ABSTRACT OF THE INVENTION

PRECISION THICKNESS VARIATION MAPPING VIA ONE-
TRANSDUCER ULTRASONIC HIGH RESOLUTION

PROFILOMETRY FOR SAMPLE WITH IRREGULAR OR ROUGH
SURFACE

An apparatus and method for determination of sample thickness and surface depression utilizing ultrasonic pulses. The sample is held in a predetermined position by a support member having a reference surface. Ultrasonic pulses travel through a medium of known velocity propagation and reflect off the reference surface and a sample surface. Time of flight data of surface echoes are converted to distances between sample surfaces to obtain computer-generated thickness profiles and surface mappings.
NOTICE

The invention disclosed in this document resulted from research in aeronautical and space activities performed under programs of the National Aeronautics and Space Administration. The invention is owned by NASA and is, therefore, available for licensing in accordance with the NASA Patent Licensing Regulation (14 Code of Federal Regulations 1245.2).

To encourage commercial utilization of NASA-owned inventions, it is NASA policy to grant licenses to commercial concerns. Although NASA encourages non-exclusive licensing to promote competition and achieve the widest possible utilization, NASA will consider the granting of a limited exclusive license, pursuant to the NASA Patent Licensing Regulations, when such a license will provide the necessary incentive to the licensee to achieve early practical application of the invention.

Address inquiries and all applications for license for this invention to NASA Lewis Research Center, Patent Counsel, Mail Code Le-LAW, 21000 Brookpark Road, Cleveland, OH 44135-3195. Approved NASA forms for application for non-exclusive or exclusive license are available from the above address.

Serial Number 08/641,132

Filing Date April 22, 1996

NASA/LeRC
Precision Thickness Variation Mapping via One-Transducer Ultrasonic High Resolution Profilometry for Sample with Irregular or Rough Surface

Background of the Invention

1. Field of Invention

This invention pertains to the art of methods and apparatuses for mapping profiles of irregularly surfaced samples of various materials, and more specifically to methods and apparatuses for thickness variation mapping using ultrasonic high-resolution profilometry.

2. Description of the Related Art

Samples that have rough or irregular surfaces can be difficult at times to characterize for thickness variation. One possible method is known as diamond-tipped profilometry. This method, however, requires contact with the sample which can cause undesirable alterations to the sample surface if further characterization is required. Another profilometry method
potentially useable for precision thickness measuring uses lasers. However, this method requires specularly reflecting surfaces for accurate measurements.

Ultrasonic methods are also currently available for thickness measurements. Such methods require the ultrasonic energy to travel through the mass of the sample. However, because of the high frequencies required for precise, high-resolution characterization, penetration of the ultrasonic energy can be very difficult or even impossible to obtain. Further, in the latter method, it is generally required that the ultrasonic velocity in the material be known and assumed to be constant. Unless the material is perfectly homogenous, the necessary assumption gives less than desirable results.

Another known ultrasonic method for thickness measurement requires two transducers, a contact measurement, and volumetric ultrasonic travel. The method is significantly more complicated to implement than the method disclosed herein.

Summary of the Invention

In accordance with the practice of the present invention, there is provided a method and apparatus for precision thickness variation mapping utilizing non-contact, ultrasonic means.
More particularly, in accordance with the present invention, the method employs a single transducer to obtain time delay data for ultrasonic pulses reflected from a sample surface.

According to one aspect of the present invention, a method for determining the perpendicular distance between first and second surfaces of a sample comprises the steps of:

(a) transmitting a reference ultrasonic signal through an ultrasonic medium having a known velocity of propagation, \( V_{\text{med}} \), to a reference surface a constant distance from a transducer able to send and receive ultrasonic signals, said second surface of said sample interfacing with said reference surface whereby said second surface and said reference surface are the same constant distance from said transducer;

(b) receiving a reference ultrasonic echo from said reference surface;

(c) transmitting a first ultrasonic signal through said medium to a first location on said first surface;

(d) receiving a first ultrasonic echo with said transducer from said first location;

(e) recording time delay data from the transmission of said signals to the reception of said echoes; and,

(f) calculating said perpendicular distance from said time delay data and said ultrasonic velocity.
According to another aspect of the present invention, a method for obtaining a thickness profile between a first surface and an opposite planar second surface of a sample comprises the steps of:

(a) positioning said sample on a support member within an immersion tank, said support member having a uniform thickness and a planar reference surface so that said second surface interfaces with said reference surface of a said support member in a first plane, the immersion tank containing an ultrasonic medium of known ultrasonic velocity;

(b) scanning said reference surface and a plurality of locations on said first surface with ultrasonic pulses transmitted from a transducer maintained in a second plane a constant distance from said first plane, said ultrasonic pulses travelling through said medium, each of said locations being associated with a pair of x-y coordinates;

(c) receiving echoes of said ultrasonic pulses off said reference surface and said first surface in the form of time delay data;

(d) converting said time delay data to thickness map data for each echo received from said plurality of locations on said first surface; and,

(e) using said thickness map data to generate a thickness profile of said sample.
According to another aspect of the invention, an apparatus for measuring a plurality of perpendicular distances between first and second opposite surfaces of a sample comprises:

- a support member having a flat reference surface lying in a first plane, said second surface of said sample interfacing with said reference surface so that said second surface lies in said second plane;
- scanning means for scanning said reference surface and said first surface by moving an ultrasonic transducer in a second plane, said second plane being a constant distance from said first plane, said transducer being capable of emitting ultrasonic pulses at a predetermined frequency and receiving ultrasonic echoes;
- an immersion fluid of known velocity of propagation disposed between said transducer and said support member;
- means for recording time delay data between the emission of an ultrasonic pulse and the reception of an echo; and,
- means for converting said time delay data into said perpendicular distances.

One advantage of the present invention is amount of data in a short length of time. For example, about 10 times the data can be obtained in 1/100th the time over diamond-tip profilometry.

Another advantage of the present invention is the elimination of sample contact with the measuring device.
Another advantage of the present invention is the elimination of the need for ultrasonic penetration of the sample thereby eliminating the need to know or assume the speed of sound therethrough.

Another advantage of the present invention is the precision measurement of the thickness profile obtained by the method disclosed herein.

Another advantage of the present invention is the ability to obtain surface profiling over the entire sample.

Still other benefits and advantages of the invention will become apparent to those skilled in the art to which it pertains upon a reading and understanding of the following detailed specification.

**Brief Description of the Drawings**

The invention may take physical form in certain parts and arrangement of parts, a preferred embodiment of which will be described in detail in this specification and illustrated in the accompanying drawings which form a part hereof and wherein:
Figure 1 is a perspective view of an assembly for ultrasonic profilometry for thickness variation determination according to the invention.

Figure 2 is a front view of the assembly of Figure 1.

Figure 3 is a representation of a time location of an ultrasonic reflection off the upper surface of the support material.

Figure 4 is a representation of a time location of an ultrasonic reflection off the upper surface of the sample at any given location, \((x,y)\).

Figure 5 is an ultrasonic thickness profile of a sample before burning obtained by the method of the present invention.

Figure 6 is an ultrasonic thickness profile obtained by the method of the present invention after burning the sample of Figure 5.

**Description of the Preferred Embodiment**

Referring now to the drawings wherein the showings are for purposes of illustrating a preferred embodiment of the
invention only and not for purposes of limiting the same, Figure 1 shows a perspective view of an assembly for ultrasonic profilometry for thickness variation determination, hereinafter assembly 10. Generally, assembly 10 includes a tank 14 for holding an immersion medium 18. The sample 20 rests on a support member 24 within medium 18. A transducer 30 sends an ultrasonic signal through the medium 18 which reflects off sample 20. The return signal is received by the transducer 30. The lapse of time from signal generation to echo reception is related to the distance traveled by the signal. The method of the present invention further requires an ultrasonic scan system and an oscilloscope with accurate time base and time synthesis capability (the ultrasonic scan system and oscilloscope are not shown).

With reference to Figure 2, support member 24 comprises a uniform thickness and a flat upper surface 34 which lies in a first x-y plane. Transducer 30 is moveable in a second x-y plane a constant distance ZZ from the upper surface 34 of support member 24. Sample 20 includes a flat lower surface 36 which is flush against upper surface 34 of the support member 24. When an ultrasonic scan is made over sample 20, at any location (x,y) on the upper surface 40 of the sample 20, the distance between the upper surface 40 and the transducer is given by, d_{x,y}. The thickness of the sample at location (x,y) is then the difference between ZZ and d_{x,y}:
Thickness_{x,y} = ZZ - d_{x,y}

It is readily apparent, that Thickness_{x,y} is a measure of the perpendicular distance from upper surface 40 to lower surface 36 at the x-y location.

The distance, ZZ, can be determined by:

$$ZZ = \frac{V_{\text{med}} \cdot \Delta t_{zz}}{2}$$

where water is the immersion medium, $V_{\text{med}}$ is the velocity of sound in water, and:

$$\Delta t_{zz} = t_{SM} - t_i$$

where $t_{SM}$ is the time location of the peak of the first ultrasonic reflection off the upper surface 34 of support member 24 and $t_i$ is the time location of the pulse initially leaving the transducer 30. Figure 3 shows a representation of a time location peak 42 as might be recorded on an oscilloscope.

In like manner, distance $d_{x,y}$ can be determined by:

$$d_{x,y} = \frac{V_{\text{med}} \cdot \Delta t_{d}}{2}$$

where:

$$\Delta t_{d} = t_{x,y} - t_i$$

corresponding to the time location peak 46 as shown in Figure 4.
The thickness of sample 20 at each \((x,y)\) location can thus be determined by inserting equations (2) and (4) into equation (1):

\[
\text{Thickness}_{x,y} = \left[ \frac{V_{\text{med}} \cdot \Delta t_{zz}}{2} \right] - \left[ \frac{V_{\text{med}} \cdot \Delta t_{d}}{2} \right]
\]

and inserting equations (3) and (5) into equation (6):

\[
\text{Thickness}_{x,y} = \left[ \frac{V_{\text{med}} \cdot (t_{SM} - t_{i})}{2} \right] - \left[ \frac{V_{\text{med}} \cdot (t_{x,y} - t_{i})}{2} \right]
\]

Canceling terms and factoring equation (7) gives:

\[
\text{Thickness}_{x,y} = \frac{V_{\text{med}}}{2} \cdot (t_{SM} - t_{i})
\]

The surface depression at any \(x,y\) location can be obtained in like manner:

\[
\Delta Z_{x,y} = \frac{V_{\text{med}}}{2} \cdot (t_{x,y} - t_{\text{min}})
\]

where \(t_{\text{min}}\) is the echo time corresponding to the highest surface position of upper surface 40.

Because \(V_{\text{med}}\) is greatly temperature dependent, the medium temperature should be measured accurately.
Transducer focal spot size determines the sample area of the sample surface 40\textsuperscript{\circ} at each (x,y) location. Relationships exist between focal spot size, transducer frequency and focal length for transducers. In one preferred embodiment of the present invention, it has been found that using a 100 MHz center frequency focused transducer with a focal length of 0.5 inches (1.27 cm) results in a focal spot size of 25-50 \textmu m. Another preferred embodiment of the invention utilizes a broad band focused 50 MHz transducer with a focal length of 0.5 inches (1.27 cm), with a focal spot size of 50-100 \textmu m.

Resolution of thickness variation is a function of how finely time variation can be resolved and is dependent on analog-to-digital sampling rate and the number of bits available to which a time extent can be mapped.

Although the preferred embodiment of the present invention utilizes water as the immersion medium, other media may be employed as long as the velocity of sound therein is precisely determined.

In addition to the velocity of sound in the immersion medium, it is important to precisely measure $t_{x,y}$ and $t_{SM}$. The system should also be free from external vibration and preferably include a high digital sampling rate (1 GHz) of the ultrasonic A/D converter.
The following example of the implementation of the inventive method is given for clarification and is not intended to limit the invention.

EXAMPLE

A map over a sample of ultrasonic time delay data was obtained using a commercially available ultrasonic scan system manufactured by Sonix, Inc. A broadband focused 50 MHz transducer with focal length = 1.27 cm (0.5 in.), focal spot size ~ 50-100 μm and 1 GHz analog-to-digital sampling rate were used. Water temperature was measured and maintained at 69°F. Gate length was set to cover the entire time extent corresponding to the thickness variation being tracked. A computer program converted the time delay data to thickness map data.

Specifically, the equation used to obtain Thickness_{x,y} from time delay data is:

\[
\text{Thickness}_{x,y} (\text{mm}) = \frac{V_{\text{med}} (\text{mm/μsec})}{2} \times \left( T_{\text{SM}} - (\text{TOF}_{\text{start}} + (\text{TOF}_{\text{increment}})(\text{graylevel}_{x,y})) \right)
\]

where:

\[
\text{TOF}_{\text{increment}} = \left( \frac{1}{\text{sampling rate}} \right) \times \frac{\text{gate length}(\text{points})}{(248 \text{ gray levels})}
\]

where:
1\
\text{sampling rate} = \frac{\text{gate length(\mu sec)}}{\text{gate length(points)}}

According to present Sonix convention, \( TOF_{\text{increment}} \) and \( TOF_{\text{start}} \) have units of microseconds and are obtained from the header of the Sonix image file after converting to ascii text file. \( TOF_{\text{start}} \) corresponds to the right end position of the gate. Graylevel \( x,y \) which is the gray level value obtained at scan location \( x,y \) and is a value between 0 and 248 (8 bits of TOF resolution), increases as TOF decreases. The 248 gray levels represent \( \sim \) 8 bits of resolution mapping available in the commercial scan system. As is readily apparent, ultrasonic digital system design and experimental variables have significant effects on the resolution of thickness variations. These variable include: transducer frequency, transducer spot size, sampling rate, gate length, maximum sampling rate, and number of available gray levels (or bits = \( \log_2 \) gray levels).

The resulting data in the form of \( x \) (position), \( y \) (position), and \( z \) (thickness) was imported into a 3-dimensional plotting program. Two such programs to plot thickness data include TableCurve 3D from Jandel Scientific and PVWave from Precision Visuals. Figures 5 and 6 show representations of 3-dimensional computer generated sample thickness profiles before and after the sample was burned. In Figure 5, the representation 50 indicates the sample thickness profile before burning and in
Figure 6 representation 52 indicates the sample thickness after burning.

With reference again to Figure 2, a method for obtaining a surface depression mapping will now be described. The minimum distance, $d_{\text{min}}$, from the upper surface 40 of the sample to the second x-y plane corresponds to the $(x,y)$ location where the ultrasonic echo yields a minimum value, $t_{\text{min}}$. The difference between $d_{x,y}$ and $d_{\text{min}}$ yields the surface depression $\Delta Z_{x,y}$ at any location $(x,y)$. With the Sonix, Inc. system a surface depression mapping may be obtained by using the following relationship:

$$\Delta Z_{x,y} (\text{mm}) = \frac{V_{\text{med}} (\text{mm}/\mu \text{sec})}{2} \ast (\text{TOF}_{\text{increment}}) \ast (\text{graylevel}_{x,y} - \text{graylevel}_{\text{max}})$$

Graylevel$_{\text{max}}$ is the maximum gray level value in the file of data values obtained for the scan.

The preferred embodiments have been described, hereinabove. It will be apparent to those skilled in the art that the above methods may incorporate changes and modifications without departing from the general scope of this invention. It is intended to include all such modifications and alterations in so far as they come within the scope of the appended claims or the equivalents thereof.
Having thus described the invention, it is now claimed:
FIG-3

FIG-4
Ultrasound Thickness Profile of Unburned Sample