Fabrication of Iron-Containing Carbon Materials From Graphite Fluoride

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Prepared for the
22nd Biennial Conference on Carbon
sponsored by the American Carbon Society
San Diego, California, July 16–21, 1995
FABRICATION OF IRON-CONTAINING CARBON MATERIALS FROM GRAPHITE FLUORIDE

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SUMMARY

Carbon materials containing iron alloy, iron metal, iron oxide or iron halide were fabricated. Typical samples of these metals were estimated to contain 1 iron atom per 3.5 to 5 carbon atoms. Those carbon materials containing iron alloy, iron metal, and/or Fe3O4 were magnetic. The kinetics of the fabrication process were studied by exposing graphite fluoride (CF0.68) to FeCl3 over a 280 to 420 °C temperature range. Between 280 and 295 °C, FeCl3 quickly entered the structure of CF0.68, broke the carbon-fluorine bonds, and within 10 to 30 min, completely converted it to carbon made up of graphite planes between which particles of crystalline FeF3 and noncrystalline FeCl2 were located. Longer reaction times (e.g., 28 hr) or higher reaction temperatures (e.g., 420 °C) produced materials containing graphite, a FeCl3-graphite intercalation compound, FeCl2•4H2O, and FeCl2•2H2O. These products were further heat treated to produce iron-containing carbon materials. When the heating temperature was kept in the 750 to 850 °C range, and the oxygen supply was kept at the optimum level, the iron halides in the carbon structure were converted to iron oxides. Raising the heat to temperatures higher than 900 °C reduced such iron oxides to iron metal. The kinetics of these reactions were used to suggest processes for fabricating carbon materials containing iron alloy. Such processes were then tested experimentally. In one of the successful trial runs, commercially purchased CF0.7 powder was used as the reactant, and NiO was added during the final heating to 1200 °C as a source of both nickel and oxygen. The product thus obtained was magnetic and was confirmed to be a nickel-iron alloy in carbon.

INTRODUCTION

In a previous investigation (ref. 1), ferric chloride (FeCl3) was found to react with graphite fluoride (CFx) between 300 and 400 °C to give a graphite intercalation compound (GIC). The GIC’s always contained a large quantity of iron halides, which were either iron chloride or a mixture of iron chloride and iron fluoride. The GIC’s could be further heated to change the iron halide component to iron oxide in or on the carbon. The products of these reactions were characterized (see ref. 1) by using x-ray diffraction (XRD) and energy-dispersive spectroscopy (EDS). Reaction kinetics, however, were not studied in the previous investigation.

The graphite fluoride used in these reactions included CF0.68 made from highly graphitized P-100 carbon fibers, CF1.0 made from less graphitized P-55 carbon fibers, CF0.9 made from nongraphitized P-25 fibers, and commercially purchased CF0.9 made from crystalline graphite powder. The reactions appeared to occur regardless of the source of the carbon from which CFx was made or the fluorine-to-carbon ratio of the CFx reactants, at least when 0.68 ≤ x ≤ 1.0. The main reaction observed can be divided into two subreactions:

In the first, FeCl3 enters the CFx structure and causes CFx to defluorinate, which results in a carbon material that contains an iron halide mixture:

\[ \text{CF}_x + \text{FeCl}_3 \xrightarrow{300 \text{ to } 420 \degree \text{C}} \text{C(iron halides)} \quad 0.68 \leq x \leq 1.0 \] (1)

In the second subreaction, the carbon–iron-halide mixture reacts with low concentrations of oxygen at about 800 °C to produce carbon that contains FeO and Fe3O4:

\[ \text{C (iron halides)} \xrightarrow{\text{low O}_2 \atop 800 \degree \text{C}} \text{C(FeO, Fe}_3\text{O}_4) \] (2)
The temperature and oxygen concentration are the important parameters in determining the type of products to be obtained in reaction (2). For example, 800 °C and 1-atm air converted all carbon into CO₂, and Fe₂O₃ resulted. On the other hand, the reaction between carbon and 1-atm air at 370 °C was so slow that the reaction products were deintercalated carbon and Fe₂O₃:

\[
\text{C (iron halides)} \xrightarrow{1\text{-atm air \; 370 °C}} \text{C + Fe}_2\text{O}_3
\]  

In this report, the format C(Y,Z) represents a carbon material that contain the materials Y and Z in the space between the carbon planes.

A study of the reaction kinetics became important when it was found that a product of the aforementioned reactions, Fe₃O₄-containing carbon, was attracted to a magnet (fig. 1). Through a study of the kinetics, the effects of operating conditions (e.g., reaction time, reaction temperature, or reactant quantities) on the product’s properties can be understood. Then, it may be possible to optimize the operating conditions and improve the magnetic properties of these products.

In this research, the kinetics of reactions (1) and (2) were constructed from experimental data. The kinetics thus obtained, together with the known chemistry of iron, oxygen, and carbon, were then used to suggest processes that might produce new iron-alloy-bearing carbon products with high permeability values. Experiments were conducted to verify the suggested processes.

EXPERIMENTAL METHODS

Two series of experiments were conducted to investigate reactions (1) and (2). For each reaction, every single experiment was conducted so as to reach a different degree of completeness by choosing a different time-temperature combination for the reaction. The reaction kinetics were then inferred by characterizing, examining, and comparing the products obtained from the individual experiments.

Formation of Iron-Halide Mixtures in Carbon

For the CFₓ-FeCl₃ reaction, the reactants were placed in a glass tube reactor filled with 99.99-percent nitrogen at room temperature in anticipation of heating them to the reaction temperature of 280 to 350 °C in a tube furnace. The reaction started before the furnace and the reactor reached the reaction temperature. A reaction during heatup may be significant, especially if the reaction time is short. In this research, several reactions were allowed to continue for time intervals ranging from 10 min (0.17 hr) to 28 hr after they reached the desired reaction temperature. The CFₓ samples were fibers obtained by several cycles of fluorination (1 atm, 330 to 370 °C fluorine exposure) and defluorination (1 atm, 330 to 370 °C nitrogen exposure) of P-100 carbon fibers that had been preintercalated with bromine and iodine (ref. 2).

Conversion of Iron Halides to Iron Oxides in Carbon

The reactants for the conversion of iron halides to iron oxide in carbon (reaction (2)) were the products from two of the experiments in the series for reaction (1). They were placed in a quartz tube filled with 99.99-percent nitrogen and allowed to react over a temperature range of 650 to 1200 °C for periods ranging from 30 min to 3 hr. During this reaction, nitrogen flowed through the quartz tube at a rate of about 0.05 to 0.5 mL/sec.

The reaction products were characterized for noncarbon content by weight analysis, for structure identification by x-ray diffraction (XRD), for chemical element identification by energy-dispersive spectroscopy (EDS), and for morphology by scanning electron microscopy (SEM). It should be noted that the EDS data were obtained with the instrument operated at 25 kV. At this voltage, the electrons penetrated, and therefore examined, only the outer 2 to 3 μm of the samples. The XRD, on the other hand, examined the entire diameter of the fiber samples, typically 10 to 20 μm.
RESULTS AND DISCUSSION

Formation of Iron Halide Mixtures in Carbon

Table I summarizes the experiments conducted to investigate reaction (1). The data in the table reflect four reactions at a constant temperature between 280 and 300 °C, one reaction at 295 to 325 °C for 3.25 hr, and one from reference 1 at 330 to 420 °C. Of the five recent reactions, the 28-hr (285 °C) and the 3.25-hr (295 to 325 °C) ones were conducted by using CF0.68 and distilled anhydrous FeCl3 according to the method described in reference 1. The 10-min, 30-min, and 3-hr reactions at 280 to 295 °C were conducted in vials that contained mixtures of CF0.68 and commercially purchased anhydrous FeCl3 powder. The vials containing the reactants were exposed to a nitrogen environment in the glass tube reactor for the predetermined time at the predetermined temperature. During the reaction the vials were plugged by glass rods wound with PAN-based carbon fibers.

For comparison, a product obtained from the reaction between FeCl3 and the precursor of the CF0.68 (i.e., the pitch-based P-100 carbon fibers described in the previous section) was also included in table I (see test G).

The kinetics of reaction (1) can be inferred from the data shown in table I and are described in the following subsections.

**Quick FeCl3 absorption and CF0.68 defluorination.—**The data in table I show that low reaction temperatures and short reaction times favor the presence of FeF3 and the absence of crystalline graphite. Exposing FeCl3 to CF0.68 fibers at 295 °C for 10 min increased the fiber mass. In addition, most of the CF0.68 disappeared, and highly ordered FeF3 was produced. After 30 min of reaction at 290 °C, the FeF3 persisted and there were no additional mass changes observed, but the CF0.68 disappeared completely. These observations suggest that immediately after direct contact, FeCl3 quickly reacted with all the fluorine in the CF0.68 to produce FeF3.

**Formation of FeF3 in disrupted graphene layers.—**After CF0.68 was defluorinated and FeF3 produced, most (if not all) of the covalent bonds between carbon and fluorine had been broken, and the electrical resistance of the fiber product plunged from about $10^{13}$ Ω/cm to a typical value of 1 to 3 kΩ/cm. This is approximately 4 to 12 times the value for the P-100 graphitized carbon fibers from which the CF0.68 was made. The data suggest that the carbon structure changed from sp3 for the CF0.68 to sp2 for the disrupted graphene layers. However, the XRD shows a broad, barely visible graphite peak, even after 28 hr of reaction at 285 °C. It appears, then, that the FeF3 formed during this reaction remains in the disrupted graphene layers at 285 °C for at least 28 hr.

**State of chlorine in reaction products.—**Significant amounts of chlorine were found in the products of all the reactions described in table I. This information was obtained by EDS, which detects the outer 2 to 3 μm of the 10- to 20-μm-diam fibers. The atomic ratio of chlorine to iron was about 1 shortly after the beginning of a 280 to 300 °C reaction. After 3 hr at 280 °C, the atomic ratio increased to a value between 1.5 and 2 (EDS data). However, no chlorine-containing compounds were detected by XRD for any reaction between 280 and 300 °C for up to 28 hr of reaction time. After the 295 to 325 °C reaction, however, FeCl2·4H2O was identified by XRD analysis of the reaction products (ref. 3). One possible explanation is that during defluorination of CF0.68 and formation of FeF3, the chlorine atoms were in the form of an FeCl3 intercalate that was between the disrupted graphene layers and surrounded the FeF3 crystals. Higher reaction temperatures caused this intercalate to slowly react with FeF3 and form FeCl2. Subsequently a hydrate was formed when the products were exposed to the ambient air.

This explanation assumes that the material between the disrupted graphene layers in the reaction product is a mixture of FeF3 and intercalated FeCl3. If the reaction time is prolonged, this mixture also contains FeCl2.

**High iron concentration.—**The amount of iron in this product was estimated by heating the products in air at 370 °C, slowly increasing the temperature to 500 °C over a 1-week duration, and then measuring the weight of Fe2O3 thus obtained. This method produced an error due to the evaporation of a small amount of iron halide during heating. Therefore, the true iron concentration is believed to be slightly higher than the values obtained from this method.

If all the fluorine in CF0.68 reacted to form FeF3, the ratio of FeF3 to carbon would be 0.68/3, or 0.23, and the atomic ratio of total iron to carbon in this product would be 0.23 plus the remaining iron contribution from the intercalated FeCl3. This compares to the estimated experimental values of at least 0.18 and 0.22 for the products of the 10- and 30-min reactions (table I), respectively. This reasoning explains the high iron concentration in the carbon product obtained in this research.

**Distortion and/or disappearance of FeF3 crystals.—**Table II shows the XRD peak for FeF3 in the carbon products formed after 30 min and 28 hr of FeCl3-CF0.68 reaction. For comparison, standard XRD data for a pure FeF3 crystal (ref. 4) are also included in this table. Note that the XRD for the FeF3 produced in the 30-min reaction
is very close to that for standard rhombohedral FeF$_3$. The data from the 28-hr reaction, however, deviate somewhat from the standard values.

Another observation, which cannot be ascertained from tables I and II, was made: The FeF$_3$ XRD peaks obtained from the product of the longest reaction (28 hr) are much lower and broader than other FeF$_3$ XRD peaks obtained from the product of the 30-min reaction.

The data shown in table II suggest that immediately after the reaction, the FeF$_3$ produced has the structure of a pure crystal. Longer reaction times allow more FeCl$_3$ intercalation, which causes the structure of FeF$_3$ to change. This may be due to either the diffusion of chlorine into the FeF$_3$ structure, or the increasing external mechanical pressure that results from the continuous influx of FeCl$_3$ into the carbon structure.

**Removal of FeF$_3$ at high reaction temperature.**—Test F in table I indicates that if the CF$_{0.68}$-FeCl$_3$ reaction is conducted at a much higher temperature (330 to 420 °C), the fiber product becomes very different. Its XRD shows a large graphite peak, small first-stage FeCl$_3$ GIC peaks (identity period, $I_c = 9.3$ Å), and the presence of FeCl$_2$$\cdot$2H$_2$O (see ref. 5). No trace of fluorine in or on the carbon fibers was detected, either by XRD or by EDS.

These data suggest that, at a high temperature and over a long time, the fluorine atoms produced from FeF$_3$ at an early stage of the reaction between CF$_{0.68}$ and FeCl$_3$ are removed from the carbon structure while the FeCl$_3$ continues to enter the carbon structure. A probable mechanism of fluorine removal is the reaction of FeF$_3$ and the nearby FeCl$_3$ intercalate, causing production and evaporation of either mixed iron halides (FeCl$_x$F$_y$) or chlorine fluoride (ClF). This may result in a product which, upon exposure to ambient air, has XRD peaks of FeCl$_3$-GIC, graphite, and FeCl$_2$$\cdot$2H$_2$O.

From this analysis, the formation of an iron halide mixture in carbon can be described as follows:

\[
\text{CF}_x + \text{FeCl}_3 \xrightarrow{\text{N}_2, 280 \text{ to } 325 \degree \text{C}} \text{C(FeF}_3, \text{Fe, Cl)}
\]

\[
\text{C(FeF}_3, \text{Fe, Cl)} + \text{FeCl}_3 \xrightarrow{\text{N}_2, 295 \text{ to } 325 \degree \text{C}} \text{C(FeF}_3, \text{FeCl}_2, \text{Fe, Cl)}
\]

\[
\text{C(FeF}_3, \text{FeCl}_2, \text{Fe, Cl)} + \text{FeCl}_3 \xrightarrow{\text{N}_2, 420 \degree \text{C, 6.5 hr}} \text{C(FeCl}_2, \text{Fe, Cl)}
\]

\[
\text{FeCl}_2 + \text{ambient air} \xrightarrow{25 \degree \text{C}} \text{FeCl}_2 \cdot 2\text{H}_2\text{O}
\]

\[
\text{FeCl}_2 + \text{ambient air} \xrightarrow{25 \degree \text{C}} \text{FeCl}_2 \cdot 4\text{H}_2\text{O}
\]

In the remainder of this report, C(FeF$_3$, FeCl$_2$, Fe, Cl) and C(FeCl$_2$, Fe, Cl) will be abbreviated by using C(FeX$_n$), where X represents a halogen.

**Oxidation of C(FeX$_n$) in a High Temperature, Low-Oxygen Environment**

When the products of reactions (5) and (6) were treated at 800 °C in nitrogen in a quartz reactor for 30 min, the products became FeO and Fe$_3$O$_4$ contained in carbon (ref.1). The source of oxygen was believed to be the water that had been adsorbed on the carbon before the heating was begun (ref.1). Note that the oxygen supply had to be low enough to keep carbon consumption and CO and CO$_2$ formation from being significant, and to prevent Fe$_2$O$_3$ from being produced.

The oxidation of C(FeX$_n$) in a high-temperature, low-oxygen environment was further studied experimentally and is described in the following subsections.

**Effects of heating temperature in the 750 to 1200 °C range.**—Five samples of the C(FeX$_n$) product from reaction D (see table I) were heated in a quartz reactor in a nitrogen environment at 650 to 750, 850, 900, 950, and 1200 °C, respectively. Another C(FeX$_n$) sample obtained from reaction E (table I) was similarly tested at 1180 °C.
The heating time and heating products are described in table III. The chemicals produced were identified by XRD (refs. 6 to 9).

By examining and comparing the reactants and the products in table III, one can determine that heating at 750 °C

- transforms the FeF₃ structure from rhombohedral to cubic
- reduces part of the cubic FeF₃ in carbon to FeF₂
- oxidizes part of the FeF₂ to FeO
- reduces part of the FeCl₃ intercalate in carbon to FeCl₂
- oxidizes the FeCl₂ to FeO
- oxidizes part of the FeO to Fe₃O₄

The EDS data indicated the presence of carbon, iron, and chlorine in the sample, but no fluorine. However, the XRD shows the presence of fluorine in the form of FeF₃ crystals. This suggests that most, if not all, fluorine is located at the interior, more than 2 to 3 μm from the sample surface, where the x-ray can reach, but the 25-kV electron beam used for EDS examination cannot.

Oxidation of FeF₂ and FeO to Fe₃O₄ reached completion after 1 hr of heating at 800 °C in nitrogen. Further oxidation was not observed at this low-oxygen condition. On the other hand, the Fe₃O₄ began to be reduced to Fe at 900 °C, when the reducing power of carbon intensified. It is believed that CO (produced by carbon reacting with Fe₃O₄, O₂, or CO₂) was also an important reducing agent in this reaction.

Effects of oxygen.—The quantity of oxygen supplied to reaction (2) appears to have been a key parameter in determining the products. Too little oxygen caused incomplete oxidation, which resulted in evaporation of unreacted iron halides at the reaction temperature and a low iron concentration in the carbon product. With too much oxygen, on the other hand, the carbon host was consumed, and a structurally damaged carbon product resulted. In addition, the oxygen could have completely oxidized the FeXₙ and produced Fe₂O₃.

The oxygen for this reaction was originally thought to have come from water adsorbed by the reactant of reaction (2) (i.e., C(FeXₙ)) when it was temporarily stored in ambient air (ref. 1). However, results from recent experiments indicate that the oxygen supply may depend more on the quartz (SiO₂) sample holder and the quartz tubular reactor and less on the water adsorbed by the samples in air.

In one such recent experiment, a relatively large sample of C(FeXₙ) powder was exposed to ambient air for more than 10 min to allow moisture adsorption; then, together with sections of thin quartz rods, it was placed on a piece of nickel foil and heated to 1100 °C in a quartz reactor containing nitrogen. In this case, even though the powder sample picked up some moisture during the ambient air exposure, the oxygen from all available sources was not sufficient to convert most of the iron halides into iron oxides. Most of the product contained little iron and was not attracted to a regular magnet. Only the small fraction of the sample that was in direct contact with the quartz rods was magnetic.

It is believed that the fluorine emitted from the sample attacked the SiO₂, which released oxygen and initiated the oxidation of some metal halides. Other possible oxygen sources include the diffusion of water vapor from ambient air through the quartz tube reactor at 1000 °C, impurity (0.01 percent) of the “inert” nitrogen environment, or the oxygen and water that remained in the residual air or on the reactor’s inner wall after the nitrogen purging.

When enough oxygen was supplied, carbon could be completely oxidized, Fe₃O₄ could be completely reduced by the CO thus produced, and pure iron would be produced. Figure 2(a) is an SEM micrograph showing iron fibers thus produced by heating sample D (see table I) at 1200 °C in nitrogen. Figure 2(b) is an SEM photo of iron-containing carbon fibers produced by heating sample E (table I) at 1180 °C in nitrogen. This product has an estimated Fe/C atomic ratio of 1:3.6. The oxygen quantity necessary for carbon oxidation was apparently different for the two tests heated at approximately 1200 °C. The reason for such differences cannot be positively identified at this time. However, a possible reason is that, at 1180 to 1200 °C, atmospheric water vapor may diffuse into the quartz reactor at different rates because of different ambient humidity during these two runs.

Location of iron in carbon.—The surface of the fiber sample in figure 2(b), which has an Fe/C atomic ratio of 1:3.6, does not appear to have a large quantity of iron coating. This suggests that the iron particles were located in the fiber interior. To confirm this, one of the fibers shown in figure 2(b) was fractured, and the central 1- by 1-μm region of the fractured cross section was examined by EDS. The results indicated that the central region contained as much iron as the surface region of the fibers. It is not clear whether the iron and/or iron oxide particles were located
between the graphene layers or at the grain boundaries. The XRD does not give clear evidence; it shows large graphite peaks for some of these samples and small graphite peaks for others.

The reactions described in this section can be summarized by the following equations:

\[ C(\text{FeX}_n) \rightarrow_{650 \text{ to } 750 ^\circ C} C(\text{FeF}_2, \text{FeF}_3, \text{FeCl}_3) \]  

where \( \text{FeF}_3 \) is in a recently discovered (see ref. 6) cubic structure, \( \text{FeF}_2 \) is crystalline, and \( \text{FeCl}_3 \) is an intercalate.

\[ C(\text{FeF}_2, \text{FeF}_3, \text{FeCl}_3) \rightarrow_{\text{low } O_2}^{650 \text{ to } 750 ^\circ C} C(\text{FeO}, \text{Fe}_3\text{O}_4) \]  

\[ C(\text{FeO}, \text{Fe}_3\text{O}_4) \rightarrow_{\text{low } O_2}^{750 \text{ to } 850 ^\circ C} C(\text{Fe}_3\text{O}_4) \]  

\[ C(\text{Fe}_3\text{O}_4) \rightarrow_{900 \text{ to } 1200 ^\circ C} C(\text{Fe}) + \text{CO} + \text{CO}_2 \]  

\[ C(\text{Fe}_3\text{O}_4) \rightarrow_{\text{low } O_2}^{1200 ^\circ C} \text{Fe} + \text{CO} + \text{CO}_2 \]  

\[ 2\text{C} + \text{O}_2 \rightarrow 2\text{CO} \]  

\[ 2\text{CO} + \text{O}_2 \rightarrow 2\text{CO}_2 \]  

\[ \text{CO}_2 + \text{C} \rightarrow_{>800 ^\circ C} \text{2CO} \]  

\[ C(\text{Fe}) \rightarrow_{\text{1-atm air}}^{500 ^\circ C} \text{Fe}_2\text{O}_3 + \text{CO}_2 \]  

Oxidation of \( C(\text{FeX}_n) \) in 1-atm Air

It has been shown that at 370 °C in 1-atm air, oxygen reacts with the products of reactions (5) and (6) to form small \( \text{Fe}_2\text{O}_3 \) particles that migrate to the carbon surface (ref. 1). The \( \text{Fe}_2\text{O}_3 \) thus formed was a powder that covered the carbon surface unevenly (ref. 1). This oxidation reaction occurred at an upper limit of below 420 °C; above this, carbon oxidation in air becomes significant (ref. 10). Recent experiments indicated that this reaction occurred at as low as 200 °C for a \( \text{C(iron halide)} \) sample made from a P-75-pitch-based CF0.75.

The preceding phenomenon can be described as follows:

\[ C(\text{FeX}_n) \rightarrow_{\text{1-atm air}}^{\text{200 to } 420 ^\circ C} \text{C} + \text{Fe}_2\text{O}_3 \]
Iron Alloy in or on Carbon

Previous sections described the formation of iron and/or iron oxide particles in or on carbon materials. These materials can be attracted to a magnet. Their magnetic properties have been examined and reported elsewhere (ref. 11). In the research reported herein, experiments were conducted to test if the iron and/or iron oxide particles can be replaced by an iron alloy having higher permeability values. Since nickel-iron alloys (NiFe and Ni₃Fe) are known to have permeability values more than one order of magnitude higher than pure iron (ref. 12), a decision was made to attempt to put a nickel-iron alloy into carbon. Three different approaches were used. They are described in the following paragraphs.

First approach: Reaction between CFₓ and NiCl₂–FeCl₃ mixture.—An attempt was made to form a mixed-metal halide in the carbon lattice and then treat it according to the process described in this report to produce a nickel-iron alloy in carbon. Toward this end, a CF₀.₇₅ sample made from P-75 was treated with a NiCl₂–FeCl₃ mixture for 2 hr. However, the CF₀.₇₅ selectively reacted with the FeCl₃, so the product contained no nickel.

Second approach: Dissolution between iron/iron compound and NiO in carbon.—Another approach was based on the hope that NiO would be able to diffuse into carbon and dissolve or react with either the iron or the iron compounds. In this scenario, the NiO could serve the dual function of supplying the oxygen for CO formation and iron oxide reduction and supplying the nickel for nickel-iron alloy formation. In the experiment, a sample of CF₀.₇ powder made from graphite was treated with FeCl₃ at about 300 °C for 80 min and then at 380 °C for 45 min. The product was mixed with an excess of NiO, placed in sections of small quartz tubes, and heated to 1200 °C for 45 min in a reactor that had been purged by 99.99-percent nitrogen at a high flow rate for 16 hr. The resulting product was magnetic, and its EDS showed the presence of iron, nickel, and carbon (fig. 3). A more detailed EDS analysis indicated that the chemical composition of the product was not uniform: A small part of it had only nickel peaks, but most of it was carbon with nonuniform concentrations of both nickel and iron. The average Ni:Fe atomic ratio for this product was estimated to be 2.8:1. The XRD of the product shows high, sharp nickel peaks (ref. 3) in the proximity of the low, broad nickel-iron peaks. In figure 4 the XRD of this product is compared to an XRD of nickel powder obtained from the same machine. According to the XRD of nickel-iron obtained from the literature (ref. 14), the broad nickel-iron peaks suggest a wide range of Fe:Ni atomic ratios.

This experiment demonstrated that a nickel-iron alloy can be made at 1200 °C from NiO, even though pure NiO has a higher melting point (1990 °C).

Third approach: Dissolution between iron/iron compound and NiCl₂ in carbon.—The third approach was based on the hope that NiCl₂ would either melt (at 1001 °C) or sublime (at 973 °C), diffuse into the carbon, and dissolve the iron or the iron compounds. A C(FeXₙ) sample produced from the reaction between CFₓ and a NiCl₂–FeCl₃ mixture (see First approach) was exposed to an excess of NiCl₂ at 1100 °C in nitrogen for 30 min. A quartz tube was again used as the reactor. The XRD of the resulting product showed large graphite peaks and small nickel-iron peaks (ref. 14). The relatively small peaks suggest a low alloy concentration. This was confirmed by the EDS data, which detected iron and nickel atoms in the outer 2 μm of the carbon fibers. The EDS data, however, also indicated that chlorine was present. A semiquantitative analysis of the EDS data determined that the atomic ratios of Cl, Fe, and Ni were 32, 21, and 47 percent, respectively. The low alloy concentration and the presence of chlorine atoms in the product probably explain why the product was barely attracted to a magnet. These results demonstrate that a nickel-iron alloy can be made at 1100 °C in carbon according to the method just described.

The reactions described in this section can be summarized in the following equations:

\[
\text{C(FeX}_n\text{) + NiO} \quad \xrightarrow{\text{N}_2\text{, }1100\text{ °C}} \quad \text{C(Ni, Ni–Fe alloy)}
\]  

\[
\text{C(FeX}_n\text{) + NiCl}_2 \quad \xrightarrow{\text{N}_2\text{ in quartz tube, }1100\text{ °C}} \quad \text{C(Ni–Fe alloy, Cl)}
\]
CONCLUDING REMARKS

The kinetics of the reaction between FeCl₃ and graphite fluoride (CFₐ₀.₆₈) were examined. Analyses indicated that FeCl₃ quickly entered the carbon structure of CFₐ₀.₆₈ and reacted with the fluorine. This reaction produced carbon with disrupted graphene planes between which crystalline FeF₃ and noncrystalline FeCl₃ were located. Long reaction times between CFₐₓ and FeCl₃ appeared to allow slow graphite intercalation compound (GIC) formation, FeF₃ structural distortion, and FeF₃−FeCl₃ reactions. This resulted in products that had XRD peaks indicating graphite, FeCl₃−GIC, FeCl₃•4H₂O, and FeCl₃•2H₂O.

The products of the CF₀.₆₈−FeXₙ reaction were further heat treated to produce iron-containing carbon materials. When the oxygen supply was kept at the optimum level, the FeXₙ evaporation was kept to a minimum, and the iron halide in or on the carbon was converted to iron oxide. The iron oxide was eventually reduced to iron metal at temperatures higher than 900 °C. During such a heat treatment, NiO or NiCl could be added to the reaction to produce a carbon material containing a nickel-iron alloy, a highly ferromagnetic material.

REFERENCES

TABLE I.—REACTION CONDITIONS AND PRODUCT CHARACTERIZATION FOR FeCl₃-CFo.68 REACTION

<table>
<thead>
<tr>
<th>Sample</th>
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</tr>
<tr>
<td>G</td>
<td>300</td>
<td>5</td>
<td>1.28</td>
<td>---</td>
</tr>
</tbody>
</table>

aRatio estimated by comparing the sample weight before and after treatment at 500 °C air, which converted sample to pure Fe₂O₃.
bCl/Fe ratio estimated by EDS from SEM operated at 25 kV; therefore, only outer 2- to 3-µm depth of sample was examined.
cBecause of short reaction times, length of heatup (sample A = 7 min; sample B = 20 min) may have significant effect on product properties.
dSample post-heated in nitrogen at 350 °C for 7 hr.
eSample obtained from reaction between FeCl₃ and precursor of CF₀.68 (i.e., P-100 carbon fibers). It was post-heated in nitrogen at 350 °C for 0.35 hours.

TABLE II.—X-RAY DIFFRACTION DATA FOR THE PRODUCTS OF FeCl₃-CFo.68 REACTION

<table>
<thead>
<tr>
<th>Standard pure rhombohedral FeF₃</th>
<th>Reaction product 290 °C, 30 min.</th>
<th>Reaction product 285 °C, 28 hr</th>
</tr>
</thead>
<tbody>
<tr>
<td>Interatomic spacing, Å</td>
<td>Relative intensity, percent</td>
<td>Interatomic spacing, Å</td>
</tr>
<tr>
<td>3.731</td>
<td>100</td>
<td>3.725</td>
</tr>
<tr>
<td>2.678</td>
<td>15</td>
<td>2.675</td>
</tr>
<tr>
<td>2.602</td>
<td>7</td>
<td>2.601</td>
</tr>
<tr>
<td>2.244</td>
<td>14</td>
<td>2.243</td>
</tr>
<tr>
<td>2.133</td>
<td>2</td>
<td>---</td>
</tr>
<tr>
<td>1.866</td>
<td>21</td>
<td>1.869</td>
</tr>
<tr>
<td>1.689</td>
<td>21</td>
<td>1.691</td>
</tr>
<tr>
<td>1.649</td>
<td>10</td>
<td>1.649</td>
</tr>
<tr>
<td>1.562</td>
<td>3</td>
<td>---</td>
</tr>
<tr>
<td>1.516</td>
<td>6</td>
<td>1.519</td>
</tr>
<tr>
<td>1.501</td>
<td>5</td>
<td>---</td>
</tr>
<tr>
<td>1.339</td>
<td>5</td>
<td>1.341</td>
</tr>
<tr>
<td>1.300</td>
<td>2</td>
<td>---</td>
</tr>
<tr>
<td>1.278</td>
<td>3</td>
<td>---</td>
</tr>
<tr>
<td>1.243</td>
<td>2</td>
<td>1.247</td>
</tr>
<tr>
<td>1.228</td>
<td>5</td>
<td>1.229</td>
</tr>
</tbody>
</table>

aIncludes all FeF₃ peaks with relative intensity values ≥ 2 percent.
bIncludes all peaks that can be observed from the diffractogram for the product.
cGraphite peak.
### TABLE III—PRODUCTS OF CF0.68 FeCl3 REACTIONS DESCRIBED IN TABLE I AFTER SUBSEQUENT FINAL HEATING

[Heated in a quartz tube containing 99.99-percent nitrogen.]

<table>
<thead>
<tr>
<th>Reactants from reaction—</th>
<th>Time to each final temperature, hr</th>
<th>Final temperature, °C</th>
<th>Heating time, hr</th>
<th>Surface observed by SEM</th>
<th>X-ray diffraction peaks of heated products</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>Graphite Fe FeO Fe3O4 Others</td>
</tr>
<tr>
<td>D</td>
<td>0.75</td>
<td>650 then 750</td>
<td>0.5</td>
<td>Clean</td>
<td>Large None Small Small Cubic FeF3 FeF2</td>
</tr>
<tr>
<td>D</td>
<td>2.25</td>
<td>850</td>
<td>1</td>
<td>Big particles</td>
<td>Small None None Large None</td>
</tr>
<tr>
<td>D</td>
<td>3.25</td>
<td>900</td>
<td>3</td>
<td>Heavy coating</td>
<td>Large Small None None None</td>
</tr>
<tr>
<td>D</td>
<td>1.20</td>
<td>950</td>
<td>1.23</td>
<td>Clean</td>
<td>Small Large None None None</td>
</tr>
<tr>
<td>D</td>
<td>2.10</td>
<td>1200</td>
<td>.67</td>
<td>(b)</td>
<td>Very small or none Large None None None</td>
</tr>
<tr>
<td>E</td>
<td>1.8</td>
<td>1180</td>
<td>.33</td>
<td>Small particles</td>
<td>Medium Large None None None</td>
</tr>
</tbody>
</table>

*Reactants are products of CF0.68-FeCl3 reactions described in table II.

*After 1200 °C heating, this sample became mostly fibers of pure α iron and some carbon powder with high iron content.
Figure 1.—Iron-containing carbon materials on magnets.
Figure 2.—Scanning electron micrograph of fibers from reaction of FeCl$_3$-CF$_6$O$_{.68}$ subsequently heated to 1200 °C. (a) Iron produced by reduction of iron oxides in presence of carbon. (b) Iron particles in carbon fibers produced when carbon is not completely consumed in reduction of iron oxide.
Figure 3.—Product obtained from reaction of CF$_{0.7}$ powder and FeCl$_3$ at 300 to 380 °C, followed by heating to 1200 °C with NiO in a quartz tube containing nitrogen. (a) Scanning electron micrograph. (b) Energy-dispersive spectrum.
Figure 4.—X-ray diffraction data of product obtained from reaction of CF$_{0.7}$ powder and FeCl$_3$ at 300 to 380 °C, followed by heating to 1200 °C with NiO in a quartz tube containing nitrogen. (a) X-ray count in linear scale. (b) Comparison between this product and nickel powder; x-ray count in log scale.
# Fabrication of Iron-Containing Carbon Materials From Graphite Fluoride

**Title:** Fabrication of Iron-Containing Carbon Materials From Graphite Fluoride

**Authors:** Ching-cheh Hung

**Performing Organization:** National Aeronautics and Space Administration

**Report Date:** April 1996

**Report Type:** Technical Memorandum

**Funding Numbers:** WU-233-1A-1E

**SPONSORING AGENCY:** NASA TM-107133

**Subject Terms:** Magnetic particles in carbon; Graphite fluoride; Intercalation; Disrupted graphene layers; Reactions in carbon host; Iron particles in carbon

**Abstract:**

Carbon materials containing iron alloy, iron metal, iron oxide or iron halide were fabricated. Typical samples of these metals were estimated to contain 1 iron atom per 3.5 to 5 carbon atoms. Those carbon materials containing iron alloy, iron metal, and/or Fe$_3$O$_4$ were magnetic. The kinetics of the fabrication process were studied by exposing graphite fluoride (CF$_{0.68}$) to FeCl$_3$ over a 280 to 420 °C temperature range. Between 280 and 295 °C, FeCl$_3$ quickly entered the structure of CF$_{0.68}$, broke the carbon-fluorine bonds, and within 10 to 30 min, completely converted it to carbon made up of graphite planes between which particles of crystalline FeF$_3$ and noncrystalline FeCl$_3$ were located. Longer reaction times (e.g., 28 hr) or higher reaction temperatures (e.g., 420 °C) produced materials containing graphite, a FeCl$_3$-graphite intercalation compound, FeCl$_2$$\cdot$4H$_2$O, and FeCl$_2$$\cdot$2H$_2$O. These products were further heat treated to produce iron-containing carbon materials. When the heating temperature was kept in the 750 to 850 °C range, and the oxygen supply was kept at the optimum level, the iron halides in the carbon structure were converted to iron oxides. Raising the heat to temperatures higher than 900 °C reduced such iron oxides to iron metal. The kinetics of these reactions were used to suggest processes for fabricating carbon materials containing iron alloy. Such processes were then tested experimentally. In one of the successful trial runs, commercially purchased CF$_{0.7}$ powder was used as the reactant, and NiO was added during the final heating to 1200 °C as a source of both nickel and oxygen. The product thus obtained was magnetic and was confirmed to be a nickel-iron alloy in carbon.