( out ) ( inidx( i ), i = 1, ninsel )
   WRITE( out ) ( inhead( i ), i = 1, ninsel )
ENDIF
* Count real variables and save real indexes and headings

nrlsel = 0
DO 20, i = 1, nreals
   READ( set, '( I1, 1X, A8 )' ) iyes, name
   IF ( iyes .EQ. 1 ) THEN
      nrlsel = nrlsel + 1
      rlidx( nrlsel ) = i
      rlhead( nrlsel ) = name
   ENDIF
20 CONTINUE
* Write unformatted: real outputs, indexes and headings

WRITE( out ) nrlsel
IF ( nrlsel .GT. 0 ) THEN
   WRITE( out ) ( rlidx( i ), i = 1, nrlsel )
   WRITE( out ) ( rlhead( i ), i = 1, nrlsel )
ENDIF
END
* SUBROUTINE writer( STIME )

******************************************************************************
* Collects and writes selected output data for one output interval
* The data is written unformatted.
******************************************************************************
* DIMENSION idata( nints ), rdata( nreals )
* INCLUDE 'output.com'

91
INCLUDE 'units.com'
COMMON /outvar/ ivar( nints ), rvar( nreals )

* 
DO 10 i = 1, ninsel
   idata(i) = ivar( inidx(i) )
10 CONTINUE
WRITE( out ) STIME, (idata(i), i = 1, ninsel)

* 
DO 20 i = 1, rlnsel
   rdata(i) = rvar( rlidx(i) )
20 CONTINUE
WRITE( out ) (rdata(i), i = 1, nrlsel)
END

92
The next section presents data COMMON blocks. The BLOCK DATA module initializes labeled COMMON blocks.

**BLOCK DATA**

***********************************************************************
* Labeled COMMON blocks are defined in files '*.com'
* This module initializes labeled COMMON
* COMMON blocks have been reorganized to the following extent:
* 1) output variables of all modules have been moved to a single
   labeled COMMON block 'outvars' in 'outcom'
* 2) other variables recognized as not shared between modules were
   removed from COMMON blocks
***********************************************************************

**COMMON /FUEL/ fuels(59)
DATA fuels / 59 * 0. /
**COMMON /hgas/ gasses(55)
DATA gasses / 55 * 0. /
**COMMON /oxid/ oxids(71)
DATA oxids / 71 * 0. /
**COMMON /oxidil/ oxdils(13)
DATA oxdils / 13 * 0. /
**COMMON /contrl/ rcons(55), icons(8)
DATA rcons, icons / 55 * 0., 8 * 0 /
**COMMON /balc/ balcs(73)
DATA balcs / 73 * 0. /
**COMMON /valves/ vals(115)
DATA vals / 115 * 0. /
**COMMON /pogo/ pogos(5)
DATA pogos / 5 * 0. /
**COMMON /outvar/ ITS(16), outs(564)
DATA outs / 564 * 0. /

**INCLUDE 'fgen.com'
DATA /now, (npts(i), i = 1, NCURVE) /1, NCURVE * 0 /
**INCLUDE 'integ.com'
DATA nstart, limited / intogs * 0, intogs * .FALSE. /

**END**

**SUBROUTINE IniCom**

***********************************************************************
* Initializes blank common not otherwise initialized.
*
**COMMON DT, STIME, Reals(28)**

DO 10 I = 1, 28
   Reals(I) = 0.
10 CONTINUE
**END**

**COMMON/outvar/**

+ **ITS(16),**
+ **ABMOV,** ACCV, AFPOV, AGC, AHPV,
+ **AIN,** AMFV, AMOV, APOOV, APV,
+ **ATH,** DDW1, DX, DPFPAS, DPOP1,
+ **DPOPAS,** DQHEAT, DPHGMF, DPHGMO, DTPSTH,
+ **DTPSTL,** DW(13), DW1(3), DW2(3), DW10P,
+ **DW3P,** DW4P, DW7P, DW8P, DWC,
+ **DWCOD,** DWCOD1, DWCOD2, DWF, DWFBPV,
+ **DWFI,** DWIF(6), DWFNP, DWFPF, DWFO,
+ **DWFOPO,** DWFPFR1, DWFPFR2, DWFT1, DWFT2,
+ **DWG,** DWGAS, DWGO, DWGOP, DWH,
+ **DWHO,** DWHOP, DWIO, DWMC, DWMCP,
+ **DWMOV,** DWO, DWOE2, DWOE3, DWFIG(3),
+ **DWFN,** DWNIG(3), DWNB, DWNB3, DWOI,
+ **DWOIN,** DWOPF, DWOPL, DWOPI, DWO2,
+ **DWOP3,** DWOP3C, DWOPO, DWOP1, DWOPI,
+ **DWOPV,** DWOS, DWOT1, DWOT1D, DWOT1I,
+ **DWOT2,** DWOTJ, DWPO, DWFPF, DWPOI,
+ **DWQNCN,** DWRE, DWSFS, ELCOM, ELENT,
+ **ELFC,** ELFCM, ELLFI, ELFFP, ELFFPM,
+ **ELFOP,** ELFOPM, ELOG, EMRC, EMRCR,
+ **EMRE,** EMRF, EMAF, EMRO, EMROPO,
+ **EPC,** ERROR, EETA1, EETA2, ETAOT1,
+ **FAC,** FCOMP, FHEOD1, FHEOD2, FHEO1I,
+ **FHEOP1,** FHEOT1, FR, GF1, GF2,
+ **H(13),** H3, H10P, H7P, H8P,
+ **HCAVP1,** HCAVP2, HCAVP3, HOD2, HOD3,
+ **HOT2,** HOS, HOS1, HOT1, HP,
+ **HT,** OD,
+ **P(13),** P1, P10P, P1NP5, P2,
+ **P2NP5,** P3NP5, P4(3), P7P, P8P,
+ **PANS,** PCFPO, PCIE, PCIG, PCNS,
+ **PCPO,** PCTPERT, PD, PFI, PFP,
+ **PFPO,** PFPOI, PFPOV, PFS,
+ **PFSP,** PFSP1, PFSPF, PFSP1, PG,
+ **PGI,** PGCO, PHES, PIF(6), PIL(12),
+ **PMOV,** POD1, POD1M, POD2, POD3,
+ **POI1,** POI2, POINJ, POINVP, POJ,
+ **POP,** POPOI, POPOV, POPOV,
+ **POS,** PPOPURG, PPOUS, PRFT2,
+ PROTI, PROT2, PT, PTOL, QINI(13), 268
+ QB(13), QBFLO, QF, QINT, QIN1(13), 297
+ QOUT1(13), QOUT2(13), 323
+ R1(3), R2(3), R3(3), 332
+ RBPV, RCCV, RCOM, 335
+ RFPOV, RHO1(13), RHO10P, RHO7P, RHO8P, 352
+ RHOD1, RHOD2, RHOGOX, RHOHE, RHOHI, 357
+ RHOI2, RHOLO, RHOMOV, RHOOS, RHOP, 362
+ RHOP1, RHOP3, RHEREC, RHT, RHT1, 367
+ RJTPVD, RMFV, RMOV, RON, ROPOV, 372
+ RR(13), RVASE, 386
+ SCUT, SF1, SF2, S01, S02, 407
+ SRATE, STOPT, SU(13), SU10P, SUOD2, 412
+ SU7P, SU8P, SUCOD1, SUOD1, SUOD2, 428
+ SUO12, SUOIN, SUOT1, T(13), TFI, 433
+ TCAVP1, TCAVP2, TCAVP3, TEMP, TFI1D, 438
+ TFLS, TFP, TFP1, TFPM, TFP1, 438
+ TFT2D, TFTP2DI, TGAS, TETA(5), TETA1(5), 451
+ THTA2(5), TOP, TOPM, TOT2D, 459
+ TOT2DI, TP(5), TPERT, TRQFP1, TRQFP2, 468
+ TRQFT1, TRQFT2, TRQOP1, TRQOP2, TRQOP3, 473
+ TRQOT1, TRQOT2, TSAT, TSTART, TSTOP, 478
+ TW, TW1(13), TW2(13), UG, UOD1, 505
+ U, UCF2T, UCOT2, UO12, UOIN, UP, 510
+ UOD2, UO12, UOIN, UOT1, UP, 515
+ VG, VHEOD1, VHEOD2, VHEO12, VHEOT1, 520
+ VL, VOLPV, WHE, WHECD1, WHECD2, 527
+ WFPOI, WGOX, WHE, WHECD1, WHECD2, 532
+ WHEOD1, WHEOD2, WHEO12, WHEOT1, WLOX, 532
+ WCOM, WOD1, WOD2, WOI2, WOIN, 537
+ WPOI, WOT1, WT1BK, WT2BK, WTASI, 542
+ WTIGN, X1, X2, X3, XCCV, XHVP, 547
+ XCFPOV, XCOPOV, XFP0V, XGC, XHVP, 552
+ XCMFV, XCMOV, XMFP, XMOV, XOPOV, 557
+ YCCCV, YCFPOV, YCMFV, YCMOV, YCOPOV, 562
+ ZCOM, ZOIN, 564

'blank.com':

*  
par
COMMON DT, STIME,  
par par
+ QIN2(13), AOPTO, RFT1V, PA, RHOO3, PFPD, DWCCV,  
par par par  
+ DWOPC, RHOOP2, RHOOP3, RFBV, ROBV, DPR, DPL, PINMC, TCUT  

95
'fuel.com':

    COMMON /FUEL/
    *        par     par:4,5,6,12  par
    +   VOL(13), R(13), AHT1(13), AHT2(13), PFP1R, PFP2R, TFT1
    *        PRFT1, DWFT2C, TTI, UCFT1

'hgas.com'

    COMMON /HGAS/  CFOI, RFPO, WFPF, WFPO,
    *        +   TFPc, CFPF, GAMFP, EMWFP, RGCFP, WTPP, WFP,
    *        +   WOPOI, COOI, ROPO, WOPF, Wopo, TOPC, CPOp,
    *        +   GAMOP, EMWOP, RGCP, WTOP, WOP,
    *        +   WTOT1, WDMU, TOT1, POT1A, TOT1D, WTI, GAMFI,
    *        +   WFIF, WFIO, RGCFI, WCO, WC, WTC, TC, WCF, RGCC, GAMC,
    *        +   WOPOV, WFPPOV, RFPIGB, RPOPIGB, RHOOFT,
    *        +   ROHOTF, ROHOFI, DWFTF, PX, DWX, PXF, DWXF,
    *        +   DWACV, DWPS, DWBAF

'oxid.com':

    COMMON /OXID/  DPOP2, DPOP3, PRIMO1,
    *        +   WOI, RHOOP1, POP1R, POP2R, POP2A,
    *        +   POP3R, DDWOS, QO, TOS, TOD2, WOV, H1, H2,
    *        +   ZPO, ZOPO, U1, U2, U3, HLPT1, HIOP2, H3I,
    *        +   ULPOT, HLPOTD, TOD1, TOI2, TOD3,
    *        +   UOD1, WOD1, RHOD1, HOD1,
    *        +   UOI2, SUOI2, RHOI2, UOD2, UOT1, WOT1, ZCOM, RCOM,
    *        +   ROIN, ZOIN, RJTPD, TCAVP3,
    *        +   UCOD1, WCOD1, RHOC01, QC0D1, PCOD1,
'contrl.com':

COMMON /CONTRL/ TIMEVC, TIMEPR, TIMECP, TIMETR, TIMFME,
* + TIMFMC, TIMMRF, TIMFMA, TIMELM, EMRGC,
* + DXFPOV, EPCGC, DXOPOV, XCRV, PCOPOI, TO, DXMFV, XCCV, DXCCV,
par par par par par par
+ TPA, PCMALF, ABCCV, ABMFV, ABOPO, ABFPO, RH0H,
* + DTMC, FRADS, ORADS, RH00,
* + PIPF, PIPO, QF0, Q0,
par par
+ XCMOVC, DTFMRA, TSMFV, RESET, XOPLIM,
par
+ PNOISE, PFRNZ, PMRNZ, TOPEN, FRFZ, EMRFZ,
* + POPVNZ, PFPVNZ, PMOVNZ, PMFVNZ, PCCVNZ,
* + FZOPV, FZFPV, FZMOV, FZMFV, FZCCV,
* + NCF, NCO, IFIND, IOIND, KOUNTF, KOUNTO,
* + MODESTST, IPFLAG

'valves.com ':    

COMMON/VALVES/
out
+ DTHETA(5), ESAC(5), DESA(5), ESA(5), DESV(5), ESV(5),
* + VS(5), EMF(5), DVM(5), VM(5),
* + THET1L(5), THET2L(5),
* + ISTIC(5), IHYS(5), VR(5), DTHETL(5),
par par par par par
+ AD(5), BD(5), CS(5), CPS(5), DSS(5), ESS(5), VPD(5)

'igni.com':

97
COMMON /IGNI/ TCIG(3), ELFIG(3), DW3(3), TF(3), PFU(3)

'balc.com':

* COMMON/BALC/ AHT14, AHT15, AHT16, AHT112,
  par par par par par par par par
  + CDPFP1, CTQFP1, CDPFP2, CTQFP2, CTQFT1, CDPOP1, CTQOP1,
  par par par par par par par par
  + CDPOP2, CTQOP2, CDPOP3, CTQOP3, CTQOT1, FT2S, AFT2, CTQFT2,
  par par par par par par par par par
  + EOT2S, AOT2, CTQOT2, AFI, EFFCM, ACN, THRSTC, AHTC4, AHTC5,
  par par par par par par par par par
  + AHTC6, DMOT2, DMFT1, DMFT2, CP(5), ANOT1, BNOT1, CNOT1, AOT1,
  par
  + BOT1, R4, R5, R6, R7, R8, R9, R10, R11, R12, R13,
  par par par par par par par par par
  + RFCOD, RFMCF, RFMCO, RACV, RBAF, RPFS, RSFS, RFPFI, ROPFI,
  par par par par par par par par par
  + RITN, RMCI, ROS, RFPOI, ROPOI, RFPOL, ROPOI, RFT2C, ROP2C,
  par par par par par par par
  + ROI, ROCOD, RMOVL, ROP3C, ROT1F, QHT412, TFACT

'pogo.com'

COMMON /POGO/ P2, RHOREC, TGAS, XGC, XHPV
PROGRAM SSME

***********************************************************************************************************************************************
*  This version of the Space Shuttle Main Engine Simulation has
*  been written to provide an efficient vehicle for the study of
*  life-extending modes of operation through knowledge-based control.
*  
C
C
C

PROGRAM FLOW:
*  Read Run Parameters from rundata file designated in the command line
*  IF restart requested THEN
      *  Initialize run data from restart file
*  ELSE
      *  Initialize for normal zero start
*  ENDIF
*  REPEAT
      T <- T + DT
      IF perturbing THEN
         *  add perturbations(T)
      ENDIF
      CALL FUELF() FOR FUEL FLOW CALCULATION
      CALL OXIDF() FOR OXID FLOW CALCULATION
      CALL HOTGAS() FOR HOT GAS CALCULATION
      CALL CTROL() FOR CONTROLLER SIMULATION
      CALL VALDY() FOR VALVE DYNAMIC SIMULATION
      Calculate closed loop variables
      IF T = output time THEN
         *  Write archival and display output
      ENDIF
      UNTIL T = stop time
      IF resume desired THEN
         *  Generate resume file
      ENDIF
C
END OF SIMULATION
C
INCLUDE 'change.com'
   Call IniCom0

*** Removed "no effect" initializations.
*
*** Removed commented out calls to ERRSET
C
C
FOLLOWING FILES ARE USED FOR SIMULATION INPUTS AND OUTPUTS
C
DTMINP.DAT: MAIN INPUT FILE FOR BASIC PARAMETERS
C NZR100.DAT: RESTART AT 100% STEADY STATE
C START4.DAT: PATCH FILE USING "NAMELIST" READING
C OUT2.DAT: MAIN OUTPUT FILE
C PERTINP.DAT: PERTURBATION SERIES INPUT FILE
C RESULTS.DAT: QUICK GLANCE OUTPUT FILE FOR PCIE AND MIX-RATIO
C STATE.DAT: OUTPUT FILE OF SELECTED IMPORTANT VARIABLES
C     PLOT2.DAT: PLOT FILE FOR DEFINED PLOTTER
C
* Assignments of unit numbers are system dependent. Assignments are
* made global by Common /units/
  run = 2
  dat = 3
  prt = 4
  str = 6
  res = 8
  out = 9
  dsp = 1
* Input/output files are specified on the command line, when possible.
* For Fortran giving no access to the command line, use pre-assigned
* file names:
  rundat = 'ssme.run'
  functs = 'ssme.dat'
  output = 'ssme.out'
  pertrb = 'ssme.ptb'
  restart = 'ssme.rst'
  atstop = 'ssme.end'
* HP-UX command line: ssme rundat output [ pertrb ] [ restart ] [resume]
* CALL getarg( 2, rundat )
* CALL getarg( 3, output ), etc.
* OPEN( UNIT = run, FILE= rundat, STATUS='OLD')
OPEN( UNIT = dat, FILE= functs, STATUS='OLD')
C
read( run,'(A // 2X, 6(2X,L12) ) title, restrt, resume, pertb
* loading blank common:
+ DT, DPR, DPL, DPUN, TPUN, TSTOP,
+ TPA, PCMALF, DTVC, DTPR, DTCVP, DTTR, SSM42200
+ DTFMRE, DTFMC, DTMRFC, DTFMRA, DTMCX, DTLM
* READ( run, '(/2X, 2I12, 4F12.4)' )
+ NONZRO, MODESTST, PCTPERT, TOPEN, TPERT, DTPERT SSM42240
READ( run, 30) TSTART, TPRINT2, TPLT2
Relaxation factors for energy balance convergence
READ( run, 30) rxfact
30 FORMAT(/2X,6(G10.4,2X))
* loading BALT common:
READ(run, 30)
+ AHT1(4), AHT1(5), AHT1(6), AHT1(12), CDPFP1, CTQFP1,
+ CDPFP2, CTQFP2, CTQFT1, CDPOP1, CTQOP1 CDPOP2
+ CTQOP2, CDPOP3, CTQOP3, CTQOT12, FT2S, AFT2,
READ(run,30) TLOW, THIGH, (TPRINC(I), I=1,6)
READ(run,'(/2X,3III2)') NOUTD, IREDAT, ISAVE
IF pertb THEN
   OPEN( UNIT = prt, FILE = pertrb, STATUS='OLD')
ENDIF
IF restrt THEN
   OPEN( UNIT = str, FILE = restart, STATUS='OLD')
ENDIF
IF resume THEN
   OPEN( UNIT = res, FILE = atstop, STATUS='NEW')
ENDIF
*
* See perturb.for for perturbation code
* All NAMELIST input has been eliminated.
* Instead, edit the input parameter file ssme.run
* All initialization echo output is gone.
* Instead, save a copy of ssme.run as documentation
*
CALL fgset(24, nerr)
PA = FGEN(24, 0.0)
RBPV = 1.0E+30
TTEMP = AMINI(2.3, TSTOP)
TIME = 0.0
TIMEVC = DTVC
TIMEPR = DTPR
TIMECP = DTCVP
TIMETR = DTTR
TIMFME = DTFMRE
TIMFMC = DTFMC
TIMMRF = DTMRFC
TIMFMA = DTFMRA
TIMELM = DTLM
C C Initialize subsystems
C
CALL FUELF0
PRINT *, 'Fuel flow parameters loaded.'
CALL OXIDF0

101
PRINT *, 'Oxygen flow parameters loaded.'
* DWFPB=DWFPF+DWOPF
CALL HOTGAS0
PRINT *, 'Hotgas parameters loaded.'
CALL CNTROL0
PRINT *, 'Control parameters loaded.'
CALL VALDYM0
PRINT *, 'Valve dynamics parameters loaded.'
CALL TRBTRQ(0.,0.,0.,0.,0.,1,1,0.,0.,0.)
CALL fgset( 26 )
CALL fgset( 27 )
CALL fgset( 40 )
*** See 'nonzro.for' for restart code
*
* Identify output variables and ready file to save output
* CALL writeset( runID )
*
* Simulation loop
*
   istop = tstop / dt
   isec = 1.0 / dt + .1
*
   DO 400 itime = 1, istop
      STIME = float( itime ) * DT
      PA = FGEN(24, 2, STIME)
      CALL FUELF
      CALL OXIDF
   * DWFPB=DWFPF+DWOPF
      CALL HOTGAS
      CALL CNTROL
      CALL VALDYM
*
* Open loop output was removed. Use offline output programs instead.
* At the print interval, a multiple of the solution interval,  
  write selected data, unformatted.
   IF ( MOD( itime, iwrite ) .EQ. 0 ) THEN
      CALL writer( STIME )
   ENDIF
*
* Write one line per second to display.
*   IF ( MOD( itime, isec ) .EQ. 0 ) THEN
      PRINT *, 'Time = ', STIME, ' seconds.'
   ENDIF
*
400 CONTINUE

102
PRINT *, 'Normal end of simulation'
END

SUBROUTINE fuelf0
***********************************************************************
* fuelf0 initializes variables.
* A second entry fuelrst does restart initialization and a time step.
* A third entry fuelf does a simulation time step only.
* IFCNTRL was eliminated.
***********************************************************************
C
C
SUBROUTINE FUELF(IFCNTI)

PURPOSE: COMPUTE FUEL FEED SYSTEM FLOW AND PRESSURE DYNAMICS SSM15200
IN THIS SUBROUTINE, THERE ARE 13 NODES DEFINED FOR THE CALCULATION OF
FLOW AND OTHER PROPERTIES OF FUEL.
1) INLET FROM FUEL TANK TO LOW PRESSURE FUEL PUMP (LPFP)
2) DUCT BETWEEN OUTLET OF LPFP AND INLET OF HPFP
3) DUCT BETWEEN OUTLET OF HPFP AND MAIN FUEL VALVE (MFV)
4) UPPER NOZZLE COOLING FLOW
5) MAIN COMBUSTION CHAMBER COOLING (BELOW THROAT)
6) MAIN COMBUSTION CHAMBER COOLING (ABOVE THROAT)
7) COOLING CONTROL VALVE (CCV) FLOW
8) MIXER OF NOZZLE COOLING (4) AND CCV FLOW (7)
9) PREBURNER SUPPLY DUCT (DISTRIBUTER NODE)
10) COOLING FLOW FROM MFV TO NODE (11)
11) DOWN COOLING FLOW TO LOWER END OF NOZZLE
12) COOLING FLOW OF LOWER 15% OF NOZZLE
13) COOLING FLOW FROM MFV TO THROAT END
THOSE NODES WITH * ARE THE ONES THAT CONTACT WITH COMBUSTION CHAMBER OR
NOZZLE AND HAVING HEAT EXCHANGE BETWEEN THEM.

C******ARGUMENT*****
INPUT: IFCNTL = INITIALIZATION ARGUMENT

C******COMMON USAGE******
INPUT:
VARIABLES
TRQFP2,PFI,PINMC,PFP,POP,QIN1,RFMV,RCCV,DWFIG
RMFV,RCCV
DWFIG
SOURCE
HOTGAS
VALDYM
IGN
SSM15300

C
OUTPUT:
VARIABLES
DWFPF,DWOF,DFWBV,DWFT2C,SF2,TW1
DW(2)
P(3),P(10),P(7),P(8),RHO(3),RHO(7),DW(3),DW(7)
DESTINATION
HOTGAS
CTRL
EMCO

103
C SUBROUTINES CALLED: PROP0, hyprop
C
***********************************************************************
*
INTEGER Tstep
LOGICAL fuelOK
*
DIMENSION ZH(13),A6(13),ZZ(13),VVOL(13),DWA(13)
DIMENSION TUBEN(13),PIFP(6),DWIFP(5),QOUT(13)
DIMENSION ACS(13),ELEN(13),DHYD(13),WW1(13),WW2(13)
DIMENSION ELENF(6),ZFL(6),ZFC(6),RIF(6)
A runtime division was replaced by a multiplication.
PARAMETER ( v9336 = 1.0 / 9336.0, v386p4 = 1.0 / 386.4 )
PARAMETER ( Tstep = 0 )
* Labelled COMMON blocks
*
INCLUDE 'units.com'
INCLUDE 'blank.com'
INCLUDE 'out.com'
INCLUDE 'fuel.com'
INCLUDE 'igni.com'
INCLUDE 'balc.com'
INCLUDE 'units.com'
*
NAMELIST/FUELFD/ELENF,ZFL,ZFC,RIF,DHYD,ELEN,AHT2,WW1,WW2,TW1,TW2
* Namelists have been eliminated, in favor of an editable input
* parameter file.
SSM15900
* Modern compilers default to dynamic memory allocation of local
* variables. The following statement requires memory for all local
* variables to be retained between calls.
SAVE
*
UNEWF( ) IS TO CALCULATE NEW SPECIFIC INTERNAL ENERGY (SU) FOR A GIVEN
* NODE WHERE INPUT FLOW (DWIN), INPUT ENTHALPY (HIN), OUTPUT FLOW (DOUT),
* NEW PRESSURE (PNEW) AND NEW DENSITY (RHONEW) ARE KNOWN.
*
UNEWF(I, DWIN, HIN, DOUT, PNEW, RHONEW) =
+ ( RHO(I)*SU(I) + VVOL(I) * 
+ ( QOUT(I) + HIN - DOUT*PNEW/( RHONEW * 9336.0 ) ) * DT ) / 
+ ( RHO(I) + VVOL(I)*DWIN*DT )
* Though the Euler form x + rate * dt appears, the function above is not
* taken to involve time integration in the usual sense. Else it should
be rewritten as the ratio of two trial integrations, as

* UNEWF(I, DWIN, HIN, DWOUT, PNEW1, RHONEW) =
* + tryint( RHO(I)*SU(I), vVOL(I) * + ( QOUT(I) + HIN - DWOUT*PNEW1/( RHONEW * 9336.0 ) ), N ) /
* + tryint( RHO(I), vVOL(I)*DWIN, N+1 )
CHGX( ) was replaced by a more detailed monitoring system for balancing iterations
Statement functions Z1 and Z2 were eliminated, to simplify maintenance.

rlimit(floor, ceiling, x) = AMAX1( floor, AMINI( ceiling, x) )

Replacing rlimit with IF ( x .LE. floor ) THEN
x = floor
ELSE IF ( x .GT. ceiling ) THEN
x = ceiling
END
would be faster, but only by straightline coding, not as a FUNCTION.

recpos(x) = AMAX1(0.,x)
recneg(x) = AMINI(0.,x)

As a mechanism for bypassing initialization code,
IF(FLAG.EQ.15.) GO TO 999
is obscure, and can be unreliable if FLAG is not initialized at load time. The function was accomplished more directly, and at no runtime cost, by the ENTRY statement.

In the initialization, the following were eliminated:
- statement function formal parameters, which created new variables unused by the simulation.
- initializations overwritten by reading input parameters
- local variables written before being read

CPH2=0.0
DDW2=0.0
DSF1=0.0
DSF2=0.0
DWFPFP=0.0
DWOPFP=0.0
HI=0.0
DO 991 I = 1, 13
   QOUT (I) = 0.0
   ZH (I) = 0.0
CONTINUE
DO 993 I = 1, 5
   DWIFP (I) = 0.0
CONTINUE

READ INPUT Parameters

READ (run, 30) (ELENF (J), J = 1, 6), (ZFL (J), J = 1, 6),
                (ZFC (J), J = 1, 6), (RIF (J), J = 1, 6)
READ (run, 30) (DHYD (J), J = 1, 13), (ELEN (J), J = 1, 13),
                (AHT2 (J), J = 1, 13), (WW1 (J), J = 1, 13),
                (WW2 (J), J = 1, 13), (TW1 (J), J = 1, 13),
                (TW2 (J), J = 1, 13), (P (J), J = 1, 13),
                (T (J), J = 1, 13), (TUBEN (J), J = 1, 13)
READ (run, 30) DWF, ELENT, ZFT1, ZCCV, ZFCOD, ZPFDP
READ (run, 30) ELEFPF, ACSFPF, ELEOPF, ACSOPF, ELENFN
READ (run, 30) HTCON, VOLFP1, VOLFP2, PCFP1, PCFP2
* READ(5,30) intentionally skipped
READ(run,30) TRQF1B, TRQF2B, TDRAGF
READ(run,'(/2X,3G12.4,I12)') GF1, GF2, PTOL, MAXL
30 FORMAT(/2X,6G12.4) SSM17910

* Namelist input and formatted echo of input parameters were eliminated.
* READ(7,FUELFD)
* WRITE(6,29)(ELENF(J),ZFL(J),ZFC(J),RIF(J),J=I,6) , etc
* This section loads fuel flow interpolated functions.
* Calls to FGEN( n, 1, x ), which reads the DTMINP file, were
* replaced by calls to fgset( n ), which reads the editable function
* file attached to unit 'dat'. Initializations recognized as
* unnecessary were removed.
*
CALL fgset( 30 )
CALL fgset( 22 )
* STIME=TIME
CALL fgset( 9 )
PT = fgen(9, 1, STIME)

* Functions of the same variable use different call numbers unless the
* interpolation intervals are identical
*
CALL fgset( 7 )
HT = fgen(7, 7, STIME)
CALL fgset( 10 )
CALL fgset( 51 )
CALL fgset( 52 )
CALL fgset( 53 )
CALL fgset( 54 )
GAMF = H2GAM0( PT, 40.0, 1 )
CALL PROP0

SF2 = 0.01
QHT412 = 0.464
RHOST = 2.552E-3
SUT = HT - PT / ( RHOST * 9336.0 )

* RHOST is reset from the t(u,rho) table, X = throwaway temperature
* CALL hyrt(SUT, RHOST, 1, PT, X )

* WRITE(6,37)DWF,PT,HT,RHOST,ELENT was removed.

* The replacement of mandatory full output by selective unformatted
* output eliminated the destination for this initialization
* documentation. DWF and ELENT echo input, and are documented by the
* 'run' unit file. PT, HT, and RHOST appear in the selectable output as
PIF(1), H(1), RHO(1), etc.

CALCULATION OF CONSTANTS AND INITIALIZATION

PIF(1)=PT
PIFP(1)=PT
DWIF(1)=DWF
DWIFP(1)=DWF
DO 71 J = 2, 5
   PIF(J)=PIF(J-1)+ELENF(J-1)*RHOT
   PIFP(J)=PIF(J)
   DWIF(J)=DWF
   CALL unint0( PIF(J), J + 27 )
71 CONTINUE
DO 72 J = 1, 5
   CALL unint0( DWIF(J), J + 23 )
72 CONTINUE
PFS = PIF(5) + ELENF(5)*RHOT
CALL unint0( PFS, 33 )
PFSP=PFSP
PIF(6)=PFS
PIFP(6)=PFS

DO 60 J = 1, 3
   RHO(J) = RHOT
   H(J) = HT
60 CONTINUE
DO 70 J = 4,13
   RHO(J)= 1.0875E-4 * P(J) / T(J)
   CALL PROP(SU(J),RHO(J),J,P(J),T(J),4) was replaced by
   CALL hyut( SU(J), RHO(J), 2 * J, P(J), T(J) )
   which adjusts SU(J) based on the p(u,rho) table, and reserves call
   points 2, ..., 27 -

   H(J) = SU(J) + P(J) / ( RHO(J) * 9336.0 )

   ACS(J) = 3.14*DHYD(J)**2/4.0*TUBEN(J) replaced by
   ACS(J) = 0.7854 * DHYD(J)**2 * TUBEN(J)

   VOL(J) = ACS(J) * ELEN(J)

   ZZ(J)=ELEN(J)/ACS(J)/386.4 replaced by
   ZZ(J) = ELEN(J) / ( ACS(J) * 386.4 )
   RR(J) = R(J)
A6(J) = HTCON / ( DHYD(J) * X10th(DHYD(J), 8) )

Interpolation of x**(-1.8) is not necessary as long as the function is used only in initialization.

DW(J) = DWF
QOUT1(J) = 0.0
QOUT2(J) = 0.0
QIN1(J) = 0.0
QIN2(J) = 0.0
CALL unint0( TW1(J), J - 1 )
CALL unint0( TW2(J), J + 9 )
70 CONTINUE

ZFS = ZZ(2) + 1.0/ZFCOD + ZZ(3) + 1./ZPFPD
ZZ(6) = ZFTI
ZZ(10) = 0.5*ZZ(11)
ZZ(11) = 0.5*ZZ(11)

Configuration constants set during initialization are documented on an output file on unit 'init'.

WRITE(init,90)(J,ACS(J),VOL(J),A6(J),ZZ(J), J=1,13)
90 FORMAT( ' J ACS VOL A6 ZZ ' )

WRITE(init,260)ZFS
260 FORMAT( '0START TRANSIENT ASSUMES PRECHILLED PUMPS AND LIQUID H2',
' THROUGH TO PUMP DISCHARGE' / ' ZFS' /1PE11.3)

DWMC = 0.0
CALL unint0( DWMC, 36 )
DWFNBP = 0.0
CALL unint0( DWFNBP, 37 )
DWFT1 = 0.0
DWFPF = 0.0
DWOFPF = 0.0
undw2c = 0.0
CALL unint0( 0.0, 23 )
ZFPF = ELEFPF/(ACSFPF*386.4)
ZOPF = ELEOPF/(ACSOFP*386.4)
SF1 = 0.01
CALL lmint0( SF1, 1, 0.1, 1.E20 )
SF2 = 0.01
CALL lmint0( SF2, 2, 0.001, 1.E20 )
TRQFP1 = 0.0
TRQFP2 = 0.0
PFT1 = 0.0
PRFTI = 1.0
TFT1 = T(6)
fgen21 = 9340.0 * fgen(21, 2, 0.0)

* Load relative change tolerance for energy balance convergence tests
*
CALL chg0( PTOL )
*
IF ( STIME .EQ. 0.0 ) RETURN

C

RESTART INITIALIZATION
C

DWFAHI = DFIG(1) + DFIG(2) + DFIG(3)
RHOPI = .5 * ( RHO(1) + RHO(2) )
PHIP1 = DW(2) / (RHOPI * SF1)
DP1 = fgen(51, 3, PHIP1) * RHOPI * SF1**2 * CDPFP1
DP1P = DP1
PHIP2 = DW(2) / (RHO(3) * SF2)
DP2 = fgen(53, 4, PHIP2) * RHO(3) * SF2**2 * CDPFP2
DP2P = DP2
PFSP = PFS
DO 2010 J=1,6
   PIFP(J) = PIF(J)
   DWIFP(J) = DWIF(J)
2010 CONTINUE

DW2P = DW(2)
CALL unintO( DW2P, 34 )
CALL unintO( DW(10), 35 )
DW100 = DW(10) + DWMC + DWFNBP + DWFAHI
DW10I = DW(3)
P4P = P(4)
P5P = P(5)
P6P = P(6)
P7P = P(7)
P8P = P(8)
P9P = P(9)
P10P = P(10)
P11P = P(11)
P12P = P(12)
P13P = P(13)
DO 2015 J=4,13
   SU(J) = H(J) - P(J) / (RHO(J) * 9336.0 )
2015 CONTINUE

CALL unintO( RHO(10), 38 )
CALL unintO( DW(11), 39 )
CALL unintO( RHO(11), 40 )
CALL unintO( DW(12), 41 )
CALL unintO( RHO(12), 42 )
CALL unintO( DW(4), 43 )
CALL unintO( RHO(4), 44 )
CALL unint0( DW(13), 45 )
CALL unint0( RHO(13), 46 )
CALL unint0( DW(5), 47 )
CALL unint0( RHO(5), 48 )
CALL unint0( DW(6), 49 )
CALL unint0( RHO(6), 50 )
CALL unint0( DW(7), 51 )
CALL unint0( RHO(7), 52 )
CALL unint0( DW(8), 53 )
CALL unint0( RHO(8), 54 )
CALL unint0( DWFPF, 55 )
CALL unint0( DWOPF, 56 )
CALL unint0( RHO(9), 57 )

* ENTRY fuelf
*********************************************************************************************************************************************
C TIME TRANSIENT CALCULATIONS
C
C DWFASI = DWFIG(1) + DWFIG(2) + DWFIG(3)
C
C STIME = TIME
C
C LOW RATE CALCULATIONS
C
C FUEL PUMP SPEEDS (RAD/SEC)
C
C IF(SFI .LT. 11.0 .AND. TRQFT1 .LT. TRQFP1+TRQF1B) THEN
C DSFI = 0.0
C ELSE
C DSFI = (TRQFT1-TRQFP1)/GFI
C END IF

* Integral limited below by 0.1

* SF1 = prlint( DSF1, delt, 1 )
C IF(SF2 .LT. 11.0 .AND. TRQFT2 .LT. TRQFP2+TRQF2B) THEN
C DSF2 = 0.0
C ELSE
C DSF2 = (TRQFT2-TRQFP2-TDRAGF)/GF2
C END IF

* Integral limited below by 0.001

* SF2 = prlint( DSF2, delt, 2 )
C
C QIN1(12)=QIN1(4)*QHT412
C QIN1(4)=QIN1(4)-QIN1(12)

DO 2050 J=4,13

111
vVOL(J) = 1.0 / VOL(J)
ZH(J) = A6(J) * HTF(T(J), P(J))

2050 CONTINUE

THE AVERAGE FLOW USED TO CALCULATE THE HEAT EXCHANGE IS THE AVERAGE OF
1) THE FLOW OF CURRENT NODE
2) THE FLOW OF UPSTREAM NODE(S)

THIS IS A VERY ROUGH ESTIMATION SINCE IT REALLY DEPENDS ON THE TIME
INTERVAL OF THE SIMULATION AND THE LENGTH OF EACH SEGMENT.

DWA(4) = ABS(0.5*(DW(12) + DW(4)))
DWA(5) = ABS(0.5*(DW(13) + DW(5)))
DWA(6) = ABS(0.5*(DW(5) + DW(6)))
DWA(7) = ABS(0.5*(DWFNB + DW(7)))
DWA(8) = ABS(0.5*(DW(7) + DW(4) + DW(8)))
DWA(9) = ABS(0.5*(DW(8) + DWFPF + DWOFP))
DWA(10) = ABS(0.5*(DW10I + DW100))
DWA(11) = ABS(0.5*(DW(10) + DW(11)))
DWA(12) = ABS(0.5*(DW(11) + DW(12)))
DWA(13) = ABS(0.5*(DWMC + DW(13)))

THE FOLLOWING SECTIONS OF PROGRAM CALCULATE THE HEAT EXCHANGE OF THE
COOLING FLOW AND THE COMBUSTION CHAMBER.

THE EQUATIONS USED IN THE PROGRAM IS DIFFERENT FROM THOSE GIVEN IN THE
SSME SPECIFICATION PP.31-32.
I BELIEVE THEY ARE THE SIMPLIFIED VERSION OF THE EQUATION.

IF THE COOLING EFFECT BECOME IMPORTANT IN THE SIMULATION THEN THE FOLLOWING
SECTION OF CODE WILL HAVE TO BE VERIFIED.

THERE ARE TWO TYPES OF HEAT FLOW OCCURED IN THE HEAT EXCHANGE
1) BY CONDUCTION DESCRIBED AS QOUT1(J) AND QOUT2(J)
2) BY CONVECTION DESCRIBED AS FUNCTION OUTPUT QFLUX().

IN THE FOLLOWING SECTION, THE REPRESENTATIONS ARE
1) QOUT1: HEAT TRANSFERED FROM MAIN COMB. CHAMBER AND NOZZLE WALLS
2) QFLUX(**1,...): BOILING HEAT FROM MCC AND NOZZLE WALLS
3) QOUT2: HEAT TRANSFERED FROM AMBIENT WALLS
4) QFLUZ(**1,...): BOILING HEAT FROM AMBIENT WALLS
5) QBM: HYDROGEN SATURATION ENTHALPY AT THE PRESSURE

One unnecessary real**real has been eliminated, and the remaining
real**.55 and real**.8 replaced by equally spaced linear interpolations.

DO 2060 J=4,13
  IF(J.GT.6.AND.J.NE.12) THEN
    Q1=0.
    QOUT2(J) = ZH(J) * XtoY(T(J)/TW2(J), .55 ) * +
                 X10th(DWA(J), 8) * (TW2(J)-T(J))
  ELSE
    dwtemp = X10th(DWA(J), 8)

112
QOUT1(J) = ZH(J) * XtoY(T(J)/TW1(J), .55) *
            dwtemp * (TW1(J)-T(J))
Q1=(QOUT1(J)+QFLUX(TW1(J),T(J),P(J),H(J)))*AHT1(J)
TW1(J) = pruint(
            ( QIN1(J) - Q1 ) / ( fgen( 22, 1+J, TW1(J) ) * WW1(J) ),
            0, J - 1 )
QOUT2(J) = ZH(J) * XtoY(T(J)/TW2(J), .55) *
            dwtemp * (TW2(J)-T(J))
END IF
QBM = DWA(J)* ( H2SATH(P(J) ) - H(J) )
QB(J) = rlimit( 0., QBM, QFLUX(TW2(J), T(J), P(J), H(J) ) )
Q2 = ( QOUT2(J) + QB(J) )*AHT2(J)
TW2(J) = print( TW2(J),
            ( QIN2(J) - Q2 ) / ( fgen( 22, 11+J, TW2(J) ) * WW2(J) ),
            0, J + 9 )
QOUT(J) = Q1 + Q2

2060 CONTINUE

C FUEL TANK CHARACTERISTIC AS A FUNCTION OF TIME
C
PT = fgen(9, 1, STIME)
HT = fgen(7, 7, STIME)
H(1) = HT
PIFP(1) = PT
SUT= HT - PT / (RHOST * 9336.0)
CALL hyrt( SUT, RHOST, i, PT, X )

RHOFS = RHOST

LOW PRES FUEL TURBINE

THIS IS TO CALCULATE THE PERFORMANCE OF LPFT (FT1). HOWEVER, THE
EQUATION USED HERE TO CALCULATE THE TURBINE PARAMETER (ETAFT1) AND
THE SPECIFIC HEAT CONSTANT (CPH2) ARE NOT DESCRIBED IN THE DOCUMENT.

TFT1=T(6) -
ETAFT1 = DMFT1 * SF1 * 33.0965 /
            ( MAX1(0.0001, 9270. * TFT1 * (1.0/PRFTI- 1.0) ), 5 )

RITNV = RITN / fgen(30, 25, ETAFT1)**2
R6 = RITNV + RFTIV + RMCI

CPH2 = fgen(15, 26, TFT1) - 0.0887 +
            (0.1241 * PFT1 - 3.732E-5 * PFT1**2) /
            ( AMAX1(51.,TFT1) - 50. )

TRQFT1 = TRBTRQ( SF1, UCFT1, TFT1, PFT1, PRFT1, CPH2, DWFT1,
            H2GAMA(PFT1,TFT1,7)) * CTQFT1

PFT1 = P(6) - RFT1V / RHO(6) * DW(6) * ABS( DW(6) )
\[ PRFT1 = \left( \frac{PFT1 - RITNV/RHO(6) \cdot DWFT1 \cdot ABS(DWFT1)}{FGEN21 \cdot DWFT1 + 1.0E-06} \right) / PFT1 \]

\[ PFT1D = PFT1 \cdot PRFT1 \]

\[ TFT1D = TFT1 - \left( \frac{TRQFT1 \cdot SF1}{fgen21 \cdot DWFT1 + 1.0E-06} \right) \]

TURBINE COOLANT FLOW STARTS AT DP=185

THE EXTRA COOLANT FLOW TO COOL THE HIGH PRESSURE FUEL TURBINE:
THE VALVE START TO OPEN AT DP=185 AND BECOME FULLY OPEN AT DP=195.

\[ DWFT2C = \text{FLOW}(\text{DWFT2C}, 0.1, RFT2C/RHO(3), P(3)-PFI, 23) \]

\[ DWFT2C = DWT2C \cdot \text{rlimit}(0.0, 1.0, (P(3) - PFI - 185.) \cdot 0.1) \]

If the rlimit < 1, the effect is to drive DWFT2C down with a time constant dependent on the integration step size, which surely isn't intended.

The model is replaced by a variable limit imposed on an unlimited integrator.

\[ \text{undw2c} = \text{prflow}(\text{undw2c}, 0.1, RFT2C/RHO(3), P(3)-PFI, 23) \]

\[ \text{DWFT2C} = \text{undw2c} \cdot \text{rlimit}(0.0, 1.0, (P(3) - PFI - 185.) \cdot 0.1) \]

BEGIN PRESSURE FLOWRATE ITERATION


Initialize change monitor iteration counts

\[ \text{CALL its0} \]

\[ \text{DO 4000 LOOPS = 1, MAXLOOPS} \]

Reset change monitor for balance iteration test

\[ \text{fuelOK} = \text{.TRUE.} \]

THIS SECTION IS TO CALCULATE THE CAVITATION FOR FP1 AND FP2.

IN THE FOLLOWING CALCULATIONS, THE FUNCTION PROP( ) IS USED TO FIND OUT THE STATUS OF THE CURRENT HYDROGEN GIVEN KNOWN PARAMETERS.

PROP( ) IS A CHARACTERISTIC DATA MAP FOR HYDROGEN - RELATIONS AMONG INTERNAL ENERGY, DENSITY, PRESSURE, AND TEMPERATURE.

\[ PVFP1 = H2VP(T(2)) \]

\[ PVFP2 = H2VP(T(3)) \]

\[ PFPP1R = PVFP1 + PCFPP1\cdot SF1**2 \]

\[ PFPP2R = PVFP2 + PCFPP2\cdot SF2**2 \]

\[ RHOP1 = 0.5 \cdot (RHO(1) + RHO(2)) \]

\[ RHOP2 = RHO(3) \]
IF (PFS .GT. PFPIR) THEN
   RHOP1C = RHOP1
ELSE

   CAVITATION FOR FP1
   RHOP1C = RHOP1 * rlimit( 0.25, 1.0,
   + 0.25 + (PFS-PVFPI) *.75/(PFPIR - PVFPI + 1.0E-10) )
   END IF
   TRQFP1 = fgen(52, 27, DW2P/(RHOP1C * SF1) ) *
   + RHOP1C * SF1**2 * CTQFP1
   TRQFP1 = ABS(TRQFP1)
   IF( PFS2.GT.PFP2R) THEN
      RHOP2C = RHOP2
   ELSE

   CAVITATION FOR FP2
   RHOP2C = RHOP2 * rlimit(0.05, 1.0,
   + 0.05 + (PFS2-PVFPP) * 0.95 / (PFP2R - PVFPP + 1.0E-10) )
   END IF
   TRQFP2 = fgen(54, 28, DW2P/(RHOP2C * SF2) ) *
   + RHOP2C * SF2**2 * CTQFP2
   TRQFP2 = ABS(TRQFP2)

   FEEDLINE
   THIS IS THE FEEDLINE BETWEEN FUEL TANK AND LPFP
   DO 1060 J = 1, 5
   DWIFP(J) = trflow( DWIF(J), ZFL(J), -RIF(J),
   + PIFP(J) - PIFP(J+1) + ELENF(J) * RHOFS * DDX * v386p4, J+23 )
1060 CONTINUE
   DO 1070 J = 2, 5
   PIFP(J) = truint( ( DWIFP(J-1) - DWIFP(J) ) / ZFC(J),
   + Tstep, J + 27 )
1070 CONTINUE
   PNEW = truint( ( DWIFP(5) - DW2P ) / ZFC(6), Tstep, 33 )
   CHANGE=CHGX(CHANGE,PNEW,PFSP) was replaced by
   PFSP = relax( fuelOK, PNEW, PFSP, 1 )
   part of a convergence
   management system recommended to give more maintenance control
   over iterative energy balancing.
   PIFP(6) = PFSP

   PUMPS
   LPFP AND HPFP AND FLOW BETWEEN FEEDLINE AND MFV
IF( RMFV .GT. 1.0E10 ) THEN
   DW2P = 0.
ELSE
   RP1 = CP(2) * CDPFP1 / RHOP1C
   RP2 = CP(3) * CDPFP2 / RHOP2C
   RFS = RFCOD/RHO(2) + RP1 + RP2 + ( RR(3) + RMFV ) / RHO(3)
   DW2P = trflow( DW(2), ZFS, -RFS,
                  + (PFSP - P10P + DP1P + DP2P) + (RP1 + RP2) * DW2P * ABS(DW2P),
                  + 34 )
END IF
DDW2 = ( DW2P-DW(2) ) / DT
DW(1) = DW(2)
IF(DW2P.EQ.0.) THEN
   H(2)=H(1)
   H(3)=H(2)
ELSE
   H(2) = H(1) + TRQFPI * SF1 / (DW2P * 9336.)
   H(3) = H(2) + TRQFP2 * SF2 / (DW2P * 9336.)
ENDIF
DW3P = DW2P - DWFT2C
pDW3P = recpos(DW3P)

PHIP1 = DW2P / ( RHOP1C * SF1 )
DW2A = ( DW2P + DW(2) ) * 0.5
DP1P = fgen(51, 3, PHIP1) * RHOP1C * SF1**2 * CDPFP1
P(2) = PFS + DP1 - DDW2 * ZZ(2)

PHIP2=DW2P / (RHOP2C * SF2)
DP2P = fgen(53, 4, PHIP2) * RHOP2C * SF2**2 * CDPFP2
P(3) = PFS2 + DP2 - DDW2 * ZZ(3)

SU1 = HT - PFS / ( RHO(1) * 9336. )
SU2 = H(2) - P(2) / ( RHO(2) * 9336. )
SU3 = H(3) - P(3) / ( RHO(3) * 9336. )
CALL hyrt( SU1, RHO(1), 1, PFS, TTI )
CALL hyrt( SU2, RHO(2), 3, P(2), T(2) )
CALL hyrt( SU3, RHO(3), 5, P(3), T(3) )
T(2) = T(1) + T(2) - TTI
T(3) = T(1) + T(3) - TTI

MFV DIFFUSER

HI=H(3).LT.0.0) HI=H(10)

DW10P = trflow( DW(10), ZZ(10), -RR(10)/RHO(10), P10P-P11P, 35 )
DWMC = trflow( DMC, ZZ(13), -RR(13)/RHO(10), P10P-P13P, 36 )
DWFNP = trflow( DWFNP, ZZ(7), -RR(7)/RHO(10), P10P-P7P, 37 )
* Doing rectifications once instead of three times each.

pDW10P = recpos(DW10P)
DW10Pn = recneg(DW10P)
pDWMCP = recpos(DWMCP)
DWMCPn = recneg(DWMCP)
pDWFNP = recpos(DWFNP)
DWFNPn = recneg(DWFNP)
DW100P = pDW10P + pDWMCP + pDWFNP + DWFASI - DW3Pn
DW10IP = pDW3P - DW10Pn - DWMCPn - DWFNPn
RH010P = truint( vVOL(10) * (DW10IP - DW100P), Tstep, 38 )
H10IN = pDW3P * HI - DW10Pn * H1IP - DWMCPn * H13P - DWFNPn * H7P
SU10P = UNEWF( 10, DW10IP, H10IN, DW100P, P10P, RH010P )
H10P = SU10P + P10P / ( RH010P * 9336. )
CALL hypt(SU10P, RH010P, 10, PNEW, T(10) )

P10P = relax( fuelOK, PNEW, P10P, 2 )

DOWNCOMERS

DW11P = trflow( DW(11), ZZ(11), -RR(11)/RHO(11), P11P-P12P, 39 )
DW11Pp = recpos(DW11P)
DW11Pn = recneg(DW11P)
RH011P = truint( vVOL(11)*(DW11P - DW11P), 40 )
DW11I = pDW11P - DW11Pn
HI = pDW11P * H10P - DW11Pn * H12P
DW11O = DW11Pp - DW11Pn
SU11P = UNEWF( 11, DW11I, HI, DW11O, P11P, RH011P )
H11P = SU11P + P11P/(RH011P * 9336.)
CALL hypt( SU11P, RH011P, 11, PNEW, T(11) )

P11P = relax( fuelOK, PNEW, P11P, 3 )

LOWER 15% OF NOZZLE

DW12P = trflow( DW(12), ZZ(12), -RR(12)/RHO(12), P12P-P4P, 41 )
DW12Pp = recpos(DW12P)
DW12Pn = recneg(DW12P)
RH012P = truint( vVOL(12)*(DW12P - DW12P), 42 )
DW12I = DW12Pp - DW12Pn
HI = DW12Pp * H11P - DW12Pn * H4P
DW12O = DW12Pp - DW12Pn
SU12P = UNEWF( 12, DW12I, HI, DW12O, P12P, RH012P )
H12P = SU12P + P12P/(RH012P * 9336.)
CALL hypt( SU12P, RH012P, 12, PNEW, T(12) )

P12P = relax( fuelOK, PNEW, P12P, 4 )

NOZZLE REGEN COOLING FLOW
C

DW4P = trflow( DW(4), ZZ(4), -RR(4)/RHO(4), P4P-P8P, 43 )
RHO4P = truint( vVOL(4)* (DW12P - DW4P), 44 )
DW4Pp = recpos(DW4P)
DW4Pn = recneg(DW4P)
DW4I = DW12Pp - DW4Pn
HI = DW12Pp * H12P - DW4Pn * H8P
DW4O = DW4Pp - DW12Pn
SU4P = UNEWF( 4, DW4I, HI, DW4O, P4P, RHO4P )
H4P = SU4P + P4P/(RHO4P * 9336.)
CALL hypt( SU4P, RHO4P, 4, PNEW, T(4) )  SSM2190C

P4P = relax( fuelOK, PNEW, P4P, 5 )

MCC SUPPLY DUCT

DW13P = trflow( DW(13), ZZ(13), -RR(5)/RHO(13), P13P-P5P, 45 )
RHO13P = truint( vVOL(13)* (DWMCP - DW13P), 46 )
DW13Pp = recpos(DW13P)
DW13Pn = recneg(DW13P)
DW13I = DWMCPp - DW13Pn
HI = DWMCPp * H13P - DW13Pn * H5P
DW13O = DW13Pp - DWMCPn
SU13P = UNEWF( 13, DW13I, HI, DW13O, P13P, RHO13P )
H13P = SU13P + P13P/(RHO13P * 9336.)
CALL hypt( SU13P, RHO13P, 13, PNEW, T(13) )  SSM22000

P13P = relax( fuelOK, PNEW, P13P, 6 )

MAIN COMBUSTOR REGEN COOLING FLOW

NODE 5 BELOW THROAT

DW5P = trflow( DW(5), ZZ(5), -RR(6)/RHO(5), P5P-P6P, 47 )
RHO5P = truint( vVOL(5)* (DW13P - DW5P), 48 )
DW5Pp = recpos(QW5P)
DW5Pn = recneg(DW5P)
DW5I = DW13Pp - DW5Pn
HI = DW13Pp * H13P - DW5Pn * H6P
DW5O = DW5Pp - DW13Pn
SU5P = UNEWF( 5, DW5I, HI, DW5O, P5P, RHO5P )
H5P = SU5P + P5P/(RHO5P * 9336.)
CALL hypt( SU5P, RHO5P, 5, PNEW, T(5) )  SSM22200

P5P = relax( fuelOK, PNEW, P5P, 7 )

NODE 6 ABOVE THROAT

DW6P = trflow( DW(6), ZZ(6), -R6/RHO(6), P6P - PINMC, 49 )
RHO6P = truint( vVOL(6)* (DW5P - DW6P), 50 )

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DW6Pp = recpos(DW6P)  
DW6Pn = recneg(DW6P)  
DW6I = DW5Pp - DW6Pn  
HI = DW5Pp*H5P - DW6Pn*H6P  
DW6O = DW6Pp - DW5Pn

SU6P = UNEWF(6, DW6I, HI, DW6O, P6P, RHO6P)  
H6P = SU6P + P6P/(RHO6P * 9336.)  
CALL hypt(SU6P, RHO6P, 6, PNEW, T(6))

P6P = relax(fuelOK, PNEW, P6P, 6)

CCV INLET DUCT

DW7P = trflow(DW(7), .04, -(RCCV + RR(9))/RHO(7), P7P - P8P, 51)  
RHO7P = truint(RHO(7), vVOL(7)*(DWFNP - DW7P), 52)

DW7Pp = recpos(DW7P)  
DW7Pn = recneg(DW7P)  
DW7I = pDWFNP- DW7Pn  
HI = pDWFNP*H10P - DW7Pn*H8P  
DW7O = DW7Pp - DWFNPn

SU7P = UNEWF(7, DW7I, HI, DW7O, P7P, RHO7P)  
H7P = SU7P + P7P/(RHO7P*9336.)  
CALL hypt(SU7P, RHO7P, 7, PNEW, T(7))

P7P = relax(fuelOK, PNEW, P7P, 7)

MIXER

DW8P = trflow(DW(8), ZZ(8), -RR(8)/RHO(8), P8P-P9P, 53)  
RHO8P = truint(vVOL(8)*(DW7P + DW4P - DW8P), 54)

DW8Pp = recpos(DW8P)  
DW8Pn = recneg(DW8P)  
DW8I = DW4Pp + DW7Pp - DW8Pn

HI = DW4Pp*H4P + DW7Pp*H7P - DW8Pn*H9P  
DW8O = DW8Pp - DW7Pn - DW4Pn

SU8P = UNEWF(8, DW8I, HI, DW8O, P8P, RHO8P)  
H8P = SU8P + P8P/(RHO8P*9336.)  
CALL hypt(SU8P, RHO8P, 8, PNEW, T(8))

P8P = relax(fuelOK, PNEW, P8P, 8)

PREBURNER SUPPLY DUCT

DWFPFP = trflow(DWFPF, ZFPF, -RFPFI/RHO(9), P9P-PFP, 55)  
DWOPFP = trflow(DWOPF, ZOPF, -ROPFI/RHO(9), P9P-POP, 56)

DW9P = DWFPFP + DWOPFP  
RHO9P = truint(vVOL(9)*(DW8P - DW9P), 57)

DW9Pn = recneg(DW9P)
DW9I = DW8Pp - DW9Pn
HI = DW8Pp*H8P - DW9Pn*H9P
DW9O = recippos(DW9P) - DW8Pn
SU9P = UNEWF( 9, DW9I, HI, DW9O, P9P, RHO9P )
H9P = SU9P + P9P/(RHO9P * 9336.)
CALL hypt( SU9P, RHO9P, 9, PNEW, T(9) )

* P9P = relax( fuelOK, PNEW, P9P, 11 )

* IF( fuelOK.AND.LOOPS.GT.2) GO TO 3500 was replaced by
*       IF( fuelOK ) GO TO 3500
* balancing keeps up with changing conditions. Output of variable
* names was eliminated as unnecessary for a simulation monitoring
* function.
4000 CONTINUE

3500 DO 4100 J = 2, 6
       PIF(J) = step( J + 27 )
4100 CONTINUE

3500 DO 4100 J = 1, 5
       DWIF(J) = step( J + 23 )
4110 CONTINUE

PFS=PFSP
DP1=DP1P
DP2=DP2P
DW(2) = step( 34 )
DW(3)=DW3P
DWFNBP = step( 37 )
DWFN=DW10P
DWMC = step( 36 )
DW100=DW10OP
DW10I=DW10IP

P(4)=P4P
RHO(4) = step( 44 )
SU(4)=SU4P
H(4)=H4P
DW(4) = step( 43 )

P(5)=P5P
RHO(5) = step( 48 )
SU(5) = SU5P
H(5) = H5P
DW(5) = step(47)

C
P(6) = P6P
RHO(6) = step(50)
SU(6) = SU6P
H(6) = H6P
DW(6) = step(49)
DWFT1 = DW6P

C
P(7) = P7P
RHO(7) = step(52)
SU(7) = SU7P
H(7) = H7P
DW(7) = step(51)

C
P(8) = P8P
RHO(8) = step(52)
SU(8) = SU8P
H(8) = H8P
DW(8) = step(53)

C
P(9) = P9P
RHO(9) = step(57)
SU(9) = SU9P
H(9) = H9P
DW(9) = DW9P
DWFPP = step(55)
DWOFP = step(56)

C
P(10) = P10P
RHO(10) = step(38)
SU(10) = SU10P
H(10) = H10P
DW(10) = step(-35)

C
P(11) = P11P
RHO(11) = step(40)
SU(11) = SU11P
H(11) = H11P
DW(11) = step(39)

C
P(12) = P12P
RHO(12) = RHO12P
SU(12) = SU12P
H(12) = H12P
DW(12) = step(41)

C
P(13) = P13P

121
RHO(13) = step( 46 )
SU(13) = SU13P
H(13) = H13P
DW(13) = step( 45 )

C QF IS FUEL FLOW IN GALLON/MIN
C
QF = 0.25974 * DW2P / RHO(2)
TFP1 = T(2)
PPF1 = P(2)
PPFD1 = P(2)
PPFD = P(3)

RETURN
END

C HTF FUNCTION IS TO CALCULATE THE HEAT TRANSFER COEFFICIENT
C SUCH AS THE ONES IN PAGE 31 OF THE DOCUMENT.
C I BELIEVE THIS IS THE SIMPLIFIED VERSION OF CALCULATION.
C
FUNCTION HTF(T, P)
HTF = 0.1425 + (2.85E-4 + 1.8E-8 * P) * T
RETURN
END

HTF FUNCTION IS TO CALCULATE THE HEAT TRANSFER COEFFICIENT
SUCH AS THE ONES IN PAGE 31 OF THE DOCUMENT.
I BELIEVE THIS IS THE SIMPLIFIED VERSION OF CALCULATION.

FUNCTION HTF(T, P)
HTF = 0.1425 + (2.85E-4 + 1.8E-8 * P) * T
RETURN
END
'hyprop.for':

```fortran
subroutine prop0

***********************************************************************

C
C SUBROUTINE PROP(SU,SRHO,N,P,T,NN)
C PURPOSE: HYDROGEN PROPERTY DATA
C
C THIS TABLE IS THE ENERGY MAP OF HYDROGEN PROPERTY. IT IS ABOUT THE
C RELATIONSHIP AMONG SPECIFIC ENERGY (SU), DENSITY (SRHO), PRESSURE (P)
C AND TEMPERATURE. PRESUMEDLY, FOR ANY GIVEN TWO PARAMETERS, THE OTHER
C PARAMETERS CAN BE FOUND.
C
C******ARGUMENTS******
C
C SU = SPECIFIC INTERNAL ENERGY, BTU/LB
C SRHO = DENSITY, LB/IN3
C P = PRESSURE, PSI
C T = TEMPERATURE, DEG R
C N = CALLER NODE INDEX
C
* PROP was divided into four separate entries:
* prop0 - precomputes slopes for all interpolations
* hypt - interpolates P and T, given SU and SRHO
* hyrt - interpolates SRHO and T, given SU and P
* hyut - interpolates SU and T, given SRHO and P
*
***********************************************************************

C PARAMETER (NCALL=50, NU=14, NRHO=18, NSAT = 7 )
PARAMETER ( v1728 = 1728. )

* Hydrogen data, saturation curves:
* DIMENSION U(NU), RHO(NRHO), PRES(NU,NRHO), TEMP(NU,NRHO),
+ RSAT(NSAT), PSAT(NSAT)
*
* Precomputed slopes: ( DRHO was inverted )
* DIMENSION XP(NU,NRHO), TXP(NU,NRHO), vDRHO(NRHO),
+ UvsP(NU, NRHO), RHOvsP(NU, NRHO),
+ RSvsU(NSAT), PSvsU(NSAT), vPS(NSAT), DRSAT(NSAT)
*
* Call point identifiers, initially at lowest interval
* DIMENSION ICALL(NCALL), JCALL(NCALL), R(2)
DATA ICALL / NCALL*2 /, JCALL / NCALL*2 /
*
DATA RSAT / 4.6, 4.44, 4., 3.33, 2.5, 1.9, 1.25 /

123
```
DATA PSAT / 5.4, 12.5, 49.9, 121.9, 181., 188., 200. /  
*  
DATA U /  
* 79., 88., 113., 147., 181., 200., 225., 250.,  
* 275., 300., 350., 400., 600., 2600./  
*  
DATA RHO /  
* .0050, .0125, .0250, .0500, .1000, .1250, .2500, .5000,  
* 1.0000, 1.2500, 1.9000, 2.5000, 3.3300, 4.0000, 4.4000, 4.6000,  
* 4.9000, 5.5000/  
*  
Pressure( su, rho )  
*  
DATA (PRES(I,01), I=1,14) /  
* .000, .000, .000, .000, .000, .000, .000, .000,  
* .000, .103, .1303, 1.575, 2.229,  
* 3.358, 4.486, 6.733, 8.808, 14.890, 64.580/  
*  
part of table omitted  
*  
DATA (PRES(I,02), I=1,14) /  
* 4014.0, 4715.0, 6267.0, 8170.0, 9887.0,10808.0,11949.0,13029.0,  
* 14030.0,14979.0,16704.0,18270.0,20000.0,20000.0/  
C  
TEMPERATURE AS A FUNCTION OF SU AND RHO  
C  
DATA (TEMP(I,01), I=1,14) /  
* .00, .00, .00, .00, .00, .00, .00, .00,  
* .00, .00, .00, .00, 223.60, 968.20/  
*  
part of table omitted  
*  
DATA (TEMP(I,18), I=1,14) /  
* 37.26, 44.66, 60.93, 81.27, 100.50, 110.76, 123.77, 136.08,  
* 147.70, 158.93, 179.14, 197.82, 264.75, 987.65/  
*  
subroutine prop0  
* :::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::  
C  
INITIALIZE SLOPES  
C  
DO 26 J = 1,NRHO  
RHO(J)=RHO(J) * v1728  
26 CONTINUE  
CALL XYset( NU, U, NRHO, RHO, PRES, XP, VDRHO )  
CALL XYset( NU, U, NRHO, RHO, TEMP, TXP, VDRHO )
DO 30 J = 2, NRHO
   drho = RHO(J) - RHO(J-1)
DO 25 I = 2, NU
   UvsP(I,J) = 1.0 / XP(I,J)
   RHOvsP(I,J) = drho / ( PRES(I,J) - PRES(K,J-1) )
25 CONTINUE
30 CONTINUE
DO 40 I = 2, NU
   du = U(I) - U(I-1)
   RSvsU(I) = ( RSAT(I) - RSAT(I-1) ) / ( du * 1728.0 )
   PSvsU(I) = ( PSAT(I) - PSAT(I-1) ) / du
   vPS(I) = 1.0 / ( PSAT(I) - PSAT(I-1) )
   DRSAT(I) = RSAT(I) - RSAT(I-1)
40 CONTINUE
RETURN

* ENTRY hypt( SU, SRHO, N, P, T )

PRESSURE COMPUTATIONS

200 UP1 = SU - U(I-1)
   RHOP1 = ( SRHO - RHO(J) ) * vdrho(J)
   P1 = PRES(I-1,J) + XP(I,J) * UP1
   P2 = PRES(I-1,J+1) + XP(I,J+1) * UP1

IF(SU.LT.225.) THEN
   RHOSAT = RSAT(I-1) + RSvsU(I) * UP1
   R1=RHO(J)
   R2=RHO(J+1)
   IF((SRHO.GT.RHOSAT).AND.(RHOSAT.GT.R1)) THEN
      R1=RHOSAT
      P1 = PSAT(I-1) + PSvsU(I) * UP1
   ELSE IF( (SRHO.LT.RHOSAT) .AND. (RHOSAT.LT.R2) )THEN
      R2=RHOSAT
      P2 = PSAT(I-1) + PSvsU(I) * UP1
   ELSE IF( (SRHO.GT.R1) .AND. (R1.GT.RHOSAT) ) THEN
      R1=RHOSAT
      P1 = PSAT(I-1) + PSvsU(I) * UP1
   ELSE IF( (SRHO.LT.R2) .AND. (R2.LT.RHOSAT) ) THEN
      R2=RHOSAT
      P2 = PSAT(I-1) + PSvsU(I) * UP1
   ELSE IF( SRHO.GT.R1 .AND. R1.LT.R2 ) THEN
      P = P1 + (P2-P1)*((SRHO-R1)/(R2-R1))
   ELSE
      P = P1
   END IF

125
\[ P = P_1 + (P_2 - P_1) \times RHOP_1 \]

END IF

\[ T = xylint( \text{SU, SRHO, NU, U, NRHO, RHO, TXP, VDRHO, TEMP,} + \text{icall(N), icall(N)}) \]

RETURN

ENTRY hyrt( \text{SU, SRHO, N, P, T} )

*******************************************************************************

CALL intval( icall(N), SU, NU, U,
+ 'The hydrogen energy is below the table.',
+ 'The hydrogen energy exceeds the table.', 0 )

intval could not be used below, because consecutive row elements
of PRES are not consecutive in memory. The table escape error stop
was added, however.

\[ K = \text{icall(N)} \]
\[ K=I-1 \]
\[ J=J\text{CALL(N)} \]

310 IF(PRES(K,J,J).LT.P) GO TO 330
320 IF(PRES(K,J-1,LE.P) GO TO 340
\[ J=J-1 \]
GO TO 320
330 J=J+1
GO TO 310

* Replaced 340 J=\text{MAXO}(2,\text{MINO}(J,\text{NRHO})) by

340 IF ( J .LT. 2 ) THEN
PRINT *, 'The hydrogen pressure is below the table.'
STOP
ELSE IF ( J .GT. NRHO ) THEN
PRINT *, 'The hydrogen pressure exceeds the table.'
STOP
END IF

IF(K.EQ.I-1) jcall(N) = J
R(K-I+2) = RHO(J-1) + ( P-PRES(K,J-1) ) \times RHOVsP(K,J-1)
IF(K.EQ.I) GO TO 350
K=I
GO TO 310

ASSUME RHO LINIER WITH U

PROVIDE FOR LIQUID SIDE OF SATURATION LINE ONLY

350 U1=U(I-1)
U2=U(I)
IF(I.LT.8 .AND. J.LE.17-I) THEN
X = ( P - PSAT(I-I) ) * vPS(I)
U2 = U1 + X * ( U2 - U1 )
R(2) = ( RSAT(I-I) + X * DRSAT(I) ) * v1728
END IF
SRHO = R(1) + ( R(2)-R(1) ) / (U2-U1) * (SU-U1)

* Now T is found from input SU and interpolated RHO. We use the next call
* number to remember the previous interval of the above interpolated RHO.

CALL intval( icall(N+1), SRHO, NRHO, RHO,
+ 'The interpolated density is below the table.',
+ 'The interpolated density exceeds the table.', 0 )

T = xylint( SU, SRHO, NU, U, NRHO, RHO, TXP, VDRHO, TEMP,
+ icall(N), icall(N+1) )
RETURN

ENTRY hyut( SU, SRHO, N, P, T )

*****
GET U AND T FROM RHO AND P ( Uses call number N + 1 )
*****

* Was optimized by using precomputing slopes and replacing search from
* table edge with search from point at last call. An error stop is now
* in effect when density or pressure leaves the tabulated range.
* The segment was recoded so that K does not change.

CALL intval( icall(N), SRHO, NRHO, RHO,
+ 'The hydrogen density rho is below the table.',
+ 'The hydrogen density rho exceeds the table.', 0 )

K = icall(N)
CALL intval( jcall(N), P, NU, PRES(1,K-1),
+ 'The hydrogen pressure is below the table.',
+ 'The hydrogen pressure exceeds the table.', 0 )

U1 = U(M-1) + ( P - PRES(M-1,K-1) ) * UvsP(M,K-1)

CALL intval( jcall(N), P, NU, PRES(1,K),
+ 'The hydrogen pressure is below the table.',
+ 'The hydrogen pressure exceeds the table.', 0 )
M = jcall(N)

U2 = U(M-1) + ( P - PRES(M-1,K) ) * UvsP(M,K)
SU = U1 + ( SRHO-RHO(K-1) )* vdrho(K-1) * (U2 - U1)

* Now T is found from interpolated SU and input RHO. We use the next call
* number to remember the previous interval of the above interpolated SU.
CALL intval( icall(N+1), SU, NU, U,
+     'The interpolated energy is below the table.',
+     'The interpolated energy exceeds the table.', 0 )
*
T = xylint( SU, SRHO, NU, U, NRHO, RHO, TXP, VDRHO, TEMP,
+     icall(N+1), icall(N) ) END

'h2gama.for':

FUNCTION H2GAM0( XPRES, XTEMP, N)
***********************************************************************
* Initializes temp, pressure points, returns value at XPRES, XTEMP
* C
C PURPOSE:  COMPUTATION OF HYDROGEN SPECIFIC HEAT RATIO
C AS A FUNCTION OF PRESSURE AND TEMPERATURE
C CALCULATES GAMMA FOR PARA HYDROGEN
C
C*****ARGUMENTS*****
C INPUT:
C XPRES = PRESSURE, PSI
C XTEMP = TEMPERATURE, DEG R
C N = CALLER NODE INDEX
C
C OUTPUT:
C H2GAMA = GAMMA
C
* H2GAMA0 does initialization and lookup ( NN .LE. 0 )
* The main entry H2GAMA does lookup alone.
***********************************************************************
*
DIMENSION TEMP(20),PRES(25),GAMA(20,25),II(10),JI(10),XP(20,25), 9700
IDPRES(25)
INCLUDE 'units.com'

* Reads temperature and pressure points, tabulated values.
* READ(dat,11)NTEMP,NPRES,(TEMP(I),I=1,NTEMP),(PRES(I),I=1,NPRES)
11 FORMAT( //2X, 2(2X,I10)//2X,6(2X, G10.0) ) SSM79750
READ(dat,12)((GAMA(I,J),I=1,NTEMP),J=1,NPRES)
12 FORMAT(/(//3X,12(IX,F6.0) ) ) SSM79770
*
* Precomputation of slopes for two-way interpolation was moved to the
* interpolation module.
CALL XYset(n, ntemp, temp, npres, pres, gama, xp, dpres)
DO 23 I = 1, 10
   Ii(I) = 2
   Jl(I) = 2
23 CONTINUE
*
ENTRY H2GAMA(XPRES, XTEMP, N)
***********************************************************************
* This is the simulation loop entry, with no initialization.
* Keeps track of last entry location for each caller, identified by N.
* If it is really desired to return H2GAMA = 1.4 temperature is off the
* table, then intval can be used instead of the special code below, by
* adding one point to TEMP, and a column to GAMA defining the range where
* this return is OK.
***********************************************************************
*I = I1(N)
IF( xtemp .GT. temp(i) ) THEN
   Search from there up
   DO 10 k = i + 1, ntemp
      IF( xtemp .LE. temp(k) ) THEN
         i = k
         GO TO 30
      ENDIF
10 CONTINUE
ELSEIF ( xtemp .LT. temp(i - 1) ) THEN
   Search down from there
   DO 20 k = i, -2, 1, -1
      IF( xtemp .GE. temp(k) ) THEN
         i = k + 1
         GO TO 30
   ENDIF
20 CONTINUE
PRINT *, 'Temperature is below H2GAMA table.'
STOP
ELSE
   Error traps were added in case input variables escape the table.
   The table can be readily extended, after all.
30 CALL intval(j1(N), xpres, npres, pres,
   'Pressure is below H2GAMA table.',

129
'Pressure is above H2GAMA table.', 0 )

H2GAMA = xylint( xtemp, xpres, ntemp, temp, npres, pres,
    + xp, dpres, gama, i, j1(n) )

And to support H2GAM0 as a function:

H2GAM0 = H2GAMA

END
SUBROUTINE OXIDF0

C *********************************************************************
C THIS IS ANOTHER MAJOR PART OF THE SIMULATION PROGRAM. THIS SIMULATES
C THE OXIDIZER FLOW AND ENERGY BALANCE OF THE SYSTEM.
C THE SUBROUTINE FLOW IS:
C 1) INITIALIZATION ( OXIDF0 )
C 2) READ DATA ( OXIDF0 )
C 3) CALCULATE THE PUMP INLET AND OUTLET DUCTS CONDITIONS ( OXIDF0 )
C 4) CALCULATE THE FLOW RATE OF EACH NODE
C 5) CALCULATE THE PUMP/TURBINE PERFORMANCE
C 6) CALCULATE THE PUMP CAVITATION EFFECT
C 7) CALCULATE THE CHANGES OF THE OXID LINE FROM TANK TO LPOP
C 8) PRIMING FUNCTION OF MOV AND INJECTOR
C 9) CALCULATE THE PUMP SPEEDS
C 10) RETURN

DIMENSION RIL(12),ELENO(12),ZIL(12),ZIC(12), TPR(6)
DIMENSION N1(3), N4(3), N5(3), N6(3)
LOGICAL adjOK, XMOVPF, PRIMIF

COMMON/PVCHEK/ POTVP, DWOPIL, DUMME1, DUMME2, INONZ,
2 POSX,TAU,ABKFLO,FHECD1,FHECD2
3 ,FLI2,FL2,PCOD1L,PCOD2L,POD1L,POD2L,POI2L,VHECD1,VHECD2

INCLUDE 'blank.com'
INCLUDE 'out.com'
INCLUDE 'contrl.com'
INCLUDE 'igni.com'
INCLUDE 'oxid.com'
INCLUDE 'hgas.com'
INCLUDE 'balc.com'
INCLUDE 'pogo.com'

** COMMON/PURGE/DWGN2,TCUTPR,DWF2F,DWGN20 **

** Often used constant reciprocals:**

PARAMETER ( v386p4 = 1. / 386.4, v9336 = 1. / 9336., + v41p34 = 1. / 41.34, v8p866 = 1. / 8.866, + v77 = 1. / 77. )
PARAMETER ( TooBig = 1.E50 )

** Obsoleted printout control **
DATA TPR / 10*100.0 /, IPR / 2 /, FLAG / 0.0 /
DATA PRIMIF / .TRUE. /, QBKFL2 / 0.0 /, XMOVPF / .TRUE. /
DATA TL / 0.0 /, TH / 0.0 /
DATA ROP3IN /0.0/
DATA WTOP1 / 14.4 /

* recpos(x) = AMAX1( 0.0, x )
recneg(x) = AMIN1( 0.0, x )
rlimit(x, floor, ceiling) = AMAX1( floor, AMIN1( ceiling, x ) )

WTHE() IS THE FUNCTION TO CALCULATE THE HELIUM CONTENT OF A FLOW MIXER.

WTHE(DWHE1, FHE1, FHE2, DWHE2, FHE3, DWHE3, FHE4) =
+ FHE2* ( recneg( DWHE1 ) - recpos( DWHE2 ) + recneg( DWHE3 ) ) +
+ FHE1*recpos( DWHE1 ) - FHE3*recneg( DWHE2 ) + FHE4*recpos( DWHE3 )

ENINOX() IS THE FUNCTION TO CALCULATE THE ENTHALPY OF AN ACCUMULATOR.

ENINOX(WI, WO, H1, HO, HU) = H1 * recpos( WI ) +
+ HO * ( recneg( WI ) - recpos( WO ) ) - HU * recneg( WO )

* Name this function appropriately

* quadr( x ) = 620.15 + x * ( 19.1202 + .149371 * x )

******************************************************************************
******************************************************************************

READ (run, 30) POT, ZOS, DUM, RROOT, ZMOV, ZOPI, ZOP2, TQOT1B, TQOT2B, ZOI
1, TOS, WOV, TDRAGO
READ (run, 30) GO1, GO2
READ (run, 30) ELOT1, AAOAT1, RMOVU8, RMOVQ, VOLOP1, VOLOP2, VOLOP3, VOLOT1
*, WCOD, WOTD
READ (run, 30) PVOP1, PVOP2, PVOP3, PCOP1, PCOP2, PCOP3
READ (run, 30) (ELENO(J), J=1, 12), (ZIL(J), J=1, 12), (ZIC(J), J=1, 12),
1 (RIL(J), J=1, 12)
READ (run, 30) AOS, AHE, XLO, XL1, XL2, VTOT, PHES, GAMHE
30 FORMAT(/ '2X, 6G12.4)
READ (run, '(/ '2X, 3I12)' ) INONZ, IRHOP2, ICAVMD
READ (run, 30) TCU72, TCU73, BASEAR, BOS, TDCOM, RL1, RPV, ZJTPV, ROP3IN,
1 E1JPV, BQ1, BOPVDN, WOCOM, WOIN, DTPV, TCLPV, ABK2, THEADD, VOLOD1,
2 VOLOD2, VOLOD3, VOLCD1, VOLCD2, TCAV1, TCAV2, TIMCAV, GLOPC, TL1, TH1,
3 TL2, TH2
DUCTS=1.
ELENT=0.0
FAC = 8.0
THE = 180.
HOI2AD = -41.

DUMME1 = WOCOM
DUMME2 = WOIN

* STIME=TIME
CALL fgset( 5 )
HOS = FGEN(5, 8, STIME)
CALL fgset(37)
POT = FGEN(37, 9, STIME)
PIL(1) = POT
DO 90 J= 2, 8
   PIL(J) = PIL(J-1) + ELENO(J-1) * RHOOT
   DWIL(J) = 0.0
90 CONTINUE
DWIL(1) = 0.0
POS = PIL(8) + ELENO(8) * RHOOT
POSX = POS
POD1 = POS
POD2 = POS
POD3 = POS
POI2 = POS
POINJ = PA
SO1 = 1.0E-10
SO2 = 1.0E-10
SO1SQ = SO1 ** 2
SO2SQ = SO2 ** 2
WOI = 0.0
DWOI = 0.0
DWOP1 = 0.0
DWOP2 = 0.0
DWOP3 = 0.0
DWCOD = 0.0
DWMOV = 0.0
DWOT1 = 0.0
DWOP2C = 0.0
DWOP3C = 0.0
DDX = 386.4
DPOP1 = 0.0
DPOP2 = 0.0
DPOP3 = 0.0
TRQP1 = 0.0
TRQP2 = 1.0E-10
CALL fgset (44)
CALL fgset (45)
CALL fgset (46)
CALL fgset (47)
CALL fgset (48)
CALL fgset (49)
CALL fgset (50)
CALL fgset (51)
CALL fgset (52)
ELCOM = FGEN(58, 29, 0.)
CALL fgset (59)
RCOM = FGEN(59, 30, 0.)
CALL fgset (60)
ZCOM = FGEN(60, 31, 0.)
CALL fgset( 61 )
ELOIN = FGEN(61, 32, 0.)
CALL fgset( 62 )
ROIN = FGEN(62, 33, 0.)
CALL fgset( 63 )
ZOIN = FGEN(63, 34, 0.)
CALL fgset( 64 )
APV = FGEN(64, 35, 0.)
CALL fgset( 65 )
DWOE2 = FGEN(65, 36, 0.0)
CALL fgset( 66 )
CALL fgset( 67 )
CALL fgset( 68 )
CALL fgset( 69 )
CALL fgset( 70 )
CALL fgset( 71 )
CALL fgset( 72 )
CALL fgset( 73 )
CALL fgset( 74 )
CALL fgset( 75 )
CALL fgset( 76 )
CALL fgset( 77 )
CALL fgset( 78 )
CALL fgset( 79 )
CALL fgset( 81 )
CALL fgset( 82 )
CALL O2DFPE(HOS, POS, RHOOS, TOS, 4, -1, 1)
CALL O2PROP(HOS, RHOOS, 1, POS, TOS, -1)
CALL O2PROP(HOS, RHOOS, 1, POS, TOS, 3)
TOD2=180.
RHOP1=RHOOS
RHOOP1=RHOOS
RHOOP2=RHOOS
RHOP3=RHOOS
RHOOP3=RHOOS
RHOD1=RHOOS
RHOD2=RHOOS
RHOT1=RHOOS
RHOI2 = RHOOS
RHOC2 = RHOOS
fgset ( 3 )
PRIMOI = FGEN(3, 37, 0.0)
*
ZOT1 = EL0T1 / ( AAOT1 * 386.4)
hZOT1 = EL0T1 / ( AAOT1 * 772.8)
ROT1N=ANOT1
COV=1.0
HCAVP1=1.
HCAVP2=1.
HCAVP3=1.

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TCAVP1=1.
TCAVP2=1.
TCAVP3=1.
WHEOD1=0.0
FHEOD1=0.0
HOS1=HOS
WHECD1=0.0
FHECD1=0.0
WHECD2=0.0
FHECD2=0.0
WHEOI2=0.0
FHEOI2=0.0
WHEOD2=0.0
FHEOD2=0.0
WHEOT1=0.0
FHEOT1=0.0
DWOTJ=0.
DWOE3=0.
DWOEPV=0.
RJTPVD=3.05E-6
DWOIN=0.
POINVP=15.
VOLPV=0.
QBFKFO=0.
HLPT1=HOS
HIOP2=HOS
H3I=HOS
H3=HOS
HOD2=HOS
HOD1=HOS
HOD3=HOS
HOI2=HOS
HLPOTD=HOS
CALL POGO0
WRITE(init,100).(PIL(J),J=1,8)
100 FORMAT( ' PIL(1) PIL(2) PIL(3) PIL(4) PIL(5)
1 PIL(6) PIL(7) PIL(8)' /1PE11.3)
* 
* Initialization was extended to include the following:
C 
* IF (FLAG .GT. 0.0) GO TO 1160 
* FLAG = 100.0 
* obsoleted method of 
* triggering restart adjustment
* 
* IF (DWOPI .GE. 0. ) HOP = HOS 
VOLOI2 = VOLOI2 + VOLCD1 + VOLCD2
* 
* IF (TIME .GT. 0.001) GO TO 1160 
* Apparently an error. It calls for 
* adjustment to occur only if start time < .001 
*
IF ( STIME .LE. 0.001 ) RETURN

POT = FGEN (37, 9, STIME)
HOS = FGEN (5, 8, STIME)
ELCOM = FGEN (58, 29, WOCOM)
ELOIN = FGEN (61, 32, VOLPV)
IF (TCUT2 .LT. STIME) DWOE2 = 0.0
IF (TCUT3 .LT. STIME) DWOE3 = 0.0
RHOLO = -1.0
RHOHI = -1.0
ICOUNT = 0

THE FOLLOWING "ERROR CHECKING" (FROM HERE TO STATEMENT 1100)
IS TO FIND THE CONSISTANCY AMONG THE GIVEN INITIAL CONDITIONS
OF THE OXID LINE INPUTS, POS (OXID INPUT PRESSURE), SU (INTERNAL
SPECIFIC ENERGY), AND RHOOS (OXID LINE INPUT DENSITY). IF THE CALCULATE
VALUE OF PRESSURE FROM SU AND RHOOS IS NOT TOO FAR OFF FROM "POS" THEN
RHOOS IS ADJUSTED TO MATCH THE CONDITION.

The adjustment loop described above is executed when restarting
at nonzero time. Its omission from the restart procedure may account
for the restart transients mentioned elsewhere. Reporting on the
restart convergence is handled by the change monitor.

CALL chgo( .0001, 1 )
adjOK = .TRUE.
DO 10, I = 1, 30
   POS = POT + RHOOS * DDX * (ELCOM + ELOIN) *V386p4
   SUT = HOS - POS / (9336.0 * RHOOS)
   CALL OXPROP(PANS, HOX, RHOOS, RHOLI2, RHOGI2,
               HGI2, HLI2, FLI2, SUT, N4)
   CALL chgmnt( adjOK, PANS, POS, 1 )
    IF ( adjOK ) GO TO 1100
    IF (PANS .LE. POS) THEN
       RHOLO = RHOOS
       IF (RHOHI .LE. 0.0 ) THEN
          RHOOS = 1.002* RHOLO
       ELSE
          RHOOS = (RHOLO + RHOHI)* 0.5
       ENDIF
    ELSE
       RHOHI = RHOOS
       IF (RHOLO .LE. 0.0) THEN
          RHOOS = 0.998* RHOHI
       ELSE
          RHOOS = (RHOLO + RHOHI)* 0.5
       ENDIF
    ENDIF
10 CONTINUE
CALL wrchg ( init, 1, 'OXIDF initial adjustment error' )
The following re-initializations are necessary because of the restart adjustment.

1100 CONTINUE

POJ = POT + RHOOS * DDX * ELCOM * v386p4
POPVDN = POJ + RHOOS * DDX * ELJPV * v386p4
SUOIN = HOS - POS / (9336.0 * RHOOS)
UOIN = SUOIN * WOIN
HOD1 = HOS
SUOD1 = SUOIN
RHOD1 = RHOOS
WOD1 = VOLOD1 * RHOOS
UOD1 = SUOIN * WOD1
POD1 = POS
POD1L = POS
HOI2 = HOS
SUOI2 = SUOIN
RHOI2 = RHOOS
WOI2 = VOLOI2 * RHOOS
UOI2 = SUOIN * WOI2
POI2 = POS
POI2L = POS
HOD2 = HOS
SUOD2 = SUOIN
RHOD2 = RHOOS
WOD2 = VOLOD2 * RHOOS
UOD2 = SUOIN * WOD2
POD2 = POS
POD2L = POS
HOT1 = HOS
SUOT1 = SUOIN
RHOT1 = RHOOS
WOT1 = VOLOT1 * RHOOS
UOT1 = SUOIN * WOT1
POT1 = POS
POT1L = POS
HOD3 = HOS
POD3 = POS
RHODCD2 = RHOOS

CALL unint0( UOD1, 58 )
CALL unint0( WOD1, 59 )
CALL unint0( WHEOD1, 60 )
CALL unint0( UOI2, 61 )
CALL unint0( WOI2, 62 )
CALL unint0( WHEOI2, 63 )
CALL unint0( UOD2, 64 )
CALL unint0( WOD2, 65 )
CALL unint0( WHEOD2, 66 )
* 1160 CONTINUE for reference to original
RETURN *

ENTRY OXIDF

THE CALCULATION OF OXID FLOW IS IN GENERAL THE BALANCE OF ENERGY FLOW AND THE BALANCE OF MATERIAL. IN THIS SECTION AND ALSO FOLLOWING SECTIONS, THE NOTATIONS ARE AS FOLLOWS:

Pxyz: PRESSURE OF DUCT xyz
RHOxyz: DENSITY OF DUCT xyz
Hxyz: ENTHALPY OF DUCT xyz
SUxyz: SPECIFIC HEAT OF DUCT xyz
Uxyz: TOTAL INTERNAL ENERGY OF DUCT xyz
DWxyz: FLOW OF DUCT xyz
Wxyz: MASS OF DUCT xyz
WHExxyz: HELIUM WEIGHT OF DUCT xyz (BECAUSE OF POGO SYSTEM, HELIUM DOES APPEAR IN THE OXIDIZER SUPPLY DUCTS)
VHExyz: HELIUM VOLUMEN OF DUCT xyz
FHExyz: FRACTION OF HELIUM IN DUCT xyz

WHERE xyz CAN BE ONE OF THE FOLLOWING:
OS: OXIDIZER SUPPLY
OD1: LPOP OUTLET DUCT (COD IS ALSO USED FOR FLOW)
OI2: HPOP INLET DUCT
BECAUSE OF THE HIGH OPERATION TEMPERATURE AND ENERGY, THE OXIDIZER CAN BE WORKING UNDER TWO PHASE CONDITIONS. FUNCTION OXPROP() IS CALLED TO CALCULATE THE CONDITIONS OF GAS AND LIQUID PHASES OF OXIDIZER.

LPOP DISCHARGE DUCT

LPOP DISCHARGE DUCT "OD1" IS A MERGE POINT OF BOTH LPOP AND LPOT. THE INPUT FLOWS ARE DWOP1 AND DWOT1. AND THE OUTPUT FLOW IS DWCOD.

ABKFLO IS THE ENERGY BACK FLOW RATIO TO THE UPSTREAM OF THE PUMP.

IF(DWOP1.LE.0.)HOP=HOD1
HOD1=HOD1
IF (DWCOD .LT. 0.0) HOD1 = HOI2
UOD1 = pruint( DWOP1*HOP + (1. - ABKFLO)*TRQOPI*SOI*v9336 1 + DWOT1*HOI2 - DWCOD*HOD1 - TRQOTI*SOI*v9336, 0, 58) SSM60700
WOD1 = pruint( DWOP1 + DWOT1 - DWCOD, 0, 59 )
SUODI = UOD1 / WOD1
WHEODI = pruint( + WTHE(DWOP1, 0.0, FHEOD1, DWCOD, FHEOI2, DWOT1, FHEOT1), 0, 60 ) SSM60700
FHEOD1 = WHEOD1 / WOD1
VHEOD1 = .99*VHEOD1 + .01*WHEOD1 * 4632.*(THE/AMAX1(PODI-3.,
RHOD1 = WOD1 / AMAX1(1., VOLODI - VHEOD1)
RHOP1 = WOD1 / VOLODI
PODI = POD1 SSM60800
CALL OXPROP(PODI,HOD1,RHOD1,RHOLD1,RHOGD1,HGD1,HLD1,FLD1,SUOD1,N1)
HOD1 = SUOD1 + POD1 / (RHOD1 * 9336.)

HPOP INLET DUCT

THIS IS THE DUCT RIGHT BEFORE THE HIGH PRESSURE OXID PUMP.

THE INPUTS TO THIS DUCT ARE:

DWOP2C: BYPASS FLOW FROM DOWNSTREAM OF HPOP BOOSTER STAGE
DWOP3C: BYPASS FLOW FROM DOWNSTREAM OF HPOP
DWG0P: OXID FLOW FROM POGO SYSTEM IN GAS PHASE (CAN BE + OR -)

THE OUTPUTS OF THIS DUCT ARE:

DWO: OXID FLOW TO POGO SYSTEM IN LIQUID PHASE (CAN BE + OR -)

UOI2 = pruint( DWOP2C*HOD1 + DWOP2C*HOD3 + DWOP3C*HOD2 1 - DWO*HOI2 - DWOP2*HOI2 + 75.0*DWG0P + 1.25*(530.-TGAS)*DWHOP 2 + QBKFL2*WOI2 / AMAX1(10.0, WT2BK), 0, 61 )
WOI2 = pruint( + DWCOD + DWOP2C + DWOP3C - DWO - DWOP2 + DWG0P, 0, 62 ) SSM60900
SUOI2 = UOI2 / WOI2
WHEOI2 = pruint(
    + WTHE (DWCOD, FHEOD1, FHEOI2, DWOP2, FHEOD2, DWHOP, 1.0), 0, 63 )
FHEOI2 = WHEOI2 / WOI2
VHEOI2 = .99 * VHEOI2 + 46.32 * WHEOI2 * THEADD / 
    + rlimit( POI2L - 3., POI2L + 3., POI2))
RHOI2 = WOI2 / AMAX1(1., VOLOI2 - VHEOI2)
FHEOI2 = WHEOI2 / WOI2
POI2L = POI2
CALL OXPROP(POI2, HOI2, RHOI2, RHOI2, RHOGI2, HGI2, HLI2, FLI2, SUOI2, N4)
HOI2 = SUOI2 + POI2 / (RHOI2 * 9336.)

HPOP DISCHARGE DUCT TO MOV

THIS DUCT IS THE CONNECTION BETWEEN HPOP AND MOV.
THE INPUTS TO THIS DUCT ARE:
DWOP2: HPOP FLOW
THE OUTPUTS FROM THIS DUCT ARE:
DWOP3: OXID FLOW TO HPOP BOOSTER STAGE
DWOP3C: BYPASS FLOW BACK TO HPOP INLET DUCT
DWMOV: OXID FLOW TO MAIN OXID VALVE
DWOTII: FLOW TO HPOT INLET DUCT

UOD2 pruint( DWOP2*HOI2 + TRQOP2*SO2*v9336 - 
    + (DWOP3 + DWOP3C + DWMOV + DWOTII)*HOD2 - 
    + QBKFL2*WOI2/AMAX1(10., WT2BK), 0, 64 )
WOD2 = pruint( DWOP2 - DWOP3 - DWOP3C - DWMOV - DWOTII, 0, 65 )
SUOD2 = UOD2 / WOD2
WHEOD2 = pruint(
    + WTHE(DWOP2,FHEOI2,FHEOD2,DWOTII,FHEOTI,-DWMOV,FHEOD2), 0, 66 )
FHEOD2 = WHEOD2 / WOD2
VHEOD2 = .995 * VHEOD2 + 23.16 * WHEOD2 * THE / 
    + rlimit( POD2L - 3., POD2L + 3., POD2)
RHOD2 = WOD2 / AMAX1(1., VOLOD2 - VHEOD2)
VRHOD2 = 1. / RHOD2
RHOP2 = WOD2/VOLOD2
IF (IRHOP2 .EQ. 1) RHOP2 = WOI2/VOLOI2
POD2L = PO2
CALL OXPROP(POD2, HOD2, RHOD2, RHOLD2, RHOGD2, HGD2, HLD2, FLD2, 
1 SUOD2, N5)
HOD2 = SUOD2 + POD2 / (RHOD2 * 9336.)

LPOP TURBINE SUPPLY DUCT

THIS IS A SIMPLE ONE INPUT ONE OUTPUT DUCT FROM HPOP OUTLET TO LPOT INLET
INPUT TO THE DUCT:
DWOTII: FROM HPOP OUTLET
OUTPUT FROM THE DUCT:
C  DWOT1:  TO HPOT INLET

UOT1 = pruint( DWOT1*HOD1 - DWOT1*HOT1, 0, 67 )
WOT1 = pruint( DWOT1 - DWOT1, 0, 68 )
SUOT1=UOT1/WOT1
WHEOT1 = pruint( + WTHE(DWOT1,FHEOD1,FHEOT1,DWOT1,FHEOD1,0.0,0.0), 0, 69 )
FHEOT1=WHEOT1/WOT1
VHEOT1 = .99*VHEOT1 + 46.32*WHEOT1*THE /
+ rlimit( POT1L - 3., POT1L + 3., POT1 )
RHOT1 = WOT1 / AMAX1(1., VOLOT1 - VHEOT1)
RHOT1A=WOT1/VLOT1
POTIL=POT1
CALL OXPROP(POT1,HOT1,RHOT1,RHOT1A,RHOT1,HGT1,HLT1,FLT1,
1 SUOT1,N6)
HOT1 = SUOT1 + POT1 / (RHOT1 * 9336.)

HPBP DISCHARGE

THE HPBP DISCHARGE DUCT HAS:

INPUTS TO THE DUCT:
DWOP3:  HPOP BOOSTER PUMP FLOW

OUTPUTS FROM THE DUCT:
DWOP2C:  BYPASS FLOW BACK TO HPOP INLET DUCT
DWOP0V:  OXID SUPPLY TO OXID PREBURNER OXID CONTROL VALVE
DWFOV:  OXID SUPPLY TO FUEL PREBURNER OXID CONTROL VALVE

HOWEVER, FOLLOWING EQUATION USES AN EMPIRICAL EQUATION TO ESTIMATE
THE NEXT STATE OF SPECIFIC ENTHALPY.  THE EXACT MEANING OF THE EQUATION
IS UNKNOWN.  BUT IT SEEMS TO CONSIDER THE TIME DELAY OF THE DUCT AND
USE DT/0.2 AS A SMOOTH FACTOR.

*  HOD3=HOD3+DT/.2*(TRQOP3*SO2/(AMAX1(.3*SQR(AMAX1(100.,DPOP3)),1
1 DWOP3)*9336.))=HOD3+HOD2)
HOD3 = pruint( 5.*( TRQOP3*SO2/
+ ( AMAX1(.3*X10th( AMAX1(100., DPO3), 5 ), DWOP3 )*9336. ) -
+ HOD3 + HOD2 ),0, 70 )
POD3 = POD2 + DP02P1 - DWOP1 * ABS(DWOP1) * ROP3IN / RHOP2
CALL O2DFFP(HOD3,POD3,RHOP3,TOD3,3,1,1)
CALL O2DFP(HOD3,RHOP3,1,POD3,TOD3,3)

FLOW RATES

ALL THE OXID FLOW CALCULATED EXCEPT OPOV, FPOV AND POGO SYSTEM.

DWPO1L=DWPO1
CALL unint0( HOD3, 70 )
CALL lmin0( DWPO1, 71, 0.0, TooBig )
DWPO1 = prflow( DWPO1, Z0P1 + ZOIN, -.4*ROC0/RHOP1 - ROIN,
+ POPVDN + ELOIN*RHOOS*DDX*v386p4 + DPO1 - POD1, 71 )
rorhoi = - ROCOD / RHOI2
CALL lmint0( DWCOD, 72, 0.0, TooBig )
DWCOD = prflow( DWCOD, ZOCOD, rorhoi, POD1 - POI2, 72 )
IF ( DWOP2.GE.0. ) THEN
CALL lmint0( DWOP2, 73, 0.0, TooBig )
   DWOP2 = prflow( DWOP2, ZOP2, rorhoi, POI2 + DPOP2 - POD2, 73 )
ELSE
   DWOP2 = prflow( DWOP2, ZOP2, -.3*ROCOD*VRHOD2, POI2, DPOP2 - POD2, 73 )
ENDIF
DWOTII = prflow( DWOTII, hZOTI, - ROTIF * VRHOD2, POD2 - POT1, 74 )
DWOTI = prflow( DWOTI, hZOTI, - ROTIN/RHOTIA, POT1 - POD1, 75 )
ROIX = ROI * PRIMO1
DWMOV = prflow( DWMOV, ZMOV, + - (COV*RMOV + RMOV1 + ROIX)*VRHOD2, POD2-PCIE, 76 )
SSM61600
DWP3 = DWPO + DWFPO + DWPO2
DWP2C = X10th( recpos( (POD3 - POI2)*RHOP3/ROP2C ), 5 )
DWP3C = X10th( recpos( (POD2 - POI2)*RHOD2/ROP3C ), 5 )
PHIOT1 = S01 / (DWOT1+1.E-10)
* ROT1N=ANOT1+BNOT1*PHIOT1-CNOT1*PHIOT1**2
ROT1N = ANOT1 + PHIOT1*( BNOT1 - CNOT1*PHIOT1 )
PROTI=PODI/AMAX1 (POT1,.01)
DWO1A = recpos( DWOPI )

PUMP/TURBINE PERFORMANCE

SSM61700
IN THIS PUMP/TURBINE SECTION, THE NOTATIONS ARE:
FLOCOE: FLOW COEFFICIENT
DPxyz: PRESSURE CHANGE ACROSS THE PUMP/TURBINE
TRQxyz: TORQUE REQUIRED
CDPxyz: PRESSURE RAISE COEFFICIENT (CONSTANT, PUMP CHARACTERISTICS)
CTQxyz: TORQUE COEFFICIENT (CONSTANT, PUMP CHARACTERISTICS)
HCAVxyz: CAVITATION FACTOR FOR PRESSURE RAISE
TCAVxyz: CAVITATION FACTOR FOR TORQUE
WHERE xyz IS ONE OF THE FOLLOWING
OP1 (OR P1): LOW PRESSURE OXID PUMP
OP2 (OR P2): HIGH PRESSURE OXID PUMP
OP3 (OR P3): HIGH PRESSURE OXID PUMP BOOSTER STAGE
was 1/3 optimized

rhosol1 = RHOP1 * S01
FLOCOE = AMAX1(-39.5, DWOP1 / rhosol1)
rhoso = rhosol * S01
DPOP1 = FGEN(45, 38, FLOCOE) * rhoso * CDPOP1 * HCAVP1
TRQOP1 = FGEN(46, 39, FLOCOE) * rhoso * CTQOP1 * TCAVP1
rhoso2 = RHOP2 * S02
FLOCOE = DWOP2 / rhoso2
rhoso = rhoso2 * S01
DPOP2 = FGEN(47, 40, FLOCOE) * rhoso * CDPOP2 * HCAVP2
TRQOP2 = FGEN(48, 41, FLOCOE) * rhoso * CTQOP2 * TCAVP2
rhoso3 = RHOP3 * S02

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FLOCOE = DWOP3 / rhoso3  
rhoso = rhoso3 * SO2  
DPOP2 = FGEN(49, 42, FLOCOE) * rhoso * CDPOP3 * HCAVP3  
TRQOP2 = FGEN(50, 43, FLOCOE) * rhoso * CTQOP3 * TCAVP3  
* replaces typical  
* DPOP3=FGEN(49,2,DWOP3/(RHOP3*SO2) )*RHOP3*SO2**2*CDPOP3*HCAVP3  
* TRQOP3=FGEN(50,2,DWOP3/(RHOP3*SO2) )*RHOP3*SO2**2*CTQOP3*TCAVP3  
* Eliminated formatted output here  
*
IF ( GLOPC .GT. 0. ) THEN  
  DDX = 386.4 * GLOPC * PCIE  
ELSE  
  DDX = 386.4  
ENDIF  

PUMP CAVITATION DESCRIPTIONS

PUMP CAVITATION IS RATHER COMPLICATED IN NATURE. SINCE I DON'T HAVE THE DOCUMENT OR NBS TABLE ON HAND, I CAN ONLY FOLLOW THE CODE AND TRY TO EXPLAIN WHAT IS MEANT BY THE PROGRAM.

THE FIRST SECTION OF THE PROGRAM SEEMS TO FIND THE CAVITATION STATUS OF LPOP AT LOW OR NO FLOW CONDITIONS. THIS IS THE SITUATION WHEN THE ENGIN IS SHUTTNG DOWN AND THE OXID PREVALVE IS CLOSING. (PREVALVE IS THE VALVE BEFORE THE LPOP INPUT LINE TO CONTROL THE FLOW OF OXIDIZER FROM THE OXID TANK FOR AN INDIVIDUAL ENGIN.)

TIMCAV: AN INPUT VARIABLE, CAVITATION HAPPENS ONLY AFTER TIMCAV  
POINVP: OXID INPUT LINE VAPOR PRESSURE  
P1NPSH: NET POSITIVE SUCTION HEAD (NPSH) VARIABLE OF P1  
ICAVMD: FLAG TO SELECT THE METHOD OF CALCUALTING CAVITATION AT ZERO OXID FLOW OF P1 WHEN PREVALVE IS CLOSING

IF ( STIME .GT. TIMCAV) THEN  
  P1NPSH = (POS - POINVP)/(12.0*RHOOS)  
  FLOCI = AMINI(.8, DWOIA/rhosol*v41p34)  
  X1 = P1NPSH/(1. + solsq)  
  IF ( FLOCI .LT. 0.3) THEN  
    IF (ICAVMD .EQ. I) THEN  
      DUMY= AMAX1(0.,APV)  
      dubasl = AMINI(1. , DUMY/BASEAR)  
      dubas2 = 1. - dubasl  
      ZERHFL= dubasl*FGEN(66, 44, X1) + dubas2 * FGEN(81, 56, X1)  
      ZERTFL= dubasl*FGEN(67, 45, X1) + dubas2 * FGEN(82, 57, X1)  
    ELSE  
      ZERHFL= FGEN(66,44,X1)  
      ZERTFL= FGEN(67,45,X1)  
    ENDIF  
  ELSE  
    ZERHFL= FGEN(66,44,X1)  
    ZERTFL= FGEN(67,45,X1)  
  ENDIF
THE FOLLOWING CONDITION IS WHEN THE DWOP1 IS LESS THAN 0.0 (FLOW BACK)
AND THE CAVITATION IS COLLAPSING IN DIRECT PROPORTIONAL TO FLOW.

IF (DWOP1 .LT. 0.0) THEN
        accel = - DWOP1 / (RHOPI * WTOPI)
        HCAVP1 = prlint( accel, 0, 77 )
        TCAVP1 = prlint( accel, 0, 78 )
ENDIF

INTERPOLATION OF CAVITATION FACTOR FOR FLOW COEF BETWEEN 0.0 AND 0.3 OF
TCAV1 IS THE TIME CONSTANT TO GENERATE (OR COLLAPSE) CAVITATION.

ELSE
        fact2 = FLOC1 * 3.33333
        fact1 = 1. - fact2
        HCAVP1 = prlint( ( fact1*ZERHFL +
                        + fact2*FGEN(72, 46, X1) - HCAVP1 ) / TCAV1, 0, 77 )
        TCAVP1 = prlint( ( fact1*ZERTFL +
                        + fact2*FGEN(74, 47, X1) - TCAVP1 ) / TCAV1, 0, 78 )
ENDIF

INTERPOLATION OF CAVITATION FACTOR FOR FLOW COEF BETWEEN 0.3 AND 0.8 OF
TCAV1 IS THE TIME CONSTANT TO GENERATE (OR COLLAPSE) CAVITATION.

ELSE
        fact1 = 1.6 - 2. * FLOC1
        fact2 = 1. - fact1
        HCAVP1 = prlint( ( fact1*FGEN(72, 46, X1) +
                        + fact2*FGEN(73, 48, X1) - HCAVP1 ) / TCAV1, 0, 77 )
        TCAVP1 = prlint( ( fact1*FGEN(74, 47, X1) +
                        + fact2*FGEN(75, 49, X1) - TCAVP1 ) / TCAV1, 0, 78 )
ENDIF

FLOC2 = rlimit( .2, .8, DWOP2 / rhoso2 * v8p866)

POI2VP = quadr( HOI2 )
P2NPSH = (POI2 - POI2VP) / (12.0*RHOI2)

X2 = P2NPSH / ( so2sq + 1.)

IF( FLOC2 .LT. 0.5) THEN

INTERPOLATION OF CAVITATION FACTOR FOR FLOW COEF BETWEEN 0.0 AND 0.5 OF
TCAV1 IS THE TIME CONSTANT TO GENERATE (OR COLLAPSE) CAVITATION.

fact1 = 1.66667 - 3.33333 * FLOC2
fact2 = 1. - fact1
HCAVP2 = prlint( ( fact1 * FGEN(68, 50, X2) +
                        + fact2 * FGEN(76, 51, X2) - HCAVP2 ) / TCAV2, 0, 79 )
TCAVP2 = prlint( ( fact1 * FGEN(69, 52, X2) +
                        + fact2 * FGEN(78, 53, X2) - TCAVP2 ) / TCAV2, 0, 80 )

INTERPOLATION OF CAVITATION FACTOR FOR FLOW COEF BETWEEN 0.5 AND 0.8 OF
ELSE
    fact1 = 2.66667 - 3.33333 * FLOC2
    fact2 = 1. - fact1
    HCAVP2 = prlint( ( fact1 * FGEN(76, 51, X2) +
        fact2 * FGEN(77, 54, X2) - HCAVP2 ) / TCAV2, 0, 79 )
    TCAVP2 = prlint( ( fact1 * FGEN(78, 53, X2) +
        fact2 * FGEN(79, 55, X2) - TCAVP2 ) / TCAV2, 0, 80 )
ENDIF
*
* POD2VP = 620.15 + 19.1202 * HOD2 + 14.9371 * HOD2**2
* P3NPSH = (POD2 - POD2VP) / (12. * RHOD2)
* X3 = P3NPSH / (1 + SO2**2)  it matters
* POD2VP = quadr( HOD2 )
* P3NPSH = (POD2 - POD2VP) * 0.833333 * vRHOD2
* X3 = P3NPSH / (1 + SO2**2)
* HCAVP3 = prlint( (FGEN(70, 58, X3) - HCAVP3) / TCAV2, 0, 81 )
* TCAVP3 = prlint( (FGEN(71, 59, X3) - TCAVP3) / TCAV2, 0, 82 )
*
* Cavitation formatted output was eliminated. Output variables are
* included in the regular output list
*
ENDIF
*
OX INLET LINE DESCRIPTION
*
OXID TANK SUPPLIES THREE ENGINES. DWOE2 AND DWOE3 ARE THE FLOWS FROM
TANK TO ENGIN #2 AND ENGIN #3 RESPECTIVELY.
THE NOTATIONS USED IN THIS SECTION ARE:
TDCOM: TIME TO DETACH OXID TANK
WOCOM: OXID WEIGHT IN THE COMMON DUCT (FOR ALL THREE ENGINES)
POT: TANK PRESSURE AS FUNCTION OF TIME
ELCOM: ELEVATION OF OXIDIZER IN COMMON DUCT (VERTICAL FEEDING)
RCOM: RESISTANCE OF OXID COMMON DUCT
ZCOM: INERTIA OF OXID COMMON DUCT
ELOIN: ELEVATION OF OXID IN INLET DUCT (BETWEEN PREVALVE AND LPOP)
ROIN: RESISTANCE OF OXID INLET DUCT (BETWEEN PREVALVE AND LPOP)
ZOIN: INERTIA OF OXID INLET DUCT (BETWEEN PREVALVE AND LPOP)
RJTPVD: THE RESISTANCE BETWEEN JUNCTION AND DOWN SIDE OF PREVALVE
*
IF (STIME .GE. TDCOM ) THEN
    WOCOM = prlint( -DWOTJ, 0, 83 )
ENDIF
*
POT = FGEN(37, 9, STIME)
ELCOM = FGEN(58, 9, WOCOM)
RCOM = FGEN(59, 9, WOCOM)
ZCOM = FGEN(60, 9, WOCOM)
ELOIN = FGEN(61, 9, VOLPV)
*
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C C C C
ROIN = FGEN(62, 33, VOLPV)
ZOIN = FGEN(63, 34, VOLPV)
APV = recpos( FGEN (64, 35 , (STIME - TCUT - TCPPV) / DTPV) )
RJTPVD = RL1 + RPV / AMAX1(1.E-10, APV)**2

THIS SECTION CALCULATE THE BACK FLOW OF PUMPS. THE EQUATIONS USED TO
DESCRIBE THE BACKFLOW AND MINIMUM WEIGHT OF PUMP INPUT LINES ARE NOT
IN THE DOCUMENT.
QBKFLO: ENERGY BACK FLOW RATE TO THE UPSTREAM OF THE PUMP, BTU/SEC
WT1BK, WT2BK: DEFINITION NOT CLEAR, DIMENSION = LB

 QBKFLO: ENERGY BACK FLOW RATE TO THE UPSTREAM OF THE PUMP, BTU/SEC
WT1BK, WT2BK: DEFINITION NOT CLEAR, DIMENSION = LB

FLCOE1 = DWO1A / rhosol
EFF = recpos( FLCOE1 * (.03066 - .0003709*FLCOE1) )
flcoe = ( 1. - FLCOE1*v41p34 )
QBKFLO = recpos( TRQOP1*SO1*v9336*(1.-EFF)*flcoe )
WT1BK = AMIN1(800., 33. + 2.74E+06 * P1NPSH / solsq,
1. 1310. - 1.14E+06 * P1NPSH / solsq) * flcoe

IF ( VOLPV .GE. i0. )
+ WT1BK = AMIN1( WOIN,WT1BK)
+ ABKFLO = QBKFLO*9336./( AMAX1(1. , TRQOP1)*SO1)
+ FLCOE2 = recpos( DWOP2/(RHOP2*SO2) )
+ EFF2 = recpos( FLCOE2 * ( .1537 - .008667 * FLCOE2 ) )
+ QBKFL2 = ABK2 *
+ recpos( TRQOP2*SO2*v9336*(1.-EFF2)*(1.-FLCOE2*v8p866) )
+ WT2BK = AMIN1(270., so2sq*(2.583E-4 - 2.91E-5*FLCOE2) )

THIS PART CALCULATES THE ENERGY BALANCE AND FLOW BETWEEN OXID TANK AND
LPOP. THE LAYOUT OF THE HARDWARE OF THE SYSTEM IS:

TANK ------------> JUNCTION --------------> PREVALVE --------------> LPOP
               TO OTHER
               ENGIN
               (TOP) COMMON DUCT
               EL1 OIN (DOW
               FLOW: DWOTJ DWOPV DWOI
               PRESSURE:
               POT POJ POPVDPN POS

HOTNK = FGEN(5, 8, STIME)
POTVP = quadr( HOTNK )
fact1 = AMIN1(1.0, 3.33333 * APV )
POTVP = fact1 * POTVP + (1. - fact1) * POINVP
DWOTJ = DWOPV + DWOE2 + DWOE3

IF (WOCOM .LE. 0.0) DWOTJ = 0.0

OXID FLOWS TO ENGIN #2 AND ENGIN #3 ARE TIME SCHEDULED

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DWOE2L=DWOE2
DWOE2=FGEN(65, 36, STIME-TCUT2)
DDWOE2=(DWOE2-DWOE2L)/DT
DWOE3L=DWOE3
DWOE3=FGEN(65, 60, STIME-TCUT3)
DDWOE3=(DWOE3-DWOE3L)/DT
DWOPVL=DWOPV

* Originally DWOPV step was computed at some expense, then discarded
* if WOCOM .LE. 0.

rhdd4 = RHOOS * DDX * v386p4
IF ( WOCOM .LE. 0.0) THEN
  DWOPV = 0.0
ELSE
  CALL prflow( DWOPV, ZCOM+ZJTPV, -RJTPVD,
               POT + (ELCOM + ELJPV)*rhdd4 - POPVDN -
               RCOM*DWOTJ*ABS(DWOTJ) - (DDWOE2+DDWOE3) * ZCOM, 84 ) 3000
ENDIF
DDWOTJ = DDWOE2 + DDWOE3 + (DWOPV - DWOPVL) / DT
POJ = POT + ELCOM*rhdd4 - RCOM*DWOTJ**2 - ZCOM*DDWOTJ

IN THE FOLLOWING CALCULATION, THE CONSTANT "BOPVDN" USED FOR CALCULATING POPVDN IN THE CASE OF FLOW CHANGE IN THE INPUT LINE IS SUSPICIOUSLY THE VALUE OF "BOPVDN" GIVEN IN THE FILE "START4.DAT" IS 5.0 (PSI/LB). WHILE AN EQUIVALENT CASE IN OPOV LINE, "CFACT"=400000. (PSI/LB). I BELIEVE THE VALUE SHOULD BE CHANGED ESPECIALLY IN THE TRANSIENT STUDY CONDITION FOR OUTPUT FLOW > INPUT FLOW WHERE EMPTY SPACE CAN BE GENERATE WITH THE PRESSURE EQUAL TO VAPOR PRESSURE OF THE OXID LINE.

VOLPV: EMPTY SPACE VOLUMN FILLED BY OXID VAPOR IN PREVALVE SIDE

In the original, if DWOPI .EQ. DWOPV, UOIN and WOIN get integrated twice.

pdWOPV = recpos( DWOPV )
IF ( DWOPI .GT. 0.0 ) THEN
  IF ( DWOPI .GE. DWOPV ) THEN
    CALL unint0( POPVDN, 85 )
    POPVDN = pruint( BOPVDN*(DWOPV-DWOPI), 0, 85 )
  ENDIF
  POPVDN = AMAX1(POTVP, POPVDN ) variable lower limit is implemented by re-initializing the integrator.
  *
  IF ( POPVDN .LT. POTVP ) THEN
    POPVDN = POTVP
    CALL unint0( POTVP, 85 )
  ENDIF
  IF ( POPVDN .LE. POTVP + .001) THEN
    VOLPV = pruint( ( DWOPI - pdWOPV )/RHOOS, 0, 86 )
  ENDIF

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No change in VOLPV if POPVDN .GT. POTVP + .001 ?

UOIN = pruint( pDWOPV*FGEN(5, 8, STIME) - 
        DWOP1*HOS + QBKFLO*WOIN/AMAX1(77.,WT1BK), 0, 87 )
WOIN = pruint( pDWOPV - DWOP1, 0, 88 )

CONDITION FOR INPUT_FLOW > OUTPUT_FLOW WHERE EMPTY SPACE (IF EXISTS)
ARE BEING FILLED. OR THE PRESSURE MAY RAISE IF THERE IS NO EMPTY SPACE.

ELSE
    VOLPV = prlint( (DWOP1 - DWOPV)/RHOOS, 0, 86 )
    IF( VOLPV .GE. .001) THEN
        POPVDN = POTVP
    ELSE
        POPVDN = pruint( BOPVDN*(DWOPV- DWOP1), 0, 85 )
        IF ( POPVDN .LT. POTVP ) THEN
            POPVDN = POTVP
        ELSE
            CALL unint0( POTVP, 85 )
        ENDIF
    ENDIF
    IF( DWOPV .GT.0.) THEN
        HOPV = FGEN(5, 8, STIME)
    ELSE
        HOPV = HOS
    ENDIF
    UOIN = pruint( DWOPV*HOPV - DWOPI*HODI + QBKFLO*WOIN/AMAX1(77., WT1BK), 0, 87 )
    WOIN = pruint( DWOPV - DWOP1, 0, 88 )
ENDIF

BACK FLOW FROM THE PUMP, FILLING UP THE EMPTY SPACE

ELSE
    IF ( VOLPV .GT. 0.001 ) THEN
        VOLPV = prlint( (DWOP1 - pDWOPV)/RHOOS, 0, 86)
        POPVDN = POTVP
        CALL unint0( POTVP, 86 )
        UOIN = pruint( pDWOPV*FGEN(5, 8, STIME) 
                       - DWOP1*HOD1+QBKFLO*WOIN/AMAX1(77.,WT1BK), 0, 87 )
        WOIN = pruint( pDWOPV-DWOP1, 0, 88 )
    ENDIF

BACK FLOW FROM THE PUMP, WITHOUT EMPTY SPACE IN THE LINE

ELSE
    POPVDN = pruint( BOPVDN*(DWOPV - DWOP1), 0, 85 )
    IF ( POPVDN .LT. POTVP ) THEN
        POPVDN = POTVP
        CALL unint0( POTVP, 85 )
    ENDIF
IF ( DWOPV .GT. 0.0) THEN
    UOIN = pruint( DWOPV*FGEN(5,8,STIME) - DWOP1*HOD1 +
                 QBKFLO*WOIN/AMAX1(77., WT1BK), 0, 87 )
ELSE
    UOIN = pruint( DWOPV*HOS - DWOP1*HOD1 +
                 QBKFLO*WOIN/AMAX1(77., WT1BK), 0, 87 )
ENDIF
WOIN = pruint( DWOPV-DWOP1, 0, 88 )
ENDIF
POS = POPVDN + ELOIN*rhdd4 - ROIN*DWOP1*ABS(DWOP1) -
     ZOIN*(DWOP1 - DWOP1L)/DT
IF (POS .LT. POINVP) POS = POINVP
POSX = pruint( TAU*(POS - POSX), 0, 89 )
SUOIN = UOIN/WOIN
HOS = SUOIN + POS/(RHOOS*9336.)

FOLLOWING IS AN ESTIMATION OF THE SPECIFIC ENTHALPY OF THE "OIN" LINE.
IT SEEMS THIS IS ONLY TRUE FOR A STEADY STATE FLOW.
BASED ON THE EQUATION BELOW, IT SUGGESTS THAT THE FILLED UP WEIGHT OF THE
"OIN" LINE IS 77LB.

IF ( DWOP1 .GT. 0. ) THEN
    HOS1 = pruint( DWOP1*v77*(HOS-HOS1), 0, 90 )
ELSE
    HOS1 = pruint( -DWOP1*v77*(HOD1 - HOS1), 0, 90 )
ENDIF
POINVP = quadr( HOS1 )
TRQOTI =(AOTI - BOTI*PHIOTI)*DWOTI*ABS(DWOTI)*CTQOT1

POGO SYSTEM BALANCE IS CALLED AS PART OF THE OXID FLOW.

CALL POGOS

PRIME MAIN CHAMBER

PRIMING OF MOV AND OXID INJECTOR IS DEFINED AS SIMPLE FUNCTIONS OF
FILLED UP RATION OF THE PARTICULAR SPACE.
WOV: WEIGHT TO BE FILLED, INITIAL VALUE = -2.0, FILLED = 0.0
WOI: INJECTOR OXID WEIGHT, INIT VALUE = 0.0, FILLED = 46.2

IF( XMOMPF .AND. WOV.GT.-.1) THEN
    COV = 1. + 10. * WOV
    IF(WOV.GT.-.001) THEN
        WRITE(event,'(A,E12.4)') ' MOV BUBBLE PRIMED AT ', STIME
        XMOMPF = .FALSE.
    END IF
ELSE IF ( WOV .LT. -.001 ) THEN
    COV=0.025
ELSE

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COV = 1.0
END IF

WOI = prlnt( DWMOV * COV - DWOI, 0, 91 )
WOV = prlnt( DWMOV * (1.0 - COV), 0, 92 )
rhomov = VOLOD2 / WOD2
PRIMOI = FGEN(3, 37, WOI)

IF( PRIMIF .AND. WOI .GT. 40. ) THEN
    WRITE( event,'(A,E12.4)' ) 'MC PRIMED AT ', STIME
    PRIMIF = .FALSE.
END IF

DWOI = DWMOV * PRIMOI * COV
POINJ = PCIE + ROI * DWOI**2 * rhomov
PMOV = POD2

* * *
IF ( TIME .GE. TL1 .AND. TIME .LE. TH1 ) WRITE(6,1410) TIME, WOCOM, ELCOM, etc

IN FUEL FLOW SUBROUTINE, QF IS TOTAL FUEL FLOW IN GALLON/MIN.
QO IN THE FOLLOWING EQUATION DOESN'T SEEM TO REPRESENT SIMILAR QUANTITY.

\[ QO = (1.0 - 0.002789 \times (TOS - 160.)) \times (17.5339 + 6.19891 \times (DWOTPR + DWMOV + DWOP3 - DWOP2C) + 0.208812 \times SO2) \times \text{AMINI}(1.0, (DWOTPR + DWMOV + DWOP3 - DWOP2C) \times 2.1) \]

\[ dwsunx = DWOTPR + DWMOV + DWOP3 - DWOP2C \]
\[ QO = (1.0 - 0.002789 \times (TOS - 160.)) \times (17.5339 + 6.19891 \times dwsunx + 0.208812 \times SO2) \times \text{AMINI}(1.0, dwsunx \times 2.1) \]

OXIDIZER PUMP SPEEDS

IN THE FOLLOWING CALCULATIONS:
TQxyzB: BREAKAWAY TORQUE OF PUMP xyz

IF ( SO1 .LT. 11:0 ) THEN
    IF ( TRQOT1 - TRQOP1 .LT. TQOT1B ) THEN
        DSO1 = 0.0
    ELSE
        DSO1 = ( TRQOT1 - TRQOP1 ) / GO1
    ENDIF
ELSE
    DSO1 = ( TRQOT1 - TRQOP1 ) / GO1
ENDIF

SO1 = prlnt( DSO1, 0, 93 )
solsq = SO1 ** 2
trqsum = TRQOT2 - TRQOP2 - TRQOP3
IF ( SO2 .LT. 11:0 ) THEN
    IF ( trqsum .LT. TQOT2B ) THEN
        2021, 2025, 2025
DSO2=0.0
ELSE
   DSO2 = (trqsum - TDRAGO)/GO2
ENDIF
ELSE
   DSO2 = (trqsum - TDRAGO)/GO2
ENDIF
SO2 = prlnt( DSO2, 0, 94 )
so2sq = SO2 ** 2
RETURN
END
SUBROUTINE oxprp0 (P, H, RHO, RHOL, RHOG, HG, HL, FL, SUIN, icall)

*******************************************************************************
C PURPOSE: CALCULATE LIQUID AND SATURATED OXYGEN PROPERTIES
C
C*****ARGUMENTS*****
C INPUT:
C RHO = DENSITY, LB/IN3
C SUIN = SPECIFIC INTERNAL ENERGY, BTU/LB
C
C NX = CALLER NODE INDEX ARRAY
C
C OUTPUT:
C P = PRESSURE, PSI
C H = SPECIFIC ENTHALPY, BTU/LB
C
C IF SATURATED, ADDITIONAL OUTPUT IS:
C FL = LIQUID MASS FRACTION
C RHOL = SATURATED LIQUID DENSITY, LB/IN3
C RHOG = SATURATED GAS DENSITY, LB/IN3
C SLIQ = SATURATED LIQUID SPECIFIC INTERNAL ENERGY, BTU/LBM
C SGAS = SATURATED GAS SPECIFIC INTERNAL ENERGY, BTU/LBM
C HL = SATURATED LIQUID SPECIFIC ENTHALPY, BTU/LBM
C HG = SATURATED GAS SPECIFIC ENTHALPY, BTU/LBM
C
* The entry OXPROP bypasses initialization.
*
*******************************************************************************
PARAMETER (NSAT = 74, NSU = 60, NRHO = 60, NCALL = 10 )

DIMENSION A(60,60) , PSC(74) , SLC(74) , SGC(74) , RLC(74) ,
* RGC(74) , SU(60) , RH(60) , RS(60)

* Precomputed slopes:

REAL SUvsRS(NSU), AvsSU( NSU, NRHO ), vdRHO(NRHO),
+ RLvsP( NSAT ), RGvsP( NSAT ), SLvsP( NSAT ), SGvsP( NSAT )

* Previous call intervals:

INTEGER isu(NCALL), irho(NCALL), ipres(NCALL)

DATA PSC /
* 1.10,  1.33,  1.61,  1.92,  2.29,  2.71,  3.19,
* 3.74,  4.36,  5.06,  5.85,  6.73,  7.71,  8.80,
* 10.01, 11.34, 12.81, 14.42, 16.18, 18.11, 20.20,
* 22.47, 24.94, 27.60, 30.47, 33.56, 36.88, 40.43,
* 44.24, 48.31, 52.65, 57.28, 62.19, 67.41, 72.95,
* 78.81, 85.01, 91.56, 98.47, 105.75, 113.42, 121.48,
+ 129.95, 138.84, 148.16, 157.93, 168.15, 178.83, 190.00,
* 201.66, 213.83, 226.52, 239.74, 253.50, 267.82, 282.71,
* 298.19, 314.26, 330.95, 348.27, 366.23, 384.86, 404.16,
* 424.16, 444.87, 466.32, 488.53, 511.52, 535.32, 559.97,
* 585.49, 611.92, 639.30, 731.38/

DATA SLC /
* -71.21, -70.41, -69.62, -68.82, -68.02, -67.22, -66.42,
* -65.62, -64.82, -64.02, -63.22, -62.42, -61.61, -60.81,
* -60.00, -59.20, -58.39, -57.58, -56.77, -55.96, -55.15,
* -54.34, -53.52, -52.70, -51.89, -51.07, -50.24, -49.42,
* -48.59, -47.77, -46.94, -46.10, -45.27, -44.43, -43.59,
* -42.74, -41.90, -41.04, -40.19, -39.33, -38.47, -37.60,
* -36.72, -35.85, -34.96, -34.07, -33.18, -32.27, -31.37,
* -30.45, -29.52, -28.59, -27.64, -26.68, -25.71, -24.73,
* -23.73, -22.72, -21.69, -20.65, -19.59, -18.51, -17.41,
* -16.29, -15.13, -13.95, -12.73, -11.46, -10.14, -8.76,
* -7.29, -5.72, -3.98, 4.95/

DATA SGC /
* 19.68, 19.97, 20.27, 20.57, 20.86, 21.15, 21.43,
* 21.72, 22.00, 22.28, 22.56, 22.83, 23.10, 23.37,
* 23.63, 23.89, 24.14, 24.39, 24.64, 24.88, 25.12,
* 25.35, 25.58, 25.80, 26.02, 26.23, 26.43, 26.63,
* 26.82, 27.01, 27.19, 27.36, 27.53, 27.69, 27.84,
* 27.98, 28.12, 28.37, 28.48, 28.59, 28.68, 28.80,
* 28.76, 28.84, 28.90, 28.96, 29.00, 29.03, 29.05,
* 29.06, 29.05, 29.03, 29.00, 28.95, 28.88, 28.80,
* 28.69, 28.57, 28.42, 28.26, 28.06, 27.84, 27.59,
* 27.30, 26.97, 26.60, 26.17, 25.68, 25.11, 24.45,
* 23.66, 22.69, 21.51, 4.95/

DATA RLC /
* .04450, .04431, .04413, .04394, .04376, .04357, .04338,
* .04319, .04300, .04281, .04262, .04243, .04224, .04204,
* .04185, .04165, .04145, .04125, .04105, .04085, .04065,
* .04045, .04024, .04003, .03983, .03962, .03940, .03919,
* .03897, .03876, .03854, .03832, .03809, .03787, .03764,
* .03741, .03717, .03694, .03670, .03645, .03621, .03596,
* .03571, .03545, .03519, .03492, .03465, .03438, .03410,
* .03381, .03352, .03322, .03292, .03261, .03230, .03197,
* .03163, .03129, .03093, .03056, .03018, .02979, .02938,
* .02895, .02850, .02803, .02753, .02700, .02644, .02582,
* .02515, .02440, .02353, .01576/

DATA RGC /
* .00001, .00002, .00002, .00002, .00003, .00003, .00004,
* .00005, .00005, .00006, .00007, .00008, .00009, .00010,
* .00011, .00013, .00014, .00016, .00018, .00020, .00022,
* .00024, .00026, .00029, .00032, .00035, .00038, .00041,
* .00045, .00049, .00053, .00057, .00062, .00067, .00072,
* .00077, .00083, .00089, .00096, .00102, .00110, .00117, SSM65000
* .00125, .00134, .00142, .00152, .00162, .00172, .00183, 
* .00195, .00207, .00220, .00233, .00248, .00263, .00279, 
* .00296, .00313, .00332, .00353, .00374, .00397, .00422, 
* .00448, .00476, .00507, .00540, .00577, .00617, .00663, 
* .00715, .00776, .00847, .01576/

DATA SU /
* -64.00, -63.75, -63.50, -63.25, -63.00, -62.75, -62.25, -62.00, -61.75, -61.50, -61.25, -61.00, -60.75, 
* -60.50, -60.25, -60.00, -59.50, -59.00, -58.50, -58.00, -57.50, -57.00, -56.50, -56.00, -55.50, -55.00, -54.50, 
* -54.00, -53.50, -53.00, -52.50, -52.00, -51.50, -51.00, -50.50, -50.00, -49.00, -48.00, -47.00, -46.00, -45.00, 
* -44.00, -43.00, -42.00, -41.00, -40.00, -38.00, -36.00, -34.00, -32.00, -30.00, -28.00, -26.00, -24.00, -22.00, 
* -20.00, -18.00, -16.00, -14.00/

DATA RS /
* .04281, .04275, .04269, .04263, .04257, .04251, .04245, SSM65100
* .04239, .04233, .04227, .04221, .04215, .04209, .04203, 
* .04197, .04191, .04185, .04172, .04160, .04148, .04136, 
* .04123, .04111, .04099, .04086, .04074, .04061, .04049, 
* .04036, .04024, .04011, .03998, .03985, .03973, .03960, 
* .03947, .03934, .03922, .03882, .03855, .03829, .03802, 
* .03775, .03748, .03720, .03692, .03664, .03607, .03549, 
* .03490, .03429, .03367, .03304, .03239, .03172, .03104, 
* .03033, .02960, .02884, .02805/

DATA RH /
* .70000, .75000, .80000, .85000, .90000, .95000, 1.00000, SSM65200
* 1.00002, 1.00004, 1.00006, 1.00008, 1.00010, 1.00012, 1.00016, 
* 1.00020, 1.00025, 1.00030, 1.00035, 1.00040, 1.00045, 1.00050, 1.00060, 
* 1.00080, 1.00100, 1.00120, 1.00160, 1.00200, 1.00240, 1.00300, 
* 1.00360, 1.00420, 1.00480, 1.00540, 1.00600, 1.00840, 1.00960, 1.01080, 
* 1.01200, 1.01440, 1.01680, 1.01920, 1.02280, 1.02640, 1.03000, 
* 1.03360, 1.03720, 1.04080, 1.04440, 1.04800, 1.05160, 1.05520, 
* 1.05880, 1.06240, 1.06600, 1.06960, 1.07320, 1.07680, 1.08040, 
* 1.08400, 1.08760, 1.09180, 1.09540/

DATA (A(I, 1), I=1,60) /
* .37, .39, .41, .43, .45, .47, SSM65400
* .49, .51, .54, .56, .58, .61, 
* .64, .66, .69, .72, .75, .82, 
* .88, .95, 1.03, 1.11, 1.19, 1.28, 
* 1.37, 1.47, 1.57, 1.68, 1.80, 1.92, 
* 2.04, 2.18, 2.32, 2.46, 2.62, 2.77, 
* 2.94, 3.30, 3.68, 4.10, 4.55, 5.04, 
* 5.56, 6.13, 6.73, 7.37, 8.05, 9.55, 
* 11.24, 13.11, 15.18, 17.45, 19.93, 22.61,
DATA (A(I, 2), I=1,60) /
* .40, .42, .44, .46, .48, .50,
* .52, .55, .57, .60, .63, .65,
* .68, .71, .74, .77, .81, .87,
* .95, 1.02, 1.10, 1.19, 1.27, 1.37,
most of table omitted
* 10000.00, 10000.00, 10000.00, 10000.00, 10000.00, 10000.00,
* 10000.00, 10000.00, 10000.00, 10000.00, 10000.00, 10000.00,
* 10000.00, 10000.00, 10000.00, 10000.00, 10000.00, 10000.00,
* 10000.00,SSM71900
* 10000.00, 10000.00, 10000.00, 10000.00, 10000.00, 10000.00,
* 9815.73, 8760.81, 7130.06, 6397.53, 5773.35, 5155.16,
* 4661.49, 4221.40, 3813.73, 3432.45, 3054.53, 2743.86/

Unnecessary initializations were removed.

Precomputing slopes:

DO 10 I = 2, NSU
SUvsRS(I) = (SU(I) - SU(I-I) ) / (RS(I) - RS(I-I) )
10 CONTINUE

DO 20 I = 2, NSAT
VDPRES = 1.0 / (PRES(I) - PRES(I-1) )
RLvsP(I) = (RLC(I) - RLC(I-I) ) * VDPRES
RGvsP(I) = (RGC(I) - RGC(I-I) ) * VDPRES
SLvsP(I) = (SLC(I) - SLC(I-I) ) * VDPRES
SGvsP(I) = (SGC(I) - SGC(I-I) ) * VDPRES
20 CONTINUE

CALL xyset( NSU, SU, NRHO, RH, \nAvsSU, vdRHO )
ENTRY OXPROP (P, H, RHO, RHOL, RHOG, HG, HL, FL, SUIN, icall)

This entry bypasses initialization

Interpolation with TABLX and TABLXY was replaced by interpolation
with the reorganized interpolation module routines. Extrapolation
if an input value escapes its table. Also interpolation is based on
precomputed slopes.

CALL intval( isu(icall), SUIN, NSU, SU, 
+ 'Oxygen energy is below the table.', 
+ 'Oxygen energy exceeds the table.', 0 )
iu = isu(ical1)
R = RHO / xlint( SUIN, NSU, SU, RS, SUvsRS, iu)

* CALL intval( irho(ical1), R, NRHO, RH,
+ 'Oxygen density is below the table.',
+ 'Oxygen density exceeds the table.', 0 )
ir = irho(ical1)
P = xylint( SUIN, R, NSU, SU, RS, SUvsRS, ir )

* H = SUIN + P / (9336.0 * RHO)
IF (R .GE. 1.0) THEN
  FL = 1.0
ELSE
  CALL intval( ipres(ical1), P, NSAT, PSC,
+ 'Oxygen pressure is below the table.',
+ 'Oxygen pressure exceeds the table.', 0 )
  ip = ipres(ical1)
  RHOL = xlint( P, NSAT, PSC, RLC, RLvsP, ip )
  RHOG = xlint( P, NSAT, PSC, RGC, RGvsP, ip )
  SLIQ = xlint( P, NSAT, PSC, SLC, SLvsP, ip )
  SGAS = xlint( P, NSAT, PSC, SGC, SGvsP, ip )
  FL = (SUIN - SGAS) / (SLIQ - SGAS)
  HL = SLIQ + P / (9336.0 * RHOL)
  HG = SGAS + P / (9336.0 * RHOG)
END IF
RETURN
END

'o2prime.for':
SUBROUTINE O2PRM0

SUBROUTINE O2PROP(SU,SRHO,N,P,T,NN)
PURPOSE: OXIGEN PROPERTY DATA

THIS SUBROUTINE IS THE OXIDIZER PROPERTY TABLE LOOK-UP. (NOT HYDROGEN)
THERE ARE ACTUALLY TWO TABLES.
FIRST ONE IS THE TWO DIMENTIONAL CURVES: PRESSURE(U, RHO)
SECOND ONE IS THE TWO DIMENTIONAL CURVES: TEMPERATURE(U, RHO)
SPECIFIC ENTHALPY U RANGE FROM -57.5 TO 110.0
DENSITY RHO RANGES FROM 0.08 TO 80.0
THE PROGRAM ONLY DO INTERPOLATION AND WILL BE KICKED OUT IF THE RANGE IS
OUT OF REACH.

*****ARGUMENTS*****
NN = 0  INITIALIZATION
NN = 1 OR 2  SU,SRHO, P,T

156
PARAMETER (N=CALL=20, NU=15, NRHO=21, NSAT=NU)
PARAMETER (NP=NSAT*NRHO, NT=NRHO-4)

DIMENSION U(NU), RHO(NRHO), PRES(NU,NRHO), TEMP(NU,NRHO)
REAL UvsP(NU,NRHO), TXP(NU,NRHO), vDRHO(NRHO), H(NU,NRHO),
+ apo2(NRHO, NU), bpo2(NRHO, NU), cpo2(NRHO, NU), dpo2(NRHO, NU),
+ ato2(NRHO, NU), bto2(NRHO, NU), cto2(NRHO, NU), dto2(NRHO, NU),
+ JSAT(NSAT)
DIMENSION II(NCALL), J1(NCALL), J2(NCALL), R(2)

SAVE

DATA II /NCALL*2/, J1 /NCALL*2/, J2 /NCALL*2/
* DATA G / NP*0.0 /
* DATA H / NP*0.0 /
* DATA C / NT*1.0 /

DATA JSAT / 19, 18, 17, 16, 15, 14, 12,
11, 11, 10, 9, 8, 8, 7, 7 /

DATA U
* -57.5, -55.1, -51.0, -46.8, -39.9, -29.8, -20.0, -10.0,
* .0, 10.0, 30.0, 50.0, 70.0, 90.0, 110.0/
DATA RHO
* .0800, .2000, .4000, .8000, 1.200, 2.00, 4.00,
8.0, 52900
* 16.000, 32.000; 40.00, 50.00, 55.00, 58.430, 63.400, 66.590,
* 68.450, 70.20, 71.29, 75.00, 80.00 /
DATA (PRES(I,01), I=1,15) /

most of tables omitted

* 161.90, 165.40, 171.40, 177.50, 187.80, 203.40, 218.80, 234.60,
* 200.00, 200.00, 200.00, 200.00, 200.00, 200.00, 200.00/
DATA (TEMP(I,20), I=1,15) /
* 152.00, 154.00, 162.00, 164.00, 174.00, 192.00, 210.00, 220.00,
* 200.00, 200.00, 200.00, 200.00, 200.00, 200.00, 200.00/
DATA (TEMP(I,21), I=1,15) /
* 131.00, 137.00, 143.00, 150.00, 165.00, 180.00, 200.00, 200.00,
* 200.00, 200.00, 200.00, 200.00, 200.00, 200.00, 200.00/
**INITIALIZE SLOPES**

```
DO 26 J = 1, NRHO
   RHO(J) = RHO(J)/1728.
DO 25 I = 2, NU
   UVSP(I,J) = (U(I) - U(I-1)) / (PRES(I,J) - PRES(I-1,J))
   TXP(I,J) = (TEMP(I,J) - TEMP(I-1,J)) / (U(I) - U(I-1))
25 CONTINUE
IF(J .NE. NRHO) THEN
   DRHO = RHO(J+1)/1728. - RHO(J)
   vDRHO(I) = 1. / DRHO
ENDIF
26 CONTINUE
```

This overcomplicated precomputation replaced by a more efficient, more straightforward, and generally reusable cubic spline system.

**GET U CURVATURE, H AND RHO CURVATURE, G, FOR SPLINE INTERPOLATION**

```
DO 30 J = 1, 21
   CALL splin0(15, RHO, PRES(I,J), apo2(1,J), bpo2(1,J), cpo2(1,J), dpo2(1,J))
   CALL splin0(15, RHO, TEMP(I,J), ato2(1,J), bto2(1,J), cto2(1,J), dto2(1,J))
30 CONTINUE
```

Removed echo of O2 tables

**RETURN**

**ENTRY o2pt(SU, SRHO, N, P, T)**
P2 = spline(I, SRHO + apo2(l, I), bpo2(l, I), cpo2(l, I), dpo2(l, I))

* RHOP1 = (SRHO - RHO(J)) * vDRHO(J)

U1 = U(I-1)
U2 = U(I)
JS = JSAT(I)
JS1 = JSAT(I-1)
IF((J.EQ.JS.AND.JS.NE.JSI) .OR. (I.EQ.7.AND.J.EQ.JS+1)) THEN
  USAT = U2 + (U1-U2)*(SRHO-RHO(JS))/(RHO(JSI)-RHO(JS))
  PSAT = PRES(I-1,JS1) + (PRES(I,JS)-PRES(I-1,JS1))/(U2-U1)
ENDIF

IF(SU.GT.USAT) THEN
  PI = PSAT
  U1 = USAT
  H1 = 0.0
ELSE
  P2 = PSAT
  U2 = USAT
  H2 = 0.0
ENDIF

P = SPLINE(P1, P2, H1, H2, SU-U1, U2-SU)

The above spline fit of pressure parallel to the enthalpy axis is misapplied. Only two points have been found on the surface at the interpolated cross section. To fit a spline, it would be necessary to find more than four cross section points. It might be desirable to find four points and interpolate with a cubic through them. Here, we substitute a linear interpolation in SU.

UP1 = SU - U(I-1)
P = P1 + UP1 * vdu(I) * (P2 - P1)

T1 = TEMP(I-1,J) + TXP(I,J) * UP1
T2 = TEMP(I-1,J+1) + TXP(I,J+1) * UP1
T = T1 + (T2 - T1) * RHOP1

159 RETURN

ENTRY rto2(SU, SRHO, N, P, T)

C
C
C

300 CONTINUE
K=I-1

159
J = J2(N)
310 IF(PRES(K,J).LT.P) GO TO 330
220 IF(PRES(K,J-1).LE.P) GO TO 340
J = J-1
GO TO 320
330 J = J+1
GO TO 310

* Should be recoded to halt with message, rather than limit J
* If rows and columns of PRES were reversed, intvval could be
* used.

340 J = MAX0(2,MIN0(J,NRHO))
IF(K.EQ.I-1) J2(N) = J

* R(K-I+2) = RHO(J-1) + (P-PRES(K,J-1))/(PRES(K,J) - PRES(K,J-1))

* $ *DRHO(J-1) should use precomputed slope

* R(K-I+2) = RHO(J-1) + (P-PRES(K,J-1)) * RvsP(K,J) * RvsP(K,J)
IF(K.EQ.I) GO TO 350
K = I
GO TO 310

C ASSUME RHO LINIER WITH 1/U
350 SRHO = R(1) + (U(I) - U(I)*U(I-1)/SU)*(R(2) - R(1))/(U(I) - U(I-1))
GO TO 140

* ENTRY uTo2( SU, SRHO, N, P, T )

**********************************************************************
C
C GET U AND T FROM RHO AND P
C
**********************************************************************
1000 DO 1010 K = 1, NRHO
IF(RHO(K).GT.SRHO) GO TO 1030
1010 CONTINUE
K = NRHO
1030 IT = 1
1035 DO 1040 M = 1, NU
IF(PRES(M,K-1).GT.P) GO TO 1050
1040 CONTINUE
M = NU
1050 IF(IT.NE.1) GO TO 1060

* Should be recoded to halt with message, not limit M
M = MAX0(2, M)

* U1 = U(M-1) + (P-PRES(M-1,K-1))/(PRES(M,K-1) - PRES(M-1,K-1))*(U(M-1)

* 1 * UvsP(M,K)

SSM56000
SSM56100
SSM56200
IT=2
K=K+1
GO TO 1035
1060 M=MAX0(2,M)
*
* U2=U(M-1)+(P-PRES(M-1,K-1))/(PRES(M,K-1)-PRES(M-1,K-1))*(U(M)-
* 1  U(M-1))
*
U2 = U(M-1) + (P-PRES(M-1,K-1)) * UvsP(M,K)
* SU=U1+(RHO(K-1)-RHO(K-1)*RHO(K-2)/SRHO)/(RHO(K-1)-RHO(K-2)) *
* §   (U2-U1)
C   SU=U1+(SRHO-RHO(K-2))/(RHO(K-1)-RHO(K-2))*(U2-U1)
*  SU = U1 + (SRHO-RHO(K-2)) * vdrho(K-1)*(U2-U1)
* 
UP1 = SU - U(I-1)
T1 = TEMP(I-1,J) + TXP(I,J) * UP1
T2 = TEMP(I-1,J+1) + TXP(I,J+1) * UP1
T = T1 + (T2 - T1) * RHOP1
RETURN
END
SUBROUTINE HOTGAS0

* PURPOSE: COMPUTE ENGINE HOT GAS PRESSURE AND FLOW DYNAMICS

***ARGUMENT***
IHCNTL = INITIALIZATION ARGUMENT was eliminated by use of two entries

***COMMON USAGE***

**INPUT:**
VARIABLE
POD3, DWOI, PMOV, POINJ, RHOMOV, RHOOP3, SO2
DWFPPF, DWFOPF, DWFT1, DWFBPF, DWFT2C, SF2, TW1
RFPOV, ROPOV

**OUTPUT:**
VARIABLE
DWOPO, DWFPO, TRQOT2, PCIE
DWOPO, DWFPO, PFPOV, POPOV, PFPOI, POPOI
PCIE
PFPO, POP, PFI, PINMC, TRQFT2, QIN1

**SUBROUTINES CALLED:** IGN

********************************************************************************

LOGICAL FFPTV, FFPVI, FFPTI, FFPOI, FFPOI, FFPTA
LOGICAL OPOIPF, OPOVPF, wtason, wtigon
LOGICAL FOPTV, FOPVI, FOPTI, FOPOI, FOPTA, FOPF, FPIG
INTEGER Tstep
PARAMETER ( NPREO = 11, NFSO = 6, NFSOI = NFSO - 1 )
PARAMETER ( NPREF=11, NFSF=7,
+ NPREF1 = NPREF - 1, NFSF1 = NFSF - 1 )
PARAMETER ( TooBig = 1.E20, Tstep = 0 )

REAL sawop(4), sawfp(4),
+ sdwfp( NPREF1, NFSOI ), vdfs( NPREF1 ),
+ vdfs2( NFSOI )
DIMENSION DWOIG(3), DWFIG(3)
DIMENSION DW2(3), DW1(3), DW3(3)
DIMENSION WFPTAB(4), AFPTAB(4), WOFTAB(4), AOPTAB(4)
DIMENSION FPRO(NPREO), FSOTAB(NFSO), DWOTAB(NPREO, NFSO)
DIMENSION FPROF(NPRE), FSOTABF(NFSF), DWOTABF(NPRE, NFSF)
DIMENSION JSF(2), JSO(2), ZFIG(3), RFIG(3)

INCLUDE 'blank.com'
INCLUDE 'hgas.com'
INCLUDE 'oxid.com'
INCLUDE 'igni.com'

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C
INCLUDE 'balc.com'
INCLUDE 'fuel.com'
INCLUDE 'contrl.com'
INCLUDE 'out.com'
INCLUDE 'units.com'

DATA TINIT / 460.0 /
DATA AFPR1 / 0.0142 /
DATA AFPR2 / 0.04323 /
DATA AFPTAB/ 0.100, 0.0013, 0.0013, 0.0 / SSM26100
DATA AOPTAB/ 0.1513, 0.00166, 0.00166, 0.0 /
DATA AOPRG / 0.0039 /
DATA ASFPC / 0.53899 /
DATA ASOPC / 0.53899 /
DATA PHES / 750.0 /
DATA PRINLO/ 100.0 /
DATA RSES / 50000.0 /
DATA TAUH / 0.01 /
DATA TFPDH / 250.0 /
DATA TOPDH / 250.0 / SSM26200
DATA TPRG / 520.0 /
DATA TPRC / 250.0 /
DATA WFPTAB/ 0.0, 2.2, 3.2, 3.3 /
DATA WOPTAB/ 0.0, 0.8, 2.0, 2.1 /
DATA WTASI / 0.06643 /
DATA WTIGN / 0.0154 /
DATA RHGFM / 0.0340E-4 /
DATA RHGOM / 0.1060E-4 /
DATA ICOFU / 1 /
DATA ICOOX / 1 /
DATA FSFTAB / 0.0, 946.9, 2470., 4117., 5352., 6999., 8192. /
DATA FPRF / 1.0, 1.204, 1.307, 1.411, 1.515, 1.619, 1.7, 1.8, 2.0, 2.4, 3.0 /
DATA FSOTAB / 0.0, 3000., 4000., 5000., 6000., 7000. /
DATA FPRO / 1.0, 1.2, 1.3, 1.4, 1.5, 1.6, 1.7, 1.8, 2.0, 2.4, 3.0 /
DATA DWFTAB/ *
 DATA DWOTAB/ *

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DATA CDWFT2 / 1.0 /
DATA CDWOT2 / 1.0 /

recpos(x) = AMAX1( 0.0, x )
recneg(x) = AMIN1( 0.0, x )
rlimit( floor, ceiling, x ) = AMAX1( floor, AMIN1( ceiling, x ) )

SAVE

***********************************************************************
Precompute slopes for DATA tables
CALL sxset( sawop, 4, WOPTAB, AOPTAB )
CALL sxset( sawfp, 4, WFPTAB, AFPTAB )
CALL xyset( NPREF, FPREF, NFSF, FSF2, DWFTAB, sdwfp, vdfs )
CALL xyset( NPREO, FPRO, NFSO, FSO2, DWOTAB, sdwofp, vdfs2 )

C INITIALIZE LOCAL VARIABLES AND ARRAYS WHICH AREN'T ASSIGNED VALUES
C THIS IS A NECESSARY REQUIREMENT FOR SUCCESSFUL EXECUTION ON THE IBM
C
A=0.0
AFPOI=0.0
AFPTA=0.0
AFPTI=0.0
AFPTV=0.0
AFPVI=0.0
AOPT2=0.0
AREAF=0.0
AR4=0.0
CFACT=0.0
DIAT=0.0
DPOPAS=0.0
DWACV=0.0
DWBADF=0.0
DWFPBI=0.0
DWFPRI=0.0
DWPFI=0.0
DWPFS=0.0
EW=0.0
FDWFT2=0.0
FDWOT2=0.0
FOPTV=.TRUE.
FSF2=0.0
FSO2=0.0
GAM6=0.0
IF1=0.0
IF2=0.0
ISV=0.0

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OPOVPF = .TRUE.
PFPBF = 0.0
RC = 0.0

initializations omitted

WOPTA = 0.0
WOPTI = 0.0
WOPTV = 0.0
WOPVI = 0.0
wtason = .TRUE.
wtigon = .TRUE.
ZFPOI = 0.0

9999 CONTINUE

DATA INPUT

READ (run, 30) ZFPO, VOLFP, ZOPO, VOLOP, AOPTO, VOLOT, VOLFI, VOLC, AR4, AR5, AR6, EMCL, EMC6, EW, DIAT, RC, WOPOV, WFPV, RFPIGB, ROPIGB

FORMAT ('/2X, 6EG12.4')
READ (run, 30) AHTMCF, TKMCF, AHTMCO, TKMCO, VOLMCF, VOLMCO, VOLFTD, VOLOTD
*, RFPVUG, ROPVUG
READ (run, 30) CDWFT2, CDWOT2, DPRNT, PRINLO, PRINHI, PHES

* Added here to eliminate a simulation loop division:

vVOLC = 1.0 / VOLC
ROPO = 0.0
CALL IGN0(1, PFPOV, PFPOI, RH003, P(9), RHO(9), PFP)
CALL IGN0(2, POPOV, POPOI, RH003, P(9), RHO(9), POP)
CALL IGN0(3, PMOV, POINJ, RHOMOV, P(9), RHO(9), PCIE)
WOPOI = 0.0
EMC7 = 1.0
AR7 = 1.0
WFPOI = 0.0
ELFFP = 0.0
CALL fgset(15)
CPH2 = fgen(15, 61, TINIT)
CALL fgset(1)
COOI = FGEN(1, 62, WOPOI)
CALL fgset(2)
CFOI = FGEN(2, 63, WFPOI)
CALL fgset(4)
SC4 = FGEN(4, 64, AR4)
CALL fgset(8)
BC4 = FGEN(8, 65, AR4)
CALL fgset(20)
TFPC = FGEN(20, 66, ELFFP)
CALL fgset(21)
CPFP = FGEN(21, 67, ELFFP)
CALL fgset(13)
GAMFP = FGEN(13, 68, ELFFP)
CALL fgset(12)
EMWFP = FGEN(12, 69, ELFFP/(1.-ELFFP))
CALL fgset(25)
EMUC = FGEN(25, 70, ELFFP)
CALL fgset(23)
EKC = FGEN(23, 71, ELFFP)
CALL fgset(28)
ETAOT2 = FGEN(28, 72, 0.0)
CALL fgset(29)
ETAFT2 = FGEN(29, 73, 0.0)
CALL fgset(41)
CFG = FGEN(41, 74, 0.)
CS=CSTAR(0,0.,0.)

INITIALIZATION

DWFPO=0.0
DWFPOI=0.0
RHOO3=RHOOP3
PFP=PA
WTFP=PFP*VOLFP/9270.0
ELFFPM=0.0
DWFT2=0.0
WFPO=0.0
WFP=WTFP/TINIT
WFPF=WFP
WOPOI=0.0
DWOPO=0.0
DWOPOI=0.0
POP=PA
WTOP=POP*VOLOP/9270.0
WOP = WTOP/TINIT
WOPF=WOP
WOPO=0.0
ELFOP=0.0
ELFOPM=0.0
DWOT2=0.0
TRQOT2=0.0
DWOT1=0.0
POT1=PA
PROT1 = 1.0
PRFT2 = .999
PROT2 = 0.999
WTOT1=POT1*VOLOT1/9270.0
WOT1=WTOT1/TINIT
TOT1=TINIT
TOP=TINIT
TFP=TINIT
TRQOT1=0.0
TOT1D=TINIT
PFI=PA
PFT2D=PFI
POT2D=PFI
WTI = PFI*VOLFI/9270.0
TFI=TINIT
WFI=WTI/TFI
WFIF=WFI
WFIO=0.0
GAMFI=1.4
RGCFI=9270.0
DWC=0.0
SC4 = FGEN(4, 64, AR4)
BC4 = FGEN(8, 65, AR4)
AA2 = EW * .2
A3=0.8-A2
A5 = X10th(DIAT/RC, 1)
PCIE=PA
PCNS=PA
TC=TINIT
WTC=PCIE*VOLC/9270.0
WCO=0.0
WC=WTC/TC
WCF=WC
ELFCM=0.0
ELFC=0.0
GAMC=FGEN(13, 75, ELFCM)
GAM6=FGEN(13, 76, 0.0)
GAM4=GAM6
RGCC=18540.0/FGEN(12, 77, ELFC/(1.-ELFC))
RG6=18540.0/FGEN(12, 78, 0.0)
WOPGN2=0.
WFPGN2=0.
RGN2=0.
RGC4=RGC6
WCN=0.
ENOFC=0.
DWOI=0.0
DWFI=0.0
PFPOV=POD3
PFPOI=PA
POPOV=POD3
POPOI=PA
CFOV=1.0
RHOFTF=RHO(6)
RHOOTF=RHO(6)
PINMC=PA
PFIS=PA
RHOFTF=RHO(6)
PPURG=50.0
DWSFS=0.
DWFTF=0.
DWX=0.
FFPTV = .TRUE.
FFPVI = .TRUE.
FFPTI = .TRUE.
FFPOI = .TRUE.
FFPTA = .TRUE.
FFPOT = .TRUE.
DWFPTV = 0.0
DWFVPVI = 0.0
DWFPSG = 0.0
WFPTV = 0.0576
WFVPVI = 0.5356
WFPTI = 0.00376
WFPOI = 0.0128
WFPTA = 0.0136
ZFPOI = 2.000 E-03
RFPTV = 68.77
RFPOVT = 29.02
RFPOVI = -0.885
RFPTOI = -141.97
RFPTOA = -470.16
POPRG = PA
PFPRG = PA
AFPTV = 4.34 E-03
AFPVT = 6.677E-03
AFPVI = 3.82 E-02
AFPTI = 3.019E-03
AFPOI = 2.62 E-01
AFPTA = 1.659E-03
AFPRS = 1.761 E-02
RHOFTV = RHOOP3
RHOFVI = RHOOP3
RHOFTI = RHOOP3
RHOFOI = RHOOP3
RHOFTA = RHOOP3
CFACT = 400000.
FOPTV = .TRUE.
FOPTI = .TRUE.
FOPOI = .TRUE.
FOPTA = .TRUE.
FOPOT = .TRUE.
DWOPTV = 0.0
DWOVPVI = 0.0
DWOPTI = 0.0
DWOPTA = 0.0
WOPTV = 0.0587
WOPVI = 0.5150
WOPTI = 0.00376
WOPOT = 0.01372
WOPTA = 0.01393
ZOPOI = 2.00E-03
ROPOTV = 110.895
ROPOVT = 46.853
ROPOVI = -1.393
ROPOTI = -100.20
ROPOTA =-781.830
POPOT = 700.0
POPOV = 700.0
AOPTV = 3.420E-03
AOPTA =-781.830
AOPTI = 3.590E-03
AOPTA = 1.290E-03
AOPR1 = 2.553E-03
AOPR2 = 2.502E-03
RHOOTV = RHOOP3
RHOOVI = RHOOP3
RHOOTI = RHOOP3
RHOOII = RHOOP3
RHOOIT = RHOOP3
RHOOTA = RHOOP3
DWXF = 0.

* Initialization moved from simulation loop.

RFLEAK = 1.0 / (772.8 * (FGEN(18, 79, 20.) * ABFFO / 100.) ** 2)
WFPOIZ = FGEN(2, 80, 0.999) + 0.01
RHOFGN = RHOOP3
vTP46 = 1. / (4632. * TPRC)
CALL unint0(DWPO, 95)
CALL unint0(DWPOI, 96)
CALL unint0(WFPOI, 97)
CALL unint0(WFPTV, 98)
CALL unint0(DWFPTV, 99)
CALL unint0(WFPIV, 100)
CALL unint0(DWFPIV, 101)
CALL unint0(WFPTI, 102)
CALL unint0(DWFPTI, 103)
CALL unint0(WFPVT, 104)
CALL unint0(WFPOI, 105)
CALL unint0(DWFPOI, 106)
CALL unint0(WFPTA, 107)
CALL unint0(DWPO(1), 108)
CALL unint0(PFPOV, 109)
CALL unint0(PFPOT, 110)
CALL unint0(PFPPI, 111)
CALL lmint0(WFPF, 112, 0.0, TooBig)
CALL lmint0(WFPO, 113, 0.0, TooBig)
CALL lmint0(WFPT, 114, 0.0, TooBig)
CALL lmint0(DWFIG(1), 115, 0.0, TooBig)

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CALL lmint0( WOPOV, 116, 0.05, TooBig )
CALL unint0( WOPOI, 117 )
CALL lmint0( DWOPO, 118, 0.0, TooBig )
CALL unint0( WTIGN, 119 )
CALL unint0( WTASI, 120 )
CALL unint0( WOPTV, 121 )
CALL lmint0( DWOPTV, 122, 0.0, TooBig )
CALL unint0( WOPVI, 123 )
CALL lmint0( DWOPVI, 124, 0.0, TooBig )
CALL unint0( WOPOI, 128 )
CALL unint0( WOPTI, 125 )
CALL lmint0( DWOPTI, 126, 0.0, TooBig )
CALL unint0( WOPOT, 127 )

dwmax = .002 / DT
CALL unint0( DWOPOI, 129 )
CALL unint0( POPOI, 134 )
CALL unint0( WOPTA, 130 )
CALL lmint0( DWOPTA, 130, 0.0, TooBig )
CALL unint0( POPRG, 131 )
CALL unint0( POPOV, 132 )
CALL unint0( POPOT, 133 )
CALL lmint0( WOPF, 135, 0.0, TooBig )
CALL lmint0( WOPO, 136, 0.0, TooBig )
CALL lmint0( WTOP, 137 )
CALL unint0( TFT2DI, 138 )
CALL lmint0( WTFI, 139, 0.0, TooBig )
CALL lmint0( WFIF, 140, 0.0, TooBig )
CALL lmint0( WFIO, 141, 0.0, TooBig )
CALL lmint0( WTCI, 142, 0.0, TooBig )
CALL lmint0( WCO, 143, 0.0, TooBig )
CALL lmint0( WCF, 144, 0.0, TooBig )
CALL lmint0( WCN, 145, 0.0, TooBig )

* ENTRY HOTGAS

******************************************************************************
C FUEL `PREBURNER INJECTION FLOWS
C
******************************************************************************
C IN THE FOLLOWING, IGOFU IS USED TO INDICATE THE STATE OF THE PREBURNER
C INJECTION FLOWS, THEY ARE:
C IGOFU=1: INITIALIZE
C IGOFU=2: BEFORE THE INJECTOR AND MFV ARE PRIMED
C IGOFU=3: MAIN STAGE, INJECTOR AND MFV ARE PRIMED
C IGOFU=4: MAIN STAGE TO PURGE TRANSITION
C IGOFU=5: FLOW LINES PURGE, POWER CUT
C
C VALVE AND INJECTOR PRIMING IS THE DYNAMIC THAT THE INJECTOR STARTS
C EMPTY AND REQUIRE TO BE FILLED BEFORE FULL INJECTION CAN HAPPEN.
C CFOV IS THE FACTOR OF TRANSFER FOR FPOV
C CFOI IS THE FACTOR OF TRANSFER FOR OXID INJECTOR
C THEY ARE FUNCTIONS OF THE PERCENTAGE OF FILL OF THE EMPTY SPACE.

* The convoluted logic of the restart conditions was commented, for
* the sake of maintenance. Single precision time is good enough for
* state transition tests.

C TRANSIENT CALCULATION SECTION

GO TO (1200, 1240, 1260, 1280, 1320), IGOFU

* Test restart time once ( IGOFU is changed ).

1200 IF ( STIME .GT. 2.5) THEN
  CFOV = 1.0
  WFPOI = WFPOIZ
  CFOI = 1.0
  WFPOV = 0.05
  FPIG = .TRUE.
  * Bypass OPRIME
  IGOFU = 3
  GO TO 1260
ELSE IF ( STIME .LT. 1.5) THEN
  CFOV = 0.025
  * OPRIME until time = 1.5
  IGOFU = 2
END IF

1240 CALL OPRIME(POD3, PFP-DPFPAS, RFPOV, DWFPoi, DWFO)

* RHOFGN = PFPOV / (1159.0 * 200.0) was replaced by
* RHOFGN = PFPOV * 4.314064E-7
* When time reaches 1.5,
* - stop OPRIME, start mainstage
  IF( TIME .LT. 1.5 ) GO TO 1280
  * if 1.5 < restart time < 2.5,
  * do OPRIME once, then start mainstage
  IGOFU = 3
  GO TO 1340

1260 RFPO = (RFPO + RFPOV + RFPOI) / RHOOP3
  DWFO = prflow( DWFO, ZFO, RFPO, POD - PFP + DPFPAS, 95 )
  DWFPoi = prflow( DWFPoi, ZFOI, RFPOI/RHOOP3, PFPOI-PFP+DPFPAS, 96 )

* IF (XFPOV .GT. 20. .OR. PFPOV .GT. PHES) GO TO 1280 , that is
* IF ( XPOV .LE. 20. .AND. PFPOV .LE. PHES ) THEN

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stop integrating DWFPO and DWFPOI

TDWFPO = 0.
IGOFU = 4
END IF

DPFPAS IS THE SUCTION PRESSURE DUE TO BERNOULLI EFFECT OF THE FUEL FLOW INSIDE THE FUEL PREBURNER

• 1280 DPFPAS = ASFPC * (DWFPF / 258.0) ** 2 / (PFP / (9272.0 * T(9)))
• is replaced by
 1280 DPFPAS = ASFPC * DWFPO**2 * T(9) / PFP * 0.1392945

PFPOI = PFP + RFPOI * DWFPO**2 / RHOOP3 - DPFPAS
PFPOV = (POD3 / RFPOV + PFPOI / RFLEAK) * (RFPOV * RFLEAK)

IF (TIME.GT.TCUTPR .AND. PFPRG.LT.100.) PFPRG = AMINI(PHES,PFPOV)
IF (IGOFU .LT. 4) GO TO 1340
IF (TIME .GT. TCUTPR .AND. PFPOI .LT. PHES) THEN
  C  C
  C!!! I CHANGE THE SECOND EQUATION TO THE ONE FOLLOWS. THIS IS THE SITUATI
  C!!! WHEN THE FUEL LINE IS PURGED BY THE HELIUM.
  C
  WFPOI = WFPOI - recneg(DWFPOI) * DT
  WFPOI = pruint( - DWFPOI, Tstep, 97 )
  GO TO 1340
END IF

THIS IS TO PURGE THE OXID CONTENT IN LINE FPTV (BETWEEN PFPOT AND PFPOV)

PFPTV was changed from a real variable, tested for 0.0, to a logical value. Similar logical variables were introduced throughout.
Limiting the integrated value to positive values was an unnecessary operation, and was dropped.

1320 IF ( FFPTV ) THEN
  WFPTV = pruint( - ABS(DWFPTV), Tstep, 98 )
  FFPTV = WFPTV .GT. 0.0
*  DWFPTV = FLOW(DWFPTV, ZFPOI, RFPOTV/RHOOP3, DT, PFPOT - PFPOV)
*  IF (PFPOT .LT. PFPOV)  DWFPTV = 0. - FLOW(DWFPTV,
*  1 ZFPOI, RFPOTV/RHOOP3, DT, PFPOV - PFPOT)
*  RHOFTV = PFPOT / 4632. / TPRC
*  DWFPTV = GFLOW (PFPOT, PFPOV, TPRC, 4632., 1.66) * AFPTV
*  IF (PFPOT .LT. PFPOV)  DWFPTV = 0. - GFLOW (PFPOV, PFPOT, TPRC,
The above sequence was replaced. It does an integration step, then if the wrong sign was used, does it again. The replacement code looks first, then does the integration step once. Also, since the second integration does not depend on RHOFTV, there is no need to test twice. Similar replacements are made below without comment.

IF (PFPOT .LT. PFPOV) THEN
  DWFPTV = 0. - prflow(DWFPTV, ZFPOI, RFPOVT/RHOOP3, PFPOV - PFPOT, 99 )
  DWFPTV = 0. - GFLOW (PFPOV, PFPOT, TPRC, 4632., 1.66) * AFPVT
ELSE
  DWFPTV = prflow( DWFPTV, ZFPOI, RFPOVT/RHOOP3, PFPOT - PFPOV, 99 )
  DWFPTV = GFLOW (PFPOV, PFPOT, TPRC, 4632., 1.66) * AFPVT
END IF

RHOFTV = PFPOT * vTP46
END IF

THIS IS TO PURGE THE OXID CONTENT IN LINE FPVI (BETWEEN PFPOI AND PFPOV)

IF ( FFPVI ) THEN
  WFPVI = pruint( - DWFPVI, Tstep, 100 )
  FFPVI = WFPVI .GT. 0.0
  DWFPVI = prflow( DWFPVI, ZFPOI, RFPOVI/RHOOP3, PFPOV - PFPOI, 101 )
ELSE
  RHOFVI = PFPOV * vTP46
  WFPVI = GFLOW (PFPOV, PFPOI, TPRC, 4632., 1.66) * AFPVI
END IF

THIS IS TO PURGE THE OXID CONTENT IN LINE FPTI (BETWEEN PFPOT AND PFPOI)

IF ( FFPTI .OR. "FFPOT ) THEN
  IF ( .NOT. FFPOT ) WFPTI = pruint( - DWFPTI, Tstep, 102 )
  FFPITI = WFPTI .GT. 0.0
  DWFPTI = prflow(DWFPTI, ZFPOI, RFPOTI/RHOOP3, PFPOT - PFPOI, 103 )
ELSE
  RHOFITI = PFPOT * vTP46
  DWFPTI = GFLOW (PFPOT, PFPOI, TPRC, 4632., 1.66) * AFPTI
END IF

IF ( FFPOT ) THEN
  WFPOT = pruint( - (DWFPTV + DWFPTI+ DWOIG(1) ), Tstep, 104 )
  FFPOT = WFPOT .GT. 0.0
END IF

IF ( FFPOI ) THEN
WFPOI = pruint( - DWFPPOI, Tstep, 105 )
FFPOI = WFPOI .GT. 0.0
DFPOI = DWFPPOI

DFPOI = prflow( DWFPPOI, ZFPPOI, -RFPOI/RHOOP3, PPFOI-PFP+DPFPAS, 106 )

DFPOI = WDPOI - AMIN1(WDPOI - DWFPPOI, 0.002)
IF (DFPOI.GT.WDPOI)
   DFPOI = WDFPOI - AMINI(WDFPOI - DWFPOI, 0.002)
ELSE
   DWFPOI = 0.0
   DWPFI = GFLOW(PFPOI, PFP - DPFPAS, TFPDH, 4632., 1.66) * AREF
END IF

IF (DFPTA .OR. FFPOT ) THEN
   IF (.NOT. FFPOT ) WFPTA = pruint( - DWOIG1, Tstep, 107 )
   FFPTA = WFPTA .GT. 0.0
   DWOIG1 = prflow(DWOIG1, ZFPPOI, RFPOTA / RHOOP3, PFPOT - PFP, 108 )
   ELSE
      RHOFTA = PFPOT * vTP46
      DWOIG1 = GFLOW(PFPOT, PFP, TPRC, 4632., 1.66) * AFPTA
   END IF

DPFPAS = ASFPC * DWFPF**2 * T(9) / PFP / 0.1392945
DPFPAS = ASFPC * (DPFPF / 258.) **2 / (PFP / 9272 / T(9))
DWFPRI = recpos( GFLOW(PHES, PFPOV, TPRG, 4632.0, 1.66) * AFPR1 )
PFPOV = pruint( + DWFPRI + CFAC * ( DWFPTV/ RHOFTV - DWFPVI / RHOFTV ) * + PFPOV * vTP46, Tstep, 109 )
PFPRG = PFPOV + .9422 * 4632 * TPRG / PFPOV * DWFPRI ** 2
PFPRG = PFPOV + 4364.3 * TPRG / PFPOV * DWFPRI ** 2
PFPRG = recpos( GFLOW(POPRG, PFPOV, TPRG, 4632.0, 1.66) * AFPR2 )
PFPOV = pruint( CFAC * ( DWFP2 - + ( DWOIG1/RHOFTA + DWFPTI/RHOFTI + DWFPV/RHOFTI ) * + PFPOV * vTP46 ) ), Tstep, 110 )
PFPOI = pruint( CFAC * ( + ( DWFPTI / RHOFTI + DWFPV / RHOFTI - DWFPOI / RHOFOI ) * + ( PFPOI * vTP46 ) - DWFI ) , Tstep, 111 )

END OF PURGE PROCESS

FUEL PREBURNER COMBUSTION
1340 CONTINUE

IN THE FOLLOWING:

DWFPF: FUEL PREBURNER FUEL FLOW
DWFPBI: FUEL PREBURNER TOTAL INLET FLOW
WPF: FUEL PREBURNER TOTAL FUEL
WPPO: FUEL PREBURNER TOTAL OXIDIZER
ELFFPM: FUEL PREBURNER OXIDIZER FRACTION
ELFFP: FUEL PREBURNER OXIDIZER FLOW FRACTION
FPIG: IGNITOR INDICATOR, = .TRUE. FOR FUEL PREBURNER IGNITED
TFPC: FUEL PREBURNER COMBUSTION TEMPERATURE
CPPF: SPECIFIC HEAT INSIDE FUEL PREBURNER
GAMFP: RATIO OF SPECIFIC HEAT (GAMMA) OF FUEL PREBURNER
EMWFP: MOLECULAR WEIGHT IN FUEL PREBURNER
RGCFP: GAS CONSTANT IN FUEL PREBURNER (PSI-IN**3/LB)
TFP: FUEL PREBURNER TEMPERATURE
PFP: FUEL PREBURNER PRESSURE
WFP: FUEL PREBURNER TOTAL MASS
WTFP: WEIGHT TIMES TEMPERATURE WITHIN FUEL PREBURNER

DWFPFA = recpos( DWFPF )
posdwo = recpos( DWOIG(1) )
DWFPBI = DWFPFA + DWFPFI + DWFIG(1) + posdwo

DURING THE PURGE FPOI = .FALSE.

IF ( .NOT. FPOI ) DWFPBI = DWFPFA + DWFPFI + DWFIG(1) + posdwo

* WPF = AMAX1(0.0, WFPF + (DWFPFA + DWFIG(1) - (1.0 - ELFFPM) * DWFT2) * DT)
* WFP = PRINT(DWFPFA + DWFIG(1) - (1.0 - ELFFPM) * DWFT2, 0, 112)
ELFFPM = WPFO / (WPFP + WFPF + 0.1E-6)
ELFFP = ( DWPOI + posdwo ) / ( DWPOI + DWFPFA + DWFIG(1) + posdwo + 0.1E-06 )

IF ( .NOT. FPIG ) THEN
TFPC = T(9) + 20.
IF ( ELFFP .GE. 0.20 AND. STIME .GT. 0.3 ) THEN
FPIG = .TRUE.
WRITE(6,*)' FPB IGN AT', TIME
END IF
ELSE
TFPC = (1.0927E-05 * PFP + 0.91985) * FGEN(20, 66, ELFFP) + T(9)
END IF
CPPF = FGEN(21, 81, ELFFPM)

SPECIAL CONSIDERATION FOR SMALL O/F RATIO

IF (ELFFPM .GT. 0.1) A = recpos(1.0 - 10.0*ELFFPM)
GAMFP = A * H2GAMA(PFP, TFP, 1, 2) + (1.0 - A) * FGEN(13, 68, ELFFPM)
CPH2 = FGEN(15, 61, TFP) - 0.0887 + PFP * (0.1241 - 3.732E-5 * PFP) / 
+ (AMAX1(50., TFP) - 50.)
CPFP = A * CPH2 + (1.0 - A) * CPFP
GO TO 1380
1360 GAMFP = FGEN(13, 68, ELFFPM)
1380 CONTINUE
EMWFP = FGEN(12, 69, ELFFPM/(1. - ELFFPM))
RGCFP = 18540.0 / EMWFP
TFP = AMAX1(10.0, WTFP / (WFP + 1.0E-12))
PFP = RGCFP * WTFP / VOLFP
PFP = AMAX1(0.01, PFP)
WTFP = prlinit(GAMFP*(DWFPBI*TFC - DWFT2*TFP), 0, 114)

FUEL PREBURNER IGNITOR

PFPBFB = P(9) - RFPIGB / RHO(9) * DWPF**2
IF (IGOFU .EQ. 5) THEN
  DWFIG(1) = + prlflow(DWFIG(1), ZFIG(1), RFIG(1) / RHO(9), PFPBFB - PFP, 115)
ELSE
  CALL IGN(1, PFPOV, PFPOI, RHOFGN, PFPBFB, RHO(9), PFP, 2)
  PFPOT = P4(1)
  POPOT = P4(2)
  DWFTV = -DW2(1)
  DWFTI = DW2(1)
END IF

HIGH PRESSURE FUEL TURBINE PERFORMANCE

TURBINE FLOW EFFICIENCY FDWFT2 IS THE FUNCTION OF EFFECTIVE PRESSURE RATIO (PREFT2) AND NORMALIZED TURBINE SPEED (FSFT2). A LOOK-UP TABLE IS GIVEN AS DWFTAB WITH FPRF ARRAY AS X-AXIS AND FSFTAB ARRAY AS Y-AXIS. THE ACTUAL EQUATIONS USED FOR SIMULATION IS NOT IN THE DOCUMENT RL00001.

GAMPI = GAMFP + 1.
GAMMI = GAMFP - 1.
PRFT2 = AMAX1(1.0, PFP/PFT2D)

X ** Y may require evaluation of a slowly converging series for the logarithm of X, and another series for the exponentiation, after the multiplication by Y. Replacement routines involving two-way linear interpolation in a table of equal intervals were defined.

PREFT2 = (1. - .166667 * GAMPI/GAMMI * 
+ (1. - PRFT2**(-GAMMI/GAMFP))**(-3.5)
** preft2 = 1.0 - .166667 * gampl/
+ (1.0 - 1.0 / xtoy( prft2, gamm1/gamfp ))
preft2 = 1.0 / ( preft2 ** 3 * x10th(preft2, 5 ) )

** tcrft2 = ( gamfp/gampl * rgcfp * tfp * 5.15917e-6 )
(2.32.174/12.1019.5**2)

** The square root is taken immediately, since it is used more than
once. Since the x ** y interpolation routines use a table of
x ** (.1 * n ) values, the square root can be obtained faster
as x ** .5, than by the square root function.

** tcsqrt = x10th( tcrft2 )

** fsf2 = sf2 / tcsqrt * 9.5493
(60./2*pi)

** fdwft2=tablxy(npref,if1,preft2,fprf,nfsf,if2,fsf2,fsftab,dwftab)
** was replaced by an interpolation using precomputed slopes.

** fdwft2 = xylint( preft2, fsf2, npref, fprf, nfsf, fsf2, 
+ sdwfp, vdfs fsftab, dwftab, if1, if2 )

** A table of epsf vs gamfp is needed here. It would be used for
epsf vs gamop as well.

** epsf = .739594/gamfp*(2./gampl)**(-gamfp/gamml)
epsf = .739594 / ( gamfp * xtoy( 2./gampl, gamfp/gamml ) )
dwft2 = fdwft2*cdwft2*pfp/(14.7*tcsqrt*epsf)
if (stime.lt.0.1) then
   treqft2=0.0
else
   treqft2=trbtrq(sf2,ucft2,tfp,pfp,1./prft2,2,cpfp,dwft2,gamfp)
end

*ctqft2

end
if( dwft2.le.0) then
   tft2d = tfp
else
   tft2d=tfp-rlimit( 0.0, 300.0, (treqft2 * sf2)/ 
+ (9340.0*cpfp*dwft2 + 1.0e-6) )
endif
hpfi = 0.5 * pfi
pft2d = hpfi + sqrt( hpfi**2 + rhglm*rgcfp*tft2d*dwft2**2)

*** Oxid PreBurner Injection Flows

* IN THE FOLLOWING, IGOFU IS USED TO INDICATE THE STATE OF THE PREBURNER
* INJECTION FLOWS, THEY ARE:
**INITIALIZATION**

**BEFORE THE INJECTOR AND MOV ARE PRIMED**

**MAIN STAGE, INJECTOR AND MOV ARE PRIMED**

**MAIN STAGE TO PURGE TRANSITION**

**FLOW LINES PURGE, POWER CUT**

Valve and injector priming is the dynamic that the injector starts empty and requires to be filled before full injection can happen.

COOV is the factor of transfer for OPOV. COOI is the factor of transfer for oxidizer injector. They are functions of the percentage of fill of the empty space.

**************************************************************************

```fortran
IF (WTIGN .GT. 0.0)  RHOIGN = RHOOP3
GO TO (1500, 1540, 1560, 1580, 1680), IGOOX

1500 ROLEAK = 1.0
*/ (772.8 * (FGEN(17, 82, 20.) * ABOPO / 100.) ** 2)
WOPOIZ = FGEN(1, 83, 0.999) + 0.01
IF (STIME .GT. 2.5) GO TO 1520
COOV = 0.025
IGOOX = 2
GO TO 1540 SSM32900

1520 COOV = 1.0
WOPOI = WOPOIZ
COOI = 1.0
WOPOV = 0.05
IGOOX = 3
GO TO 1560 SSM33000

* * * PRIME OPB OXIDIZER INJECTOR * *

*1540 WOPOV = AMIN1 (0.05, WOPOV + (1.0 - COOV) * DWOPD * DT)
*
1540 WOPOV = praint( (1.0 - COOV) * DWOPD, Tstep, 116 )
CALL praint( WOPOI, DWOPD * COOI - DWOPD, Tstep, 117 ) SSM33000

C IF (WOPOV .GT. 0.0)  COOV = 1.0
C
IF( OPOVPF .AND. WOPOV.GT.-0.05) THEN
COOV = 1. + WOPOV * 20.
IF(WOPOV.GT.-0.001) THEN
PRINT *, ' OPOV BUBBLE PRIMED AT', TIME
OPOVPF = .FALSE.
COOV=1.
END IF
END IF SSM33100

C IF( OPOIPF .AND. WOPOI.GT.1.75) THEN
PRINT *, ' OPB INJECTOR PRIMED AT', TIME
OPOIPF = .FALSE.
END IF

C
```

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ROPO = (ROPOL + ROPOV * COOV + ROPOI * COOI * COOV) / RHOOP3
DWOPO = prFlow( DWOPO, ZOPO, ROPO, POD3 - POP + DPOPAS, 118 )
DWOPOI = COOI * COOV * DWOPO
RHOIGN = POPOV / (1159.0 * 200.0)
RHOIGN = PPPOV * 4.314064E-7

IF (WOPOI .LT. WOPOIZ) GO TO 1580
WOPOI = WOPOIZ
IGOOX = 3

C * * * MAINSTAGE CALCULATIONS

C 1560 ROPO = (ROPOL + ROPOV + ROPOI) / RHOOP3
IF (ROPOV .LT. 1.0E+10) THEN
DWOPO = prFlow( DWOPO, ZOPO, ROPO, POD3 - POP + DPOPAS, 118 )
DWOPOI = DWOPO
ELSE
DWOPO = 0.0
DWOPOI = 0.0
IGOOX = 4
END IF

*1580 DPOPAS = ASOPC * (DWOPF / 120.)**2 / (POP / (9272. * T(9)))
1580 DPOPAS = ASOPC * (DWOPF**2 * T(9) / POP * 0.1392945

POPOI = POP + ROPOI * DWOPOI**2 / RHOOP3 - DPOPAS
POPOV = (POD3 / ROPOV + POPOI / ROLEAK) * (ROPOV * ROLEAK)
1 / (ROPOV + ROLEAK)
IF (IGOOX .LT. 4) GO TO 1800

C * * * COMPUTE OPB ASPIRATION BACKFLOW

C

DWOPOI = recpos( -DWOIG(2) * RHOOP3 / RHOIGN )
WOPOI = pruint( DWOIG(2), Tstep, 117 )

* Changed next two tests to be independent of DT and consistent with
* previous approach.

* IF (wtigon ) THEN
  WTIGN = pruint( DWOIG(2), Tstep, 119 )
  IF ( WTIGN .GT. 0.0) THEN
    WRITE (init, 1590) STIME
  1590 FORMAT (IH0, 10X,
    + '* * * * BACKFLOW REACHED ORIFICE BLOCK AT TIME = ',',
    + F8.3, ' SECONDS * * * * ')
  wtigon = .FALSE.
  GO TO 1640
  END IF
END IF

1600 RHOIGN = PCIG(2) / (9272.016 * T(9))
IF( wtason ) THEN
WTASI = pruint( DW1(2) * RHOOP3 / RHOIGN, Tstep, 120 )
IF (WTASI .LT. 0.0) THEN

179
WRITE (6, 1610) TIME
1610 FORMAT (1H0, 10X,
+ ' * * * * BACKFLOW REACHED OPOV AT TIME = ',
+ F8.3, ' SECONDS * * * * ')
     wtason = .FALSE.
     ENDF
     ENDF
1640 IF (TIME .LT. TCUTPR) GO TO 1800
     POPRG = AMINI (PHES, POP)
     IF (POPOI .GT. PHES) GO TO 1800
     IGOOX = 5
C
C
C
C
C
C
C
****** COMPUTE PURGE FLOW AND PRESSURE
C
C
C
C
C
C
C
OXIDIZER PREBURNER OXIDIZER LINES HAVE THE SAME SET UP AS THOSE OF
C
C
C
C
C
FUEL PREBURNER. SAME PURGE SEQUENCE APPLIED.
C
C
* The code was restored to read like 1320 above, where a logical
* variable shuts off the integration when its state change function
* is completed.
*
1680 IF ( FOPTV ) THEN
     WOPTV = pruint( - ABS(DWOPTV), Tstep, 121)
     FOPTV = WOPTV .GT. 0.
     IF (POPOT .LT. POPOV) THEN
          DWOPTV = 0. - prflow (DWOPTV, ZOPOI, ROPOTV / RHOOP3,
          POPOV - POPOT, 122)
     ELSE
          DWOPTV = prflow(DWOPTV, ZOPOI, ROPOTV/RHOOP3,
          POPOT - POPOV, 122)
     ENDIF
     ELSE
          RHOOPTV = POPOT * vTP46
          IF (POPOT .LT. POPOV) THEN
               DWOPTV = 0. -
               GFLOW (POPOV, POPOT, TPRC, 4632., 1.66) * AOPVT
          ELSE
               DWOPTV = GFLOW (POPOV, POPOV, TPRC, 4632., 1.66) * AOPTV
          ENDIF
     ENDIF
     IF ( FOPVI ) THEN
     WOPVI = pruint( - DWOPVI, Tstep, 123)
     FOPVI = WOPVI .GT. 0.0
     IF ( FOPVI ) THEN
          DWOPVI =
          prflow( DWOPVI, ZOPOI, ROPOVI/RHOOP3, POPOV - POPOI, 124)
     ELSE
          RHOOVI = POPOV * vTP46
          DWOPVI = GFLOW(POPOV, POPOI, TPRC, 4632., 1.66) * AOPVI
     ENDIF
SSM33600
ENDIF
IF ( FOPTI ) THEN
  WOPTI = pruint( DWOPTI, Tstep, 125 )
  FOPTI = WOPTI .GT. 0.0
ENDIF
IF ( FOPTI .OR. FOPOT ) THEN
  DWOPTI = prflow(DWOPTI, ZOPOI, ROPOTI/RHOOP3, POPOT - POPOI, 126 )
ELSE
  RHOOOI = POPOI * vTP46
  DWOPTI = GFLOW(POPOI, POPOI, TPRC, 4632., 1.66) * AOPTI
ENDIF
ENDIF
1730 IF ( FOPOT ) THEN
  WOPOT = pruint( -(DWOPTV + DWOPTI+ DWOPTA), Tstep, 127 )
  FOPOT = WOPOT .GT. 0.0
ENDIF
IF ( POPOI ) THEN
  WOPOI = pruint( - DWOPOI, Tstep, 128 )
  FOPOI = WOPOI .GT. 0.0
ENDIF

* Limit integration increase or decrease to .002, obscurely.

* WDOPOI = DWOPPOI
* DWOPOI = FLOW(DWOPPOI, ZOPOI, ROPOI/RHOOP3,DT, POPOI-POP+DPOAS)
* DWOPOI = DWOPPOI - AMIN1 (DWOPPOI - DWOPPOI, 0.002)
* IF (DWOPPOI.GT.DWOPPOI ) DWOPPOI=DWOPPOI +AMIN1(DWOPPOI-DWOPPOI ,.002)
* Now modelled as an unlimited integration of a limited flow rate.

  dwrate = rlimit( -dwmax, dwmax,
          + POPOI - POP + DPOAS - ROPOI/RHOOP3*DWOPPOI**2/ZOPOI )
  DWOPOI = pruint( dwrate, Tstep, 129 )

  AREAO = xlint( WOPOI, ISO, WOPTAB, AOPTAB, sawop, 4)
  DWPOI = GFLOW (POPOI, POP - DPOAS, TOPDH, 4632., 1.66) * AREAO
ELSE
  RHOOOI = POPOI * vTP46
  DWOPOI = GFLOW(POPOI, POP - DPOAS, TPRC, 4632., 1.66) * AREAO
END IF
IF ( FOPTA ) THEN
  WOPTA = pruint( - DWOPTA, Tstep, 130 )
  FOPTA = WOPTA .GT. 0.0
ENDIF
IF ( FOPTA ) THEN
  DWOPTA = prflow( DWOPTA, ZOPOI, ROPOTA / RHOOP3, POPOT - POP, 130 )
ELSE
  RHOOOTA = POPOT * vTP46
  DWOPTA = GFLOW (POPOT, POP, TPRC, 4632., 1.66) * AOPTA
ENDIF
ENDIF
181
DPOPAS = ASOPC * DWOPF**2 / POP * T(9) * 0.1392945

DWFPSG = GFLOW(PHES, POPRG, TPRG, 4632.0, 1.66) * AFPRS

POPRG = pruint(
         + 48849. * ( DWFPSG - DWFPR2 - DWOPR - DWOPR2),
         + Tstep, 131 )

POPRG = AMINI( PHES - .01, POPRG )

DWOPR = GFLOW( POPRG, POPOV, TPRG, 4632.0, 1.66) * AOPR1

POPOV = pruint( CFACT * ( DWOPR +
                    + (DWOPTV/RHOOTV - DWOPVI/RHOOVI) * POPOV * vTP46, Tstep, 132 )

DWOPR2 = GFLOW( POPRG, POPOT, TPRG, 4632.0, 1.66) * AOPR2

POPOP = pruint( CFACT * (DWOPR2 -
                     + (DWOPTA/RHOTA + DWOPTI/RHOITI + DWOPTV/RHOUTV) *
                     + (POPOP * vTP46), Tstep, 133 )

POPOI = pruint( CFACT * ((DWOPTI / RHOOITI + DWOPVI / RHOOVI +
                          - DWPOI / RHOOOI) * (POPOI * vTP46 - DWPOI), Tstep, 134 )

END OF OXIDIZER PREBURNER PURGE

1800 CONTINUE

OXID PREBURNER IGNITOR

POPBFB = P(9) - ROPIGB / RHO(9) * DWOPF**2

CALL IGN (2, POPOV, POPOI, RHOIGN, POPBFB, RHO(9), POP)

OXID PREBURNER COMBUSTOR

IN THE FOLLOWING:

DWOPF: OXID PREBURNER FUEL FLOW
WOPF: OXID PREBURNER TOTAL FUEL
WOPO: OXID PREBURNER TOTAL OXIDIZER
ELFOPM: OXID PREBURNER OXIDIZER FRACTION
ELFOP: OXID PREBURNER OXIDIZER FLOW FRACTION
TOPC: OXID PREBURNER COMBUSTION TEMPERATURE
CPOP: SPECIFIC HEAT INSIDE OXID PREBURNER
GAMOP: RATIO OF SPECIFIC HEAT (GAMMA) OF OXID PREBURNER
EMWOP: MOLECULAR WEIGHT IN OXID PREBURNER
RGCOP: GAS CONSTANT IN OXID PREBURNER (PSI-IN**3/LB)
TOP: OXID PREBURNER TEMPERATURE
POP: OXID PREBURNER PRESSURE
WOP: OXID PREBURNER TOTAL MASS
WTOP: WEIGHT TIMES TEMPERATURE WITHIN OXID PREBURNER

DWOPFA = recpos(DWOPF)
WOPF = prlins( DWOPFA + DWFIG(2) - (1.0 - ELFOPM) * DWOT2,
               + 0, 135 )

posig = recpos( DWOIG(2) )
WPO = prlins( DWPOI + posig - ELFOPM*DWOT2, 0, 136 )

ELFOPM = WPO / (WPO + WOPF + 1.0E-6)

ELFOP = ( DWPOI + posig ) /
        + (DWPOI + DWOPFA + DWFIG(2) + posig + 1.0E-06)

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TOPC = FGEN(20, 66, ELFOP) + T(9)
CPOP = FGEN(21, 67, ELFOPM)

SPECIAL CONSIDERATION WHEN O/F RATIO IS REALLY SMALL

IF (ELFOPM.LE.0.1) THEN
  A = recipos(1.0 - 10.*ELFOPM)
  GAMOP = A * H2GAMA(POP, TOP, 2, 2) +
         (1.0 - A) * FGEN(13, 68, ELFOPM)
  CPH2 = FGEN(15, 61, TOP) - 0.0887 +
         POP * (0.1241 - 3.732E-5 * POP) / (AMAX1(51., TOP) - 50.)
  CPOP = A * CPH2 + (1.0 - A) * CPOP
ELSE
  GAMOP = FGEN(13, 68, ELFOPM)
ENDIF

EMWOP = FGEN(12, 69, ELFOPM/(1. - ELFOPM))
RGCOP = 18540.0 / EMWOP
TOP = AMAX1(10.0, WTOP/(WOP + 1.0E-12))
POP = RGCOP*WTOP/VOLOP
POP = AMAX1(0.01, POP)
WTOP = print( GAMOP *
          (recpos(DWOPFA) + DWOP1 + DWFIG(2) + posig)*TOPC
          - DWOT2*TOP, 0, 137)

HIGH PRESSURE OXIDIZER TURBINE

TURBINE FLOW EFFICIENCY FDWOT2 IS THE FUNCTION OF EFFECTIVE PRESSURE RATIO (PREOT2) AND NORMALIZED TURBINE SPEED (FSO2). A LOOK-UP TABLE IS GIVEN AS DWOTAB WITH FPRO ARRAY AS X-AXIS AND FSOTAB ARRAY AS Y-AXIS. THE ACTUAL EQUATIONS USED FOR SIMULATION IS NOT IN THE DOCUMENT RL00001.

GAMPI = GAMOP + I.
GAMM1 = GAMOP - I.
PROT2 = AMAX1 (1.0, POP/POT2D)
tmp = 1.0 - 1.66667 * GAMPI / GAMM1 +
      (1.0 - XtoN(Y( PROT2, -GAMM1/GAMOP))
PREOT2 = 1.0 / (X10th(tmp, 5) * tmp**3)
TCROT2 = GAMOP/GAMPI * RGCOP * TOP * 5.15917E-6
tcsqrt = X10th(TCROT2, 5)
FSO2 = SO2 / tcsqrt * 9.54927
FDWOT2 = xylint( PREOT2, NPREO, FPRO, NFSO, FSO2, +
                 sdwofp, vsfo2, FSOTAB, DWOTAB, IO1, IO2)
EPSO = .739594 / GAMAP * XtoY(.5 * GAMPI, GAMAP/GAMM1)
DWOT2 = FDWOT2 * CDWOT2 * POP/(14.7 * tcsqrt(TCROT2) * EPSO)
TRQOT2 = TRBTRQ(SO2, UCOT2, TOP, POP, 1./PROT2, 4., CPOP, DWOT2, GAMOP)
1 * CTQOT2
IF (DWOT2.LE.0.0) THEN
TOT2D = TOP
ELSE
    TOT2D = TOP - rlimit( 0.0, 300.0,
        + TRQOT2 * SO2 / ( 9340.0 * CPOP * DWOT2 + 1.0E-6 ) )
ENDIF

POT2D = hpfi + X10th( hpfi**2 + RHGOM*RGCOP*TOT2D*DWOT2**2, 5 )

HOTGAS MANIFOLD COOLING

Since the fuel flow out of the LPFT passes the outside of the hotgas manifold before entering the fuel injector, the heat exchange of these two flows has to be accounted for.

QOTMC: Heat flow from the outlet of Oxid Preburner
TOTMC: Temperature of fuel line at OP side
QFTMC: Heat flow from the outlet of fuel preburner
TFTMC: Temperature of fuel line at FP side
TFT2DI: Temperature of hot gas at injector end, FP side
TOT2DI: Temperature of hot gas at injector end, OP side
RHOFTF: Fuel density of fuel line at FP side
RHOOTF: Fuel density of fuel line at OP side
PFIS: FIS (Fuel injector supply) is the point before FI which also supply fuel direct to combustion chamber

IF ( DWFT1.LE.0..OR.DWOT2.LE.0. ) THEN
    QOTMC=0.
ELSE
    QOTMC = TKMCO*AHTMCO*(TOT2D - TFT1D)
ENDIF

Not an integration step:

TOTMC = TFT1D + QOTMC/(2.435*RHOOTF*VOLMCO)*DT

IF(DWFT1.LE.0..OR.DWFT2.LE.0.) THEN
    QFTMC=0.
ELSE
    QFTMC = TKMCF*AHTMCF*(TFT2D - TFT1D)
ENDIF

Not an integration step:

TFTMC = TFT1D + QFTMC/(2.435*RHOFTF*VOLMCF)*DT

TFT2DI = pruint( - QFTMC*RGCFP*TFT2D/(CPFP*PFT2D*VOLFTD),
    + Tstep, 138 )

Not an integration step:

TOT2DI = TOT2D - QOTMC*RGCOP*TOT2D/(CPOP*POT2D*VOLOTD)*DT
RHOUTF = rlimit(4.0E-03, 1.0E-06, PFIS/(TOTMC*9201.6) )
RHOFIT = rlimit(4.0E-03, 1.0E-06, PFIS/(TFTMC*9201.6) )
PINMC=PFI+RSFS*ABS(DWSFS)*DWSFS/RHOFI+RFMCF*ABS(DWFTF)*DWFTF/ * RHOFIT

DWFT1 SEPARATED INTO DWFTF AND DWOTF AND THEY MERGE AGAIN AT NODE FI
FOR A GIVEN PRESSURE DROP DP, THE STEADY FLOW EQUATION IS:
DP = (RI/RHOI)*(DWI)**2

DWFTF = DWFT1 / (1.0 + X10th(RFMCF*RHOUTF/(RFMCO*RHOFIT), 5 ) )
DWOTF = DWFT1 - DWFTF
IF(DWFT1.LE.0.) THEN
  TFIS = (TOTMC+TFTMC)*.5
  RHOFI = RHO(6)
ELSE
  TFIS = (DWOTF*TOTMC + DWFTF*TFTMC)/DWFT1
  RHOFI = (DWFTF + DWOTF)/(DWFTF/RHOFIT + DWOTF/RHOUTF)
ENDIF
PFIS = PINMC - RFMCF*DWFTF*ABS(DWFTF)/RHOFIT

DEMON = TOTAL_FLOW / SQRT(RHO) IN STEADY STATE

DEMON = X10th( ABS(PFIS - PFI) / RSFS, 5 ) +
+ X10th( ABS(PFIS - PCIE), 5 ) *
+ ( 1./X10th(RACV, 5) + 1./X10th(RBAF, 5) + 1./X10th(RPFS, 5) )
IF(DEMON.EQ.0.0) THEN
  DWSFS=0.0
  DWACV=0.0
  DWBAF=0.0
  DWPSFS=0.0
ELSE
  DWSFS = DWFT1 * X10th(ABS(PFIS-PFI)/RSFS, 5) / DEMON
  DWACV = DWFT1 * X10th(ABS(PFIS-PCIE)/RACV, 5) / DEMON
  DWBAF = DWFT1 * X10th(ABS(PFIS-PCIE)/RBAF, 5) / DEMON
  DWPSFS = DWFT1 * X10th(ABS(PFIS-PCIE)/RPFS, 5) / DEMON
ENDIF

DPHGMF=PFIS-PFT_D
DPHGMO=PFIS-POT2D

MAIN CHAMBER FUEL (HOT GAS) INJECTOR

FUEL INJECTOR INPUTS ARE:
  DWFT2: OUTPUT FROM FP THROUGH FP TURBINE
  DWOT2: OUTPUT FROM OP THROUGH OP TURBINE
  DWSFS: FROM NODE FIS
  DWFT2C: FT2 COOLING WHEN DP >=185 PSI
  DWFBPV: BLEEDING VALVE FROM NOZZLE COOLING FLOW (NOT USED)

FUEL INJECTOR OUTPUTS ARE:
  DWFI: EXIT TO MAIN COMBUSTION CHAMBER
WTFI = prlint( GAMFI * 
+ ( DWFT2*TFT2DI + DWOT2*TOT2DI + DWSFS*TFIS + DWFBPV*T(4) + 
+ DWFT2C*T(3) - DWFI*TFI ), 0, 139 ) 
WFIF = prlint( DWFBPV + DWSFS + DWOT2*(1.0 - ELFOPM) + 
+ DWFT2*(1.0 - ELFFPM) + DWFT2C - DWFI*(1.0 - ELFFI) ), 0, 140 ) 
WFIO = prlint( DWOT2*ELFOPM + DWFT2*ELFFPM - DWFI*ELFFI, 0, 141 )

* WFI = WFIO + WFIF
TFI = AMAXI(10.0, WTFI/(WFI + 1.0E-12) )
PFI = RGCFI*WTFI/VOLFI
PFI=AMAXI(PA,PFI)
IF(DWFT2.LE.0..AND.DWOT2.LE.0.) THEN
  GAMFI = GAM6
  RGCFI=RGC6
ELSE
  GAMFI=(GAMOP*DWOT2 + GAM6*DWSFS+(DWFBPV+DWFT2C)*GAM4+
1 DWFT2*GAMFP)/(DWOT2+DWSFS+DWFT2+DWFBPV+DWFT2C+1.0E-06)
  GAMFI = rlimit(1.01, 10.0, GAMFI)
  RGCFI=(RGCOP*DWOT2+RGC6*DWSFS+RGCFP*DWFT2+RGC4*(DWFBPV+
+DWFT2C))/(DWOT2+DWSFS+DWFT2+DWFBPV+DWFT2C+1.0E-6)
  RGCFI = rlimit(100.0, 20000.0, RGCFI)
ENDIF
DWFIX = GFLOW(PFI,PCIE,TFI,RGCFI,GAMFI)*AFI
DWFIR= DWFI + 0.05*(DWFIX - DWFI)
DWFIR = recpos( DWFI )
ELFFI = WFIO/(WFI + 1.0E-6)

MAIN CHAMBER IGNITOR

CALL IGN(3,PMOV,POINJ,RHOMOV, P(10),RHO(10),PCIE)

MAIN CHAMBER COMBUSTOR

IN THE MAIN COMBUSTION CHAMBER, FOLLOWING NOTATION ARE USED:
ELFC:  OXID FLOW / TOTAL FLOW IN COMBUSTION CHAMBER
ELFCM: OXID / TOTAL MASS IN COMBUSTION CHAMBER
TCC:  COMBUSTION TEMPERATURE IN THE CHAMBER
GAMC: GAMMA IN COMBUSTION CHAMBER
WTC:  WEIGHT TIME TEMPERATURE IN COMBUSTION CHAMBER
WCO:  OXID WEIGHT IN COMBUSTION CHAMBER
WCF:  FUEL WEIGHT IN COMBUSTION CHAMBER
WCN:  NITROGEN WEIGHT IN COMBUSTION CHAMBER
DWC:  EXIT FLOW OF COMBUSTION CHAMBER
DWGN2:  NITROGEN PURGE DURING SHUT DOWN (NOT USED)
TC:  TEMPERATURE IN COMBUSTION CHAMBER
WC:  TOTAL MASS IN COMBUSTION CHAMBER
EMRC:  O/F RATIO
PCIE:  CHAMBER PRESSURE AT INJECTOR END
PCNS:  CHAMBER PRESSURE AT NOZZLE END

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EMWC: EQUIVALENT MOLECULAR WIGHT IN COMBUSTION CHAMBER
C CPC: SPECIFIC HEAT RATIO IN COMBUSTION CHAMBER
C EMUC: VISCOSITY WITHIN COMBUSTION CHAMBER
C EKC: THERMAL CONDUCTIVITY WITHIN COMBUSTION CHAMBER
C PRDC: PRANDTL NUMBER IN COMBUSTION CHAMBER
C REYC: REYNOLDS NUMBER IN COMBUSTION CHAMBER

\[
dsum = DWOI + DWFI + DWACV + DWFIG(3) + DWBAF + DWPFS
\]
\[
ELFC = (DWOI + DWFI*ELFFI) / (dsum + 1.0E-6)
\]
\[
ELFCM = WCO/(WC+1.0E-6)
\]
\[
TCC = FGEN(20, 84, ELFC) + T(9)
\]
\[
GAMC = FGEN(13, 85, ELFCM)
\]
\[
WTC1 = prlnt( GAMC*(dsum * TCC - DWC * TC), 0, 142 )
\]
\[
WCO = prlnt( DWOI + DWFI*ELFFI - DWC*ELFCM, 0, 143 )
\]
\[
WCF = prlnt( DWACV + DWBAF + DWPFS + (1.0 - ELFFI) * DWFI
\]
\[
- (1.0 - ELFCM)*DWC + DWFIG(3), 0, 144 )
\]
IF ( PA/PCNS .LE.
+ XtoNY( 2./(GAMC + 1.0), GAMC/(GAMC - 1.0) ) ) THEN
\[
DWC = PCNS * ACN * 32.2 / CSTAR(I, EMRC, PCNS)
\]
ELSE
\[
DWC = GFLOW(PCNS,PA,TC,RGCC,GAMC) * ACN
\]
ENDIF
\[
WCN = prlnt( DWGN2*RGN2 - DWC*ENFC, 0, 145 )
\]
IF( WCN.GT. 0.0)
\[
ENFC = WCN/(WC + 1.0E-06)
\]
DWC = recpos( DWC )

* Unit 6 formatted output was removed
* 
\[
WC = WCO + WCF + WCN
\]
\[
TC = AMAXI(10.0, WTC/( WC + 1.0E-12) )
\]
\[
vTC = 1.0 / ( 2.0 * TC )
\]
\[
EMRC = WCO / ( WCF + 1.0E-12 )
\]
\[
PCIE = RGCC * WTC * vVOLC
\]
\[
PCIE = AMAXI( PCIE, PA )
\]
\[
PCNS = PCIE * EFFCM
\]
* Order was changed to calculate EMWC and CPC once,
and to test ENFC once.
IF ( ENFC.GT.0.0)
\[
EMWC = ( (WCO + WCF) * FGEN(12, 86, EMRC) + WCN * 28.0) / WC
\]
\[
CPC = ( (WCO + WCF) * FGEN(21, 87, ELFCM) + WCN * 0.274 ) / WC
\]
ELSE
\[
EMWC = FGEN(12, 86, EMRC)
\]
\[
CPC = FGEN(21, 87, ELFCM)
\]
END IF
\[
RGCC = 18540.0 / EMWC
\]
\[
EMUC = FGEN(25, 88, ELFCM)
\]
\[
EKC = FGEN(23, 89, ELFCM)
\]

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\[ \text{GAMAC} = (\text{GAMC} - 1.0) \times 0.5 \]
\[ \text{PRDC} = (\text{CPC} \times \text{EMUC}) / \text{EKC} \]
\[ \text{A4C} = \text{ABS} (\text{DWC}) / \text{ACN} \]
\[ \text{REYC} = \text{CPC} \times \text{X10th} (\text{EMUC}, 2) / \text{X10th} (\text{PRDC}, 6) \]

**Fixed Nozzle Hot Gas Side Heat Transfer**

The heat transfer equations used for the following codes are described in the document 29-30 with a slight modification. Similar explanations can be found in Hill's Book of "Mechanics and Thermodynamics of Propulsion". However, there is a major problem! The node 12 (down-comer) heat transfer is not calculated here. And, the following code includes node 7 heat transfer which does not contact with the nozzle.

**In the following:**
- EMC#: Mach number at specific point
- DIAT: Throat diameter
- QIN1(): Heat flow from hot gas to wall

\[ \text{EMC4} = \text{SC4} \times \text{GAMC} + \text{BC4} \]
\[ \text{EMFTR4} = 1.0 + \text{GAMAC} \times \text{EMC4}^{2} \]
\[ \text{SIGMA4} = 1.0 / (\text{XtoY}(\text{TWI}(4) \times \text{vTC} \times \text{EMFTR4} + 0.5, A3) \times \text{XtoY}(\text{EMFTR4}, A4) + \text{XtoY}(\text{EMFTR4}, A5)) \]
\[ \text{HTCC} = 0.026 / \text{DIAT}^{0.2} \times \text{REYC} \times \text{X10th} (\text{A4C}, 8) \times \text{A5} \]
\[ \text{HTCC4} = \text{HTCC} \times \text{X10th} (\text{AR4}, 9) \times \text{SIGMA4} \]
\[ \text{QIN1}(4) = \text{HTCC4} \times \text{AHTC4} \times (\text{TC} - \text{TWI}(4)) \]

**Main Chamber Hot Gas Side Heat Transfer**

\[ \text{EMFTR5} = 1.0 + \text{GAMAC} \times \text{EMC5}^{2} \]
\[ \text{EMFTR6} = 1.0 + \text{GAMAC} \times \text{EMC6}^{2} \]
\[ \text{EMFTR7} = 1.0 + \text{GAMAC} \times \text{EMC7}^{2} \]
SIGMA5 = 1.0 / ( XtoY(TW1(5) * vTC * EMFTR5 + 0.5, A3) * 
+ XtoY(EMFTR5, AA2) 
SIGMA6 = 1.0 / ( XtoY(TW1(6) * vTC * EMFTR6 + 0.5, A3) * 
+ XtoY(EMFTR6, AA2) 
SIGMA7 = 1.0 / ( XtoY(TW1(7) * vTC * EMFTR7 + 0.5, A3) * 
+ XtoY(EMFTR7, AA2) 
HTCC5 = HTCC * X10th(AR5, 9) * SIGMA5
HTCC6 = HTCC * X10th(AR6, 9) * SIGMA6
HTCC7 = HTCC * X10th(AR7, 9) * SIGMA7
QINI(5) = HTCC5 * AHTC5 * (TC - TW1(5))
QINI(6) = HTCC6 * AHTC6 * (TC - TW1(6))
QINI(7) = HTCC7 * AHTC7 * (TC - TW1(7))
RETURN
END
SUBROUTINE IGN0(I, POU, POD, RHOO, PFU, RHOF, PC)
*****************************************************************
C
C PURPOSE: SIMULATE THE IGNITION SYSTEM TRANSIENTS
C
C******ARGUMENTS******
C I = CHAMBER INDEX
C 1 = FPB
C 2 = OPB
C 3 = MCC
C
C A1 = OXIDIZER VALVE PRESSURE, PSI
C A2 = OXIDIZER INJECTOR MANIFOLD PRESSURE, PSI
C A3 = OXIDIZER VALVE DENSITY, LB/IN3
C A4 = FUEL SUPPLY PRESSURE, PSI
C A5 = FUEL SUPPLY DENSITY, LB/IN3
C A6 = IGNITOR CHAMBER DISCHARGE PRESSURE, PSI
C A7 = NOT USED
C N = INITIALIZATION FLAG inactivated
C
C IGNITOR ITSELF IS A SMALL COMBUSTION CHAMBER INSIDE (?) THE
C COMBUSTION CHAMBER.
C FUEL FEED LINES FOR IGNITORS ARE JUST LIKE REGULAR PIPE LINES
C WITH SMALLER SIZE. THE CALCULATION OF FUEL FEED LINE IS SIMPLE
C FOR A GIVEN CONDITION.
C OXID FEED LINES FOR IGNITORS ARE THE BYPASS LINES AFTER THE CONTROL
C OXID VALVES. THE FOLLOWING CALCULATION IS MAINLY DEALING WITH
C THE FLOW AND PRESSURE BALANCE OF THE IGNITOR LINES AND MAIN OXID LINES.
C THE SCHEMATIC OF THE OXID LINES FOR A COMBUSTOR IS:
C
C diagram omitted
C
C******COMMON USAGE******
C INPUT:
C VARIABLE
C T(3), T(9)
C
C OUTPUT:
C VARIABLE
C DWFIG,DWOIG,DW1,DW2,P4, PCIG
C DWFIG
C
C SUBSCRIPT (1)=FUEL PB, (2)=OXID PB, (3)=MAIN CHAMBER
C Eliminated superfluous arrays:

190
DIMENSION POU(3), POD(3), RHOO(3), PC(3), RHOF(3)

REAL AN(3), TAUC(3), ZFIG(3),
+ RFIG(3), P4(3), EL1(3), EL2(3), EL3(3),
+ R1I(3), R2I(3), R3I(3)

C

INCLUDE 'blank.com'
INCLUDE 'out.com'
INCLUDE 'igni.com'
INCLUDE 'units.com'

INTEGER Tstep
PARAMETER( Tstep = 0 )

C

IF ( I .EQ.1) THEN
  DO 11 J=1,3
    READ(run,12) R1I(J), R2I(J), R3I(J), AN(J), TAUC(J),
    + ZFIG(J), RFIG(J), RI(J) = RII(J)*0.0412
    R2(J) = R2I(J)*0.0412
    R3(J) = R3I(J)*0.0412
  11 CONTINUE
ENDIF

C

P4(I)=PA
PCIG(I)=PA
DWOIG(I)=1.0E-30
DW3(I)=DWOIG(I)
DW2(I)=1.0E-30
DW1(I)=2.0E-30
DWFIG(I)=1.0E-25
DWNIG(I)=1.0E-25
ELFIG(I)=0.0

C

CALL unint0( DWOIG(I), 213 + I )
CALL unint0( DW1(I), 216 + I )
CALL unint0( DW1(I), 219 + I )
CALL unint0( DWFIG(I), 222 + I )
CALL unint0( PCIG(I), 225 + I )

GAM=1.4
R=9270.0
TC=460.0
XINT=1.0
RETURN

ENTRY IGN(I, POU, POD, RHOO, PFU, RHOF, PC)

POU(I)=A1
POD(I)=A2
THIS IS TO CALCULATE THE PRESSURE CHANGE OF THE SEPARATION NODE (P4) AS THE RESULT OF THE CHANGES OF NEIGHBOR NODES POD, POU AND PCIG WITHIN THE TIME FRAME DT. THIS IS A TRANSIENT CALCULATION, FOR A STEADY STATE CONDITION (DT = LARGE) AND THE LAST TERM DROPS OUT.

IN THE FOLLOWING:

E = DELTA_POU / DELTA_DW1
F = DELTA_PCIG / DELTA_DW2
G = DELTA_POD / DELTA_DW3

E = 2.0*RI(I)/RHOO(I) *ABS(DW1(I)) + EL1(I)/DT
F = 2.0*R2(I)/RHOO(I) *ABS(DW2(I)) + EL2(I)/DT
G = 2.0*R3(I)/RHOO(I) *ABS(DWOIG(I)) + EL3(I)/DT

A = (-P4(I) + POD + R2(I)/RHOO(I) *ABS(DW2(I)) * DW2(I))/F
B = (-P4(I) + PCIG(I) + R3(I)/RHOO(I) *ABS(DWOIG(I)) * DWOIG(I))/G
C = (POU(I) - P4(I) - R1(I)/RHOO(I) *ABS(DW1(I)) * DW1(I))/E
D = 1.0/E + 1.0/F + 1.0/G

DP4 = (A + B + C)/D  

vRHOO = 1.0 / RHOO
rvt = 2.0 * vRHOO * DT
abdw = ABS( DW1(I) )
vedt = 1.0 / ( rv * R1(I) * abdw + EL1(I) )
cvdt = ( POU - P4(I) - R1(I)*vRHOO * abdw * DW1(I) ) * vted
abdw = ABS( DW2(I) )
vedt = 1.0 / ( rv * R2(I) * abdw + EL2(I) )
avdt = (-P4(I) + POD + R2(I)*vRHOO * abdw * DW2(I) ) * vfdt
abdw = ABS( DWOIG(I) )
vfdt = 1.0 / ( rv * R3(I) * abdw + EL3(I) )
bvdt = (-P4(I) + PIG(I) + R3(I)*vRHOO * abdw * DWOIG(I) ) * gdt
dvdt = vted + vfdt + vgdt
p4rate = ( avdt + bvdt + cvdt ) / ( dvdt * DT )

DWOIG(I) = prflow( DWOIG(I), EL3(I), -R3(I)*vRHOO, + P4(I) - PCIG(I), 213 + I )
DW1(I) = prflow( DW1(I), EL1(I), -R1(I)*vRHOO, + POU - P4(I), 216 + I )

P4(I) = pruint( p4rate, Tstep, 219 + I )

RF = RFIG(I) / RHOF
DWFIG(I) = prflow( DWFIG(I), ZFIG(I), RF, PFU - PCIG(I), 222+I )
ELFIG(I) = AMAX1(0.0, AMIN1(1.0, DWOIG(I)/(DWOIG(I) + DWFIG(I) + I.E-25)))

dwigs = DWOIG(I) + DWFIG(I)
IF ( ABS( dwigs ) .LT. 1.E-25 ) THEN
   ELFIG(I) = 1.0
ELSE
   ELFIG(I) = AMAX1( 0.0, AMIN1(1.0, DWOIG(I)/dwigs) )
ENDIF

GAM = fgen(13, 120 + I, ELFIG(I))

Example of limiting table input to avoid extending table,
* instead of looking up ABS(DWOIG(I))/(ABS(DWFIG(I))+1.E-6))

IF ( ABS( DWFIG(I) .LT. 1.0E-10 ) THEN
   EMRIG(I) = 1.0
   R = 1000.
ELSE
   EMRIG(I) = DWOIG(I) / DWFIG(I)
dwigs = ABS( EMRIG(I) )
IF ( dwigs .GT. 9999. ) THEN
   R = 600.
ELSE
   R = 18540.0 / fgen(12, 123 + I, dwigs )
ENDIF
ENDIF

TCIG(I) = AMAX1( 40.0, fgen(20, 126 + I, ELFIG(I)) + TF(I) )
DWNIG(I) = DWNIG(I) + 0.3 *
   + ( GFLOW(PCIG(I), PC, TCIG(I), R, GAM) * AN(I) - DWNIG(I) )
   SSM39000
PCIG(I) = pruint((DWFIG(I) + DWOIG(I) - DWNIG(I))/TAUC(I),
   + Tstep, 225 + I )
EMRIG(I) = DWOIG(I) / (DWFIG(I) + 1.0E-10) replaced by above
END
'gflow.for':

FUNCTION GFLOW(UP,PD,TU,R,G)
******************************************************************************************************************
C
C PURPOSE: COMPUTE ISENTROPIC IDEAL GAS FLOW FOR CHOKE
AND UNCHOKED ORIFICES
C
C*****ARGUMENTS*****
C INPUT:
C UP = UPSTREAM PRESSURE, PSI
C PD = DOWNSTREAM PRESSURE, PSI
C TU = UPSTREAM TEMPERATURE, DEG R
C R  = GAS CONSTANT, IN-LBF/(LBM-DEG RF)
C G  = GAMMA, RATIO OF SPECIFIC HEAT
C
C OUTPUT:
C GFLOW = MASS FLOW RATE/AREA LB/IN2-SEC
C
******************************************************************************************************************
* slowl(gee) = 2.0 * xtoy( gee + 1.0, - gee / (gee - 1.0) )
* slow2(pr,gee) = xtoy( pr, 2.0/gee ) - xtoy( pr, (gee + 1.0)/g )
* test = 772.8 * G / (R * TU * (G-1.0))
IF ( test .LT. 0.0 ) THEN
  GFLOW = 0.0
ELSE
  IF ( UP .LT. PD ) THEN
    P1 = - PD
    ratio = UP / PD
  ELSEIF ( UP .EQ. PD ) THEN
    P1 = 0.0
    ratio = 1.0
  ELSE
    P1 = PD
    ratio = PD / PU
  ENDIF
  PR = AMAX1( slowl(G), ratio )
  IF ( PR .LT. 0.0 ) THEN
    GFLOW = 0.0
  ELSE
    test2 = slow2(PR)
    IF ( test2 .LT. 0.0 ) THEN
      GFLOW = 0.0
    ELSE
      GFLOW = P1 * X10th( test * test2, 5 )
    ENDIF
SUBROUTINE CNTRL0
*******************************************************************************
C THIS IS THE PROGRAM SIMULATE THE DIGITAL CONTROL FUNCTIONS OF SSME.
C IT IS APPARENT THAT THE DATA WERE READ AND WRITTEN EVERY 0.02 SECOND.
C D/A DELAY AND INSTRUMENT DELAYS ARE ACCOUNTED FOR BY TIME CONSTANTS
C TIMEVC, TIMECP, TIMEPR, AND OTHERS.
C THE PURPOSE OF THIS SIMULATION IS TO READ MEASUREMENT OUTPUT AND
C CALCULATE THE NECESSARY OUTPUT AS DEFINED BY THE CONTROL SCHEME.
C
C ONLY INPUTS THAT CAN BE USED TO CALCULATE CONTROL SIGNALS ARE
C THOSE ACTUALLY MEASURED AND USED.
*******************************************************************************
C
C*****ARGUMENT*****
C ICCNTL = INITIALIZATION FLAG eliminated in favor of initialization
C
C*****COMMON USAGE*****
C INPUT:
C VARIABLE SOURCE
C DW(1),DW(2),P(3),T(2),RHO(2) FUELF
C PCIE,DWPO,DWFPO HOTGAS SSM01500
C DMMOV OXIDF
C XOPOV VALDYM
C
C OUTPUT:
C VARIABLE DESTINATION
C XCFPOV,XCOPOV,XCMOV,XCMPV,XCCCV VALDYM
C
C SUBROUTINES CALLED: EMCO
C
C*******************************************************************************
C
C LOGICAL RESET, first
DIMENSION D(5),PIN(5),DEN(5),PD(5),XP(5),I1(5)
DIMENSION AT(5),BT(5)
DIMENSION STHETA(5)

C
C INCLUDE 'blank.com'
C INCLUDE 'out.com'
C INCLUDE 'contrl.com'
C INCLUDE 'hgas.com'
C INCLUDE 'oxid.com'
C INCLUDE 'balc.com'
C INCLUDE 'valves.com'

COMMON/PURGE/DWGN2,TCUTPR,DWGN2F,DWGN2O SSM02000

195
* Computation constants

PARAMETER ( PI = 3.141596, tpcnst = 8. / (386.4 * PI ** 2),
  + piov2 = PI * .5 , twopi = PI * 2. )
PARAMETER ( v1728 = 1./1728., v41p12 = 1./41.42,
  + v14p06 = 1./14.06, v29p95 = 100. / 2995. )
PARAMETER ( v29p95 = i00. / 2995. )

DATA XOPOMS/ 100.0 /
DATA I1/11,14,16,32,36/

C INITIALIZE LOCAL VARIABLES AND ARRAYS NOT ASSIGNED VALUES
C THIS IS NECESSARY FOR SUCCESSFUL EXECUTION ON THE IBM
* Unnecessary initialization was eliminated. It created unused
* variables, due to confusion between 'O' and '0' characters.
* IF(FLAG.EQ.15.) GO TO 9999
  C2=0.0
  EEMR=0.0

initializations omitted

YCOPVL=0.0
DO 9998 I=I,5
  D(I)=O.O
  DEN(I)=0.0
  PD(I)=O.O
  PIN(I)=0.O
  STHETA(I)=0.O
  XP(I)=0.O
9998 CONTINUE
IPBCO=0

C********************************************************************
C THIS IS THE INPUT READING FOR MOST CONTROL PARAMETERS.
C THESE PARAMETERS DETERMINE THE SCHEDULE, LEVEL VS. TIME, OF:
  1) THRUST REQUESTS,
  2) MIX-RATION REQUESTS,
  3) OPEN-LOOP OPOV SETTINGS,
  4) CLOSED-LOOP GAINS, K, KP AND KI, OF THRUST CONTROL (OPOV),
  5) OPEN-LOOP FPOV SETTINGS,
  6) CLOSED-LOOP GAINS, K, KP AND KI, OF MIX-RATION CONTROL (FPOV)
  7) MAIN OXID VALVE (MOV),
  8) MAIN FUEL VALVE (MFV),
  9) COOLANT CONTROL BYPASS VALVE (CCV),
C********************************************************************

30 FORMAT(IX,6FI2.0)
READ(run, 30)TIDMO,TOPOV,TMOVST,TMOVRA,TBPV,XMOVST,DTF,FRZ
1, DBEF,DBMR,TPI,DTPS,DTOPFS,DTVFS,DTMCR,TCUT,TCLF,F1,DF1,F2,FC,TVC
C

* load function interpolation tables
*

CALL fgset( 6 ) SSM04500
CALL fgset( 17 ) SSM05000
CALL fgset( 18 )
CALL fgset( 19 )
CALL fgset( 31 )
CALL fgset( 33 )
CALL fgset( 55 )
YCMFV = FGEN(55, 90, 0.)
CALL fgset( 56 )
CALL fgset( 57 )

* Added for TLIMIT
CALL fgset( 84 ) SSM05100
XOPOV=0.0
XFPOV=0.0
XMOV=0.0
ROPOV=1.0E+12
RFPOV=1.0E+12
RMOV=1.0E+12
EMRG=0.0
EMRFPO=0.0
EMROPO=0.0
DXFPOV=0.0
DXOPOV=0.0
PCOPO=5.0
PCFPO=0.0
FR=60000.0
XCOPOV=0.0
XCFPOV=0.0
XCMFV=0.0
XCMOV = 0.0
XCMOVC=XCMOV
XCCCV=100.
YCFPOV=0.0
YCOPOV=0.0
YCMOV=0.0
YCCCV=100.0
TFT2D=TFP
TOT2D=TOP

197
EPCGC=0.0
EPC=0.0
TCUTFP=1000.0
TCUTOP=1000.0
TCUTCV=1000.0
TCUTFV=1000.0
TCUTOV=1000.0
TMPL=1000.0
DPRI=DPR
DPLI=DPL
DTI=DT
IFIND=0
IOIND=0
PIPF=-1.
PIPO=-1.
NCF=0
NCO=0
ICUT=1
RESET = .FALSE.
NMALF = 0
STEPO = 0.0

* Resetting of TIMExx values in EMCO(1), now EMCO0, was eliminated.
* Initializing timing values to STIME works for a restart as well.

TIMECP = STIME
TIMEPR = STIME
TIMETR = STIME
TIMEVC = STIME
TSMFV=AMIN1(TSMFV+TPA,TSMFV+TCUT)
CALL EMCO0
inkdt = 300000. * DT
df1dt = DF1 * DTMC
dfrcdt = DFRC * DTMC
frbias = 1. + .01 * PFRNZ
osdt = DTMC * OSLAM
op0dt = DTMC * OFCR0
op1dt = DTMC * OPCR1
op2dt = DTMC * OPCR2
fp0dt = DTMC * FPCR0
fp1dt = DTMC * FPCR1
fp2dt = DTMC * FPCR2
omvdt = OMVCR * DTMC
omvodt = OMVCR0 * DTMC
omvfdt = OMVCRF * DTMC
ydt1 = .32 - DTMC
ydt2 = DTMC / (.32 + DTMC )
dmovdt = DMVO * DTMC
dcc3dt = DCCV3 * DTMC


```plaintext

dcc2dt = DCCV2 * DTMC
dccvdt = DCCVC * DTMC
dccldt = DCCVI * DTMC
dcc0dt = DCCV0 * DTMC
dptdt = DP1MFV * DTMC
dp2dt = DP2MFV * DTMC
IF ( ipflag .EQ. 1 ) THEN
  fzopvb = FZOPV
  fzycf = FZFPV
  fzycm = FZMOV
  fzyc = FZCCV
  fzycmf = FZMFV
ELSE
  fzopvb = FZOPV * ( 1. + .01 * POPVNZ )
  IF ( fzopvb .GE. 100.0 ) fzopvb = FZOPV
  fzycf = FZFPV * ( 1. + .01 * PFPVNZ )
  IF ( fzycf .GE. 100.0 ) fzycf = FZFPV
  fzycm = FZMOV * ( 1. + .01 * PMOVNZ )
  IF ( fzycm .GE. 100.0 ) fzycm = FZMOV
  fzyc = FZCCV * ( 1. + .01 * PCCVNZ )
  IF ( fzyc .GE. 100.0 ) fzyc = FZCCV
  fzycmf = FZMFV * ( 1. + .01 * PMFVNZ )
  IF ( fzycmf .GE. 100.0 ) fzycmf = FZMFV
ENDIF

dtm100 = 100. * DTMC
dtm200 = 200. * DTMC
CALL unint0( FRADS, 146)
CALL unint0( ORADS, 147)

ENTRY CNTROL

C CONTROLLER SIMULATION BEGINS HERE
C PIN( ) : INPUT PRESSURE TO THE VALVE
C D( ) : FLOW RATE TO THE VALVE
C DEN( ) : DENSITY OF FLOW MEDIA
C PD( ) : DOWN STREAM PRESSURE
C VPD( ) : VALVE PORT DIAMETER
C XP( ) : % OPENNING OF VALVE ANGLE
C READER SHOULD REFER TO THE SSME DOCUMENT FOR FURTHER DETAILS ON
C VALVE CHARACTERISTICS.
C**************************NMALF IS THE FLAG OF PURGE REQUEST WHEN MALFUNCTIONS DETECTED*********
C
IF ( NMALF .GT. 0 ) THEN
  NMALF = 1
  TCUTPR = AMINI( TCUTPR, TPA + DTPURG )
  DT=DTI change in DT disallowed
  IF ( STIME .LE. TPA + DTPNC ) RETURN
  CALL EMCO(2)
```

199
**CALCULATE HYDRAULIC AND SLIDING FRICTIONAL TORQUE TP( ) **********

ALTHOUGH THE VALUE TP( ) SHOULD BE USED IN CALCULATING THE WIND-UPS AND STICTIONS, THIS VALUE IS REALLY NEVER USED IN THIS SIMULATION. THE WIND-UPS AND STICTIONS ARE SET TO BE CONSTANTS IN THE VALVE DYNAMIC SIMULATION SUBROUTINE VALDYN( ).

The calculation of TP is left in, on the theory that the values can be monitored or later used in the simulation.

DO 250 I=1,5
  IF( DTHETA(I) .EQ. 0.D0 ) THEN
    * STHETA(I) = DTHETA(I) replaced to avoid unnecessary conversion
    STHETA(I) = 0.
    THK = 0.0
    TP(I)=0.
  ELSE
    THK = FGEN(I1(I), 90 + I, XP(I)*.01 )
    TP(I) =
    * * SIGN(AT(I)+(BT(I)+0.8*ESS(I))*(PIN(I)-8./386.4/DEN(I)*(D(I)/
I have absolutely no idea of what this section of codes is doing.

PPFM and POFM are pressures of MFV and MOV (?)

DENF and DENO are calculated densities

FRADS and ORADS are accumulated volumes

SIN() of FRADS and ORADS means ???????????

Since PIPF is the previous value of SFRADS (DT=0.0002), the following condition seems to indicate the change of sign from - to +.

IF(IFIND.NE.2.OR. SFRADS.LT.0.) GO TO xx

IF(IFIND.NE.2.OR. PIPF.GT.0.) GO TO xx

However, none of the variables generated in this section are used anywhere in the simulation of the SSME.

Unfortunately for simulation speedup, the code of this section does affect the simulation. The KOUNTF and KOUNTO set NCF and NCO, affecting EMRF.

PFFM=P(3)-DW(2)*ABS(DW(2))/RHO(2)*2.87137E-06

DENF=(( -1.4013E-03+3.09257E-06*PFFM)*T(2)**2+(6.5220E-02-

+ 2.14666E-04*PFFM)*T(2)+3.8956+4.27390E-03*PFFM)/1728. replaced b

DENF = v1728-( 3.8956 + 4.27390E-03*PFFM + T(2) *

+ ( 6.5220E-02 - 2.14666E-04*PFFM +

+ (-1.4013E-03 + 3.09257E-06*PFFM)*T(2) ) )

FRADS = pruint( DW(2)*v41pI2/DENF, 0, 146 )

POFM = POD2 -

+ (DWOP2 - DWOT1)*ABS(DWOP2 - DWOT1)/RHOOP2*1.543474E-05 SSM06100

DENO = (( -0.16603+5.6683E-06*POFM)*TOD2 + 98.5 -1.8237E-04*POFM )

+ * v1728

ORADS = pruint( (DWMOV+DWOPO+DWFPO)/DENO*v14p06, 0, 147 )

IF(FRADS.GT.1.0E+20) THEN

FRADS = 0.

uint0( 0., 146 )

ENDIF

IF(ORADS.GT.1.0E+20) THEN

ORADS = 0.

uint0( 0., 147 )
ENDIF

* SFRADS=SIN(FRADS) sin and arcsin series had been used, where
* SORADS=SIN(ORADS) only a mod function is required.
sfrads = MOD( FRADS, twopi )
sorads = MOD( ORADS, twopi )

* The selection sequence based on IFIND and IOIND was rewritten
* for clarity and to eliminate repeated tests.

   GO TO ( 40, 50 ) IFIND
   GO TO 60
* case IFIND is 1

40 IF ( SFRADS .LT. PI .AND. PIFP .LE. 0. ) THEN
* Statements of the form kountx = kountx + realexpression
* force the unnecessary conversion of kountx to REAL and
* reconversion of the sum to integer. They are replaced by
* a sequence requiring the minimum single conversion.
* KOUNTF=KOUNTF+300000.*ASIN(SFRADS)*DENF*41.12/DW(2) replaced by
* ink = 12.336E+6 * MOD( FRADS, piov2 ) * DENF / DW(2)
* KOUNTF = KOUNTF + ink
* IFIND=2
ENDIF
GO TO 60
*
* case IFIND is 2
*
50 IF ( SFRADS .GE. 0. .AND. PIFP .LE. 0. ) THEN
* ink = 12.336E+6 * ABS( MOD( PIFP, piov2 ) ) * DENF / DW(2)
* KOUNTF = KOUNTF + ink
* IFIND=3
ENDIF
*
* The simulation loop invariant inkdt = 300000. * DT is computed in CNTRL0
* KOUNTF = KOUNTF + inkdt
*
60 dwsum = DWMOV + DWOPO + DWFP0
GO TO( 70, 80 ) IOIND
GO TO 95
*
* case IOIND is 1
*
70 IF ( SORADS .LT. PI .AND. PIFO .LE. 0. ) THEN
* ink = 12.336E+6 * MOD( ORADS, piov2 ) * DENO /

202
+ ( dwsum + 1.0E-06 )
KOUME = KOUME + ink
IOIND=2
ENDIF
GO TO 95

* case IOIND is 2
* 
80 IF ( SORADS .LT. PI .AND. PIFO .LE. 0. ) THEN
ink = 12.336E+6 * ABS( MOD( PIPO, piov2 ) ) * DENO / 
+ ( dwsum + 1.0E-06 )
KOUME = KOUME + ink
IOIND = 3
ENDIF
KOUMF = KOUMF + inkdt

95 PIFP = SFRADS
PIPO = SORADS
DPL = DPLI
DPR = DPRI
F = FCOMP
EMRE = dwsum / (DW(1) + 1.0E-10)

C**** RESET INTEGRAL OF ERROR FOR PI CONTROLLER AT MAINSTAGE ******
C
IF ( STIME .GE. TMS .AND. .NOT. RESET) THEN
RESET = .TRUE.
EMROPO = YCOPOV - STEPO
EPGCG=0.
* PCPOI=0. Ineffective assignment replaced by
PCPOP = 0.
*
PCPOI= -VPG*EPC
EMRFPO = YCFPOV - STEPF
EMRGC=0.
ENDIF

C THIS SECTION DESCRIBES THE SCHEDULE OF THE SHUTDOWN PROCESS
IT INCLUDES THE VALVE CLOSING, AND LINE PURGE SEQUENCES.

IF ( TPI .GT. 0.0 .AND. STIME .GE. TPI ) THEN
C***** SIMULATION OF THE PNEUMATICAL CUT-OFF OF THE POWER *****
C
IF ( STIME .LT. TPI + DTPS) RETURN
IF( STIME .LT. tpm ) THEN
*
* Eliminated unnecessary save and restore of TIMExx.

203
tpm = TPI + DTMCR
TPA = TPI + DTPS
CALL EMCO(2)
EMRE = (DWOV+DWOPO+DWFPO)/(DW(1)+1.0E-10)
RETURN
ENDIF

* This section makes obscure timing interval adjustments that
* should be explained. Perhaps it compensates for roundoff errors
* accumulated in time advance. The first one is partially interpreted
* below. Relief from roundoff time advance roundoff error should be
* obtained by going to a frequency based, integer time advance. With all
* important time intervals as multiples of the sampling interval.
*
* IF ( TIMFMA .LE. tpm) THEN
* TLMC = TIMFMA - DTFMRA
* IF ( TIMECP .LT. TLMC ) THEN
* TIMECP = DTM + TIMECP
* advances controller interval
* TIMECP=TIME+TIMECP-TLMC
* essentially TIMECP = TIMECP + DT, with
* perhaps some accuracy dependent effect
*
* IF(TIMEPR.LT.TLMC) TIMEPR=DTMC+TIMEPR
* TIMEPR=TIME+TIMEPR-TLMC
* IF(TIMEVC.LT.TLMC) TIMEVC=DTMC+TIMEVC
* IF(TIMFME.LT.TLMC) TIMFME=DTMC+TIMFME
* TIMFME=TIME+TIMFME-TLMC
* IF(TIMFMC.LT.TLMC) TIMFMC=DTMC+TIMFMC
* TIMFMC=TIME+TIMFMC-TLMC
* IF(TIMETR.LT.TLMC) TIMETR=TIMETR+DTMC
* TIMETR=TIME+TIMETR-TLMC
* IF(TIMMRF.LT.TLMC) TIMMRF=TIMMRF+DTMC
* TIMMRF=TIME+TIMMRF-TLMC
* IFIND=0
* KOUNTF=0
* IOIND=0
* KOUNTO=0
* TIMEVC=TIME+TIMEVC-TLMC
* TIMFMA=TIME+DTFMRA
ENDIF

5015 IF(TIMEVC.GT.TPI+DTPF) GO TO 5020
5020 IF( STIME .GE. TPI + DTVF ) THEN
   TPI=0.
   tpm = DTMCR
   TPA=0.
TPA = DTPS
GO TO 1008
ENDIF
5030 IF ( STIME .LT. TPI + DTOPFS ) THEN
CALL EMCO(2)
EMRE=(DWMOV+DWOPO+DWFP)/((DW(1)+1.0E-10)
IF(TIMEVC.LT.STIME) TIMEVC=TIMEVC+DTMC
GO TO 1008
ENDIF
5040 XX=XCOPOV
CALL EMCO(2)
XCOPOV=XX
IF(TIMEVC.GT.TIME) GO TO 1008
TIMEVC=TIMEVC+DTMC
XCOPOV=YCOPOV
GO TO 1008
ENDIF

IF ( TPA .GT. 0.0 .AND. STIME .GE. TPA ) THEN
C * Initiates purge request from malfunction detected
C
NMALF = 1
TCUTPR = AMIN1( TCUTPR, TPA + DTPURG )
* DT=DTI Change in DT was disallowed, no restoration necessary.
IF ( STIME .LE. TPA + DTPNC ) RETURN
CALL EMCO(2)
EMRE = ( DWMOV + DWOPO + DWFP ) / ( DW(1) + 1.0E-10 )
RETURN
ENDIF

GO TO (1002,1004,1006,1008),ICUT

* Case ICUT is 1

*1002 IF(TIME.GT.TCUT.AND.FR.LT.1500.) ICUT=2
* IF(TIME.GT.TCUT:AND.IPBCO.EQ.1) ICUT=2 Time vs TCUT once.
* IF (TCUT.LT.TMS.AND.TIME.GT.TCUT)ICUT=2
1002 IF ( STIME .GT. TCUT .AND.
+ ( FR .LT. 1500. .OR. IPBCO .EQ. 1 .OR. TCUT .LT. TMS )
+ ICUT = 2
* Delay transition state one DT
GO TO 1008

* Case ICUT is 2: transition state goes immediately into state 3 or 4

1004 TCUTFP = STIME
TCUTOP = STIME
TCUTOV = STIME
ICUT = 3
* Case ICUT is 3: wait until XCOPOV .LE. OPOVPB, then ___

1006 IF(XCOPOV.GT.OPOVPB) GO TO 1008
ICUT=4
TCUTFV = STIME + DTCOMF
TCUTCV = STIME + DTCOCV
TMPL = STIME

* Case ICUT is 4: all transitions completed

1008 CONTINUE

C

C******** FOLLOWING LINE CHECK WHETHER IT IS TIME TO ACTIVATE THE CONTROLLER
C******** THE CONTROLLER SAMPLING AND CYCLE TIME IS DTMC (=0.02)

C
IF(TIME.LT.TIMECP.AND.ICCNTL.EQ.2) GO TO 4000 The ICCNTL test is unnecessary, provided TIMECP is initialized to the starting time.

IF ( STIME .LT. TIMECP ) GO TO 4000

C

CALCULATION OF CONTROL REFERENCE VALUES

C

C******** SAVE THE PREVIOUS CALCULATED VALUE WHICH WILL BE SENT OUT
C******** AT NEXT VALVE-COMMAND-OUTPUT TIME

C
YCOPVL=YCOPOV
YCFPVL=YCFPOV
YCOMVL=YCMOV
YCFMVL=YCMFV
YCCVL=YCCCV

C

THRUST REFERENCE

C

IF ( STIME .LE. TCUT ) THEN
IF ( STIME .LE. TMOVRA ) THEN
IF ( STIME .LE. TCLF ) THEN
FR = F1
ELSE
FR = AMAX1(FRZ, FR - dfldt)
ENDIF
ELSE
IF( STIME .GT. TVC ) THEN
FR = FGEN(33, 96, STIME)
ELSE
FR = AMIN1( F2 + DTF*(STIME - TMOVRA), FC )
ENDIF
ENDIF
ELSE

206
* 1015 DT=DTI restored DT after reset to 0.0001. But unless time runs
* backward, each restoration is immediately undone by the
* next statement.
* 
* IF(TIME.GT.TCUT+0.5) DT=0.0001 was deleted. It reset the time step
* of the entire simulation to a constant, overriding the input parameter
* DT. This disrupts all multistep integrators, and cannot be permitted.
* The philosophy is questionable, allowing the simulated controller to
* interfere with the simulation itself. There is no need to supply a
* local version of DT for the controller to manipulate, since it doesn't
* use DT. Increasing the time step DT with better integrators, speeding
* up the simulation, and going to selective output should eliminate the
* need for changing DT after TCUT.
* 
* \[ FR = \text{AMAX1}(FCO, FR - dfrcdt) \]
* ENDIF

**THRUST CONTROL OF OXID PREBURNER OXID VALVE**

**THRUST AND PREBURNER OVERTEMP ERRORS**

C*****
THE FOLLOWING LINE IS USED TO SIMULATE A PERTURBATION ON THE
C*****
REFERENCE INPUT FR (CHAMBER PRESSURE) REQUEST DURING THE CLOSED-
C*****
CONTROL. PFRNZ IS THE % NOISE APPLIED TO THE REFERENCE INPUT FR
C*****
PFRNZ is a constant bias set by the main program perturbation section
but initialized to zero in CNTRL.
C*****
FR = FR*(1. + PFRNZ/100.) was moved to CNTRL0
C*****
FR = FR * frbias

C*****
TOPEN IS A PARAMETER ADDED TO OPEN THE CONTROL LOOP TO SIMULATE
C*****
OPEN LOOP CONDITION OF THE SSME MAIN STAGE OPERATION.
C*****
IT TURNS OUT THAT THE SSME IS A STABLE SYSTEM AS SIMULATED
C
Does the last comment mean open loop simulation is no longer needed?
if so TOPEN and its activated sections should be removed. Assuming
that open loop tests will continue, open loop operations were
were consolidated, with one test per iteration for open loop
conditions. Control through IPFLAG, described below, was implemented.

C
 IF ( STIME .LT. TOPEN .OR. IPFLAG .EQ. 0 ) THEN
    EPC = FR - PCIE
    EPCGCL = EPCGC
 C
 C*****
 PCGC IS THE GAIN FACTOR DETERMINE HOW MUCH THE POSITION ERROR IS
 C*****
 USED FOR PI CONTROLLER.
 C
 PCGC = rlimit( GMIN, 1., GPCI + GPC2*FR )
 EPCGC = EPC * PCGC
THE NEXT LINE SHOULDN'T BE HERE. IT IS ABOUT THE MIX-RATIO CONTROL
AND AN EXACT SAME LINE IS IN SSM07570. THIS IS THE DEAD-BAND OF
CONTROLLER. I ADDED THE LINE AFTER THAT FOR CHECKING EPCGC.

IF(ABS(EMRGC) .LT.DBMR) EMRGC=0.0
* IF(ABS(EPCGC) .LT.DBEF) EPCGC=0.0

FOR T < TCLF  OPEN-LOOP, NO CONTROL
FOR TCLF < T < TUT  POSITION CONTROL ONLY, KI=0
FOR T > TUT  PI CONTROLLER APPLIES

IF ( STIME .LE. TUT) THEN
  VIG=0.0
  VPG=0.01444
ELSE
  VIG=VIGMS
  VPG=VPGMS
ENDIF

OPOVIP = FGEN(56, 97, STIME + DTMC)
IF ( STIME .LT. TMS )
   EMROPO=OPOVIP
ENDIF

IF ( STIME .LT. TCLF) THEN
  PCOPO = 0.0
ELSE
  PCOPOP = VPG*EPCGC
  PCOPOI = AMINI( XOMAX, 0.5*(EPCGC + EPCGCL)*VIG*DTMC )
  PCOPO = rlimit( -100., 100., PCOPOP + PCOPOI )
ENDIF

OXID PREBURNER OXID VALVE POSITION

IF ( STIME .GE. TCUTOP ) THEN
  CUT-OFF SCHEDULE OF OPOV ********
  OSLAM was added as a input parameter, and invariant multiplies
  removed from simulation loop
  *
  IF ( STIME .GT. TCUTOP + DTSLAM) THEN
    YCOPOV = AMAX1(.00001, YCOPOV - osdt)
  ELSE IF ( XCOPOV .GT. OPOVCM) THEN
    YCOPOV = AMAX1(.00001, YCOPOV - op0dt)
  ELSE IF ( XCOPOV .GT. OPOVCP) THEN
    YCOPOV = AMAX1(.00001, YCOPOV - op1dt)
  ELSE
    YCOPOV = AMAX1(.00001, YCOPOV - op2dt)
  ENDIF

208
CALCULATE OPOV COMMANDS AT DIFFERENT STAGE

ELSE
    IF ( STIME .LT. TUT ) THEN
        IF( STIME .GT. TCLF) THEN
            RO = RO3
        ELSE IF ( YCOPOV .LT. OPOVOP ) THEN
            RO = ROI
        ELSE
            RO = RO2
        ENDIF
    IF ( STIME .LE. TOPOV ) THEN
        YCOPOV = 0.0
    ELSE
        YCOPOV = AMIN1( EMROPO + PCOPO, YCOPOV + RO*DTMC )
    ENDIF
ELSE
    STEPO = OSTEP
ENDIF

** OPOV COMMAND LIMIT

Function TLIMIT was replaced by a call to fgen, which does linear interpolation in an optimal manner. TLIMIT data was reconstructed and added to SSME.DAT file. TLIMIT was optimized, but extrapolated beyond the table. fgen halts the simulation and identifies the table if the input escapes the interpolation table.

EFFPL = 100.0 * FR / 2995.0 + 1.5 * XOPOMS - 97.5
YCOPOV = TLIMIT (FR, XOPLIM, XOPOMS, YCOPOV, NMR)

EFFPL = V29.95 * FR + 1.5 * XOPOMS - 97.5
YCOPOV = rlimit(.00001, 100.0, EMROPO + PCOPO + STEPO )
YCOPOV = fgen( 84, 114, EFFPL )

IF (YCOPOV .LT. XOPLIM) THEN
    NMR = 1
ELSE
    NMR = 0
    YCOPOV = XOPLIM
ENDIF
ENDIF

MRC REFERENCE

IF ( TMRS .GE. 1.0 .AND. STIME .GE. TMRS ) THEN
    EMRCR = 5.5
ELSE
    EMRCR = 6.026
ENDIF
MR CONTROL USING FUEL PREBURNER OXID VALVE

***** THE FOLLOWING LINE IS USED TO SIMULATE A PERTURBATION ON THE REFERENCE INPUT EMRCR (MIX-RATIO) REQUEST DURING THE CLOSED-LOOP CONTROL. THE MIX-RATIO (EMRF) TO BE CONTROLLED IS NOT THE ACTUAL MIXRATIO IN THE COMBUSTION CHAMBER (NOT MEASURABLE), IT IS THE ESTIMATED MIX-RATIO BASED ON CHAMBER PRESSURE AND FUEL FLOW RATE.

EMRCR = EMRCR * pmrnzb

HERE: ERROR = (REFERENCE - OUTPUT/MEASUREMENT)

WHICH IS BECAUSE OF THE NEGATIVE GAIN OF FPOV VS. MIX-RATIO.

IF ( TIME .LT. TMRC ) THEN
  EEMR=0.0
  EMRGCL=EMRGC
ELSE
  EEMR=EMRF-EMRCR
  EMRGCL=EMRGC
ENDIF

GCEMR = rlimit( GMRMIN, GMRMAX, GMR1 + GMR2 * FR )
EMRGC=EEMR*GCEMR
IF ( ABS(EMRGC) .LT. DBMR ) EMRGC=0.0

***** THE ADJUSTMENT OF FPOV IS IN PROPORTIONAL TO THE OPOV ADJUSTMENT THIS RATIO IS A FUNCTION OF TIME

IF( STIME .GE. TMS ) THEN
  PCFPO = CFGMS * PCOPO
ELSE
  PCFPO = PCOPO * rlimit( CFG1, CFG2,
                     + DCFG*(STIME - TCLF) + CFGC )
ENDIF

***** IF TIME < TMRC OPEN LOOP WITH SCHEDULED VALVE POSITION
***** > TMRC PI CONTROL

IF ( STIME .GE. TMRC ) THEN

***** THE INTEGRAL GAIN IN THIS CASE IS 40.0 AND KP = VPM (=7.0)
***** 20. = 40. / 2.

EMRFPO = rlimit(.00001, 100., EMRFPO +
+ DTMC*20.*(EMRGC + EMRGCL) + VPM*(EMRGC - EMRGCL) )

***** START-UP SCHEDULING OF FPOV

ELSE

210
IF ( STIME .LE. -0.1 ) THEN
    EMRFPO = 0.0
ELSE
    FPOVIP = FGEN(57, 98, STIME + DTMC)
    IF ( STIME .GT. TCLF) THEN
        RO = RF3
    ELSE IF ( YCFPOV .LT. FPOVOP) THEN
        RO = RFI
    ELSE
        RO=RF2
    ENDIF
    EMRFPO = AMINI( FPOVIP, EMRFPO + RO*DTMC )
ENDIF

ENDIF

* IF (TIME .LE. TCFG) PCFPO = 0.0
STEPF = FSTEP
IF (TIME .LT. TUT) THEN
    STEPF = 0.0
    IF ( STIME .LT. TCUTFP ) THEN
        YCFPOV = AMINI(EMRFPO + PCFPO, YCFPOV + RO*DTMC)
    ELSE IF ( XCFPOV - XCOPOV .GE. DXCFPO + OR. XCOPOV .LE. 10. ) THEN
        IF ( XCFPOV .GT. FPOVCM ) THEN
            YCFPOV = AMAXI( .00001, YCFPOV - fp0dt )
        ELSE IF ( XCFPOV .GT. FPOVCP) THEN
            YCFPOV = AMAXI(.00001, YCFPOV - fp1dt)
        ELSE
            YCFPOV = AMAXI(.00001, YCFPOV - fp2dt)
        ENDIF
    ENDIF
ENDIF
ELSE IF ( STIME .LT. TCUTFP ) THEN
    IF ( STIME .GE. TMOVRA ) THEN
        IF ( STIME .GT. TMS ) THEN
            YCFPOV = rlimit(.00001, 100.0, EMRFPO + PCFPO + STEPF)
        ENDIF
    ENDIF
ENDIF
ENDIF
IF (TIME .LT. T1FPV) YCFPOV = AMINI (FPOVMX, YCFPOV)

MOV POSITION

MOV OPENING IS TIME SCHEDULED BEFORE THE MAIN STAGE
AFTER THAT, IT IS PROPORTIONAL TO THRUST REQUEST (FR)

XCMOVL = XCMOVIC
IF ( STIME .LT. TCUTOV ) THEN
    IF ( STIME .GE. TMOVRA ) THEN
        IF ( STIME .GT. TMS ) THEN

211
XCMOVC = AMIN1(100., DFMOV*FR + FMOVC)
ELSE
    XCMOVC = AMIN1(XMOVM, XMOVST + (STIME - TMOVRA)*DMOVUT)
ENDIF
ELSE IF ( STIME .LT. TMPL) THEN
    IF ( XCFPOV - XCOPOV .LT. DXCFPO ) THEN
        XCMOVC = XCMOVC + omv0dt
    ELSE
        XCMOVC = AMAXI(.00001, XCMOVC - omv0dt)
    ENDIF
ELSE IF ( STIME .GT. TIMOV .AND. STIME .LT. T2MOV ) THEN
    XCMOVC = XMOVPT
ELSE
    IF ( T2MOV .GE. 1. .AND. STIME .GE. T2MOV) omvdt = omvfdt M08000
    XCMOVC = AMAXI(.00001, XCMOVC - omvdt)
ENDIF

YCMOV = (YCMOV*(2.0*.I6-DTMC)+DTMC*(XCMOVL+XCMOVC))/(2.0*.I6+DTMC)

Is this correct? Was average xcmov intended? Invariants were removed.

YCMOV = YCMOV * ydt1 + (XCMOVL + XCMOVC) * ydt2

ELSE IF ( STIME .GT. TSMOV) THEN
    XCMOVC = AMINI(XMOVST, XCMOVC + dmovdt)
    IF ( SF2 .GE. SF2R ) XMOVST = XMOV2
    YCMOV = YCMOV * ydt1 + (XCMOVL + XCMOVC) * ydt2
ENDIF

COOLANT CONTROL VALVE

THE CCV OPENING IS MAINLY TIME SCHEDULED
HOWEVER, WHEN T > 2.8 AND FR > 1500, CCV IS PROPORTION TO FR
THE VALVE POSITION IS FULLY OPEN DURING THE MAIN STAGE OPERATION

IF(TIME.LT.TCUT+.5) GO TO 1800
YCCCV=AMAX1(75.-_YCCCV-DCCVI*DTMC)
GO TO 1800

IF ( STIME .LE. TCUT ) THEN
    IF ( FR .GE. 1500. ) THEN
        CCV NOT RATE LIMITED HERE - THRUST SCHEDULED
        IF ( STIME .GT. 2.8 ) THEN
            YCCCV = AMIN1( DFCV*FR + FCCVC, 100. )
        ENDIF
    ELSE IF ( STIME .LT. TCUTCV) THEN
        IF ( STIME .GT. TCCVI ) THEN
            IF ( STIME .GE. TMOVRA) THEN
                212
YCCCV = AMAX1(CCV3, YCCCV - dcc3dt)
ELSE
YCCCV = AMAX1(YCCCV - dcc2dt, CCV2)
ENDIF
ELSE
YCCCV = AMIN1(YCCCV + dccvdt, CCVC)
ENDIF
ELSE IF ( STIME .LT. TMPL + DTMFVR ) THEN
YCCCV = AMIN1 (CCV1, YCCCV + dcc1dt)
ELSE
YCCCV = AMAX1 (.00001, YCCCV - dcc0dt)
ENDIF
ELSE IF ( ICUT .EQ. 1 ) THEN
CCV NOT RATE LIMITED HERE - THRUST SCHEDULED
IF ( STIME .GT. 2.8 ) THEN
YCCCV = AMIN1( DFCCV*FR + FCCVC, 100. )
ENDIF
ELSE IF ( STIME .LT. TCUTCV ) THEN
IF (XCFPOV - XCOPOV .GE. DXCFPO .AND. XOPOV .GT. OPOVPB) THEN
YCCCV = AMAXI (XCCCV0, YCCCV - dcc0dt)
ENDIF
ELSE IF ( STIME .LT. TMPL + DTMFVR ) THEN
YCCCV = AMINI (CCVl, YCCCV + dccldt)
ELSE
YCCCV = AMAXI (.00001, YCCCV - dcc0dt)
ENDIF
C
C MAIN FUEL VALVE
C
C***** MFV OPENING IS MAINLY TIME SCHEDULED AT THE BEGINING
C***** WHEN T > TFRMFV, THE OPENING IS PROPORTIONAL TO FR
C***** HOWEVER, THE VALVE IS FULLY OPEN AT THE MAIN STAGE.
C
IF ( TCUT .GE. 5.0 .OR. STIME .LE. TCUT ) THEN
IF( STIME .GT. TCUTFV ) THEN
SHUT-OFF PROCESS
ENDIF
ELSE IF ( STIME .LT. TMPL + DTMFVR ) THEN
YCMFV = rlimit( FMVM, XMFVM, CMFV + DFMFV * FR )
ELSE
YCMFV = FGEN(55, 90, STIME + DTMC)
213
ENDIF
ENDIF
ELSE
* Open loop operation
*
EPC = 0.
EPCGCL = 0.

C
****
FOLLOWING FOUR LINES ARE ADDED TO SIMULATE PERTURBATION ON THE V
**** OPENINGS AT THE MAIN STAGE.
**** IPFLAG = 0 FOR CLOSED-LOOP CONTROL
**** 1 FOR OPEN-LOOP NO PERTURBATIONS
**** 2 FOR OPEN-LOOP AND PERTURBATIONS ON VALVE OPEN
C ipflag = 2 had not been implemented. Since it involves changing the
* constant setting of the frozen control valve, it was
* implemented in CNTRL0.
*
* YCOPOV = FZOPV * (1 + POPVNZ/100)
* IF(YCOPOV.GE.100.0)YCOPOV = FZOPV was replaced by
*
* YCOPOP = fzopvb
* and invariant operations moved to CNTRL0.
*
* EEMR=0.0
EMRGCL=0.

C
****
FOLLOWING FOUR LINES ARE ADDED TO SIMULATE PERTURBATION ON THE V
**** OPENINGS AT THE MAIN STAGE.
C
* IF (TIME.LT.TOPEN) GO TO 1208
* YCFPOV = FZFPV * (1 + PFPVNZ/100) was replaced,
* IF(YCFPOV.GE.100.0)YCFPOV = FZFPV moving invariant operations to
*1208 CONTINUE
C
YCFPOV = fzycf
C
****
FOLLOWING FOUR LINES ARE ADDED TO SIMULATE PERTURBATION ON THE V
**** OPENINGS AT THE MAIN STAGE.
C
* IF (TIME.LT.TOPEN) GO TO 1488
* YCMOV = FZMOV * (1 + PMOVVNZ/100)
* IF(YCMOV.GE.100.0)YCMOV = FZMOV
*1488 CONTINUE
*
YCMOV = fzycm
C
****
FOLLOWING FOUR LINES ARE ADDED TO SIMULATE PERTURBATION ON THE V
**** OPENINGS AT THE MAIN STAGE.
C
* IF (TIME.LT.TOPEN) GO TO 1888
*
214
* YCCCV = FZCCV * (1 + PCCVNZ/100)
* IF(YCCCV.GE.100.0)YCCCV=FZCCV
*1888 CONTINUE
*
  YCCCV = fzycc
C
C***** FOLLOWING FOUR LINES ARE ADDED TO SIMULATE PERTURBATION ON THE V
C***** OPENINGS AT THE MAIN STAGE.
C
* IF(TIME.LT.TOPEN) GO TO 1588
* YCMFV = FZMFV * (1 + PMFVNZ/100)
* IF(YCMFV.GE.100.0)YCMFV=FZMFV
*1588 CONTINUE
*
  YCMFV = fzymcf
ENDIF
*
* IF(ICCNTL.EQ.2) TIMECP=TIMECP+DTMC
*
  TIMECP = TIMECP + DTMC
C
C***** THESE VALUES ARE TO FREEZE THE OPENINGS OF CONTROL VALVES ****
* Simulation loop invariant perturbations added.
C
IF ( IPFLAG .EQ. 0 .AND. STIME + DTMC .GE. TOPEN) THEN
  FZOPV = YCOPOV
  fzopvb = FZOPV * ( 1. + .01 * POPVNZ )
  IF ( fzopvb .GE. 100.0 ) fzopvb = FZOPV
  FZFPV = YCFPOV
  fzycf = FZFPV * ( 1. + .01 * PFPVNZ )
  IF ( fzycf .GE. 100.0 ) fzycf = FZFPV
  FZMOV = YCMOV
  fzycm = FZMOV * ( 1. + .01 * PMOVNZ )
  IF ( fzycm .GE. 100.0 ) fzycm = FZMOV
  FZMFV = YCMFV
  fzycmf = FZMFV * ( 1. + .01 * PMFVNZ )
  IF ( fzycmf .GE. 100.0 ) fzycmf = FZMFV
  FZCCV = YCCCV
  fzycc = FZCCV * ( 1. + .01 * PCCVNZ )
  IF ( fzycc .GE. 100.0 ) fzycc = FZCCV
  IPFLAG = 1
ENDIF
C
C***** FOLLOWING IS THE SCHEDULE OF HANDLING DIFFERENT INSTRUMENTATION
C***** TIME DELAYS DURING THE SAMPLING TIME PERIOD DTMC (=0.02) OF
C***** CONTROL LOOP.
C
4000 IF ( STIME .GE. TIMEPR .OR. first ) THEN
  PCF = PCFACT * PCIE
  IF ( .NOT. first ) TIMEPR=TIMEPR+DTMC
ENDIF
IF ( STIME .GE. TIMETR .OR. first ) THEN
  TO=TOD2
  IF( .NOT. first ) TIMETR=TIMETR+DTMC
ENDIF

EXECUTION OF VALVE OPENING COMMANDS *************
NOTICE THE OUTPUT COMMANDS ARE USING THE OLD (YCxxVL) VALUES STO
CURRENT CALCUALTED VALUES ARE TO BE SENT OUT IN NEXT TIME INTERV
THE RATE OF CHANGE IS LIMITED TO 200% OPENING/SEC.
* Method changed to eliminate a multiply and divide per value.

IF ( STIME .GE. TIMEVC .OR. first ) THEN
  IF (TIME .GT. TCLF .AND. TIME .LT. TCUT) THEN
    XRFPV = dtm100
  ELSE
    XRFPV = dtm200
  ENDIF

  yxdiff = YCFPVL - XCFPOV
  abdiff = ABS( yxdiff )
  IF ( abdiff .LT. XRFPV ) THEN
    XCFPOV = XCFPOV + SIGN( abdiff, yxdiff )
  ELSE
    XCFPOV = XCFPOV + SIGN( XRFPV, yxdiff )
  ENDIF

  yxdiff = YCOPVL - XCOPOV
  abdiff = ABS( yxdiff )
  IF ( abdiff .LT. dtm200 ) THEN
    XCOPOV = XCOPOV + SIGN( abdiff, yxdiff )
  ELSE
    XCOPOV = XCOPOV + SIGN( dtm200, yxdiff )
  ENDIF

  yxdiff = YCOMVL - XCMOV
  abdiff = ABS( yxdiff )
  IF ( abdiff .LT. dtm200 ) THEN
    XCMOV = XCMOV + SIGN( abdiff, yxdiff )
  ELSE
    XCMOV = XCMOV + SIGN( dtm200, yxdiff )
  ENDIF

  yxdiff = YCCVL - XCCCV
  abdiff = ABS( yxdiff )
  IF ( abdiff .LT. dtm200 ) THEN
    XCCCV = XCCCV + SIGN( abdiff, yxdiff )
  ELSE
    XCCCV = XCCCV + SIGN( dtm200, yxdiff )
  ENDIF

216
yxdiff = YCFMVL - XCMFV
abdiff = ABS( yxdiff )
IF ( abdiff .LT. dtm200 ) THEN
XCMFV = XCMFV + SIGN( abdiff, yxdiff )
ELSE
XCMFV = XCMFV + SIGN( dtm200, yxdiff )
ENDIF
ENDIF

IF(ICCNTL.EQ.2) TIMEVC=TIMEVC+DTMC

IF ( STIME .GE. TIMFMA) THEN
IF(IFIND.EQ.0) IFIND=1
IF(IOIND.EQ.0) IOIND=1
TIMFMA=TIMFMA + DTMC
ENDIF
IF ( STIME .GE. TIMFME ) THEN
TIMFME = TIMFME + DTMC
IF( IFIND .EQ. 3) THEN
NCF=KOUNTF
KOUNTF=0
IFIND=0
ENDIF
IF( IOIND .EQ. 3 ) THEN
NCO=KOUNTO
KOUNTO=0
IOIND=0
ENDIF
ENDIF

*4050 IF(TIME.LT.TIMFMC) GO TO 4060
* TIMFMC=TIMFMC+DTMC

C
C***** QF0, Q0, RHOH, AND RHO0 ARE NEVER USED EXCEPT PRINT-OUTS *****
C
* QF0=67.11*300000./(NCF+1.0E-5) Computations for output only
* Q0=22.95*3000001/(NCO+1.0E-5) are to be done in offline
* RHOH=DENF plotting programs, not in the
* RHO0=DENO simulation
*
4060 IF(TIME.LT.TIMRF) RETURN
C
C***** EMRF IS THE CALCULATED MIX-RATION FROM MEASURED VARIABLES OF
C***** CHAMBER PRESSURE AND FUEL FLOW RATE
C
IF ( STIME .GE. TMRC) THEN
IF (NMR .EQ. i) THEN
EMRF = PCNS / (C2 * DW(2)) - 1.0
ELSE
EMRF = FR / (C2 * DW(2)) - 1.0
ENDIF
ENDIF
ENDIF
ENDIF

* Here is where the KOUNT variables affect the simulation. There is
* an effect only when TIME .GE. TMRC
*
IF ( TIME .LT. TMRC) THEN
  EMRF = 6.0
ELSE IF ( NCO.EQ.0 .OR. NCF.EQ.0) THEN
  EMRF = 0.
ENDIF
F = ( FA1*PCF + FB1*EMRF*PCF +FC1*EMRF +FD1 ) * TFACT
F = AINT(F/512.)*512.
TIMMRF = TIMMRF + DTMC
FCOMP = F
END

* The function TLIMIT was removed. Its interpolation is done by
* fgen. Its data was reconstructed from the interpolation
* coefficients below.

FUNCTION TLIMIT(FR,OXPLIM,XOPOMS,YCOPOV,NMR)

PURPOSE: COMPUTE THE OPOV COMMAND LIMITS USING FLIGHT 38 - MERGE

C*****ARGUMENTS*****
C INPUT:
C FR = COMMAND PC
C XOPLIM = MAXIMUM OPOV POSITION ALLOWED
C XOPOMS = VALUE OF OPOV POSITION AT RPL (NOMINALLY 65%)
C YCOPOV = CONTROLLER COMMAND VALUE OF XOPOV BEFORE LIMITING
C NMR = FLAG TO SELECT METHOD OF MIXTURE RATIO COMputation

C OUTPUT:
C TLIMIT = LIMITED YCOPOV

**********************************************************************
C
DIMENSION EPLTAB(11), A1TAB(11), A0TAB(11)

SM10100

DATA EPLTAB/ 0.0, 70.0, 75.0, 80.0, 85.0, 90.0, 95.0, 100.0, 105.0,110.0,1000./
DATA A1TAB / 0.0, .100, .118, .218, .340, .414, .428, .447, .689,1.564,3.722/
DATA A0TAB / 0.0,49.55,48.29,40.79,31.03,24.74,23.48,21.71, -2.57,-94.4,-331.78/
DATA M / 8 /

The y value is available from the interpolation coefficients
* a0(i), a1(i) as y(i-1) = a0(i) + a1(i) * x(i-1)
* where x = EPLTAB and y = TLIMIT:
*
* TLIMIT = 49.55, 56.55, 57.14, 58.23, 59.93, 62.0, 64.18,
* 66.33, 69.82, 77.64, 3390.
*
* TLIMIT vs. EPLTAB was put in 'ssme.dat', as fcn # 84, after
* fcn #57

'emco.for':

SUBROUTINE EMCO0

******************************************************************************
C
C PURPOSE: COMPUTE ACTUATOR POSITIONS DURING PNEUMATIC SHUTDOWN
C DURING THE EMERGENCY CUT-OFF THE VALVE COMMANDS HAS A SPECIAL
C CIRCUIT FOR SEQUENTIALLY SHUT-DOWN (OR OPEN) THE VALVES.
C
C !!!!! THIS PORTION OF PROGRAM HAS NOT BEEN CHECKED OUT BECAUSE OF THE LACK
C !!!!! OF DOCUMENT ON THE ACTUAL SHUT-DOWN PROCEDURE AND DYNAMICS
C
C******ARGUMENT******
C INPUT:
C N = INITIALIZATION ARGUMENT was eliminated
C
C******COMMON USAGE******
C INPUT:
C
2   HKT2(5), HKL2(5), CKT3(5), CKL3(5), HKT3(5), HKL3(5), HTO(5, 3), W2 (3)
3   , H2(3), H3(3), ORFMAX(3), ORFMIN(3), TOMAX(3), TOMIN(3), PNFRIC(3)
4   , PNLOAD(3), PNORGX(3), PKN(3), WTO(3), Y(5), A0(5), PHID(5), X2DOT(5)
5   , FY1(5), FY2(5), X1DOT(5), II(5), XI(5), DY(5)
6   , N1(5), PIN(5)
7   , W(5), DEN(5), PD(5), A4(5)

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* KT0(5), K3
DIMENSION XP(5), VGI(5), XHE(5)
LOGICAL JK(5)
REAL dmesq(5), twod(5), sqm(5), slx(5)
*
PARAMETER ( PI = 3.141597, degprd = 180. / PI,
+ vperi = 8.0/(386.1 * PI ) )
*
INCLUDE 'blank.com'
INCLUDE 'units.com'
INCLUDE 'contrl.com'
INCLUDE 'oxid.com'
INCLUDE 'hgas.com'
*
DATA I1/11,14,16,32,36/
DATA JK, FY1, FY2, D1, D2/ 5 *.TRUE., 10*0., -1.085, 1.02/
**************************************************************************
*
CALL fgset( 34 )
CALL fgset( 35 )
CALL fgset( 11 )
CALL fgset( 14 )
CALL fgset( 16 )
CALL fgset( 32 )
CALL fgset( 36 )
FR = fgen( 36, 108, 100. )
*
READ(run,10) PHE, PR, FRDEL, FS, TL,
+ TEMP, PCT,( A1(I), A2(I), I=1,5 ),
+ A3, B1, S, L, M, D, E,
+ MU, CKT1, CKL1, HKT1, HKL1, CKT2, CKL2, HKT2, HKL2, CKT3, CKL3, HKT3, HKL3,
+ ( (HTO(I,J), I=1,5 ), J=1,3 ),
+ W2, H2, H3, ORFMAX, ORFMIN, TOMAX, TOMIN,
+ PNFRIC, PNLOAD, PNORGX, PNK, WTO,
+ TSFPV, TSMOV, TSMFV,
+ (AT(I),I=1,5), (BT(I),I=1,5),
3, (CS(I),I=1,5), (CPS(I),I=1,5), (DSS(I),I=1,5), 4,
4, (ESS(I),I=1,5), (VPD(I),I=1,5), (A4(I),I=1,5)
10 FORMAT (//2X,6g12.4)
**TIMETR=0.0**

**TPT=TPA**
**PRC=PR**
**FPB=PHE**

**TEMP IS THE TEMPERATURE INDICATOR, 1=COLD, 2=NORMAL, 3=HOT**

```
TIMETR=0.0
TPT=TPA
PRC=PR
FPB=PHE

TEMP IS THE TEMPERATURE INDICATOR, 1=COLD, 2=NORMAL, 3=HOT

IF(TEMP.LE.1.0) GAM=SQR(0.86158)
IF(TEMP.EQ.2.0) GAM=SQR(0.83974)
IF(TEMP.EQ.3.0) GAM=SQR(0.7895)
IT=TEMP+0.1
G2=4.*146.2*.62*W2(IT)*H2(IT)/GAM
W3=(ORFMAX(IT)-ORFMIN(IT))
K3=4.*146.2*.62*W3*H3(IT)/GAM
XV=(PPB*.1398-PR*.1398-PNFRIC(IT)-6.0*PNLOAD (IT)-6.0*PNORGX(IT)
1.*PNK(IT))/(PNK(IT)*6.0)
IF(XV.LT.0.) XV=1.E-5
IF(XV.GT.WTO(IT)) XV=WTO(IT)
G3=(K3*(XV-ORFMIN(IT)))/(ORFMAX(IT)-ORFMIN(IT))
IF(XV.LT.ORFMIN(IT))G3=0.000001
IF(XV.LT.ORFMIN(IT))G2=0.00001
IF(XV.GE.ORFMAX(IT))G3=K3
GE=SQR(1.)/((1./G3)**2+(1./G2)**2))

1 = FPOV
2 = OPOV
3 = MOV
4 = MFV
5 = CCV

DO 720 I=1,5
   KT1(I)=CKT1(I)
   KL1(I)=CKL1(I)
   KT2(I)=CKT2(I)
   KL2(I)=CKL2(I)
   KT3(I)=CKT3(I)
   KL3(I)=CKL3(I)
   IF( TEMP .GE. 2.0 ) THEN
     KT1(I)=HKT1(I)
     KL1(I)=HKL1(I)
     KT2(I)=HKT2(I)
     KL2(I)=HKL2(I)
     KT3(I)=HKT3(I)
     KL3(I)=HKL3(I)
   ENDIF
CG0 = ( D(I)**2 + M(I)**2 + L(I)**2 - E(I)**2 ) /
      + ( 2.*D(I)*SQR( M(I)**2 + L(I)**2 ) )
SG0 = SQR(1. - CG0**2)
GA0 = ATAN2(SG0,CG0)
```

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BE0 = ATAN( M(I) / L(I) )
A0(I) = PI - GA0 - BE0
KTO(I) = 146.2*.62*HTO(I,IT)/GAM
XHE(I)=0.
IF( XV .LE. TOMIN(IT) ) THEN
  vG1(I) = 1.E6
ELSEIF ( XV .GT. TOMAX(IT) ) THEN
  vG1(I) = 1.0 / ( KTO(I)*(TOMAX(IT) - TOMIN(IT) ) )
ELSE
  vG1(I) = 1.0 / ( KTO(I)*(XV - TOMIN(IT) ) )
ENDIF
720 CONTINUE
DO 5 I = 1, 5
  Y(I) = THETA(I) / PCT(I)
  DY(I) = -1.0E-5
  CALL unint0( Y(I), 198 + I )
  X2DOT(I) = DY(I)
  X1DOT(I) = DY(I)
  XI(I) = Y(I)
  dmesq(I) = D(I)**2 + M(I)**2 - E(I)**2
  twod(I) = 2. * D(I)
  sqm(I) = M(I)**2
  slx(I) = L(I) + S(I) - XI(I)
5 CONTINUE
RETURN
ENTRY EMCO

******************************************************************************************
1000 CONTINUE
PIN(1)=PFPOV
PIN(2)=POPOV
PIN(3)=PMOV
PIN(4)=P(3)
PIN(5)=P(7)
W(1)=DWFPO
W(2)=DWOPO
W(3)=DWMOV
W(4)=DW(3)
W(5)=DW(7)
DEN(1)=RHOOP3
DEN(2)=RHOOP3
DEN(3)=RHOOP2
DEN(4)=RHO(3)
DEN(5)=RHO(7)
PD(1)=PFPOI
PD(2)=POPOI
PD(3)=POINJ
PD(4)=P(10)
PD(5)=P(8)
XP(1) = .01 * XFPOV

******************************************************************************************
XP(2) = .01 * XOPOV
XP(3) = .01 * XM0V
XP(4) = .01 * XM0V
XP(5) = .01 * XCMV
X1D0T(5) = DTHETA(5)

DO 2000 I = 1, 5

* IF (I.EQ.1.AND.THETA(2).GT.TSFPOV) GO TO 2000
* IF (I.EQ.3.AND.THETA(2).GT.TSMOV) GO TO 2000
* IF (I.EQ.4.AND.TIME.LE.TSMFV) GO TO 2000
* IF (I.EQ.5.AND.TIME.LE.TSMFV) GO TO 2000 requires too many tests of I

GO TO ( 15, 50, 20, 40, 40 ), I

15 IF ( THETA(2) .GT. TSFPOV ) GO TO 2000
GO TO 50

20 IF ( THETA(2) .GT. TSMOV ) GO TO 2000
GO TO 50

40 IF ( STIME.LE.TSMFV ) GO TO 2000
50 CONTINUE

* IF ( N1(I) .EQ. 0 ) GO TO 422
*     Y(I) = THETA(I) / PCT(I) Moved to EMCO
*     DY(I) = -1.0E-5
*     X2DOT(I) = DY(I)
*     X1D0T(I) = DY(I)
*     X1(I) = Y(I)
*     N1(I) = 1
 *
IF (Y(I) .LE. 0.) GO TO 2000
X2 = Y(I)

CG = (D(I)**2 + M(I)**2 + (L(I) + X2)**2 - E(I)**2) / (2*D(I)*SQRT(M(I)**2 + (L(I) + X2)**2)) was replaced by

x21 = X2 + L(I)
x21sq = x21 ** 2
vdenBE = 1. / X10th( sqm(I) + x21sq, 5 )
CG = ( dmesq(i) + x21sq ) * vdenBE / twod(I)

SG = X10th( 1. - CG**2, 5 )
GA = ATAN2(SG, CG)
BE = ATAN( M(I)/x21 )
A = PI - GA - BE
PHI = A - A0(I)
PHID(I) = degprd * PHI

* IF( X2DOT(I) .EQ. 0. ) THEN
  TP = 0.
ELSE

223
THK=FGEN(I1(I),2,XP(I)/100.)
THK = fgen( I1(I), I + 103, xp(I) )

TP = SIGN( AT(I) + ( BT(I) + 0.8*ESS(I) ) * ( PIN(I) - vperi/DEN(I)*( W(I)/VPD(I)**2 )**2 ) + 0.8*DSS(I) + CPS(I) + CS(I)*( PIN(I) - PD(I) ) , X1DOT(I)) + THK*W(I)**2/DEN(I)/VPD(I)/1728. was replaced by

THK = fgen( I1(I), I + 103, xp(I) )
TP = SIGN( AT(I) + ( BT(I) + 0.8*ESS(I) ) * ( PIN(I) - vperi/DEN(I)*W(I)/VPD(I)**2 )**2 ) + 0.8*DSS(I) + CPS(I) + CS(I)*( PIN(I) - PD(I) ) , X1DOT(I)) + THK*W(I)**2/DEN(I)/VPD(I)/1728. 

ENDIF

FB1=MU(I)*ABS(FY1(I))
FB2=MU(I)*ABS(FY2(I))

BV1 = B1(I)*.5
BV2 = BV1

IF(ABS(X2DOT(I)).LT..9E-4) JK(I)=1
JK(I) = JK(I) .OR. X2DOT(I) .LT. .9E-4
IF( JK(I) ) THEN
FRIC1 = -SIGN( FS(I)*.5, X2DOT(I) )
FRIC2 = FRIC1
ELSE

IF(I.LT.3.OR.I.EQ.5) FR=FGEN(34,2,PHID(I)) Why lookup twice for I = replaced by
IF(I.GT.2)FR=FGEN(35,2,PHID(I))

IF( I .LT.3 ) THEN
FR = FGEN( 34, 108 + I, PHID(I) )
ELSE
FR = FGEN( 35, 108 + I, PHID(I) )
ENDIF
FR = FR + FRDEL(I)
FRIC1 = -SIGN(FR*.5, X1DOT(I) )
FRIC2 = -SIGN(FR*.5, X2DOT(I) )

ENDIF

SINA=SIN(A) 
COSA=COS(A) replaced by

sinBE = M(I) * vdenBE
cosBE = x21 * vdenBE
SINA = SG * cosBE + CG * sinBE
COSA = SG * sinBE + CG * cosBE

U1 = D(I) * SINA
U2 = -.5*(E(I)**2-(M(I)-U1)**2)**(-.5)*(-2.*(M(I)-UI)*(-D(I)*COSA)) replaced by
dmul = M(I) - U1
U2 = -.5 / X10th( E(I)**2 - dmul**2, 5 ) * twod(I) * dmul * COSA

224
UA = (U1 + U2) / (U1 - U2)

* TAND1 = dmul / ( slx(I) - D(I)*COSA )
TAND2 = dmul / ( D(I)*COSA + x21 )
XDHE = -X2DOT(I)
XHE(I) = S(I) - X2
SIGN1 = SIGN(1., X2DOT(I) )
Q1 = A1(I) * X1DOT(I)
Q2 = A2(I)*X2DOT(I) + A4(I)*XDHE
IF ( XV .LE. TOMIN(I) ) Q1=0.
IF ( XV .LE. ORFMIN(I) ) Q2=0.
Q3 = Q2 - Q1
PR1 = ( KT3(I)*ABS(Q3) + KL3(I) )*Q3 + PR
C1 = ( KT1(I)*ABS(Q1) + KL1(I) )*(-Q1)
C2 = ( KT2(I)*ABS(Q2) + KL2(I) )*Q2
P1 = PR1 - SIGN1*( A1(I)*X1DOT(I)*vG1(I) )**2
IF( XV .LE. .046) THEN
  P2 = PHE
ELSE
  P2 = SIGN1*( ( A2(I) - A4(I) )*X2DOT(I) )*vGE)**2 + PR1
ENDIF
D1 = -TAND1*D(I)*COSA - U1
vD2 = 1.0 / ( U1 - TAND2*D(I)*COSA )
FX1 = ( P1 + C1 - PRC )*A1(I) + FRIC1 - BV1*X1DOT(I)
FX2 = ( TP + FX1*D1 )*vD2
FY1(I) = -FX1 * TAND1
FY2(I) = FX2 * TAND2

X (I)**2)*SIGN1
* VB=-BV2-D1/D2*(-BV1*UA)
* VC=-PR1+C2)*(A2(I)-A4(I))-PHE*A3(I)+FRIC2-1./D2*(TP(I)+D1*(A1(I)*
  X PR1+C1*A1(I)+FRIC1-PRC*A1(I)))+PRC*A2(I)
* VA = ( ( A2(I) - A4(I) )*2 * vGE)**2 +
  + D1*vD2*( A1(I)*( A1(I)*UA*vG1(I) )**2 )*SIGN1
  SSM13400
VB = D1*vD2*BV1*UA - BV2
VC = FRIC2 - (PR1 + C2)*( A2(I) - A4(I) ) - PHE*A3(I)
+ - vD2*( TP + D1*( A1(I)*(PR1 + C1 - PRC) + FRIC1 ) )
+ + PRC*A2(I)
VRAD = VB**2 - 4.*VA*VC
IF ( VRAD .GE. 0. ) THEN
  X2DOT(I) = ( -VB - SQRT(VRAD) )/(2.*VA)
  DY(I) = X2DOT(I)
  PHIDOT = X2DOT(I) / (U1 - U2) * degprd
  X1DOT(I) = UA * X2DOT(I)
  X1(I) = - twod(I)*COSA + S(I) - X2
  THETA(I) = PHID(I)
  DTHETA(I) = PHIDOT
  Y(I) = pruint( DY(I), Tstep, 198 + I )

225
JK(I) = .FALSE.
ELSE
1500 WRITE(event, 1510) STIME, I
1510 FORMAT(' AT ',F10.4,' VALVE',I3,' MOVING IN WRONG DIRECTION')
ENDIF
2000 CONTINUE
RETURN
END
PURPOSE: SIMULATE POGO SUPPRESSOR OPERATION

POGO SUPPRESSOR SYSTEM IS THE "STABILIZER" OF THE OXIDIZER SYSTEM. IT USES THE PRESSURIZED HELIUM SYSTEM TO SUPPLY ENOUGH OXID LINE PRESSURE AT THE BEGINNING OF THE OPERATION. A BACKFLOW LINE IS ALSO USED TO DRAIN THE OVERFLOW OF THE EXCESS OXIDIZER DURING THE OPERATION.

POGO SYSTEM HAS THREE DUCTS/VALVES CONNECTED:
- OI2: HOPO INPUT DUCT, DOWN SIDE OF THE POGO ACCUMULATOR
- RIV TUBE: OVERFLOW TUBE BACK TO OXID TANK
- DIFFUSER VALVE: INPUT VALVE FOR EITHER PRESSURIZED HELIUM OR PRESSURIZED LOX FROM HPOP OUTLET.

ARGUMENT

INPUT:
- I = INITIALIZATION ARGUMENT inactivated

COMMON USAGE

INPUT:
- VARIABLES SOURCE
  - PDI2, PDD2, POJ

OUTPUT:
- VARIABLES DESTINATION
  - DWO, DWGOP, OWHOP

DOUBLE PRECISION TIME replaced by STIME

INCLUDE 'blank.com'
INCLUDE 'pogo.com'
INCLUDE 'oxid.com'

PARAMETER ( NPTS = 4, MPTS = 12 )
DIMENSION WGTAB(NPTS), FACTAB(NPTS), PGTAB(MPTS), SATTAB(MPTS), + SATvPG(MPTS), FACvWG(NPTS)

INTEGER Tstep
PARAMETER ( Tstep = 0, TooBig = 1.E50 )
PARAMETER ( workc = 12.0 * 778.16 )

DATA WGTAB / 0.0 , 0.2 , 0.3 , 1.0 / SSM80900
DATA FACTAB / 0.0 , 0.2 , 0.9 , 1.0 / SSM80900
DATA PGTAB / 0.022 , 6.7 , 20.2 , 52.6 , 98.5 , 148.2 , 201.7 , 298.2 , 404.2 , 511.5 , 611.9 , 731.38 /
+ 97.831 , 150.0 , 168.0 , 186.0 , 204.0 , 216.0 ,
+ 226.0 , 240.0 , 252.0 , 262.0 , 270.0 , 278.24 /
DATA DTPSTH / 4.0 /
DATA DTPSTL / 0.0 /
DATA QINT / 0.01792 /
DATA QNCON / 955.5 /
DATA QNEXP / 2.006 /
DATA QSLP / 0.00491 /
DATA TGOX / 650.0 /
DATA THE / 520.0 /
DATA THTHI / 2.0 /
DATA THTLO / 1.4 /
DATA TLOX / 180.0 /

* Is Z below a function of the step size? If so, compute it so step size can be changed. *
* DATA Z / 0.0005 /

C
R(X)=I./(772.8*X*X+1.0E-12)

DQHEAT=0.0
ISAVE = 1
JSAVE = 1
TSAT=0.0
WLOX=0.0
WORK=0.0
X=0.0

C
READ (run,50) ATH, AIN, AHPV, AGC, RGC, RS, RGHS, RREC, ZREC, HP, + PHS, TGC, THEO, RHS, THEC, RGVO, ZCD, RGSL, VTOT, + RHPV, DTPSTL
50 FORMAT(//2X,6G12.4)

P1=POI2
P2 = POI2
PD = POI2

* TPRINT = TPR(1) - 0.1 * DT replaced by one print interval
* Input echo eliminated.
* CALL fgset( 42 )
CALL fgset( 43 )
*
DO 60 I = 2, MPTS
   SATvPG(I) = ( SATTAB(I) - SATTAB(I-1) ) / + ( PGTAB(I) - PGTAB(I-1) )
60 CONTINUE
DO 70, I = 2, NPTS
   FACvWG(I) = ( FACTAB(I) - FACTAB(I-1) ) / + ( WGTAB(I) - WGTAB(I-1) )
70 CONTINUE

228
CONTINUE
*
  dwfac2 = 500. * DT
IF ( dwfac2 .LE. 1.0 ) THEN
  dwfac1 = 1.0 - dwfac2
ELSE
  PRINT *, "Time step assumed less than 1/500 in pogosup."
  STOP
END

tgox5 = 579.5 * TGOX
rhfac2 = 20. * DT
rhfac1 = 1. - rhfac2
*
CALL imint0( XHPV, 204, 0.0, 100.0 )
CALL imint0( XGC, 205, 0.0, 100.0 )
CALL unint0( UG, 206 )
CALL imint0( WLOX, 207, 0.00001, TooBig )
CALL imint0( WGOX, 208, 0.00001, TooBig )
CALL imint0( WHE, 209, 1.0E-08, TooBig )
CALL unint0( DWO, 210 )
CALL unint0( DWGAS, 211 )
CALL unint0( PD, 212 )
CALL unint0( DWRE, 213 )
*
The following restart section is added to initialization.
*
vrHOHE = 4636.0 * THE / PHES
TGAS = 470.0
WLOX = 16.24
WGOX = 1225.0 * POI2 / (579.5 * TGAS)
WHE = 25.0 * POI2 / (4636.0 * TGAS)
UG = TGAS * (0.17811 * WGOX + 0.74824 * WHE)
RHOREC = 0.01
IPR = 2
*
RETURN
*
ENTRY POGO
*******************************************************************************
C COMPUTE GAS FLOWRATES INTO THE POGO ACCUMULATOR
C * COMPUTE VALVE POSITIONS
C
C VALVE OPENING SCHEDULE TIMES ARE:
C THEO: HELIUM VALVE OPENING TIME
C THEC: HELIUM VALVE CLOSING TIME
C TCUT: SYSTEM POWER CUT DOWN TIME
C DTPSTL: SYSTEM POWER CUT TO PURGE DELAY
C DTPSTH: TIME PERIOD OF HELIUM PURGE DURING POWER CUT DOWN

229
C TGC: LOX VALVE OPENING TIME, THIS WORKS WITH "THEC"
C XGC: VALVE OPENING OF LOX FLOW BACK FROM "OD2" DUCT, % OF AREA
C XHPV: VALVE OPENING OF PRESSURIZED HELIUM SYSTEM, % OF AREA
C (NOTE: XGC AND XHPV VALVES OPEN EXCLUSIVELY.)

IF ( STIME .LT. THEO 
   + .OR. ( STIME .GT. THEC .AND. STIME .LT. TCUT + DTPSTL ) 
   + .OR. STIME .GT. TCUT + DTPSTH ) THEN SSM82100
C
C TIME PERIODS WHEN HELIUM FLOWS ARE NOT EXISTING, START OR MAIN STAGE

XHPV = prlint( - RHPV, Tstep, 204 )
IF (XHPV .GT. 0.2) GO TO 260
IF (STIME .GT. TGC) THEN
   XGC = prlint( RGC, Tstep, 205 )
ENDIF
IF (XGC .GT. 0.01) GO TO 300
IF (XHPV .LE. 0.01) THEN
   DWG = 0.0
   DWH = 0.0
   GO TO 400
ENDIF
ELSE SSM82200
C
C TIME PERIODS WHEN HELIUM FLOWS DOMINATE, DURING START OR PURGE

XGC = prlint( - RGC, Tstep, 205 )
IF (XGC .GT. 0.2) GO TO 300

* Do you really want to skip the integration of XHPV in this case?

XHPV = prlint( RHPV, Tstep, 204 )
ENDIF
*
* * * * COMPUTE HELIUM FLOWRATE INTO ACCUMULATOR
*
C HELIUM FLOW INTO ACCUMULATOR, GOX FLOW MUST BE ZERO (OR ALMOST ZERO).
C THE FOLLOWING SECTION OF PROGRAM CALCULATE THE HELIUM FLOW BY:
C 1) COMPUTE INITIAL FLOW VALUE WHEN XHPV < 0.2%
C 2) WHEN XHPV > 0.2%, USES THE SMOOTHING FACTOR OF 500*DT=0.1 TO
   CALCULATE THE NEXT FLOW VALUE: DWH(NEXT)=0.9*DWH(OLD)+0.1*DWH(IN)
   (500*DT CAN BE CONSIDERED AS THE TIME DELAY OF THE DUCT.)
C FOLLOWING NOTATIONS ARE USED:
C PHES: HELIUM SYSTEM PRESSURE
C P1: PRESSURE OF JUNCTION OF HELIUM DUCT AND GOX DUCT
C P2: PRESSURE BEFORE THE DIFFUSER
C PGCO: PRESSURE AFTER THE GOX VALVE
C PG: POGO SYSTEM PRESSURE
C DWG: GOX FLOW INTO THE DIFFUSER
C DWH: HELIUM FLOW INTO THE DIFFUSER

230
C

260 RAHPV = R(XHPV * AHPV / 100.0)
   IF (XHPV .LT. 0.2) THEN
     DWH = SQRT(ABS(PHES - P1) / (VRHOHE * RAHPV))
   ENDIF
   dwsr = VRHOHE * DWH ** 2
   PHPV = PHES - RHS * dwsr
   P1 = PHPV - RAHPV * dwsr
   IF (P1 .LT. P2) P1 = P2
   PGCO = P1
   DWG = 0.0
   DWH = dwfac1 * DWH +
     dwfac2 * AIN * GFLOW(P1, P2, P1*VRHOHE, 1.0, 1.684)
   P2 = PG + RGH5 * DWH ** 2 * VRHOHE
   GO TO 400
*
* * * * COMPUTE GOX FLOW INTO THE ACCUMULATOR
*

THIS IS THE FLOW FROM DUCT "OD2" TO THE DIFFUSER IN GAS OXID FORM TO
SUPPLY PRESSURE FOR POGO SYSTEM DURING THE MAIN STAGE OPERATION.
GAS OXID FLOW INTO ACCUMULATOR, HELIUM FLOW MUST BE ZERO (OR ALMOST ZERO
THE FOLLOWING SECTION OF PROGRAM CALCULATE THE HELIUM FLOW BY:
1) COMPUTE INITIAL FLOW VALUE WHEN XGC < 0.2%
2) WHEN XGC > 0.2%, USES THE SMOOTHING FACTOR OF 500*DT=0.1 TO
   CALCULATE THE NEXT FLOW VALUE: DWG(NEXT)=0.9*DWG(OLD)+0.1*DWG(IN)
   (500*DT CAN BE CONSIDERED AS THE TIME DELAY OF THE DUCT.)
FOLLOWING NOTATIONS ARE USED:
PCCI: PRESSURE OF OUTPUT SIDE OF THE RETURING GOX VALVE
PGCO: PRESSURE OF OUTPUT SIDE OF THE RETURING GOX VALVE

300 RAGCV = R(XGC * AGC / 100.0)
   VRHOGO = tgox5 / POD2
   IF (XGC .LT. 0.2) THEN
     DWG = SQRT(ABS(POD2 - P1) / (VRHOGO * RAGCV))
   ENDIF
   dwgr = VRHOGO * DWG ** 2
   PCCI = POD2 - RGH5 * dwgr
   PGCO = PCCI - RAGCV * dwgr
   P1 = PGCO - RGV5 * dwgr
   IF (P1 .LT. P2) P1 = P2
   IF (PGCO .LT. P1) PGCO = P1
   DWH = 0.0
   DWG = dwfac1 * DWG + dwfac2 *
     GFLOW(P1, P2, P1/RHOGOS, 1.0, 1.4) * AIN
   P2 = PG + RGH5 * DWG ** 2 * VRHOGO
C
C COMPUTE PROPERTIES IN THE ACCUMULATOR

C PROPERTIES IN THE ACCUMULATOR IS DEFINED BY THE FOLLOWING:
C UG:  TOTAL ENERGY OF THE GAS PHASE IN THE ACCUMULATOR

231
DQHEAT: HEAT TRANSFERRED BETWEEN LOX AND GAS PHASE
WORK: WORK DONE BY GAS PHASE IN PUSHING LOX (= P * Delta V)

DWLOX: LOX FLOW INTO THE ACCUMULATOR, INCLUDING:
DWQ: LOX FLOW FROM DUCT "012"
DWQNCH: LOX FLOW FROM GAS PHASE DUE TO QUENCHING EFFECT

DWLO: LOX FLOW FROM THE ACCUMULATOR TO OXID TANK

DWORD: GAS OXID FLOW INTO THE ACCUMULATOR, INCLUDING:

DWG: GAS OXID INPUT FROM "0D2" THROUGH XGC VALVE
DWQNCH: GAS FLOW TO LIQUID PHASE DUE TO QUENCHING EFFECT

DWGOP: GAS FLOW TO DUCT "012"

DWGO: GAS FLOW TO OXID TANK IN BACK FLOW TUBE

DWHE: HELIUM FLOW INTO THE ACCUMULATOR, INCLUDING:

DWH: HELIUM FLOW FROM HELIUM SUPPLY THROUGH XHPV VALVE
DWHO: HELIUM FLOW TO DUCT "012"

400 DLTUG = 1.24471 * (DWH * THE - (DWHOP + DWHO) * TGAS)
1 + 0.24017 * (DWG * TGOX - (DWGOP + DWQNCH + DWGO) * TGAS)
2 +DQHEAT - WORK

UG = pruint( DLTUG, Tstep, 206 )

DWLOX = DWO + DWQNCH - DWLO

WLOX = prlinit( DWLOX, Tstep, 207 )

DWGOX = DWG - DWQNCH - DWGOP - DWGO

WGOX = prlinit( DWGOX, Tstep, 208 )

DWHE = DWH - DWHOP - DWHO

WHE = prlinit( DWHE, Tstep, 209 )

VL = WLOX / 0.04061
VG = AMAX1(1.0, VTOT - VL)

TGAS = UG / (0.17811 * WGOX + 0.74824 * WHE)

PG = (579.5 * WGOX + 4636.0 * WHE) * TGAS / VG
RHOHE = PG / (4636.0 * TGAS)
RHOGOX = PG / (579.5 * TGAS)

COMPUTE FLOWRATES

FLOWRATES AT THE ACCUMULATOR NECK

THIS SECTION IS TO CALCULATE THE CONDITIONS OF THE LIQUID AND GAS FLOW
OF THE POGO SYSTEM. FOLLOWING NOTATIONS ARE USED:

ALIQ: FRACTION OF THE LOX IN THE DUCT BETWEEN "012" AND NECK
ALIQ=1 FOR LOX FILLED DUCT, ALIQ=0 FOR GOX FILLED DUCT, AND
0<ALIQ<1 FOR PARTIALLY FILLED DUCT

FAC: DIFFUSING FACTOR TO CALCULATE GAS FLOW IN A GAS MIXTURE

ALIQ = AMAX1(1.0E-10, AMIN1(1.0, VL/130.6))

DWO = prflow(DWO, Z, -RS/(RHOC2*ALIQ**2), POI2-PG, 210)

* The translation below is accurate, but the intent is doubted.

IF (VL .GE. VTOT - 1.0 .AND. DWO .GE. 0.0) THEN

CALL unint0( 0., 210 )

232
DWO = 0.0
PG = POI2
ENDIF
500 IF (ALIQ .GE. 0.9999) THEN
   DWGOP = 0.0
   DWHOP = 0.0
ELSE
   THE CONDITION OF PARTIALLY FILLED DUCT BETWEEN "OI2" AND POGO NECK.
   DWGAS: TOTAL GAS FLOW (HELIUM AND GOX)

   wgx = WGOX/AMAX1(1.0E-12, WGOX+WHE)
   CALL intval( ISAVE, wgx, NPTS, WGTAB, 
               + 'Below WG table in pogosup.',
               + 'Above WG table in pogosup.', 0 )
   FAC = xlint( wgx, NPTS, WGTAB, FACTAB, FACvWG, ISAVE )  SSM82800

   RHOG = PG / (TGAS * (579.5 * FAC + 4636.0 * (1.0 - FAC)))
   DWGAS = prflow(DWGAS, Z, RS/RHOG*(1.0-ALIQ)**2), PG-POI2, 211)
   IF (WHE .GE. 1.0E-07) THEN
      DWGOP = FAC * DWGAS
      DWHOP = (1.0 - FAC) * DWGAS
   ELSE
      DWGOP = DWGAS
      DWHOP = 0.0
   ENDIF
ENDIF

* *
* * * * COMPUTE THE FLOWRATES OUT THE RIV TUBE  SSM82900
*
*
C BACK FLOW TUBE CONDITIONS:
C HP: LOX HEIGHT IN POGO ACCUMULATOR
C AREAH: LOX AREA INSIDE BACK FLOW TUBE (RIV TUBE)
C DWDUM: GAS FLOW OF RIV TUBE, (WHEN AREAH < ATH)
C PD: PRESSURE OF THE DUCT OF RETURNING LOX, BEFORE CHECK VALVE
C DWRE: RECIRCULATING FLOW INTO OXID TANK

700 HP = FGEN(42, 119, VL)
    AREAH = FGEN(43, 120, HP)
    DWDUM = GFLOW(PG, PD, PG*VG/(WHE+WGOX), 1.0, 
                 1 (1.684*WHE+1.4*WGOX)/(WHE+WGOX)) * AMAX1(0.0, ATH-AREAH)
    IF (WHE .GE. 1.0E-07) THEN
      DWGO = DWDUM * WGOX / (WHE + WGOX)
      DWHO = DWDUM - DWGO
    ELSE
      DWGO = DWDUM
      DWHO = 0.0
    ENDIF

800 DWLO = SIGN(SQRT(ABS(PG-PD) * RHOCd2 / R(AREAH)), PG-PD)
    PD = pruint( (DWDUM + DWLO - DWRE) / ZCD, Tstep, 212 )

233
CALCULATING RECIRCULATING DUCT DENSITY USING TIME AVERAGE 20*DT(=.004)
LOOKS LIKE THE DUCT IS VERY HUGE AND TAKES LONG TIME TO FILL

\[
\text{RHOREC} = \text{rhfac1} \times \text{RHOREC} + \text{rhfac2} \times \left( \frac{\text{ABS(DWLO} + \text{DWGO} + \text{DWHO})}{\text{AMAX1} \left( \frac{\text{ABS(DWLO}}}{\text{RHOC2}} + \frac{\text{DWGO}}{\text{RHOGOX}} + \frac{\text{DWHO}}{\text{RHOHE}}, 0.00001 \right)} \right)
\]

\[
\text{DWRE} = \text{prflow}(\text{DWRE}, \text{ZREC}, -\text{RREC/RHOREC}, \text{PD-POJ}, 213)
\]

* * * COMPUTE HEAT TRANSFER AND LOX QUenchING

DQHEAT IS THE HEAT FLOW FROM LOX TO GAS. AS TO WHY IT IS A FUNCTION OF IS UNKNOWN.

\[
\text{DQHEAT} = (\text{QSLP} \times \text{AMAX1(DW0, 0.0)} + \text{QINT}) \times (\text{TLOX} - \text{TGAS})
\]

IF (TIME .GT. THTHI) GO TO 860

STIME=TIME SSM83100

DQHEAT = DQHEAT * AMAX1 (0.0, (STIME-THTLO) / (THTHI-THTLO))

860 CONTINUE .sequence replaced by

IF ( STIME .LE. THTHI ) THEN

DQHEAT = (QSLP * AMAX1(DWO, 0.0) + QINT) * (TLOX - TGAS)
ELSE

DQHEAT = DQHEAT * AMAX1 (0.0, (STIME-THTLO) / (THTHI-THTLO))

ENDIF

TSAT: THE SATURATING TEMPERATURE UNDER THE PRESSURE PG.

CALL intval( JSAVE, PG, MPTS, PGTAB,
+ 'The pressure PG is below SATTAB in pogosup.',
+ 'The pressure PG is above SATTAB in pogosup.', 0 )

TSAT = xlint( PG, MPTS, PGTAB, SATTAB, SATvPG, JSAVE )

\[
\text{DWQNCH} = \text{WGOX} \times \text{QNCON} \times \text{XtoY} (\text{AMAX1(1.0, TGAS-TSAT)}, -\text{QNEXP})
\]

WORK = -PG \times (\text{DWO} + \text{DWQNCH} - \text{DWLO}) / (\text{workc} \times \text{RHOC2})

Eliminated PRINT OUT DATA

END
SUBROUTINE VLDYMO

Purpose: Compute valve dynamics

This subroutine simulates the dynamics of the valve servo system and
valve motion including stickies and backlashes. The inputs are:

- \( X_{xyzV} \): Position command to move valve \( xyz \).
- \( \Theta() \): Current valve position, DEG
- \( D\Theta() \): Current valve velocity, DEG/SEC

Arguments:
- \( N \): Initialization flag eliminated

Common usage:

Input:
- \( X_{CFPOV}, X_{COPOV}, X_{CMOV}, X_{CMFV}, X_{CCCV} \)
- \( \Theta, D\Theta \)

Output:
- \( R_{FPOV}, R_{ROPOV} \)
- \( R_{MOV}, R_{MFV}, R_{CCV} \)
- \( X_{FPPOV}, X_{OPPOV}, X_{MOV}, X_{MFV}, X_{CCV} \)
- \( X_{OPOV} \)

Source control EMCO

Output destination HOTGAS, OXIDF, FUELF, EMCO, CNTROL

Double precision is probably unnecessary with double precision
accumulators in the integration routines. It should be restored only
on evidence of actual accuracy problems outside of integration.

Double precision EVP, DDESA, DDESV, DVR, DELTA, ALIM, Q
Double precision DTHETA, ESAC, ESA, DESA, ESV, DESV
Double precision TIME

Dimensions:
- \( DPPC(5) \), THETAC(5), CL(5), CSV(5), A(5)
- \( \ThetaHY(5), \ThetaST(5), \Theta1T(5), \Theta2T(5) \)
- \( \ThetaWU(5), \ThetaSK(5), \ThetaBL(5), \ThetaWO(5), \ThetaMAX(5) \)
- \( \text{REAL CvA}(5), vdppc(5) \)

Include:
- 'blank.com'
- 'out.com'
- 'units.com'
- 'contrl.com'
- 'valves.com'

235
SAVE

WINDUP IS ADDED TO THE SIMULATION IN DATA FORMAT
THETMAX IS THE MAXIMUM ACTUATOR STROKE LIMIT

DATA WINDUP/0.091, 0.115, 0.1, 0.141, 0.067/
DATA THETMAX/79.0, 79.0, 84.25, 84.25, 80.0/

DATA SLOPF/0.0/ added to input parameters

Please rename this function.

Rename(Z) = 1.0 / (772.8 * Z**2 + 1.0E-12 )

ALIM biases the magnitude of Q down minutely. If Q is small enough,
it is replaced by 0.D0. It probably had been intended to function
differently. As it stands, ALIM was not considered of value and
was discarded. The reimplementer should note that double precision
outside the integrators has been eliminated.

ALIM(Q) = DMAX1(0.D0, DABS(Q) - 1.D-20) * DSIGN(1.D0,Q)

rlimit(floor, ceiling, x ) = AMAX1( floor, AMIN1( ceiling, x ) )

********************
* IF(FLAG.EQ.15.)GO TO 9999 is obsolete
* Unnecessary initializations were eliminated

READ( run, '(/2X, 6G12.4 )' )
+ CA, WA, SA, CSV, WSV, SSV, A, CL, CRS, TRS, CLS,
+ TLS, CMF, TMF, CM, WM, SM, CRVDT, CLVDT,
+ ( THETHY(I), THETST(I), DPPC(I), I = 1, 5 ),

* The following input parameters were transferred from NAMELIST input
  + AR1, AR2, TL, TH, XOMAX,
  + OPLEAK, OPX1, OPX2, FPLEAK, FPX1, FPX2, SLOPF,
  + IBKLASH, IWUSTN,

  DELTA was made an input parameter.

  + DELTA

  Functions of DELTA for Euler and AB2 integrators

  h(1) = DELTA

  DO 30 I=1,5
      DESA(I)=0.0

236
\begin{verbatim}
ESA(I)=0.0
DESV(I)=0.0
ESV(I)=0.0
THETA(1)=DPPC(1)*XCFPOV
THETA(2)=DPPC(2)*XCOPOV
THETA(3)=DPPC(3)*XCMOV
THETA(4)=DPPC(4)*XCMFV
THETA(5)=DPPC(5)*XCCCV
VS(I)=0.0
EMF(I)=0.0
DVM(I)=0.0
VM(I)=0.0
THET1L(I)=0.0
THET2L(I)=0.0
THETA1(I)=0.0
THETA2(I)=0.0
ISTIC(I)=1
IHYS(I)=1
DTHET1L(I)=0.01
ESAC(I)=0.0
VR(I)=0.0
CvA(I) = CL(I) * CSV(I) / A(I)
vdppc(I) = 1. / DPPC(I)
30 CONTINUE
fbklsh = FLOAT(IBKLASH)wustn = FLOAT(IWUSTN)
LOOP=(DT+0.00001)/DELTA
twosa = 2. * SA
twossv = 2. * SSV
vTRS = 1. / TRS
crsv = CRVDT * CRS
vfpx = 1. / (FPX2 - FPX1)
abfp = ABFPO * .01
vopx = 1.0 / (OPX2 - OPX1)
abopf = ABOPO * 0.01
abmov = ABMOV * 0.01
abmfv = ABMFV * 0.01
abccv = ABCCV * 0.01
RFBV = 1.0E+12

* DELTA=0.0001
C
C DELTA IS CHANGED TO 0.00002 SECOND TO BETTER SIMULATE THE ANALOG SERVO
C OF THE VALVE DYNAMIC. THIS IS NECESSARY WHEN APPLYING STEP INPUTS TO
C THE VALVE OPENINGS.
C
* DELTA=0.00002 DELTA was made an input parameter.
*
* Initialize integrators:
*
237
\end{verbatim}
CALL unint0(DESA(I), 147 + I)
CALL lrint0(ESA(I), 152 + I, -20.0, 20.0)
CALL unint0( DESV(I), 157 + I)
CALL lrint0(ESA(I), 162 + I, -20.0, 20.0)
CALL lrint0( THETA(I), 167 + I, 0.0, THETAMAX(I))
CALL unint0( VR(I), 172 + I)

* GO TO 310
* 
ENTRY VALDYM

SERVO CALCULATIONS

200 CONTINUE
THETAC(1)=DPPC(1)*XCFPOV
THETAC(2)=DPPC(2)*XCOPOV
IF ( STIME .GE. TL .AND. STIME .LE. TH) THETAC(2)=DPPC(2)*1000.
THETAC(3)=DPPC(3)*XCMOV
THETAC(4)=DPPC(4)*XCMFV
THETAC(5)=DPPC(5)*XCCCV

SCALING FOR BACKLASH, WINDUP, AND STICTION FROM % OPENING TO DEGREE

DO 205 I=1,5
THETBL(I) = THETHY(I) * DPPC(I) * fbklsh
THETWU(I) = WINDUP(I) * DPPC(I) * fwustn
THETSK(I) = THETST(I) * DPPC(I) * fwustn
205 CONTINUE
DO 300 I=1,5
IF( TPA.GT.0.0 .AND. STIME.GE.TPA) THEN
DO 210 J=I,LOOP
EVP = THETAC(I)*CRVDT - VR(I)
210 CONTINUE
* DDESA=CA*WA**2*EVP-WA**2*ESAC(I)-2.0*SA*WA*DESA(I) replaced by
* DDESA = ( ( CA*EVP - ESAC(I) ) * WA - twosa * DESA(I) ) * WA
* DDESV = ((ESA(I) -ESV(I) ) * WSV - twossv*DESV(I) ) * WSV
DTHETA(I) = CvA(I) * ESV(I)
CvA(I) is CL(I)*CSV(I)/A(I)
DVR=THETA(I)*CRVDT*CRS/TRS-VR(I)/TRS replaced by
DVR = ( THETA(I) * crvs - VR(I) ) * vTRS

TIIE POWER AMPLIFIER LIMIT SHOULD BE PUT AT THE OUTPUT END NOT IN
THE MIDDLE.

IF(ESA(I).GT.23..AND.DESA(I).GT.0.) DESA(I)=0.0
IF(ESA(I).LT.-23..AND.DESA(I).LT.0.) DESA(I)=0.0

238
The statements above illustrate how to limit the internal double precision accumulator of an integrator, by zeroing the input rate. The effect of the commenting out is to substitute an unlimited accumulator, for the limited one, with limits applied to the output of the integration. This is the approach used throughout other modules of the simulation.

\[
\text{ESAC}(I) = \text{ESAC}(I) + \text{ALIM}(\text{DESA}(I)) \times \Delta T \\
\text{ESA}(I) = \text{ESAC}(I)
\]

Without arguments to the contrary, it appears that the integration of ESA and ESV with old rates must be in error. Accordingly, the higher order integrations are done first.

LIMITS ON INPUT AMPLIFIER ARE \(\pm 23\) VOLTS. AND LIMITS ON SERVO AMPLIFIER ARE \(\pm 20\) VOLTS.

\[
\begin{align*}
\text{IF}(\text{ESA}(I) & .GT. 23.) \text{ ESA}(I) = 23. \\
\text{IF}(\text{ESA}(I) & .LT. -23.) \text{ ESA}(I) = -23. \\
\text{IF}(\text{ABS}(\text{ESA}(I)) & .LT. 0.25) \text{ ESA}(I) = 0.0 & \text{ replaced by} \\
\text{DESA}(I) & = \text{pruint}( \text{DDESA}, 1, 147 + I ) \\
\text{ESA}(I) & = \text{prlint}( \text{DESA}(I), 1, 152 + I ) \\
\text{IF} & (\text{ABS}(\text{ESA}(I)) .LT. 0.25) \text{ THEN} \\
\text{ESA}(I) & = 0.0 \\
\text{CALL} & \text{lmint0}( 0.0, 152 + I, -20., 20. ) \\
\text{ENDIF} \\
\end{align*}
\]

\[
\text{DESA}(I) = \text{DESA}(I) + \text{ALIM} (\text{DDESA}) \times \Delta T 
\]

was moved ahead of ESA integration

\[
\begin{align*}
\text{IF}(\text{ESV}(I) & .GT. 20.. \text{AND.} \text{DESV}(I) \times \text{GT.} 0.0) \text{ DESV}(I) = 0.0 \\
\text{IF}(\text{ESV}(I) & .LT. -20.. \text{AND.} \text{DESV}(I) \times \text{LT.} 0.0) \text{ DESV}(I) = 0.0 \\
\text{ESV}(I) & = \text{ESV}(I) + \text{ALIM}(\text{DESV}(I)) \times \Delta T \\
\text{IF}(\text{ESV}(I) & .GT. 20.) \text{ ESV}(I) = 20. \\
\text{IF}(\text{ESV}(I) & .LT. -20.) \text{ ESV}(I) = -20. \\
\text{DESV}(I) & = \text{pruint}( \text{DDESV}, 1, 157 + I ) \\
\text{ESV}(I) & = \text{prlint}( \text{DESV}(I), 1, 162 + I ) \\
\text{DESV}(I) & = \text{DESV}(I) + \text{ALIM}(\text{DDESV}) \times \Delta T \\
\text{THETA}(I) & = \text{THETA}(I) + \text{ALIM}(\text{DTHETA}(I)) \times \Delta T \\
\text{CALL} & \text{intgrl}( \text{THETA}(I), \text{DTHETA}(I), \Delta T, 167 + I ) \\
\text{ACTUATOR STROKES ARE LIMITED TO THE MAXIMUM THETA} \\
\text{THETA}(I) & = \text{rlimit}( 0.0, \text{THETMAX}(I), \text{THETA}(I) ) \\
\text{VS}(I) & = \text{VS}(I) + \text{ALIM}(\text{DVS}) \times \Delta T
\end{align*}
\]
IF(EMF(I).GT.12.5.AND.DEMF.GT.0.0) DEMF=0.0
IF(EMF(I).LT.-12.5.AND.DEMF.LT.0.0) DEMF=0.0
EMF(I)=EMF(I)+ALIM(DEMF)*DELTA
VM(I)=VM(I)+ALIM(DVM(I))*DELTA
DVM(I)=DVM(I)+ALIM(DDVM)*DELTA
VR(I)=VR(I)+ALIM(DVR)*DELTA
VR(I) = pruint( DVR, 1, 172 + I )
CONTINUE
ENDIF

NEW PROGRAM

BACKLASH IS DEFINED AS THE AMOUNT OF ACTUATOR OUTPUT SHAFT TRAVEL REQUIRED TO REVERSE DIRECTION OF VALVE BALL MOTION UNDER CONDITIONS OF ZERO LINKAGE WINDUP AND TORQUE LOADING. THE VALUES USED HERE IS HALF OF THE AMOUNT OF THE TOTAL TRAVELING, WELL HALF ON EACH SIDE.

IF ( I .EQ. 3 .AND. THETA(I) .GT. 33.8 .AND. THETA(I) .LT. 84.0 ) THEN
   FAC = 0.0
ELSE IF( I .EQ. 4 .AND. THETA(I) .GT. 38.3 .AND. THETA(I) .LT. 75.8 ) THEN
   FAC = 0.0
ELSE
   FAC = 1.0
ENDIF
IF ( ABS(THETA(I) - THETA1(I) ) .LT. THETBL(I)*FAC ) THEN
   DTHET1(I) = 0.0
   THET1L(I) = THETA1(I)
ELSE IF (ABS(DTHETA(I)).LT.1.0E-06) THEN
   DTHET1(I) = 0.0
   IF( THETA1(I) .LE.THETA(I)) THEN
      THETA1(I) = THETA(I) - THETBL(I)*FAC
   ELSE
      THETA1(I) = THETA(I) + THETBL(I)*FAC
   ENDIF
ELSE
   IF (THETA1(I).LE.THETA(I)) THEN
      THETA1(I) = THETA(I) - THETBL(I)*FAC
   ELSE
      THETA1(I) = THETA(I) + THETBL(I)*FAC
   ENDIF
   DTHET1(I) = DTHETA(I)
ENDIF

WINDUP AND STICION SIMULATION:
WINDUP IS DEFINED AS THE AMOUNT OF ACTUATOR OUTPUT SHAFT TRAVEL REQUIRED AFTER LINKAGE BACKLASH HAS BEEN ABSORBED TO INITIATE VALVE MOTION. STICION IS DEFINED AS THE AMOUNT OF VALVE BALL OVERTRAVEL RESULTING
FROM A CHANGE IN LINKAGE WINDUP DURING THE TRANSITION FROM A STATE OF
STATIC FRICIONAL RESISTANCE TO SLIDING FRICIONAL RESISTANCE AT
START OF BALL MOTION.

IF (ABS(DTHET1(I)) .LT. 1.0E-06) DTHET2(I)=0.0
IF( ABS(DTHET2(I)) .LT. 1.0E-06 OR.
+ ABS(THETA1(I) - THETA2(I)) .LE. (THETWU(I) - THETSK(I)) ) THEN
IF(ABS(THETA1(I)-THETA2(I)).LE.THETWU(I)) THEN
  DTHET2(I)=0.0
ELSE
  DTHET2(I) = DTHET1(I)
ENDIF
IF ( THETA2(I) .GT. THETA1(I) ) THEN
  THETA2(I) = THETA1(I) + THETWU(I) - THETSK(I)
ELSE
  THETA2(I) = THETA1(I) - THETWU(I) + THETSK(I)
ENDIF
ELSE
  DTHET2(I) = DTHET1(I)
IF ( THETA2(I) .GT. THETA1(I) ) THEN
  THETA2(I) = THETA1(I) + THETWU(I) - THETSK(I)
ELSE
  THETA2(I) = THETA1(I) - THETWU(I) + THETSK(I)
ENDIF
ENDIF

300 CONTINUE

THIS SECTION OF CODE USES THETA2(I) AS THE ACTUAL VALVE OPENINGS TO
FIND THE VALE OPENING AREAS AND VALE RESISTANCES.
THE LEAK (FPLEAK AND OPLEAK) PHENOMENRA DEFINED IN THE FOLLOWING IS NOT
CLEAR. HOWEVER, BOTH OPLEAK AND FPLEAK ARE SET TO 0.0 IN INPUT DATA.

FUEL PREBURNER OXIDIZER VALVE

OXIDIZER PREBURNER OXIDIZER VALVE

IF ( SLOPF .GT. .01 ) THEN
  XFPOV = XCFPOV
ELSE
  XFPOV = rlimit( 0.0, 100.0, THETA2(1)* vdppc(1) )
ENDIF
AFPOV = FGEN(18, 99, XFPOV)
+ + FPLEAK * rlimit( 0.0, abfp, (XFPOV - FPXl) * vfpx )
RFPOV = Rename(AFPOV)

OXIDIZER PREBURNER OXIDIZER VALVE

IF ( SLOPF.GT..01 ) THEN
  XOPOV = XCPOV

241
ELSE IF (STIME .GE. TL .AND. STIME .LE. TH) THEN
XOPOV = XOPOV + 210. * DT

XOPOV has a maximum increasing rate of 210%/sec and maximum decreasing rate of 270%/sec. not percents

ELSE

* XOPOV follows THETA2(2)/DPPC(2) perfectly between limits imposed by max rates and fixed limits 0. and 100. Otherwise XOPOV increases at the maximum rate. There is no need to use a higher order integrator here, because at the constant limit rate, Euler's is exact.

* XOPOV = AMIN1( 100., XOPOV + 210.*DT, + AMAX1( 0., XOPOV - 270.*DT, THETA2(2)*vdppc(2) ) )
ENDIF

XOPOV = AMIN1( XOMAX, XOPOV )

AOPOV = FGEN(17, 100, XOPOV) + OPLEAK *
+ rlimit( 0., abopf, ( XOPOV - OPX1) * vopx )
ROPOV = Rename(AOPOV)

MAIN OXIDIZER VALVE

XMOV = THETA2(3) * vdppc(3)
AMOV = FGEN(6, 101, XMOV) * abmov
RMOV = Rename(AMOV)

MAIN FUEL VALVE

XMVF = THETA2(4) * vdppc(4)
AMVF = FGEN(31, 102, XMVF) * abmfv
RMVF = Rename(AMVF)

COOLANT CONTROL VALVE

XCCV = THETA2(5) * vdppc(5)
ACCV = FGEN(19, 103, XCCV) * abccv
RCCV = Rename(ACCV)

FUEL BLEED VALVE

IF(TIME.LE.TFBV) GO TO 400
RFBV=AMIN1(1.0E+12,0.012/(AMIN1(20.0*(STIME-TFBV),1.0)))
GO TO 410
* 410 CONTINUE
RETURN
END
FUNCTION CSTAR0(EMR, P)

* PURPOSE: INTERPOLATE C* FROM TABLE VS PRESSURE AND MIXTURE RATIO *
* ARGUMENTS *****
* INPUT: 
  N = INITIALIZATION FLAG inactivated 
  EMR = MIXTURE RATIO 
  P = PRESSURE, PSI 
* OUTPUT: 
  CSTAR = CHARACTERISTIC VELOCITY, FT/SEC 

DIMENSION CS(12,9), PR(12)
REAL MR(9), scspr(12), vdmr(9)
INCLUDE 'units.com'
* READ(run,10) NPR,NMR
READ(run,11) (PR(I),I=1,NPR),(MR(I),I=1,NMR)
10 FORMAT('2X,2I12')
11 format('2X,6G12.4')
READ(run,12) (CS(I,J),I=1,NPR),J=1,NMR)
12 FORMAT('2X,12F6.0')
CALL xyset( NPR, PR, NMR, CS, scspr, vdmr )
RETURN
FUNCTION xylint( x, y, nx, xp, ny, yp, sx, vdy, table, 
+ itop, jtop )
SUBROUTINE xyset( nx, xp, ny, yp, table, sx, vdy )
* ENTRY CSTAR( EMR, P )
* INTERVAL( I1, EMR, NPR, PR, 
+ 'EMR below range of PR in CSTAR.', 
+ 'EMR above range of PR in CSTAR.', 0 )
* INTERVAL( J1, P, MPR, MR, 
+ 'P below range of MR in CSTAR.', 
+ 'P above range of MR in CSTAR.', 0 )
CSTAR = xylint( EMR, P, NPR, PR, NMR, MR, scspr, vdmr, CS, I1, J1)
END
'qflux.for':

C
C FUNCTION H2SATH(P)
C
C PURPOSE: CALCULATE HYDROGEN SATURATION ENTHALPY
C
C******ARGUMENTS******
C INPUT:
C P : PRESSURE, PSI
C OUTPUT:
C H2SATH : SATURATION ENTHALPY, BTU/LB
C
C ENTER PRESSURE, P IN PSIA
C RETURN SATURATED VAPOR ENTHALPY IN BTU/LB (NBS REF H + 200)
C
DIMENSION H(10), DH(10)
C
DATA DH / .44, .175, 0., -.1, -.18, -.265, -.345, -.475, -.85, -.3 /
C
C
C IF( P .LT. 187.5) THEN
H2SATH = 0.
ELSE

I = INT(P/10.) / 2 + 1
H2SATH = H(I) + DH(I)*((P-20*I+20)

H2SATH = H(I) + DH(I) * (P - 20.0 * AINT( P * 0.05 ) )
END IF

FUNCTION QFLUX(TW, TF, P, HF)
C
C PURPOSE: CALCULATE HYDROGEN BOILING HEAT FLUX
C
C******ARGUMENTS******
C INPUT:
C TW = WALL TEMPERATURE, DEG R
C TF = FLUID TEMPERATURE, DEG R
C P = FLUID PRESSURE, PSI
C HF = FLUID ENTHALPY, BTU/LB
C
C OUTPUT:

244
QFLUX = HEAT FLUX TO FLUID, BTU/IN2-SEC

CALCS. HEAT FLUX FOR NUCLEATE, TRANSITION AND FILM BOILING REGIONS
BASED ON DATA FROM R-5598, FIG.26, PG. 90

THE PARAMETER VALUES USED HERE IS SLIGHTLY DIFFERENT FROM THE ONES
GIVEN IN THE DOCUMENT PAGES 32 AND 33.
I ASSUME THAT THIS IS NOT TOO IMPORTANT BECAUSE THAT THE HEAT TRAN
IS ONLY A SMALL FRACTION OF THE ENERGY FLOW OF THE SYSTEM.

*  * The replacement code assumes that the limits are intended, and
*  * avoids repeatedly taking logarithms of limiting constants.

              rlimit(floor, ceiling; x) = AMAXI( floor, AMINI( ceiling, x) )

HS = H2SATH(P)
IF ( TW .LT. 80.0 .OR. HF .GT. HS) THEN
QFLUX = 0.0
ELSE
  X=ALOG10(AMAX1(0.01,TW-TF))
  Y=AMAX1((2.0+4.0*X-2.0*X**2)*AMINI(1.0,AMAX1(0.0,(100.0-TF)/40.0)))
  QFLUX=10.0**((AMAX1(0.01,AMINI(5.0,Y)))/5.184E+05

  test = TW - TF
  IF ( test .GT. 0.01 ) THEN
    X = ALOG10( test )
    Y = AMAX1( 2.1 + X, 0.05 * (1.0 + X * (2.0 - X) ) * 
                  rlimit( 0.0, 40.0, 100.0 - TF ) )
    QFLUX = 1.0 /
    XntoYn( 0.1, rlimit( 0.01, 5.0, Y ) * 1.929E-6 )
  ELSE
    QFLUX = 1.0
  ENDIF
ENDIF
END

THE SETPT( ) FUNCTION IS NOT USED

'h2vp.for':

FUNCTION H2VP(T)

Purpose: CALCULATE HYDROGEN SATURATION PRESSURE

IT IS USED FOR CALCULATING CAVITATION OF HYDROGEN PUMPS.
FOR A GIVEN TEMPERATURE, IF THE LIQUID HYDROGEN PRESSURE IS LESS THAN THE VAPOR PRESSURE AT CERTAIN POINT THEN BUBBLES WILL START TO GROW. THIS HAPPENS ESPECIALLY ON THE FOLLOWING EDGE OF THE PUMP BLADE WHERE THE PRESSURE IS LOWEST.

*****ARGUMENTS*****

INPUT:
T = TEMPERATURE, DEG R

OUTPUT:
H2VP = SATURATION PRESSURE, PSI

H2VP can be speeded up considerably by using an fgen linear approximation. One function can be used for all three segments, eliminating the tests for segment boundaries 29.0 and 32.976

DATA CA, CB, CC, CD, CE
+ 2.0062, -50.09708, 1.0044, 1.748495E-2, 1.317E-03
+ CF, CG
+ -5.926E-5, 3.913E-6

TK = T / 1.8 replaced by
TK = T * .555555

IF( TK .LT. 32.976 ) THEN
  ALOGPV = CA + CB/(TK + CC) + CD * TK
  H2VP = XtoY( 10.0, ALOGPV )
IF(TK .GT. 29.0) THEN
  tk29 = TK - 29.0
  tk29sq = tk29 ** 2
  H2VP = H2VP + tk29 *
  ( tk29sq * (CE + tk29sq * (CF + tk29sq * CG ) ) )
  PVAPOR = PVAPOR + CE*(TK-29.0)**3+CF*(TK-29.0)**5+CG*(TK-29.0)**7
ELSE
  H2VP = H2VP * 14.696
END IF
ELSE
  H2VP = 0.
END IF
END

'oprime.for:

SUBROUTINE OPRIMO
* Initializes integrators for OPRIME

************************************************************************

246
INTEGER Tstep
PARAMETER (NVOL=4, MAXN=6, MAXC=5)
PARAMETER (MAXIT=30, TOL= .0005)
PARAMETER ( Tstep = 0, TooBig = 1.E20 )
LOGICAL FLAG, prpOK

DIMENSION P(MAXN), RHO(MAXN), RHOP(MAXN), U(MAXN), UP(MAXN),
          H(MAXN), T(MAXN), TW(MAXN), D(MAXN), AHT(MAXN),
          W(MAXN), VOL(MAXN), QC(MAXN), QF(MAXN), QB(MAXN),
          QOUT(MAXN)
DIMENSION DW(MAXC), DWP(MAXC), R(MAXC), Z(MAXC)

* Keep all local variables between calls
*
SAVE
*
DATA RHOV /9.693E-4/
DATA RHOVAL/9.693E-4/
DATA RHOP3 / .03944 /
DATA RHOSL / .0365 /
DATA HSL / -39.1 /
DATA HV / 39.4 /
DATA HL / -50.0 /
DATA RLINE /6.331E-4/
DATA ZLINE / .02 /
DATA XLINE / 2563. /
DATA WPOVI / -2.2 /
DATA WPOV / -2.2 /
DATA WPOVP / 0.0 /
DATA FLAG / .TRUE. /
DATA DWLINE/ 0.0 /
DATA DWLINP/ 0.0 /
DATA P1 / 103.2 /

DATA P / MAXN*14.7 /, RHO / MAXN*4.69E-5/, RHOP / MAXN*4.69E-5/,
          H / MAXN*117.4 /, U / MAXN*83.6 /, UP / MAXN*83.6 /,
          T / MAXN*540. /, TW / MAXN*540. /, QC / MAXN*0.0 /,
          QF / MAXN*0.0 /, QB / MAXN*0.0 /, QOUT / MAXN*0.0 /,
          DW / MAXC*0.0 /, DWP / MAXC*0.0 /

DATA D / 0.0, 2*1.40, 1.45, 1.75, 0. /
DATA AHT/ 0.0, 40.25, 30.25, 155.9, 198., 0. /
DATA W / 0.0, 1.13, .85, 4.4, 5.5, 0. /
DATA VOL/ 0.0, 2*12.35, 29.3, 27.8, 0. /

DATA R / 0.0, 2*5E-4, 1.E-4, -78.0E-4 /
DATA Z / .020, 2*.0065, .0080, .013 /

* Statement function UNEWF deleted. It is only used once.
CHGF(CHG,XNEW,OLD)=AMAX1(CHG,ABS(XNEW-OLD)/(ABS(OLD)+.1))
replaced by relaxation system.

OXHPF(RH)=AMAX1(.0149,.0149+.013*(RH-5.E-4)/.0389) replaced by
OXHPF(RH)=AMAX1(.0149,.0149+.3342*(RH-5.E-4))

************************************************************************
CALL imint0(WPOV,178,-TooBig,.05)
CALL unint0(WPOVP,179)
CALL imint0(P(1),184,37.,TooBig)
CALL unint0(DWLINE,185)
CALL unint0(DW(1),186)
DO I = 2, MAXN-1
   CALL unint0(TW(I),178+I)
   CALL unint0(DW(I),185+I)
   CALL unint0(RHOP(I),189+I)
   CALL unint0(RHO(I) *(1. + U(I)),193+I)
10 CONTINUE
RETURN

ENTRY OPRIME(P0,PC,RVALVE,DWINJ,DWVALV)
************************************************************************
THIS SUBROUTINE IS TO CALCULATE THE PRIME CHARACTERISTICS OF
THE FPOV AND OXID INJECTOR FOR FUEL PREBURNER. THIS SUBROUTINE IS
ONLY CALLED BY FUELF SUBROUTINE. THERE MUST BE A BIG DIFFERENCE BETWEEN
THE FPOV AND OPOV SET UP. THE OPOV USES A SIMPLIFIED VERSION OF THE
PRIMING FUNCTION.

THIS SUBROUTINE USES THE ITERATION TO FIND THE NEW STEADY STATE VALUES
FOR A GIVEN CONDITION.
THE INJECTOR IS DIVIDED INTO SIX NODES AND THE ITERATION IS TO FIND THE
ENERGY BALANCE AMONG THEM. OF THE SIX NODES, THE FIRST NODE IS THE
FPOV VALVE, AND THE LAST NODE IS THE INJECTOR OUTLET. THESE ARE USED AS
THE BOUNDARY CONDITIONS.

********************************************************************************

PRIME VALVE BUBBLE

WPOV = prlint((RHOSL/RHOVAL - 1.) * DWVALV, Tstep, 178)

* WPOV =< .05

IF ( FLAG ) THEN
   X = 1. - WPOV/WPOVI
   HT = AMIN1( 100., 100.+(X-.5)*(HV-100.)*2.5 )
   H(1) = AMIN1(HT,(HV+.900/.100*(HV-HSL)) - X*(HV-HSL)/.100) replaced by
hvhs1 = HV - HSL
H(1) = AMINI(HT, HV + hvhs1*(9.0 - 10.*X) )

X = (H(1) - HSL) / hvhs1
IF( X.LT. 1. ) THEN
   RHOVAL = 1./(X/RHOV + (1. - X)/RHOSL )
ELSE
   RHOVAL = RHOV * HV / H(1)
END IF
IF (WPOV .GT. -.001) THEN

   The effect of the reset is hold WPOV output at 1.0, but
   compute X above with a WPOV of .05 . If this is right, it
   should be recoded to look intentional.

   WPOV = 1.
   CALL lmint0( WPOV, 178, -TooBig, .05 )
   WPOVP = pruint( DWVALV, Tstep, 179 )
   IF( WPOVP .LT. .04 ) THEN
      hlhs1 = HL - HSL
      H(1) = HSL + 25. * WPOVP * hlhs1
      RHOVAL = RHOSL + (H(1) - HSL)/hlhs1*(RHOP3 - RHOSL)
   ELSE
      RHOVAL=RHOP3
      H(1)=HL
      FLAG = .FALSE.
   ENDIF
ENDIF
ENDIF
ENDIF

H(MAXN)=H(MAXN-1)
P(MAXN)=PC
RHOP(1)=RHOVAL
RHOP(MAXN)=RHOP(MAXN-1)

DO 110 I=2,MAXN-1
   QC(I)=.0227/D(I)**1.8*OXHPF(RHO(I))*AHT(I)*1.5 replaced by
   QC(I)=.03405/(D(I)*X10th(D(I), 8 ) )* OXHPF(RHO(I))*AHT(I)
   TW(I) = pruint( - QOUT(I) /( W(I) * FGEN(22, 113+I, TW(I)) ),
                     + Tstep, 178+I )
110 CONTINUE

BEGIN ITERATION LOOP

prpOK = .TRUE.

DO 310 ITER = 1, mxopit
   P1 = trlint( XLINE*(DWLINP - DWP(1)*RHOP3/RHOVAL),
                + Tstep, 184 )
310
case="249"
C

P(1) = relax( prpOK, P1, P(1), 12 )

DWLINP = trflow( DWLINE, ZLINE, -RLINE/RHOP3, P0 - P(1), 185 )
IF( RHOVAL .LT. 1.E-3 ) THEN
    DWP(1) = GFLOW(P(1), P(2), P(1)/RHOVAL, 1., 1.4) /
             X10th( 772.8*RVALVE, 5)
ELSE
    DWP(1) = trflow( DW(1), Z(1), -RVALVE/RHOVAL, P(1)-P(2), 186 )
ENDIF

C

DO 300 I = 2, MAXN-1
    J=I-1
    DWNEW = trflow( DW(I), Z(I), -R(I)/RHOP(I), P(I)-P(I+1),
                   185 + I )
    IF( I.LT.MAXN-I ) THEN
        DWP(I) =DWNEW
    ELSE
        DWP(I)=.5*( DWP(I)+ DWNEW )
    ENDIF
    RHOP(I) = truint( (DWP(J) - DWP(I) ) /
                        VOL(I), Tstep, 189+I )
    DWIN = recpos( DWP(J) ) - recpos( DWP(I) )
    HIN = recpos( DWP(J) ) * H(I-1) - recneg( DWP(I) ) * H(I+1)
    DWOUT = recpos( DWP(I) ) - recneg( DWP(J) )

* Replaced the reference to the statement function UNEWF with:

UP(I) = truint( QOUT(I) + HIN -
            DWOUT*P(I)/(RHOP(I)*9336.*VOL(I) ) +
            DWIN/VOL(I), Tstep, 193+I )

H(I) = UP(I) + P(I)/(RHOP(I) * 9336.)
CALL o2pt( H(I), RHOP(I), I+4, PNEW, T(1) )

P(1) = relax( prpOK, PNEW, P(I), 11+I )

DWA = .5*( ABS( DWP(I) ) + ABS( DWP(J) ) )
QF(I) = QC(I) * XtoY( T(I)/TW(I), 0.47) * X10th( DWA, 8 ) *
       ( TW(I) - T(I) )
QB(I) = 0.
HG = AMIN1(28.7 + 2.13*ALOG( P(I) ), 38.6 - .00762*P(I) )
IF ( H(I) .LT. HG) 
    QB(I) = AMIN1( DWA*(HG - H(I) ),
                   OXBOIL( TW(I), T(I) ) * AHT(I) )
QOUT(I) = QF(I) + QB(I)
300 CONTINUE
RHOP(MAXN)=RHOP(MAXN-1)

C

IF ( prpOK ) GO TO 400
310 CONTINUE

250
* Convergence failure if do loop is completed
*      CALL wrchg( 12, 16, "OPROP convergence failure." )
C
400 CONTINUE
C
* Formatted output to unit 6 was deleted.
C
DO 500 I=2,MAXN-1
   DW(I) = step( 185 + I )
   RHO(I) = step( 189 + I )
   U(I) = step( 193 + I )
500 CONTINUE

DW(1) = step( 186 )
P1 = step( 184 )
DWLINE = step( 185 )
DWINJ = DW(MAXC)
DWVALV = DW(1)
C
END

FUNCTION OXBOIL(TW, T)

C
C THIS FUNCTION IS THE BOILING HEAT TRANSFER OF THE OXIDIZER INSIDE THE
C INJECTOR. THE OUTPUT IS THE HEAT TRANSFER RATE BTU/IN**2 FROM THE WALL
C TO OXID.
C
PARAMETER ( twlo = 10.**.4217, twhi = 10.**1.135,
+            oxb01 = 1.929E-6 * 10.** -.29, tenl = 10.**1.75 )

*  X=ALOG10(AMAX1(.01,TW-T))
*  Y=AMAX1(5.15-2.3*(X-1.)**2,1.75+1.02*X)
*  OXBOIL=10.**Y*1.929E-6 is faster when reduced to
*  twmt = TW - T
IF ( twmt .LE. .01 ) THEN
   OXBOIL = oxb01
ELSEIF ( twlo .LE. twmt .AND. twmt .LE. twhi ) THEN
   OXBOIL = tenl * XtoY( twmt, 1.02 )
ELSE
   X = ALOG10( twmt )
   OXBOIL = XtoY( 10., 5.15 - 2.3 * (X - 1)**2 )
ENDIF
END
'trbtrq.for':

FUNCTION TRBTQ0
******************************************************************************
C
FUNCTION TRBTQ0(S,UC,T,PRII,NCH,IFLG,CP,DW,G)
C
PURPOSE: COMPUTE TURBINE TORQUE AS A FUNCTION OF INPUTS
C
THE EQUATIONS AND FUNCTION TABLES USED ARE DESCRIBED IN PAGE
C
37-38 (ANALOG SIMULATION) OF THE DOCUMENT. THE EQUATIONS IN PAGE 24
C
ARE INCOMPLETE.
C
*****ARGUMENTS*****
C INPUT:
C S = SPEED, RAD/SEC
C T = TEMPERATURE, DEG R
C PI = NOT USED eliminated
C PRII = PRESSURE RATIO, OUT/IN
C NCH = TURBINE DESIGNATION, 1=LPFT, 2=HPFT, 4=HPOT
C IFLG = FLAG=0 FOR INPUT MODE eliminated
C CP = SPECIFIC HEAT AT CONSTANT PRESSURE, BTU/LBM-DEG R
C DW = FLOWRATE, LB/SEC
C G = GAMMA
C
OUTPUT:
C UC = ISENTROPIC VELOCITY RATIO
C TRBTQ0 = TURBINE TORQUE
C
******************************************************************************
C
DIMENSION NFG(4),D(4)
PARAMETER ( const = 12. * 0.1446 )
DATA NFG/38,39,0,40/
DATA D/7.4,10.19,6.0,I0.09/
*
CALL fgset( 38 )
CALL fgset( 39 )
CALL fgset( 40 )
*
Next to make TRBTQ0 a function so the
entry TRBTRQ will be one.
*
TRBTQ0 = 0.0
RETURN
C
ENTRY TRBTRQ(S, UC, T, PRII, NCH, CP, DW, G)
******************************************************************************
C
DH = AMAX1( 1.0E-04, CP*T*(1. - XTOY( PRII, (S - 1.)/S ) ) )
sqrttdh = X10th( DH, 5 )

252
UC = D(NCH) * S / ( 5371.2 * sqrt dh )
EF = fgen( NFG(NCH), 129 + NCH, UC)
TRBTRQ = const * EF * DW * sqrt dh * D(NCH)
RETURN
END
APPENDIX B: SUPPORTING INPUT DATA FILES

This appendix shows the contents of input data files supporting the report version of the SSME simulation.

'ssme.run' is an edit-and-run file of input parameters defining the run. The top line is a run identifying header, which is reproduced on the output file.

| BALDATA FILE FROM RKDYN 10/84 MOD FOR FUEL2/NEW PROP,O2PROP,START DATA |
|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| RESTRT          | RESUME          | PERTB           | iwrite          |                  |
| false           | false           | false           | 100             |                  |
| DT              | DPR             | DPL             | DPUN            | TPUN            | TSTOP           |
| 0.0002          | 0.01            | 0.00567         | 15.             | 40.             | 4.00            |
| TPA             | PCMALF          | DTVC            | DTPR            | DTCVP           | DTTR            |
| 40.0            | 0.              | 0.008           | 0.05            | 0.0035          | 0.015           |
| DTFMRE          | DTFMC           | DTMRFC          | DTFMRA          | DTMCX           | DTLM            |
| 0.012           | 0.013           | 0.017           | 0.001           | 0.02            | 0.006           |
| NONZRO          | MODEST          | PCTPERT         | TOPEN           | TPERT           | DTPERT          |
| 0               | 0.              | 116.9999        | 100.            | 100.            | 100.            |
| rxfact(1)       | rxfact(2)       | rxfact(3)       | rxfact(4)       | rxfact(5)       | rxfact(6)       |
| 1.0             | 1.0             | 1.0             | 1.0             | 1.0             | 1.0             |
| rxfact(7)       | rxfact(8)       | rxfact(9)       | rxfact(10)      | rxfact(11)      | rxfact(12)      |
| 1.0             | 1.0             | 1.0             | 1.0             | 1.0             | 1.0             |
| rxfact(13)      | rxfact(14)      | rxfact(15)      | rxfact(16)      |                  |                  |
| 1.0             | 1.0             | 1.0             | 1.0             |                  |                  |
| AHT1(4)         | AHT1(5)         | AHT1(6)         | AHT1(12)        | CDPFP1          | CTQFP1          |
| 1.4049E+04      | 3.8770E+03      | 2.6510E+03      | 3.4395E+04      | 1.0000E+00      | 1.0000E+00      |
| CDPFP2          | CTQFP2          | CTQFT1          | CDPOP1          | CTQOP1          | CDPOP2          |
| 1.0000E+00      | 1.0000E+00      | 8.9498E-01      | 1.0000E+00      | 1.0000E+00      | 1.0000E+00      |
| CTQOP2          | CDPOP3          | CTQOT12         | FT2S            | AFT2            |                  |
| 1.0000E+00      | 1.0000E+00      | 1.0000E+00      | 1.0000E+00      | 8.7225E-01      | 9.4153E+00      |
| CTQFT2          | EOT2S           | AOT2            | CTQOT2          | AFI             | EFFCM            |
| 1.0072E+00      | 9.3861E-01      | 2.9433E+00      | 1.0000E+00      | 2.4725E+01      | 1.0000E+00      |
| ACN             | THRSTC          | AHTC4           | AHTC5           | AHTC6           | ABMOV           |
| 8.1810E+01      | 1.5626E+02      | 2.7770E+03      | 2.0200E+02      | 2.4600E+02      | 1.4460E+01      |

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1 XMOV
1 XOPOV
1 YCCCV
1 YCFPOV
1 YCMFV
1 YCMOV
1 YCOPOV
1 ZCOM
1 ZFIG
1 ZOIN

259
Analysis of the Space Shuttle Main Engine Simulation

J. Alex De Abreu-Garcia and John T. Welch

Department of Electrical Engineering
University of Akron
Akron, Ohio 44325

National Aeronautics and Space Administration
Lewis Research Center
Cleveland, Ohio 44135-3191

This report analyzes the digital code used to simulate dynamic performance of the Space Shuttle Main Engine. This simulation program is written in Fortran. The purpose of the analysis is to identify a means to achieve faster simulation execution, and to determine if additional hardware would be necessary for speeding up the simulation. The analysis included the use of custom integrators based on the Matrix Stability Region Placement method. In addition to speed of execution the accuracy of computations, the useability of the simulation system, and the maintainability of the program and data files were examined. A revised code implementing the study recommendations was implemented but not verified for accuracy.