PLANNING COLLISION FREE PATHS FOR TWO COOPERATING ROBOTS USING A DIVIDE-AND-CONQUER C-SPACE TRAVERSAL HEURISTIC

by

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CONTENTS

LIST OF TABLES ........................................ vi
LIST OF FIGURES ....................................... vii
ACKNOWLEDGEMENT ........................................ ix
Abstract .................................................. x

1. Introduction ........................................... 1
   1.1 Motivation .......................................... 1
   1.2 Direction of this Work .............................. 5
      1.2.1 Assumptions .................................. 5
      1.2.2 Goals ........................................ 6
      1.2.3 Strategy ..................................... 6
      1.2.4 Results ..................................... 8
   1.3 Overview of Thesis ................................ 9

2. Literature Review ....................................... 11
   2.1 Path Planning for Single Robots .................... 11
      2.1.1 The Graph Search Approach .................... 12
      2.1.2 The Potential Fields Approach ................. 22
      2.1.3 The Human Assisted Approach .................. 26
   2.2 Path Planning for Cooperating Robots ............... 28
   2.3 Other Related Areas of Research .................... 32
      2.3.1 Mobile Robot Path Planning ..................... 32
      2.3.2 Coordination of Multiple Robots ............... 33
      2.3.3 Piano Mover's Problem ......................... 33
      2.3.4 Nonholonomic Motion Planning ................. 34
   2.4 Summary of the Literature Review ................... 34
      2.4.1 Difficulties With Complete Solutions ............ 35
      2.4.2 Practical Incomplete Solutions .................. 35
      2.4.3 Potential Fields Solutions ...................... 36
      2.4.4 Cooperating Robots ............................ 36
3. Statement of the Problem .................................................. 37  
  3.1 Background ................................................................. 37  
  3.2 Assumptions ................................................................. 38  
  3.3 Goals ......................................................................... 43  
  3.4 Single Robot Path Planning Problem Statement ...................... 44  
  3.5 Cooperating Robot Path Planning Problem Statement ............... 45  

4. Divide-and-Conquer C-Space Traversal Heuristic .......................... 47  
  4.1 Motivation for a New Approach ......................................... 47  
  4.2 Conceptual Description of Heuristic ................................... 50  
    4.2.1 More 2D Examples .................................................. 54  
    4.2.2 A 3D example ....................................................... 55  
    4.2.3 Philosophy Behind the Heuristic ................................ 55  
  4.3 Vector Description of Heuristic ....................................... 58  
    4.3.1 Failure Condition .................................................. 60  
  4.4 Computing Search Directions .......................................... 62  
    4.4.1 Selecting a Procedure ............................................. 67  
  4.5 Prioritizing Search Directions ....................................... 68  
  4.6 Comparison of the Heuristic to the Literature ...................... 70

5. Utilizing the Heuristic for Robot Path Planning .......................... 73  
  5.1 Single Robot Path Planning ............................................. 73  
    5.1.1 Handling Robots with Mixed Joint Types ....................... 74  
    5.1.2 Joint Limit Problems .............................................. 75  
    5.1.3 Choosing λ .......................................................... 75  
    5.1.4 Choosing Number of Bins ......................................... 75  
    5.1.5 Multiple Robot Configurations .................................. 76  
    5.1.6 Singularity Concerns .............................................. 76  
  5.2 Cooperating Robot Path Planning ..................................... 76  
    5.2.1 Choosing a Lead Robot ............................................ 77  
    5.2.2 Handling Cooperating Redundant Robots ......................... 79  
    5.2.3 Multiple Robot Configurations .................................. 82  
    5.2.4 Singularity Concerns .............................................. 82  
  5.3 String Tightening ....................................................... 83
<table>
<thead>
<tr>
<th>Section</th>
<th>Title</th>
<th>Page</th>
</tr>
</thead>
<tbody>
<tr>
<td>5.3.1</td>
<td>History of Smoothing</td>
<td>83</td>
</tr>
<tr>
<td>5.3.2</td>
<td>String Tightening Algorithm</td>
<td>84</td>
</tr>
<tr>
<td>5.3.3</td>
<td>Comparison to Other Path Smoothing Approaches</td>
<td>88</td>
</tr>
<tr>
<td>5.4</td>
<td>Handling Constrained Motions</td>
<td>88</td>
</tr>
<tr>
<td>6.</td>
<td>Implementation and Results</td>
<td>89</td>
</tr>
<tr>
<td>6.1</td>
<td>Characteristics Common to All Implementations</td>
<td>89</td>
</tr>
<tr>
<td>6.1.1</td>
<td>Heuristic is Applied Generically</td>
<td>90</td>
</tr>
<tr>
<td>6.1.2</td>
<td>Geometric Modeling with Polytopes</td>
<td>90</td>
</tr>
<tr>
<td>6.1.3</td>
<td>Hierarchical Interference Detection</td>
<td>90</td>
</tr>
<tr>
<td>6.1.4</td>
<td>Animation of Paths</td>
<td>92</td>
</tr>
<tr>
<td>6.1.5</td>
<td>Description of Programs</td>
<td>93</td>
</tr>
<tr>
<td>6.2</td>
<td>CIRSSE Testbed</td>
<td>95</td>
</tr>
<tr>
<td>6.2.1</td>
<td>Single Puma 560</td>
<td>96</td>
</tr>
<tr>
<td>6.2.2</td>
<td>Single 9 DOF Robot</td>
<td>100</td>
</tr>
<tr>
<td>6.2.3</td>
<td>Cooperating Puma 560’s</td>
<td>102</td>
</tr>
<tr>
<td>6.2.4</td>
<td>Cooperating 9 DOF Robots</td>
<td>106</td>
</tr>
<tr>
<td>6.2.5</td>
<td>Effect of String Tightening</td>
<td>110</td>
</tr>
<tr>
<td>6.3</td>
<td>NASA Langley's Automated Structure Assembly Lab</td>
<td>111</td>
</tr>
<tr>
<td>6.4</td>
<td>Cooperating Pumas Assemble a Truss</td>
<td>113</td>
</tr>
<tr>
<td>7.</td>
<td>Discussion of the Path Planning Strategy</td>
<td>117</td>
</tr>
<tr>
<td>7.1</td>
<td>Completeness</td>
<td>117</td>
</tr>
<tr>
<td>7.2</td>
<td>Computational Complexity</td>
<td>118</td>
</tr>
<tr>
<td>7.2.1</td>
<td>Possible Benefits of Parallel Processing</td>
<td>119</td>
</tr>
<tr>
<td>7.3</td>
<td>Overall Effectiveness</td>
<td>120</td>
</tr>
<tr>
<td>8.</td>
<td>Conclusions and Future Work</td>
<td>121</td>
</tr>
<tr>
<td>8.1</td>
<td>Conclusions</td>
<td>121</td>
</tr>
<tr>
<td>8.1.1</td>
<td>Advantages</td>
<td>122</td>
</tr>
<tr>
<td>8.1.2</td>
<td>Disadvantages</td>
<td>123</td>
</tr>
<tr>
<td>8.2</td>
<td>Future Work</td>
<td>124</td>
</tr>
<tr>
<td>8.2.1</td>
<td>Improvement to String Tightening Process</td>
<td>124</td>
</tr>
<tr>
<td>8.2.2</td>
<td>Integration with the CIRSSE Geometric State Manager</td>
<td>125</td>
</tr>
</tbody>
</table>
8.2.3 Utilization of Parallel Processing ................................. 125
8.2.4 Guaranteeing Completeness ........................................ 125
8.2.5 Decidability ....................................................... 126

LITERATURE CITED .................................................................. 127

APPENDICES ........................................................................... 136

A. CIRSSE Testbed Kinematic Frames ...................................... 136
   A.1 Coordinate Frames ....................................................... 136
      A.1.1 Assignment/Labeling of Frames ............................... 136
   A.2 Software Joint Limits for the PUMAs .............................. 140
   A.3 Pose Names .............................................................. 142

B. Data for Examples Presented in Thesis .................................. 146
   B.1 Data for Examples 1 and 2 ............................................ 146
   B.2 Data for Example 3 ...................................................... 147
   B.3 Data for Example 4 ...................................................... 148
LIST OF TABLES

Table 2.1  Single Robot vs Cooperating Robot Path Planning .... 28
Table 2.2  Mobile Robot vs Manipulator Path Planning ........... 33
Table 6.1  Summary of Results for CIRSSE Testbed Examples (times in seconds) ......................................................... 97
## LIST OF FIGURES

<table>
<thead>
<tr>
<th>Figure 1.1</th>
<th>Two 9-DOF Robots Working Cooperatively</th>
<th>2</th>
</tr>
</thead>
<tbody>
<tr>
<td>Figure 1.2</td>
<td>The CIRSSE Testbed</td>
<td>4</td>
</tr>
<tr>
<td>Figure 2.1</td>
<td>A 2D Planar Robot and its Configuration Space</td>
<td>13</td>
</tr>
<tr>
<td>Figure 2.2</td>
<td>Exhaustive Mapping of Concavities Using A* Heuristic</td>
<td>14</td>
</tr>
<tr>
<td>Figure 2.3</td>
<td>Goal Directed Sliding</td>
<td>17</td>
</tr>
<tr>
<td>Figure 2.4</td>
<td>Vector Based Divide-and-Conquer</td>
<td>20</td>
</tr>
<tr>
<td>Figure 2.5</td>
<td>Hypercube Subdivision Algorithm</td>
<td>31</td>
</tr>
<tr>
<td>Figure 3.1</td>
<td>Choice of Goal Joint Angles May Affect Solvability</td>
<td>40</td>
</tr>
<tr>
<td>Figure 4.1</td>
<td>2D Example of C-Space Traversal Heuristic</td>
<td>52</td>
</tr>
<tr>
<td>Figure 4.2</td>
<td>Example Which Dismisses an Intermediate Point</td>
<td>55</td>
</tr>
<tr>
<td>Figure 4.3</td>
<td>Scenario Which Would Result in Non-Disjoint C-Space</td>
<td>56</td>
</tr>
<tr>
<td>Figure 4.4</td>
<td>Example with Non-Disjoint Safe Space and Multiple Searches</td>
<td>57</td>
</tr>
<tr>
<td>Figure 4.5</td>
<td>3D Example of C-Space Traversal Heuristic</td>
<td>57</td>
</tr>
<tr>
<td>Figure 4.6</td>
<td>2D Example for which Heuristic Fails by Cycling</td>
<td>61</td>
</tr>
<tr>
<td>Figure 4.7</td>
<td>Procedure 3 vs Procedure 4</td>
<td>68</td>
</tr>
<tr>
<td>Figure 5.1</td>
<td>Local Effect During String Tightening</td>
<td>86</td>
</tr>
<tr>
<td>Figure 5.2</td>
<td>String Tightening May Not Produce Optimal Path</td>
<td>87</td>
</tr>
<tr>
<td>Figure 6.1</td>
<td>Some 2D Polytopes</td>
<td>91</td>
</tr>
<tr>
<td>Figure 6.2</td>
<td>Flowchart of Path Planning Program</td>
<td>94</td>
</tr>
<tr>
<td>Figure 6.3</td>
<td>Sample Results for Single Puma (Example 1)</td>
<td>98</td>
</tr>
<tr>
<td>Figure 6.4</td>
<td>Start Configuration for Example 1</td>
<td>99</td>
</tr>
<tr>
<td>Figure 6.5</td>
<td>Trace of Payload Path for Example 1</td>
<td>99</td>
</tr>
<tr>
<td>Figure 6.6</td>
<td>Sample Results for Single 9 DOF Robot (Example 2)</td>
<td>101</td>
</tr>
</tbody>
</table>
Figure 6.7 Sample Results for Cooperating Pumas (Example 3) .......... 104
Figure 6.8 Start Configuration for Example 3 ........................................ 105
Figure 6.9 Goal Configuration for Example 3 ........................................ 105
Figure 6.10 Sample Results for Cooperating 9 DOF (Example 4) .......... 108
Figure 6.11 Start Configuration for Example 4 ........................................ 109
Figure 6.12 Goal Configuration for Example 4 ........................................ 109
Figure 6.13 String Tightening a Path for Cooperating Nine DOF Robots . 110
Figure 6.14 NASA Langley's Automated Structure Assembly Lab .......... 114
Figure 6.15 6 DOF Merlin Robot with End Effector for Truss Assembly . 115
Figure 6.16 102 Strut Truss Structure .................................................... 115
Figure 6.17 Workcell for Cooperating Pumas Assembling Truss .......... 116
Figure A.1 Coordinate Frame Assignments .......................................... 144
Figure A.2 Left Half Coordinate Frame Assignments ........................... 145
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Abstract

A method has been developed to plan feasible and obstacle-avoiding paths for two spatial robots working cooperatively in a known static environment. Cooperating spatial robots as referred to herein are robots which work in 6D task space while simultaneously grasping and manipulating a common, rigid payload. The approach is configuration space (c-space) based and performs selective rather than exhaustive c-space mapping. No expensive precomputations are required. A novel, divide-and-conquer type of heuristic is used to guide the selective mapping process. The heuristic does not involve any robot, environment, or task specific assumptions. A technique has also been developed which enables solution of the cooperating redundant robot path planning problem without requiring the use of inverse kinematics for a redundant robot.

The path planning strategy involves first attempting to traverse along the configuration space vector from the start point towards the goal point. If an unsafe region is encountered, an intermediate via point is identified by conducting a systematic search in the hyperplane orthogonal to and bisecting the unsafe region of the vector. This process is repeatedly applied until a solution to the global path planning problem is obtained. The basic concept behind this strategy is that better local decisions at the beginning of the trouble region may be made if a possible way around the "center" of the trouble region is known. Thus, rather than attempting paths which look promising locally (at the beginning of a trouble region) but which may not yield overall results, the heuristic attempts local strategies that appear promising for circumventing the unsafe region.

Although this method cannot guarantee finding a solution even if one exists, and in spite of its $O(k^{n-1})$ (where $k = 2$ or $3$ as implemented) complexity for $n$ degree of freedom problems, it has demonstrated the ability to solve a variety of practical yet potentially difficult path planning problems within a reasonable amount
of computation. The method inherently handles singularities and is applicable to robots having any number and type of joints. Parallel processing could be used to greatly reduce solution time.

Because the main emphasis of the path planning method is to produce a feasible path without regard to any type of optimality, the paths developed are often rather inefficient. Thus, a configuration space based algorithm was developed to modify any feasible path found by the planner into a more efficient one, where efficiency is measured by the length of the c-space trajectories.

Although the key motivation behind this work was to address the path planning problem for two cooperating robots, the methods developed are directly applicable to single robots as well. The path planner is implemented in C and utilizes polytope models of the robots and obstacles for purposes of interference detection. The path planner is demonstrated via computer graphics simulation on a Sun SparcStation 1 for several single and cooperating robot cases, including cooperating nine degree of freedom (1P-8R) robots.
1.1 Motivation

Robotics is a technology with a promising future. The explosion of knowledge resulting from past and present research efforts will manifest itself in robotic systems capable of emulating the human attributes of mobility, dexterity, intelligence, and sensory perception. There will be mobile bases with multiple cooperating arms having extensive sensing capability which are able to receive high level instructions and translate those instructions into a specific sequence of low level actions required to execute the desired task. Robotic systems of the near future will strive for increased flexibility, improved reliability, and greater autonomy.

One issue which arises in attempts to develop more autonomous robotic systems is the path planning problem. The path planning problem involves determining if a continuous and obstacle avoiding path exists between a robot's start and goal positions, and, if so, to determine such a path. If the mathematical space of concern is considered to be the configuration space (c-space) of the robot, then the problem is effectively that of finding a connected graph through c-space between the start and goal positions which traverses only feasible and collision free points. This path planning problem can become very computationally intensive. In fact, an upper bound on the complexity of the n degree of freedom (dof) path planning problem is $O(n^n)$, i.e., complexity of the path planning problem is exponential in the number of dof [1-3]. To illustrate the rapid growth in complexity with number of dof, note that a six dof problem would be more complex than a two dof problem by a factor of $6^6 / 2^2$, or 11,664.

A subset of the general path planning problem just described is the path
planning problem for two cooperating robots. Robotic cooperation herein refers to the scenario whereby both robots simultaneously grip and manipulate a common, rigid, payload. Since the two arms grasp the object rigidly, the relative position and orientation of the two grippers must be invariant during the motion. As an example of two arm cooperation, refer to Figure 1.1, where two nine degree of freedom robots are shown cooperatively manipulating a long, cylindrical payload.

![Figure 1.1: Two 9-DOF Robots Working Cooperatively](image)

The effective number of degrees of freedom or mobility, $m$, for two spatial robots working cooperatively in six dimensional task space can be simply computed from:

$$m = n_1 + n_2 - 6$$  

(1.1)

where $n_i$ represents the number of degrees of freedom for robot $i$, and the '$-6$' term results from the closure constraint imposed by cooperation.

There are many potential applications for two arm cooperation. For example, a space station will most likely be built using robots to minimize the expense and risk of putting humans into space. In order to be most effective, the robot arms
would likely cooperate and be autonomous or at least semi-autonomous. The attractiveness of lightweight robots for space applications increases the likelihood that robotic cooperation would be necessary to manipulate large or massive payloads. In industry, robotic cooperation might be employed for moving very large or very flexible payloads which exceed the capacity of a single arm or require support at more than one point. Cooperating robots could also be used to manipulate two parts with mating surfaces but which are not fastened to each other.

The addition of a second manipulator for cooperative work leads to an inherently complex system. One key research issue and open problem associated with a system of cooperating robots is the path planning problem. The cooperating robot path planning problem must consider not only collision avoidance but also the kinematic closure requirement that both robots are able to reach their respective grasp positions at all times. Dooley [4] shows how the closure constraint plus obstacle constraints for cooperating planar robots can combine to produce a configuration space containing many unusually shaped unsafe regions and relatively little safe space. One can conclude both intuitively and from Dooley’s work that the path planning problem in the cooperating robot case will typically be more difficult than in the single robot case.

Numerous approaches to the general single arm path planning problem have appeared in the literature. Most do not appear directly suited to the case of two cooperating robot arms. Many of these approaches do, however, attempt to find a path while applying some heuristic to selectively search configuration space. The only practical planners to date for a general six degree of freedom (dof) robot involve simplifications or heuristics and are not complete, i.e., they cannot guarantee finding a solution even if one may exist. Many of the approaches in the literature which do address path planning for cooperating robots consider only planar systems and cannot be practically extended to the case of two robots having six or
more dof each. Some researchers have solved the cooperating arm path planning problem with multi-dof spatial (working in 6D task space) robots but they present results only for relatively (or completely) obstacle-free environments. The difficulty which researchers have experienced in trying to solve the general cooperating robot path planning problem is evidence of the inherent complexity of the problem and highlights the need for further study.

The work presented herein was funded by the Center for Intelligent Robotic Systems for Space Exploration (CIRSSE), a NASA sponsored research center at Rensselaer Polytechnic Institute (RPI), and is part of CIRSSE's efforts to develop autonomous and teleoperated single and cooperating robot systems for use in space. The CIRSSE testbed, a computer graphics representation of which is shown in Figure 1.2, includes two nine dof robots which may work independently or cooperatively.

Figure 1.2: The CIRSSE Testbed
Each nine dof robot consists of a 6 dof (6R) Puma 560 mounted to a 3 dof (1P-2R) platform. As shown in the figure, each platform has a translate, a rotate, and a tilt axis. The testbed has extensive sensing capabilities, including various CCD cameras, laser range finding, and force/torque sensing end effectors. The principle motivation for this work was the desire to develop a practical and potentially useful path planner for cooperating robot scenarios on the CIRSSE testbed. Nonetheless, the strategy herein is completely general and no assumptions are made which would limit the usefulness of the approach to specific robots, environments, or tasks.

1.2 Direction of this Work

This section briefly summarizes the assumptions, goals, strategy, and results of the work presented in this thesis.

1.2.1 Assumptions

This work assumes the following:

1. Forward kinematic models of the robots are available.

2. Inverse kinematic models of the robots are available for six dof robots or for the final six links of redundant robots.

3. Geometric models of the robots, payload, and obstacles are available.

4. Obstacles in the workspace are static.

5. Feasible and collision free start and goal joint configurations of the robots are known, as are the start and goal positions of the payload.

6. Motion between the specified start and goal positions may be arbitrary.

7. The planner may ignore robot dynamics.
1.2.2 Goals

The goals of this work are to develop a planner capable of solving the cooperating robot path planning problem while satisfying the following:

1. The planner shall locate reasonable collision-free paths in a time frame suitable for off-line path planning.
2. The planner shall be capable of modifying a feasible path into a more efficient one.
3. The planner shall be applicable to various robotic systems and various tasks.
4. The planner shall be practical for cooperating six dof manipulators as a minimum, and ideally for cooperating redundant robots.
5. The planner output shall be a sequential listing of closely spaced knot points in joint space which represent the discretization of a continuous, feasible, and obstacle avoiding path connecting the start and goal configurations.

1.2.3 Strategy

This thesis presents a new method for performing global path planning for two cooperating spatial robots in a static environment. Like the single arm planner presented by Dupont [5], the principle strategy is to minimize the computationally expensive mapping of configuration space by performing mapping on an as required basis. The planner satisfies the goals outlined in Subsection 1.2.2. The approach is based around a novel, divide-and-conquer style heuristic for traversing through c-space. This c-space traversal heuristic is directly applicable to the single robot path planning problem and can be easily tailored to the case of two cooperating robots. In all cases the dimensionality of the c-space considered is an accurate reflection of the actual problem complexity. Computationally expensive precomputations and
exhaustive c-space mappings are avoided. This thesis also presents a technique which allows the path planning method to be applied to cooperating redundant robots without requiring the use of inverse kinematics for a redundant robot. The path planning method is applicable regardless of the number and type of joints in the robot and for any number of obstacles in the workspace. A string tightening algorithm is presented to modify any safe path found by the planner into a more efficient one, where efficiency is measured by the length of the joint space trajectory.

The path planning method involves first attempting to traverse a c-space vector from the start to the goal of one of the robots. If this vector passes through unsafe space, the hyperspace orthogonal to and bisecting the unsafe segment of the vector is systematically searched to identify an intermediate goal point for consideration as a via point. An attempt is made to traverse from the last safe point to the intermediate goal point. This process is repeated as necessary until the attempted traversal to the newest intermediate goal point is entirely safe. At that point, progression is attempted toward all previous guide points in the opposite order in which they were found, where guide points include not only previous intermediate goal points but also the safe points found on the goal end of each unsafe region which invoked a search. When progression to a particular guide point is not entirely safe, that point is permanently dismissed and progression is attempted toward the next guide point in the specified sequence. The progression continues until an attempt has been made to progress to the global goal point. If that attempted progression is not entirely successful the overall process is repeated until the global goal point has been safely traversed to.

Unfortunately, the path planning method presented herein is not complete, i.e., it cannot guarantee finding a solution even if one exists. Though certainly undesirable, this lack of completeness does not seem unreasonable since researchers have thus far been unable to develop algorithms which achieve both completeness
and practicality for reasonably difficult yet practical path planning problems for more than a few degrees of freedom. Since our emphasis was toward achieving a potentially useful path planner for cooperating robots with at least six dof each, we sacrificed completeness in exchange for the possibility of solving some practical yet potentially difficult problems as quickly as possible.

Unlike some path planning techniques which are geometric model data structure specific, our planner may be used with any geometric modeling scheme which allows for interference detection. Our implementation utilizes polytope representations of the links of the robots and of the obstacles in the workspace as presented by Schima [6]. The polytope scheme was chosen because it allows for detailed modeling of objects while enabling relatively fast interference checking. The potential speed of the collision detection is enhanced by the fact that the method simply needs a yes or a no regarding collisions and does not require distance or direction information. Mapping a particular point in c-space involves verifying that the closure constraint can be met, updating polytope models of the robot links and payload, and performing two phase interference detection calculations on the resulting polytopes. The first phase of interference detection simply checks for interference between spheres which bound each polytope. If the spheres intersect indicating possible collision then the second phase of interference detection must be invoked. The second phase accurately determines whether or not two polytope models intersect.

1.2.4 Results

Despite its simplicity, the methodology presented herein appears to solve the cooperating robot path planning problem better than other approaches presented in the literature. The method is also applicable to the single robot path planning problem. The approach does, however, suffer from one drawback currently afflicting all practical motion planners which can handle six or more dof, namely that it may
fail to find a solution even if one exists. An upper bound on the complexity of the planner is $O(k^{n-1})$ for an $n$ dof problem, where $k < n$. For our implementation, $k = 3$ for all cases except cooperating redundant manipulators for which $k = 2$. This compares favorably to the actual problem complexity which has an upper bound of $O(n^n)$.

Sample results are included for a single six dof robot, a single nine dof robot, cooperating six dof robots, and cooperating nine dof robots. The results illustrate the planner’s ability to solve practical yet potentially difficult problems. The path planner was implemented in the C programming language and runs on a Sun SparcStation 1. Paths found by the planner are animated using CimStation, a commercially available computer graphics robot simulation package [7]. Typical time required to find a feasible path for cooperating nine dof robots (the most complex scenario considered) with several workspace obstacles is less than 30 minutes. After finding a feasible path, the string tightening process for cooperating nine dof robots typically requires about 15 minutes of computation. Parallel processing could be used to significantly reduce execution times for both the path planning and string tightening routines since both involve a large number of independent calculations.

1.3 Overview of Thesis

The remainder of this thesis is presented in seven main chapters:

- Literature Review
- Problem Statement
- Divide-and-Conquer C-Space Traversal Heuristic
- Utilizing the Heuristic for Robot Path Planning
- Implementation and Results
• Discussion of the Path Planning Strategy
• Conclusions and Future Work

A literature review on published techniques for single and cooperating robot path planning is discussed in Chapter 2. The path planning problem is formally defined in Chapter 3. Chapters 4 and 5 present the central contribution of this thesis, namely a new c-space traversal heuristic and means for utilizing the heuristic to solve single and cooperating robot path planning problems. In Chapter 6, implementation details and results are presented for application of the path planning strategy with string tightening to four cases: a single six dof robot, a single nine dof robot, two cooperating six dof robots, and two cooperating nine dof robots. A discussion of the path planning strategy is given in Chapter 7. Finally, Chapter 8 presents some conclusions and some areas for future work.
CHAPTER 2
Literature Review

This chapter presents a literature review on the subject of robot path planning. The chapter is organized into the following main sections:

• Path Planning for Single Robots
• Path Planning for Cooperating Robots
• Other Related Areas of Research
• Summary of the Literature Review

While we are specifically interested in path planning for cooperating robots, an understanding of current methods for a single robot is pertinent to determining the possible suitability of extending those methods to consider cooperating robots. Hence, the discussion below includes methods for both single robots, presented in Section 2.1, as well as for cooperating robots, presented in Section 2.2. Other related areas of path planning research are briefly discussed in Section 2.3. Finally, a brief summary of the literature review is presented in Section 2.4. A brief review of literature regarding algorithms for string tightening is presented later in Section 5.3.1.

2.1 Path Planning for Single Robots

Published approaches to the single robot path planning problem are discussed in this section. Most of these approaches can be characterized as one of the following three types:

• A graph search approach
• A potential fields approach

• A human assisted approach

These categorizations are not mutually exclusive, and a combination of them is often used in a path planning strategy. These approaches are discussed below.

2.1.1 The Graph Search Approach

One approach to solving the path planning problem could be referred to as the graph search type approach. Such an approach will work directly in the configuration space (c-space) in attempt to find a connectivity graph of safe points between an initial configuration and a goal configuration [5,8-33].

Configuration space as first suggested by Lozano-Perez and Wesley [33] refers to the $n$-dimensional space formed by the $n$ values of the joint variables of a robot with $n$ degrees of freedom (dof). Thus, each possible configuration which the robot can assume is represented by a point in the configuration space. The robot path planning problem is thus equivalent to the motion planning problem of a point in c-space. The concept of c-space is illustrated in Figure 2.1. Consider the 2R planar manipulator shown in Figure 2.1a. If it is assumed that each joint has both upper and lower limits then the resulting c-space is rectangular as shown in Figure 2.1b. If there were no joint limits the resulting c-space would be toroidal.

C-space can be divided into two regions: safe and unsafe. Safe space refers to the locus of all points in configuration space which represent feasible and collision free configurations. All space which is not safe for any reason is simply categorized as unsafe space.

A path planning technique is considered complete if it can either guarantee finding a solution if one exists or prove that one does not exist. Early efforts at developing complete graph search techniques indicate that path planning in this fashion is exponential in the number of degrees of freedom. For example, Reif [1]
examined the 3D generalized mover's problem. The mover's problem (often referred to as the piano mover's problem) involves path planning for a single solid object. The generalized mover's problem involves path planning for an object which may consist of multiple objects kinematically linked together (such as a robot arm). The fact that Reif could show this generalized problem is PSPACE-hard is evidence that the computational bounds for robot motion planning problems in fact grow exponentially with degrees of freedom. An explanation of PSPACE-hardness may be found in [34]. An upper bound on complexity of the robot path planning problem is $O(n^n)$ for an $n$ dof robot [2, 3].

Most graph search techniques utilize global world knowledge. In addition, many use an A* type of heuristic search to find a feasible path. The A* algorithm is a common search procedure whereby paths to the goal are built and compared based
on a heuristic estimate of the cost remaining to reach the goal. The algorithm continually expands the most promising path until a solution is found. Unfortunately, searching for the optimal path has led most researchers to transform all obstacles into c-space [9,17-19,21-25,28,30,31]. Because of the higher order complexity of such a technique, the more successful works involved simplifications to reduce problem dimensionality [12, 17, 18, 26]. The basic shortcoming of the A* type searches is the fact that they tend to exhaustively map out concavities encountered in trying to go between the start and the goal. A 2D example of this phenomenon is illustrated in Figure 2.2. The likely computational expense of such an approach makes it impractical for motion planning for robots with more than a few dof. The A* algorithm can also be applied bidirectionally by considering extending the path from both the start and the goal positions. Bidirectional searching can be effective since it is generally easier to move from a cluttered space to an open space than vice versa.

Figure 2.2: Exhaustive Mapping of Concavities Using A* Heuristic

Other complete techniques which are not computationally practical for higher degrees of freedom are presented by Branicky [35], Canny [13], and Paden [36]. Kondo [37] has reported a fast and complete algorithm for six dof robots, but the algorithm's speed is only demonstrated for apparently simple problems.

Chen and Hwang [38] present a complete solution technique with performance
commensurate with task difficulty. Essentially, they use a global planner to select regions of collision free space which connect the start and goal and then use a local planner to solve the path planning problem within each region. The resolution of the regions is only as fine as necessary to find a solution using a heuristic to select promising regions for further subdivision. In this way, easy problems may be solved relatively quickly and yet an extremely difficult problem may be resolved to whatever level is required to obtain a solution or conclude one does not exist. Their algorithm solves a relatively simple yet practical disassembly task for a five dof Adept robot in three minutes on a 16 MIPS workstation.

Sharir [32] notes the mathematical complexity and size of the general complete solution of robot motion planning in an n-dimensional c-space and presents a graph search algorithm aimed at solving it. Sharir develops an algorithm which is conceptually applicable to a system of arbitrary dimension. His algorithms can be most easily described by considering the 2D problem of planning the movement of a line segment in a planar space containing polygonal obstacles. The line segment is free to translate but may not rotate. Sharir's algorithm groups the 2D c-space into closed polygonal regions which are homogeneous (completely safe or unsafe). Then the problem of motion planning becomes that of searching for a connectivity graph between the initial and final positions in the polygon which contains those points. While this approach is interesting and successful in 2D, Sharir acknowledges that both the breaking down of regions in configuration space and the graph search suffer from higher order explosion; to the point of intractability.

The mathematical complexity of the general motion planning problem has resulted in many techniques which reduce the problem dimensionality via simplifications. Some such simplifications have included allowing only cartesian manipulators [24], requiring arm seperability (small wrists which orient a spherical payload) [15,17,18,23,26,28,39-41], or allowing only certain motions and obstacle
types [12, 20, 26, 42]. None of these constraints can be used for path planning for two cooperating robot arms.

Gupta [43] presents a sequential search strategy which plans the motion of each robot link successively starting from the base. While not complete for robots with three or more links, this technique is very efficient and may be useful for quickly solving some simple problems.

One technique which has been used for path planning in c-space involves hypothesizing a path and then testing it at a finite number of intermediate points for collisions. The path is repeatedly modified heuristically until a solution is found. Lewis [44] suggested precomputing commonly used path segments referred to as freeways and recommended the use of intermediate safe points to avoid detected collisions. However, he presented no mechanism by which to determine these intermediate safe points.

Pieper [45] applied various cartesian heuristics to attempt to bypass obstacles. The arm could fold to move in front of or above detected obstacles. Pieper found that certain obstacle arrangements resulted in the manipulator oscillating between obstacles. In addition, the algorithm generally failed if the only acceptable path led between two obstacles.

Glavina [46] presents a heuristic path planning method which combines goal-directed searches with randomized searches as needed. The algorithm proceeds straight in c-space from start towards goal until an obstacle boundary is encountered. At that point, the point slides along the obstacle boundary if and only if such motion will reduce the distance to the goal. In 2D, sliding is attempted by searching for a safe point along a line orthogonal to the desired direction passing through the first point which violated an obstacle boundary. This concept is illustrated in Figure 2.3. If this sliding alone is not sufficient to clear the obstacle, a new subgoal is created at random and the process is repeated until a feasible path to the goal is found.
Glavina has results for a 2D prototype and hopes to extend the procedure to a six dof general purpose manipulator. For the six dof problem, Glavina proposes perhaps checking 10 possible sliding directions corresponding to each direction of the basis axes of the 5D hyperplane along which sliding can be attempted. Further research is planned to determine if it is necessary to expand the set of test vectors beyond this set.

Many papers have dealt with the motion planning of polygons or polyhedral objects [8, 11, 13, 15, 18, 24, 47]. While this is the simplest form of the motion planning problem, this research is useful for mobile robot path planning and forms a foundation for planning problems of higher dimensionality. The actual methods used, however, have generally not extended into higher dimensions easily due to the added complexity of that space. Mobile robot path planning has been an attractive
research area because of the low dimensionality involved and because of the practical applications of mobile robots [9, 21, 22].

Lozano-Perez and Wesley [26, 33] present a visibility graph (vgraph) technique for polygonal and polyhedral objects. Vgraphs are graphs whose nodes are the vertices of polyhedral c-space obstacles. Nodes which are visible to each other are linked and assigned a weight proportional to the distance between them. The graph is then searched for the optimal path. It is difficult to effectively apply vgraphs to problems in more than two dimensions. For example, the vgraphs can be constructed from the vertices of polyhedra, but the shortest path no longer lies in the visibility graph.

Rovetta [48] presents a more recent variation on the vgraph method whereby all obstacles which impede the traversal straight from start to goal are grouped into a single monoobstacle consisting of the convex hull of the individual problem obstacles. Such an approach reduces computation and produces more efficient paths but it may convert a solvable problem into an unsolvable one.

Two other free space searching techniques include generalized cones [49] and voronoi diagrams [8, 50, 51]. The first technique produces a safe path by piecing together the centerlines of generalized cones whose sides are the faces of the obstacles. The generalized cone algorithm translates a polygonal moving body along the axes of the generalized cones and rotates it at cone intersections. This algorithm may fail when an object must translate and rotate simultaneously to avoid obstacles. A voronoi diagram is a collection of surfaces that are equidistant from two or more obstacles. A safe path is found by traversing appropriate regions of these surfaces. These two techniques have the desirable feature of keeping the robot as far from obstacles as possible. In a narrow corridor, this is a desirable feature. In cases which much open space, however, it may yield a much longer path than necessary. It is difficult to apply either of these techniques in more than 2D.
An interesting path planning technique is presented by Lumelsky [52-56]. He makes three assumptions: (1) The arm endpoint can move through a simple curve, (2) when the arm hits an obstacle, it can identify the contact point on the arm, and (3) the robot can follow an obstacle boundary. While only local information is used, Lumelsky's algorithm is complete. He reduces planning a path for a robot to planning a path for a point on the surface of some manifold. In two dimensions he is able to apply his algorithm using the "same turn first" strategy for traversing the surface of any obstacles encountered in the straight line path from start to goal. His work has yet to be implemented for more than two degrees of freedom since, in that case, there are an infinite number of possible directions to follow on the obstacle boundary. To simplify this situation, Petroz and Sirota [57] suggest cutting the obstacles in the higher dimensional c-space with planes to limit the boundary following directions to right and left. The difficulties with this approach are that an infinite number of such planes exist and that a solution will typically need to employ more than one such plane.

Lozano-Perez and Wesley [24, 25, 33] describe an approach for motion planning which is based on the idea of expanding obstacles. This approach essentially involves the expansion of the obstacles in such a manner as to reduce the path planning problem for an n-dimensional shape to an equivalent problem for a single point in that n-dimensional space, where it is the expansion of the obstacles that allows the equivalence. Computational complexity becomes excessively burdensome for cases of dimensionality greater than two. Very little is known about how to apply Lozano-Perez's algorithm to systems with three or more degrees of freedom, although Lozano-Perez has expanded the procedure to consider cartesian manipulators (robots with three prismatic joints).

Warren [58] presents a vector based algorithm currently being developed for planning the path of a robot among irregularly shaped obstacles. In this technique,
a c-space vector is created from the start position to the goal position. If this vector crosses unsafe space, a second vector is used to determine a new intermediate goal and the previous goal is stored for later use. This second vector is drawn from the centroid of the obstacle though the midpoint of the unsafe potion of the initial vector and continues until reaching a point in safe space. The overall procedure is applied repeatedly until the ultimate goal can be reached. A 2D illustration of this approach is shown in Figure 2.4. This technique has a divide-and-conquer flavor to it but has drawbacks which limit its effectiveness to only a few dof. These drawbacks include requiring exhaustive mapping of obstacles and having no guarantee of finding a safe point along the vector from the centroid through the midpoint of the unsafe region.

A recent divide-and-conquer based approach is a heuristic approach for cartesian manipulators presented by Lee [59]. Lee divides the cartesian robot pick-and-place task into a vertical departure motion, an intermediate planar motion, and a vertical approach motion. The 2D vgraph algorithm is used to solve each phase of the problem using heuristics to address part rotation about a vertical axis. This

![Figure 2.4: Vector Based Divide-and-Conquer](image-url)
approach cannot be practically applied to spatial manipulator path planning problems.

Dupont [5] addresses the path planning problem for kinematically redundant manipulators. The basic philosophy employed by Dupont is that of performing selective rather than exhaustive mapping of configuration space thereby minimizing the exponential growth problems associated with complete graph search techniques. The strategy which Dupont follows involves first creating a path which is linear in joint space (c-space) between the start and goal positions. This path is discretized and checked for collisions at each point along the path. Dupont attempts to traverse around regions along the initial path where collisions occur by applying some heuristics to choose a cartesian strategy direction that will likely allow circumvention of the trouble regions. The Jacobian is then used to determine the possible safe c-space moves that achieve the desired task space strategy directions. Octree representations are used to determine if collisions occur for a given configuration. Dupont's algorithm successfully planned obstacle avoiding paths for a seven dof redundant manipulator.

A somewhat similar approach is taken by Kondo et al [60]. Although Kondo's intended application is the movement of parts and assemblies within CAD system representations (this type of problem is often referred to as the piano mover’s problem), the nature of that problem directly parallels the robot motion planning problem. Kondo's basic approach is similar to Dupont's in that he tries to restrict the amount of c-space referred to during a path search (by selectively mapping c-space) in order to avoid executing unnecessary collision detections. Kondo uses octrees and combines a global strategy with a local strategy. The global strategy finds the limits of free space which are encountered in going from the start toward the goal and from the goal toward the start. The local strategy then enumerates only cells along the boundary of the free space which was encountered in attempting
to traverse directly between the start and goal positions. It is in this manner that Kondo’s algorithm greatly reduces the typically burdensome amounts of computation and storage required to fully define an octree representation of the workspace. In addition, by looking only from the start towards the goal (and vice versa) until a collision occurs, Kondo is avoiding searching potentially large islands of safe space which are unreachable. Using the piano mover’s analogy and trying to move the piano from the hallway to the dining room, Kondo’s algorithm will avoid searching the bedroom if there is no possible way the piano could have gotten into the bedroom. Kondo applied his algorithm to determine a collision free path for moving a heat exchanger between two positions in a CAD model of a nuclear power plant.

2.1.2 The Potential Fields Approach

An alternate type of approach is based on the use of artificial potential fields. Such an approach typically regards obstacles as a source of repelling potential field, while the desired goal position represents a strong attractor [61]. The hope is that the moving body can safely traverse from its initial position to the desired goal position simply by following the potential gradient of the resulting field. The square of the inverse of distance to obstacles and the negative of the inverse of distance to the goal are commonly used obstacle and goal potentials, respectively. The potential fields approach is typically implemented in task space [62, 63] although some researchers have examined implementing it in configuration space [64, 65]. Some advantages and disadvantages of potential fields approach are noted below.

2.1.2.1 Advantages of the Potential Fields Approach

1. They are faster than other algorithmic methods developed to date.

2. They are readily extended to systems of higher dimensionality.
3. They inherently tend to produce paths which avoid obstacles with significant clearances.

2.1.2.2 Disadvantages of the Potential Fields Approach

1. They tend to have difficulty with local minima, particularly for systems of higher dimensionality.

2. It is difficult to maintain a global nature since the strength of the attractors and repellors generally is significant only over small distances.

3. They can have difficulty dealing with arbitrarily shaped obstacles.

4. Implementation in c-space requires knowledge of c-space obstacles.

5. The expression for the obstacle potential becomes cumbersome when there are many concave objects.

6. They are not as thorough as graph search techniques.

7. The solutions which are found are not generally not optimal.

8. They require robot to obstacle distance and direction information, a more computationally expensive requirement than a simple yes or no regarding interference.

9. They typically disallow motion very near or along obstacle surfaces, yet docking, parts mating, and other common tasks require navigation near or along the boundary of the safe configuration space.

Hirukawa and Kitamura [66] claim to avoid the deadlocks at local minima by forming a graph in cartesian space of the positions farthest from obstacles. The end effector tries to follow this graph to the goal while the robot links are attracted
toward the lines of the graph. The formation of the graph involves global world knowledge.

Some researchers' efforts to address the local minima problem involve combining the potential fields planning approach with a higher level global planner [65, 67-70].

Warren [65, 71, 72] presents several techniques for global path planning using potential fields. One approach is to first choose a trial path and then to modify that path by the addition of intermediate points until it represents an acceptable solution. The intermediate points are found using the potential function. By choosing the trial path as a series of more closely spaced points than the entire global problem, Warren greatly reduces (but does not eliminate) the possibility of being caught in local extrema of the field. Another approach utilizes the penalty function simply to modify the unsafe regions of a trajectory initially proposed by the planner. The result is that the path is modified only where it intersects an obstacle thereby reducing global sensitivity to the local minima problem. Warren illustrates his techniques for several cases: a 2D revolute manipulator, a mobile robot capable of translation only, and a mobile robot capable of translation and rotation.

Munger [70] takes an approach much like Warren's described above in that he divides the global problem into a series of shorter problems which go through some number of safe intermediate points. The idea then is to solve a series of shorter problems which can be combined to yield a global solution. Munger applies his algorithm to a nine degree of freedom manipulator assembling struts to form a tetrahedron. The workcell for Munger's application is relatively uncluttered. Applying this technique to general robot path planning problems is potentially troublesome due to the difficulty in identifying the intermediate points appropriately so as to enable a solution to be found.
Kim and Khosla [73] propose a different means to handle the local minima problem. Their approach uses harmonic function based potential functions with the property that they are free from local minima in a singularity free space. The panel method, a tool from computational fluid mechanics, is used to solve the potential flow problem. For point mobile robots this ensures well behaved potential functions which can be solved quickly even with complex and concave obstacles. For nonpoint robots the geometry introduces structural local minima which are positions where the robot can no longer safely move along the potential's gradient. Kim and Khosla have applied this method to a bar shaped mobile robot and a 3 dof planar manipulator. They note that it should be possible to extend their technique to 3D problems by using 3D harmonic functions. Their work also illustrates that the local minima problem still persists even with obstacles having simple shape.

Other means of addressing the local minima problem include generalized potentials [74], a Laplacian approach [75], and a local minima free technique for generalized disc obstacles in a generalized sphere world [76].

Faverjon et al [77] address the problem of having the potential function discourage paths near obstacles by basing the potential function on the object approach velocity.

Barraquand and Latombe [78] present an algorithm which is geometrically similar to Glavina's (see Section 2.1.1). Barraquand combines potential functions and graph search techniques to solve problems with a high number of dof. The algorithm builds a graph connecting local minima of a potential function in c-space and searches this graph for sequences which will produce a solution. Local minimum are connected to each other using a Monte-Carlo randomized motion as needed to escape the first local minimum followed by a gradient motion based on the potential function. The local minima graph is searched depth first with random backtracking. The algorithm is complete since, given due computation time, an exhaustive search
would eventually result. Barraquand presents results for a relatively simple problem with a 31 dof manipulator which was solved in 15 minutes. The planner’s ability to quickly solve more difficult but practical problems is not demonstrated in [78].

Lozano-Perez [79] present a task-level approach which involves both potential fields and c-space graph search methods. Lozano-Perez solves the pick-and-place problem by decomposing it into nearly independent, computationally feasible, sub-problems. The two main subproblems are the grasp locations and approaches thereto (at both the pick and place ends of the motion) and the gross translational motion from the general locality of the pick location to the general locality of the place location. A grasp position is determined by transforming the obstacles at the place location to their equivalently limiting positions at the pick location and searching the resulting c-space for a feasible grasp position. Having determined the grasp points, Lozano-Perez uses a potential fields approach (and some trial and error) to determine an arbitrary free approach/departure point in the vicinity of both the pick and the place locations. The final phase of Lozano-Perez’s task planning is then to plan the free motion plan between the departure point and the approach point. This is done using c-space obstacle mapping and includes the assumptions that orientation may be neglected and that the first three robot joints invoke 3D translation. Exhaustive mapping of the resulting 3D c-space is avoided by progressing in 2D slices within that space until a solution is found.

2.1.3 The Human Assisted Approach

The mathematical complexity of a computed complete (even if suboptimal) solution to the general motion problem apparently make it intractable for more than a few degrees of freedom. Humans seem to possess some natural abilities to “see” solutions to many motion planning problems for which computing a solution is still difficult or excessively computationally intensive. It is precisely this apparent human
ability that the human assisted approach to path planning attempts to capitalize on.

In its simplest form, human assisted path planning is accomplished on-line. This usually involves moving the robot using a teach pendant and storing a series of points along a collision-free path. The points can later be re-played in sequence to execute the desired task.

More typically, the human assisted approach employs computer graphics models of the robot and its environment. The user can then perform the motion planning in an off-line graphical manner. It is usually possible to display multiple views to allow the user to detect any potential collisions. More advanced systems can automatically perform the collision checking. Systems which can compute estimated task execution time can also allow the user to search for a very efficient path. As the number of times a particular task is to be repeated increases, the benefits of obtaining a very efficient path become more pronounced.

Some systems presented in the literature which are suitable for the human assisted approach to off-line path planning are presented by Derby [80], Hornick and Ravini [81], Stobart [82], and Han [83].

More recently, advances in telerobotics has produced systems in which people may be employed as on-line path planners. Telerobotics, as described by Weisbin [84], includes three main paradigms of control:

1. **Teleoperation**, in which a human directly controls the remote device in real time

2. **Robotics** - in which the remote device is preprogrammed

3. **Supervisory Control** - in which the human controller gives high level commands which are decomposed and executed by the machine under human supervision.

Human assisted path planning would typically be involved in paradigm (1), whereas
autonomous path planning could be integrated into paradigm (3) to eliminate some of the burden on the operator.

2.2 Path Planning for Cooperating Robots

While they are inherently similar, there are some key differences between motion planning for single manipulators and for cooperating robots. Some of these differences are shown in Table 2.1. These differences are discussed later in Section 4.1.

<table>
<thead>
<tr>
<th>Single Robot Path Planning</th>
<th>Cooperating Robot Path Planning</th>
</tr>
</thead>
<tbody>
<tr>
<td>Typically relatively large amounts of free space available.</td>
<td>Closure constraint leads to comparatively little free space.</td>
</tr>
<tr>
<td>Translations and rotations may often be decoupled.</td>
<td>End effector orientation important for maintenance of feasible configurations.</td>
</tr>
<tr>
<td>Task space heuristics often effective for path planning.</td>
<td>Second robot makes effective use of task space heuristics very difficult.</td>
</tr>
<tr>
<td>C-space approaches inherently handle multiple arm configurations.</td>
<td>Configuration of second robot must be considered explicitly.</td>
</tr>
</tbody>
</table>

Table 2.1: Single Robot vs Cooperating Robot Path Planning

In comparison to the single robot path planning problem, the cooperating robot path planning problem has thus far received relatively little attention in the research community. Perhaps this is because an efficient exact algorithm for single robot planning is yet to be developed. Nonetheless, several researchers have specifically considered the cooperating robot path planning problem. Their efforts are summarized below.

Chien [85] presents a path planning technique for two cooperating planar robots each having two links and three revolute joints. Chien's solution process
involves dividing the subspace into two 2D subspaces, one for each of the two possible configurations of the second robot given a specified configuration of the first. These two subspaces are connected by transition configurations for which the configuration in each of the two subspaces is the same. The "same turn first" strategy, an algorithm which guarantees finding a solution if one exists, is used to search for a sequence of moves within and between the two 2D subspaces which will connect the start and goal configurations. While this technique is complete, its practicality is apparently limited to planar robots.

Koga and Latombe [86] present a complete planning technique for cooperating arms with only a few degrees of freedom. The technique is based upon systematic searches of c-space grids. They present another planner which is not complete but is practical for more dof. This technique uses randomized potential fields planning techniques similar to Latombe's prior single arm work [78] discussed in Section 2.1.2. The technique has been implemented for redundant planar manipulators. Unlike other research discussed herein, Koga and Latombe allow the grasp positions of the robots to be altered during a manipulation by temporarily halting motion of the payload and repositioning an end effector. Thus far, their potential fields planner requires some assumptions which significantly affect the planner's reliability. Difficulty was also experienced with more than a few obstacles.

An analytical technique for single robot path planning involves the use of kinematic constraints to pose the path planning problem as an analytical optimization problem. Seereeram and Wen [87] present an example of such a technique by posing the path planning problem as a finite time nonlinear control problem and solving it using a Newton Raphson type algorithm. This approach represents the requirement of obstacle avoidance with a set of inequalities on the configuration variables. Such approaches are still under development and may prove useful in the future for solving practical problems for robots with many dof. Lim and Chyung [88] apply
a similar technique to the cooperating robot path planning problem by reformulating the problem as a non-linear optimization problem. Their methodology essentially involves determining an admissible trajectory for the object being grasped, where admissibility involves reachability by both robots. This method determines a feasible path by employing optimization methods to modify the cartesian straight line/constant rotation path of the object. Since the feasibility of an object path is investigated at the joint level, the resulting solution is in joint space. No provisions are made for collision detection or obstacle avoidance. Lim presents results for determination of a simple trajectory for two cooperating five degree of freedom RHINO robot arms. It is unclear whether Lim's methodology would be applicable to more difficult problems requiring obstacle avoidance and arm configuration changes.

Hu [89] presents an approach to control multiple cooperating redundant manipulators. While control rather than path planning is Hu's primary concern, the approach allows use of the redundancy to avoid collisions between the robots and obstacles while traversing a specified task space trajectory. Determination of a suitable task space trajectory for the payload would still require some type of higher level path planner.

McCarthy and Bodduluri [90] examine the design and motion planning problem for closed kinematic chains such as cooperating robots. Their motion planning algorithm utilizes selective mapping of c-space and involves subdividing c-space into hypercubes until a safe path may be found by traversing edges of the hypercubes. A 2D depiction of this algorithm is given in Figure 2.5. Figure 2.5a shows a bounded 2D space, some circular obstacles, and prescribed start and goal points (S and G, respectively). The space is subdivided at the start point (Figure 2.5b), and further subdivided at the goal point (Figure 2.5c). Finally, all non-empty regions with reachable vertices are subdivided until a solution is found (Figure 2.5d). This type of approach is referred to as cell decomposition. McCarthy and Bodduluri solve
the cooperating Puma problem for several cases for which maintaining closure and avoiding collisions between the robots appear to be the main concerns. The closure constraint utilized is simplified by modeling each puma as a 3R-1S robot and then requiring a constant length between the S joints of each robot.

Chen and Duffy [91] also present a path planner for two cooperative Puma robots. Their approach is to find a feasible position for the first three links of one of the robots along a discretized path from start to goal. For each point along this discretized path the possible closure configurations (cones) are investigated to find a feasible and collision free configuration for the second robot. Because of some simplifications and assumptions it does not appear as though their approach would be successful for problems much more difficult than the relatively simple example illustrated in [91].
2.3 Other Related Areas of Research

Other related areas of path planning research which will not be discussed in depth in this thesis include:

- Mobile robot path planning
- Coordination of multiple robots
- Piano Mover's problem
- Nonholonomic motion planning

These areas of research are briefly discussed below.

2.3.1 Mobile Robot Path Planning

While all robot path planning problems have inherent similarities, mobile robot path planning differs in many ways from path planning for general manipulators. Some of the key differences as identified by McKerrow [92] are summarized in Table 2.2. These differences result in path planning for manipulators being more complex than path planning for mobile robots. The path planning problem for a 2D mobile robot in the presence of known stationary obstacles has many real-time optimal (minimum time or minimum distance) solutions. Many researchers of the mobile robot path planning problem have also considered dynamic obstacles and/or unknown environments. Such results are made possible by the limited dimensionality of the mobile robot path planning problem. Since we are concerned with path planning for manipulators, no detailed discussions will be given to path planning techniques suitable only for mobile robots. Areas where the algorithms used to solve mobile robot path planning problems may impact the general manipulator path planning problem have been included in earlier discussion.
Table 2.2: Mobile Robot vs Manipulator Path Planning

<table>
<thead>
<tr>
<th>Mobile Robot Path Planning</th>
<th>Manipulator Path Planning</th>
</tr>
</thead>
<tbody>
<tr>
<td>Movement restricted to 3D.</td>
<td>End effector may move in 6D.</td>
</tr>
<tr>
<td>Whole robot moves from start to goal.</td>
<td>End effector and payload move from start to goal.</td>
</tr>
<tr>
<td>Robot typically occupies a fixed volume.</td>
<td>Volume occupied by robot changes as joints move.</td>
</tr>
<tr>
<td>Model of environment typically incomplete.</td>
<td>Exact location and description of objects in the workspace are typically known.</td>
</tr>
<tr>
<td>Dead-reckoning control of a mobile robot is subject to significant errors which accumulate.</td>
<td>Typically assume high accuracy and repeatability of joint motions.</td>
</tr>
</tbody>
</table>

2.3.2 Coordination of Multiple Robots

Coordination of robots is typically done assuming the individual paths of the robots are known with the timing to be determined so as to avoid collisions. Research into the coordination of multiple robots will not be discussed herein since it does not appear that cooperating robot path planning research will benefit directly from it at this time.

2.3.3 Piano Mover's Problem

As mentioned earlier, the nature of the robot path planning problem is very similar to the piano mover's problem. The piano mover's problem involves planning a collision free path between two poses for a single, rigid object amongst obstacles. Because of the inherent similarities between manipulator path planning and the piano mover's problem, many algorithms such as vgraphs, voronoi diagrams, and graph search methods may be applied to either. Earlier discussions include such algorithms. There are also a number algorithms which are specific to a particular subset of mover's problems and are not applicable to the robot path planning...
A recent survey of the status of motion planning research including the mover's problem is provided by Hwang et al [93]. Hwang suggests that, as a result of problem complexity, future research should concentrate on heuristic algorithms that run in a few seconds at the expense of failing to find a solution to very hard, pathological, puzzle-like problems.

2.3.4 Nonholonomic Motion Planning

The complexity of a certain class of motion planning problems is compounded by nonholonomic constraints. Nonholonomic constraints are constraints on the derivatives of configuration variables which cannot be integrated. For example, a unicycle may maneuver to achieve any position and orientation, but its direction of motion at any one instant is constrained. Path planning for single and cooperating robots is holonomic. The nonholonomic problem is much more difficult and efforts for developing implementable algorithms are just beginning. A review of the current status of motion planning with nonholonomic constraints may be found in [93].

2.4 Summary of the Literature Review

This section presents a summary of the above literature review. The summary is presented in four sections:

- Difficulties with Complete Solutions
- Practical Incomplete Solutions
- Potential Fields Solutions
- Cooperating Robots
2.4.1 Difficulties With Complete Solutions

Many complete algorithms have been developed for solving the motion planning problem. However, it appears as though the mathematical complexity of such techniques renders them computationally intractable when applied to a reasonably difficult robot motion planning with six or more dof. A general, practical, and complete solution to the motion planning problem has not yet been developed.

There are a number of complete approaches which attempt to achieve solution time commensurate with problem difficulty. The computational practicality of these techniques for reasonably difficult yet practical path planning problems remains to be demonstrated.

2.4.2 Practical Incomplete Solutions

As a result of problem complexity, practical techniques used to solve the single robot motion planning problem for six or more dof involve some heuristics or simplifying assumptions and lack completeness. Some typical simplifications include:

- Simplified models of the robots and obstacles
- Decoupling of rotations from translations
- Compact wrists and payloads
- Restrictions on allowable motions and allowable obstacles

These simplifications and heuristics are typically robot and/or task specific and would not be expected to perform well in more general cases or for two robots working cooperatively due to the differences presented earlier.

The speed and success of the most useful algorithms can be attributed to their pruning of the search space by reducing problem dimensionality or by their ability to selectively map c-space thereby avoiding intractable exhaustive mappings.
2.4.3 Potential Fields Solutions

The potential fields approach to single arm path planning constitutes an effective way to combine the constraints resulting from several obstacles for many simple cases, but the fact that motion planning using potential fields is based solely on local information has led to some difficulty in achieving effective high level planning. The most effective potentials fields approaches determine a sequence of intermediate via points between which there are no local minima.

2.4.4 Cooperating Robots

Of the work which has been published for path planning of cooperating robots, much of it is limited in effectiveness to planar systems. The researchers who have addressed cooperating robots with six or more degrees of freedom have apparently been successful only in solving problems which appear to be relatively simple.

Research pertaining to path planning for cooperating robots utilizing potential fields appears to be still in its early stages. Results so far have been limited to redundant planar systems with only a few obstacles.
CHAPTER 3
Statement of the Problem

This chapter presents a formal definition of the robot path planning problems being addressed by this thesis. Some general background information is given in Section 3.1. Sections 3.2 and 3.3 discuss assumptions and goals, respectively. Formal definitions of the single and cooperating robot path planning problems are given in Sections 3.4 and 3.5, respectively.

3.1 Background

A robot can be described by its forward kinematic equation

$$T_0^m = f(\Theta)$$

(3.1)

where $T_0^m \in \mathcal{R}^m$ represents the task space transformation (position and/or orientation) of the end effector and $\Theta = (\theta_1, \ldots, \theta_n) \in \mathcal{R}^n$ represents the robot’s joint configuration, where $n$ is the number of degrees of freedom (dof). For spatial robots with three translational and three rotational dof, $m = 6$.

A robot’s inverse kinematic equation

$$\Theta = f(T_0^m)$$

(3.2)

identifies joint configurations $\Theta$ which would result in a specified task space transformation $T_0^m$. For a non-redundant robot capable of achieving any desired position with any desired orientation (within workspace limits), $n = m$, and Equation 3.2 will possess only a finite number of solutions $\Theta$ for a given $T_0^m$. For redundant robots $n > m$ and equation 3.2 is underdetermined, indicating that an infinite number of robot configurations $\Theta$ exist which produce the end effector transformation $T_0^m$. The problem of solving Equation 3.2 for a redundant robot is referred to as the
redundancy resolution problem. A robot with \( n < m \) has fewer dof than required to arbitrarily position and orient its end effector in the workspace. The inverse kinematic equation for such a robot is overdetermined, i.e., it will have solutions only for transformations which lie in the limited workspace of the robot.

3.2 Assumptions

This section restates the assumptions presented in Subsection 1.2.1 and provides a discussion regarding each assumption.

Assumption 1 Forward kinematic models of the robots are available.

Discussion: A robot may be represented using the Denavit-Hartenberg convention from which the forward kinematic model (Equation 3.1) can be easily derived [94].

Assumption 2 Closed-form inverse kinematic models of the robots are available for six dof robots or for the final six links of redundant robots.

Discussion: This thesis addressed full spatial robots for which \( n \geq m = 6 \) (see Section 3.1). Most commercial six dof robots satisfy one of the following sufficient conditions which enables a closed-form inverse kinematic solution [94]:

1. Three adjacent joint axis intersect.

2. Three adjacent joint axis are parallel to one another.

Unimation Puma manipulators, which will be used in the case studies for this thesis, satisfy the first condition. In general, multiple solutions will exist representing various possible robot configurations. For redundant robots, it is assumed that the final six links can be treated as a single six dof robot for which a closed-form inverse kinematic model is available. The usefulness of this assumption regarding redundant manipulators will become evident later in this thesis.
The path planning strategy in this thesis does not require inverse kinematics for single robot path planning problems.

Assumption 3 *Geometric models of the robots, payload, and obstacles are available.*

Discussion: Robots and their environment may be represented by some form of geometric model. Some typical forms of geometric modeling include boundary representations (b-reps), constructive solid geometry (csg), and polytope representations. The geometric model will contain knowledge of the geometry, position, and orientation of the robot links, the payload, and each obstacle in the workcell. The only constraint regarding geometric modeling is that a facility for performing collision detection is required. Neither the source of this geometric information nor the data structure format of the geometric model is important from the perspective of the path planner. For static obstacle path planning purposes, the geometric model need only consist of a geometric description of the robots, payload, and objects in the environment.

Assumption 4 *Obstacles in the workspace are static.*

Discussion: The added complexity of a dynamic environment make it unlikely that a practical planner for cooperating multi-dof robots with dynamic obstacles will be developed anytime soon.

Assumption 5 *Feasible and collision free start and goal joint configurations of the robots are known, as are the start and goal positions of the payload.*

Discussion: There are several key consequences of this assumption. First, note that the grasp positions are inherently defined by this assumption. The determination of suitable grasp positions is highly task specific, potentially very difficult,
and beyond the scope of this thesis. Secondly, note that specifying the start and goal joint configurations as opposed to the start and goal task space configurations eliminates the need for the path planner to choose particular solutions to the inverse kinematics at the start and goal positions. It is reasonable to assume that the start joint configurations are known since some single arm planning must have been done to position the robots at their initial positions. Requiring that the goal joint configurations be known is more demanding than simply specifying a task space goal for the payload. Typically even non-redundant robots would have several possible configurations (such as elbow up or elbow down) which satisfy a particular task space goal. The solvability of the path planning problem can depend upon which joint configuration is specified as the goal. An example where the choice of goal joint configurations determines the solvability of a path planning problem is illustrated in Figure 3.1. Figure 3.1a shows the start position for two cooperating 3R planar robots. Figure 3.1b shows a choice of goal joint configurations which result in a solvable problem for the case illustrated. As shown in Figure 3.1c, a different choice of goal joint configurations which produce the same task space goal can result in an

![Figure 3.1: Choice of Goal Joint Angles May Affect Solvability](image)
unsolvable problem. In the case of redundant robots some form of redundancy resolution is required to specify the goal joint angles. Redundant robots will typically possess one or several regions in c-space which yield a desired task space goal.

It is a clear disadvantage to require the goal joint configurations be specified at the outset of the problem since this information must come from some higher level source and may directly determine the existence of a solution. However, a few incidental advantages arise from the extra knowledge required by Assumption 5:

- **Path cyclicity concerns are eliminated.** A path planner will often be required to execute a task which is repetitive in task space. Path planners which do not specify the start and goal joint angles for a particular path planning problem often suffer from path cyclicity problems whereby the robot does not achieve the same configuration on subsequent repetitions of identical task space tasks.

- **Path planning problems may be attacked either from start to goal or vice versa.** The ability to attempt to solve a path planning problem from either direction (or even from both directions simultaneously) may prove to be beneficial if the algorithm or heuristic being used happens to be more successful in one direction than in the other for a particular path planning problem. For example, planning a path to remove a peg from a hole would intuitively seem much simpler than planning a path to put the peg in the hole. The 2-D problem illustrated earlier in Figure 2.2 is one which would have proven easier to solve backwards if using an A* graph search approach. As discussed earlier in Section 2.1.1, the ability to search bidirectionally is often valuable.

- **A preferred goal robot configuration may be achieved.** In some cases it may be desirable to supply the path planner with a specified goal robot configuration rather than allowing the path planner to choose any which satisfy the goal position/orientation in task space. For example, a reliability analysis or
robot flexibility analysis might be used to prescribe a preferred goal robot configuration.

Our need for Assumption 5 stems from the fact the our approach is configuration space based. This will become clear as our solution technique is presented later in this thesis.

Assumption 6 *Motion between the specified start and goal positions may be arbitrary.*

**Discussion:** This assumption illustrates that interest is solely to move from start to goal without restriction on the path. This is the most general form of the path planning problem and is acceptable for solving the vast majority of problems. As an example of a task for which this assumption would not be valid, consider two robots cooperatively manipulating a trough of water. Clearly such a task would impose a constraint on the motion between the start and goal positions such that the trough would remain level so as not to spill the water. Another example requiring restricted motion involves contact between the robot/payload and its environment. Although such cases are not considered herein, some discussion of how they might be addressed is presented later in Section 5.4.

In cases where a specific task space path must be followed the problem becomes one of configuration selection or redundancy resolution rather than a classical path planning problem. For example, a nine dof robot performing arc welding along a specified task space path is not a nine dimensional path planning problem but rather a much simpler three dimensional redundancy resolution problem.

Assumption 7 *The planner may ignore robot dynamics.*

**Discussion:** This assumption is valid when considering only static obstacles and since a time optimal trajectory is not sought. Algorithms which consider
dynamics typically assume that an initial path is given and dynamic optimization is done locally along the path [95]. Under dynamic optimization, path curvature becomes an important characteristic.

3.3 Goals

This subsection restates and discusses the goals presented in Subsection 1.2.2.

Goal 1 The planner shall locate reasonable collision-free paths in a time frame suitable for off-line path planning.

Discussion: It appears as though the search for an optimal path and/or a real time solution for non-trivial path planning problems with more than a few dof will remain computationally intractable for some time to come (See Chapter 2).

Goal 2 The planner shall be capable of modifying a feasible path into a more efficient one.

Discussion: It is typically possible to modify a suboptimal path found by a path planner to produce a smoother, more efficient path.

Goal 3 The planner shall be applicable to various robotic systems and various tasks.

Discussion: Some path planning techniques perform well only with specific types of robots or for certain types of tasks due to their use of simplified, case specific assumptions or heuristics. We would like our solution technique to remain free of any assumptions which would limit its use as a general-purpose path planner.
Goal 4 *The planner shall be practical for cooperating six dof manipulators as a minimum, and ideally for cooperating redundant robots.*

**Discussion:** It should be noted that the practicality of a path planning technique for a robot with six or more dof is important since at least six dof are required to arbitrarily position and orient an end effector. Many of the path planning techniques discussed in Chapter 2 are not practical for robots with six or more dof.

Goal 5 *The planner output shall be a sequential listing of closely spaced knot points in joint space which represent the discretization of a continuous, feasible, and obstacle avoiding path connecting the start and goal configurations.*

**Discussion:** This goal is consistent with integrating a path planner into the CIRSSE testbed system using a traditional three-step decomposition of the *move robot* problem. The three steps are path planning, trajectory generation, and motion control. A *trajectory generator* may be used on the output of the path planner to provide timing information consistent with the dynamic constraints of the system. The knot points determined by the path planner shall be spaced closely enough that the trajectory generator need not be concerned with maintaining the closure requirement between knot points. Execution of the time parameterized trajectory may be carried out by a motion control system. Some fine compliance will typically be required due to inaccuracies in the robot model or tracking errors at the control level. Such compliance could be either passive, such as a compliant end effector, or active, such as compliance based on force/torque feedback. Details of the trajectory generation and motion control steps are separate areas of research which are beyond the scope of this thesis.
3.4 Single Robot Path Planning Problem Statement

Per the background and assumptions stated above, the single robot path planning problem may be formally defined as follows:

**Given:**

1. A single robot described by its forward kinematic equation, Equation 3.1.
2. Geometric models of the robot, the payload, and workspace obstacles.
3. Start and goal joint configurations of $\Theta_s$ and $\Theta_g$, respectively.

**Determine:**

A closely spaced sequence of $k$ joint space knot points $(\Theta_1, \ldots, \Theta_k)$, where $\Theta_1 = \Theta_s$ and $\Theta_k = \Theta_g$, which represent a discretization of a feasible and collision free c-space path connecting $\Theta_s$ and $\Theta_g$.

3.5 Cooperating Robot Path Planning Problem Statement

Per the background and assumptions stated above, the cooperating robot path planning problem for two cooperating spatial robots, referred to as robots 1 and 2, may be formally defined as follows:

**Given:**

1. Two robots work cooperatively satisfying the closure constraint:

   $$ T_{10}^6 T_{r1}^{r2} = T_{20}^6 $$

   (3.3)

   where $T_{r1}^{r2}$ is an invariant transformation relating the relative positions of the robot end effectors as they grasp a common, rigid object.

2. The robots are described by forward kinematic equations:

   $$ T_{i0}^6 = f(\Theta_i), \ i=1,2 $$

   (3.4)
where \( \Theta_i = (\theta_{i1}, \ldots, \theta_{ini}) \) represents robot \( i \)'s joint configuration, \( n_i \geq 6 \) is the number of degrees of freedom (dof) of robot \( i \).

3. The robots are described by inverse kinematic equations with at most one solution:

\[
\Theta_i = f(T_i^{6_0}, \Theta_i', C_{ji_i}), \quad i=1,2
\]  

(3.5)

where \( \Theta_i' = (\theta_{i1}, \ldots, \theta_{ini-6}) \), and \( C_{ji_i} \) represents one of \( j_i \) possible robot configurations for robot \( i \), and \( j_i \) is finite and known.

4. Geometric models of the robots, the payload, and workspace obstacles.

5. Start and goal joint configurations of \( \Theta_is \) and \( \Theta_ig \), respectively, where \( i = 1,2 \).

Determine:

A closely spaced sequence of \( k \) paired joint space knot points \(((\Theta_{11}, \Theta_{21}), \ldots, (\Theta_{1k}, \Theta_{2k}))\), where \( \Theta_{11} = \Theta_is \) and \( \Theta_{1k} = \Theta_ig \), which represent a discretization of a feasible, continuous, and collision free path connecting \((\Theta_{1s}, \Theta_{2s})\) and \((\Theta_{1g}, \Theta_{2g})\). Each paired knot point \((\Theta_{1j}, \Theta_{2j})\) shall satisfy the closure constraint, Equation 3.3. Also, the discretization shall be sufficiently fine so that a trajectory planner may ignore the nonlinearities of the closure constraint between knot points.
CHAPTER 4
Divide-and-Conquer C-Space Traversal Heuristic

This chapter presents the configuration space traversal heuristic which is the heart of the path planning strategy presented in this thesis. This chapter merely presents the heuristic. The utilization of the heuristic is discussed in subsequent chapters. This chapter is organized into eight main sections:

- Motivation for a New Approach
- Conceptual Description of Heuristic
- Vector Description of Heuristic
- Computing Search Directions
- Prioritizing Search Directions
- Comparison of the Heuristic to the Literature

Section 4.1 discusses the motivation for a new path planning technique for cooperating robots. Sections 4.2 and 4.3 present conceptual and vector descriptions of the c-space traversal heuristic, respectively. Computation and prioritization of search directions used by the heuristic are discussed in Sections 4.4 and 4.5, respectively. Finally, a comparison of the heuristic to published path planning algorithms and heuristics is presented in Section 4.6.

4.1 Motivation for a New Approach

This section attempts to make a case that there is sufficient motivation for this new research in the area of path planning for cooperating robots. First, recall from Section 2.2 that path planning approaches in the literature for cooperating robots
are generally limited with regard either to the number of degrees of freedom (dof) of the robots or to the apparent difficulty of problems which they are capable of solving. Thus, there appears to be sufficient motivation for this research.

Due to the fact that researchers' interest in cooperating robotic systems is relatively young compared to the much longer history of interest in single robots, thorough consideration should be given to the application of methods developed for single robot path planning when searching for a solution to the cooperating robot path planning problem. There are, however, some unique elements to the general cooperating robot path planning problem that make it unlikely that any of the single arm path planning methodologies discussed in Chapter 2 could be successfully applied to cooperating robots without significant modifications. These differences were presented earlier in Table 2.1. Some of these special elements of the cooperating arm problem and the way in which they impact the solution process are discussed in this section.

Consider, for instance, two cooperating six degree of freedom manipulators. The effective number of degrees of freedom for the closed kinematic chain is six (from Equation 1.1). Hence, the problem is essentially six dimensional (almost as if it were a single arm problem) but possesses the added closure constraint. This restriction does not affect the dimensionality of the space in which a graph search algorithm must perform, but does affect the validity of some of the assumptions typically used to reduce the system to one of a lower dimensionality. For example, a common assumption for single arm planning is to neglect orientation for large, gross moves through space. This assumption would not likely prove effective for two cooperating robots since the orientation of the load will usually be crucial to the maintenance of configurations reachable by both robots.

The added difficulty induced by the closure constraint would also make it extremely difficult to implement a planner based on task space heuristics. One
of the difficulties with task space based heuristics for single robot path planning problems is that they often produce collisions with one obstacle while trying to avoid another. Such difficulties could only be more severe for a closed kinematic chain such as results during robotic cooperation. An additional difficulty which would be magnified by the reduction in free space during cooperation is the fact that the avoidance strategy suggested by a task space heuristic may not always be feasible to achieve.

Although the potential fields method should, in theory, be applicable to the cooperating robot motion planning problem, much difficulty in achieving a reliable implementation would be anticipated. Much thought would be required to attempt to develop potential field functions that would be well behaved for the closed kinematic chain which results during cooperation. Also, the practice of selecting a grid of trial points and perturbing them or rerouting the path through a different set of via points would be significantly more difficult for cooperating robots than for a single robot. The basis for the preceding statement is that a far more restricted safe space results for cooperating arms. As a result, the practice of determining safe trial points more closely spaced than the overall global problem would be more difficult. Also, there would be increased likelihood that some intermediate trial points would lie in unreachable regions of safe space. Results in the literature seem to support the premise that achieving a practical and reliable potential fields based planner for cooperating robots would be difficult (see Section 2.2).

The human assisted approaches still maintain their advantage of capitalizing on the natural ability of humans to solve complicated geometric problems. In fact it is the human assisted approach by which most non-trivial collision free robot motion planning is currently accomplished. However, the level of insight which the user would be required to supply would clearly be much greater for two cooperating
arms than for a single arm. This increase in difficulty may make an already potentially undesirable task for a human prohibitively tedious, frustrating, and difficult. In addition, while the human assisted approach offers the best chance for nearly immediate results, it is contrary to our longer term goals of creating more autonomous robotic systems capable of complete task planning and execution from a task level command.

The path planning procedure being presented herein is of the graph search type and, in a fashion similar to Dupont’s approach to path planning for a single redundant manipulator (see Section 2.1.1), the procedure involves selective mapping of c-space on an as needed basis to reduce computational burden. Because of the added difficulty of the cooperating arm problem, an improved heuristic was sought to guide the mapping of c-space in a manner directed towards finding a solution with a minimal amount of mapping. This resulted in the development of the “divide-and-conquer” c-space traversal heuristic presented below.

4.2 Conceptual Description of Heuristic

In this section, a novel “divide-and-conquer” style heuristic is presented for traversing an n-dimensional space consisting of safe and unsafe regions. For purposes of robot path planning, the space to be traversed is c-space. The heuristic is general in nature and, while our intended application is to solve the robot path planning problem, this technique could be used to attempt to traverse any space consisting of regions of safe and of unsafe points. An example of another possible application is the “piano movers’ problem.” Because of the impracticality of mapping the space exhaustively for dimensionality greater than perhaps three, the heuristic was formulated to be compatible with selective mapping of c-space with no computationally expensive precomputations. The c-space traversal heuristic is the
"backbone" of the path planning technique being presented in this thesis. Discussion of the application of the c-space traversal heuristic to the robot path planning problem is deferred until the next Chapter.

This section describes the heuristic conceptually using several simple 2D and one 3D illustrative examples. A vector description of the heuristic is given in Section 4.3. Although the pictorial examples herein are mainly 2D for simplicity of illustration, the approach suffers no loss of generality regardless of problem dimensionality (although the complexity of the searches increases with problem dimensionality). The vector description presented later is applicable to a space of arbitrary dimension.

To illustrate the heuristic, consider the 2D path planning problem illustrated in Figure 4.1a, where \( \Theta_s \) and \( \Theta_g \) are the start and goal positions, respectively. The following note is important:

In this example and subsequent examples herein the boundary of the unsafe c-space is defined in the figure as though the c-space obstacle has been mapped out. This is not the case, but the entire unsafe region is shown a priori to provide better understanding of the subsequent steps.

First, the \( n \)-dimensional direction vector from the start point to the goal point is calculated and an attempt is made to traverse along that vector until the first unsafe point is found. This involves discretizing the path from the start to the goal and mapping each successive step along that path until the first unsafe point is found. In the example, the progression from \( \Theta_s \) is safe through point \( \Theta_a \) (Figure 4.1b). Points safely mapped are indicated by the solid circles in the Figure.

Next, the progression along the straight line path from start to goal is continued through the unsafe region until the first safe point is found. In the example, this first safe point is labeled \( \Theta_b \) in Figure 4.1b. Unsafe points mapped in this process are indicated by the open circles. Although in this example \( \Theta_b \) lies in the
same connected region of safe space as the start and the goal points, this will not be true in general. Next, the intent is to find a safe point in the $n-1$ dimensional space orthogonal to and bisecting the vector between the last safe point ($\Theta_a$ in the example) and the first safe point on the other side of the homogeneously unsafe region ($\Theta_b$ in the example). It is apparent that such a safe point must exist if the problem at hand is solvable. In this example, this reduces to searching the 1D line shown in Figure 4.1c. The search methodology depends upon whether this is an initial search or a subsequent search:

- For an *initial* search, the search space is effectively searched for the safe point nearest to the midpoint of the unsafe line segment which was mapped previously. This is done by radiating out equal amounts in all search directions until a safe point is found.
• For a subsequent search, the search directions are prioritized and searched non-uniformly per the methodology discussed in Section 4.3. In 2D, a prioritized search would first search in the search direction which has a component in the direction of the previously successful search direction. If no safe point can be found in that direction, the opposite direction is searched.

Since this is the initial search in the example, the line is searched discretely and in both directions equally from the midpoint until safe point $\Theta_c$ is found (see Figure 4.1d). Next, an attempt is made to traverse to the safe point from the last safe point initially found in trying to go directly from the start to the goal (that point being $\Theta_d$ in the example). The following steps depend upon the result of that attempted traversal, as detailed by the following two cases:

Case 1: The Traversal to the New Safe Point is Entirely Safe

In this case it is attempted to traverse to any previously determined guide points, where guide points are previously determined safe points such as those found at the other side of the homogeneously unsafe region or intermediate goal points found in any prior searches. The sequence for considering the guide points is the opposite of the order in which they were found with the global goal point to be considered as a final guide point. When progression to a particular guide point is not entirely safe, that guide point is permanently dismissed and progression is attempted toward the next guide point in the specified sequence. It is in this manner that productive use may be made of safe points which could be in unreachable regions of safe space. As a result, intermediate guide points may or may not be part of the final path. The attempted progressions continue until an attempt has been made to progress to the global goal point. If progression can be made to the global goal point the entire path planning problem has been solved. Otherwise, the last safe point progressed to becomes the new start point and the entire heuristic is repeated until the global goal point has been safely progressed to.
Note that only points which have been safely progressed to from the start point are mandatorily included as part of the final path but those which may be in unreachable regions are used to help guide the overall process. All points actually comprising part of the path will, of course, be in the same connected region of safe space as the start point.

The 2D example of Figure 4.1 invoked this case since the attempt to traverse from $\Theta_a$ to $\Theta_c$ can be seen to be successful (Figure 4.1e), after which progression is made to guide points $\Theta_b$ and $\Theta_g$ thereby completing this simple 2D path planning problem with the resulting path shown in Figure 4.1e. The c-space points which required mapping during the process are shown in Figure 4.1f. Note how relatively few points were mapped by this technique.

Case 2: The Traversal to the New Safe Point is Not Entirely Safe

In this case the heuristic is recursively applied taking the last point safely progressed to as the start point and the safe point found in the last search as the goal point.

4.2.1 More 2D Examples

Another 2D illustration of the heuristic is given in Figure 4.2. The solution sequence in this example is similar to that in the previous example except in this case, following the safe traversal to the safe point $\Theta_c$, no progression can be made toward $\Theta_b$. Thus $\Theta_b$ is disregarded, progression is attempted toward the second guide point $\Theta_g$ resulting in the solution shown in Figure 4.2e. Note that the disregarded point did not necessarily have to lie in the same region of safe space as the start and goal positions (although it did in this example).

An example of a 2D task which would result in a c-space having an unreachable safe region is shown in Figure 4.3. A 2D illustration of the c-space traversal heuristic for a problem with two disjoint regions of safe space is illustrated in Figure 4.4. This
Figure 4.2: Example Which Dismisses an Intermediate Point

illustration also demonstrates the inherent reversal nature of the heuristic when a joint limit problem is encountered (the second search hits a joint limit in the preferred direction after which reversal occurs). This example also illustrates the heuristic for a problem requiring multiple searches.

4.2.2 A 3D example

An example of the c-space traversal heuristic applied to a 3D problem is illustrated in Figure 4.5. In the 3D case, the search space is 2D (planar). For this example eight evenly distributed search directions were considered with the search directions prioritized into two groups (prioritization is discussed below).

4.2.3 Philosophy Behind the Heuristic

The basic idea behind the "divide-and-conquer" c-space traversal heuristic is that better local decisions at the beginning of the trouble region may be made if a
possible way around the "center" of the trouble region is known. Thus, rather than attempting paths which look promising locally (at the beginning of a trouble region) but which may not yield overall results, the heuristic attempts local strategies that appear to have a possible overall solution around the trouble region. A comparison of how this heuristic relates to the literature is given later in Section 4.6.
Figure 4.4: Example with Non-Disjoint Safe Space and Multiple Searches

Figure 4.5: 3D Example of C-Space Traversal Heuristic
4.3 Vector Description of Heuristic

Given $\Theta_s$ and $\Theta_g$, the start and goal positions in $n$-dimensional space, respectively, the heuristic may be described in vector notation by the following ten step procedure:

**Step 1**

Compute the direction vector from start to goal and normalize:

$$D = \frac{\Theta_g - \Theta_s}{||\Theta_g - \Theta_s||}$$

**Step 2**

Compute the number of discrete steps along $D$ from start to goal:

$$n = c ||\Theta_g - \Theta_s||$$

where $c$ = constant which determines discretization size

**Step 3**

Discretize from $\Theta_s$ to $\Theta_g$ in the direction of $D$ until the first unsafe point is found. Call the last safe point $\Theta_a$:

$$\Theta_a = \Theta_s + j \frac{D}{c}$$

where $j$ = last integer in $1, 2, ..., n$ before an unsafe point is found

**Step 4**

Continue the discretization through the unsafe region until the next safe point is found. Call that point $\Theta_b$:

$$\Theta_b = \Theta_s + k \frac{D}{c}$$

where $k$ = first integer in $j+2, j+3, ..., n$ which yields a safe point
Step 5

Establish a set of $n_{SD}$ normalized search directions, $\Theta_{SD_i}$, orthogonal to $D$:

$$\Theta_{SD_i} \cdot D = 0$$

where $i=1,2,...,n_{SD}$ and $\cdot$ represents the dot product operator.

Calculation of search directions is discussed in Section 4.4.

Step 6

If this is a subsequent search, prioritize the search directions by grouping them according to their dot product with the last successful search direction. A technique for so prioritizing the search directions is described in Section 4.5. The number of groups used will affect the emphasis given to continuing searches in the previously successful direction. The purpose of the prioritization is to favor search directions based on their component in the direction of the last successful search direction.

Step 7

Search from the midpoint of the unsafe region, $(\Theta_a + \Theta_b)/2$, in the (possibly prioritized) search directions until a safe point, designated as $\Theta_C$, is found. The search technique shall depend upon whether this is the initial search or a subsequent search.

If this is the initial search, search the entire set of search directions for the safe point nearest to the center of the trouble region by radiating out equal discrete steps in each search direction until a safe point is found or until all directions exceed a joint limit and no safe point has been found.

If this is a subsequent search, search the highest priority group by radiating out equal discrete steps in each search direction in that group until a safe point is found or until it is determined that no safe point can be found in any of those directions (such as a joint limit has been reached in each direction). If no safe point
is found in the highest priority group then repeat for the next highest priority group.
Repeat until a safe point is found or until all groupings of search directions have
been exhausted and no safe point has been found.

If no safe point could be found, reinitialize the global problem as from the last
point safely progressed to the global goal point and restart the entire procedure.

Step 8

Discretize along $\Theta_a$ to $\Theta_c$ and traverse as far along this segment as is safe. If this
entire segment is safely traversed goto Step 9. Otherwise goto Step 10.

Step 9

Progress toward all previous guide points in the opposite order in which they were
found, where guide points include not only previous intermediate goal points but
also the safe points found on the goal end of each unsafe region which invoked a
search. The global goal point is added as a final guide point. When progression
to a particular guide point is not entirely safe, that point is permanently dismissed
and progression is attempted toward the next guide point in the specified sequence.
The progression continues until an attempt has been made to progress to the global
goal point. If progression to the global goal point is safe, the global path planning
problem has been solved. Otherwise, redefine $\Theta_s$ as the last safe point in that
progression, $\Theta_g$ as the global goal point, and go to Step 1.

Step 10

Set $\Theta_s$ equal to the last safe point, and $\Theta_g$ equal to $\Theta_c$, and go to Step 1.

4.3.1 Failure Condition

The heuristic fails when a call is made to Step 1 above with identical values
of $\Theta_s$ and $\Theta_g$ as a previous call. This can occur by one of the following two failure
modes:
1. Cycling occurs

2. The first search following reinitialization fails to locate a safe point.

A 2D example which results in the first failure mode is shown in Figure 4.6. In spite of the possibility that the heuristic will fail, the results presented later in this thesis seem to indicate that the heuristic provides the capability to solve realistic and potentially difficult path planning problems. The example shown in Figure 4.6 does involve a concave obstacle. The heuristic does appear to perform better with convex obstacles however the complexity and nonlinearity of the task space to c-space mapping makes it unlikely that even simple problems will result in a c-space with strictly convex obstacles. In addition, the ability to attack the problem from either direction (see discussion following Assumption 5 in Section 3.2) would mean that a problem would have to induce cycling if approached from either direction in order to result in inability to find a solution. As the dimensionality of the space increases, the likelihood of actual, practical robot path planning problems possessing
deep concave cavities of safe c-space in both directions (start toward goal and vice versa) would intuitively seem to decrease. Such a c-space shape would probably not occur for practical problems.

The cyclic failure mode is not sufficient to rule out the existence of a solution since this mode can occur for a problem in which the search directions on the first search following reinitialization happens to miss all available safe space in the search hyperplane.

4.4 Computing Search Directions

This section discusses methods for computing search directions as required for Section 4.3 Step 5.

Recall from above that the c-space traversal heuristic involves searching the space orthogonal to and bisecting the unsafe region encountered in an attempted traversal. For an n-dimensional space \( \Theta = (\theta_0, \ldots, \theta_n) \), the n-1 dimensional hyperplane to be searched shall be orthogonal to direction vector \( \mathbf{D} = (d_0, \ldots, d_n) \) and shall include point \( \Theta_c = (\theta_{c0}, \ldots, \theta_{cn}) \), where \( \Theta_c \) is the center point of the unsafe segment. Thus, points to be considered in the search shall satisfy:

\[
d_0(\theta_0 - \theta_{c0}) + d_1(\theta_1 - \theta_{c1}) + \ldots + d_n(\theta_n - \theta_{cn}) = \sum_{i=1}^{n} d_i(\theta_i - \theta_{ci}) = 0 \quad (4.1)
\]

From Equation 4.1, it can be seen that the search directions \( \mathbf{S} = (\theta - \theta_c) \) must be orthogonal to \( \mathbf{D} \):

\[
d_0s_0 + d_1s_1 + \ldots + d_ns_n = \sum_{i=1}^{n} d_is_i = \mathbf{S} \cdot \mathbf{D} = 0 \quad (4.2)
\]

Four procedures for determining search directions which satisfy Equation 4.2 were considered:

1. Searching a uniform grid
2. Radiating out along orthogonal basis vectors and their negatives.
3. Radiating out along a set of vectors made up of combinations of the \( n-1 \) free variables in Equation 4.2.

4. Radiating out along uniformly distributed vectors made up of combinations of orthogonal basis vectors.

These four procedures are discussed below. Selecting amongst the procedures for implementation is then addressed in Section 4.4.1.

**Procedure 1 Searching a uniform grid.**

Searching a uniform grid would involve discretizing uniformly in the \( n - 1 \) dimensional search space defined by Equation 4.2. Such an approach would clearly produce a very effective search from the standpoint that it would ensure finding a safe point if one exists (within discretization limitations). However, this approach can be quickly dismissed due to its computational complexity. For example, an \( n \) dof problem discretized 100 points per axis (approximately every three degrees for a typical revolute joint) would produce a grid containing \( 100^{(n-1)} \) points. For a nine dof problem, this would result in \( 10^{16} \) points. Even if one million points could be mapped every second (far from achievable today) it would take more than 300 years to exhaustively perform one search of such a uniform grid!

**Procedure 2 Radiating out along orthogonal basis vectors and their negatives.**

A set of \( n-1 \) \( n \)-dimensional linearly independent and orthogonal unit vectors satisfying Equation 4.2 can be computed. Such a set of vectors would constitute a basis for the search space, i.e., each possible search direction could be represented as a linear combination of the basis vectors. A set of orthogonal basis vectors will be uniformly distributed in the space. Referring to the \( i^{th} \) basis vector as \( \mathbf{B}_i = (b_{i1}, \ldots, b_{in}) \),
the basis vectors must satisfy:

\[ \mathbf{D} \cdot \mathbf{B}_i = \sum_{k=1}^{n} d_k b_{ik} = 0 \quad i = 1, \ldots, n - 1 \quad (4.3) \]

\[ \mathbf{B}_i \cdot \mathbf{B}_j = \sum_{k=1}^{n} b_{ik} b_{jk} = 0 \quad i, j = 1, \ldots, n - 1 \text{ and } i \neq j \quad (4.4) \]

\[ \| \mathbf{B}_i \| = 1 \quad i = 1, \ldots, n - 1 \quad (4.5) \]

where \( \mathbf{D} \) is the normal vector to the search space as per Equation 4.2, Equation 4.3 ensures that the basis vectors lie in the search hyperplane, and Equations 4.4 and 4.5 require all the basis vectors to be mutually orthogonal unit vectors.

There are, of course, an infinite number of orthogonal bases. Calculation of search directions requires only one. The following set of vectors could be calculated in the sequence shown and then normalized to yield one such orthogonal basis:

\[
\begin{align*}
\mathbf{B}_1 &= (1, h_1, 0, \ldots, 0) \\
\mathbf{B}_2 &= (b_{11}, p_2, h_2, 0, \ldots, 0) \\
\mathbf{B}_3 &= (b_{21}, b_{22}, p_3, h_3, 0, \ldots, 0) \\
&\vdots \quad \vdots \quad \vdots \\
\mathbf{B}_{n-1} &= (b_{n-1}, b_{n-2}, \ldots, b_{n-2}, p_{n-1}, h_{n-1})
\end{align*}
\]

where the \( p_i \) are chosen so that the \( \mathbf{B}_i \) and \( \mathbf{B}_{i-1} \) satisfy Equation 4.4 and then the \( h_i \) are chosen so that the \( \mathbf{B}_i \) satisfy Equation 4.3.

Radiating out along the orthogonal basis vectors and their negatives would amount to considering search directions of the form \( \pm \mathbf{B}_i \). This approach would yield \( 2(n-1) \) search directions for an \( n \) dof problem (16 for a nine dof problem). Thus, the number of search directions using this procedure would increase linearly with the number of dof, i.e., the complexity of searching with search directions based on this procedure would be \( O(n) \). While this is an attractive feature it could be expected to perform poorly for cooperating robot path planning problems since such a reduced set of search vectors might miss the relatively little safe space available.
This expectation was verified when search directions based on Procedure 2 were found to be ineffective even for very simple robot path planning problems. The reason for discussion of this procedure is to illustrate that attempts were made to utilize as small a set of search directions as possible.

**Procedure 3** Radiating out along a set of vectors made up of combinations of the n-1 free variables in Equation 4.2.

The third approach attempts to bridge the gap between the intractability of Procedure 1 and the oversimplification of Procedure 2. This procedure involves allowing the n-1 independent variables to take on all combinations of $\pm sd_i$ and solving for the dependent variable using Equation 4.2, where the $sd_i$ may be chosen for each joint $i$ as desired to vary the amount of motion being prescribed for joint $i$.

This approach will yield $2^{n-1}$ search directions for an $n$ dof problem. While this procedure results in tractable numbers of search directions (256 for a nine dof problem), better performance may be possible using still more search directions.

A more extensive set of search directions could be computed by allowing the $n - 1$ independent variables to take on all combinations of $\pm sd_i$ and 0 (except all zeros) and solving for the dependent variable using Equation 4.2, where the $sd_i$ may again be chosen for each joint $i$. This will result in $3^{(n-1)} - 1$ search directions for an $n$ dof problem (6560 for a 9 dof problem).
This procedure for computing search directions is equivalent to considering all combinations of $\pm sd_i$ (and 0 for the more extensive set) times the following $n - 1$ vectors:

\[
\begin{align*}
V_1 &= (sd_1, 0, \ldots, 0, \frac{d_1 \cdot sd_1}{d_n}) \\
V_2 &= (0, sd_2, 0, \ldots, 0, \frac{d_2 \cdot sd_2}{d_n}) \\
& \vdots \\
V_{n-1} &= (0, \ldots, 0, sd_{n-1}, \frac{d_{n-1} \cdot sd_{n-1}}{d_n})
\end{align*}
\]

(4.7)

The potential disadvantage of this procedure is that the search directions will not, in general, be uniformly distributed in the search space. The degree to which coverage of the search space is non-uniform will depend upon the coefficients in Equation 4.2. Uniform distribution will occur only in the special case where $d_n \gg d_i$, for all $i \neq n$.

Procedure 4 Radiating out along uniformly distributed vectors made up of combinations of orthogonal basis vectors.

The final approach for computing search directions, radiating out along uniformly distributed vectors made up of combinations of orthogonal basis vectors, eliminates the non-uniformity which results using Procedure 3. A uniformly distributed set of search directions could be computed by considering all combinations of $\pm 1$ times the basis vectors. The basis vectors may be calculated per Equation 4.7. This approach will yield $2^{n-1}$ search directions for an $n$ dof problem. Note that these search directions each involve a component along all of the orthogonal basis vectors.

An even more extensive set of search directions could be computed by considering all combinations $\pm 1$ and 0 (except all zeros) times the basis vectors. This will yield $3^{(n-1)} - 1$ search directions for an $n$ dof problem (6560 for a nine dof problem).
4.4.1 Selecting a Procedure

As mentioned above, Procedures 1 and 2 were eliminated from further consideration due to their computational complexity and apparent inadequacy, respectively.

Procedures 3 and 4 are similar in that they result in tractable numbers of search directions and in that the search density will automatically decrease with increasing distance from the center of the trouble region. Since it is impractical to have a uniform grid, it would seem desirable to decrease search resolution with distance from the center of the unsafe region since it is generally more desirable to find a point closer to the center of that region in order to attempt an efficient circumvention strategy. In other words, given a choice between failing to find a safe point near the center of the unsafe region and failing to find a safe point far from the center of the trouble region, one would choose the latter.

The differences between Procedures 3 and 4 are:

- Procedure 3 produces a non-uniformly distributed set of search directions whereas Procedure 4 guarantees uniform distribution.

- Procedure 3 allows for easy computation of search directions which favor certain joints whereas it is difficult to achieve such joint favoring using Procedure 4 since the basis vectors will, in general, have components in all joint directions.

The following example illustrates the uniform versus non-uniform distribution effect. Consider a three dimensional problem (so the search space will be planar) and let \( D = (2, 2, 1) \). The search directions that would be produced in the search plane using Procedures 3 and 4 are shown in Figure 4.7, where \( sd_1 = sd_2 \) for Procedure 3. Figure 4.7 shows that Procedure 4 consistently produces uniformly distributed search directions while Procedure 3 does not.
Experimentation was done with Procedures 3 and 4 for the cases implemented in Chapter 6. In all four scenarios considered (single 6 dof, single 9 dof, cooperating 6 dof, and cooperating 9 dof) both procedures were successful in solving a variety of problems. For more difficult problems, however, Procedure 4 produced noticeably better results, often with fewer search directions. This was true in spite of the ability to favor certain joints using Procedure 3.

As discussed in Chapter 6, search directions computed from the more extensive set based on combinations of $\pm sd_i$ and 0 times the basis vectors proved to be practical and effective for six dof problems. For 12 dof problems (such as cooperating nine dof robots), however, this procedure would produce 177146 search directions and thus could potentially result in very long execution times. In the 12 dof case, search directions computed from the smaller set based on combinations of $sd_i$ times the basis vectors (which yields 2048 for a 12 dof problem) proved to be a good compromise between practicality and effectiveness.

4.5 Prioritizing Search Directions

This section discusses methods for prioritizing search directions as required for Step 6 of Section 4.3.
Recall from above that the search directions are to be prioritized based on their dot product with the previously successful search directions. Recall also that the searches are conducted by looking at successively prioritized groups of search directions. Two methods were considered for achieving this prioritization:

- Sorting the search directions
- Grouping the search directions into bins

The first method would simply involve sorting the entire list of search directions based on their dot products with the previously successful search direction. Following the sorting, the search directions will be divided into groups of search directions having similar priority. This type of sorting was found to be computationally burdensome, unacceptably so for cases with several thousand search directions.

Grouping the search directions into bins involves much less computation than sorting the entire list and would seem to provide similar performance to sorting since the treatment of each search direction within a particular group differs only in the order in which they are considered (and not in the relative depths considered in each direction). Sorting into bins can be easily accomplished. If the dot product of the $i^{th}$ search direction, $S_i$, with the previously successful (or reference) search direction, $S_{ref}$, is $dp_i$, and the maximum and minimum dot products are $dp_{max}$ and $dp_{min}$, respectively, then a set of search directions can be grouped into $g$ equal breadth groups (bins) by the following rule:

$$S_i \in \text{bin}(j) \quad \text{if} \quad \frac{j - 1}{g} \leq \frac{dp_i - dp_{min}}{dp_{max} - dp_{min}} \leq \frac{j}{g} \quad (4.8)$$

It is this technique of bin sorting which is implemented in Chapter 6.

Another variation on the prioritization method is to consider the past history of successful search directions rather than simply considering the previous successful search direction. This can be accomplished by computing dot products with the
following reference search direction computed following a successful search:

\[ S_{\text{ref}} = \lambda S_{\text{ref}'} + (1 - \lambda) S_s \quad (4.9) \]

where \( S_{\text{ref}'} \) is the previous reference search direction, \( S_s \) is the most recent successful search direction, and \( \lambda \in [0, 1) \) represents a forgetting factor which may be used to vary the emphasis on the past history. With \( \lambda = 0 \), the method results in prioritizing exclusively based on the last successful search direction. The case \( \lambda = 1 \) is disallowed since \( S_{\text{ref}} \) would be invariant in that case.

Since in cooperating robot cases the role between leading robot and tracking robot may change (as discussed in the next Chapter), an effective reference search direction must be calculated for the tracking robot after each successful search. This effective reference search direction is the search direction which would have yielded the safe point found had the search been based on the tracking robot rather than the leading robot.

4.6 Comparison of the Heuristic to the Literature

This heuristic is somewhat similar to many of the c-space graph search techniques in that it is based around selective rather than exhaustive mapping of c-space. Aside from that broad similarity, this heuristic is fundamentally and significantly different from any of the approaches discussed in Chapter 2, with the most significant difference stemming from the process used to guide the selective mapping process. Nonetheless, it bares some some resemblance to Dupont's selective mapping [5], Glavina's goal directed sliding [46], and Warren's vector based approach [58] (see Section 2.1.1). Specific similarities and differences are discussed below.

The heuristic is similar to Dupont's approach in that both attempt to initially follow a c-space vector from start to goal and employ heuristics to attempt to minimize the amount of mapping required to circumvent unsafe portions of the path. The key difference is the type of heuristic used to attempt to traverse the trouble
regions. Interested only in single (redundant) robots, Dupont successfully used task space heuristics to build paths from each end of the trouble region until a feasible solution was found. The approach being presented here utilizes the c-space traversal heuristic described above to guide the selective mapping process.

The resemblance to Glavina's approach is that both perform a search in the n-1 dimensional hyperplane containing a point which was unsafe in the straight traversal between two points. Glavina's approach, however, performs those searches at the beginning of the trouble region and is therefore subject to blindly following strategies which look locally promising at the beginning of the trouble region but which may not lead to traversal around that region. Glavina's approach does, however, have the advantage over the heuristic being presented in this thesis in that it does not introduce intermediate points which may be in unreachable regions of free space. It is felt that that advantage does not outweigh the inherent inability of a completely local strategy to adopt a promising global course. It is expected that Glavina's approach would become excessively computationally intensive for problems with six or more dof even if the safe c-space possessed only relatively shallow concavities.

The resemblance to Warren's approach is that both are graph search type and "divide-and-conquer" in nature in that they attempt to identify an intermediate via point by searching outward from the center of the trouble region. The resemblance ends, however, when comparing the means used to identify a safe intermediate point. As discussed in Section 2.1.1, Warren's approach projects a vector from the centroid of the obstacle through the center of the unsafe region whereas the heuristic presented in this thesis utilizes structured searches of the hyperplane bisecting the trouble region. Warren's approach, while relatively new and still under development, has some potential difficulties:

- Obstacle centroids must be known in the space being considered (typically c-space). This is computationally intractable for more than a few dof.
• If the centroid lies on or near the unsafe vector the resulting intermediate point will lie at or near a previously found point thereby providing no new information.

• The case for which no safe point is found along the vector is not considered. As the dimensionality of the problem increases, the likelihood of finding a safe point along one particular vector would decrease rapidly.

• The case of obtaining an intermediate point in an unreachable region of space is not addressed.

These potential difficulties are all either addressed or eliminated by the approach being presented in this thesis.

Some of the potential fields approaches also adopt a "divide-and-conquer" style solution to attempt to circumvent local minima difficulties. Some techniques used in conjunction with potential fields approaches to locate intermediate trial points (via points) include task space heuristics, uniform grids, randomized motions, and use of potential functions (see Section 2.1.2). The heuristic presented herein does not resemble any of these approaches beyond the fact that each involve a divide-and-conquer style strategy.
CHAPTER 5
Utilizing the Heuristic for Robot Path Planning

This chapter explains how the divide-and-conquer c-space traversal heuristic presented in the preceding chapter may be utilized to solve single and cooperating robot path planning problems. This chapter is organized into three main sections:

- Single Robot Path Planning
- Cooperating Robot Path Planning
- String Tightening
- Handling Constrained Motions

Sections 5.1 and 5.2 discuss the utilization of the heuristic for single and cooperating robot path planning problems, respectively. A “string tightening” method to improve the efficiency of a path found by the planner is presented in Section 5.3. The implementation of the path planning strategy for particular single and cooperating robots is deferred until the following chapter.

5.1 Single Robot Path Planning

The single n dof robot path planning problem as defined in Section 3.4 can be addressed by direct application of the heuristic presented in Chapter 4 where the n dimensional space to be traversed is simply the configuration space of the n dof robot. C-space points are mapped only as needed by updating the geometric models of the robot links and the payload and performing interference detections as required to determine whether or not the specified joint variables correspond to a collision free configuration.
In all cases, the parameter \( c \) which determines step size (see Step 2 of Section 4.3) should be established for each task such that the largest possible step is many times smaller than the step size necessary for thinnest part of the robot/payload to step through the thinnest obstacle in one step.

Some potential issues which arise are:

- Handling robots with mixed joint types
- Joint limit problems
- Choosing \( \lambda \)
- Choosing number of bins
- Multiple robot configurations
- Singularity concerns

These issues are addressed below.

5.1.1 Handling Robots with Mixed Joint Types

Mixed unit concerns for robots with mixed joint types (some prismatic and some revolute) may be eliminated by linearly mapping each joint's actual range onto the interval \([0, 1]\), i.e.:

\[
\theta = \frac{q_a - q_{\text{min}}}{q_{\text{max}} - q_{\text{min}}} \tag{5.1}
\]

where \( q_a \), \( q_{\text{min}} \), and \( q_{\text{max}} \) represent the actual joint value, the lower joint limit, and the upper joint limit, respectively, all in identical units for each joint. Robots with revolute joints having no joint limits may be treated by replacing the denominator on the right hand side of Equation 5.1 with 360 degrees (\( 2\pi \) radians). No multiple rotations are permitted.
5.1.2 Joint Limit Problems

The joint limit problem is handled inherently since any point which would violate a joint limit is simply mapped as unsafe. In addition, the prioritization of search directions allows a reversal to take place when a potential joint limit is encountered. The prioritization strategy will then favor the direction away from the joint limit even after the immediate danger of hitting a joint limit is avoided. This reversal tendency is more global than the technique often employed with potential fields methods whereby a joint is repelled if it is in proximity to a joint limit.

5.1.3 Choosing $\lambda$

Recall from Equation 4.9 that prioritization of search directions utilizes a parameter denoted as $\lambda$. Experimentation with the test cases in Chapter 6 indicates that small $\lambda$ (near or equal to 0) provides the most robust path planner from the standpoint of finding a path for difficult problems, particularly for single robot problems. Path efficiency, however, appears to decrease with decreasing $\lambda$. In addition, small $\lambda$ does not perform particularly well for cooperating robot cases. This is likely partially due to the swapping of roles between the leading and tracking robot. The values used for $\lambda$ for the cases implemented will be presented in Chapter 6.

5.1.4 Choosing Number of Bins

Recall from Equation 4.8 that prioritized searches consider search directions grouped into bins. For the wide variety of problems considered, either 5 or 10 bins proved successful. In most cases, any number of bins in the 5 to 10 range would yield a solution although the path efficiency may decrease with an increase in the number of bins. Fewer than 5 bins did not provide robust performance and more than about 20 bins led to very inefficient paths (if a solution could even be found).
5.1.5 Multiple Robot Configurations

Recall from the problem definition in Chapter 3 that the start and goal joint angles are given. In addition, note that the path planner operates exclusively in c-space. As a result, multiple robot configurations which achieve identical end effector position/orientation need not be explicitly considered by the path planner.

5.1.6 Singularity Concerns

There are no singularity concerns using this approach for single robot path planning since singularities are a task space phenomena whereas the path planning approach is strictly configuration space based.

5.2 Cooperating Robot Path Planning

The two cooperating arm path planning problem is essentially equivalent to the single arm problem with the addition of the closure constraint, Equation 3.3. The closure constraint requires that, in order for a point in the configuration space of the one robot to be considered safe, it must correspond to a reachable and collision free configuration of the second robot. Thus, the basic concept for attacking the cooperating robot path planning problem is to apply the c-space traversal heuristic to one of the robots, referred to herein as the lead robot, with the other robot, referred to herein as the tracking robot, acting as a constraint. For example, the straight line path in c-space is determined for the lead robot and an attempt is made to traverse from the start position towards the goal position. If this attempted traversal is not entirely safe a search is conducted in the c-space of the lead robot with due consideration to the tracking robot. When the lead robot reaches the global goal position the entire path planning problem will have been solved. Mapping a particular point in the c-space of the lead robot involves verifying that the closure constraint can be met, updating geometric models of the robot links and payload,
and performing the required interference detection calculations.

The above rather simplistic conceptual explanation of applying the c-space traversal algorithm to two cooperating robots neglects the following potential issues:

- Handling robots with mixed joint types
- Joint limit problems
- Choosing a lead robot
- Handling cooperating redundant robots
- Multiple robot configurations
- Singularity concerns

The first two of these issues are identical for the cooperating robot case as for the single robot case discussed in Section 5.1. The remainder of these issues are discussed below.

5.2.1 Choosing a Lead Robot

The simplest way to choose a lead robot would be to always choose the same robot. This simple approach can be dismissed for the following reasons:

- A small change in the configuration of the lead robot might correspond to a much larger change in the configuration of the tracking robot thereby making it difficult to discretize the path to ensure that it is collision free. In an extreme case, it is possible that the lead robot may have the same start and goal positions for radically different start and goal configurations of the tracking robot (such as an arm configuration change).

- It would not allow the tracking robot to easily change configuration since this would typically involve passing the tracking robot through a singularity. It
is highly unlikely that the traversal heuristic would happen to prescribe lead robot positions which would allow the tracking robot to change configuration.

These difficulties may be eliminated by choosing the lead robot for each call to the heuristic based on relative distances (in c-space) between start and goal positions of each of the robots. This approach can be represented as follows:

\[
\text{if } ||\Theta_1 - \Theta_1|| < r ||\Theta_2 - \Theta_2|| \quad \text{then robot 1 leads} \\
\text{otherwise robot 2 leads}
\]  

(5.2)

where \( r \geq 1 \) represents a relative weighting between the two robots. Setting \( r = 1 \) would result in simply choosing the lead robot as the one with the greatest distance to travel. Equation 5.2 is evaluated to select the lead robot for each segment of the path where the \( s \) and \( g \) subscripts represent not the global start and goal positions but rather the start and goal positions for the particular segment of the path being addressed.

Experimentation with the cases in Chapter 6 revealed that oscillation tends to occur using this method for \( r = 1 \). These oscillations resembled a tug-of-war between the two robots.

Better path planner performance was achieved by choosing the lead robot based on relative c-space distances with consideration to past history. This approach favors the robot which led the previous segment unless the other robot has some multiple \( r \) further to go, i.e.:

\[
\text{if robot } i \text{ had led robot } j \text{ and} \\
\text{if } ||\Theta_j - \Theta_j|| < r ||\Theta_i - \Theta_i|| \quad \text{then robot } i \text{ leads} \\
\text{otherwise robot } j \text{ leads}
\]  

(5.3)

where \( r > 1 \) represents a relative weighting by which the distance for the formerly tracking robot must exceed the distance for the formerly leading robot before the
roles are reversed. Essentially, this method incorporates some hysteresis into the determination of the leading robot.

This approach was used to select the lead robot for the cases implemented in Chapter 6.

5.2.2 Handling Cooperating Redundant Robots

The implementation of the c-space traversal heuristic for cooperating robots as described in Section 5.2 requires that the closure constraint be checked for the tracking robot. Since each point in the c-space of the lead robot defines a position of the end effector of the tracking robot, inverse kinematics must be applied to determine if and how the tracking robot can reach a prescribed position/orientation. For cooperating non-redundant robots, the reachability of the second robot can be easily determined using inverse kinematics which are one-to-one. Checking the closure constraint for cooperating redundant robots, however, can be potentially difficult since the inverse kinematics are not one-to-one. Two possible methods of addressing the cooperating redundant robot path planning problem are:

- Applying the heuristic directly to one of the robots
- Applying the heuristic to a composite c-space with dimensionality equal to total number of degrees of freedom for the cooperating system

These two approaches are discussed below.

5.2.2.1 Applying the Heuristic Directly to One of the Robots

Application of the procedure directly to one of the robots would require some means for performing inverse kinematics on the redundant tracking robot. This inverse kinematics problem could be handled either by iterative testing of a number of prescribed positions for all but six of the joints or by utilization of a potential fields
based inverse kinematics solution. Iterative testing would likely prove very computationally expensive. A potential fields based inverse kinematic solution would be computationally tractable. Such an approach, however, has an intuitive disadvantage, namely that it does not treat all the free variables of the path planning problem in the same fashion. In implementation terms, this means that the treatment of the tracking robot would not contribute significantly to the overall strategy for solving the global cooperating robot path planning problem.

In attempt to further clarify this point, consider an example for which a potential fields inverse kinematics solution is used for the tracking robot. The inverse kinematics applied to each point prescribed by the lead robot must consider the position of the tracking robot at the previous point. This is necessary to avoid a discontinuous path for the tracking robot. The difficulty arises when the lead robot prescribes a point in the progression for which the inverse kinematics fail for the tracking robot. That failure of the inverse kinematics is contingent upon the path of the tracking robot up to the point before failure. Since no global path planning strategy was incorporated into the inverse kinematics of the tracking robot, it seems likely that better results might be obtained using a different strategy for selecting the configuration of the tracking robot.

5.2.2.2 Applying the Heuristic to a Composite C-Space

This technique for considering cooperating redundant robots was developed to enable the heuristic to be applied to a space with dimensionality equal to the effective number of dof for a cooperating system of robots. To illustrate this method, consider an $n_1$ dof robot (Robot 1) working cooperatively with an $n_2$ dof robot (Robot 2), $n_i > 6$. The mobility of the cooperating system is $m = n_1 + n_2 - 6$ per Equation 1.1. The two robots can be conceptually replaced with an $m$ dof lead robot and a six dof tracking robot by treating $n_2 - 6$ links of Robot 2 as if they belong to Robot 1.
In this manner, the c-space traversal heuristic can be applied to the mD c-space of the composite lead robot while one-to-one inverse kinematics can be applied to determine if the tracking robot can satisfy the closure constraint.

The main concern regarding this approach is that it results in increased dimensionality of the space which must be searched when implementing the c-space traversal heuristic. This increased dimensionality does, however, accurately reflect the problem complexity and is therefore considered reasonable. It also seems reasonable to expect that the traversal heuristic would handle the extra dof in a more logical fashion than considering them in the inverse kinematics of the tracking robot.

Application of this procedure to cooperating nine dof robots would amount to considering a twelve dof composite robot being tracked by a six dof robot. The heuristic would then be applied to the 12D c-space of the composite robot. Results presented in Chapter 6 illustrate that this technique is a practical and effective way to address the path planning problem for cooperating nine dof robots.

A similar approach could be applied to cooperating robots with less than six degrees of freedom. For example, consider two five dof manipulators. Since the inverse kinematics for the five dof robot would be overdetermined (i.e., not every position and orientation would have a solution), it would appear more effective to plan based on, for example, the first four joints of a lead robot. The lead robot's remaining joint and the five joints of the tracking robot would effectively result in a six degree of freedom robot with one-to-one inverse kinematics. In this case, such an approach would actually reduce the dimensionality of the search space (from five to four) as compared to direct application of the heuristic to one of the robots. Once again, the heuristic is applied to a space with dimensionality equal to the actual mobility of the cooperating system.
5.2.3 Multiple Robot Configurations

In general, a six dof robot will possess a finite number of distinct robot configurations which achieve identical end effector position/orientation (such as elbow up or elbow down for a Puma). This situation is represented mathematically in Equation 3.5. Multiple configurations are handled inherently for the lead robot just as in the single robot case. However, special consideration is required to address this issue for the tracking robot. The following set of rules address this issue:

1. Configurations must be defined such that, for the robot in any one configuration, an infinitesimal change in end effector position/orientation will always correspond to an infinitesimal change in the corresponding joint angles.

2. During progressions forward through safe space (Steps 3 and 9 of Section 4.3), the tracking robot shall maintain the same configuration as it had at the start of that segment of the path.

3. While mapping through unsafe space in search of a safe point (Step 4 of Section 4.3), only the configuration of the tracking robot at the goal position of the current segment of the path shall be considered.

4. While conducting searches (Step 7 of Section 4.3), all possible configurations of the tracking robot shall be considered.

These rules will enable full use of all available configurations while prohibiting discontinuous motions of the tracking robot for smooth motions of the leading robot.

5.2.4 Singularity Concerns

Robot arm degeneracy at singularities is handled inherently by the path planning method. For the lead robot, only singularity-free c-space is considered. For the tracking robot, any region prescribed by the lead robot which cannot be tracked
by the other robot is mapped out as an unsafe region. This combined with the ability to swap roles between the leading and tracking robots results in a planner which inherently handles singularity concerns for cooperating robots. This means of handling singularities does not attempt to physically avoid singular configurations but rather allows either robot to pass through singularities as necessary when attempting to solve the path planning problem.

5.3 String Tightening

The path planning procedure presented thus far has a principle objective of finding a feasible solution. As a result, the paths found will typically be sub-optimal in some sense and it should be possible to modify a feasible path found by the planner to produce a better one. This process of path modification may be referred to as string tightening. This section presents a brief history of approaches used for string tightening and then presents an approach which can be utilized for string tightening paths found for two cooperating robots.

5.3.1 History of Smoothing

Once a collision free path has been found by a robot path planner, it can be further optimized by numerical methods. A commonly used cost function aims to minimize the length of the path while incorporating safety clearances from obstacles. The resulting performance index to be minimized can be expressed as:

\[ J = \int_{\Theta_s}^{\Theta_g} (1 + \frac{w}{D(\Theta)}) d\Theta \]  \hspace{1cm} (5.4)

where \( D(\Theta) \) is the minimum distance between the robot and obstacles, \( w \) is a weighting factor, and the integral is taken over all configurations connecting \( \Theta_s \) and \( \Theta_g \). Polytope methods seem to be the current state of the art for computing robot to obstacle distances. Bryson and Ho [96] note that several numerical methods
may be used to find a path with minimum $J$ using any feasible path as an initial guess. Simple gradient methods perform reasonably well for this purpose. The resulting path, however, is only optimal in the vicinity of the initial guess.

An alternate technique for path smoothing which also attempts to shorten a path while maintaining due safety clearances is Thorpe’s [97] path relaxation technique. This process begins with a mobile robot path consisting of straight line connections between a sequence of nodes. The relaxation involves moving one node at a time in either direction perpendicular to the line connecting the preceding and following nodes in order to minimize the cost of traversing between the three nodes. The cost function is similar to Equation 5.4 since it includes length of path segment with a penalty for proximity to obstacles or unmapped (unknown) regions. Since moving a node may affect its neighbors, the process is repeated until no nodes move more than some small tolerance.

Another technique which can be used to smooth paths, avoid collisions, and move paths away from objects is based on potential fields. Krogh [74] presents one such approach. Krogh uses sensory measurements of obstacles as feedback during execution of paths planned with another algorithm. This feedback can help to smooth jagged paths and to steer the path away from obstacles.

5.3.2 String Tightening Algorithm

This section presents a method for improving upon a path produced by the cooperating robot path planner. Recall from Chapter 3 that the path planner output consists of a sequence of closely spaced knot points for both robots along a feasible and collision free path.
5.3.2.1 Measure of Goodness

A variety of possible criterion may be used to evaluate the quality of a path. For string tightening purposes, the goodness of a path may be measured by the sum of the lengths of the joint space trajectories for the two cooperating robots. Since the path planner produces discretized paths for both robots, the objective during string tightening is to reduce the following cost function:

\[
L_1^N = 2 \sum_{r=1}^{N} \sum_{i=1}^{n_r} \sqrt{\sum_{j=1}^{n_r} \left( \theta_{rj}(i+1) - \theta_{rj}(i) \right)^2}
\]

(5.5)

where:

- \(L_1^N\) = the sum of the joint space trajectory lengths
- \(N\) = number of knot points in path
- \(r\) = robot identifier
- \(n_r\) = number of dof for robot \(r\)
- \(\theta_{rj}(i)\) = \(i^{th}\) knot point for robot \(r\) joint \(j\)

If the original path is considered to be a string passing through the knot points in the joint space of each of the robots, then the objective for improving upon the path is to shorten the sum of the string lengths while maintaining the same endpoints. Hence the name string tightening as suggested by Dupont [5].

The tightening algorithm which was implemented involves examining each sequence of three adjacent knot points and performing whichever of the three options below produces the most desirable effect on \(L_1^N\):

1. Make no changes to the knot points.
2. Modify the second knot point for robot 1 so that the three knot points are straight in the joint space of robot 1 (if not already so).
3. Modify the second knot point for robot 2 so that the three knot points are straight in the joint space of robot 2 (if not already so).

The feasibility of options 2 and 3 must be determined with consideration to closure and collisions. The procedure described in Section 5.2 can again be used to simplify the question of closure for cooperating redundant robots. The incremental effect which each of the above options will have on $L_i^N$ can be assessed using Equation 5.5 over the appropriate three knot point segment.

These local adjustments are continued until no significant improvement can be obtained from further adjustments.

A conceptual illustration of the string tightening algorithm for cooperating robots is shown in Figure 5.1. An initial three knot point segment for the two robots is shown in Figure 5.1a. These three knot points are a portion of a much longer many knot point path. Figure 5.1b and c show the effect of options 2 and 3, above. In this example, option 2 (moving the second knot point of robot 1 in line with its neighbors) produces the most significant reduction in path length. Thus, this iteration would move each robot’s second knot point to their positions in Figure 5.1b.

![Figure 5.1: Local Effect During String Tightening](image)

For single robot problems, Equation 5.5 need only be evaluated for one robot and the options are reduced to two:
1. Make no changes to the knot points.

2. Modify the second knot point so that the three knot points are straight in the robot's joint space (if not already so).

### 5.3.2.2 Limitations of the String Tightening Algorithm

Because this string tightening method involves a discretized approximation to continuous deformation, the tightened path may still be far from optimal. For example, consider Figure 5.2. A safe path may be found as shown in Figure 5.2a. A shorter path found by continuous deformation of the original path is shown in Figure 5.2b. However, this path is suboptimal as shown by Figure 5.2c.

![Figure 5.2: String Tightening May Not Produce Optimal Path](image)

One disadvantage of the approach is that the shortened paths tend to provide very little obstacle clearance. This property is generally more acceptable for manipulators than for mobile robots because the manipulator environment is generally accurately known and the manipulator control is typically precise. Possible means for addressing this limitation are discussed in Section 8.2.1.

This string tightening algorithm is also unable to find any paths which would require temporary lengthening of the path in order to ultimately achieve a better path.
5.3.3 Comparison to Other Path Smoothing Approaches

This approach is very similar to Thorpe's approach discussed in Section 5.3.1 where the differences are as follows:

- Cooperating robots are considered.

- The cost function is c-space distance only, whereas Thorpe includes distance from obstacles in the cost function.

- The sequences of points are closely spaced knot points, whereas Thorpe's node points may be far apart.

5.4 Handling Constrained Motions

Earlier, it was assumed that the end effector motion between the start and goal positions may be arbitrary. Though this is a valid assumption for the typical robot path planning problem in free space, there are cases where contact between the payload and an obstacle may lead to constrained rather than arbitrary end effector motion. For example, the payload may come into planar contact with a table surface. As such, the end effector motion is confined to 3 dof (two translations and a rotation) as opposed to 6 dof. Although such cases are not considered in this thesis, the heuristic could be utilized to solve such problems by applying the heuristic in the task space defined by the reduced degrees of freedom rather than in the joint space of the robot. The robot must be away from singularities in order for such an approach to be effective.
CHAPTER 6
Implementation and Results

This chapter presents the implementation details and results of applying the path planning method described in the preceding chapters to the following single and cooperating robot scenarios:

- The CIRSSE Testbed (single 6 dof, single 9 dof, cooperating 6 dof, and cooperating 9 dof cases)
- The Automated Structure Assembly Lab at NASA Langley (6 dof case)
- Cooperating Pumas Assemble a Truss Structure

The specifics of each of these implementations and sample results are presented in sections which follow. First, some points common to all of these implementations are presented in the next section.

6.1 Characteristics Common to All Implementations

All of the implementations that will be discussed in this chapter have the following common characteristics:

- Heuristic is applied generically
- Geometric modeling is done with polytopes.
- A hierarchical interference detection scheme is used.
- Paths may be visually simulated using CimStation.
- The programs are written in C.

These characteristics are discussed below.
6.1.1 Heuristic is Applied Generically

All of the cases invoke the c-space traversal heuristic in its completely general form. In other words, in no case are task or hardware specific assumptions or modifications utilized. Search direction computation is always done strictly mathematically. The ability to directly apply the heuristic generically to a variety of problems suggests that the planning methodology presented herein could be quickly and effectively applied to hardware or tasks not addressed herein.

6.1.2 Geometric Modeling with Polytopes

The geometric modeling scheme implemented to enable interference detection utilizes polytope models of the robot links, payload, and obstacles in the workspace. Details of the modeling may be found in [6]. A polytope is a set of points whose convex hull (the smallest volume which encloses all points) describes the object being represented. The polytope representation incorporates a radius which can be used to achieve a safety margin. A few simple 2D polytopes are shown in Figure 6.1. In 3D, a two vertex polytope would correspond to a cylinder with hemispherical end caps, where the radius of the cylinder and of the end caps is specified by the polytope radius. A 3D block can be made using eight vertices and a radius of zero.

The polytope representation scheme was chosen because it permits accurate modeling of the robots and typical obstacles in the workcell while enabling relatively fast interference checking. Although each polytope represents a convex object, concave objects may be easily modeled as several distinct convex polytopes.

6.1.3 Hierarchical Interference Detection

Collision checking is currently being done in a two level hierarchy. First, spherical approximations for each pair of potentially colliding objects are examined. If the spherical approximations do not intersect then there is no possibility of collision
between the pair of objects under consideration. If the spherical approximations do intersect then a polytope distance calculation routine is invoked to determine whether or not the two objects intersect (collide). The polytope routines being used were provided by Hamlin and Kelley [98, 99]. The reason for the spherical approximation level of the hierarchy is to reduce the number of computationally expensive calls to the polytope distance calculation routine.

Mapping a point in c-space thus reduces to the following steps:

1. Verifying the closure constraint and determining the configuration of the tracking robot (not necessary in single robot cases).

2. Updating the coordinates of the sphere centers and polytope vertices based on the joint angles of the point being mapped.

3. Performing interference detection per the hierarchy discussed above.

The interference detection routine for the path planner simply needs to determine a yes or a no regarding collision. This enables use of faster routines than would be required if the path planner needed to know distances and directions between pairs of objects.
6.1.4 Animation of Paths

Paths found by the path planner may be visually animated using any suitable robot simulation package. We use CimStation, a commercially available package, for path animation purposes. The interface between the path planning programs and CimStation is a file storing the sequence of knot points determined by the path planner. CimStation then replays the sequence to animate the path found by the planner. The CimStation workcell model must, of course, be consistent with the world model given to the path planner. The CimStation model of the CIRSSE testbed used for this work was developed by Hron [100]. The CimStation model of NASA Langley’s ASAL lab was provided to us by NASA Langley. The model used for the cooperating Pumas assembling a truss is an edited version of the model of the CIRSSE testbed.

For CIRSSE testbed cases, path planning program output may also be run on the actual hardware by first applying a trajectory generation routine to the planner output and then running the resulting trajectory in the typical fashion. For cooperating robot cases, path execution in this manner requires use of active compliance on one of the two end effectors at any given time to maintain acceptable internal forces on the payload. Further work to be done in the area of integrating the path planner into the CIRSSE testbed is discussed in Section 8.2.2.

CimStation was also found to be very useful in defining the start and goal joint angles for path planning problems, particularly in the cooperating robot case. Due to the tremendous loss of workspace due to the closure constraint, it is easy to inadvertently define start and goal positions of the robot which are feasible but which probably have no path which can connect them. CimStation may be used to view different robot configurations and to quickly determine the feasibility of a robot reaching a particular pose. The various robot configurations may be tried as input to the path planner until a solution is found.
6.1.5 Description of Programs

All of the path planning programs were implemented in the C programming language. Portions of the program utilize code developed by Schima [6]. The path planning programs are similar for all cases considered. A sample flowchart is shown in Figure 6.2.

Program inputs and outputs are per the problem statements in Chapter 3. Additional output is included to document and evaluate the performance of the path planner. This output includes the following:

- $N_p =$ Number of knot points in path.
- $N_s =$ Number of searches required.
- $\Delta L/L =$ Percent reduction in path length due to string tightening.
- $L_f =$ Final path length after string tightening (Eqn. 5.5).
  - Note that this is dimensionless since joints are scaled using Equation 5.1
- $N_{sph} =$ Calls to spherical interference check function.
- $N_{poly} =$ Calls to polytope interference detection function.
- $t_{path} =$ Time to find safe path.
- $t_{tight} =$ Time to string tighten.
- $t_{cc} =$ Time spent collision checking (both phases).
- $t_{poly} =$ Time spent in polytope phase of collision detection.
- $t_{tot} =$ Total time.

The condition used to terminate string tightening is that a knot point will be moved only if doing so will reduce the distance over the three knot point segment centered at that point by at least 0.5 percent.
Figure 6.2: Flowchart of Path Planning Program
6.2 CIRSSE Testbed

The path planning method described herein has been implemented for the robotic testbed system of the Center for Intelligent Robotic Systems for Space Exploration (CIRSSE) at Rensselaer Polytechnic Institute (RPI). The CIRSSE testbed, shown earlier in Figure 1.2, consists of two 6R Puma 560's, each of which rides on a separate Aronson 1P-2S platform. The kinematic parameters including joint limits may be found in [101] and in Appendix A.

The methods described in this thesis have been implemented for four different CIRSSE testbed scenarios:

- Single Puma
- Single 9 dof robot (platform plus Puma)
- Cooperating Pumas
- Cooperating 9 dof robots

Numerous path planning problems were contrived for these different scenarios in attempt to illustrate the effectiveness of the path planner for various potentially difficult path planning problems. Implementation details and sample results for each of the scenarios are presented below. Applications of the path planner to more practical path planning problems are discussed later in Sections 6.3 and 6.4. Except as noted for the case specifically illustrating the effect of string tightening, all paths illustrated herein are the final path obtained after string tightening. Start and goal joint angles and obstacle definitions for the included CIRSSE testbed examples (Examples 1 through 4) are provided in Appendix B.
6.2.1 Single Puma 560

The path planner was implemented for such a single Puma path planning problem. The specific parameters of the implementation are as follows:

\[
c = \frac{1}{200} \text{ step size (See Step 2 of Section 4.3)}
\]

\[
N_{SD} = 242 \text{ search directions per Procedure 4}
\]

\[
g = 10 \text{ bins (see Equation 4.8)}
\]

\[
\lambda = 0.5 \text{ forgetting factor (See Equation 4.9)}
\]

6.2.1.1 Example 1

A sample path found by the single Puma path planner is shown in Figure 6.3. Figure 6.4 provides a top and side view of the start configuration. A trace of the path followed by the payload is shown in Figure 6.5.

The results for this example are summarized in Table 6.1. The variables in the Table are as defined in Section 6.1. As shown in the table, the total time required to find a path and perform string tightening was just over three minutes. Approximately 60% of the total time involved finding a safe path with the remaining time utilized for string tightening.

The payload for this example is a 0.7 meter long strut, a scale version of the type which might be used to construct space structures such as Space Station Freedom. A long, thin payload such as this highlights the need for consideration to rotational as well as translational degrees of freedom. This path planning problem is potentially difficult because limits on joint 1 prohibit a simple counterclockwise rotation (viewed from above) which would move the payload from start to goal. As a result, the prominent motion is clockwise and escaping from the box-like obstacle near the start requires some backtracking to remove the strut from within the box. Once the strut is out of the box there is also potential for allowing the strut back
Table 6.1: Summary of Results for CIRSSE Testbed Examples (times in seconds)

<table>
<thead>
<tr>
<th></th>
<th>Single Puma (Example 1)</th>
<th>Coop. Pumas (Example 2)</th>
<th>Single 9 DOF (Example 3)</th>
<th>Coop. 9 DOF (Example 4)</th>
</tr>
</thead>
<tbody>
<tr>
<td>$N_p$</td>
<td>717</td>
<td>524</td>
<td>1124</td>
<td>1307</td>
</tr>
<tr>
<td>$N_s$</td>
<td>112</td>
<td>154</td>
<td>42</td>
<td>78</td>
</tr>
<tr>
<td>$\Delta L/L$</td>
<td>20.2</td>
<td>16.4</td>
<td>8.4</td>
<td>14.2</td>
</tr>
<tr>
<td>$L_f$</td>
<td>3.04</td>
<td>2.14</td>
<td>9.35</td>
<td>14.27</td>
</tr>
<tr>
<td>$N_{sph}$</td>
<td>745K</td>
<td>1.72M</td>
<td>1.60M</td>
<td>3.34M</td>
</tr>
<tr>
<td>$N_{poly}$</td>
<td>128K</td>
<td>390K</td>
<td>94.5K</td>
<td>189.5K</td>
</tr>
<tr>
<td>$t_{path}$</td>
<td>114 sec</td>
<td>560</td>
<td>158</td>
<td>167</td>
</tr>
<tr>
<td>$t_{tight}$</td>
<td>71</td>
<td>38</td>
<td>185</td>
<td>384</td>
</tr>
<tr>
<td>$t_{cc}$</td>
<td>101</td>
<td>283</td>
<td>118</td>
<td>247</td>
</tr>
<tr>
<td>$t_{poly}$</td>
<td>69</td>
<td>201</td>
<td>52</td>
<td>115</td>
</tr>
<tr>
<td>$t_{tot}$</td>
<td>185</td>
<td>598</td>
<td>343</td>
<td>551</td>
</tr>
</tbody>
</table>

into the box. Similarly, achieving the goal position requires passing the triangular obstacle, aligning the strut for insertion between the sides of the triangle, and performing that insertion. This example also illustrates the fact that concave objects such as the box and the triangle may be easily modeled as several distinct convex polytopes whose combined effect defines a concave task space object.
Figure 6.3: Sample Results for Single Puma (Example 1)
Figure 6.4: Start Configuration for Example 1

Figure 6.5: Trace of Payload Path for Example 1
6.2.2 Single 9 DOF Robot

The path planner was implemented for a single nine dof robot consisting of one of the testbed's platforms plus the attached Puma. The specific parameters of the implementation are identical to those presented in Section 6.2.1 for a single Puma except for the number of search directions. In the single 9 dof case, the number of search directions is:

\[ NSD = 6560 \text{ search directions} \]

6.2.2.1 Example 2

A sample path found by the single 9 dof path planner is shown in Figure 6.6. This problem is identical to the problem in Example 1 except that the extra three dof of the platform may be utilized. The path found by the planner uses the platform translation and tilt capabilities to aid in obstacle avoidance.

The results for this example are summarized in Table 6.1. As shown in the table, the total time required to find a path and perform string tightening was just under ten minutes. The results also show that the redundancy was utilized to produce a path which was approximately 50% shorter than the path obtained for the Puma alone. Over 90% of the total time involved finding a safe path with the remainder of the time utilized for string tightening.
Figure 6.6: Sample Results for Single 9 DOF Robot (Example 2)
6.2.3 Cooperating Puma 560's

Addressed in this implementation is the path planning problem for the two CIRSSE testbed Pumas working cooperatively. Thus, the platforms may be used to initially position the two Pumas but are stationary throughout the planning problem. The specific parameters of the implementation are as follows:

\[ c = \frac{1}{300} \quad \text{step size} \]
\[ N_{SD} = 242 \quad \text{search directions} \]
\[ g = 5 \quad \text{bins} \]
\[ \lambda = 0.5 \quad \text{forgetting factor} \]
\[ r = 4 \quad (\text{See Equation 5.3}) \]

6.2.3.1 Example 3

This example involves a space containing six obstacles arranged in a maze-like fashion. The path planner successfully finds the path shown in Figure 6.7 which traverses from start to goal with no collisions. The payload is a 3cm x 3cm x 110 cm box. The clearance between the long horizontal obstacles is 15cm. Figure 6.8 provides a top and side view of the start configuration. Similarly, Figure 6.9 provides a top and side view of the goal configuration.

The results for this example are summarized in Table 6.1. As shown in the table, the total time required to find a path and perform string tightening was under six minutes. Approximately 46% of the total time involved finding a safe path with the remaining time utilized for string tightening.

This example seems to reflect the maximum level of difficulty which the cooperating Puma path planner as presently implemented can solve within a reasonable amount of time. For example, if the obstacle near the goal end of the passageway between the two long obstacles is lengthened downward by 0.1 meters the planner
fails to find a path (when allowed to try for over an hour). This failure to find a solution occurs even though it is apparent to the user that a solution does exist. Example 3 is also a path planning problem which the planner cannot solve if the start and goal positions are interchanged. In that case the planner begins by going below the open passageway between the long obstacles and then fails to find a path which can circumvent the lowest obstacle. Once in this position, it seems likely that a planner would need to resort to an impractical exhaustive mapping of a huge concavity before determining that significant backtracking would need to take place to find the opening to the passageway.

When difficulty was experienced with the cooperating robot path planner (cooperating 6 and cooperating 9 dof case), the source of the difficulty virtually always turned out to be in the choice of the start and goal robot configurations (i.e., the start and goal joint angles). Such difficulties appear difficult to address intuitively but are easily addressed brute force by trying all combinations of feasible Puma configurations at the start and goal positions. This typically resulted in at least one suitable problem definition for which the planner was successful.
Figure 6.7: Sample Results for Cooperating Pumas (Example 3)
Figure 6.8: Start Configuration for Example 3

Figure 6.9: Goal Configuration for Example 3
6.2.4 Cooperating 9 DOF Robots

Addressed in this implementation is the path planning problem for the two 9 DOF CIRSSE testbed robots working cooperatively. The specific parameters of the implementation are as follows:

\[
c = \frac{1}{150} \text{ step size}
\]

\[
N_{SD} = 2048 \text{ search directions}
\]

\[
g = 10 \text{ bins}
\]

\[
\lambda = 0.5 \text{ forgetting factor}
\]

\[
r = 10
\]

Recall from Chapter 5 that the c-space traversal heuristic is applied in a 12D space for cooperating 9 dof path planning problems. As a result, the complexity of the cooperating 9 dof robot path planning problem is immensely higher than the complexity of the cooperating 6 dof. This increased complexity would result in \(3^{11} - 1\) or 177146 search directions using Procedure 4. Since such a number of search directions would be computationally impractical, this implementation utilized the reduced set considering all combination of \(\pm 1\) times the basis vectors. This results in \(2^{11}\) or 2048 search directions.

6.2.4.1 Example 4

A sample path found by the cooperating 9 dof robot path planner is shown in Figure 6.10. The start and goal positions appear in the upper left and lower right, respectively. Figures 6.11 and 6.12 provide top and side views of the start and goal configurations, respectively.

The results for this example are summarized in Table 6.1. As shown in the table, the total time required to find a path and perform string tightening was just
under 10 minutes for this example. Approximately 30% of the total time involved finding a safe path with the remaining time utilized for string tightening.
Figure 6.10: Sample Results for Cooperating 9 DOF (Example 4)
Figure 6.11: Start Configuration for Example 4

Figure 6.12: Goal Configuration for Example 4
6.2.5 Effect of String Tightening

An example of the effect of string tightening on the payload path for a cooperating nine dof robot path planning problem is shown in Figure 6.13. Parts (a) and (b) of the figure show traces of load positions along the path before and after string tightening, respectively. The string tightening phase required approximately 30 minutes computation time and resulted in a 37% reduction in path length.

Figure 6.13: String Tightening a Path for Cooperating Nine DOF Robots
6.3 NASA Langley's Automated Structure Assembly Lab

A CimStation model of NASA Langley's Automated Structure Assembly Lab (ASAL) is shown in Figure 6.14. The system consists of a 6 dof Merlin robot, shown in Figure 6.15, mounted to a xy-positioning table (referred to as the carriage), and a turntable. The turntable includes a triangular platform which can rotate around a vertical axis through its center. The Merlin robot is kinematically similar to a Puma. The objective of the ASAL is to assemble truss structures consisting of 102 2 meter long struts. Such a truss is illustrated in Figure 6.16. The truss is assembled upon the turntable of the ASAL by positioning the carriage and the turntable such that the Merlin may take each strut from a canister near the base of the Merlin and install it in its final position in the assembly.

A single arm path planner was implemented for the ASAL environment. The implementation parameters are as follows:

\[
c = \frac{1}{400} \quad \text{step size}
\]
\[
N_{SD} = 242 \quad \text{search directions}
\]
\[
g = 5 \quad \text{bins}
\]
\[
\lambda = 0.0 \quad \text{forgetting factor}
\]

The assembly sequence considered was provided by NASA. The path planner quickly found paths for the first 21 struts since there is little possible interference at that stage. Due to symmetry, the assembly of the remaining 81 struts can be accomplished using only 21 unique trajectories for the Merlin with the appropriate carriage and turntable positions for each strut. The path planner was able to find feasible paths for all 102 struts with solution times ranging from 1 to 30 minutes, with the vast majority of solution times in the 2 to 5 minute range. Since the final approach must be in a specified direction, the goal positions used were 10 cm from the final strut position with the end effector oriented to allow the final insertion to
be performed by a straight task space move.

This implementation of the path planner for the ASAL assembly task illustrates the potential usefulness of the path planning technique presented in this thesis for solving practical, potentially very difficult real-world path planning problems. Some particular comments regarding this implementation follow:

- The path planner has no trouble with goal positions placing the load or robot in very close proximity to obstacles.

- The path planner performs well even with a large number of obstacles. For example, the final few struts of the assembly involve over 100 workspace obstacles. The additional collision checks required near the end of the assembly seem to increase execution time by a factor of approximately two.

- The paths found typically include segments which are obstacle boundary tracing. Because of the close tolerances involved, it is not practical to simply model the objects larger than actual size to provide a safety margin since so doing may result in an unsolvable problem. This shortcoming was noted earlier in Section 5.3.2.2 and possible remedies are addressed in Section 8.2.1.

- The nodes to connect the struts were not modeled. As a result, some of the paths might collide with the nodes if the paths were used in an actual assembly. This could be remedied simply by modeling the nodes and including them in the collision checking routine. Due to the small size of the nodes it is expected that including them would have little impact on the difficulty of the path planning problems.

- In a few cases the path planner was not always able to solve the problem quickly in the forward direction but could quickly solve the problem in the opposite direction. Although a very confined goal position makes it likely that
solving in reverse may prove easier, trial and error was the only sure way to
decide which direction would yield better performance.

• Return paths for the robot after inserting a strut were not planned.

6.4 Cooperating Pumas Assemble a Truss

This section describes the implementation of the path planner to a task whereby
two Pumas work cooperatively to assemble a 24 strut truss. The workcell for this
implementation with the completed truss is shown in Figure 6.17. The pumas are in
their start position in Figure 6.17. The workcell includes two Puma 560's which are
500 cm apart and mounted to a carriage. The carriage can translate toward or away
from a turntable upon which the truss is assembled. The carriage and turntable
are used to position the Pumas and the partially completed truss structure such
that the Pumas may insert each strut without concurrent motion of the carriage or
turntable. The struts are 133 cm long. The robot end effectors are 100 cm apart
when grasping a strut. The parameters for this path planning implementation are
as described in Section 6.2.3 for the CIRSSE Pumas.

The planner successfully planned paths for all 24 struts with solution times
per strut ranging from less than one minute to approximately 10 minutes. Some
points regarding this implementation are as follows:

• Many of the paths found involve multiple arm configurations for one or both
  Pumas. As a result, the robots pass through many task space singularities.

• There is significant potential for collision between the robots due to their
  proximity.

• Although the start positions were identical and all the goal task space positions
  were known, trial and error was typically necessary in order to determine
  suitable goal Puma configurations which would enable a solution to be found.
Figure 6.14: NASA Langley's Automated Structure Assembly Lab
Figure 6.15: 6 DOF Merlin Robot with End Effector for Truss Assembly

Figure 6.16: 102 Strut Truss Structure
Figure 6.17: Workcell for Cooperating Pumas Assembling Truss
CHAPTER 7
Discussion of the Path Planning Strategy

This chapter discusses the path planning strategy presented in this thesis. This chapter is organized into three main sections:

- Completeness
- Computational Complexity
- Overall Effectiveness

Completeness and computational complexity are discussed in Sections 7.1 and 7.2, respectively. Section 7.3 attempts to judge the overall effectiveness of the strategy.

7.1 Completeness

Unfortunately, the path planning approach is not complete. In other words, the approach does not guarantee that a solution will be found or determine that a solution does not exist. Based on the literature (see Chapter 2), it appears to be difficult to achieve both completeness and practicality for reasonably difficult yet practical path planning problems with more than a few degrees of freedom. Since our emphasis was toward achieving a potentially useful path planner for cooperating robots with at least 6 dof each, we sacrificed completeness in exchange for the possibility (with no guarantees) of solving some practical problems within a reasonable amount of computation time.

This lack of completeness was discussed earlier in Section 4.3.1 where it was shown that the c-space traversal heuristic around which the path planner is based can fail to find a solution even if one may exist due to one of the following scenarios:
• Cycling occurs.

• No safe point is found by the limited set of search directions.

Modifying the heuristic to guarantee finding a safe point if one exists (such as by continually increasing the search resolution) would still not ensure completeness since cycling might still occur. In addition, it was shown in Section 4.4 that performing even one thorough search can be computationally intractable.

Many path planning algorithms such as those based on randomized searches are probabilistically complete, meaning that given sufficient computation time they will guarantee finding a solution if one exists. However, such algorithms offer little practical value since they inevitably take a very long time to run for reasonably difficult problems.

7.2 Computational Complexity

Computational complexity of this work can be analyzed by giving an upper or a lower bound on the number of elementary computations or the size of memory required to solve a problem. Recall from Chapter 2 that the n dof robot path planning problem is PSPACE-hard with an upper bound complexity of $O(n^2)$.

This section investigates the computational complexity of the planner in order to determine how an increase in system dof would be expected to affect solution time. The computational complexity of the planner can be addressed in three parts:

• Precomputations

• Mapping a c-space point.

• Performing searches

• Overall Complexity
These parts are discussed below.

The path planning method presented in this thesis requires no precomputations.

Consider a workspace involving an $n$ link robot and $m$ obstacles. Mapping a $c$-space point involves the following operations:

- Updating the link model
- Checking for joint limit violations
- Checking for collisions

Both updating the link model and checking for joint limit violations have an upper bound complexity $O(n)$. Checking for collisions has a higher upper bound complexity $O(nm)$. Thus, $c$-space mapping computations grow linearly with both increasing dof and number of obstacles.

The worst case complexity for performing searches will be a linear function of the number of search directions used. For search directions computed as described by Procedure 4 in Chapter 4, an upper bound on search complexity for an $n$ dof problem is $O(k^{n-1})$, where $k < n$. For our implementation, $k = 3$ for problems with a mobility $m \leq 9$ and $k = 2$ for problems with mobility $m = 12$.

An overall upper limit on computational complexity can be taken to be the worst case complexity of the above three operations. Thus, the path planner presented in this thesis has an upper bound on complexity of $O(k^{n-1})$, where $k < n$.

7.2.1 Possible Benefits of Parallel Processing

When mapping along a prescribed vector, parallel processing could be used to map each discretized point along that vector simultaneously. Even more significantly, the various possible search directions and even the different depths in those
directions could be examined simultaneously. Parallel processing could also greatly speed the interference checking by performing multiple checks simultaneously.

A massively parallel machine, such as the Connection Machine which has \(2^{16}\) (or 65536) 1-bit processors, could radically decrease the execution time of the path planner presented in this thesis.

### 7.3 Overall Effectiveness

Relatively few other approaches have appeared in the literature for solving the cooperating robot path planning problem for robots with six dof each. The path planning strategy presented in this thesis appears to be capable of solving more difficult problems than those approaches. In addition, this thesis illustrates that the strategy presented can be practically applied to cooperating nine dof robots. Results in the literature for cooperating redundant robots appear to be limited to planar manipulators. A single arm version of the planner has demonstrated the ability to solve some practical yet potentially very difficult path planning problems in a reasonable amount of time. Some general statements regarding the effectiveness of the path planner follow:

- Solution times are reasonable for off-line programming (typically under 30 minutes).
- Potential problems with joint limits and multiple arm configurations are inherently handled.
- The planner performs well and in reasonable time even with over 100 obstacles.
- The planner is effective even for start and/or goal positions involving little safety clearance.
CHAPTER 8
Conclusions and Future Work

This Chapter presents some conclusions on the subject of this thesis, Section 8.1, and discusses some areas for future work, Section 8.2.

8.1 Conclusions

The general problem of planning collision free paths for an \( n \) dof robotic systems has an upper bound on complexity of \( O(n^n) \). As a result, exact solutions to the robot path planning problem will likely remain excessively computationally intensive for some time. As a result, any implementation of autonomous robotic path planning which is likely to prove successful in the near future will probably involve some simplifying assumptions, shortcuts, or heuristics. While any inexact solution may fail for some cases, the advantage of this type of approach is that a solution may be found for many practical yet potentially difficult path planning problems with a reasonable amount of computation.

This thesis addressed the problem of planning feasible and obstacle-avoiding paths for two spatial robots working cooperatively in a known static environment. Because of the apparent impracticality of developing a general and complete path planning strategy, the main emphasis of this work involved developing a heuristic based path planner for cooperating robots which sacrifices completeness in exchange for a hope of finding a solution in a reasonable amount of time. The path planning approach presented in this thesis is configuration space (c-space) based and performs selective rather than exhaustive c-space mapping. A novel, divide-and-conquer type of heuristic is used to guide the selective mapping process. Also, a configuration space based algorithm was presented to modify any feasible path found by the planner into a more efficient one.
Although the path planner cannot guarantee finding a solution even if one exists, and in spite of its $O(k^{n-1})$ complexity for $n$ degree of freedom problems (where $k = 2$ or $3$ as implemented), it has demonstrated the ability to solve a variety of practical yet potentially difficult path planning problems with a reasonable amount of computation. This thesis presented the implementation details and illustrated sample results for the following four cases: single six dof (6R) robot, single nine dof (1P-8R) robot, cooperating six dof (6R) robots, and cooperating nine dof (1P-8R) robots. The path planning program typically requires under 10 minutes to execute for cooperating six dof robots and under 30 minutes to execute for cooperating nine dof robots. The planner appears to perform better than other cooperating robot path planners in the literature.

Some specific advantages and disadvantages of the path planning technique presented in this thesis are discussed below.

8.1.1 Advantages

1. The planner utilizes selective (non-exhaustive) mapping of c-space thus making it possible to get solutions in a reasonable amount of time.

2. The planner is global in nature but has provision for local navigation around obstacles.

3. The approach is completely general and would, in theory, be applicable to any system of arbitrary dimension. The approach is also independent of the type of geometric representation employed, so long as the chosen representation enables mapping of c-space points on an as-needed basis.

4. Unsafe space is handled in the same manner regardless of the reason for it being unsafe (such as various possible collisions or joint limit violations).
5. The approach could be applied to either single robot or cooperating robot path planning problems.

6. Robot degeneracy is not a concern for single arm problems and is inherently handled for the cooperating arm scenario (see Chapter 5).

7. While the resulting path is generally sub-optimal, it should be feasible to "tighten up" on any safe path to obtain a shorter one (Chapter 5.3).

8. The potential speed of the collision detection is enhanced by the fact that the method simply needs a yes or a no regarding collisions and does not require distance or direction information.

9. Cooperating redundant robot path planning problems may be handled without requiring use of inverse kinematics for a redundant robot.

10. The bulk of the calculations are such that they could be done in parallel (see Section 7.2).

11. Implementation of the path planner is relatively straightforward and easy.

8.1.2 Disadvantages

1. The planner is heuristic in nature and is not complete, i.e., it cannot guarantee finding a solution even if one may exist. Other approaches which are complete are computationally impractical for reasonably difficult yet practical problems for more than a few dof.

2. Joint angles at the start and goal configurations are required to be specified.

3. There is presently no means to determine that a solution exists other than to find one.
4. The number of strategy directions required to achieve an effective search increase exponentially with dimensionality. This effect may be partially offset by the fact that there may be more acceptable solutions to systems of higher dimensionality making it easier to find one of them.

5. The resulting path may be longer than necessary even after being shortened.

6. The planner cannot be directly applied to cases with dynamic obstacles.

8.2 Future Work

Some potential areas of future work include:

• Improvement to String Tightening Process

• Integration with the CIRSSE Geometric State Manager

• Utilization of Parallel Processing

• Guaranteeing Completeness

These areas of potential future work are discussed below.

8.2.1 Improvement to String Tightening Process

As discussed in Section 5.3.2.2, the string tightening algorithm presented herein has the disadvantage of yielding paths which very nearly involve collision. This issue could be addressed as part of future work by one of the following means:

• Expanding the obstacles so that paths with very little clearance in the model actually provide sufficient clearance. This is not a feasible option when the only safe path involves tight clearances.

• Modifying the cost function (Equation 5.5) to include a penalty for proximity to obstacles and considering knot point movement in any direction orthogonal to the segment between the preceding and following knot points.
• Implementing an alternate approach to string tightening, such as a potential fields approach similar to that discussed in Section 5.3.1. This is a very promising approach since the local minima problem can be effectively eliminated since the path planner provides the potential fields based path smoother with a feasible solution to the global path planning problem.

8.2.2 Integration with the CIRSSE Geometric State Manager

The path planner could be integrated with the CIRSSE Geometric State Manager (GSM) [102]. The purpose of the GSM is to maintain a time-varying geometric model of the CIRSSE robots and their environment. Once the path planner is integrated with the GSM, the planner could automatically obtain the current robot and obstacle information from the GSM when a testbed task determines the need to utilize the path planner.

8.2.3 Utilization of Parallel Processing

The path planning programs are currently implemented using serial coding. As such, the path planning program typically requires under 5 minutes to execute for cooperating six dof robots and under 30 minutes to execute for cooperating nine dof robots. The algorithm being used is ideally suited for parallel processing since each search involves a large number of independent calculations. Implementing the path planning program in parallel could drastically reduce the path planning program execution time.

8.2.4 Guaranteeing Completeness

As discussed earlier, a complete solution to the cooperating spatial robot path planning problem appear to be impractical at this time. Nonetheless, it might be possible to modify the c-space heuristic in such a way as to guarantee completeness.
At present, the usefulness of such an modification is at best questionable. However, advances in both the path planning and computer fields might warrant a second look at the completeness issue sometime in the future.

8.2.5 Decidability

At this time, there does not appear to be an easy answer to the question as to the existence of a solution to a given general path planning problem. Future research advances may make it possible to quickly determine whether or not a solution will exist.
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APPENDIX A
CIRSSE Testbed Kinematic Frames

This appendix describes the CIRSSE Testbed kinematic frames and the joint limits.

The first section describes how the coordinate frames are assigned and numbered. Section 2 defines the pose names. For reading ease, angular data presented in this appendix is given in units of degrees.

A.1 Coordinate Frames

This section describes the conventions related to the coordinate frame assignments for the 18-DOF Testbed. This section includes a set of standard labels for the coordinate frames and numbers for the joints. The joint ranges implied by the coordinate frame assignment are also given.

A.1.1 Assignment/Labeling of Frames

The consistent numbering of the joints in the Testbed results in a convention for referring to the joints by a standard set of labels. The designed convention specifies one uniform assignment of the coordinate frames, whereby each frame is associated with a single joint and each joint is associated with a single frame, (i.e., there are no redundant frames). Although the frame assignments and their association with the joints are unique, there are two different ways to number each frame/joint. This results in two different sets of frame/joint labels: one to account for an 18-DOF experiment, and one to account for a 9-DOF experiment.

The assignment of frame 0, i.e., the global origin, is made on top of the back platform rail in the middle of its length. The positive z-axis of this frame points towards the other platform rail, the positive y-axis points to the right of the Testbed, and the positive z-axis points towards the ceiling. Scribe marks will be placed on
the back rail to indicate this coordinate frame's origin, positive z-axis, and positive y-axis.

The coordinate frame numbering starts with the left cart, continues through the left PUMA, and then includes the right cart and right PUMA. The coordinate frames associated with the PUMA joints are ordered in the standard way. During an 18-DOF experiment, the frame/joint labels G1 through G18 are used sequentially in the manner just described (G indicates global). During a 6- or 9-DOF experiment, the frame/joint labels are L1 through L9, or R1 through R9, depending on whether the left or right PUMA+cart is used, respectively. Note, there is no reduced classification of the frame labels beyond those for a single PUMA+cart. Thus, a PUMA only experiment will use joints numbered L4 through L9 or R4 through R9. The following table summarizes the numbering and labeling of the coordinate frames, and gives the hardware joint limits for the PUMA (rounded to the nearest degree).
<table>
<thead>
<tr>
<th>frame number</th>
<th>name of associated axis</th>
<th>global label</th>
<th>local label</th>
<th>physical limit associated joint</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>n/a</td>
<td>G₀</td>
<td>L₀, R₀</td>
<td>n/a</td>
</tr>
<tr>
<td>1</td>
<td>left cart linear</td>
<td>G₁</td>
<td>L₁</td>
<td>(-1.3716, 0.6096) m</td>
</tr>
<tr>
<td>2</td>
<td>left cart rotate</td>
<td>G₂</td>
<td>L₂</td>
<td>(-150, 150) degs</td>
</tr>
<tr>
<td>3</td>
<td>left cart tilt</td>
<td>G₃</td>
<td>L₃</td>
<td>(-45, 45) degs</td>
</tr>
<tr>
<td>4</td>
<td>left PUMA shoulder</td>
<td>G₄</td>
<td>L₄</td>
<td>(-256, 79) degs</td>
</tr>
<tr>
<td>5</td>
<td>left PUMA upper-arm</td>
<td>G₅</td>
<td>L₅</td>
<td>(-221°, 40°) degs</td>
</tr>
<tr>
<td>6</td>
<td>left PUMA fore-arm</td>
<td>G₆</td>
<td>L₆</td>
<td>(-60, 246) degs</td>
</tr>
<tr>
<td>7</td>
<td>left PUMA wrist</td>
<td>G₇</td>
<td>L₇</td>
<td>(-126, 153°) degs</td>
</tr>
<tr>
<td>8</td>
<td>left PUMA flange tilt</td>
<td>G₈</td>
<td>L₈</td>
<td>(-100, 100) degs</td>
</tr>
<tr>
<td>9</td>
<td>left PUMA flange rotate</td>
<td>G₉</td>
<td>L₉</td>
<td>(-290°, 290°) degs</td>
</tr>
<tr>
<td>10</td>
<td>right cart linear</td>
<td>G₁₀</td>
<td>R₁</td>
<td>(-0.6096, 1.3716) m</td>
</tr>
<tr>
<td>11</td>
<td>right cart rotate</td>
<td>G₁₁</td>
<td>R₂</td>
<td>(-150, 150) degs</td>
</tr>
<tr>
<td>12</td>
<td>right cart tilt</td>
<td>G₁₂</td>
<td>R₃</td>
<td>(-45, 45) degs</td>
</tr>
<tr>
<td>13</td>
<td>right PUMA shoulder</td>
<td>G₁₃</td>
<td>R₄</td>
<td>(-253, 83) degs</td>
</tr>
<tr>
<td>14</td>
<td>right PUMA upper-arm</td>
<td>G₁₄</td>
<td>R₅</td>
<td>(-221°, 43°) degs</td>
</tr>
<tr>
<td>15</td>
<td>right PUMA fore-arm</td>
<td>G₁₅</td>
<td>R₆</td>
<td>(-60, 243) degs</td>
</tr>
<tr>
<td>16</td>
<td>right PUMA wrist</td>
<td>G₁₆</td>
<td>R₇</td>
<td>(-134, 153°) degs</td>
</tr>
<tr>
<td>17</td>
<td>right PUMA flange tilt</td>
<td>G₁₇</td>
<td>R₈</td>
<td>(-100, 100) degs</td>
</tr>
<tr>
<td>18</td>
<td>right PUMA flange rotate</td>
<td>G₁₈</td>
<td>R₉</td>
<td>(-290°, 290°) degs</td>
</tr>
</tbody>
</table>

The numbers marked with * indicate those limits which are not the mechanical limits of the joint but the encoder limits. In either case, a hardware limit has been reached. Beyond an encoder limit, the encoder count exceeds the storage capacity of a ‘C’ short, causing a sign change in the encoder value. This would have serious repercussions for any real-time control code.
The coordinate frame assignment follows a Modified Denavit-Hartenberg formulation, whereby the $i^{th}$ frame is attached to the $i^{th}$ link and has its origin on the $i^{th}$ joint axis, (ref., Craig, J. J., "Introduction to Robotics Mechanics and Control," Addison-Wesley, 1986, Chapter 3). Note that motion of a given joint throughout its entire range does not guarantee lack of collisions; this is particularly true with the linear joints of the carts.

Two figures attached to the end of this memorandum illustrate the coordinate frame assignment. Figure A.1 shows all 18 coordinate frames and joints for the carts and PUMAs. Figure A.2 shows a closer view of the coordinate frames for the left PUMA+cart.

The kinematic parameters for one of the PUMA+cart pairs are given in the following table. Entries preceded by an asterisk indicate the currently accepted approximate values which may change at a later date.

<table>
<thead>
<tr>
<th>frame number, $i$</th>
<th>$\alpha_{i-1}$</th>
<th>$a_{i-1}$ (m)</th>
<th>$d_i$ (m)</th>
<th>$\theta_i$</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>$-90^\circ$</td>
<td>*0.32000</td>
<td></td>
<td>$q_1$</td>
</tr>
<tr>
<td>2</td>
<td>$90^\circ$</td>
<td>0.00000</td>
<td>*0.54400</td>
<td>$q_2$</td>
</tr>
<tr>
<td>3</td>
<td>$-90^\circ$</td>
<td>0.00000</td>
<td>0.00000</td>
<td>$q_3$</td>
</tr>
<tr>
<td>4</td>
<td>$90^\circ$</td>
<td>0.00000</td>
<td>*0.82800</td>
<td>$q_4$</td>
</tr>
<tr>
<td>5</td>
<td>$-90^\circ$</td>
<td>0.00000</td>
<td>0.24300</td>
<td>$q_5$</td>
</tr>
<tr>
<td>6</td>
<td>$0^\circ$</td>
<td>0.43182</td>
<td>-0.09391</td>
<td>$q_6$</td>
</tr>
<tr>
<td>7</td>
<td>$90^\circ$</td>
<td>-0.02031</td>
<td>0.43300</td>
<td>$q_7$</td>
</tr>
<tr>
<td>8</td>
<td>$-90^\circ$</td>
<td>0.00000</td>
<td>0.00000</td>
<td>$q_8$</td>
</tr>
<tr>
<td>9</td>
<td>$90^\circ$</td>
<td>0.00000</td>
<td>0.00000</td>
<td>$q_9$</td>
</tr>
</tbody>
</table>

Note that frames 7, 8, and 9 have co-located origins. Specifically, the last frame is not located at the flange of the PUMA's wrist. Numerical detail for the
transformation from frame 9 to the gripper frame have not as yet been determined. HOME positions have been defined for the MCS for the PUMAs. This position corresponds to all zero joint values, and is shown in Figures A.1 and A.2. This position, because of the alignment of two the wrist joint axes, is singular.

A.2 Software Joint Limits for the PUMAs

While the hardware joint limits describe the range of motion physically permitted, it is not possible to utilize this entire range. For example, path planners may require additional restrictions to provide safe motion. The following table lists the recommended joint limits for the testbed. These values are based on the hardware joint limits with consideration given to the link size and range, and a safety region (nominally 5 degrees, except it is 6 degrees for a joint able to reach its encoder limit).
<table>
<thead>
<tr>
<th>frame number</th>
<th>name of associated axis</th>
<th>global label</th>
<th>local label</th>
<th>software range of associated joint</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>n/a</td>
<td>G₀</td>
<td>L₀, R₀</td>
<td>n/a</td>
</tr>
<tr>
<td>1</td>
<td>left cart linear</td>
<td>G₁</td>
<td>L₁</td>
<td>(-1.3716, 0.6096) m</td>
</tr>
<tr>
<td>2</td>
<td>left cart rotate</td>
<td>G₂</td>
<td>L₂</td>
<td>(-150, 150) degs</td>
</tr>
<tr>
<td>3</td>
<td>left cart tilt</td>
<td>G₃</td>
<td>L₃</td>
<td>(-45, 45) degs</td>
</tr>
<tr>
<td>4</td>
<td>left PUMA shoulder</td>
<td>G₄</td>
<td>L₄</td>
<td>(-251, 74) degs</td>
</tr>
<tr>
<td>5</td>
<td>left PUMA upper-arm</td>
<td>G₅</td>
<td>L₅</td>
<td>(-215, 34) degs</td>
</tr>
<tr>
<td>6</td>
<td>left PUMA fore-arm</td>
<td>G₆</td>
<td>L₆</td>
<td>(-55, 241) degs</td>
</tr>
<tr>
<td>7</td>
<td>left PUMA wrist</td>
<td>G₇</td>
<td>L₇</td>
<td>(-121, 144) degs</td>
</tr>
<tr>
<td>8</td>
<td>left PUMA flange tilt</td>
<td>G₈</td>
<td>L₈</td>
<td>(-95, 95) degs</td>
</tr>
<tr>
<td>9</td>
<td>left PUMA flange rotate</td>
<td>G₉</td>
<td>L₉</td>
<td>(-284, 284) degs</td>
</tr>
<tr>
<td>10</td>
<td>right cart linear</td>
<td>G₁₀</td>
<td>R₁</td>
<td>(-0.6096, 1.3716) m</td>
</tr>
<tr>
<td>11</td>
<td>right cart rotate</td>
<td>G₁₁</td>
<td>R₂</td>
<td>(-150, 150) degs</td>
</tr>
<tr>
<td>12</td>
<td>right cart tilt</td>
<td>G₁₂</td>
<td>R₃</td>
<td>(-45, 45) degs</td>
</tr>
<tr>
<td>13</td>
<td>right PUMA shoulder</td>
<td>G₁₃</td>
<td>R₄</td>
<td>(-248, 78) degs</td>
</tr>
<tr>
<td>14</td>
<td>right PUMA upper-arm</td>
<td>G₁₄</td>
<td>R₅</td>
<td>(-215, 37) degs</td>
</tr>
<tr>
<td>15</td>
<td>right PUMA fore-arm</td>
<td>G₁₅</td>
<td>R₆</td>
<td>(-55, 238) degs</td>
</tr>
<tr>
<td>16</td>
<td>right PUMA wrist</td>
<td>G₁₆</td>
<td>R₇</td>
<td>(-129, 148) degs</td>
</tr>
<tr>
<td>17</td>
<td>right PUMA flange tilt</td>
<td>G₁₇</td>
<td>R₈</td>
<td>(-95, 95) degs</td>
</tr>
<tr>
<td>18</td>
<td>right PUMA flange rotate</td>
<td>G₁₈</td>
<td>R₉</td>
<td>(-284, 284) degs</td>
</tr>
</tbody>
</table>

The information in the joint limit tables should be used in the following manner:

- Trajectory generators, controllers, path planners, etc., should use the software joint limits for specifying the manipulator motion ranges.
- The low level protection code in the robot channel drivers should use hardware joint limits.

This usage permits a consistent specification of manipulator motions and provides two levels of protection against reaching the joint limits: the channel drivers will disable a joint only when the physical limit is threatened; higher level software will never request a joint move to these limits. It is expected that the channel drivers will also include a 3 degree limit on these values to ensure safety.

A.3 Pose Names

In general, three pose variables, each with two values, are needed to select the desired solution from the eight possible solutions of a PUMA inverse kinematic problem. Selection of the pose definitions was a trade-off between easy visualization of the pose by human analogy and ease of computation. The labels to be used for the PUMA poses and their definitions are summarized in the table below—joint variables referenced are those for the left PUMA.

<table>
<thead>
<tr>
<th>pose name</th>
<th>joint range</th>
</tr>
</thead>
<tbody>
<tr>
<td>right</td>
<td>( f_{\text{thres}}(q_4, q_5, q_6) &lt; 0 )</td>
</tr>
<tr>
<td>left</td>
<td>( f_{\text{thres}}(q_4, q_5, q_6) &gt; 0 )</td>
</tr>
<tr>
<td>flex</td>
<td>( q_6 &lt; 92.6864^\circ )</td>
</tr>
<tr>
<td>noflex</td>
<td>( q_6 &gt; 92.6864^\circ )</td>
</tr>
<tr>
<td>flip</td>
<td>( q_8 &lt; 0^\circ )</td>
</tr>
<tr>
<td>noflip</td>
<td>( q_8 &gt; 0^\circ )</td>
</tr>
</tbody>
</table>

Standing on the PUMA base and looking straight at its wrist, the shoulder link of the PUMA will be on either the left or right side of your body, corresponding to the left or right configuration, respectively. It is important to only consider the
location of the PUMA's wrist coordinate frame, and not the flange of its last joint or any tool that might be attached to the wrist. The computation involves joints 4, 5, and 6. The PUMA is in the left configuration when it is in the HOME position, (as shown in Figures A.1 and A.2). With the other PUMA joints remaining stationary, this configuration variable changes when either \( q_5 \) or \( q_6 \) move to cause the wrist to pass over the "head" of the PUMA. When the wrist is directly above the PUMA, the robot is neither in the left or right configuration.

Consider, now, that the PUMA is in the left configuration. When the value of the elbow angle, i.e., \( q_6 \), is 92.6864°, the fore-arm and upper-arm align to make the PUMA stretched. In this position, the PUMA is neither in the flex or noflex configuration. As the fore-arm is drawn towards the top of the upper-arm by changing the elbow angle, i.e., the motion achievable with the unbroken human arm, the PUMA enters the flex configuration (so named since this motion mimics a human flexing his/her arm). Conversely, the PUMA is in the noflex configuration if the elbow angle is changed in the other direction. This analogy is reversed when the PUMA is in the right configuration. In this case, the orientation of the fore-arm and upper-arm unlikely for humans is the flex configuration.

The last pose label deals with the PUMA's wrist orientation. Because of the construction of the PUMA wrist, there is no human analogy to this redundancy. A piece of tape will be placed on the PUMA's wrist near the axis of \( q_8 \). When \( q_8 \) is such that the flange of the PUMA's wrist overlaps the tape, then the PUMA will be in the no flip configuration.
Figure A.1: Coordinate Frame Assignments
Figure A.2: Left Half Coordinate Frame Assignments
APPENDIX B
Data for Examples Presented in Thesis

This Appendix provides the task and obstacle descriptions for the examples presented earlier in Chapter 6. The task description has the form of start and goal joint angles. Revolute joints are measured in degrees and prismatic joints are measured in mm. The obstacle descriptions have the following format with dimensions in mm:

/ obstacle no. / number of points / polytope radius / origin of reference frame (X,Y,Z) / (X,Y,Z) of first point / ⋯ / (X,Y,Z) of last point /

Solution times and other solution parameters were presented earlier in Chapter 6.

The point coordinates are in local coordinates. The obstacle reference frames have the same orientation as the world reference frame. The world reference frame and the robot joint angle definitions are defined in [101].

B.1 Data for Examples 1 and 2

Examples 1 and 2 are identical except that the lower three joints remain fixed for Example 1 but are allowed to move for Example 2. The start and goal joint angles for these examples are:

\[ \Theta_0 = (0, 0, 0, 16.03, -148.79, -8.35, 0.00, -22.86, 106.03) \] and

\[ \Theta_f = (0, 0, 0, -184.37, -158.90, 20.22, 0.00, -41.32, 265.63), \] respectively. The eight obstacles are as follows:

/ 1 / 2 / 40 / (1000,-100,800) / (200,0,0) / (-200,0,0) /

/ 2 / 2 / 40 / (1000, -100, 800) / (200, 0, 0) / (0, 0, 346) /
B.2 Data for Example 3

For this example, platform 1 is fixed at (-900, -90, 0) and platform 2 is fixed at (900, -90, 0). The start robot 1 and 2 joint angles for this example are:

\( \Theta_1^0 = (64.40, -178.80, 121.20, 0.00, 57.60, 115.60) \) and

\( \Theta_2^0 = (-226.97, -185.55, 136.58, 0.00, 48.98, 226.97) \), respectively. The goal joint angles for this example are:

\( \Theta_1^f = (-42.00, -169.46, 115.96, 0.00, 53.40, 222.00) \) and

\( \Theta_2^f = (-111.92, -176.85, 133.07, -0.14, 43.75, 112.02) \), respectively. The six obstacles are as follows:

/ 3 / 2 / 40 / (1000, -100, 800) / (-200, 0, 0) / (0, 0, 346) / 
/ 4 / 8 / 0 / (500, 600, 1250) / (100, 100, 0) / (-100, 100, 0) / (-100, -100, 0) / 
(100, -100, 0) / (100, 100, 200) / (-100, 100, 200) / (-100, -100, 200) / 
(100, -100, 200) / 
/ 5 / 8 / 0 / (-200, 200, 1000) / (-100, -100, 0) / (-100, 100, 0) / (100, 100, 0) / 
(100, -100, 0) / (-100, -100, 100) / (-100, 100, 100) / (100, 100, 100) / 
(100, -100, 100) / 
/ 6 / 8 / 0 / (-350, 200, 800) / (-50, -100, 0) / (-50, 100, 0) / (50, 100, 0) / 
(50, -100, 0) / (-50, -100, 300) / (-50, 100, 300) / (50, 100, 300) / (50, -100, 300) / 
/ 7 / 8 / 0 / (-50, 200, 800) / (-50, -100, 0) / (-50, 100, 0) / (50, 100, 0) / 
(50, -100, 0) / (-50, -100, 300) / (-50, 100, 300) / (50, 100, 300) / (50, -100, 300) / 
/ 8 / 8 / 0 / (-200, 200, 800) / (-100, -100, 0) / (-100, 100, 0) / (100, 100, 0) / 
(100, -100, 0) / (-100, -100, 100) / (-100, 100, 100) / (100, 100, 100) / 
(100, -100, 100) /
B.3 Data for Example 4

The start robot 1 and 2 joint angles for this example are:

$\Theta_{1} = (-1300.00, 0.00, -40.00, -5.00, -110.70, 19.20, 4.30, -48.80, 83.40)$ and

$\Theta_{2} = (-500.00, 0.00, -40.00, -184.92, -72.57, 170.91, 4.76, 41.97, 82.36)$, respectively. The goal joint angles for this example are:

$\Theta_{1f} = (500.00, 0.00, 40.00, -149.81, -163.61, 46.29, 23.80, 72.91, 242.14)$ and

$\Theta_{2f} = (1300.00, 0.00, 40.00, -171.09, -157.32, 33.29, 7.09, 74.44, 82.36)$, respectively.

The eight obstacles are as follows:

/ 2 / 8 / 0 / (500, 0, 2000) / (375, 150, 0) / (375, -150, 0) / (-375, -150, 0) / (-375, 150, 0) / (375, 150, 100) / (375, -150, 100) / (-375, -150, 100) / (-375, 150, 100) / 3 / 8 / 0 / (180, 0, 2100) / (50, 150, 0) / (50, -150, 0) / (-50, -150, 0) / (-50, 150, 0) / (50, 150, 300) / (50, -150, 300) / (-50, -150, 300) / (-50, 150, 300) / 4 / 8 / 0 / (180, 0, 1450) / (50, 150, 0) / (50, -150, 0) / (-50, -150, 0) / (-50, 150, 0) / (50, 150, 300) / (50, -150, 300) / (-50, -150, 300) / (-50, 150, 300) / 5 / 8 / 0 / (825, 0, 1850) / (50, 150, 0) / (50, -150, 0) / (-50, -150, 0) / (-50, 150, 0) / (50, 150, 150) / (50, -150, 150) / (-50, -150, 150) / (-50, 150, 150) / 6 / 8 / 0 / (-175, 0, 1750) / (50, 150, 0) / (50, -150, 0) / (-50, -150, 0) / (-50, 150, 0) / (50, 150, 250) / (50, -150, 250) / (-50, -150, 250) / (-50, 150, 250) /
```
/ 4 / 8 / 0 / (-875, -1350, 700) / (-100, -50, 0) / (-100, 50, 0) / (100, 50, 0) /
(100, -50, 0) / (-100, -50, 300) / (-100, 50, 300) / (100, 50, 300) / (100, -50, 300) /
/ 5 / 8 / 0 / (-875, -850, 600) / (-175, -550, 0) / (-175, 550, 0) / (175, 550, 0) /
(175, -550, 0) / (-175, -550, 100) / (-175, 550, 100) / (175, 550, 100) /
(175, -550, 100) /
/ 6 / 2 / 100 / (1450, 1000, 0) / (0, 0, 0) / (0, 0, 650) /
/ 7 / 8 / 0 / (1550, 100, 750) / (-200, -100, 0) / (-200, 100, 0) / (200, 100, 0) /
(200, -100, 0) / (-200, -100, 100) / (-200, 100, 100) / (200, 100, 100) /
(200, -100, 100) /
/ 8 / 8/ 0 / (1800, 1000, 550) / (-100, -50, 0) / (-100, 50, 0) / (100, 50, 0) /
(100, -50, 0) / (-100, -50, 300) / (-100, 50, 300) / (100, 50, 300) / (100, -50, 300) /
```