NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

TECHNICAL NOTE

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WIND-TUNNEL INVESTIGATION OF THE EFFECT OF TAB BALANCE ON TAB AND CONTROL-SURFACE CHARACTERISTICS

By Jack D. Brewer and M. J. Queijo

Langley Memorial Aeronautical Laboratory
Langley Field, Va.

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WIND-TUNNEL INVESTIGATION OF THE EFFECT OF TAB BALANCE ON
TAB AND CONTROL-SURFACE CHARACTERISTICS

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SUMMARY

An investigation was conducted to furnish data on the effect
of tab balance on tab and control-surface characteristics. The
airfoil tested had a modified NACA 65-012 contour with a plain
flap having a chord equal to 25 percent of the wing chord and with
a tab having a chord equal to 25 percent of the flap chord and
having several nose shapes and overhang lengths.

The results of the investigation indicated that, in general,
tab balance affected tab hinge-moment characteristics in much the
same manner that flap balance affects flap hinge-moment character-
istics. A moderate amount of tab balance did not seem to have any
adverse effect on flap hinge-moment characteristics. Transition
strips placed near the leading edge of an airfoil reduced the effec-
tiveness of either plain or balanced tabs. Opening the tab gap
reduced the tab effectiveness, but the reduction became less as the
tab balance was increased.

Application (by an approximate method) of the results to two
typical airplanes indicated that the addition of overhang balance
to spring tabs was an effective means of reducing the control forces
of spring-tab ailerons. Tabs with sealed internal balances were
generally less effective in reducing aileron control forces than
tabs with round-nose overhangs of the same balance length.

INTRODUCTION

Some means of balancing the excessive aerodynamic forces on the
control surfaces have been found necessary in the designs of large
airplanes and high-speed airplanes. Results of tests reported in
references 1 to 3 show spring tabs to be one of the most effective
means of obtaining aerodynamic balance. In some cases, however, the
control forces become quite large even with a spring-tab arrangement.
A spring-tab analysis presented by Gates of Great Britain indicates
that a large part of the control forces for spring-tab ailerons may
result from tab hinge moments. Some data (references 4 and 5) are available on plain-tab hinge moments but little, on balanced-tab hinge moments. The present tests were conducted in the 2 1/2- by 6-foot test section of the Langley stability tunnel to provide such tab data in order to investigate the practicability of using tab balance to reduce control forces. The effects of transition strips and tab gap on hinge-moment characteristics were also investigated.

**SYMBOLS**

- $c_l$: airfoil section lift coefficient
- $c_{hf}$: flap (or aileron) section hinge-moment coefficient
- $c_{ht}$: tab section hinge-moment coefficient
- $P_{Rf}$: resultant flap (or aileron) balance-pressure coefficient $(P_{f,Lower} - P_{f,Upper})$
- $P_{Rt}$: resultant tab balance-pressure coefficient $(P_{t,Lower} - P_{t,Upper})$
- $P_f$: pressure coefficient above or below flap (or aileron) seal
- $P_t$: pressure coefficient above or below tab seal
- $c$: chord of basic airfoil with flap and tab neutral, feet
- $c_f$: flap (or aileron) chord from flap (or aileron) hinge line to trailing edge with tab neutral, feet
- $c_t$: tab chord from tab hinge line to trailing edge, feet
- $c_{bf}$: flap (or aileron) balance chord, distance from hinge line to a point midway between points of attachment of flexible seal of sealed internal balance, feet
- $c_{bt}$: tab balance chord; distance from tab hinge line to leading edge of exposed overhang balance or to a point midway between points of attachment of flexible seal of sealed internal balance, feet
- $y_i$: distance from plane of symmetry to inboard end of aileron, feet
\( v_0 \)  
\( \delta_f \)  
\( \Delta \delta_f \)  
\( \delta_t \)  
\( \alpha \)  
\( \phi \)  
\( F \)  
\( k_1 \)  
\( k_2 \)  
\( k_3 \)  
\( F_{1,2} \)  
\( V \)  
\( \Delta \chi_{t \alpha} \)  
\( \Delta \chi_{t \delta t} \)  
\( c_{l \alpha} \)  
\( c_{l \delta f} \)  
\( c_{l \delta t} \)  
\( c_{h f \alpha} \)  

distance from plane of symmetry to outboard end of aileron, feet  
flap (or aileron) deflection with respect to airfoil, degrees  
total deflection of right and left flaps (or ailerons), degrees  
tab deflection with respect to flap, degrees  
angle of attack, degrees  
trailing-edge angle, degrees  
control force, pounds  
ratio between angular deflection of control (stick or wheel) and aileron deflection with spring tab fixed  
ratio between angular deflection of control (stick or wheel) and tab deflection with aileron fixed  
spring constant, ratio of control (stick or wheel) force to spring-tab deflection when aileron is held fixed and airspeed is zero, pounds per degree  
correlation factors defined on page 41 of reference 9  
indicated airspeed, miles per hour  

\[ \Delta \chi_{t \alpha} = \chi_{t \alpha \text{Balanced tab}} - \chi_{t \alpha \text{Plain tab}} \]
\[ \Delta \chi_{t \delta t} = \chi_{t \delta t \text{Balanced tab}} - \chi_{t \delta t \text{Plain tab}} \]
\[ c_{l \alpha} = \left( \frac{\partial c_l}{\partial \alpha} \right)_{\delta_f, \delta_t} \]
\[ c_{l \delta f} = \left( \frac{\partial c_l}{\partial \delta_f} \right)_{\alpha, \delta_t} \]
\[ c_{l \delta t} = \left( \frac{\partial c_l}{\partial \delta_t} \right)_{\alpha, \delta_f} \]
\[ c_{h f \alpha} = \left( \frac{\partial c_{hf}}{\partial \alpha} \right)_{\delta_f, \delta_t} \]
\[ c_n f_{\delta f} = \left( \frac{\partial c_n f}{\partial \delta f} \right)_{\alpha, \beta t} \]
\[ c_n f_{\delta t} = \left( \frac{\partial c_n f}{\partial \delta t} \right)_{\alpha, \beta f} \]
\[ c_n t_{\delta t} = \left( \frac{\partial c_n t}{\partial \alpha} \right)_{\delta t, \delta f} \]
\[ c_n t_{\delta f} = \left( \frac{\partial c_n t}{\partial \delta f} \right)_{\alpha, \delta t} \]
\[ c_n t_{\delta t} = \left( \frac{\partial c_n t}{\partial \delta t} \right)_{\alpha, \beta f} \]
\[ P_{R f, \delta t} = \left( \frac{\partial P_{R f}}{\partial \delta t} \right)_{\alpha, \delta t} \]
\[ P_{R f, \delta f} = \left( \frac{\partial P_{R f}}{\partial \delta f} \right)_{\alpha, \beta t} \]
\[ P_{R f, \beta t} = \left( \frac{\partial P_{R f}}{\partial \beta t} \right)_{\alpha, \beta f} \]
\[ P_{R t, \delta t} = \left( \frac{\partial P_{R t}}{\partial \delta t} \right)_{\alpha, \beta f} \]
\[ P_{R t, \delta f} = \left( \frac{\partial P_{R t}}{\partial \delta f} \right)_{\alpha, \beta t} \]
\[ P_{R t, \beta t} = \left( \frac{\partial P_{R t}}{\partial \beta t} \right)_{\alpha, \beta f} \]
The subscripts outside the parentheses of the foregoing partial derivatives indicate factors held constant during measurement of the derivatives.

APPARATUS AND TESTS

The tests of the present investigation were conducted in the 2 1/2-by 6-foot test section of the Langley stability tunnel. The model had an airfoil chord of 2 feet and spanned the throat of the tunnel. Photographs of the model in the tunnel are presented in figure 2. The part of the model forward of the 75-percent-chord station was made of laminated mahogany and had an NACA 651-012 contour, but from the 75-percent-chord station to the trailing edge the wing had flat sides forming a trailing-edge angle of 13.5°. The ordinates of the modified airfoil are given in table I.

The model had a plain flap constructed of laminated mahogany with a steel central web to which a steel tab was attached; the flap chord was 25 percent of the airfoil chord. The tab had a chord equal to 25 percent of the flap chord and was equipped with several brass nose pieces of various shapes and overhang lengths. The dimensions of the flap and tab are shown in figure 1. The ordinates of the tab nose shapes are given in table II.

The part of the model forward of the 75-percent-chord station was attached rigidly to disks that were mounted flush with the tunnel walls. Clearance gaps of approximately 1/16 inch were left between the disks and the ends of the control surfaces.

The lift on the model was measured with an integrating manometer; flap hinge moments were measured with a calibrated spring balance; tab hinge moments were measured by calibrated electric strain gages; and the pressure differences (resultant balance pressures) were measured by U-tube manometers.

All of the tests were made at a dynamic pressure of 155.5 pounds per square foot. The corresponding Reynolds number and Mach number are $4.59 \times 10^6$ and 0.34, respectively.

The greater part of the tests were made with transition strips attached to the upper and lower surfaces of the model. The transition strips were made by cementing No. 60 carborundum grains to Scotch cellulose tape in a strip 1/4 inch wide. The tape was attached to the model so that the leading edges of the carborundum strips were at the 1.0-percent-chord station.
Tests were made with the tab gap sealed and open for the round tab nose shapes (gap = 0.004c). The tab gap was open for all other tests. The flap gap was sealed for all tests.

CORRECTIONS

Corrections applied to the test data for the effect of jet boundaries are based on the equations of reference 6. The methods of reference 6 were extended in order to obtain the corrections to flap hinge-moment coefficient and resultant balance-pressure coefficient. The equations used in making the corrections were:

\[ c_l = 0.963c_l' \]

\[ \alpha = \alpha' + 0.231c_l \left( \delta_f = 0^\circ, \delta_t = 0^\circ \right) \]

\[ c_h_f = c_h_f' + 0.0087c_l' \]

\[ P_{R_f} = P_{R_f}' - 0.042c_l' \]

Primed values refer to the uncorrected value.

The corrections do not take into account the tunnel-wall boundary-layer effects or the effects of the gaps between the ends of the control surfaces and the end disks. The angle-of-attack correction does not take into account the small effect of lift resulting from tab and flap deflections. The corrections for \( c_h_t \) and for \( P_{R_t} \) were found to be very small and were neglected.

RESULTS AND DISCUSSION

Presentation of Data

The data are presented as plots of airfoil section lift coefficient, flap section hinge-moment coefficient, tab section hinge-moment coefficient, and the resultant flap balance-pressure coefficient as functions of flap deflection, for all model configurations tested, in figures 3 to 19. The resultant tab balance-pressure coefficient is presented for the plain tab only in figure 3(d). The same coefficients are plotted against angle of attack.
in figures 20 to 27 (for $\delta_f = 0^\circ$ and $\delta_t = 0^\circ$). Parameter values obtained from these figures are presented in table III. The effects of tab nose shape and tab overhang length on the tab hinge-moment parameters are shown in figures 28 and 29. Figure 30 shows the effect of tab balance on flap section hinge-moment coefficient. The effects of fixing transition and of sealing the tab gap on tab hinge-moment parameters are indicated in figure 31.

**Effects of Tab Nose Shape and Overhang**

In figure 28 the parameters $c_{ht\alpha}$, $c_{ht\delta_f}$, and $c_{ht\delta_t}$ become more positive as the nose shape is changed from sharp to blunt or as the tab overhang is increased. In general, the parameters are affected by tab balance in the manner that should be expected on the basis of previously obtained test results for the effects of flap balance on flap hinge-moment characteristics (references 4, 7, and 8). Neither tab overhang nor tab nose shape generally has any appreciable effect on the parameters $c_{hf\delta_f}$ or $c_{hf\delta_t}$. The tab hinge-moment effectiveness increases as the tab nose shape is changed from sharp to blunt. Increasing the tab overhang length causes the tab to become more effective with the blunt and round nose shapes but causes irregular results for the tab with the elliptical and sharp nose shapes.

A correlation of the effects of overhang balances for ailerons is expressed (equations (23) and (24) of reference 9) in terms of a factor $F_1$ related to overhang length and a factor $F_2$ related to balance nose shape. The relations of these factors to the geometry of the balance are given in reference 9. The correlation has been applied to the tab balances of the present investigation and the results are compared with the experimental values of the parameters $c_{ht\alpha}$ and $c_{ht\delta_t}$. The comparison given in figure 29 shows that application of the correlation, in its present form, to tabs results in overestimating the effects of the balances on tab hinge moments. The poor agreement between the present experimental results and the correlation probably is caused by the large difference between the tab-chord ratio ($c_t = 0.06c$) of the present tests and the aileron-chord-length ratio range ($c_f = 0.155c$ to $0.30c$) used in developing the correlation. Symbols representing different nose shapes for constant overhang lengths and symbols representing different overhang lengths for constant nose shapes fall close, however, to the same line. This agreement indicates that the relative importance of nose shape and overhang length is given accurately by the present correlation. Therefore, the correlation given in reference 9 can possibly be made to
apply to almost any control surface or tab if factors related to the chord ratio were used in addition to the factors $F_1$ and $F_2'$. 

Figure 30, a plot of flap section hinge-moment coefficient against flap deflection for various ratios of tab deflection to flap deflection shows that the presence of a round-tab balance of $0.50c_t$ length does not greatly alter the effect of the tab on the flap hinge moments. Because a rather extreme tab balance was used for this comparison, tab balance, apparently, is not likely to have any serious adverse effects on flap hinge-moment characteristics for practical installations.

Effects of Transition Strips and Tab Gap

The effects of fixing transition and of sealing the tab gap on hinge-moment parameters are shown in Figure 31. Placing transition strips at the 0.01 ft station causes all the hinge-moment parameters except $c_{ht\alpha}$ to become less negative than they were for the condition of transition strips off; $c_{ht\alpha}$ becomes less positive.

Opening the tab gap causes $c_{hf\alpha}$ and $c_{ht\alpha}$ to become less negative but generally has little effect on $c_{ht\alpha}$, $c_{ht\alpha}$, and $c_{ht\alpha}$. The tab-effectiveness parameter $c_{ht\alpha}$ becomes less negative when the tab gap is unsealed, but the change is much less for a balanced tab than for a plain tab.

Application of Data to Two

Typical Airplanes

In order to illustrate the effects of tab nose shape and tab overhang length on aileron control forces, the hinge-moment data obtained in the present investigation were applied to two typical airplanes having the characteristics listed in table IV. Airplane 1 is a typical fighter-type airplane and airplane 2 is a typical large (transport or heavy bomber) airplane. The ailerons were assumed to be equipped with spring tabs having various spring strengths.

The control force per degree aileron deflection was estimated for each of the tab-nose configurations and for several assumed aileron balances at an assumed indicated airspeed of 300 miles per hour.
The procedure used for estimating the aileron control forces is necessarily approximate since the calculations are based on two-dimensional data. Reliable aspect-ratio corrections for the hinge-moment parameters of partial-span control surfaces or for tabs have not been developed. A qualitative indication of the effects of tab nose shape and tab overhang length on control forces is believed, however, to be obtainable by neglecting all aspect-ratio corrections to the hinge-moment parameters. A correction must be applied to the airfoil section tab-effectiveness parameter $c_{Flt}$, however, when the tab span is less than the aileron span. The tab correlation given in reference 9 was used to evaluate this correction. On the basis of this assumption, calculations of the control force per degree aileron deflection have been made by means of equation (40) of reference 9. Because of the limitations of the method that have been pointed out, the absolute values of the control force per degree aileron deflection are not considered to be of much significance, but the trends indicated by variation in the tab configuration are believed to be reliable. The hinge-moment parameters of ailerons or tabs with sealed internal balances were calculated by methods described in reference 10 by use of the hinge-moment parameters of plain sealed ailerons and tabs and the resultant balance-pressure parameters. The results of the calculations are presented in figures 32 and 33 as plots of control force per degree aileron deflection against tab overhang length for the nose shapes tested and for several assumed values of aileron balance and spring strength. Figure 32 presents the results obtained for airplane 1 and figure 33 presents the results obtained for airplane 2.

In general, increasing the tab overhang length or the bluntness of the tab nose shape decreases the control force. The results presented in figures 32 and 33 have been summarized in figure 34, which shows the ratio of control force with a balanced tab to control force with a plain tab plotted against spring constant for various values of aileron balance. Figure 34 shows that the effectiveness of the tab balance in reducing control force is practically independent of aileron balance and that the effectiveness decreases as the value of $k_3$ increases. The greatest percent of reduction occurs for the servotab ($k_3 = 0$).

Calculations were made of the control forces for several assumed sealed internal balances on the tab by using the plain tab data and the tab balance pressures. The results are plotted in figure 35. Control-force curves obtained from figures 32 and 33 for the tabs with round-nose overhangs are included in figure 35 for comparison. In general, the control forces for a sealed internally balanced tab with a plain nose are greater than for a tab with a round nose overhang of the same balance length.
Figure 36 shows the variation of control force per degree aileron deflection with airspeed for various aileron and spring-tab balance conditions and indicates the great reduction in control force possible with balanced spring tabs throughout the speed range.

All of the foregoing control-force results were calculated by the comparatively simple method given in reference 9, which assumes linear variations of aileron and tab hinge-moment coefficients with aileron deflection, spring-tab deflection, and angle of attack. A more difficult, but more accurate, method considering the actual nonlinear aileron and tab curves is given in reference 11. In order to check the validity of the control-force results obtained by the linear method, a plot showing the effect of tab balance on the variation of control force with aileron deflection is presented in figure 37, as determined by references 9 and 11. Although differences in the two sets of results exist, especially at large aileron deflections, figure 37 shows that the trends indicated by the results obtained from the linear method are reliable.

CONCLUSIONS

An investigation was conducted in the 2 1/2-foot test section of the Langley stability tunnel of a two-dimensional wing model having a modified NACA 651-012 contour with a plain flap having a chord equal to 25 percent of the wing chord and with a tab having several nose shapes and overhang lengths and having a chord equal to 25 percent of the flap chord. The results of the investigation and the application (by an approximate method) of the results to aileron control forces indicated the following conclusions:

1. In general, tab hinge-moment characteristics were affected by tab balance in much the same way that flap hinge-moment characteristics are affected by flap balance.

2. A moderate amount of tab balance would have no adverse effect on flap hinge-moment characteristics.

3. The tab effectiveness decreased when transition strips were placed near the leading edge of the airfoil. Opening the tab gap reduced the tab effectiveness, but the reduction decreased as the tab balance increased.

4. The addition of overhang balance to spring tabs was an effective means of reducing the control forces of spring-tab ailerons.
5. Tabs with sealed internal balances were generally less effective in reducing aileron control forces than tabs with round-nose overhang of the same balance length.

Langley Memorial Aeronautical Laboratory
National Advisory Committee for Aeronautics
Langley Field, Va., June 10, 1947
REFERENCES


### Table I

Ordinates for Modified NACA 651–012 Airfoil

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## TABLE II

ORDINATES OF TAB NOSE SHAPES

[Station and ordinates in percent airfoil chord; stations measured from forward end of overhang]

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<thead>
<tr>
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### TABLE III

PARAMETER VALUES FOR MODIFIED NACA 651-012 AIRFOIL WITH 0.25c FLAP AND VARIOUS 0.25c\(t\) TABS

<table>
<thead>
<tr>
<th>(c_{bt}/c_t)</th>
<th>Balance nose shape</th>
<th>Tab shape</th>
<th>Transition strips</th>
<th>(c_{ta})</th>
<th>(c_{15f})</th>
<th>(c_{16f})</th>
<th>(c_{16f})</th>
<th>(c_{15t})</th>
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<th>(P_{Rfa})</th>
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*Data not presented.*

NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS
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Figure 1. - Dimensions of flap and tab with various nose shapes tested on modified NACA 65-012 airfoil.
(a) Rear view. $\alpha = 10^\circ$; $\delta_f = 15^\circ$; $\delta_t = 20^\circ$.

Figure 2. - View of balanced tab model in $2\frac{1}{2}$- by 6-foot section of Langley stability tunnel.
(b) Front view. $\alpha = -10^\circ$; $\delta_f = -15^\circ$; $\delta_t = 20^\circ$.

Figure 2.- Concluded.
Figure 3 - Section aerodynamic characteristics of modified NACA 65-012 airfoil with 0.25c flap and 0.25c tab.
Tab nose shape, plain; tab gap, sealed; transition strips at 0.01c.
(d) Variation of $Pr_f$ with $\delta_f$.

Figure 3.- Concluded.
Fig. 4. Section aerodynamic characteristics of modified NACA 65-125 airfoil with 0.255 flap and 0.255 stagger.
Fig. 5b

Flap section hinge-moment coefficient, $C_{h}$

Reynolds flap balance pressures coefficient, $C_{p}$

Airfoil section lift coefficient, $C_{L}$

(a) $\alpha=1.5^\circ$

(b) $\alpha=3.0^\circ$

Figure 5. Continued.
Figure 5c: Concluded.
Figure 8: Section aerodynamic characteristics of modified NACA 65-012 airfoil with 0.25c flap and 0.25c tab. Tab nose shape, plain; tab gap, open; transition strips off; $\alpha$, 0°.
Figure 7. Section aerodynamic characteristics of modified NACA 65-012 airfoil with 0.25c flap and 0.25c tab
Tab nose shape, blunt; $c_{bf}, 0.35c$; tab gap, open; transition strips at 0.0le.
Figure 7c

(c) \( \alpha, 10.2^\circ \)

Figure 7- Concluded.
Figure 8.- Section aerodynamic characteristics of modified NACA 65°-012 airfoil with 0.25c flap and 0.25c tab.
Tab nose shape, round; $c_f = 0.35c_f$; tab gap, sealed; transition strips at 0.016c.
(b) $\alpha = 5.1^\circ$

Figure 8: Continued.
Fig. 8c

Ad section hinge-moment coefficient, Ct
Flap section hinge-moment coefficient, Cm

Resultant flap balance pressure coefficient, Cp

Flap deflection, $\delta_f$, deg

Airfoil section lift coefficient, $c_l$
Figure 9: Section aerodynamic characteristics of modified NACA 63-012 airfoil with 0.25c flap and 0.25c tab.

- Lab nose shape, rounded
- Flap deflection, $\delta_f$, deg
- Flap section lift coefficient, $C_l$
- Flap section hinge moment coefficient, $C_m$
Flap deflection, $\delta_f$, deg

Resultant flap balance-pressure coefficient, $P_f$

Flap section hinge-moment coefficient, $C_m$

Round nose shape
$C_{ly} = 0.35C_f$

Figure 10. Section aerodynamic characteristics of modified NACA 65-012 airfoil with 0.25c flap and 0.25c tab.
Tab nose shape, round; $C_{ly} = 0.35C_f$; tab gap, open; transition strip at 0.01c.
(c) $\alpha$, 10.2°.
Fig. 11

NACA TN No. 1403

Figure 11. Airfoil characteristics of modified NACA 65-202 airfoil with 0.35c flap and 0.25c flap tab.

Top. Case with round 0.25c tab gap open, transition shape at 0°.

(a) Round nose shape.
Figure 12. Section aerodynamic characteristics of modified NACA 65-012 airfoil with 0.25c flap and 0.25cf tab.

Tab nose shape, elliptical; c_p = 0.35 c_f; tab gap, open; transition strips of 0.01c.
Fig. 12b NACA TN No. 1403

Fig. 12 - Continued.

Elliptical nose shape
$c_l = 0.35$
Figure 13: Section aerodynamic characteristics of modified NACA 65-012 airfoil with 0.25c flap and 0.25cf tab.
Tab nose shape, sharp; αf, 0.35 cf; tab gap, open; transition strips at 0.01c.
Figure 13—Continued.
Fig. 13c

NACA TN No. 1403

Lab section hinge-moment coefficient, $C_{H}$, flap section hinge-moment coefficient, $C_{H}$.

Resultant flap balance-pressure coefficient, $C_{p}$.

Airfoil section lift coefficient, $C_{L}$.
Figure 14: Section aerodynamic characteristics of modified NACA 6S012 airfoil with 0.25c flap and 0.25c tab. Lab nose shape, round; c_p, 0.50 c; tab gap, sealed; transition strips at 0.01 c.
(b) $\alpha, 5.1^\circ$.

Figure 14. Continued.
Flap deflection, $\delta_f$, deg

Resist skull balance pressure coefficient, $C_{p_1}$

Flap deflection, $\delta_f$, deg

Resist skull balance moment coefficient, $C_{\theta_1}$

(c) $\alpha = 10.2^\circ$

Figure 14-Concluded.
Figure 15.-Section aerodynamic characteristics of modified NACA 65-012 airfoil with 0.25c flap and 0.25c tab.
Tab nose shape, round; \( c_h \), 0.30c; tab gap, sealed; transition strips off; \( \alpha \), 0°.
Fig. 16a

Figure 16—Section aerodynamic characteristics of modified NACA 65-012 airfoil with 0.25c flap and 0.25c tab.
Tab nose shape, round; \( \theta_y = 0.50 \) deg; tab gap, open; transition strips at 0.01c.
Fig. 16b
(b) $\alpha = 51^\circ$.
Figure 16 - Continued.
Round nose shape

Airfoil section lift coefficient, $C_l$

Resultant flap balance pressure coefficient, $C_{pl}$

Flap section hinge-moment coefficient, $C_{pH}$

Flap deflection, $\alpha$, deg

(c) $\alpha = 10.2^\circ$

Figure 16.- Concluded.
Figure 17. Section aerodynamic characteristics of modified NACA 65-012 airfoil with 0.25c flap and 0.25c cf tab. Tab nose shape, round; \( \delta_f = 0.30c_f \); tab gap, open; transition strips off; \( \alpha = 0° \).
Figure 18. Section aerodynamic characteristics of modified NACA 65-012 airfoil with 0.25c flap and 0.25c tab.
Tab nose shape, elliptical; \( \alpha_f = 0.50 \) c; tab gap, open; transition strips at 0.01c.
Elliptical nose shape

(C) α = 10.2°.
Figure 18. Concluded.
Figure 12. Section aerodynamic characteristics of modified NACA 65-012 airfoil with 0.25c flap and 0.25cf tab. Tab nose shape, sharp; $c_f = 0.50c$; tab gap, open; transition strips at 0.01c.
Airfoil section lift coefficient, $C_L$

![Graph showing airfoil section lift coefficient vs. flap deflection, $\delta_f$, deg.

Sharp nose shape
$C_L = 0.50C_f$

Resultant flap balance-pressure coefficient, $P_h$

Flap section hinge-moment coefficient, $S_h$

(b) $\alpha, 51^\circ$

Figure 19-Continued.
Fig. 19c: Afton section lift coefficient, $c_L$ vs. Flap deflection, $\delta_f$, deg.

(c) $\alpha=10.2^\circ$.

Figure 19c Continued.
Figure 20. Section aerodynamic characteristics of modified NACA 65-012 airfoil with 0.25c flap and 0.25c tab. Tab nose shape, plain; tab gap, sealed; $\alpha_f, 0^\circ$; $\alpha_t, 0^\circ$.
Figure 21. - Section aerodynamic characteristics of modified NACA 65-012 airfoil with 0.25c flap and 0.25c tab. Tab nose shape, plain; tab gap, open; d_f, 0°; d_f, 0°.
Figure 22.- Section aerodynamic characteristics of modified NACA 65-012 airfoil with 0.25c flap and 0.25c tab.
Tab nose shape, round; $c_f = 0.35c$; tab gap, sealed; $\delta = 0, \delta = 0$. 

Round nose shape $c_f = 0.35c$
Figure 23.- Section aerodynamic characteristics of modified NACA 65-012 airfoil with 0.25c flap and 0.25c tab. Tab nose shape, round; $C_f$ 0.35 cf; tab gap, open; $\delta_f 0^\circ$; $\delta_t 0^\circ$. Round nose shape $C_f = 0.35 cf$.
Figure 24. Section aerodynamic characteristics of modified NACA 65-012 airfoil with 0.25c flap and 0.25c² tab. Tab nose shapes, blunt, elliptical, sharp; c_y = 0.35c²; tab gap, open; transition strips at 0.01c; δ_f, 0°; δ_r, 0°.
Figure 25: Section aerodynamic characteristics of modified NACA 65-012 airfoil with 0.25c flap and 0.25c tab. Tab nose shape, round; $c_t$, 0.50c; tab gap, sealed; $\alpha$, 0°; $\delta$, 0°.
Figure 26: Section aerodynamic characteristics of modified NACA 65;012 airfoil with 0.25c flap and 0.25c tab. Tab nose shape, round; $c_f$, 0.50 c; tab gap, open; $\delta_f$, 0°; $\delta_f$, 0°.
Figure 27.-Section aerodynamic characteristics of modified NACA 65-012 airfoil with 0.25c flap and 0.25c tab. Tab nose shapes, elliptical, sharp; $C_f$, 0.50 $C_f$; tab gap, open; transition strips at 0.01 $C$; $\delta_t$, 0°; $\delta_c$, 0°.
Figure 28: Effect of tab nose shape and overhang length on hinge-moment parameters on the modified NACA 65;012 airfoil. Tab gap, 0.004c; transition strips at 0.01c.
Fig. 29

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Unflagged symbols, $c_b = 0.35c_f$
Flagged symbols, $c_b = 0.50c_f$

Correlation of aileron data of reference 9, $c_f = 0.15c$ to $0.30c$

Figure 29 - Effect of tab balance and nose shape on tab hinge-moment parameters.
Figure 30: Effect of tab balance on flap section hinge-moment coefficient of the NACA 65-012 airfoil. Tab gap 0.004 c; transition strips at 0.01 c.
Figure 31: Effect of fixing transition and sealing tab gap on hinge moment parameters on modified NACA 65-012 airfoil. Round-nose tabs.
Figure 32. Variation of Lift with $a_k$ for various tab nose shapes and various aileron balances. Tab gap, 0.0046; transition slipstream at 200 knots, 1 mile per hour, airplane 1.
Fig. 33a, b

Figure 33: Location of flaps with $q_f/g_f$ for various tab nose shapes and various chord balances. Tab gap 0.004; transition strips.

R. 9, 10

(a) $q_f/g_f$

(b) $q_f/g_f$

Control flare per degree Allen deflection. Flat: 1/3 leg.
Fig. 33c, d

NACA TN No. 1403

[Graph and diagram with data points and lines indicating trends across various categories and parameters.]
Figure 34: Variation of control force ratio with aerodynamic balance and spring strength.

Roundnose tab character, \( k_3 \)

Spring constant, \( k_3 \)

Balanced tab/Plain tab

Balanced tab/Plan tab

\[ \frac{C_{D}}{S\_	ext{E}} \]
Figure 35-Comparison of the variation of \( C’_{\text{ch}} \) with \( C’_{\theta} \) for overhang and internal tab balances. Transition strips at \( C’_{\theta} = 0.04; V = 500 \) miles per hour.

Control force per degree aileron deflection, \( F/\text{deg}, \) lb/day.
Figure 36: Variation of Flap\(\alpha_f\) with airspeed for various aileron and spring-tab balance conditions. \(k_5, 10;\) airplane 2; tab gap, 0.004\(c;\) transition strips at 0.01\(c.\)
Figure 37.- Effect of tab overhang on the variation of control force with aileron deflection as determined by references 9 and 11. $k_2 = 1.0$; tab gap, 0.004 c; transition strips at 0.01 c; $V$, 300 miles per hour; airplane 1.