

UNSTEADY FLOW SIMULATIONS IN SUPPORT OF
THE SSME HEX TURNING VANE CRACKING
INVESTIGATION WITH THE ATD HPOTP

by

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ABSTRACT

Unsteady flow computations are being performed with the P&W (ATD) and the Rocketdyne baseline configurations of the SSME LO₂ turbine turnaround duct (TAD) and heat exchanger (HEX). The work is in support of the HEX inner turning vane cracking investigation. Fatigue cracking has occurred during hot firings with the P&W configuration on the HEX inner vane, and it appears the fix will involve changes to the TAD splitter vane position and to the TAD inner wall curvature to reduce the dynamic loading on the inner vane. Unsteady flow computations on the P&W baseline and fix and on the Rocketdyne baseline reference follow steady-flow screening computations done by MSFC/ED32 on several trial configurations arriving at the fix.

The P&W TAD inlet velocity profile has a strong radial velocity component that directs the flow toward the inner wall and raises the local velocity a factor of two and the dynamic pressure a factor of four. The fix is intended to redistribute the flow more evenly across the HEX inner and outer vanes like the Rocketdyne baseline reference. Vane buffeting at frequencies around 4,000 Hz is the leading suspected cause of the problem. Our simulations (work in progress) are being done with the USA 2D axisymmetric code approximating the flow as axisymmetric u+v 2D (axial, u, and radial, v, components only). The HEX coils are included in the model to make sure the fix does not adversely affect the HEX environment.

Turbulent kinetic energy, k , levels where $k = 1/2 v' \text{ rms}^2$ are locally as high as 10,000 ft²/sec² for the P&W baseline at the engine interface (between the TAD and HEX) at the HEX inner vane location. However, k is less than 8,000 on the HEX outer vane and only about 4,500 on the HEX inner vane for the Rocketdyne baseline. Unsteady turbulence intensity, v'_{rms}/v , and pressure, p' , are being computed in the present computations to compare with steady-flow Reynolds-averaged computations where $p'_{\text{rms}} = \text{const} (\rho k)$ for overall rms random turbulence from 0.1 to 12,000 Hz frequency. Random overall static, p'_{rms} fluctuations as large as 1.7 psi are estimated from k on the HEX inner vane for the P&W baseline configuration but only about 0.7 psi for the Rocketdyne configuration.



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APRIL 20, 1993

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ENGINE HEX TURNING VANE CRACKING INVESTIGATION UNSTEADY CFD ANALYSIS

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OBJECTIVE

- PROVIDE UNSTEADY FLOW SIMULATIONS OF THE ATD HPOTP TURNAROUND DUCT/HEAT EXCHANGER FLOW TO SUPPORT IDENTIFICATION OF A "FIX" THAT:
 - 1) ELIMINATES HEX INNER VANE CRACKING, AND
 - 2) DOES NOT ADVERSELY AFFECT THE HEX COIL ENVIRONMENT



APPROACH

- DENSITY-BASED TIME-ACCURATE CFD CODE
 - 2ND-ORDER ACCURATE
 - PREVIOUSLY BENCHMARKED ON SIMPLE FLOW
 - RECTANGULAR CAVITY (ROSSITER)
 - EDGETONE (BROWN)
 - CURVED VANE (4 KHZ LO₂ SPLITTER VANE)
 - AXISYMMETRIC u AND v
- GEOMETRY, BOUNDARY CONDITIONS, AND REFERENCE QUANTITIES SAME AS IN STEADY-FLOW CFD ANALYSIS
- RESULTS COMPARED FOR GEOMETRY CHANGE
 - BASELINE CONFIGURATION
 - "FIX" CONFIGURATION



MODELING APPROACH

BENEFITS

- CAN SHOW POTENTIALS FOR UNSTEADY BEHAVIOR
 - FLOW INSTABILITIES, UNSTEADY SEPARATION, BUFFETING
- MATCHES 2D STEADY-FLOW CFD (MEAN VALUES)
- PROVIDES HEX VANE UNSTEADY LOADING - - p' , (t, ℓ)
- CAN PROVIDE p' AT AIRFLOW MEASUREMENT LOCATIONS
- AIDS UNDERSTANDING OF HOT FIRE AND AIRFLOW TEST DATA

AREAS FOR IMPROVEMENT

- 2D (INSTEAD OF 3D) TRUNCATED GEOMETRY CAN ALLOW ACOUSTICS TO DOMINATE
- TURBULENCE TREATMENT IS ALWAYS A QUESTION



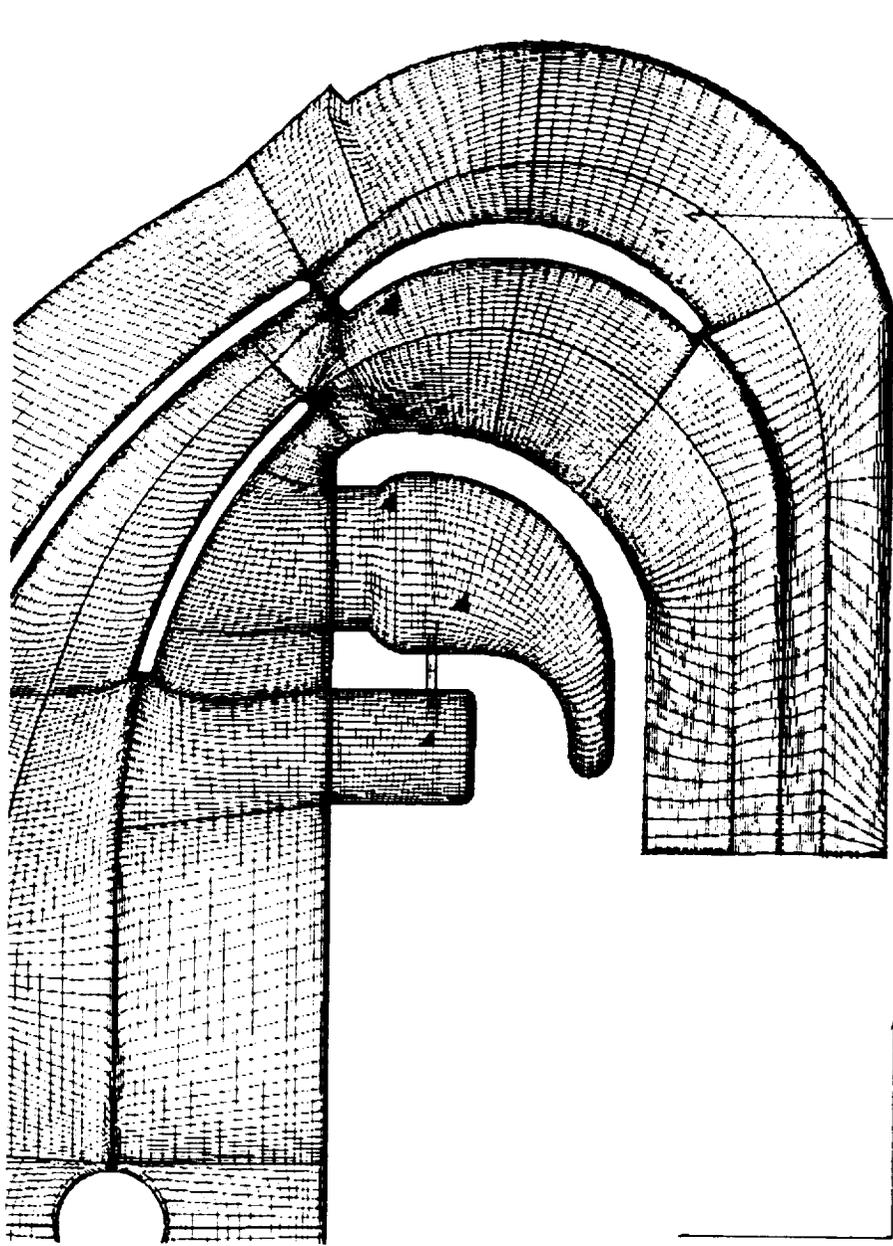
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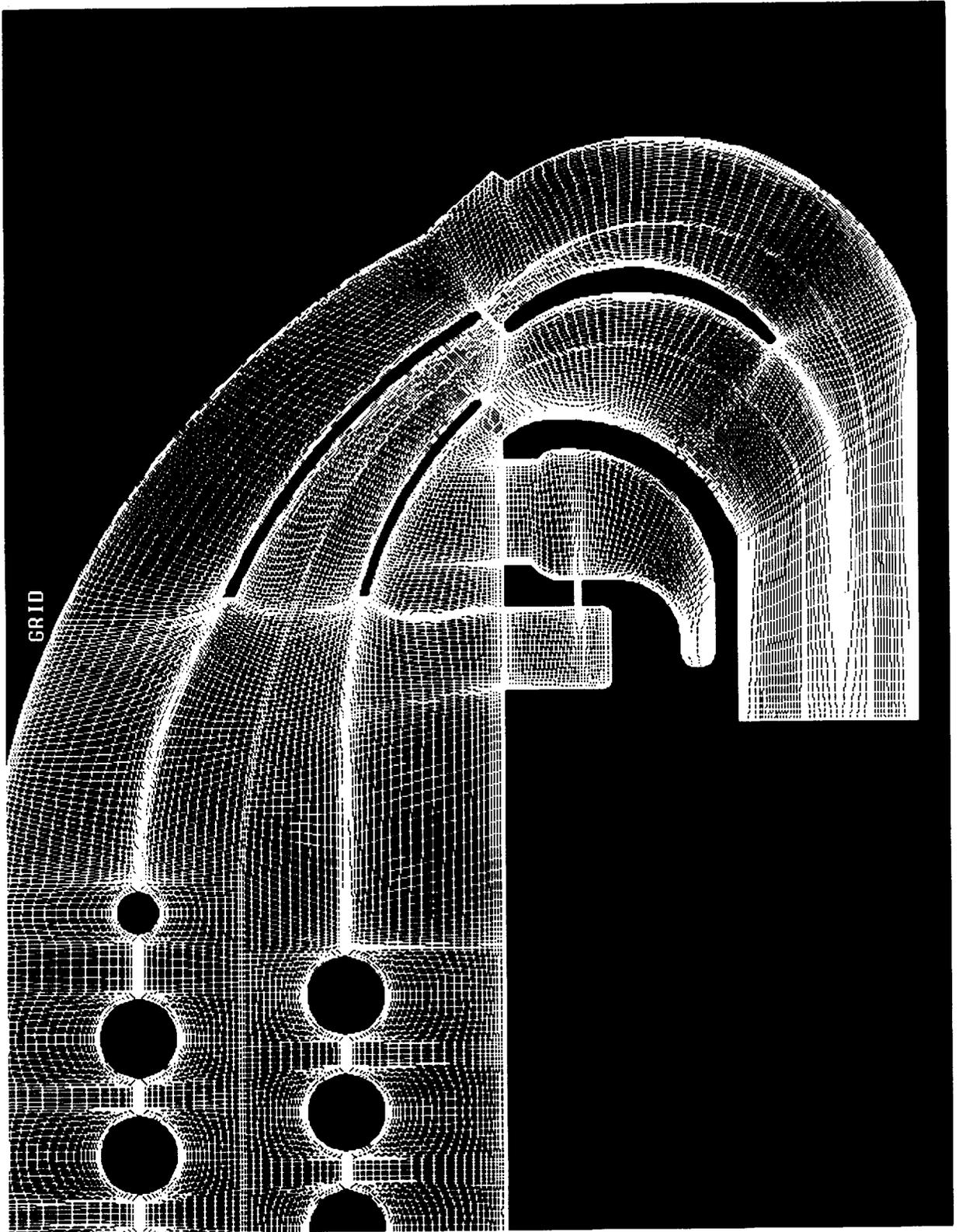
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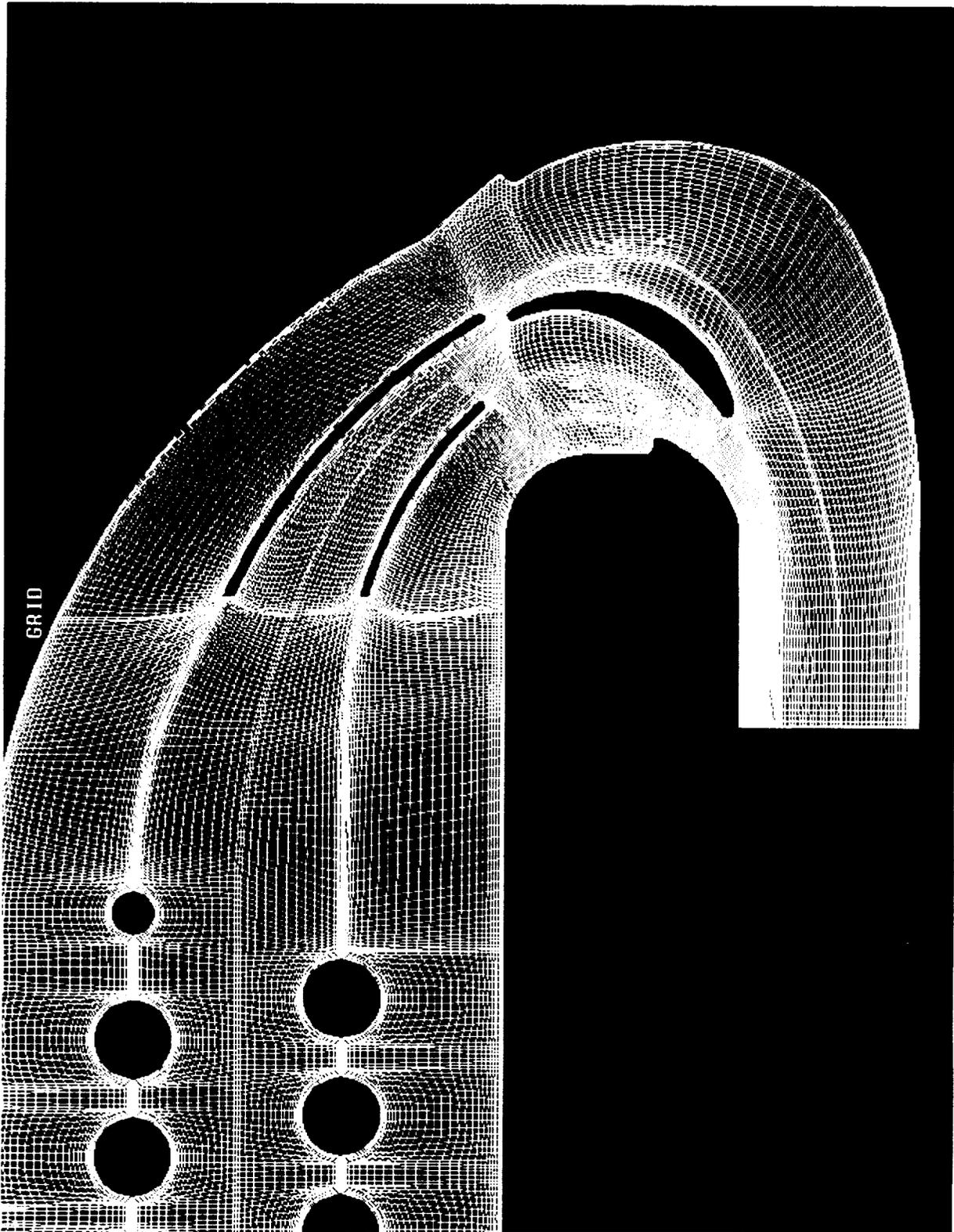
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BASELINE CONFIGURATION GRID





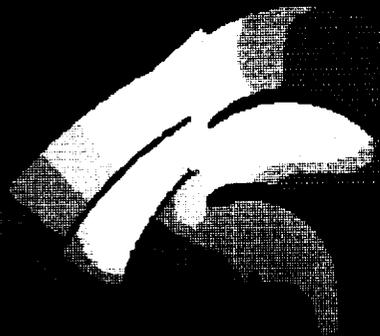


GRID

PRESSURE
Pratt & Whitney Baseline

CONTOUR LEVELS

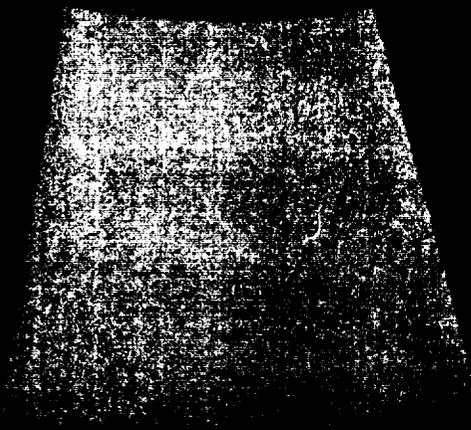
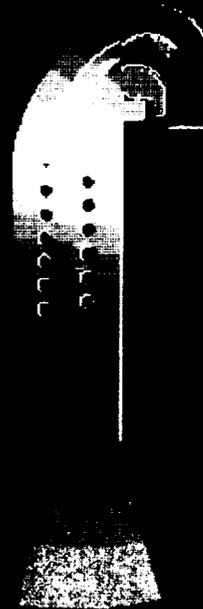
0.98800
0.99000
0.99200
0.99400
0.99600



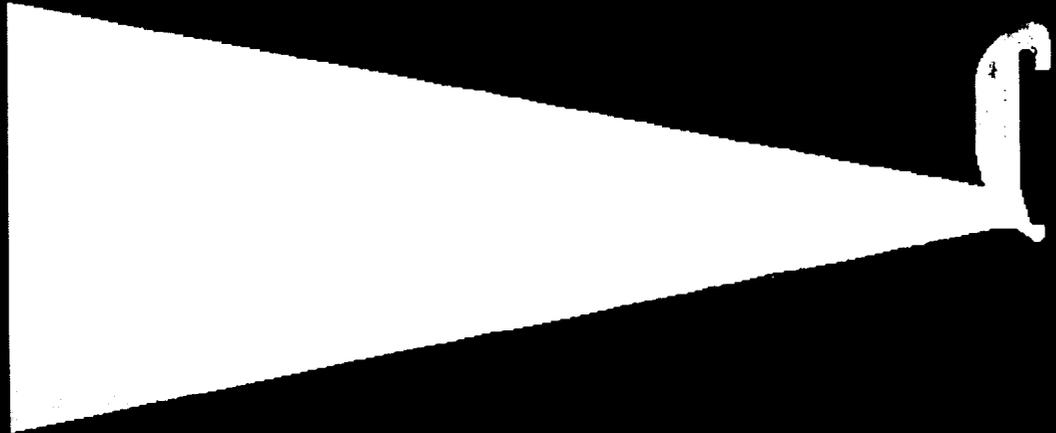
PRESSURE
Pratt & Whitney Baseline

CONTOUR LEVELS

1.01400
1.01600
1.01800
1.02000



PRESSURE
Pratt & Whitney Fix



CONTOUR LEVELS

1.00000
1.00050
1.00100
1.00150
1.00200
1.00250
1.00300
1.00350
1.00400

1.00450
1.00500
1.00550
1.00600

MACH NUMBER
Pratt & Whitney Baseline

CONTOUR LEVELS



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0.07594
0.07931
0.08309
0.08687
0.09064
0.09442

0.14810
0.15290
0.15773

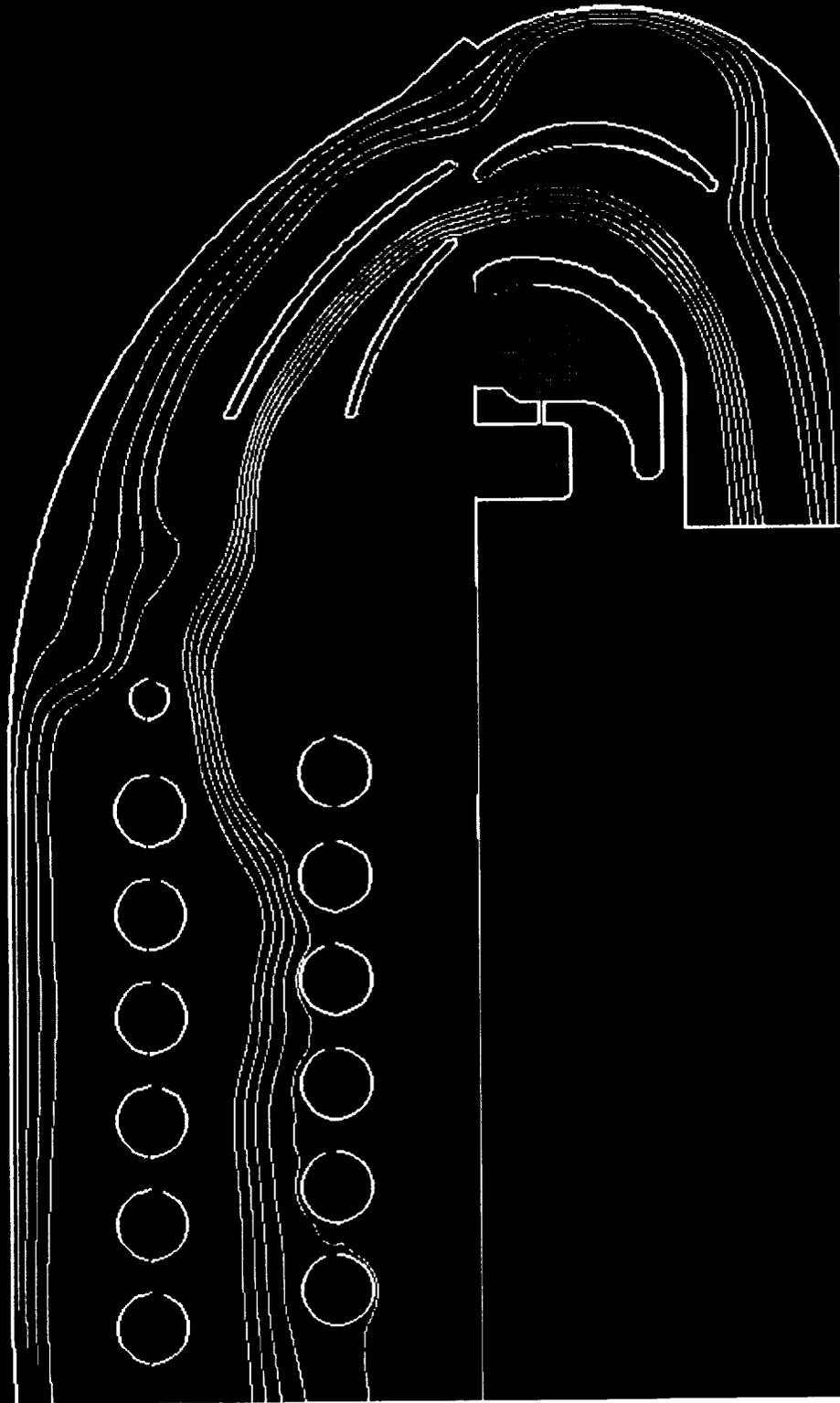
DYNAMIC PRESSURE
Prett & Whitney Baseline

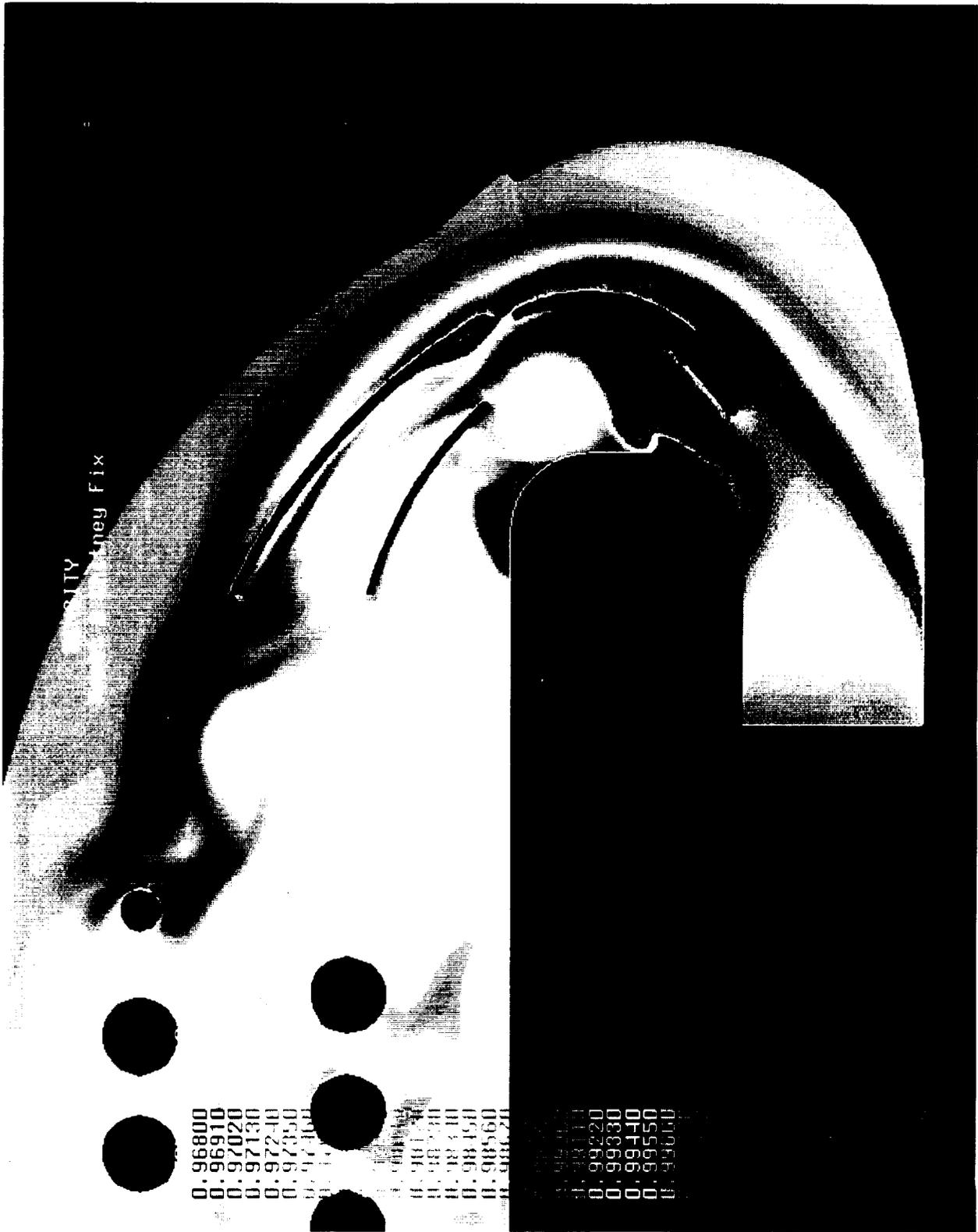
CONTOUR LEVELS

30.00000
31.00000
32.00000
33.00000
34.00000
35.00000
36.00000
37.00000
38.00000
39.00000
40.00000
41.00000
42.00000
43.00000
44.00000
45.00000
46.00000
47.00000
48.00000
49.00000
50.00000
51.00000
52.00000
53.00000
54.00000
55.00000
56.00000
57.00000
58.00000
59.00000
60.00000
61.00000
62.00000

59.00000
62.00000

PARTICLE TRACES
Pratt & Whitney Baseline





...they Fix

0.96800	0.98100
0.96910	0.98200
0.97020	0.98300
0.97130	0.98400
0.97240	0.98500
0.97350	0.98600
0.97460	0.98700
0.97570	0.98800
0.97680	0.98900
0.97790	0.99000
0.97900	0.99100
0.98010	0.99200
0.98120	0.99300
0.98230	0.99400
0.98340	0.99500
0.98450	0.99600
0.98560	0.99700
0.98670	0.99800
0.98780	0.99900
0.98890	1.00000

MACH NUMBER
Pratt & Whitney Fix

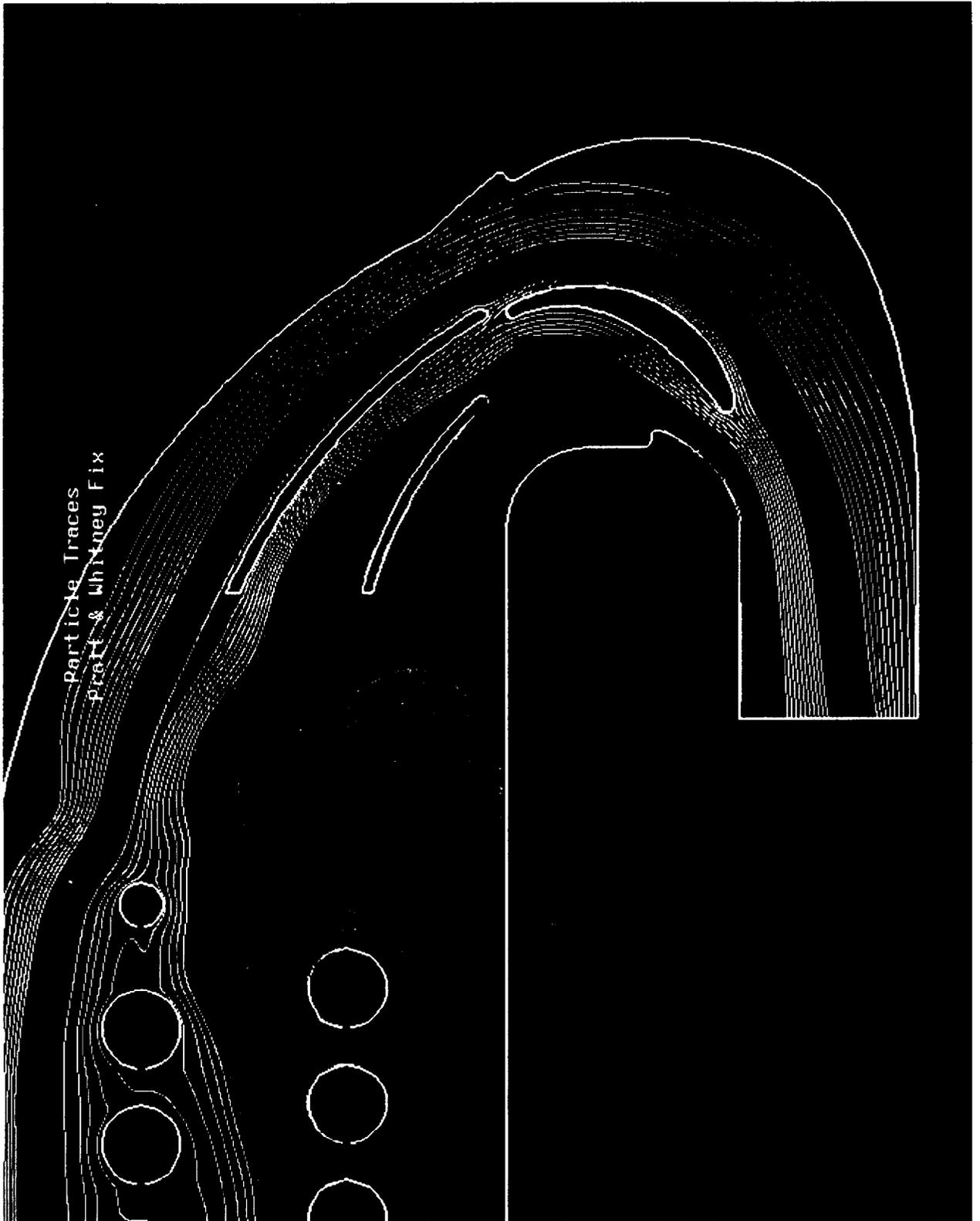
CONTOUR LEVELS

0.08096
0.08164
0.08232
0.08300
0.08368

DYNAMIC PRESSURE
Pratt & Whitney F16

CONTOUR LEVELS

27.50001
29.15001
30.47501
31.80001
33.12501
34.45001





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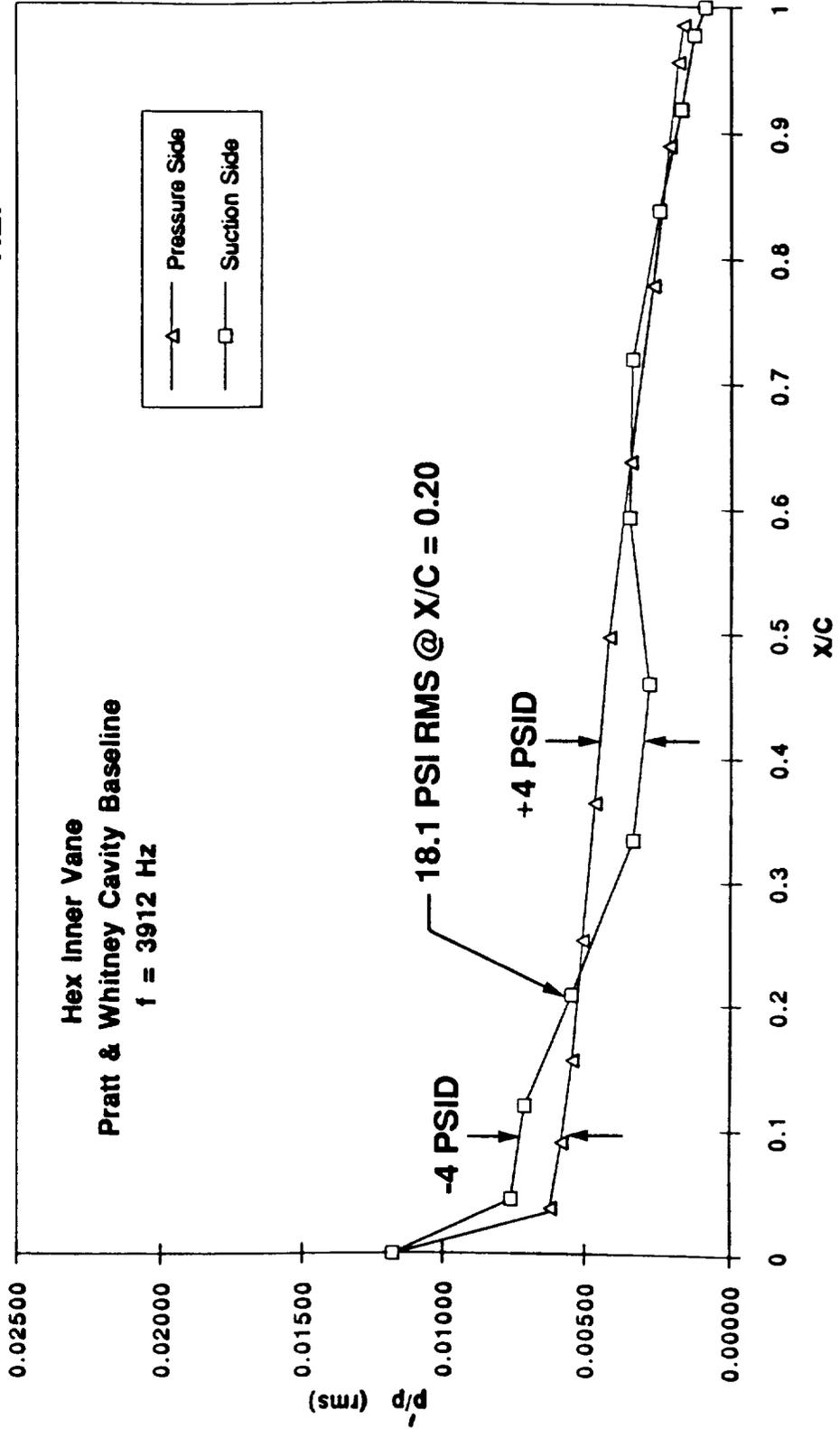
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THE ACOUSTICALLY-TUNED P&W BASELINE WITH CAVITIES CASE GAVE ABSOLUTE AND DIFFERENTIAL LOADINGS ON THE HEX INNER VANE

-- AS LARGE AS 4 PSID

P_{REF} = 3625 PSI





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PRELIMINARY CONCLUSIONS

- 1) UNSTEADY PRESSURE DIFFERENTIAL LOADINGS WERE PRODUCED LARGE ENOUGH TO CRACK THE HEX INNER VANE IN THE BASELINE CONFIGURATION. (WITH EXCESSIVE ACOUSTIC TUNING, THEY WERE LARGE ENOUGH TO CRACK THE HEX OUTER VANE ALSO)
- 2) UNSTEADY PRESSURE DIFFERENTIAL LOADINGS WERE SOMEWHAT REDUCED ON THE HEX INNER VANE FOR THE "FIX" CONFIGURATION BUT THE HEX COIL ENVIRONMENT IS INCREASED

**NOTE: ANALYSIS OF COMPUTATIONAL RESULTS STILL IN PROGRESS
DUE: APRIL 26, 1993**

